

830595

DUPONT OF CANADA
BAKER MINE

ORE RESERVE REMAINING

AUGUST 31st

1983

J. PAXTON, GEOLOGIST

In the following discussion the ore is divided into three categories

PROBABLE ORE - On which firm plans can be made

POSSIBLE ORE - For which allowance must be made in planning

INDICATED ORE - On which plans can be changed if further test work puts it in a higher category

The relationship between these categories and their definition is shown in the following diagram

	POSSIBLE ORE	INDICATED ORE	
POSSIBLE ORE	① Sampling adequate to predict ore grade and tons with confidence ② Possible major mining problems	① Sampling indicates ore grade, but is inadequate to predict tons and grade with confidence ② Possible major mining problems.	INDICATED ORE
PROBABLE ORE	① Sampling adequate to predict ore grade and tons with confidence ② No major mining problems foreseen	① Sampling indicates ore grade, but is inadequate to predict tons and grade with confidence ② No major mining problems foreseen	POSSIBLE ORE
	PROBABLE ORE	POSSIBLE ORE	

BAKER MINE

ESTIMATED ORE REMAINING AUGUST 31st 1983

		<u>TONS</u>	<u>Au</u>	<u>Ag</u>	<u>Auoz</u>	<u>Ag oz</u>
<u>PROBABLE ORE</u>						
BLOCK	<u>I</u>	2600	1.30	15.4	3380	40040
"	<u>V</u>	345	.41	3.4	141	1186
"	<u>VI</u>	<u>260</u>	<u>.47</u>	<u>5.5</u>	<u>122</u>	<u>1430</u>
		3205	1.14	13.3	3643	42656

<u>POSSIBLE ORE</u>						
BLOCK	<u>III</u>	650	.96	26.0	624	16900
"	<u>IV</u>	1461	.50	9.5	727	13823
"	<u>VII</u>	554	.45	3.6	249	1994
#8 STOCKPILE		<u>793</u>	<u>.40</u>	<u>12.1</u>	<u>317</u>	<u>9595</u>
		3458	.55	12.2	1917	42312

<u>INDICATED ORE</u>						
BLOCK	<u>II</u>	333	1.35	17.4	449	5794
"	<u>VIII</u>	167	.20	1.3	33	217
	<u>IX</u>	<u>4500</u>	<u>.38</u>	<u>6.6</u>	<u>1710</u>	<u>29700</u>
		5000	.44	7.1	2192	35711

<u>SUB ORE</u>						
#9 STOCKPILE		2501	.16	3.6	411	8993
<u>TOTAL</u>		<u>14164</u>	<u>.58</u>	<u>9.1</u>	<u>8163</u>	<u>129672</u>

This compares the estimate of June 30
of 17217 .45 9.1 7898 156868

ORE BLOCKS

I - 55-52 STOPE UNDERGROUND SALVAGE - PROBABLE
MAIN VEIN

GRADE

Back Sampling	<u>W</u>	<u>Au</u>	<u>Ag</u>	<u>WxAu</u>	<u>WxAg</u>
	5	.05	1.7	.25	8.5
	5	.06	2.5	.30	12.5
	5	.30	13.8	1.50	69.0
	5	.07	.4	.35	2.0
	5	.01	.2	.05	1.0
	3	.04	2.4	.12	7.2
	3	.40	6.5	1.20	19.5
	5	.38	9.9	1.90	49.5
	4	.37	15.7	1.48	62.8
	4	1.90	9.4	7.60	37.6
	4	.73	5.8	2.92	23.2
	7	1.14	17.0	7.98	119.0
	4	.73	5.8	2.92	23.2
	<u>59</u>				

Diamond drill hole	28	3.20	33.8	89.60	946.4
.U-81-8	<u>5.5</u>	.45	8.5	<u>2.47</u>	<u>46.7</u>
	92.5			120.64	1427.8
		1.30 Au	15.4 Ag		

VOLUME

Estimated mean width = 13'
 " area = $30 \times 30 = 900$
 $20 \times 75 = 1500$
2400

$$V = 2400 \times 13 = 31,200 \text{ ft}^3$$

$$T = \frac{31,200}{12} = 2,600$$

NOTE: Mapping of the back shows the vein to be split, with a minor 5' vein in the hang wall. The above calculation refers to the main portion of the vein

II - 55-52 STOPE UNDERGROUND SALVAGE - INDICATED
HANG WALL SPLIT VEIN

GRADE

TEST HOLE	<u>W</u>	<u>Au</u>	<u>Ag</u>	<u>WxAu</u>	<u>WxAg</u>
	4	2.40	29.9		
	4	.31	5.0		
Mean =	1.35		17.4		

VOLUME

5' wide x 46' long x 20' high = 4000

$\frac{4000}{12} = 333 \text{ Tons}$

333 Tons @ 1.35 Au 17.4 Ag

III - 55-54 STOPE CROWN PILLAR - POSSIBLE

GRADE	<u>W</u>	<u>Au</u>	<u>Ag</u>	<u>WxAu</u>	<u>WxAg</u>
DDH C-79-15	12	1.62	1.54		

BACK Samples

<u>W</u>	<u>Au</u>	<u>Ag</u>	<u>WxAu</u>	<u>WxAg</u>	<u>W</u>	<u>Au</u>	<u>Ag</u>	<u>WxAu</u>	<u>WxAg</u>
5	.10	2.7	.5	13	6.5	.24	5	1.56	33
5.5	.24	6.7	1.3	38	4	.79	16	3.16	64
8.0	.22	6.4	1.8	51	7	1.82	37	12.74	259
9.0	.06	1.6	.5	14	6.5	.43	9	2.79	58
15.0	2.40	68.0	36.0	1020	6.0	.06	1	.36	6
11.5	2.34	6.0	26.9	759	113	.98	26	110.3	2956
19.5	1.15	32.0	22.5	632					
9.5	.02	1.0	.2	9					

VOLUME

MEAN W = $\frac{113}{13} = 8.7$

650 Tons @ 0.96 Au 26.0 Ag

L = 60

V = 8.7 x 60 x 15

H = 15

= $\frac{7830}{12} = 650 \text{ Tons}$

IV 54-51 STOPE CROWN PILLAR - POSSIBLE

GRADE

Back Sampling	W	Au	Ag	WxAu	WxAg
<u>IV a</u>	8.0	.04	.8	.32	6.4
	9.5	.36	3.8	3.42	36.1
	10.5	.31	5.6	3.25	58.8
	12.0	.15	1.1	1.80	13.2
	11.0	.05	1.4	.55	15.4
	11.0	.48	2.1	5.28	23.1
	<u>8.0</u>	<u>.16</u>	<u>2.2</u>	<u>1.28</u>	<u>17.6</u>
	70.0	.23	2.4	15.90	170.6

<u>IV b</u>	6.0	1.21	28	7.26	168
	7.0	.29	13	2.03	91
	8.5	.39	12	3.31	102
	10.0	.17	3	1.70	30
	12.0	.31	13	3.72	156
	11.5	.56	13	6.44	149
	12.0	1.54	17	18.48	204
	<u>11.5</u>	<u>.27</u>	<u>3</u>	<u>3.10</u>	<u>34</u>
	78.5	.59	11.9	46.04	934

VOLUME

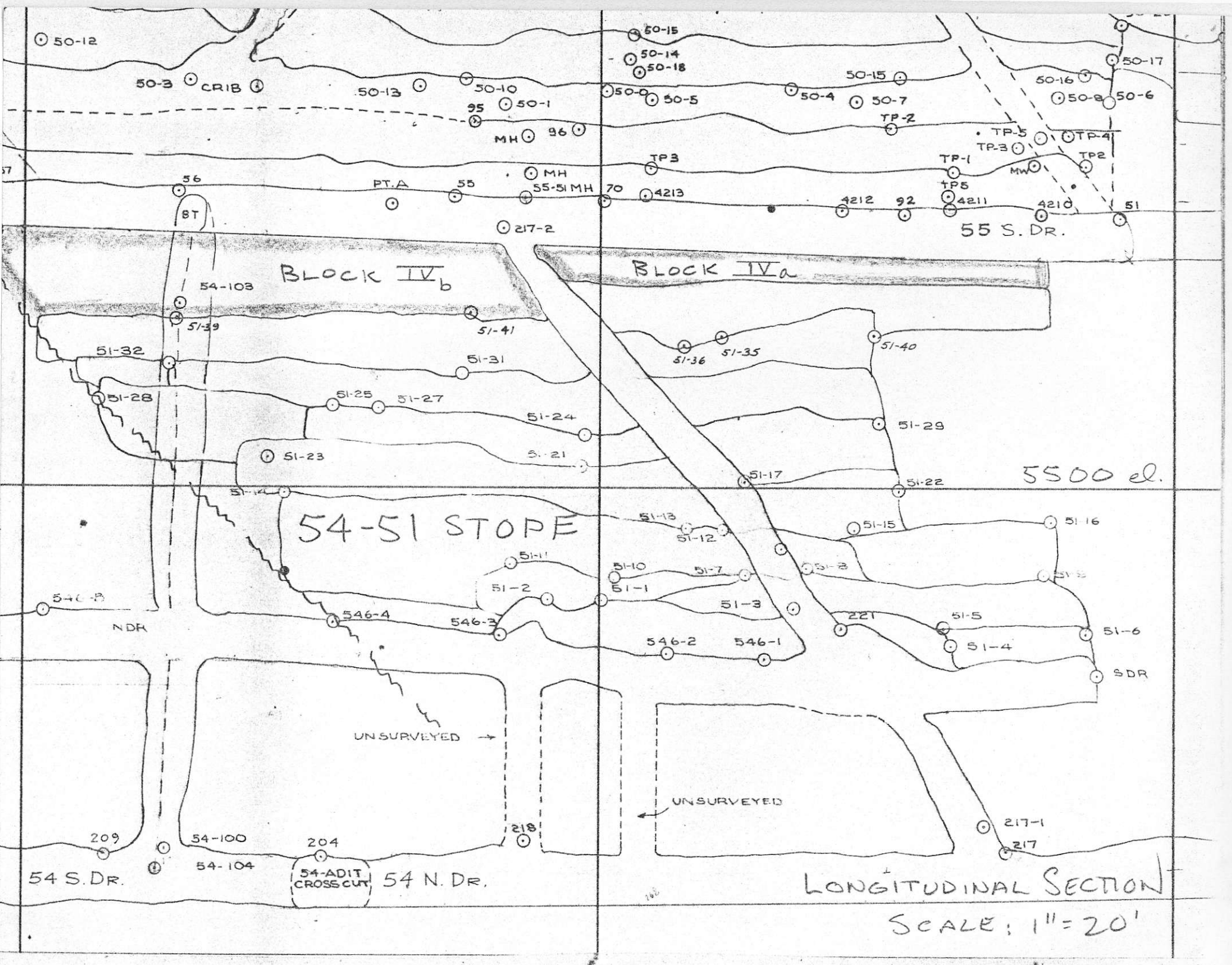
IV a
 $V = (W=10.0) \times (L=90) \times (H=5) = 4500$

Tons = $\frac{4500}{12} = 375$

IV b
 $V = (W=9.8) \times (L=95) \times (H=14) = 13034$

Tons = $\frac{13034}{12} = 1086$

	Tons	Au	Ag	Au oz	Ag oz
<u>IV a</u>	375	.23	2.4	86.2	900
<u>IV b</u>	1086	.59	11.9	640.7	12923
<u>IV</u>	1461	.50	9.5	726.9	13823



V - SS-SO B STOPE - PROBABLE

Grade	w	Au	Ag	w x Au	w x Ag
Back sample	7	.31	1.89		

Volume $5 \times 8 \times 10 = 400$

Tons = $\frac{400}{12} = 33$

33 tons @ .31 Au 1.9 Ag

Vb GRADE

Grade	w	Au	Ag	w x Au	w x Ag
Back sample	1.0	4.79	18.0	4.79	18.0
	7.0	0	0	0	0
	.6	.05	.6	.03	.36
	7.4	0	0	0	0
	1.0	.02	.3	.02	.3
	6.0	0	0	0	0
	1.0	.02	.2	.02	.2
	6.0	0	0	0	0
	2.0	6.49	64.9	12.98	129.8
	6.0	0	0	0	0
	2.3	1.12	13.4	2.58	30.8
	5.7	0	0	0	0
	3.0	1.07	9.7	3.21	29.1
	4.0	0	0	0	0
	1.0	1.26	9.1	1.26	9.1
	6.0	0	0	0	0
	<u>60</u>	<u>14.82</u>	<u>116.2</u>	<u>24.89</u>	<u>217.7</u>

VOLUME

= $50 \times 7.5 \times 10$

= 3750

Tons = $\frac{3750}{12} = 312$

@ 0.42 Au 3.6 Ag

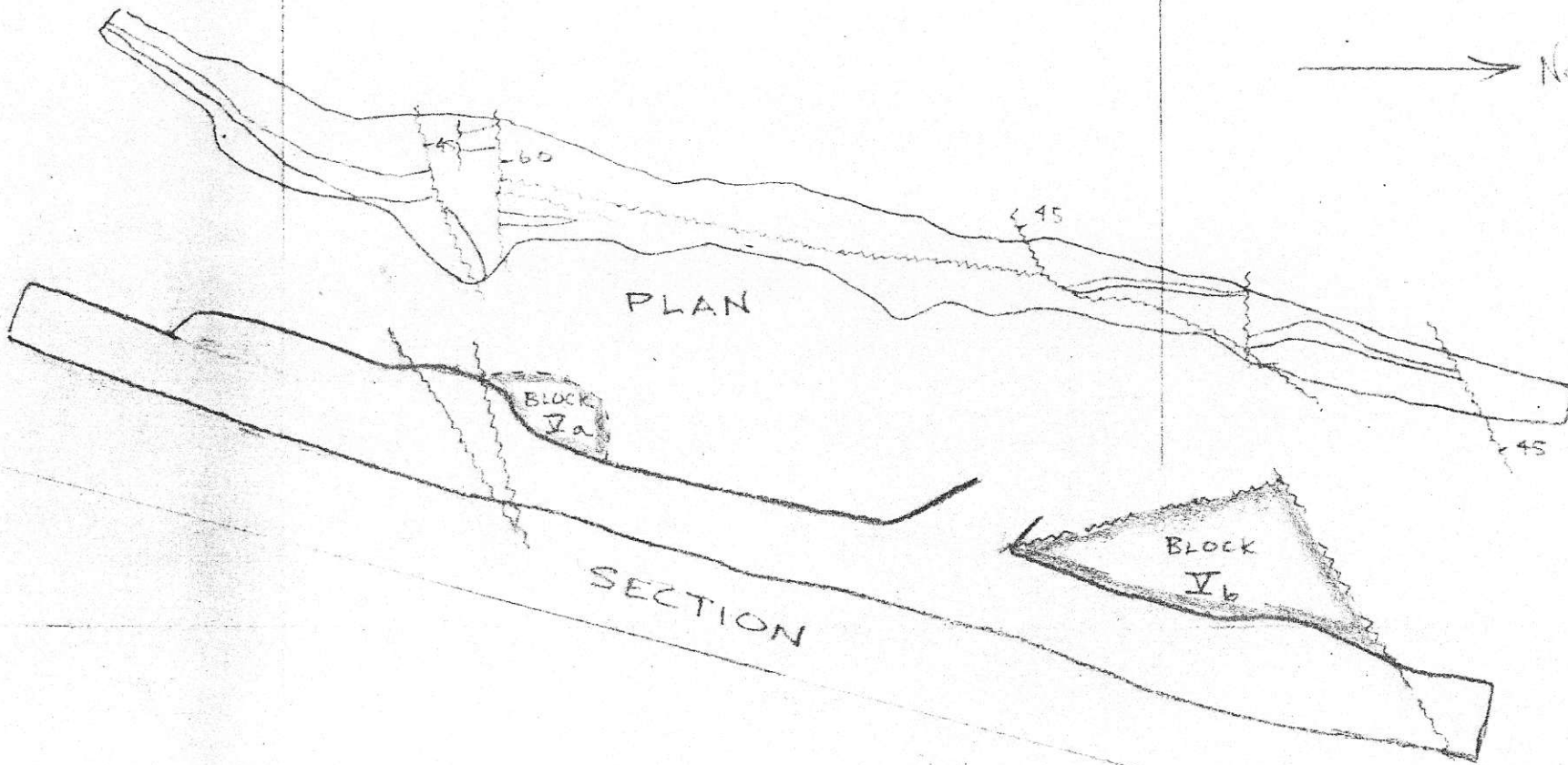
Au = .42 Ag = 3.6

	Tons	Au	Ag	Au oz	Ag oz
	33	.31	1.9	10.2	63
	312	.42	3.6	131.0	1123
<u>BLOCK V</u>	<u>345</u>	<u>.41</u>	<u>3.4</u>	<u>141.2</u>	<u>1186</u>

7+00 E

45+00 N

46+00 N



5560 d

55-50 R SLOPE

AUG 31/83

SCALE 1"=20'

VI 55-50 B DRIFT BACK - PROBABLE

An isolated section of the B vein of ore grade exists in the back of 55-50 B DRIFT between 51+35 n and 51+60 n.

Grade

Back Sample	<u>W</u>	<u>Au</u>	<u>Ag</u>	<u>W x Au</u>	<u>W x Ag</u>
	0.6	.47	15	.28	.9
Diluted to 5' min mining width	4.4	0	0	0	0
	0.9	8.14	110.5	7.33	99.9
	4.1	0	0	0	0
	1.5	.87	5.4	1.30	8.1
	3.5	0	0	0	0
	2.2	.27	1.0	.59	2.2
	<u>2.8</u>	<u>0</u>	<u>0</u>	<u>0</u>	<u>0</u>
Volume	20.0	.47	5.5	9.5	111.1

$$V = (W=5.0) \times (L=25) \times (H=25) = 3125$$

$$\text{Tons} = \frac{3125}{12} = 260$$

260 tons @ 0.47 Au 5.5 Ag

BLOCK VII 54 DRIFT SOUTH BACK - POSSIBLE
49+40m to 49+80m

GRADE

Face samples	W	Au	Ag	Wx Au	Wx Ag
10	.13	.6	1.3	6	
4	1.90	3.0	7.6	12	
6	0	0	0	0	
7	.16	.8	1.1	6	
5.5	2.50	6.2	13.7	34	
4.5	0	0	0	0	
7.5	.31	4.9	2.3	37	
5.5	.63	10.6	3.5	58	
4.5	0	0	0	0	
3.0	.14	1.4	.4	4	
5.0	.04	1.0	.2	5	
3.0	.40	8.4	1.2	25	
2.0	0	0	0	0	
3.5	.17	2.8	.6	10	
5.0	.14	2.2	.7	11	
5.0	.32	3.2	1.6	16	
7.5	.77	12.6	5.8	94	
<u>88.5</u>	<u>.45</u>	<u>3.6</u>	<u>40</u>	<u>318</u>	

VOLUME

$$V = \left[\frac{(L_1 = 40) + (L_2 = 45)}{2} \right] \times (H = 23) \times (W = 6.8)$$

$$V = 6647$$

$$Tons = \frac{6647}{12} = 554$$

554 Tons @ 0.45 Au 3.6 Ag

BLOCK VIII 54 DRIFT NORTH BACK - INDICATED
54+10 N TO 54+25 N

GRADE

FACE SAMPLES

<u>W</u>	<u>Au</u>	<u>Ag</u>	<u>Au x W</u>	<u>Ag x W</u>
3.0	.15	8.1	.45	24
9	0	0	0	0
4.5	.89	0.8	4.00	4
<u>5.5</u>	0	0	<u>0</u>	<u>0</u>
22	.20	1.3	4.45	28

VOLUME

$$V = (W = 10) \times (L = 20) \times (H = 10) = 2000$$

$$\text{Tons} = \frac{2000}{12} = 167 \text{ tons}$$

167 Tons @ 0.20 Au 1.3 Ag

Note: (1) Could possibly be a high grade pocket here which would give substantially better results than indicated

(2) Very weak caving ground conditions !!

This will require mucking out & timbering.

BLOCK IX SOUTH BLOCK ABOVE SASE XC-INDICATED

GRADE	<u>W</u>	<u>Au</u>	<u>Ag</u>	<u>Wx Au</u>	<u>Wx Ag</u>
DDH intersections	5.25	1.30	3.2	6.82	17
	5.0	.07	9.1	.35	45
	5.0	.08	16.6	.40	83
Minimum mining width = 5.0'	3.0	.26	5.0	.78	15
	2.0	0	0	0	0
	4.0	.31	1.9	1.24	8
	<u>1.0</u>	<u>0</u>	<u>0</u>	<u>0</u>	<u>0</u>
	25.25	0.38	6.6	9.6	168

Volume

$$\begin{aligned}
 \text{Area} &= (110 \times 40) + \left(100 \times \frac{60}{2}\right) + \left(105 \times \frac{65}{2}\right) \\
 &= 4400 + 3000 + 3412 \\
 &= 10812
 \end{aligned}$$

$$V = 10812 \times 5 = 54060$$

$$\text{Tons} = \frac{54060}{12} = 4505$$

4500 tons @ 0.38 Au 6.6 Ag

