# REPORT ON GEOPHYSICAL SURVEYS HEATHER PROPERTY

CAROL S, TANIA S, LUCIA S, MARINO S
CAROL S2, EFRAM S, TANIA S2,
TANIA 3, TANIA S4, CAROL S3
CLAIMS

VICTORIA MINING DIVISION NTS 92 C 15 and 16

Latitude 48°58'N, Longitude 124°30'W

for

CHEVRON CANADA RESOURCES LIMITED

January, 1984 Toronto, Ontario J.L. LeBel, P.Eng. C. Pawluk, B.Sc. MPH Consulting Limited

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#### 1.0 INTRODUCTION

This report presents the results of a program of transient electromagnetic and mise-a-la-masse geophysical surveys conducted on the Chevron Canada Resources Limited, Heather Property located on southern Vancouver Island.

The surveys were conducted on two areas designated the Showing Area and Area 1. In the Showing Area, both transient electromagnetic and mise-a-la-masse surveys were conducted. In Area 1 only transient electromagnetic measurements were made.

The purpose of the surveys was:

- (i) Showing Area identify the geophysical response of and trace the extent of a showing of Au, Cu and Zn mineralization;
- (ii) Area 1 locate the cause of weak airborne electromagnetic anomalies and related copper soil geochemical anomalies.

The surveys were conducted by MPH Consulting Limited of Toronto, Ontario during the period November 4 to December 15, 1983. The program was under the direction of J.L. LeBel, P.Eng. and C. Pawluk, B.Sc. The survey progressed at a relatively slow pace because of heavy preciptation, including snow, which made movement on the steep terraine particularly treacherous.

### 2.0 PROPERTY, LOCATION AND ACCESS

The Heather property consists of 10 mineral claims (191 units), the status of which is summarized below.

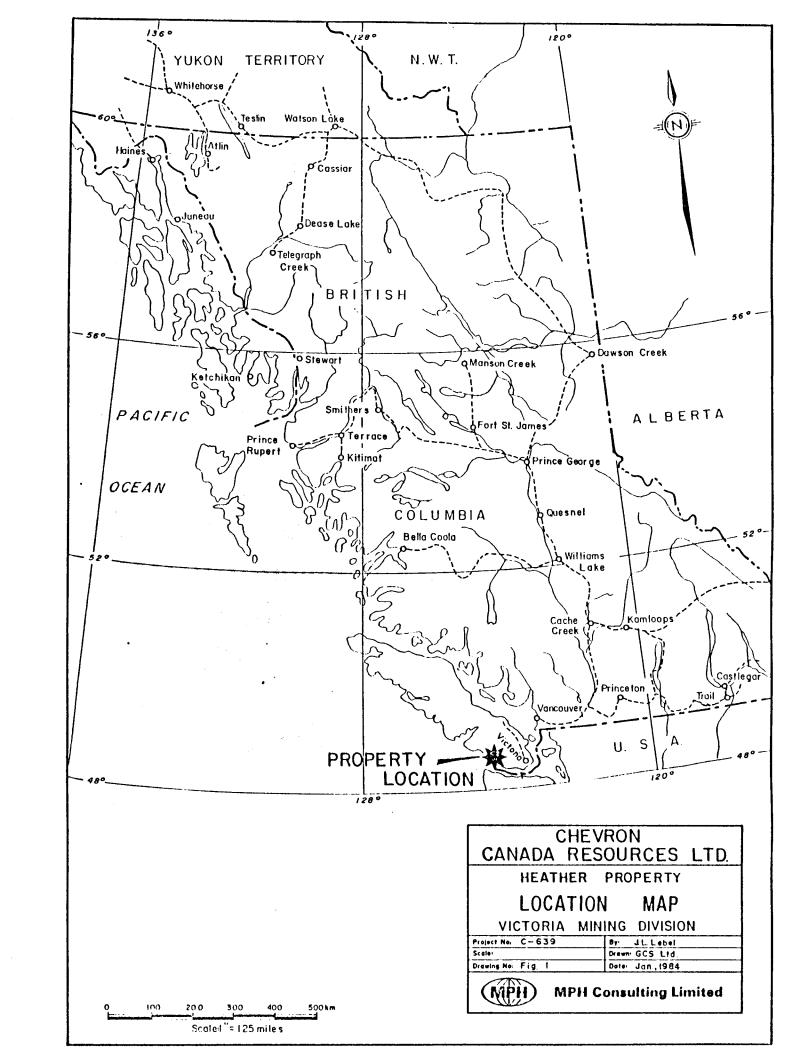
Claim Name	No. of Units	Record Date	Record No.
CAROL S	20	August 3, 1982	644
TANIA S	20	August 3, 1982	645
LUCIA S	20	August 3, 1982	646
MARINO S	20	August 3, 1982	647
CAROL S2	20	August 3, 1982	648
EFREM S	20	August 3, 1982	649
TANIA S2	15	October 5, 1982	683
TANIA S3	20	October 5, 1982	684
TANIA S4	16	October 5, 1982	685
CAROL S3	20	October 5, 1982	686

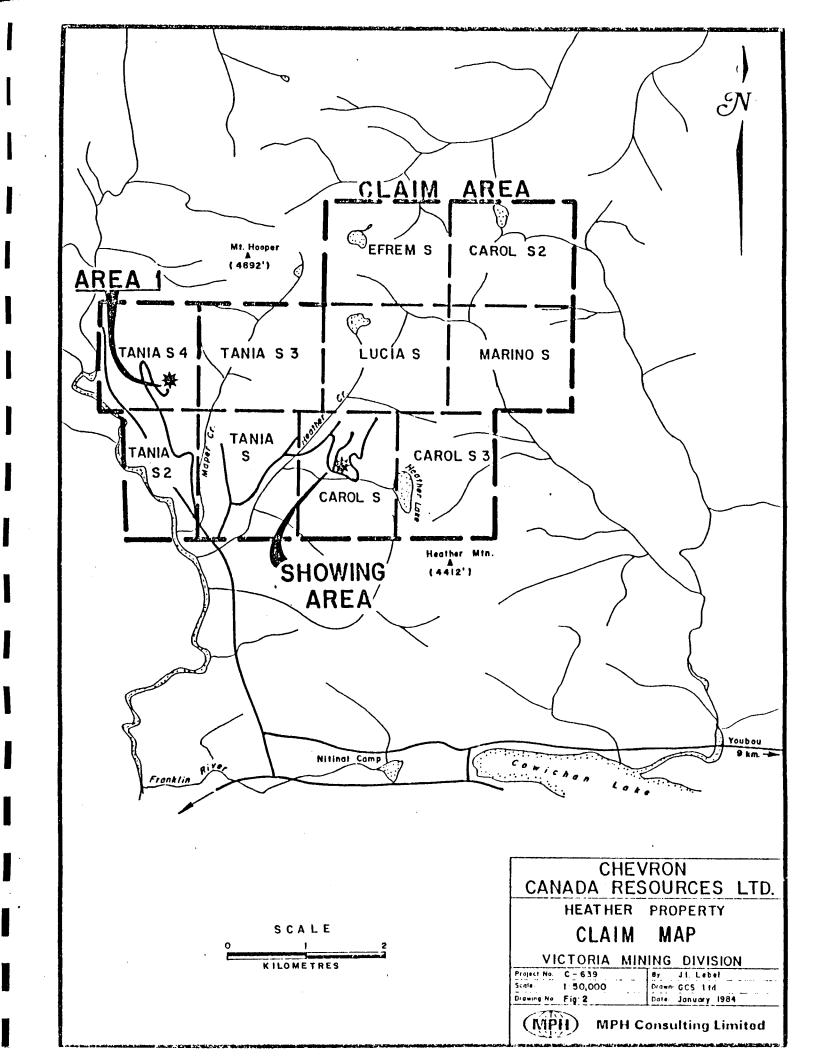
The geophysical surveys described herein focussed on the Carol S claim (Showing Area) and the Tania S4 claim (Area 1).

The property is located at the west end of Cowichan Lake on the southern end of Vancouver Island, approximatley 20 km west of the town of Youkou, B.C. at latitude 48°38'N, and longitude 124°30'W in the Victoria Mining Division-NTS 92 Cl5 and 16 (Figures 1 and 2).

Access to the property is gained from Youbou by either the north or south shore Cowichan Lake roads to the Crown Zellerbach main line. A network of branch logging roads provides access to the immediate areas of the surveys.

Road conditions at the time of the survey were poor because of heavy precipitation which caused numerous wash outs and threatened some of the bridges crossing creeks in the survey area.





### 3.0 GEOLOGY AND MINERALIZATION

### 3.1 Regional Geology

The region is underlain by the rocks of the Sicker Group.

The three major formations of the Sicker Group are the Buttle

Lake Formation, Myra Formation and Nitinat Formation.

The lowermost Nitinat formation is composed of 8,000 to 10,000 feet of altered basalt flows, breccias and tuffs which are in turn overlain, intercalated and interfingered with greywacke, argillite, felsic tuffs, mafic intrusives and chert of the Myra formation. These are unconformably overlain by up to 2,000 feet of crinoidal and cherty limestone and argillite of the Buttle Lake Formation.

### 3.2 Property Geology

Although all the Sicker Group formations are present on the property, the Myra formation is of primary interest as it hosts the Westmin Resources deposits at Buttle Lake and at Mount Sicker. Both of the grids used in this survey are located within the boundries of the 1 to 1.5 kilometer wide, northwesterly striking, steeply dipping (45° - 90°) Myra formation. It is composed of a series of well bedded tuffs and tuffaceous sediments (in some cases shaley). The tuffs are rhyodacitic in composition although some rare quartz eyes have been located which may indicate the presence of some rhyolite tuffs. The entire formation is highly contorted suggesting the entire Sicker Group may be highly deformed.

A green tuff unit, a maroon tuff unit, and a silty tuff unit comprise the three main units of the Myra Formation. The green tuff appears to be the main volcanic unit and lies above and below the other two units with the maroon tuff

overlying the silty tuff. The maroon tuff is very well bedded and locally resembles shale. The silty unit is also well bedded (beds approximately 1-2" thick) and is locally well sheared. Most of the faulting seems to have been in the silty unit.

Medium to coarse grained diorite intrudes both the Myra and the Nitinat Formations. One of these diorite intrusions underlies the area covered by Area 1.

### 3.3 Mineralization

The only significant mineralization recognized on the property consists of stringer to massive sulphides composed of quartz/pyrite/chalcopyrite exposed in a trench centered in the Showing Area. The zone is hosted by an altered (clay, chlorite and sericite) silty tuff centered in a large antiform.

Taken by itself, the showing is probably unimportant but it may represent a stringer sulphide zone on the fringe of a massive sulphide body or a faulted remnant of a massive sulphide.

#### 4.0 PREVIOUS WORK

Previous work conducted on the property consisted of geological mapping, soil geochemical surveys and an Input MVI helicopter airborne electromagnetic survey.

The soil geochemical survey detected a good multi-element (Au, Cu and Zn) anomaly in the Showing Area. Moderate Cu soil geochemical anomalies were outlined on either side of Area 1. These anomalies may be linked together with other anomalies in the area to form a semi-continuous, 2 km long zone apparently related to the altered silty tuff horizon of the Myra Formation.

The Input airborne electromagnetic survey detected several weak 1 and 2 channel anomalies in the vicinity of Area 1. The anomalies could be attributed to any number of sources such as:

- (i) deeply buried massive sulphide body;
- (ii) shallow disseminated sulphide body or sulphide body composed principally of sphalerite and galena;
- (iii) geological feature such as a contact or fault;
- (iv) noise.

No Input anomalies were registered over the Showing Area.

### 5.0 INSTRUMENTATION AND SURVEY PROCEDURES

### 5.1 Line Cutting

Two grids to accomodate the survey were cut by Bema Industries Limited. The grids were oriented so that the transmitter loops for the transient electromagnetic survey would be as close to planar as possible. As a consequence, their orientation ignored local geologic trends.

In the Showing Area, the grid was centered on the Showing. The baseline extends 400m east and 400m at an azimuth of 090° from the showing. 400m long lines were established at 100m intervals along the base line extept at the center of the grid where lines were established at 25m intervals (Figure 3).

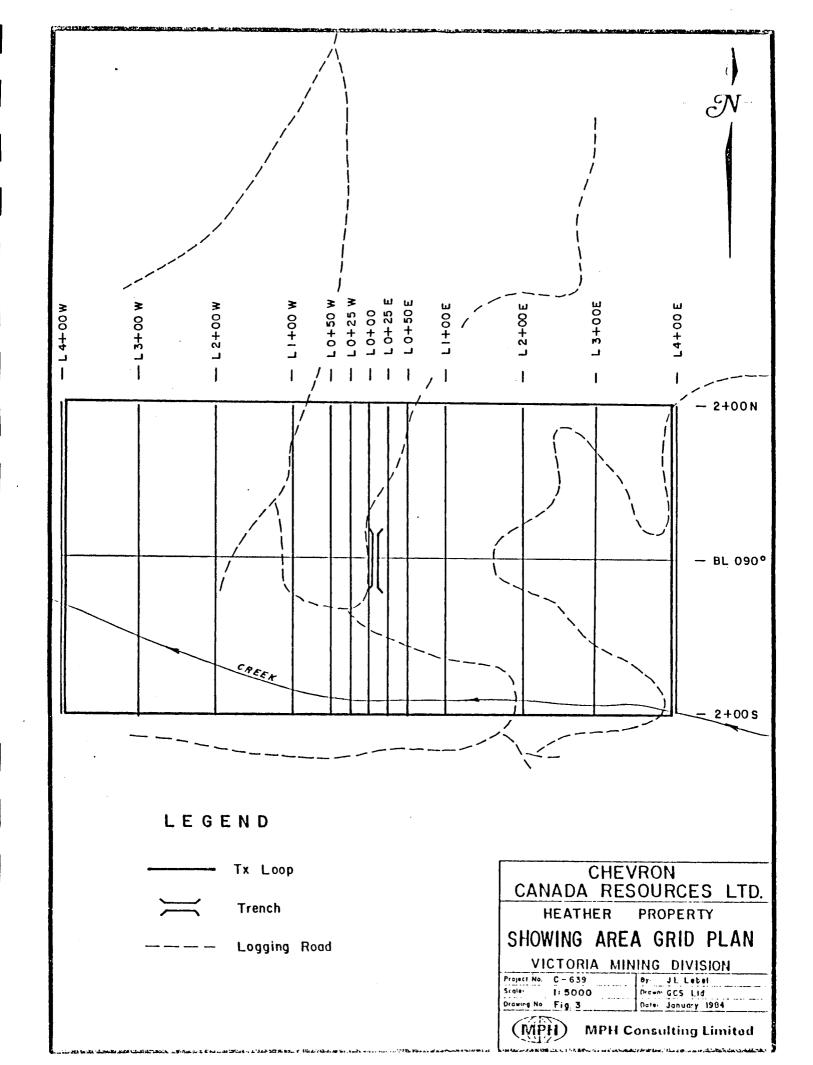
In Area 1, the grid consists of a 800m long base line with an azimuth of 000° with 800m long lines located at 100m intervals (Figure 4).

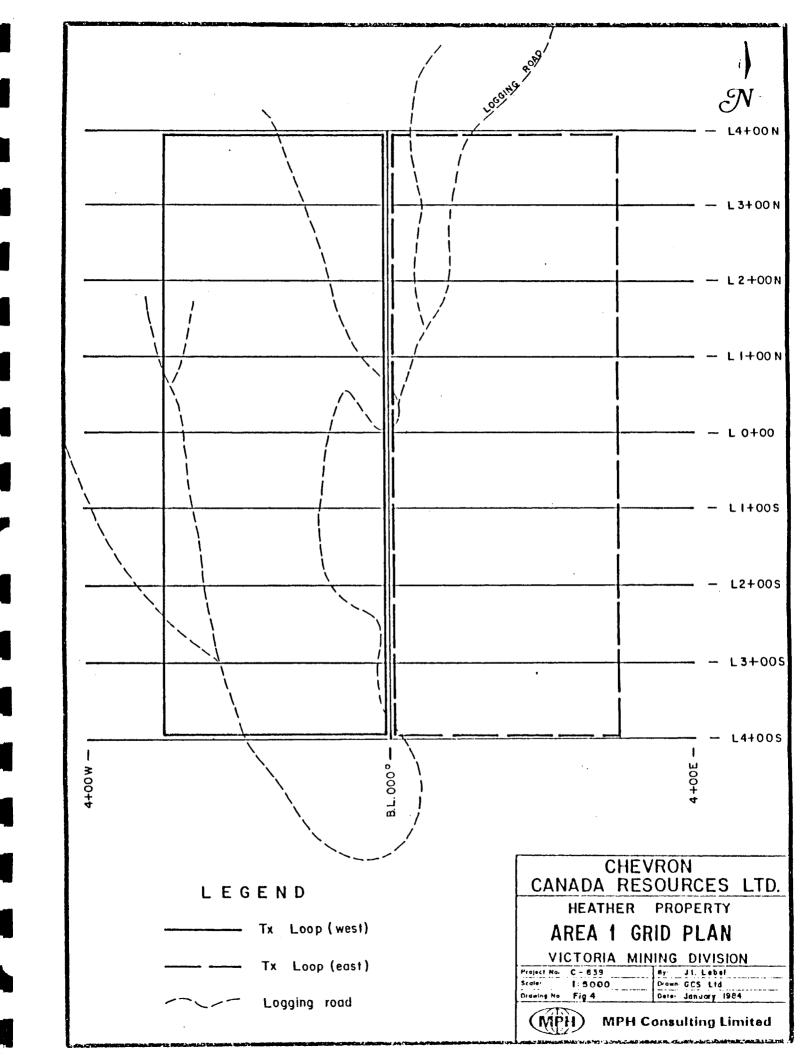
# 5.2 Transient Electromagnetic Survey

The transient electromagnetic survey was conducted with a Geonics EM-37 system. Specifications of the EM-37 are detailed in Appendix III.

The survey was conducted in the Turam Mode with large transmitter loops. One  $800 \times 400m$  transmitter loop was established in the Showing Area and two  $800 \times 300m$  were set up in Area 1 as indicated in figures 3 and 4.

An alternating commutated square wave curent form is impressed into the transmitter loop. The current in the transmitter is turned off abruptly producing a large electromagnetic field in the ground. The repetition rate of the current wave





form was set at 30 hz to respect the expected high background resistivities in the area.

Components of the secondary field induced by primary field are measured with a mobile receiver loop approximately lm in diameter. In this case, components in the x, y and z directions where x is taken parallel to the line direction, were measured.

In order to keep the orientation of the receiver coil as constant as possible, orientations are defined as true directions rather than with respect to the plane of the transmitter.

Measurement of all of the components of the secondary fields is essential in determining the size and orientation of cause of any anomalies. Also, it was considered important to measure all of the components because the ultimate strike and dip of any conductors in the area was not precisely known. The EM-37 records the secondary fields across 20 gates spaced at logarithmic intervals after the current in the transmitter is terminated. Readings were taken at 25m and/or 50m intervals inside the transmitter loop. Measuring inside of the transmitter loop assures that the primary field is as uniform as possible and coupled with attempts to keep the transmitter in the plane of the topography reduces topographic effects that otherwise might be present.

Unfortunately, with this configuration, a vertical sheet-like conductor located in the middle of the loop will be zero coupled with the primary field and will not generate an anomalous secondary field.

To increase the extent of areal coverage in Area 1, a limited amount of coverage was affected outside of the transmitter loops.

The data collected were reduced and plotted using the Geonics "GSP37" processing software.

The following data was acquired:

Showing area: L 2+00W, 1+50N - 1+00SL 1+00W, 1+75N - 1+00SL 0+00, 1+50N - 1+00SL 1+00E, 1+50N - 1+50SArea 1: Loop 1 (west) 2+00N, 0+25W - 2+75W 1+00N, 0+25W - 2+75W0+00, 0+25W - 2+75W0+50E - 3+00E1+00S, 0+25W - 2+75W2+00S, 0+25W - 4+00W3+00S, 0+25W - 4+00WLoop 2 (east) 0+00, 0+25E - 3+75E1+00S, 0+25E - 3+75E

Data was collected on lines 2+00S, 1+00N and 2+00N in Area 1 but not saved because of failure of the data logger attributed to excessively wet conditions.

# 5.3 <u>Mise-a-la-Masse-Survey</u>

The mise-a-la-masse survey was conducted on the Showing Area with a Huntec Mark IV 2.5 kw induced polarization system. Specifications of the Huntec system are detailed in Appendix III.

Two separate current electrodes, designated electrode 1 and electrode 2, were installed in the showing on line 0+00 at 0+25N and 0+25S, respectively. Each electrode consisted of 3 stakes wrapped with aluminum foil which were jammed into holes excavated by a portable drill. The infinite current electrode consisted of a sheet of aluminum foil placed in a pit. It was located approximately 1 km south of the centre of the grid.

The mobile potential electrode consisted of a steel rod. The infinite potential reference electrode consisted of a sheet of Aluminum foil located approximately 800m north of the centre of the grid.

Current was transmitted sequentially through the two current electrodes and primary voltage measurements were made along the survey lines. Currents were in the 200 to 300 ma range with the transmitter voltage set at 2,200 volts.

Measurements were not taken along line 0+00 because most of the stations were located on an abandoned logging road where the potential electrode could not be driven into the ground.

### 5.4 Personnel

The MPH Consulting Limited personnel involved in the survey were:

- L. LeBel, Senior Geophysical Consultant
- C. Pawluk, Geophysicist
- J. Ashenhurst, Technician
- R. Krawinkel, Technician
- T. Archibald, Technician

### 6.0 PRESENTATION OF DATA

The results of the transient electromagnetic survey are presented in Appendix I. Plots of the components of the secondary fields (dB/dt) in  $NV/Am^2$  versus position are given for all 20 channels on each line.

Modelling results attempted for the results from the Showing Area using the "MODLSU" program of the GSP37 software are presented in Appendix II. The field data is shown as a dotted line, while the theoretical data is indicated by a solid line.

Appendix III contains a suite of models to illustrate the response of some typical conductors. The model adopted consists of a 300m by 100m plate with a conductance of 10 siemens (mho). conductance of 10 may be low for a massive sulphide body but is considered adequately representative of a vein stringer disseminated type sulphide body. The plate is positioned in the center of an 800m by 400m transmitter loop with a strike parallel to the long dimension of the transmitter. Other strike directions would result in similarly shaped anomalies with appropriately reduced amplitudes. Results were calculated for various dips of the plate at depths of 50m and 150m. The model results assume that the transmitter loop lies in the xy-plane. In the survey areas this condition was not necessarily maintained because the x-direction was defined as true vertical and the transmitter was positioned on the land surface which, in places, sloped at up to 45°.

The results of the mise-a-la-masse survey for each current electrode position are illustrated on Map 1. The maps show the primary voltage normalized by the current in units volts/amp. Contours are at semi logarithmic intervals ... 1.0, 1.5, 2.0, 3.0, 5.0, 7.5, 10.0 ...

### 7.0 RESULTS AND INTERPRETATION

### 7.1 Showing Area

### 7.1.1 Transient Electromagnetic Survey

A weak 'cross-over' anomaly in the Z (vertical) component was recorded by the early channels at about station 1+00N on line 0+00. The observed response is consistent with the resposne expected at the north edge of a flat lying sheet with a conductance of 2 seimens and located at a depth of 50m as shown by the model modelling results in Appendix II. No response that would serve to indicate the southern edge of the sheet was recorded on the southern end of line 0+00. Note, however, that data was not collected south of the station 1+00S because of a culvert located at 1+50S. It is also possible that the edge of the sheet occurs outside of loop beyond the limits of the survey.

No anomalous responses were recorded on line 1+00W. A pseudo cross-over response observed at 0+75S on line 1+00E could not be satisfactorily modelled when considered in light of the anomaly observed on line 0+00. This response may be a topographic effect caused by a steep slope between 1+00S and the end of line 1+00E at 2+00S,

Elsewhere on the grid, no anomalies similar to the modelled responses for some typical examples shown in Appendix III were recorded.

## 7.1.2 Mise-a-la-Masse Survey

The contoured primary voltages of the mise-a-la-masse survey produce ellipses of low eccentricity. The

highest eccentricity (ratio of major axes of the ellipse to the minor axes of the ellipse) of approximately 2 occurs in a 100m x 50m area centered on electrode 2. The ellipses are elongated in a northwest/southeast direction parallel to the geological trend.

Considered separately, the results from each current electrode are consistent with the presence of a 75m x 30m conductor underneath each electrode. When the results are compared, however, it can be seen that the electrodes produce ellipses that are independent of each other. This implies that if a conductor is present it has extremely low, laterally varying conductivity.

The results may also be explained by a northwest trending zone of high resistivity flanked by low resistivities. This explanation concurs with the transient electromagnetic survey which did not detect a discrete conductive body.

### 7.2 Area 1

No transient electromagnetic anomalies similar to those illustrated by the modelling results in Appendix III were recorded in Area 1.

By way of general comments that pertain to both survey areas, it can be seen that the secondary field components decay to essentially zero amplitude by channel 10. This situation is a consequence of the high resistivities in the area which, according to the results of the mise-a-la-masse survey fall in the range of 2,000 ohm-m to 4,000 ohm-m.

### 8.0 CONCLUSIONS AND RECOMMENDATIONS

A poor, partially defined transient electromagnetic anomaly detected in the Showing Area may be explained by a small, shallow, low conductance flat lying sheet. The mise-a-la-masse survey results may also indicate a poor areally limited conductor but the results can also be explained by geological circumstances. The size of the conductor, if present, is too small to be of economic interest.

Nothing of interest was detected in Area 1.

The surveys covered only a small part of the Heather property. Economic potential for the property appears to be at depth. To completely evaluate the property additional coverage with a deep penetrating high resolution geophysical method like the transient electromagnetic method is recommended.

The modelling done indicates that a hypothetical, 300m by 100m, 10 siemen sulphide body should be detectable to a depth of at least 150m.

Respect from submitted

J(L. LaBel P,Eng.

C. Pawluk, Geophysicist
MPH CONSULTING LIMITED

#### CERTIFICATE

- I, J.L. LeBel of Vancouver, British Columbia hereby certify that:
- I hold a Bachelor of Science degree in Geological Engineering from Queen's University, Ontario, and a Master of Science degree in Geophysics from the University of Manitoba, Manitoba. I have practiced my profession in exploration geophysics continuously since graduation in 1972.
- 2) I am a Professional Engineer registered with the Association of Professional Engineers of British Columbia.
- I have based conclusions and recommendations contained in this report on knowledge of the area, my previous experience in geophysical methods and interpretation and on the results of the field work conducted on the property.
- I hold no interest, directly or indirectly in this property other than professional fees, nor do I expect to receive any interest in the property or in Chevron Canada Resources

  Limited or in any of its subsiduary companies.

J.L. LeBel, P.Eng.

Toronto, Ontario,

January, 1984

### APPENDIX I

Transient Electromagnetic Data

Showing Area

Area 1 (west transmitter loop)

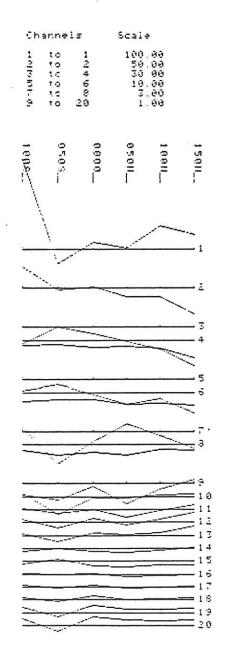
Area 1 (east transmitter loop)

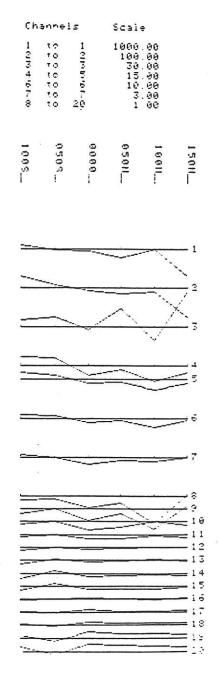
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Date File LNSHP LINE BBW - N Component dBN/dT (nW/Hm+2) TOFF corrected

Data +:10 3WSHP LINE 02W - V Component dBY/dT (nV/Am4), TOFF corrected

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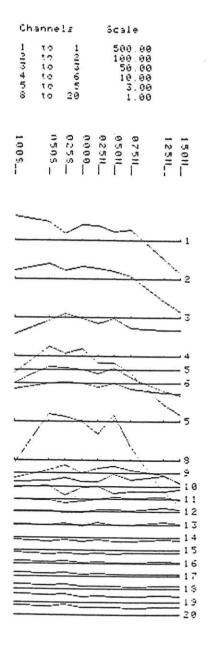
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Channels Scale
1 to 1 300.00 2 to 2 100.00 3 to 3 50.00 4 to 7 3.00 8 to 9 2.00 10 to 20 1.00
350E _ 325E _ \ 250E _ \ 260E _ 150E
2 3
10 11 12 13 14 15 16 17 18

Data file ENAIWR LINE 02N . Z Component d6Z/dT (nV/Am2), TOFF corrected

Channels

Scale

150 0							
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=	40	Ė		30.00			
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4	10	4		10 00			
5	10	6		3.00	4		
7	10	20		1.99			
27511_	750H	2001	-	-	650W_	025W_	
-1	-0	9	1261	1 0 0 M	OI.	N	
17.	2	3	2	2	2	<u>51</u>	
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- 1					-		
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- 17							
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	<i>[</i>		/	<u></u>		-5	
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Data tile 2NAINR
- Line 92N — X Component
- d8X/dT (nV/Am4)) TOFF corrected

Channels Scale			ale		
1 to 2 to 3 to	1 2 3	3 1	00.00 00.00 30.00		
1 to 2 to 3 to 4 to 6 to	5 7 20		00.00 00.00 30.00 10.00 3.00		
				ä	
250W_	2001	1501	_M801	Hese	9251
	1	1	1	1 1	
				/	
_			· · · ·	<u> </u>	1
	_			_/	2
_					
					3
$\Rightarrow$				<u></u>	4
					Э
7	>_			<del></del>	6
7				<b>V</b>	7
		_		$\Rightarrow$	3
					9
				$\equiv$	1
				=	1
					1
===				<u> </u>	1
				$\stackrel{=}{=}$	1
					2

Data tile 2NATUR LINE 32N Y Component dBY.dT (nV/Am²); TOFF corrected

Channels Scale	
1 to 1 300.00 2 to 2 100.00 3 to 3 30.00 4 to 4 10.00 5 to 8 3.00 9 to 30 1.00	
025H_ 050H_ 100H_ 150H_ 200H_ 250H_	
4	
10 11 12 13 14	
14 15 16 17 18	
20	

Data file INAIR LINE 01N - Z Component dBZ:dT (nV/Am²); TOFF corrected

Scale Channels 3000.00 300.00 60.00 30.00 3.00 1.00 1 to 2 to 3 to 4 to 5 to 3 to 11 to 1 2 3 10 20 025N\_ 275N\_ 2001\_ 100H\_ 15

Data file INAIR LINE GIN X Component dBX/dT (nV/Am2); TOFF corrected

Channels		Scale			
1 to 2 to 3 to 7 to 10 to	1 2 6 9 20	36 16	30.00 30.00 10.00 3.00 3.50		
2754	2004_	1454	1004	620H	1
			-		2
			=		3 4 5 6
X					7 8 9
					10
					1 2
					13
					12 13 16 17 18 18 18 18 18 18 18 18 18 18 18 18 18
					1 4
					1 7
					1 .
-					1 3
					2

Data tile INAIR LINE BIN Y Component GRY-dT (nV/Ami); TOFF corrected

Ch	Channels Scale					
1 2 4 8 10 14	to to to to	1 7 9 13 20		100.8 20.8 10.8 3.8 1.8	19 19 19 19 19 19	
250H_	2001		1451	1001		025W
\ \ \ -		/ /	<u> </u>	_/_	/ / _	2 3
/]	<u></u>					4 5 6 7
						3 3 10 11
						12
						15 16 17 18 19 20

Data (ile 000A1R LINE 000 - Z Component dBZzdT (nVZAm²); TOFF corrected

Channe	ls		ale		
1 to 2 to 3 to 4 to 7 to 8 to 10 to	12396799	16	00.00 00.00 30.00 5.00 3.00 1.00	•	
259W_	2004_	150W_	_H001	656M_	025W
	_				. 1
				<del>-</del>	2
X					. 3
					5
	<del></del>		<del></del>		7
				<del></del>	9
					11 12 13
	$\equiv$				14
					-17 -18 -15
					- 20

Data +11e 000A(P LINE 000 % Component dBX/dT (nV/Am²); TOFF corrected

Scale

Channels

250H 250H 2 2 3 3 4 5 6 7 3 10 11 12 13 14 15 16 17 18 19 20	1 2 3 4 8 11	to 1 to 2 to 3 to 7 to 18 to 20	10	00.00 00.00 30.00 10.00 3.00 1.00		
2 3 4 5 6 6 7 7 10 11 11 12 13 14 15 15 16 17 18 19	27511_	2091	150H_	1984_	050W_	0251
3 4 5 6 7 10 11 11 12 13 14 15 16 17 18 19	_					1
1 1 1 1 1 2 1 2 1 3 1 3 1 4 1 5 1 5 1 6 1 7 1 8 1 9 1 9	-	_				2
11 12 13 14 15 16 16 17 18	$\leq$			<u></u>		3
11 11 12 13 14 15 16 16 17 18						5 5 7
12 13 14 15 16 17 18	Z					3 3 10
14 15 16 17 18			$\geq$			12
16 17 18 19	=			_		1 4
19	_					16 17
						19

Data file 000AIR LINE 000 Y Component dBY/dT (nV/Am²); TOFF corrected

(n	anne	lε	Sca	le	÷
1 2 4 5 9	000000000000000000000000000000000000000	1 3 4 8 20	30 10 1	0.00 0.00 0.00 3.00 1.00	
275W	250N	2001	1504	100N_	0504_
_			^	$\overline{}$	<u>~</u> 1
==	===	===			2 3
=	· 			$\stackrel{\frown}{}$	4
					5 6 7 8
_			$\Rightarrow$		9 10
				_	= 11
_					= 13
					1 4
_					= 15
					16
					17
		-			== 18
_					= 13
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icale

Channels

Scale

Channels

1 2 3 4 5 8	100000000000000000000000000000000000000	10 20	11	300 ( 300 ( 100 ( 10 ( 10 (	00 00 00 00 00 00	
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						= 3 = 9 10
						= 11 = 12 = 13 = 14
						1 5 — 1 6 — 1 7 — 1 3
=	_					== 15

1 to 1 300.00 2 to 2 100.00 3 to 3 30.00 4 to 3 10.00 9 to 20 1.00  2 50 0 0 0 0 0	Chennels	Sca	le	
2 2 3 4 5 6 7 8 10 11 12 13 14 15 16 16	1 to 1 2 to 2 3 to 3 4 to 8 9 to 20	30 10 3 . 1	0.00 0.00 0.00 0.00 1.00	
2 3 3 5 5 6 7 7 8 11 12 13 14 15 16 17 18	100E_	150E_	250E_	300E_
3 5 5 6 7 8 9 10 11 12 13 14 15 16 16 17	<del>-</del>			
10 10 11 11 12 13 14 15 16				2
10 10 11 11 12 13 14 15 16 16				₹3
10 11 12 13 14 15 16 17				7
10 11 12 13 14 15 16 17				
13 14 15 16 17				10 11
15 16 17				13
16				
1				<u> </u>
19				= 1.8
				$=\frac{12}{20}$

1 to 2 to 4 to 8 to 1: to	1 3 7 10 20	i	300.0 100.0 10.0 3.0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
050E	1005	150E	200E_	250E_	300E_
<u></u>		<u>~</u>			<u>_1</u>
					≤2 =3
					≥ 4 = 5 = 6 = 7
				-	_ ; _ 9 = 10
					-11 =12 =13 =14 =15
					— 16 — 17 — 18 — 19 — 20

Ua+3 +11e ISAIWR LINE 01S - I Component dBZ/dT (nV/Am²); TOFF corrected

Channels

Scale

Channels	Scale	
1 to 2 to 3 to 5 to 9 to 2	1 100.9 2 20.9 4 10.0 3 3.0 0 1.0	9 9 9 9 9
250W_ 250W_ 275W_	150W_	025W_
		2 2 3 4 5 6 7 3
		9 10 11 12 13 14 15 16 17 18 19 20

Data file ISAIWR LINE 01S - X Component aBX/dT (nV/Ami); TOFF corrected

Channe	els		ale	
1 to 4 to 7 to 10 to	3 6 9 20	1	00.00 10.00 3.00 1.90	r
258N	2001_	1504_		025H
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			_	4 5 
	r Z	$\stackrel{\textstyle \frown}{}$		7
				10 1i
			=	12 
				16
				2

Data file 1981WF LINE 019 Y Component dBY/dT (nv/Am4); TOFF corrected

Channe	15		ale		
1 to 4 to 7 to 10 to	3699	1	09.00 10.00 3.00 1.00		
ğ					
250W_ 275W_	2004_	150W_	-M001	Mese	025W
	<u>;</u>				1 2 3
					5
					7 8 9
					10
					14 15 16
					18

Dets #11e 15A1ER LINE 935 - I Component dBI/dT inV/Amil); TOFF corrected

Dava	•11e	2SA1ER		
LINE	028	X Cor	nponer	n t
dBX/c	tT 'n'	/ Hinra ) ,	TOFF	corrected

Data	1114	15A1ER		
LINE	025	Y Cor	nponer	nt
dBY/	dT int	1/Amesi	TOFF	corrected

Channels	Scale
1 to 1 2 to 2 3 to 3 4 to 6 7 to 9	3000.00 500.00 100.00 10.00 3.00 1.00
250N_ 300N_ 350N_ 400N_	050W_ 100W_ 150W_
$\longrightarrow \mathbb{M}$	
	2
- 1	5
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	9
- <del>\</del> \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	10
	711
<u> </u>	
X //	
A 1/2	
	16
<b>3</b>	18
	19
	29

Сh	anne	lΞ		ale			
1 2 3 4 8 10	to to to to	1 2 3 7 9 20		00. 00. 30. 10.	00 00 00 00 00		
40001	3504	300H	2001	1261	100H_	ครคน_	
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_		~				-/,	13
						<del>~,</del>	1 4
=		-=		=		=	1 5
2-	-					<u> </u>	1 6
=			-	_=	_	<del>_</del>	17
==					=		18
$\equiv$		==				$\Rightarrow$	13
	_				_		

Channels			Scale					
123478	to to to	1 2 3 6 7 9		100 10 3 1	0.00 0.00 0.00 3.00 1.00	3		
4008	350N	_N00£	250H_	2001_	1501	TH001	050W_	
	-1	_			_		<b></b> 1	
_	7	V				<u> </u>	_ · _ 2	
_	/	<u> </u>	_			<u>~</u>	<u>⊃</u> ₃	
		· ·	=				<b>=</b> 4	
$\frac{2}{\pi}$	A.	~	-=-		<u> </u>	_	-6 /_	
$\mathbb{Z}$		_					<b>-</b> 3	
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				_			= 12 = 13 = 14 = 15	;
16 17 18 19								
$\equiv$					_	_	= 13 = 20	

Data +:10 38ALEP LINE 938 - I Component dBZ/dT (nV/Am²), TOFF corrected

Data file 38A1EP LINE 038 - X Component dBX/dT inv/Am4), TOFF corrected

Dava	+ 1 le	3SA1ER	
		Y Compor	nen t
			E corrected

Channels		Sca				
1 to 2 to 3 to 4 to 5 to 11 to	1 2 3 4 10 20	106	90 .0 90 .0 30 .0 1 .0	10 10 10 10 10 10		
350H_	250H_ 275W_	2001	1504_	1001	050W_	
"	$\wedge$				1	
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	<u>,                                     </u>	-				2
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				_		16
		$\equiv$	_			17
		_				18
		_	=	_		19

Channe		3!e				
1 to 2 to 3 to 4 to 5 to 8 to	12357-20	3	00.0 30.0 10.0 1.0	90 90 90 90 90		
350H	250H_ 275H_	2001_	150M_	1001	950M 1	
		/	\ \ \	\ <u>\</u> \ <u>\</u> \	4	1 2 3
		~	1	\( \lambda \) \( \lambda \)	i Fil	4 5
	**************************************		スノグラ			3 9 10 11
						12 13 14 15
						17 18 19

Channels	Scale •
1 to 1 2 to 2 3 to 3 4 to 5 6 to 20	300.00 100.00 10.00 3.00 1.00
350H_	150M_ 150M_
$\triangle$	1
	2
	3 6 6 7 8 9 10 11 12 13 14 15 16
	17 18 19 20

### APPENDIX II

Model for Showing Area Line 0+00

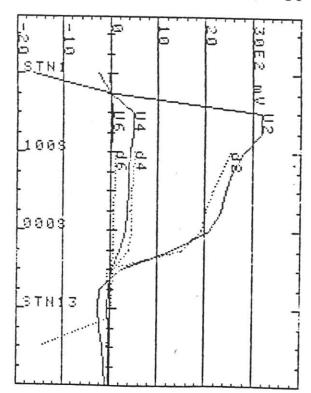
44444 Plate # 1 44444 STRike DIF -9 0 FLUnge LENath 240 DEPth 300 POSition | 50 -50 -50 CONduct\*thick 1.1  $\mathsf{Tx} = \mathsf{P1} \mathsf{M}(\mathsf{pH})$ T(ms) -197 45 .035784

Model T Plate # 1 \*1/

0+00 Z cpt, Gain, TXC= 7 11

Model U Plate # 1 %1/

0+00 Z cft. Gain, TXC= 7 11



PLUnge			ø	
LENath			150	
DEPth PO31†1on 50	-50	-50	300	
CONduct*thick		•	1.6	
Tx-pi_M(vH)			τ(ms)	
-138.17			.036098	
Madal V				

Model X Plate # 1 \*1/

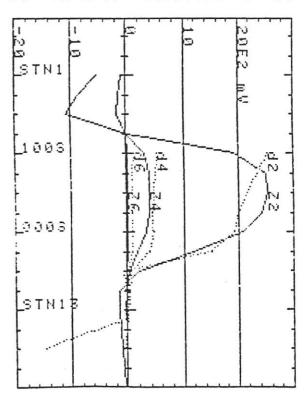
0+00 Z cpt. Gain, TXC= 7 11

Model Y Plate # 1 \*1/

0+00 Z cpt. Gain, TXC= 7 11

Model Z Plate # 1 \*1/

0+00 Z cpt. Gain, TXC= 7 11

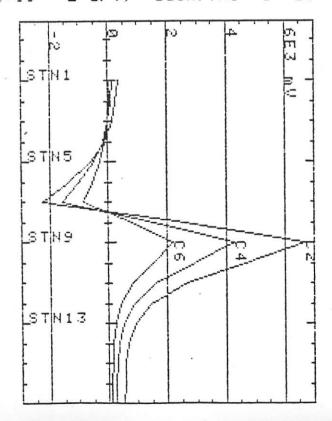


# APPENDIX III

Transient Electromagnetic
Modelling Results

late approx'n; 1 late approx'n; 2 late approxima 3 44444 Plate # 1 44444 STRike 45 DIF Ø FLUnge 300 LENath 100 DEPth POSition -36 0 -14 10 CONduct\*thick 1(ms) Tx-p1 M(vH) .15775 -44.88

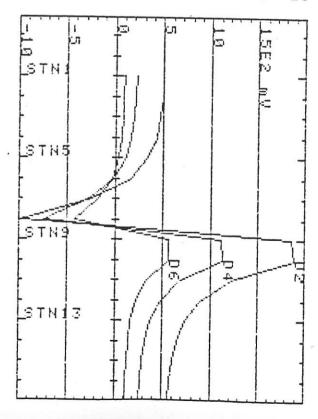
Model C HH3 R =2000/Plate # 1 \*1/ 0+00 Z cst. Gain/TXC= 6 20



late approx'n; 1 late approx'n; 2 late approx'n; 3 44444 Plate # 1 44444 STRike DIP 89 PLUnge ū LENath 300 DEPth 100 POSition -8.6 0 -.8 CONduct\*thick 10 TX-P1 M(pH) 7(ms) -10.711.15775

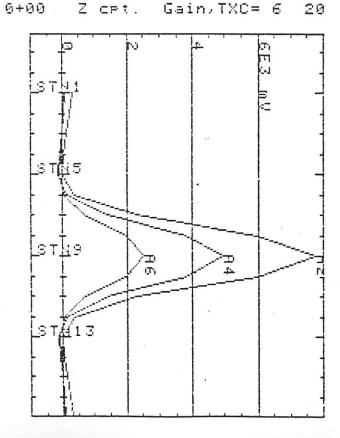
Model D HHS R =2000/Plate # 1 \*1/

0+00 Z cpt. Gain,TXC= 6 20



late approxima 1 late approx'n; 2 late approx'n; 3 44444 Plate # 1 44444 STRike DIP PLUnge LEMath 300 100 DEPth POSition -50 0 -50 CONduct\*thick 10 Tx-pl M(pH) 7(ms) -65.055 .15775

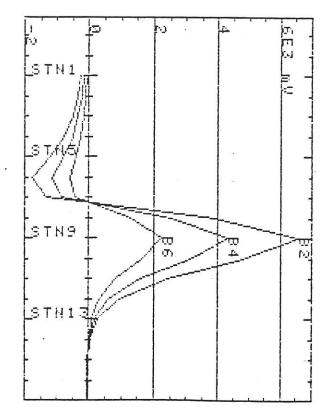
Model A HHS R =2000/Plate # 1 \*1/



44444 Plate # 1	44444
STRike	ผิ
DIF	30
PLUnge	9
LEMath	300
DEPth	100
POSition -42.5	0 -25.5
CONduct*thick	19
Tx-pl M(pH)	γ(ms)
-55.437	.15775

Model B Flate # 1 \*1/

0+00 Z cpt. Gain, TXC= 6 20



late approx'n; 1 late approx'n; 2 late approx'n; 3 44444 Plate # 1 44444 STRike DIP 80 PLUnge LENgth 300 DEPth 100 POSition -8.6. 0 -150.8 CONduct\*thick 10 Tx-p1 M(pH) τ(ms) -6.0925 .15775

Model D HHS R =2000/Plate # 1 \*1/

0+00 Z cpt. Gain,TXC= 6 20

	1775		
ST NOT NOT NOT NOT NOT NOT NOT NOT NOT NO		4.6	
1)6	<u></u>		
			$\int_{\mathbb{R}^{n}} \int_{\mathbb{R}^{n}} dx$

late approx'n; 1 late approx'n; 2 late approxim; 3 44444 Plate # 1 44444 STRike DIP 30 Pillnge . Й LENath 300 DEPth 100 POSition -42.5 0 - 125.5CONduct\*thick 19 T(ms) Tx-pl M(pH) -37.922.15775

0+00 Z cpt. Gain,TXC= 6 20

HHS R =2000/Plate # 1 \*1/

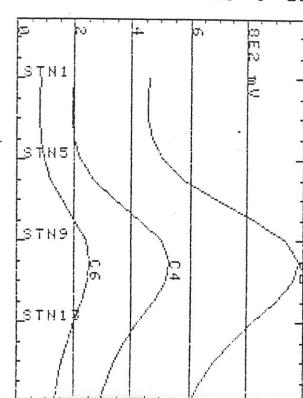
Model B

_6				
9 B6 18 STA18	8 8 8	1.0	14	18E2 MV

late approx'n; 1 late approx'n; 2 late approx'n; 3 44444 Plate # 1 44444 STRike DIF 45 PLUnge 0 LENath 300 DEPth 100 POSition -36 9 -114 CONduct\*thick 10 Tx-pl M(vH) T(ms) -31.423 .15775

Model C HHS R =2000/Plate # 1 \*1/

0+00 Z cpt. Gain,TXC= 6 20



HSSHOW HHS OVER SHOWING ON HE. ATHER PROPERTY

TXX,TXY,TXA= 400.800.0 TX P=0 0 0 t/o min,max,density= . 0001.1.3

LINES: '

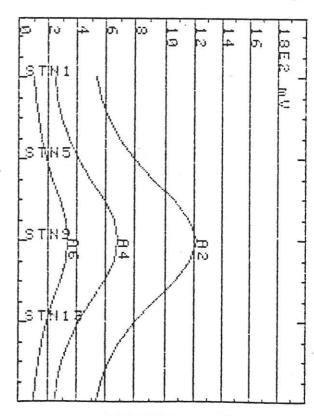
MAX # GATES = 11 MAX # PLATES = 5

0+00			
Index	Stn	X	Y
1	STN1	-200	Ø
2	STN2	-175	Ø
3	STN3	-150	Ø 9
4	STN4	-125	Ø
5	STN5	-100	Ø
UM456700	STN6	-75	9 9
7	STN7	-50	Ø
8	STNS	-25	Ø
9	STN9	0	9 9
10	STN10	25	Ø
1 1	STN11	50	0
12	STN12	75	0 0 0
13	STN13	100	Ø
13 14	STN14	125	Ø
15	STN15		Ø
16	STN16	175	Ø
17	STN17	200	Ø

late approx'n; 1 late approx'n; 2 late approx'n; 3 44444 Plate # 1 44444 STRike DIP PLUnge 0 LENath 300 DEPth 100 POSition -50 0 -150 CONduct\*thick Tx-pl M(vH) 1(ms) -43.724 .15775

Model A HHS R =2000/Plate # 1 \*1/

0+00 Z cpt. Gain, TXC= 6 20



λPPENDIX IV

Equipment Specifications

## GEONICS LIMITED

## EM37 Ground Transient Electromagnetic System Technical Specifications

Transmitter See Fig. 1 Current Waveform Repetition rate 3Hz or 30Hz in countries using 60Hz power line frequency; 2.5Hz or 25Hz in countries using 50Hz power line frequency; all four base frequencies are switch selectable. Turn-off time  $(\Delta t)$ fast linear turn-off of maximum 300 µsec. at 20 amps into 300x600m loop. Decreases proportionally with current and (loop area) to minimum of 20 usec. Actual value of  $\Delta t$  read on front panel meter. Transmitter loop any dimensions from 40x40m to 300x600m maximum at 20 amps. Larger dimensions at reduced current. Transmitter output voltage switch adjustable for smaller loops. Value of loop resistance read from front panel meter; resistance must be greater than 1 ohm on lowest voltage setting to prevent overload. Transmitter circuit breaker protection against input overprotection voltage: instantaneous solid state protection against output short circuit; automatically resets on removal of short circuit. Input voltage, output voltage and current indicated on front panel meter. 150 volts (zero to peak) maximum; Transmitter output voltage 20 volts (zero to peak) minimum

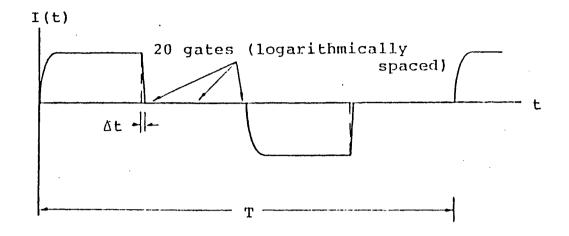
- Transmitter output power
- 2.8 kw maximum
- Transmitter wire supplied
- 1800m. #10 copper wire PVC insulated with nylon jacket; transmitter wire contained on 6 reels (supplied); 2 reel winders supplied.
- Transmitter motor generator
- 5 HP Honda gasoline engine coupled to 120 volt, 3 phase, 400Hz alternator. Approximately 8 hours continuous operation from full (built-in) fuel tank.

# Receiver

111

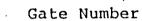
Measured quantity time rate of decay of magnetic flux along 3 axes. Sensor air-cored coil of bandwidth 40 kHz; 100cm dia. by 7x5cm cross-section. Coil holder supplied to facilitate measurement along 3 axes. Time channels 20 time channels with locations and widths as shown in Fig. 2. Successive operation at 30Hz, then 311z, effectively gives 30 channels covering range from 80 µsec. to 80 msec. Output display 4 digit plus sign LED display; display also shows channel number and gain.  $2^{n}$  cycles at 30Hz; n=4,6,8,10,12,14 (switch Integration time selectable); similar integration times at other base frequencies. Receiver output noise typically  $1.5 \times 10^{-10}$  volt/m<sup>2</sup> at last gate at 30Hz referred to input with integration time of 34 seconds. Noise will be higher during intense local spherics activity. Jutput connector all 20 channels in analogue format and housekeeping functions in digital format available from output connector. Synchronization to any of the following (switch selectable) Txreference cable (1) primary pulse (2) 27 MHz radio link (40 channels) (3)(4) high stability (oven controlled) quartz crystals. Selective clipping of atmospheric noise pulses Noise rejection circuitry at all times. Audio output of Rx coil (transmitter pulse blanked out) is available on builtin loud speaker for ready identification of interference.

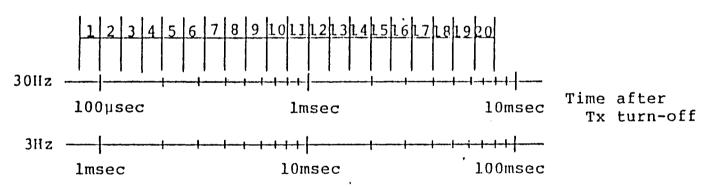
Receiver batteries - 12 volt rechargeable Gel-cell; 9 hours continuous operating time at 17°C. Two batteries and a battery charger supplied to permit charging of second battery from transmitter motor-generator during survey.



Transmitter Current Waveform

FIG. 1





Gate Location and Widths (30 and 3Hz)

FIG. 2

# GEONICS LIMITED

# DAS 40 Data Acquisition Unit Technical Specifications

Storage medium - special low-temperature Philips-type

cassette

Maximum storage - 212 kilobytes

Data format - 2 channel NRZI

Keyboard - two (sealed); one for header information,

one for numerals.

Display - 16 character alphanumeric LCD

Temperature range - -30°C to +60°C (operating)

Power source - power taken from EM37 receiver console

Dimensions - 16x23x21 cm

Weight - 2 kg

# GEONICS LIMITED

# Datel LPR 16 Tape Reader Technical Specifications

GENERAL Function Read Only
Media Standard Philips-type certified digital
tape cassette
Number of Tracks Two
Tape Motion One direction, capstan stepper motor
drive
Tape Speed 2.75 inches per second
Reading Format Complementary NRZI
Reading Density 615 bits per inch
Bit Rate 1700 bits per second
Bit Capacity 2.2 million bits per cassette (including
ali gaps)
Word Length 8, 12 or 16 bits
Record, Word or
Intercharacter Gap 2 bits
File gap 16 bits
Words per File Any (Standard is 64 words per file)
Power Required 100, 115 or 230 VAC, 47 to 63 Hz,
60 Watts max.
LOGIC OUTPUT CHARACTERISTICS (Computer Interface)
Logic Levels TTL compatible
"0" - (LO) = 0 to +0.4 Volts
"1" = (HI) = +2.4V to +5.0 Volts
Output Loading , Optional Open Collector
7406 TTL Hex driver or with 1K!!
pullup to +5V
or with 330!1 pullup to +5V and 470!1
pulldown to ground
Output Coding Selectable positive or negative true
coding using Level Control Inputs.
LOGIC OUTPUTS (Computer Interface)
(All outputs are selectable as positive or negative true unless
otherwise nated.)
Data Format 16 lines: Normally 12 A/D lines and 4
address lines. However a 16 bit digital
word can also be used.
Word Sync Output 1 line
End of File (EOF) Output 1 line, normally flags every 64 words.
Rewind Status Output 1 line
Busy Status Output 1 line
Load Forward Status
Output 1 line
Cassette-in-Place Status
Output 1 line
Head Down Status Output 1 line
EOT/BOT Status Output fine
Shift Clock Output 1 line, positive pulse
Tape Clock Output 1 line, positive pulse

Serial Data Output . . . . . . 1 line, positive true, NRZI coding

LOCIC IND	IT CHADA	CTERISTICS IC	computer Interface)	
		TTL Con	•	
Codic Caseis			D) = 0 to +0.8 volts	
			I) = +2.0V ta +5.0 valts	
Input Loadii	n <b>g</b>		one TTL load, or 1 TTL	
		foad with	1K!L pullup to +5V, or	
		1 TTL lo	ad with 330!1 pullup to +5V	
		and 470!	l pull down to ground.	
LOGIC INP	UTS (Comp	uter Interface)		
Start Input		1 line, po	sitive true	
		1 line, no		
			•	
OUTPUT		OUTPUT	The output Level Control Inputs control	
CONTROL	. INPUTS	CODING		
1	2	CODING	the coding of most	
1	1	POS. TRUE	outputs as shown in	
1	0	NEG. TRUE	the chart — see the	
0	1	Jammed LO	listing of outputs.	
0	0	ONE'S'	*With both Output	
			Level Control Inputs at	

zero, most outputs whose coding is controlled by these inputs will have cutoff open collectors. In this state, external open collector devices sharing the same data buss lines as the LPR-16 may be multiplexed onto these lines.

# CONTROLS AND INDICATORS Power On/Off (Pushbutton

Switch)	Turns power on and off. Illuminates when power is on.
EOT/BOT (LED indicator)	Illuminates when on clear leader
Load Forward (Pushbutton	beginning of tape or at clear end of tape
Switchl	Depressed to cause tape to foad
	forward from clear leader to oxide portion of tape. (EOT/BOT lamp will extinguish over oxide).
Rewind (Pushbutton switch).	Depressed to cause tape to rewind to the beginning of tape clear leader.
Busy (LED Indicator)	Illuminates when the tape is in motion.
Rewind (LED Indicator)	Illuminates while tape is rewinding.
Run/Standby (Toggle Switch)	When in "RUN", tape will contin- uously read. When in "STANDBY" tape will read one file each time the START switch is depressed.
Start (Pushbutton Switch)	When in standby mode, this switch will cause one file to be read each time it is depressed.

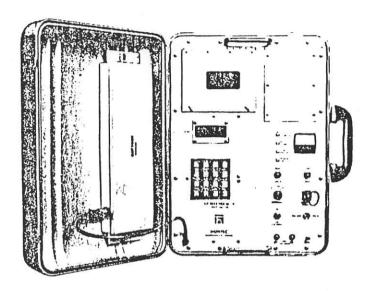
Size . . . . . . . . . . . . . . 19"W x 5:25"H x 19"D (16.25"

chassis width)
Connector Type . . . . . . Dual 25/pin PC Brd type, 0.1" Cen-

cluded with unit)

ters, Viking 3VH25/1JN-5 (1 in-

# M-4 Induced Polarization Receiver



### DESCRIPTION

The Huntec M-4 is a microprocessor based receiver for time and frequency domain IP and complex resistivity measurement. It is

Easy to operate. One switch starts a measurement, of up to 29 quantities simultaneously. The optional Cassette DataLogger records them all in seconds. Calibration, gain setting and SP buckout are all automatic.

Reliable. Using advanced digital signal processing techiques, the M-4 delivers consistently accurate data even in pisy, highly conductive areas. For mechanical reliability it is packaged in a rugged aluminum case for backpack or hand carrying.

Versatile. The operator may adjust delay and integration times, operating frequency and other measurement parameters, to adapt to a wide range of survey conditions and requirements. An independent reference channel facilitates drillhole and underground work, and guarantees transmitter-receiver synchronization in high-noise conditions.

Highly accurate. With a frequency bandwidth of 100 Hz and noise-cancelling digital signal stacking, the M-4 delivers very precise results. The details are summarized in a table overleaf.

Sensitive. The same features that make the M-4 accurate allow detection of very weak signals. The Huntec receiver requires lower transmitter power than any other, for a given set of operating conditions. Automatic correction for drifts in self-potential and gain allow long stacking times for significant signal-to-noise improvements.

Intelligent. Under the control of a powerful 16-bit microprocessor, the M-4 calibrates and tests itself between measurements. Coded error messages, flashed onto the display, inform the operator of any malfunction.

The M-4 Receiver is complemented by Huntec's new M-4 transmitters, which offer precisely timed constant-current output and both time and frequency domain waveforms, compati-

ble with the receiver's accuracy and multi-mode measurement capabilities. The RL-2 Reference Isolator connects any IP transmitter to the receiver's reference channel. The GeoDataBase field computer reads, stores and processes data from M-4 cassettes.

Contact Huntec for more information on the benefits offered by the M-4 product line.

## **FEATURES**

- Time and Frequency domain IP and Complex Resistivity operation
- Simultaneous Time domain and Complex Resistivity measurement
- Automatic calibration

gain setting SP cancellation

fault diagnosis

filter tuning

- Independent reference channel for drillhole and underground work
- 33 quantities, displayable on large 3½ digit low-temperature liquid-crystal readout
- Analogue meter for source resistance measurement
- 10° ohms differential input resistance
- 8 hours continuous operation with replaceable, rechargeable nickel-cadmium battery pack (2 supplied)
- Optional Cassette DataLogger fits inside case, has read-afterwrite error checking. Up to 350 stations per tape.
- Conveniently packaged for backpacking or hand carrying
- 100 Hz bandwidth, fine time-resolution
- Advanced digital signal stacking
- Delivers reliable, accurate data in noisy, highly conductive







JI LUINCALIO IS

Inputs Signal Channel

Range:

5 x 10<sup>-5</sup> to 10 volts. Automatic ranging.

Overload indication

Resistance: Bandwidth: Greater than 10' ohms differential

SP Cancellation:

100 Hz -5 to +5 volts (automatic)

Protection:

Low-leakage diode clamps, gas discharge surge arrestors, replaceable fuses.

Reference Channel

Level:

500 mV minimum, 10 volts peak max-

Resistance:

imum, overload indication 2 x 105 ohms differential

Controls and Functions **Operating Controls** 

Keypad:

16 keys, calculator format, function associated with each key.

Reference

Registers:

Keypad may be used to store up to ten 31/2 digit numeric values with floating decimal point, to represent station number, line number, operator, time, date, weather, transmitter current, etc. for recording on cassette.

**Programming Controls** 

Sub-panel:

All programming controls are on a covered sub-panel, not accessible during normal operation.

Thumbwheel

Switches:

Select delay time to in milliseconds, chargeability window t<sub>p</sub> in milliseconds; operating frequency; PFE frequency ratio.

Displayable Quantities

Time domain:

Primary voltage; self-potential; chargeability (total or each of 10 windows of equal width); phases of odd harmonics 3 to 15; amplitudes of odd harmonics 1 to 15; cycle count; repeating display of polarization potential and total chargeability.

Freq.domain:

Primary amplitude; Percent Frequency Effect; self-potential; cycle count.

Complex Resistivity: Phases of odd harmonics 3 to 15; amplitudes of odd harmonics 1 to 15; fundamental phase (with ref. input); cycle

Any mode:

Battery voltage, Frequency error.

Outputs Displays

Digital Display:

31/2 digit, low-temperature liquid crystal display. Indicates measurement results

and diagnostic error messages.

Analogue Meter:

Ohms scale for source resistance; also gives qualitative indication of signal-to-

noise ratio.

Cassette DataLogger (Optional)

Description:

Accommodated within M-4 chassis. If not acquired with receiver, may be retrofitted by user at any time. Two recording

Partial:

All sub-panel settings, measurement results, and contents of reference registers are recorded (2 seconds recording time).

Full:

As in partial mode, but also recorded is one cycle of averaged signal waveform (28 seconds recording time). If external reference is used, one cycle of reference waveform is also recorded (60 seconds recording time). Extra memory and software available to average and store the reference waveform for advanced offline

resistivity computation.

Format: ANSI/ECMA/ISO standard for saturation

recording: 80 bytes/record, all data re-

corded in ASCII code.

Verification:

Read-after-write data verification (auto-

matic)

Mechanical

M-4 Receiver with

battery pack: M-4 Receiver with battery

pack and Cassette

DataLogger: Replaceable

Battery pack:

Dimensions as above, 11.0 kg 33 cm x 11 cm x 4.5 cm, 3 kg

45 cm x 33 cm x 14 cm, 10.0 kg

**Environmental** 

Temperature:

Operation: -20°C to +55°C Storage: -40°C to +70°C

Humidity:

Moisture-proof, operable in light drizzle.

Altitude:

-1,525 m to +4,775 m

Shock, Vibration:

Suitable for transport in bush vehicles.

### **OUTPUT ACCURACY AND SENSITIVITY**

		1	14.5	Arm h		ligore.
	milliradians	volts	volts	volts	seconds	*
	2 milli- radians(1)	1% - 40Hz 2% to 80Hz	±1%	±1%	0.1%(2)	0 1%(3) full scale
	0.01 milliradians	10 <sup>-6</sup> volts	10-6 volts	10-) volts	10 - 1 seconds	0 001% full scale

1) Frequency domain mode: at harmonic frequencies up to 15 Hz, increases to not more than 5 milliradians at 80 Hz.

Time domain mode: at harmonic frequencies up to 7.5 Hz, increases to not more than 5 milliradians at 30 Hz.

2) of total OFF time

3) Full scale defined as 100% PFE.

Cassette Data: recorded in ASCII, 9 digits with decimal point fixed for four decimal digits.

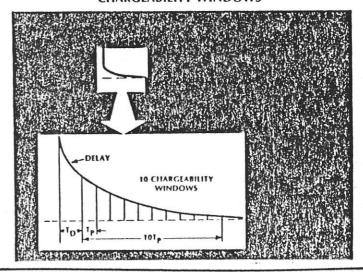
Display Data: 31/2 digits, floating decimal point

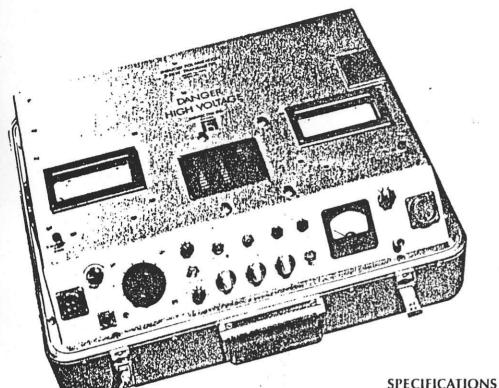
Resolution of averaged waveform limited by A/D converter to

one part or 4096 x (square root of cycle count).

Resolution of reference waveform (not averaged) limited by available memory to one part in 256. Additional memory and averaging software available as option.

## CHARGEABILITY WINDOWS





M-4 SERIES

# Induced Polarization/ Resistivity 2.5 kW **Transmitter**

# Mark-4 2.5 kW Transmitter

A) Power input:

96 - 144 V line to line 3 phase 400 Hz

(from Huntec generator set)

B) Output:

Voltage: 150 — 2200 V dc in 8 steps Current: 0.2 — 7 A regulated\*\*

C) Current regulation:

Less than ±0.1% change for ±10%

load change

D) Output frequency:

0.0625 Hz to 1 Hz (time domain,

complex resistivity)

0.0625 Hz to 4 Hz (frequency domain)

selectable from front panel

An additional range of frequencies between 0.78 and 5.0 Hz is available and can be selected by an internal switch.

E) Frequency accuracy:

±50 ppm -30°C to + 60°C

F) Output duty cycle: Ton/(Ton+Toff)

0.5 to 0.9375 in increments of 0.0625

(time domain)

0.9375 (complex resistivity) 0.75 (frequency domain)

G) Output current meter:

Two ranges: 0-5 A and 0-10 A

H) Ground resistance meter:

Two ranges:  $0-10 \text{ k}\Omega$  and  $0-100 \text{ k}\Omega$ 

I) Input voltage meter: 0-150 V

I) Dummy load:

Two levels: 500 W and 1.75 kW

K) Temperature range:

-34°C to + 50°C

L) Size:

53 cm x 43 cm x 29 cm

M) Weight:

26 kg

and overvoltage. Automatic regulation of output current eliminates errors due to changing polarization potential and load resistance.

Resistance measurement for load matching.

Precision crystal controlled timing.

The HUNTEC M-4 2.5 kW Induced Polarization

transmitter is designed for time domain, frequency

domain (PFE) and complex resistivity applications.

The unit converts primary 400 Hz ac power from

an engine-alternator set to a regulated dc output

current, set by the operator. Current regulation

eliminates output waveform distortion due to elec-

trode polarization effects. It is achieved in the trans-

mitter by varying the alternator field currents. The

transmitter is equipped with dummy loads to smooth

Solid-state switching for long life and precise timing.

Open circuit during the "off" time ensures no

Failsafe operation protects against short-circuit

\*\*Smaller currents are obtainable, but outside the current regulation range the transmitter voltage is regulated, not the current.

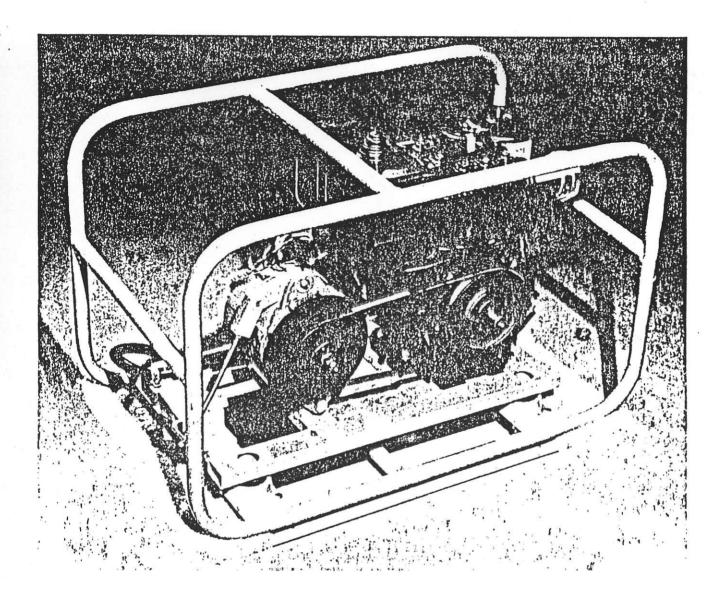
**FEATURES** 

DESCRIPTION

out generator load variations.

counter current flow.





# SPECIFICATIONS

# M-4 2.5 kW Engine Driven Alternator

Output:

120 V ac 400 Hz 3.5 kVA maximum

Engine:

6 kW air cooled, single cylinder four cycle piston engine with manual start

Fuel:

Regular grade gasoline, tank capacity 3.8 L to give 4 h duration

Alternator:

Delta connected heavy duty automobile type, belt driven, air cooled

Construction:

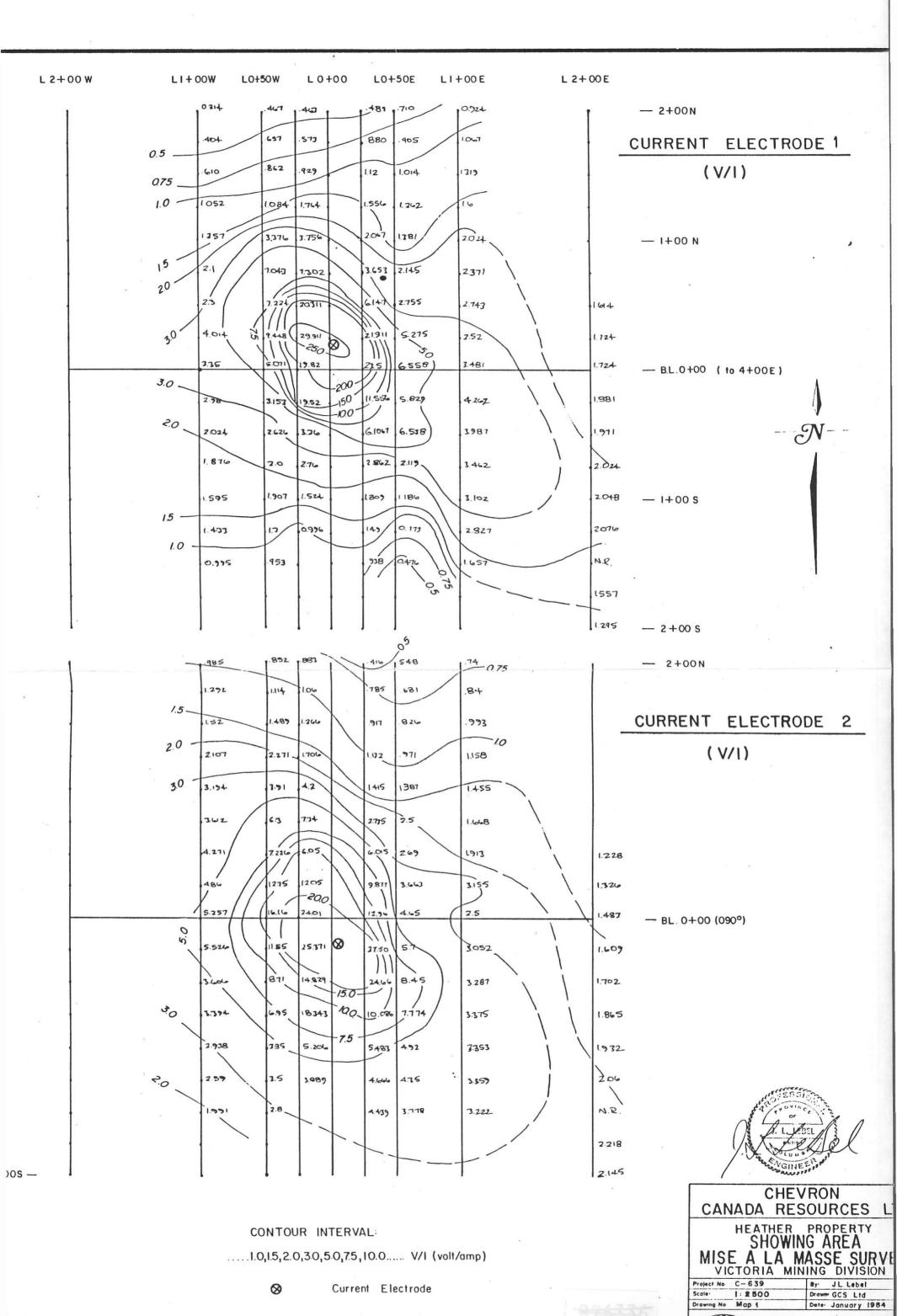
Tubular protective carrying frame with resiliently mounted engine and alternator

Size:

51 cm x 48 cm x 76 cm

Weight (dry):

61 kg



MPH MPH Consulting Limit