EXPLORATION PROPOSALS FOR THE CHUCHI LAKE PROPERTIES OF NATION RIVER RESOURCES LTD.

by Roy V. Beavon, Ph. D., P. Geo. February 1997

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EXPLORATION PROPOSAL FOR THE CHUCHI LAKE PROPERTIES OF NATION RIVER RESOURCES LTD., OMINECA MINING DIVISION, B.C.

by Roy V. Beavon, Ph.D., P.Geo.

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EXPLORATION PROPOSAL FOR THE CHUCHI LAKE PROPERTIES OF NATION RIVER RESOURCES LTD., OMINECA MINING DIVISION, B.C.

SUMMARY

The Company is the holder of mineral claims in the Intermontane Belt of British Columbia covering 14,000 hectares along the north shore of Chuchi Lake. A map depicting the location of this project within the Nechako lowland plateau is included herewith. The claimed area is centred on Lat. 55° 12' N, Long. 124° 30'W, and accessed by all weather gravel and logging roads 115 km from Fort St. James. This property consists of 32 claims and fractions that are beneficially owned by Nation River Resources Ltd. free of all encumbrance aside from statutory confirmation of the most recently acquired claims. The geology of the project area consists of Mesozoic volcanic, sedimentary, rocks of the Upper Triassic to Lower Jurassic Takla Group which are intruded by the Jurassic Hogem batholithic complex. The former are products of a weakly deformed and eroded Chuchi volcanic centre (or caldera) that is intruded by the latter. This volcanic complex is concentrically and radially faulted, tilted or down-sagged, and has been subjected to Pleistocene glaciation, so that the property is now mostly covered by glacial sands and boulder clays.

The subject claims are located in the Quesnel "trough", a geological province well known for its alkalic copper-gold deposits such as Similco, Afton, Mount Polley, and Mount Milligan (Fig.1). Other gold-bearing deposits of this belt include mesothermal sulphide veins of the Rossland mining area of southeastern B. C.. Exploration of the Chuchi Lake area commenced during the 1930s, and included prospecting, geological mapping, ground and airborne geophysical surveys, soil geochemical surveys, and diamond drilling. Some of this work was carried out by major mining companies that conducted initial drilling a silver bearing lead-zinc-barite vein known as the Wit prospect, which is now considered to contain a potential resource of over 1million tonnes containing 7.5% combined lead and zinc.

Since the acquisition of the project in 1987, Nation River Resources Ltd. has been responsible for $******* in exploration expenditures on the project area. In 1987-88 a limited program of prospecting, soil-, and rock-sampling was carried out, and

sampling, and diamond drilling. Trenching was continued in 1994, and in 1995 Westley Technologies Ltd. conducted an integrated program of sampling, trenching, and diamond drilling of the Wit prospect.

About 50% of the known previous drilling was targeted on geophysical (chargeability) anomalies found to be caused by fracture-controlled barren pyrite, but two out of at eleven BP Canada Exploration drill holes encountered interesting widths of low-grade copper enveloping potentially high-grade precious metal veins. In addition to the vein and porphyry targets there are several occurrences of chalcedonic epithermal breccias containing copper-zinc-silver-gold mineralization, two of which have received limited drilling. The chalcedonic breccias may be associated with concentric and radial fractures coincident with an arcuate faulted southern boundary of the Chuchi volcanic centre which, following its reactivation by early Tertiary faulting, predetermined the glacial excavation of the Chuchi Lake bed. Since the geochemical anomalies in the eastern part of the project area lie `down-ice' of the arcuate Chuchi Lake fault system it is possible that soil geochemical anomalies in the eastern part of the property are related to these fault-controlled epithermal breccia bodies. Similarly some of the geophyscal (chargeability) anomalies in the eastern part of the property may be due to intrusions emplaced along the strike continuation of the Chuchi Lake fault system.

The exploration results of Nation River Resources Ltd. at Chuchi Lake justify an initial program (`Phase 1') of additional soil geochemical sampling at 50 m grid spacing, limited ground geophysical surveys, overburden drilling, trenching, and diamond drilling in order to test a number of targets over selected parts of the property: including the more advanced Wit prospect (1800m diamond drilling); and the veins and breccias of the Skook West Zone and central area (500 m drilling) for a total budget of $533,000, to be followed by a `Phase 2' program composed of contingent of diamond drilling.

EXPLORATION PROPOSAL FOR THE CHUCHI LAKE PROPERTIES OF NATION RIVER RESOURCES LTD., OMINECA MINING DIVISION, B.C.

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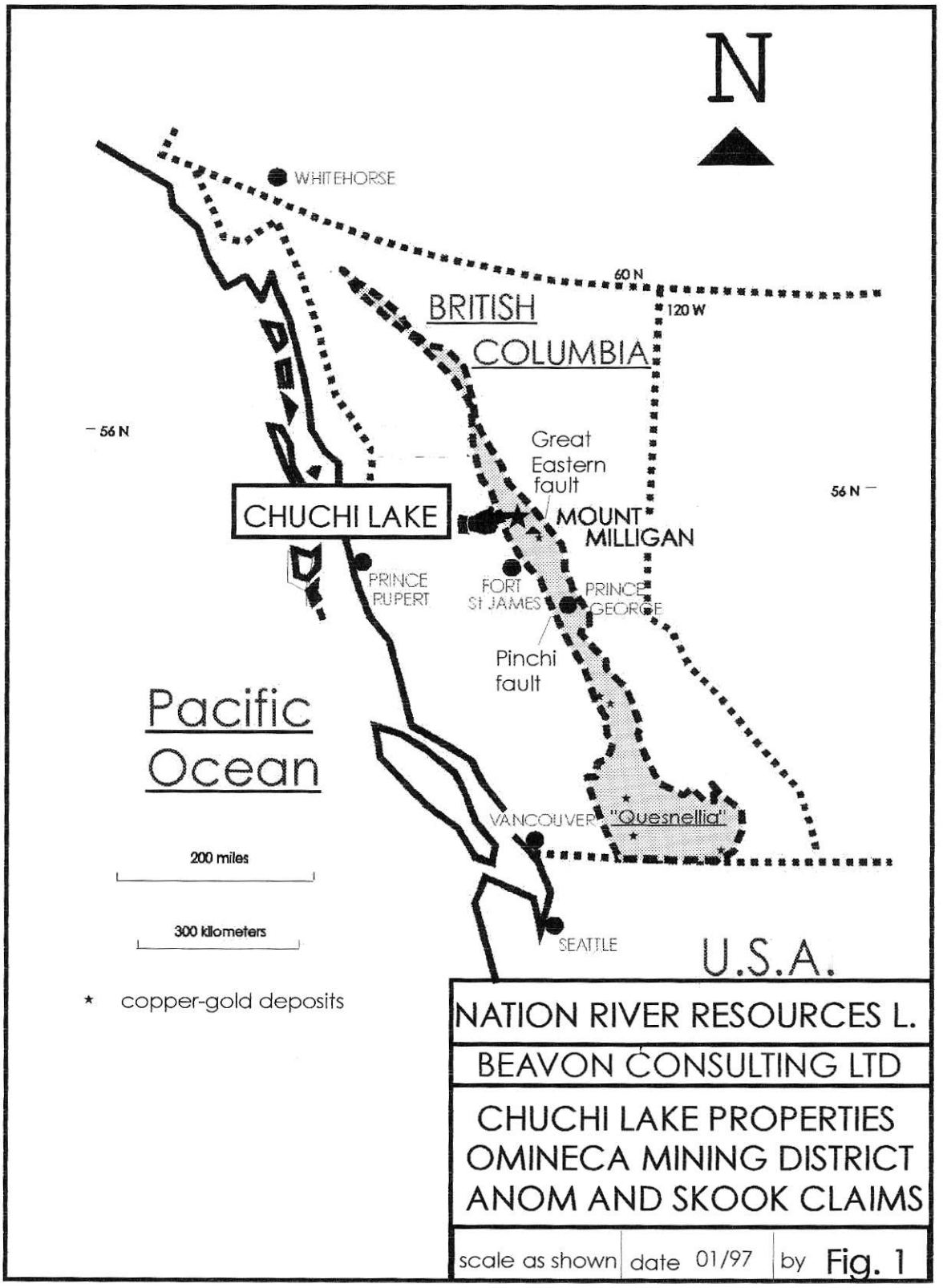


NATION RIVER RESOURCES L.

BEAVON CONSULTING LTD

CHUCHI LAKE PROPERTIES
OMINECA MINING DISTRICT
ANOM AND SKOOK CLAIMS

scale as shown	date 01/97	by Fig. 1

EXPLORATION PROPOSAL FOR THE CHUCHI LAKE PROPERTIES OF NATION RIVER RESOURCES LTD., OMINECA MINING DIVISION, B.C.

INTRODUCTION

The Chuchi Lake property is located within the Cordilleran Intermontane Belt 115 km north of fort St. James in north-central British Columbia (Fig. 1). Interest in this area stems from the nearby discovery of a large low-grade copper-gold deposit amenable to low cost open-cut mining near Mount Milligan, 15 km to the southeast of Chuchi Lake. The Chuchi Lake property contains previously drilled copper-gold and lead-zinc-barite prospects which were found as a result of prospecting that commenced in the 1930s. Exploration has continued intermittently since that time, with changing emphasis reflecting the development of geological concepts, exploration methods, and other discoveries made in the region. This report, prepared at the request of Mr. Colin Campbell of Nation River Resources Ltd., outlines the potential for volcano-tectonic precious metal and base-metal targets in a geological setting mostly explored for low-grade porphyry style deposits.

LOCATION AND ACCESS

The Chuchi Lake property is located in the Nechako Plateau of British Columbia between elevations 868 m and 1150 m. The claims are centred on Latitude 55° 12' N and Longitude 124° 30' W, within the Omineca Mining Division, and are recorded on Provincial claim maps NTS 93N/1E/2W. The property accessed by driving 110 km north of Fort St. James on the Manson Creek gravel highway, and by 14 km of good quality logging roads (Fig. 1). The terrain conditions of this area permit cost-effective exploration and development programs, and provide poorly drained areas suitable for mill-sites, tailings-disposal, and reclamation.

PROPERTY OWNERSHIP

The attached claim schedule (Table 1) enumerates the mineral claims held by Nation River Resources Ltd. along the north shore of Chuchi Lake, and indicates their status at the time of writing. It is a large claim block 30 km long by 5 km

Table 1 : Claim Schedule for the Chuchi Lake Property of Nation river Resources Ltd, Omineca Mining Division, B. C.

Claim Name	Mineral Tenure No.	No. of Units	Expiry date
Skook 1	330521	20	Sept . 4 1998
Skook 2	330522	20	Sept. 3, 1998
Skook 3	239657	20	Sept. 2, 2001
Skook 4	29658	15	Sept. 2, 2001
Skook 5	239659	10	Sept. 2, 2001
Skook 6	239660	18	Sept. 2, 2001
Skook 7 (Fr)	300340	3	June 10, 2001
Skook 8	331136	18	Sept.15 1999
Skook 9	331137	20	Sept. 18,1999
Skook 10	332496	20	Nov. 3, 1998
Skook 11	332497	18	Nov. 4, 1998
Skook 13	333092	20	Dec. 16, 1997
Skook 14	333095	20	Dec. 16 1998
Skook 16	242536	15	July 21, 2001
Skook 17	301702	10	July 14, 2001
Skook 21(Fr)	338473	1	July 17, 2001
Skook 22	347081	20	June 3, 1997
Skook 23	347082	20	June 4, 1997
Skook 24	347083	20	June 3, 1997
Skook 25	347084	20	June 4, 1997
Skook 26	350753	20	Sept. 4, 1997
Skook 27	350754	20	Sept. 23,1997
Skook 28	351907	20	Oct. 4, 1997
Skook 29	353157	20	Dec. 9, 1997
Skook 30	353158	20	Dec. 12,1997
Skook 31	353161	20	Dec. 12,1997
Skook 32	353162	20	Dec 13,1997
Anom 1	242243	20	June 20 1997
Anom 2	242244	20	June 18,1997
Anom 3	242245	12	June 19,1997
Anom 4	242246	12	June 19,1997
Anom 5	242460	18	July 14,1997

wide consisting of 560 contiguous units, and comprising 14,000 hectares (34,594 acres) known as the Skook and Anom claims. Figure 2 is a faithful reproduction of M.M.P.R. NTS areas 93N/1E and 92N/2W claim maps showing the Skook and Anom claims in relation to topographic features and other claims. The mineral rights to this tract are 100% beneficially owned by Nation River Resources Ltd. of *Vancouver, B. C., and are free of encumberance save for the statutory 12 month period allowed for disputation of claims less than 12 months old.

PREVIOUS WORK

Prospecting of the Chuchi Lake area commenced during the 1930s when George Snell found a copper-gold bearing breccia that was later rediscovered in the 1950s by Bill Rig of Prince George. Ted Taylor and George Snell also found an important barite-sphalerite-galena showing in the 'thirties, later staked as `the Wit prospect' by the former in 1964. In 1965 Noranda Exploration Co. explored the western part of the Skook claim area by Crone JEM geophysical survey, geological mapping, trenching , and sampling. At least five `Ax' diamond drill holes were put down on the Wit at this time, and a resource estimate of 20,000 short tons (Botel 1965) grading 7.5% combined lead and zinc was estimated. Elsewhere on the property previous drilling by Noranda Exploration Co. (1989) is occurred on the present Skook claims #2 and #3. Anomalous concentrations of copper were found in the soils north of Chuchi Lake, by both Noranda and by Colin J. Campbell, following silt surveys of drainage channels. The Wit prospect was subsequently explored by Royal Canadian Ventures Limited utilizing geological mapping, soil sampling, and an Induced Polarization survey. A ground magnetometer survey was also conducted in the eastern part of the property.

Nation River Resources Limited initially acquired the Skook 3-6 claims in 1987, and commenced prospecting for gold with a limited program of prospecting, soil sampling, rock-sampling, and hand trenching. Gold values up to 13.4 gm/tonne Au were found with copper and silver values in bedrock veins in hypabyssal intrusions and altered volcanic members of the Takla Group. In 1990 BP Canada Resources Ltd. optioned the Skook claims (and formerly adjoining Goldfinger and Klaw claims that were subsequently added to the Chuchi Lake property of Nation River Resources Ltd.) and conducted 210 line-km of helicopter-borne magnetic, electromagnetic, and VLF-EM surveys. In 1991, 76 line-km of survey grid was established, followed by 66 kms of Induced Polarization and Resistivity surveys,

the collection 1250 soil samples, together with geological mapping and 1243 metres of `Bq' diamond drilling. Two holes were partly completed at the Wit prospect, and the remaining 11 holes tested IP anomaly peaks with disappointing results.

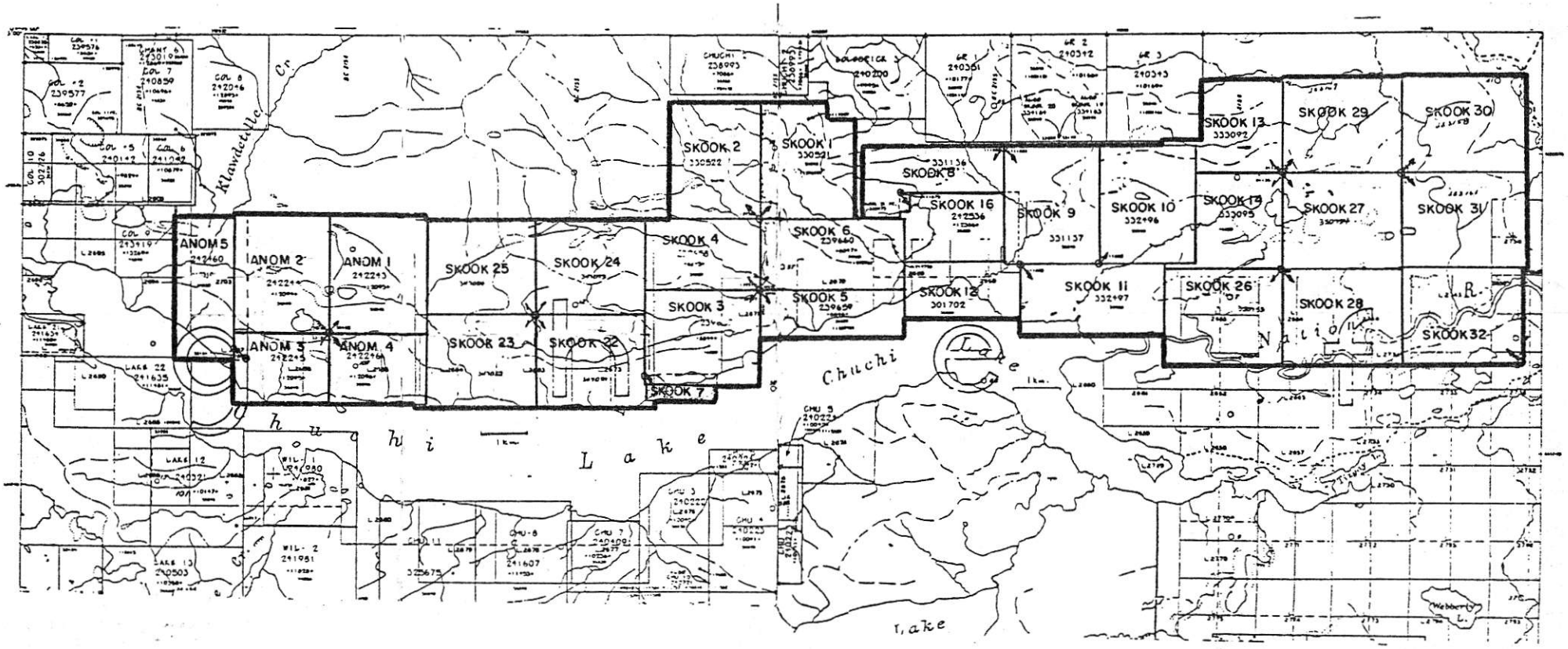
Following the return of the property to Nation River Resources Ltd., a mechanical excavator was employed in 1994 to dig 19 trenches at the Wit prospect. Additional discoveries of lead-zinc, silver, and barite were made, including 12.14% combined Pb-Zn and 34.8 gm/tonne Ag for a width of 5 metres in nearby overburden covered area. As a result the Chuchi Lake property was optioned to Wesley Technologies Ltd. and the Wit prospect was subjected to an integrated program of soil sampling, trenching, followed by a 5 hole, 736 m diamond drill program conducted in 1995. The zone was found to extend considerably further to the east of Noranda's 1965 drilling

REGIONAL GEOLOGY

Large tonnage low grade copper-gold deposits occur throughout Quesnellia (Fig. 1), which is considered to have been an island arc near the edge of a Mesozoic ocean. These mineral deposits are associated with intrusive complexes that represent the magma-chambers of eroded central volcanic complexes. One of these centres is known as the Mt. Milligan deposit of Placer Dome, which lies 15 km southeast of the subject claims, and contains about 300 million tonnes of 0.45 gm/t Au and 0.22 % Cu (Sketchley et al. 1994). Other types of copper-gold deposits also occur in Quesnellia such as the fissure -veins of the Rossland mining district in southern B.C., where individual vein systems of the Leroi-Centre Star deposit produced 1.699 million ounces (58,255,795 gm) of gold.

Regional mapping by geologists of the B.C. Ministry of Mines and Petroleum Resources (Nelson et al., 1991, 1992) show the bedrock of the Chuchi Lake area to be composed of Upper Triassic and Lower Jurassic volcanic formations of the Takla Group which are preserved in a wide graben, known as the `Quesnel Trough', bounded to the west by the Pinchi fault, and to the east by the early Tertiary Great Eastern fault (Fig 1).

The Takla Group consists of volcanic formations with intercalated volcanogenic sediments that were laid down in the late Trias and early Jurassic. It is intruded



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NATION RIVER RESOURCES LTD.	
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CHUCHI LAKE PROPERTY CLAIM MAP ANOM and SKOOK CLAIMS	
0 1 2 4 8 KM.	
SCALE: AS SHOWN	DATE: JAN. 1997.
DRAWN BY: R.B.	FIGURE No.: 2

by Lower Jurassic and Cretaceous plutons, and has suffered variable degrees of alteration, deformation, and faulting. The oldest formation of the Takla Group in the Chuchi Lake area is informally known as the Inzana Lake formation which occupies the northwestern and southwestern parts of the region (Fig. 3). It consists of volcanic sandstone', siltstones, mudstones, argillites, lapilli tuffs and bedded breccias, which locally pass laterally into the overlying Witch Lake formation.

The Witch Lake formation, consisting of between 500 m and 5 km of monotonous agglomerates and lapilli-tuffs, is largely made up of augite porphyries, and covers an area of about 1000 sq. km. (Nelson 1991). These volcanic deposits are believed to have accumulated from fissure eruptions south of Chuchi Lake, whereas a sunken central vent is suggested by the arcuate trace of the Chuchi Lake fault and the dip and strike of these formations north of the Chuchi Lake property (Figs. 3, 4a, 4b).

The Witch Lake formation is overlain more or less conformably by 1650 m of the Chuchi Lake formation, which is the youngest member of the Takla Group exposed in the region. It is composed of heterolithic Lower Jurassic breccias and subsidiary maroon lavas, including latite and trachyte flows which probably resulted from the terminal activity of the Chuchi volcanic centre. The breccias, which are considered to be 'lahars' (volcanic mud-flows) that may have spalled off the structural boundary of the subsiding centre, are intercalated with fossiliferous sandstones and thin-bedded siltstones that outcrop within the proposed caldera structure, inside and outside the subject claims (Fig. 3).

The western part of the Chuchi Lake area is underlain by the early Jurassic Hogem intrusive complex which consists of monzonitic and syenitic intrusions of batholithic dimensions, as well as satellitic stocks, and dikes. Radiometric determinations of the age of these intrusions suggest they represent the magma chamber of the Takla Group lavas (Garnett 1978).

Sandstones , mudstones, coal, pebble conglomerates, and basaltic flows, and a 19 m horizon of volcanic ash containing an early Tertiary flora (Nelson et al. 1991) ,overlie the Mesozoic formations in some places, but have mostly been removed by erosion. These deposits are present in areas of subsequent down-faulting, such as

the eastern part of the region, where Tertiary cover is preserved in a northeasterly trending graben identified by drilling near Mount Milligan.

Wares (1971) considered that Chuchi and Tchlenko Lakes conceal regional sigmoidal dilatant `gash' zones developed as a result of wrench-faulting, which may have acted as a focus for subsequent magmatic and hydrothermal activity. This interpretation contrasts with Nelson et al. (1992) who consider the regional structure of the Chuchi Lake area to be relatively simple, with few faults, and only one regional fold. Nevertheless the latter authority recognizes an easterly trending fault along the length of Chuchi Lake on the basis of northeasterly strikes to the southand east-west strikes to the north. This Chuchi Lake Fault may explain why a northwesterly trending regional anticline in the southern part of Fig. 3 does not appear further north. The displacements of the Chuchi Lake fault may have predated the emplacement of the Hogem intrusive complex because its coincident magnetic anomaly appears unaffected by the Chuchi Lake fault (Nelson et al. 1992).

The Chuchi Lake formation is gently warped into a broad depression centred near Chuchi Lake (see section, Fig.3). In spite of this structural simplicity there are occurrences of tight disharmonic folding within a thin-bedded sedimentary member of the formation further to the north. These inter-stratal folds may be explained by relative structural incompetence during gentle folding (Nelson et al 1991), but may alternatively have been produced by gravity gliding during volcanism, perhaps lubricated by relatively soft sediments sandwiched between massive flows. Such disharmonic folds commonly result from the development of a paleo-slope formed by volcanic `down-sagging' (Beavon 1997 *in press: cf* Walker 1984) of an older volcanic centre that formed the thick agglomerate pile of the Witch Lake formation. A possible early Jurassic volcanic sink of the order of 25 km in diameter is therefore suggested (Fig. 3). the evidence for which is further discussed below.

To the south of the proposed 'Chuchi volcanic centre' the steeply dipping Triassic and Jurassic formations were affected by regional tectonic folding and the formation of a north-plunging anticline with trending parallel to, and one km east of, the line of section south of Witch Lake (Fig. 3).

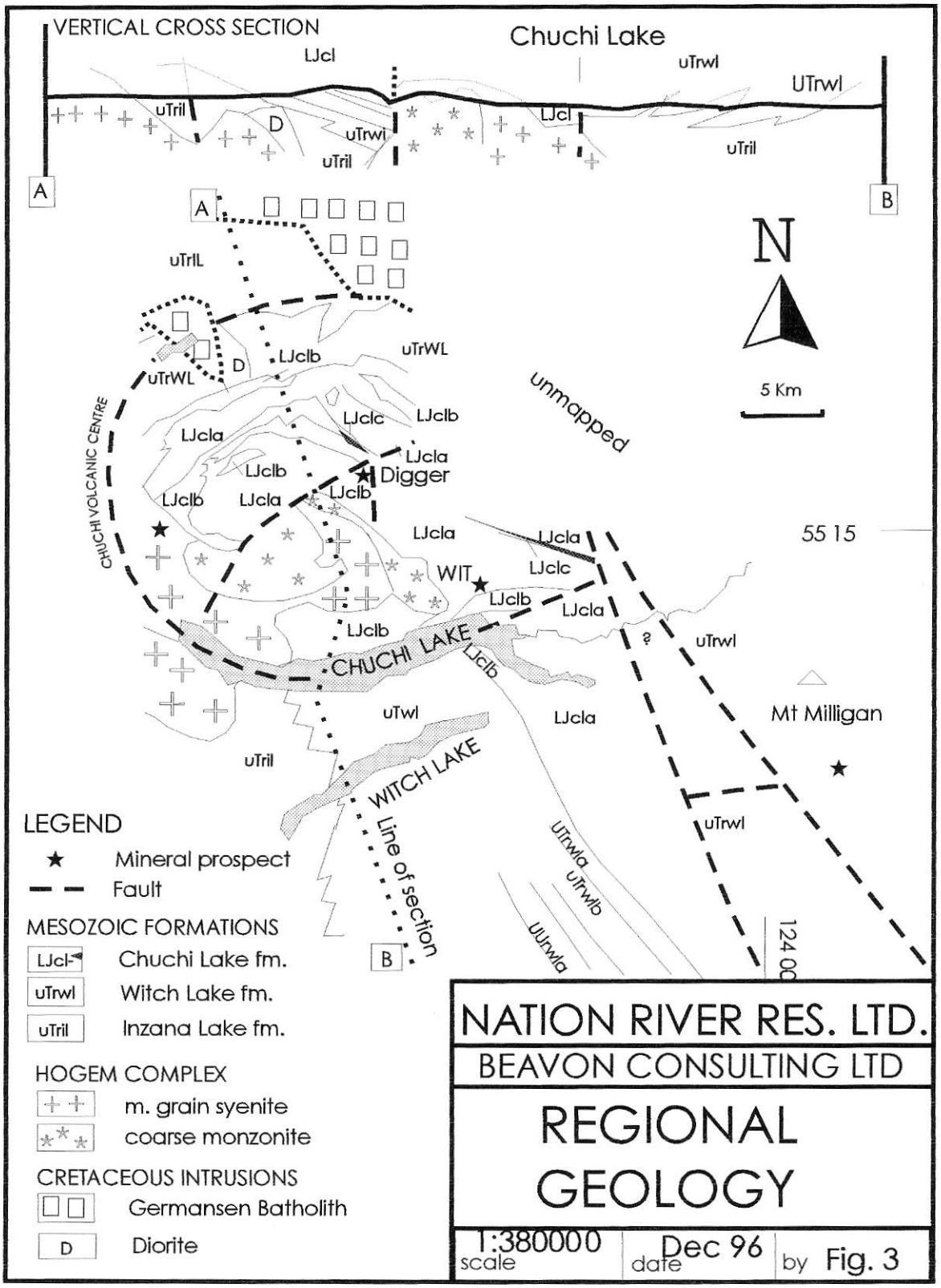
The sub-greenschist metamorphism of the Takla Group, which may be partly of sub-volcanic intrusive origin, may be attributed to the emplacement of both the Jurassic Hogem and Cretaceous intrusives such as the Germansen batholith (Fig. 3). The Mesozoic and Tertiary formations of the Chuchi Lake area are mostly covered by glacial deposits resulting from the Fraser Glaciation (Plouffe 1991). The latest advance of the ice sheet produced glacial grooves trending 060° and glacial striae striking east-northeast, but earlier glaciations may have followed different azimuths.

PROPERTY GEOLOGY

The Chuchi Lake property is underlain by the Chuchi Lake formation and the southeastern extension of the Hogem intrusive complex (Nelson et al. 1991, 1992) The following description is based on 1:10,000 mapping and drilling by BP Resources Canada geologists, supplemented by government regional maps, and airborne geophysical interpretation. Outcrop is sparse on the property and becomes scarcer towards the south and east, but the 'Calculated Vertical Magnetic Gradient Maps' (Appendix D) are useful in extending geological interpretation into adjacent unexposed areas (Yee 1991). Similarly the areas underlain by the Chuchi Lake formation may be differentiated from areas underlain by the Hogem intrusive complex by numerous dike-like magnetic signatures trending mostly north to south.

Stratigraphy: Due to the lack of continuous outcrop and faulted nature of the ground no detailed stratigraphy has been worked out for the Chuchi Lake property, but a 350 m thick, fossiliferous horizon of sedimentary and tuffaceous sediments occurs within the Chuchi Lake formation (`LJclc' of Fig. 3 = `3' of figs 4a and 4b). The ammonite fauna of these waterlain sandstones, black siltstones, and calcareous tuffs is considered to belong to the Pliensbachian Stage of the Lower Jurassic, and indicates marine conditions of sedimentation. These sediments, which are baked into hornfels adjacent to the Hogem intrusions, are therefore equivalent in age to sulphide-bearing sediments associated with the augite porphyries of the Rossland mining area (Nelson et al. 1991).

The southern and south-western parts of the Chuchi property are underlain by thick flows of green and maroon basalt, andesite, and latite (Unit 1 of Fig. 4), which may be vesicular, scoriaceous, or amygdaloidal in texture, and often include


VERTICAL CROSS SECTION
Chuchi Lake
LJcl
uTrwl
UTrwl
uTril
D
uTrwl
uTril
LJcl
uTril
A
B
A
N
5 Km
uTrlL
uTrWL
D
LJclb
uTrWL
unmapped
CHUCHI VOLCANIC CENTRE
LJclc
LJclb
LJcla
LJcla
LJclb
Digger
LJclb
LJcla
LJclb
LJcla
LJcla
55 15
WIT
LJclc
LJclb
LJcla
LJclb
CHUCHI LAKE
LJclb
?
uTrwl
uTwl
LJcla
Mt Milligan
uTril
WITCH LAKE
Line of section
uTrwl
uTrwla
uTrwlb
uTrwla
B
124 00
LEGEND
Mineral prospect
Fault
MESOZOIC FORMATIONS
LJcl Chuchi Lake fm.
uTrwl Witch Lake fm.
uTril Inzana Lake fm.
HOGEM COMPLEX
m. grain syenite
coarse monzonite
CRETACEOUS INTRUSIONS
Germansen Batholith
D Diorite
NATION RIVER RES. LTD.
BEAVON CONSULTING LTD
REGIONAL GEOLOGY
1:380000 scale
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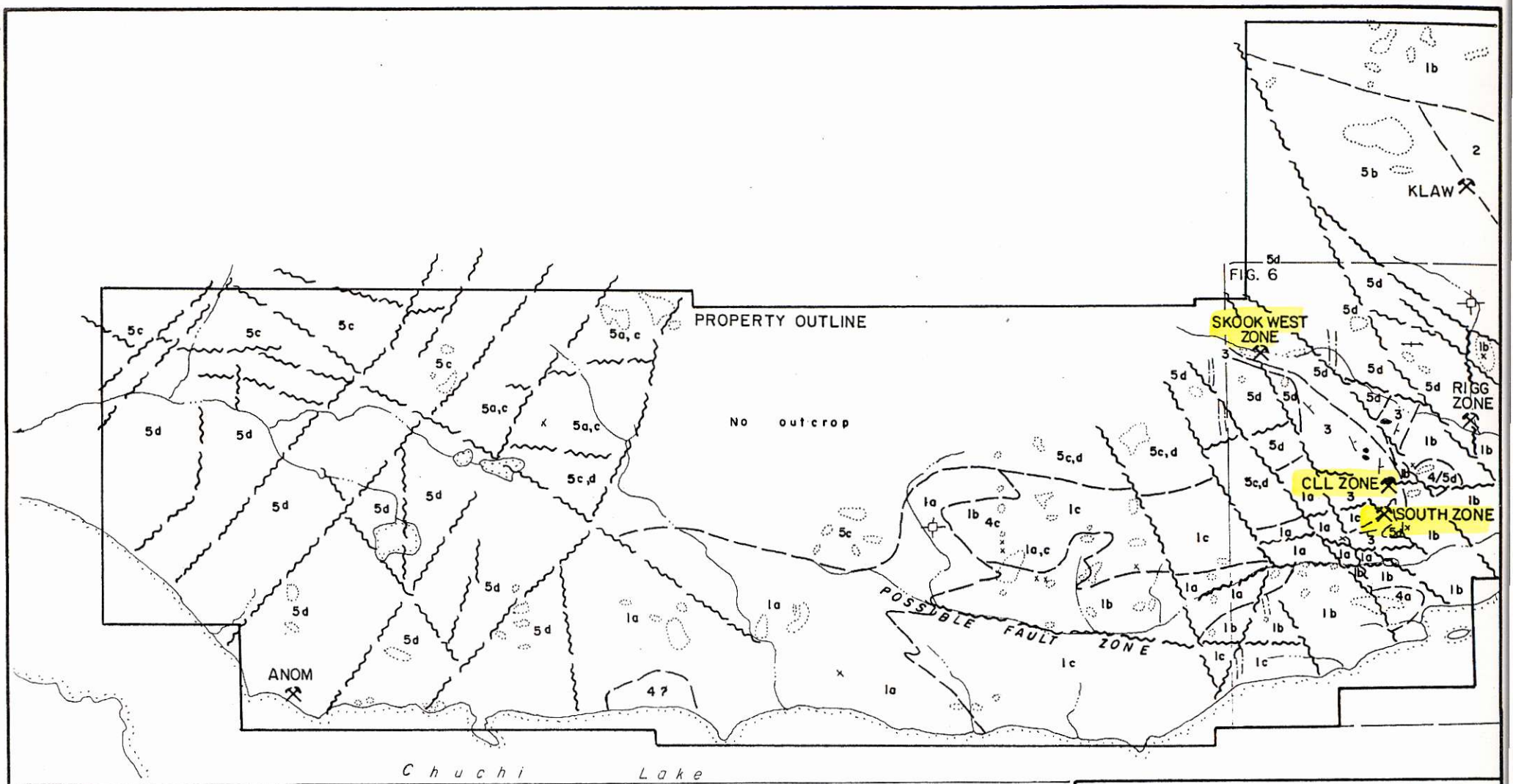
by Fig. 3



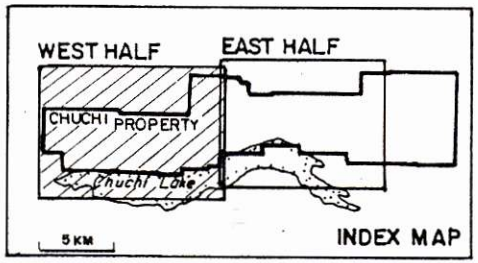
HOGEM INTRUSIVE SUITE

- 5a Syenite, quartz syenite, granite
- 5b Gabbro-diorite
- 5c Monzonite
- 5d Monzo-diorite
- 4a Monzonite porphyry
- 4b Monzo-diorite porphyry

TAKLA GROUP
Chuchi Lake Fm. (not in stratigraphic order)

- 3 Sandstone, siltstone, argillite (LJclc of Fig. 3) outcrop shown black.
- 2 Agglomerate
- 1 Basalt, andesite, latite
- 1a Augite porphyry
- 1b Plagioclase porphyry
- 1c Vesicular flows

- X Outcrop, small outcrop
- Inferred contact
- Inferred fault
- Bedding
- Foliation
- Showing
- Inferred dyke - Mesozoic or Tertiary



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CHUCHI LAKE PROPERTY
WEST HALF
PROPERTY GEOLOGY

0 1 2 3 KM.

SCALE: AS SHOWN	DATE: JAN. 1997
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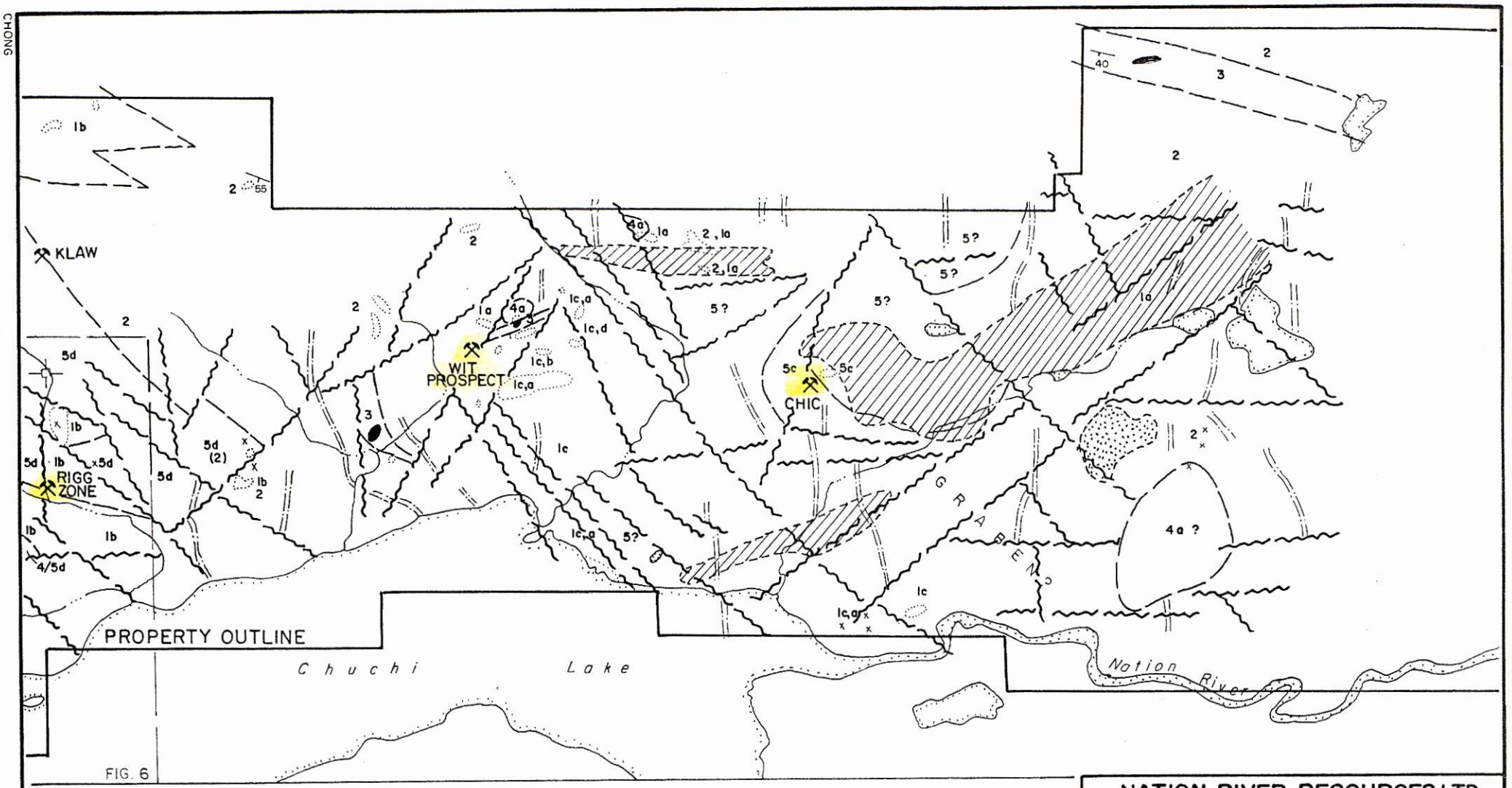
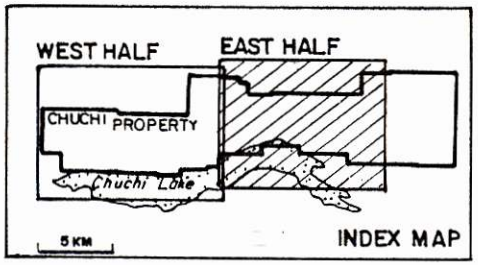


HOGEM INTRUSIVE SUITE
- 5a Syenite, quartz syenite, granite
- 5b Gabbro-diorite
- 5c Monzonite
- 5d Monzo-diorite
- 4a Monzonite porphyry
- 4b Monzo-diorite porphyry

TAKLA GROUP
Chuchi Lake Fm. (not in stratigraphic order)
- 3 Sandstone, siltstone, argillite (Lulc of Fig. 3) outcrop shown black.
- 2 Agglomerate
- 1 Basalt, andesite, latite
- 1a Augite porphyry
- 1b Plagioclase porphyry
- 1c Vesicular flows

Outcrop, small outcrop
Inferred contact
Inferred fault
Bedding
Foliation
Showing
Inferred dyke - Mesozoic or Tertiary
Multi-element geochemical anomalies (Ba, Pb, Zn, Ag)
Au enriched area



N

NATION RIVER RESOURCES LTD.

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CHUCHI LAKE PROPERTY EAST HALF PROPERTY GEOLOGY

0 1 2 3 KM.

SCALE: AS SHOWN	DATE: JAN. 1997
DRAWN BY: R.B.	FIGURE No.: 4b

related flow breccias and minor tuffs. The poorly exposed southeastern part of the Skook claims is underlain by heterolithic agglomerates, maroon flows, and flow-breccias of the Chuchi Lake formation (Unit 2 of Figs.4a and 4b). Some agglomerates are also maroon to maroon-grey in colour, and contain subrounded, angular, and rounded fragments of syeno-monzonite and diorite, crystal tuffs, and siltstones. The fragments range in grain-size form pebbles to sand and may have been deposited by lahars (Nelson et al. 1991), which are capable of transporting much coarser material. Fragments of intrusive lithologies suggests some of the agglomerates may be resedimented explosion breccias that were initially vented directly from an underlying magma-chamber.

Some geologists believe that the maroon flows came to rest under subaerial conditions, so that the marine conditions indicated by fossiliferous sandstones. black siltstones, and calcareous tuffs (Unit 3, Fig. 4) may be indicative of subsidence within a subaerial volcanic centre. Drilling in the central part of the property shows that these sediments contain moderate to heavy pyrite mineralization, notably along fractures. Their surrounding volcanic formations are more magnetic and exhibit weak propylitic alteration. Accordingly hornfelses and alteration haloes have been mapped around many of the intrusions (Nelson et al 1991).

Intrusions: The western and northwestern parts of the Chuchi property are underlain by the composite Hogem batholith (Unit 5) which consists of a series of monzonites gabbros and syenites, the most common of which are :(1) fine-to-medium-grained (leucocratic) plagioclase porphyritic monzonite with epidote, chlorite, and K-feldspar alteration (Unit 5d), and with phenocrysts of up to 2mm in length; (2) medium grained mafic diorite with K-feldspar, epidote and hematite alteration (Unit 5b); and (3) syenite and syeno-monzonitedikes (Unit 5a) striking east-southeast. The finer grained diorites may be confused with massive flows of the chuchi Lake formation and *vice versa*.

The Hogem intrusive complex forms a southeasterly trending body of unknown shape in the central part of the property (Unit 5 in Figs 4a,b), and may be concealed at a shallow depths further to the east, where it is identified by a relatively strong magnetic signature, alteration, and association with Induced Polarization anomalies.

On the Anom claims, at the western extremity of the property, the Hogem intrusions are medium and coarse-grained, and exhibit intrusive flow or cumulate texture formed by vertical pilotaxitic phenocrysts of plagioclase and/or hornblende striking norh to south. Coarser grained pegmatitic biotite syenites and medium to coarse monzonites occur further northeast.

In the north-central part of the property a foliated monzo-diorite exhibits a steeply dipping east-to west-striking foliation, parallel to the strike of a nearby broad magnetic gradient `low' suggestive of a fault zone : this foliation may be a local non penetrative structural feature unrelated to regional folding.

Porphyritic monzonite plugs containing hornblende and plagioclase phenocrysts (Unit 4) are known in several localities, and are often surrounded by low magnetic gradient anomalies. Magnetic gradient maps also indicate possible dikes striking mostly north to south in areas underlain by the Takla Group, but the age and nature of these dikes is unknown.

Structure: North of the Chuchi Lake property the strike and dips of the Chuchi Lake formation are respectively concentric and radial inwards, away from the northern boundary of the proposed volcanic centre (Fig. 3), and are discordant in relation to its proposed ring-faulted southern structural boundary. These observations suggest tilting or `downsagging' (Walker 1982) of the Chuchi caldera. Accordingly the Takla Group is tilted southwestward where the Pliensbachian sediments (LJclc of Figs. 3, 4a, and 4b) form a marker horizon outcropping in the northeastern corner of the property. These fossiliferous sediments are repeated by faulting in the central part of the of the property (Figs. 4a, 5).

The structure of the Chuchi Lake property is dominated by the Chuchi Lake Fault (Nelson et al. 1991) which separates the northwest striking Witch Lake formation to the south, from the east-to-west striking Chuchi Lake formation to the north. The eastward strike continuation of this fault probably underlies the poorly exposed eastern part of the claim block. Moreover, geological mapping and airborne geophysical surveys north and east of the lake suggest a fault system much wider than the lake itself. These faults may be viewed as a fracture zone that controlled the emplacement of the southern extremity of the Hogem intrusive complex (*cf.* Nelson et al. 1991,1992).

Magnetic gradient maps suggest that the outline of Chuchi Lake, which occupies an arcuate topographic valley, is closely related to faults striking both parallel to, and perpendicular to the length of the lake. Although airborne surveys tend to highlight cross-faulting at the expense of strike faults, it is suggested that Chuchi Lake is a glacially sculptured fault zone. Accordingly, in the western part of the property, where Chuchi Lake trends northwest, the dominant faults, which are defined by 500 m wide magnetic `lows' (Patterson 1991), also strike northwest. As indicated in Figure 3 the southern structural boundary of the proposed volcanic centre is probably represented by the Chuchi Lake fault system itself.

Lake-parallel faults in the central part of the property strike east-west and east-northeast parallel to the lake, and coincide with weak airborne conductors (*cf.* Humphreys 1991). In the eastern part of the property the displacements of these `lake-parallel faults' sometimes offset north striking dike-like magnetic features. Lake-parallel faults are cut and displaced by minor cross-faults inferred from the airborne survey results. Unlike the former faults, the latter are not associated with through-going magnetic troughs. As the `lake-perpendicular' cross-faults are traced from west to east their strike rotates gradually through an angle of 80 degrees from northeast to northwest, so that, when viewed as a group, they appear to radiate like the spokes of a wheel from a centre located north of the property boundary. Regardless of the airborne geophysical coverage (Fig. 6) the pattern of concentric and radial faults appears to be reflected throughout the property bya radial and concentric drainage pattern showing evidence of stream capture (Figs. 2, 4a).

In the east-central part of the property (Skook Claim # 16) several northwesterly striking `lake-perpendicular faults' appear to control the eastward termination of Chuchi Lake as well as the orientation of its southeast arm. In this area the airborne results suggests that the lake-perpendicular faults displace the lake-parallel faults. Both fault types are inferred to underlie the eastern part of the property, where northeasterly striking Tertiary faults similar to the horst and graben structure of the Mount Milligan mineralized area, were mapped by Nelson et al. (1991; *cf.* Richards 1976). `Block-faulting' and `block-rotation' is also mentioned in connection with the Skook claims (Barnes et al. 1991).

The geological significance of lake-parallel and -perpendicular faults of the Chuchi Lake property is that the floor of the lake may be interpreted as a glacially scoured, curved fault or fracture zone concave to the north. Such an arcuate feature, which is probably displaced by the northeasterly Tertiary block faults, may have originated as a volcano-tectonic structure of Triassic to Jurassic age (Fig. 3), constituting an important conduit for mineralizing fluids liberated during both the terminal Takla volcanism and/or plutonism of the Hogem complex. Thus the arcuate Chuchi Lake fault system, which throws the Chuchi Lake formation against the Witch Lake and Inzana Lake formations, may mark an outer ring fracture along the southern structural boundary of a Triassic-Jurassic basaltic, andesitic and latitic caldera. The lake-perpendicular faults, which converge northwards towards the Digger prospect, may be viewed as radial faults of the same centre. Experimental studies of caldera formation (Marti et al. 1994) suggest that radial fractures form as a result of pre-collapse doming. However in the Chuchi Lake area the cross-faults were probably reactivated during early Tertiary block-faulting.

The regional geological map (Fig. 3) shows a northwest trending Tertiary graben (Nelson et al. 1991) in the newly acquired eastern part of the Chuchi Lake property (*i.e.* Skook # 27, 29, 32 claims). And a similar feature, about 2 km wide is suggested by low magnetic gradient contours indicating greater depths to the magnetic basement (Fig. 4b) in the southeastern part of the property (Skook # 9, 10, 11, 26). This interpretation is supported by a float occurrence of fresh porphyritic basalt of possible Tertiary age east of the Chic showing (Fig. 4b) (C. Campbell personal communication).

MINERALIZATION

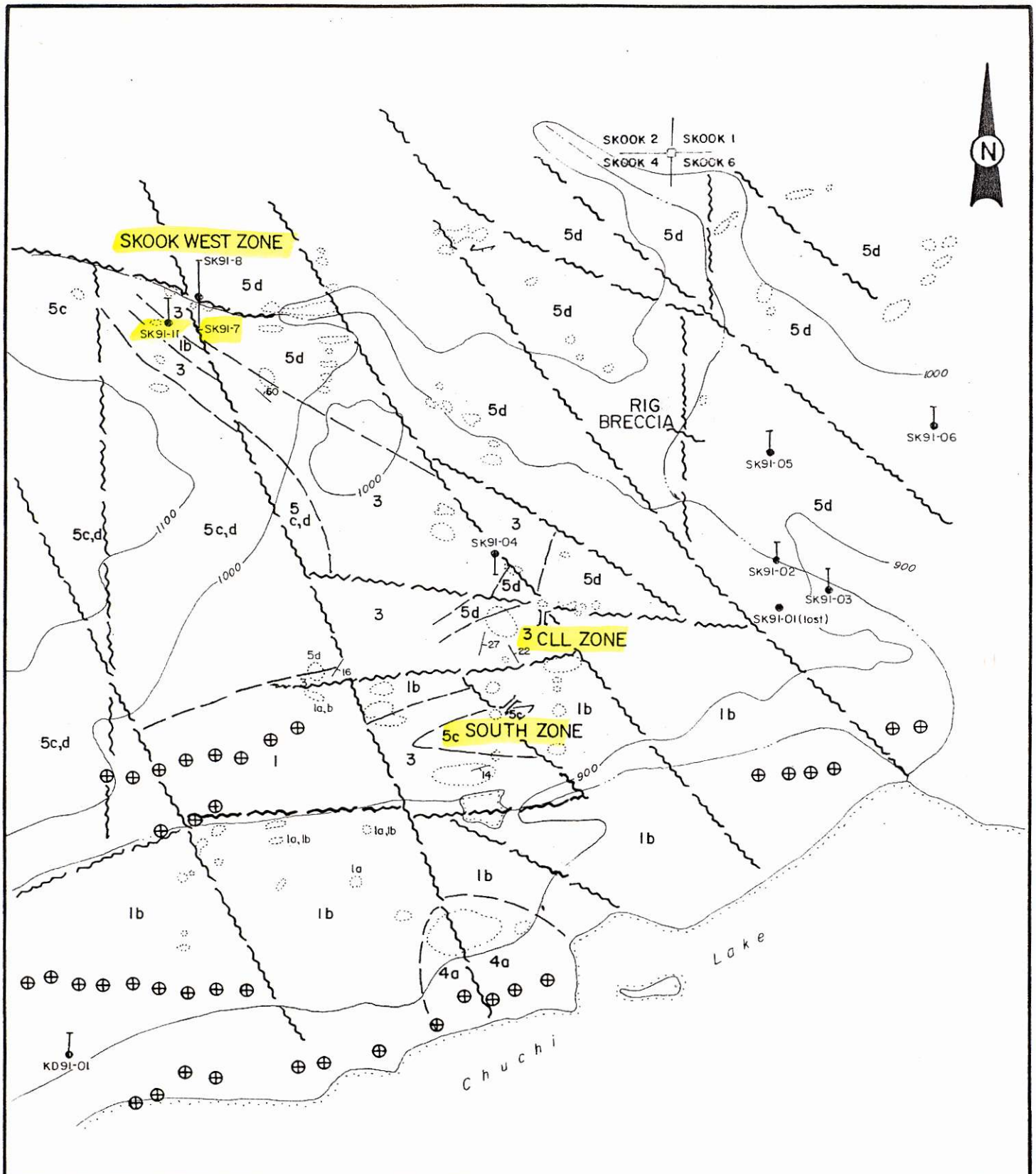
Several styles of sulphide and sulphate mineralization are known at the Chuchi Lake propety. In the central part of the Chuchi Lake property sulphides, such as pyrite and chalcopyrite, constitute up to 7% of the Pliensbachian tuffaceous and sedimentary beds intercalated with the Chuchi Lake formation, in addition to variable concentrations found by drilling the neighbouring volcanic formations and intrusive rocks. Such widespread mineralization, commonly classified as 'porphyry-type', contrasts with vein and breccia styles of mineralization found at many locations on the Chuchi Lake property.

(1) The Wit prospect (Fig. 8)

The most significant vein found to date on the subject property is over 600 m long , strikes east to west, and contains significant silver-zinc-lead and barite mineralization. This vein is known as the Wit prospect that occurs on Skook claim #9. In the past this mineralization has been regarded as satellitic to large-tonnage low grade porphyry copper-gold developments of the Mount Milligan and Digger deposits (Fig. 3). Airborne geophysical results suggest the Wit vein is coincident with a narrow magnetic trough similar to the faults that parallel the Chuchi Lake ring-fault, and offset magnetic trends suggest minor northeasterly and northwesterly oblique cross-faults. Such cross-structures may influence the location of higher grade mineralization in pitching `shoots'.

The Wit vein showings have been exposed by trenching, exposing steeply dipping, interlayered vuggy quartz and coarse-grained barite, fine-grained sphalerite, and galena, which drilling shows to occur along a steeply dipping fault-brecciated vein structure within massive mafic volcanic formations. The vein structure appears banded and crudely layered in outcrop, and exhibits colloform banding of chalcedony with numerous vugs suggestive of open-space filling, as found in epithermal precious metal deposits of the western U.S. (Berger and Eimon 1982; Plumtree and Whitehorse-Veaux 1994) and in some Mississippi Valley type lead-zinc deposits (Callahan 1965).. The layering of the Wit vein is locally disturbed by block rotation (or collapse), but it is uncertain whether the banding and contacts of the vein is parallel to the dip of the enclosing wall-rock formations (Fig. 9).

Trenching of the Wit vein has exposed considerable shearing, bleaching, and hematite alteration, some spectacular breccia sections, and drilling indicates a wide central zone of chalcedonic quartz . Some of the fragments of the Wit breccias are over 30 cm in diameter, and it is difficult to decide whether or not the original heterolithic volcanic breccias of the vein walls were permeated by sulphides prior to vein-formation. Sphalerite is usually yellow-brown in colour, and commonly carries cadmium credits normally occurring in Prime Zinc concentrates. Galena is usually coarser grained, occurring as fine to medium-grained dendrites of finely bladed crystals up to 7 mm in length, carrying silver values in the tens of ounces per ton.



HOGEM INTRUSIVE SUITE

- 5a Syenite, quartz syenite, granite
- 5b Gabbro-diorite
- 5c Monzonite
- 5d Monzo-diorite
- 4a Monzonite porphyry
- 4b Monzo-diorite porphyry

TAKLA GROUP
Chuchi Lake Fm. (not in stratigraphic order)

- 3 Sandstone, siltstone, argillite (LJclc of Fig. 3)
- 2 Agglomerate
- 1 Basalt, andesite, latite
- 1a Augite porphyry
- 1b Plagioclase porphyry
- 1c Vesicular flows

- Outcrop, small outcrop
- Inferred contact
- Inferred fault
- Bedding
- Foliation
- Airborne conductor
- Diamond drill hole
- Trench
- Creek
- Contour at 100m interval

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CHUCHI LAKE PROPERTY

GEOLOGY and DRILL PLAN CENTRAL AREA

0 500 1000 Metres

SCALE: AS SHOWN	DATE: JAN. 1997
DRAWN BY: R.B.	FIGURE Nº: 5

CHONG

Barite occurs as relatively large well-developed crystals and massive layers with `coxcomb' textrured vugs, and sometimes forms the matrix of sulphide breccia fragments (Harris in Campbell 1995). The latter are lined with colloform banded chalcedony typical of epithermal mineralization and, although gold values are recorded, its association with siliceous vugs remains to be demonstrated. The gold content of the Wit vein is low with the best assays (0.25 gm/tonne) occurring in the deepest drill intercept to date (Appendix C).

Aside from the breccias, textures of the Wit mineralization are comparable with the Bulldog Mountain silver-lead-zinc-barite-rhodochrosite vein system of the Creede district (Colorado), which is located outside the structural boundary of the Tertiary Creede caldera. The Bulldog Mountain vein is a branch of a larger vein-system where mineral zoning is developed over a vertical distance of 250 m (Plumtree and Whitehorse-Veaux 1994). It is therefore possible that branch veins and zoning may occur at the Wit prospect. On the other hand this prospect may not be just a simple fissure-vein, since further work is required to clarify its orientation in relation to its wall rocks: high-grade mineralization may have been milled into a fault breccia, or perhaps a previously unrecognized mineralized volcanic pipe, or source-bed, of the sulphide fragments may be present.

In southwestern Colorado lead, zinc, copper, gold, and silver mineralization took place in and near calderas showing complex histories of post-subsidence intrusive and extrusive activity. Most of the known ore occurs in veins or follows fractures that formed during different caldera cycles, and some may occur within intrusive bodies that were extensively mineralized (Steven et al. 1974). Gold-silver veins were worked along radial fissure zones in the Stunner -Gilmore and Platoro districts (Patton 1917). These deposits are mostly related to the youngest and most highly differentiated intrusives of a caldera cycle which would be equivalent to the porphyry stocks of the Chuchi Lake area. Elsewhere, in Pacific island arcs, important epithermal precious metal and porphyry copper deposits are associated with recent submarine volcanic centres of the Tabar-Feni island chain, Papua New Guinea which, as illustrated by the Lihir Island deposit, may contain up to 40 million ounces of gold (Herzig and Hannington 1995).

(2) The Skook West Zone (Figs. 4a, 5)

The Skook West Zone is a vein prospect discovered in 1991 by drilling near the northwest limit of an exploration grid which lies within the Skook #4 claim. Three drill holes in this locality contain low copper values, suggesting a possible porphyry style of mineralization. Two of the holes also contain precious metal-bearing veins formed by mesothermal and/or epithermal mineralization. The analytical results are shown in the logs of diamond drill holes SK - 07 and SK-11 (Appendix D).

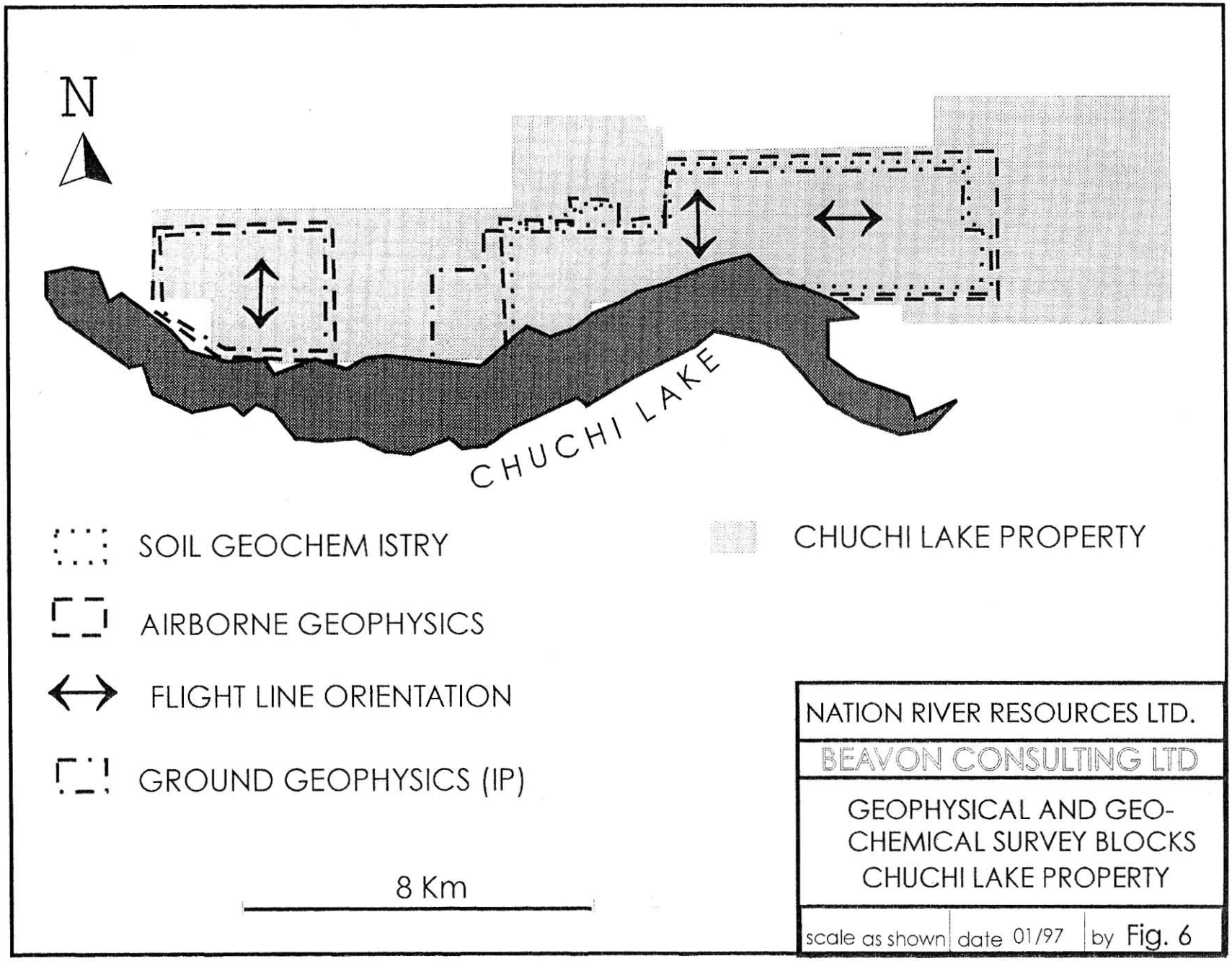
2m 2.4% Cu 3.7gpt Au

4m / 2.1% Cu, 1.2gm/t Au

The host structure of the Skook West mineralized zone consists of `late' quartz-veins, clay gouge, and shears, indicating a `lake-parallel' fault zone striking east-southeasterly along a creek bed. The length of the West Zone is unknown, but its strike-continuity may be indicated by an associated magnetic gradient `low', similar to the one associated with the Wit prospect. Although the magnetic `low' could mark the strike of a siltstone horizon intersected in diamond drill hole SK-11, the Skook West mineralized zone may be considerably longer than 100 metres, and is doubtless interrupted in places by cross-faults and dikes, as the `low' is traced east-southeast towards the central part of the property. Vein-structures of this type commonly form en echelon fissures that pinch and swell and show increasing grade adjacent to cross-faults and dikes, as for example in the Rossland mining district of southern B. C. (Drysdale 1915; Fyles, 1984).

(3) The central target area (Fig. 4a,b, and 5)

Southeast of the Skook West Zone three showings occur within a distance of 1200 m of one another in the central part of the property (Skook claims #3 and #4), in an area where Induced Polarization chargeability peaks were drilled by BP in 1991. This pyritic mineralization occurs within the Chuchi Lake formation, near the south contact of the Hogem intrusive complex, and is associated with faulting indicated by geological mapping and airborne geophysical surveys. From southwest to northeast the mineralized showings are known as the `South', the `CLL', and the Rig zones, but is not clear whether they are directly connected to one another by a continuous structure. Many of these mineralized showings, which returned encouraging assays in `grab samples', are associated with faults, chloritization, silicification, and tourmaline in quartz-lined vugs.


N
CHUCHI LAKE
SOIL GEOCHEM ISTRY
AIRBORNE GEOPHYSICS
FLIGHT LINE ORIENTATION
GROUND GEOPHYSICS (IP)
CHUCHI LAKE PROPERTY
8 Km
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GEOPHYSICAL AND GEO-CHEMICAL SURVEY BLOCKS
CHUCHI LAKE PROPERTY
scale as shown
date 01/97
by Fig. 6

(i) The Rig breccia was discovered by Bill Rig in the 'fifties and consists of a steeply dipping vuggy breccia which appears to follow a 290° striking gouge-zone containing zinc, copper, and gold values. It has been exposed in two trenches 25 m apart on opposite sides of a creek bed, with widths between 3m and 5 m enclosing a central clay-gouge zone 1.2 m wide. Sphalerite is the main sulphide, with minor galena, chalcopyrite, and anomalous silver and mercury. Analyses of 1 m wide samples from two trenches on opposite sides of a creek returned low base-metals and up to 21.8 gm/tonne Ag and 2.1 gm/tonne Au (Appendix C). The Rig showings have been interpreted as an example of epithermal mineralization (Campbell 1988) of unknown age, possibly related to a north-to south cross-fault indicated by mapping and the airborne magnetic results (Figs. 4b,5).

(ii) The CLL Zone, located 850 m southwest of the Rig zone, is a steeply dipping vein structure, 1 m wide that strikes 090°, and contains sphalerite, galena, chalcopyrite in a gangue of quartz . Assays returned 1.35% Zn, 6.4 gm/tonne Ag and 2.74 gm/tonne Au from a 1 m long continuous chip sample (Appendix C). The wall-rocks of the vein consists of chlorite and carbonate, and there are large outcrops of hornfelsic siltstones nearby. The airborne results suggest this showing is associated with radial and concentric faults of the Chuchi volcanic centre.

(iii) The South Zone is about 600 m southwest of the CLL vein, and is described as a silicified zone in andesite. It consists of a 1 m wide area containing secondary quartz,, calcite, pyrite, and chalcopyrite. A sample taken across 1 m returned 4.3 gm/tonne Au and 53 gm/tonne Ag (Appendix C). Further quartz veinlets with chalcopyrite remain to be investigated in this vicinity, which is associated with northwesterly minor faults belonging to the radial system described above. Moreover, since silicification is known to be an important prospecting guide for gold in epithermal and other environments the CLL zone merits further investigation.

(4) Porphyry prospects

Although many of the chargeability peaks of the IP surveys have been drill-tested, it is well known that porphyry targets may underlie areas of lower IP chargeabilities surrounded by high-chargeability 'pyrite haloes' so that several geophysical targets remain to be tested at Chuchi Lake (*cf.* Barrie et al. 1991),

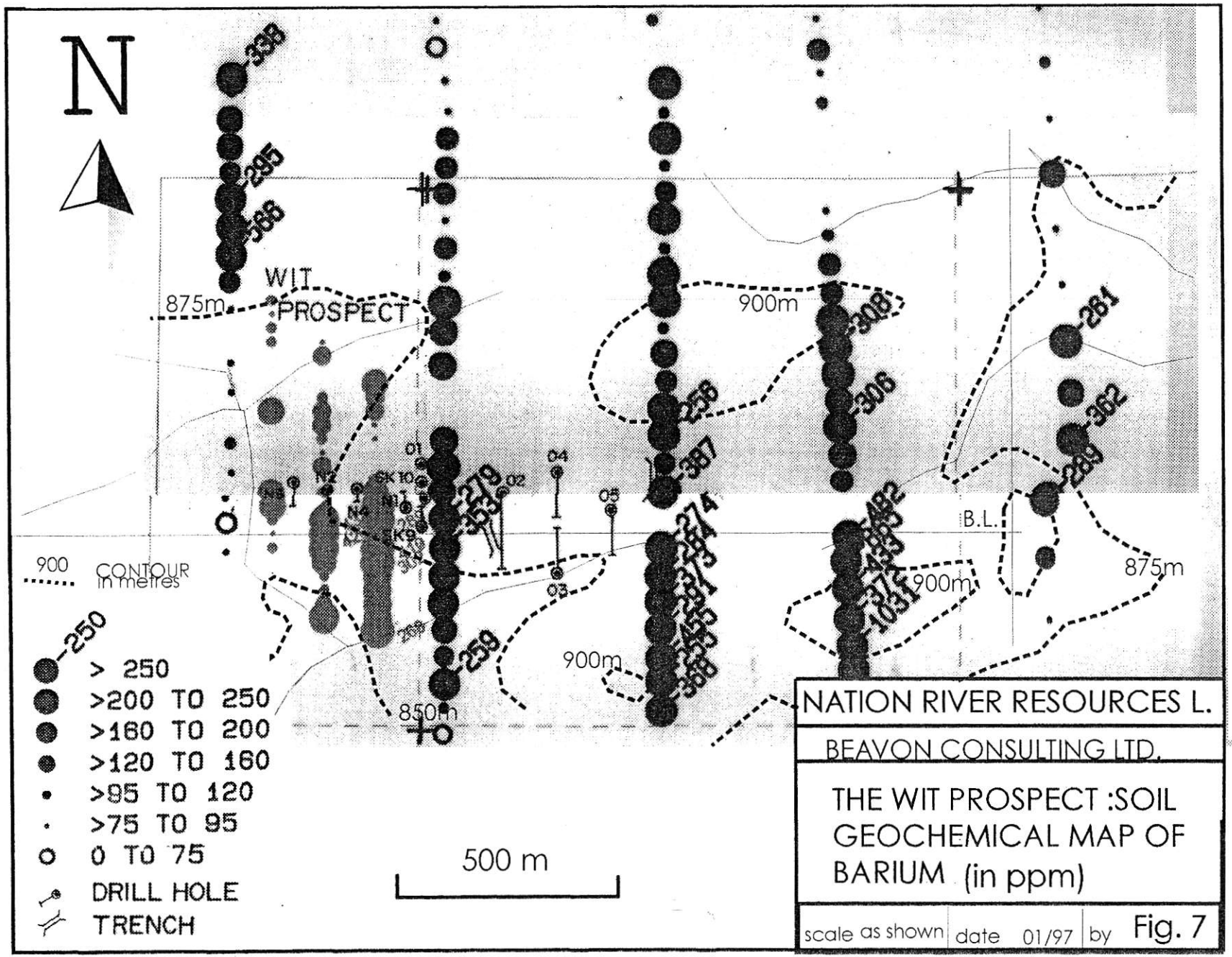
BEST HOLES 91-7 → 40 m Ave .32% Cu
91-11 → 6 m Ave .94% Cu

particularly in the heavily overburdened southeastern part of the property, where buried porphyry stocks are present along the structural boundary of the inferred Chuchi volcanic centre.. A single target was drilled at the Skook West Zone, as described below, but the mapping, airborne, and I.P results indicate intrusive stocks elsewhere on the property (Figs. 4a,b, Appendix D). Since many of the I.P. anomalies have been drilled without encountering true porphyry style mineralization, the geophysical targets are included in Appendix (D), and are subject to later review pending the results of the proposed program.

(5) Other showings listed in Minfile (Figs 4a,b)
Four mineral occurrences are listed by Minfile of the Geological Survey Branch - Mineral Resources Division M.M.P.R. Victoria are named the Klaw (Cir, Srm), Anom (Pot,Tom), and Chic showings. The Anom is a small occurrence of chalcopyrite in the Hogem intrusive complex near the northwestern shoreline of Chuchi Lake on the Anom #3 claim. The Chic showing, in the eastern part of the property on Skook # 9 claim, is described as an epithermal vein within a megacrystic potassium-feldspar porphyry containing disseminated pyrite with chalcopyrite traces in a quartz-kaolinite vein.

Several diamond drill holes were put down on the Klaw prospect by Noranda Exploration Co. in 1989, where a float occurrence was stripped to expose a 2 m wide orange coloured chalcedonic quartz-breccia vein that was subsequently recovered. An IP chargeability anomaly was also drilled by BP Canada near this locality, which now forms parts of the Skook #1 and Skook #2 claims, but the old drill hole locations are unpublished. The best assay returned was 0.7% Cu and 0.97 gm/tonne Au across a 5m core length, and described as a siliceous breccia containing chalcopyrite, malachite chalcedony, quartz and carbonate, straddling the contact between the Hogem intrusive suite and the Chuchi Lake formation (Melville et al. 1992). The epithermal character of this prospect suggests a similarities to the Rig breccia, 2 km further south.

It is concluded that the gold, silver, and base-metal mineralization of the Chuchi Lake property consists of structurally controlled mesothermal and epithermal veins, breccia-veins, and some untested porphyry style targets. Veins and breccias in the central part of the property occur close to the main contact of the Hogem batholith and Chuchi Lake formation. They form structural targets that may have


N
WIT
PROSPECT
875m
900m
850m
B.L.
900 CONTOUR in metres
> 250
>200 TO 250
>160 TO 200
>120 TO 160
>95 TO 120
>75 TO 95
0 TO 75
DRILL HOLE
TRENCH
500 m
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THE WIT PROSPECT :SOIL GEOCHEMICAL MAP OF BARIUM (in ppm)
scale as shown
date 01/97
by
Fig. 7

limited depth extension adjacent to the minor northeasterly fault zones: but mineralization may be deeper along the `lake-parallel' caldera ring-fractures of the Chuchi Lake fault system. According to Sillitoe (1993) ring fractures form permeable fluid conduits for some epithermal deposits. The writer is satisfied that the Wit prospect is the only target type of this type that has been tested previously at the Chuchi Lake property.

GEOPHYSICAL SURVEYS

Geophysical surveys were carried out over 75% of the claims (Fig.6), with the objectives of isolating conductors, chargeability anomalies, and delineating geological boundaries. Their purpose was to establish targets composed of (usually concealed) concentrations of conductive and/or magnetic minerals, notably copper and iron sulphides. However, the latter minerals are not always associated with deposits of precious metals and zinc, which may explain why the electrical methods have been unsuccessful to date at the Chuchi Lake property.

(1). Induced Polarization - Resistivity surveys have been employed over the Anom claims and Skook claims # 3-6, 9-11, 19, 22, and 26-28, along lines spaced 200 m and 400 m apart, with stations 50 m intervals on grid-lines oriented north to south Fig. 6). The surveys utilized a B.R.G.M. designed Time Domain `IP-6' manufactured in Canada by EDA, with a pole-dipole array and dipole length of 50 m. This automated system records up to 6 dipoles simultaneously integrating a 900 milliseconds window after a delay time of 120 milliseconds. Several high quality chargeability anomalies are recorded throughout the survey area and the main double-lobed anomaly extending across the central part of the claims was drill-tested by BP Canada Resources Ltd. in 1991 and found to consist of pyritic zones without significant copper mineralization. Similar anomalies are associated with the Hogem complex in the eastern part of the claims, where no drilling has been done in these intrusions. The map shown in Appendix (D) does not include the survey of the Anom claims, where a single anomaly was explained by barren pyrite in outcrop.

(2) Ground magnetometer surveys have been limited to small areas of the subject property, and need not be considered further, due to the availability of higher quality airborne magnetic results over a larger area as described below.

(3) Airborne (helicopter) combined magnetic, electromagnetic ,and VLF-EM surveys consisted of three survey blocks, the eastern two of which are contiguous, but there is a 5 km gap in the coverage in the west-central part of the property Fig. 6). Flight lines were spaced at 100 m, oriented north-south in the west and central survey blocks, and east-to-west in the east central part of the property. The surveys were flown in 1991 at a mean terrain clearance of 60 m, with EM sensors having a ground clearance of 30 m. The `Aerodat 4' frequency system was employed, in which two vertical coaxial coil pairs are operated at 4175 Hz and 32 kHz. The transmitter-receiver separation was 7 m. Inphase and quadrature signals were measured simultaneously for the 4 frequencies, with a time constant of 0.1 seconds. The VLF-EM system utilized a `Herz Totem 2 A' instrument which measures the total field and quadrature component of the selected frequency. The transmitting stations used were the NLK Seattle, Washington (24.8 kHz), and Cutler, Maine (24.0 kHz). The magnetometer employed a Scintrex Model VIW 2321 H8 cesium, optically pumped sensor, with a sensitivity of 0.1 nannoTeslas at 0.1 second sampling rate.

The airborne results include ten weak conductors the strongest of which is interpreted as a `lake-parallel' east-west fault zone (Humphreys 1991). No drill testing was proposed, but Noranda exploration drilled a chargeability anomaly on the southwest corner of Skook #3 claim, 250 m from the north shore of Chuchi Lake (Fig. 5). In view of the fact that the Wit prospect and West Zone are both associated with east to west striking structures, the strongest conductor noted by Humphries (1991) merits further attention in association with the central targets shown below (Fig. 5).

GEOCHEMICAL SURVEYS

Due to its mountainous character drainage and soil geochemical surveys have enjoyed considerable success in B. C.. Accordingly many soil geochemical surveys were conducted over 60 % of the subject property (Fig. 6), but in spite of more detailed follow up lines 100 m apart, most of the sampling employed widely spaced lines suitable for porphyry copper targets. The most extensive survey, which was completed in 1991, consisted of 1250 samples later augmented by `fill-in' sampling of anomalous areas in 1995. The 1991 surveys covered the west-central part of the property, with north to south lines cut at 200 m intervals, and sample stations at 50m intervals (Fig. 6). The eastern half of the grid employed

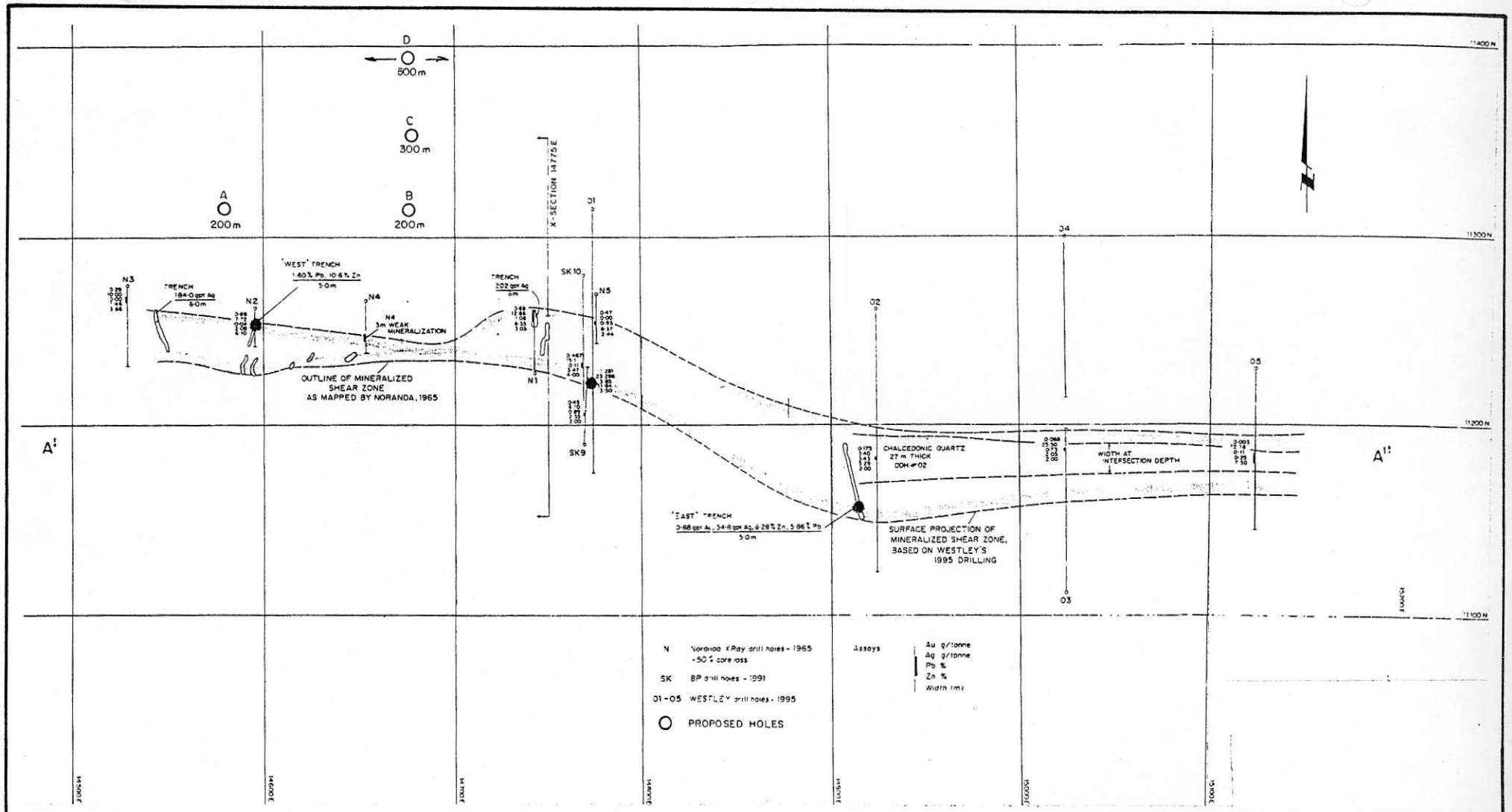
grid lines 400 m apart. The map and analytical results of these surveys are shown in Appendices (A) and (B) and Fig. 6 .

The 1995 soil sampling was conducted along short lines 100 m apart in areas selected on the basis of previous analytical results. Samples were collected in standard kraft bags, dried and sieved to -80 Mesh , and analysed by Acme Analytical Laboratories of Vancouver for Au, Cu, As, Pb, Zn, Ba, Fe, V, Mn, Mg, Ni, Co, Cr, Ti, P, Ba, Sr, Ca, Mo, Sb, Bi, Ag, Th and Al . Two analytical methods were employed : (1) *aqua regia* dissolution ICP (Induced Coupling Plasma); and (2) ICP following digestion with 3ml 3-1-2 HCL-HNO_3-H_2O at 95 deg..

The gold content of the soils was established partly by Acid leach Atomic Absorption from 10 gm samples (1991), and partly on Fire Assay/ICP from 30 gm samples (1995). It should be noted that sample preparation by the standard sieving to -80 Mesh removes coarse gold from the samples to be analyzed, which limits their utility in areas containing coarse gold. Anomalous concentrations up to 350 to 1000 ppb and were recorded (Appendix B).

At least three kinds of geochemical anomaly may be interpreted from overburden conditions found north of Chuchi Lake: (1) anomalies directly related to a bedrock source and showing limited evidence of glacial dispersion; (2) anomalies showing evidence of `glacial smear' typical of basal tills; and (3) anomalies exhibiting dispersed linear trends characteristic of drumlinoid areas. Some of the geochemical anomalies north of Chuchi Lake are clearly related to a bedrock source, which facilitates the interpretation of those anomalies without an obvious source.

The largest anomaly consists of the basal till type of dispersion exhibited by a population of anomalous elements including Pb, Zn, Ag, Cu, and Ba found in the vicinity of the exposed bedrock mineralization of the Wit trenches (Fig. 7). There is evidence of up-hill dispersion of these elements for a distance of 800-900 m north and east of the mineralized trenches, as might be anticipated from Plouffe's (1991) glacial studies. Surface slope and surface and ground waters may also affect the dispersion of these elements, depending on the solubility of the mineral compounds, but the associated insoluble elements such as Ba (in barite) show the



NATION RIVER RESOURCES LTD.

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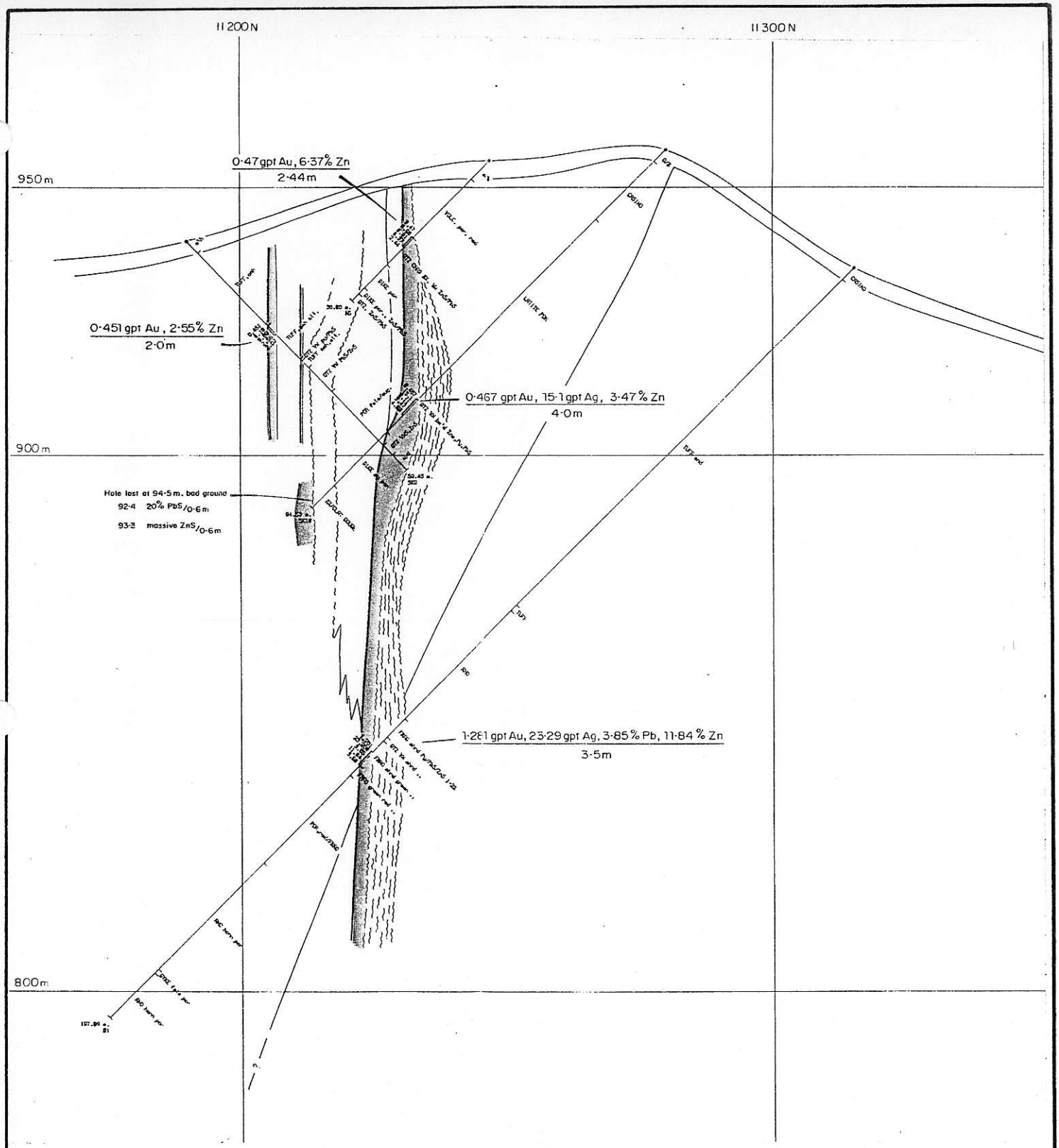
CHUCHI LAKE PROPERTY
WIT PROSPECT
DRILL HOLE & TRENCH PLAN

0 50 100 150 METRES

SCALE: AS SHOWN	DATE: JAN. 1997
DRAWN BY: R.B.	FIGURE Nº: 8



NATION RIVER RESOURCES LTD.

BEAVON CONSULTING LTD.

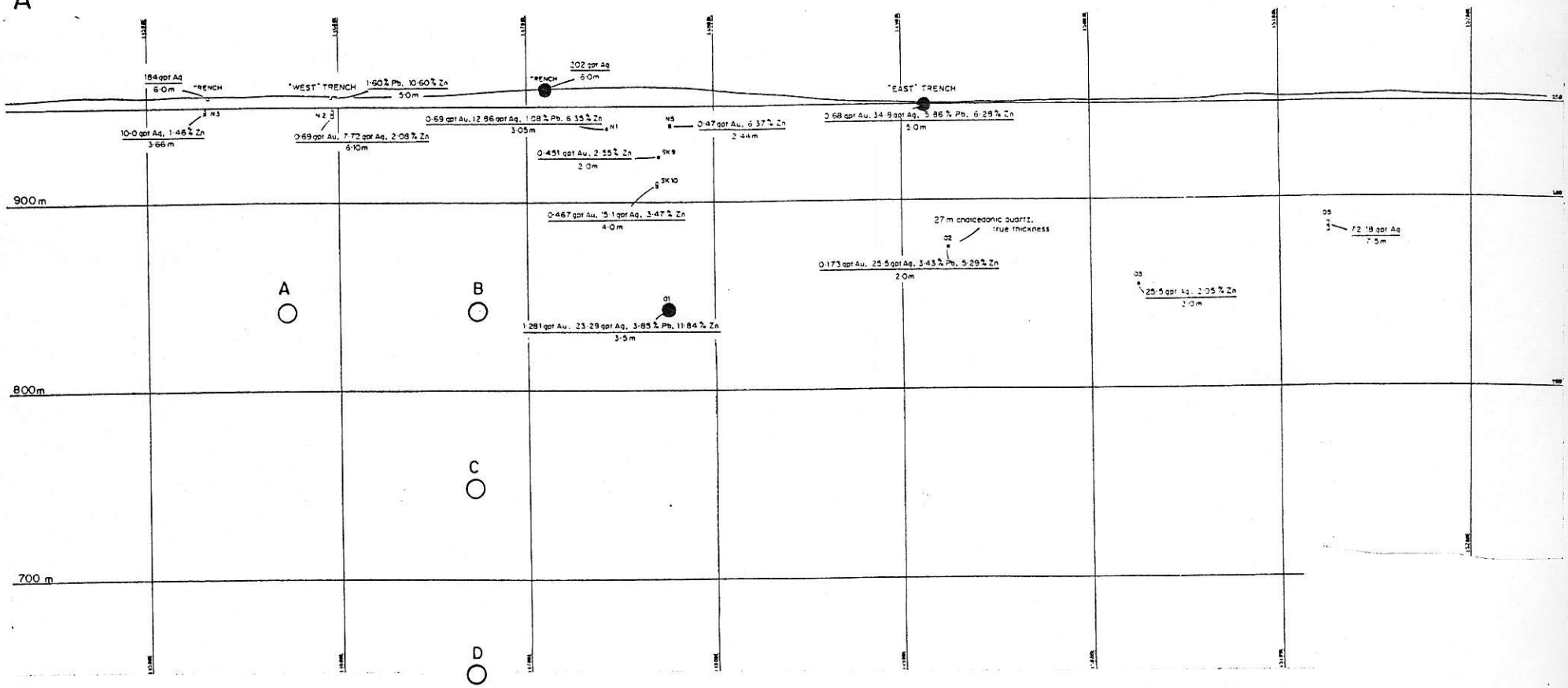
CHUCHI LAKE PROPERTY
WIT PROSPECT

SECTION 14775E

0 10 20 50 METRES

SCALE: AS SHOWN	DATE: JAN. 1997
DRAWN BY: R.B.	FIGURE No.: 9

CHONG



○ Proposed drill holes

NATION RIVER RESOURCES LTD.

BEAVON CONSULTING LTD.

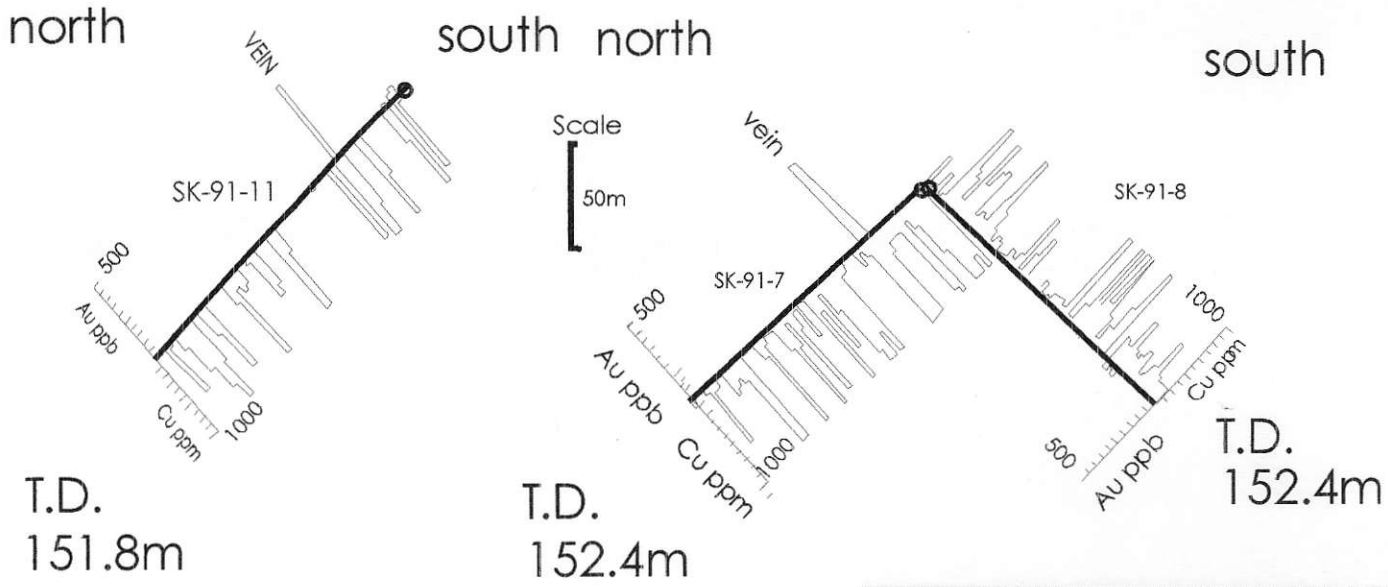
CHUCHI LAKE PROPERTY
WIT PROSPECT
LONGITUDINAL SECTION
A' - A''

0 50 100 150 METRES

SCALE: AS SHOWN	DATE: JAN. 1997
DRAWN BY: R.B.	FIGURE No.: 10

LOCATION OF SECTIONS SHOWN IN Fig. 6

Sample interval = 2m



SEE TEXT FOR RESULTS ABOVE 500 PPM Cu
AND OVER 1000 PPB Au.

NATION RIVER RESOURCES LTD.

BEAVON CONSULTING LTD

SKOOK WEST ZONE

TWO DIAMOND DRILL SECTIONS
HOLES SK 91-7, 8, AND SK91-11

scale as shown	date 01/97	by Fig. 11

same degree of dispersion as the more mobile Zn (from sphalerite), which suggests that dispersion was mostly physical rather than chemical.

The Wit geochemical anomaly/ies is/are also affected by gravity dispersion due to topography, but the main dispersion is across ground at higher elevation than the trenched showings and must have resulted from east to northeast glacial transportation. This interpretation may need modification if other bedrock sources of the stated metals are found : *n.b* the relatively isolated anomaly northwest of the present trenches (Fig. 7 , 8).

Further west on the Chuchi Lake property another association of elements, namely Cu, Zn, Pb, Ba, Fe, Co, and V, shows southeasterly trending anomalies unlike those of the Wit prospect area. Instead of mimicking the glacial transport direction the anomalies of this population appear to match the strike of the bedrock Takla siltstones and associated faults (Appendix A). It is well known that such sediments may commonly contain high background values of these elements which, in rare cases, may become eoncentrated into economic deposits.

Although there appear to be few copper-gold anomalies in the soils sampled of the Chuchi Lake property, lithogeochemical contrasts are demonstrated by analysis of diamond drill cores showing higher than normal baekgrond concentrations of copper and gold, both in the Takla Group and in the monzonitic intrusions of the central part of the property (e.g. Skook West Zone, Fig. 11). Diamond drill holes SK-7, 8, and 11 were drilled near the northwestern limit of the grid, where it is unlikely that the narrow gold-bearing quartz-sulphide vein logged in the cores of SK-7 and SK-11 would be identified by widely spaced soil samples. Moreover, since trenching is impractical in the creek-bed, a limited combined magnetic and electromagnetic survey is a necessary precursor to further drilling of the Skook West zone.

In the partly explored eastern third of the Chuchi Lake property (Fig. 4b), multi-element soil anomalies containing Ba, Pb, Zn, Ag and Mn tend to form east-northeasterly trending anomalies that have been interpreted in terms of glacial dispersion (Campbell 1995). Separated into individual elements (Appendic A) these anomalies are weak and sinuous, and may be interpreted as drumlinoid-type anomalies which commonly occur above the basal till and may indicate anomalies

transported further from their source than the basal till anomalies of the Wit prospect. Single-element gold concentrations are also evident in this eastern area (Fig. 4b), which is inferred to be underlain by a Tertiary graben. Thus the higher Au ppb concentrations of the eastern part of the property could represent redistributed lode or placer deposits associated with the Chuchi Lake fault system , with a Tertiary graben, or with both alternatives.

The highest gold analytical results occur in the eastern part of the property, (in Fig. 4b) and are flanked to the southeast by high I.P. chargeability anomalies associated with a sub-circular magnetic `low' surrounding a total field magnetic `high' thought to represent a porphyry stock suggested by a single outcrop of feldspar porphyry. Overburden thickness in this area is estimated at 50 m (Paterson 1991) and limited drilling was completed on an I.P. anomaly in the volcanic formations surrounding this intrusion, to the south of the best gold in soil results (Colin Campbell, personal communication).

The interpreted gold anomalies (Fig. 4b) may also be consistent with northeasterly dispersion of gold particles from intersecting faults and/or dike-like magnetic features indicated by the airborne survey. As discussed above, the development of mesothermal and epithermal mineralization associated with Mesozoic and inferred Tertiary block-faults, elsewhere on the property, suggests a possible source for anomalous gold in soils. Associations of early Tertiary epithermal mineralization with block faulting have recently been demonstrated in the Challis volcanic field of central Idaho (Allen and Hahn 1994).

DIAMOND DRILLING

Aside from 18 holes drilled by Noranda Exploration in the vicinity of the Klaw prospect (Skook #2, #3), at least 2334 m of diamond drilling has been completed on the subject claims, approximately one half of which tested the Wit prospect. The remaining holes, including KD-91-01 (Fig. 5), were targeted on IP chargeability anomalies caused by fracture controlled pyrite in the bedrock.. At the time, the mineralized veins, breccias, and geochemical anomalies, other than the Wit prospect, were passed over in favour of larger perceived targets. Relevant diamond drill logs and assay certificates are included in Appendix (C).

In the central part of the Chuchi Lake property four holes were drilled to test strong chargeability anomalies along the flanks of a large east to west trending magnetic `high' on the Skook #4 and #6 claims (Fig. 5). The first hole (SK-91-01) was lost in overburden, and Sk 91-2 cut 0.09% Cu over 14 m. Sk-91-3 and SK-91-5 returned no significant analytical results. Hole Sk-91-4 was collared in siltstones outcropping 1000 m west of the first five holes, and tested an east trending zone of I.P. chargeability was found to be due to 2%-6% pyrite scattered through the monzonite of the core, with anomalous gold appearing in the last run! Diamond drill hole SK-61-6 was drilled in a magnetic and pyritic (2%-3%) monzonite to the northeast of the other holes.

Interesting results were obtained from the Skook West Zone (Fig. 5), where holes SK-91-7 yielded a 35 m wide intercept of 0.32 % Cu, including a 0.3 m core length that assayed 12.5% Cu, 19.3 gm/tonne Au, and 69 gm/tonne Ag (Appendix C). A similar vein intersection appears in the logs of SK-91-11, and all three of the holes drilled in this area yielded anomalous copper results (Fig. 11). The two diamond drill sections across Skook West Zone illustrate one or more precious metal-bearing veins which appear to be enveloped by the low grade disseminated and fracture-controlled sulphides (Fig. 11)..

The 1991 drill program in the central part of the Chuchi Lake property suggests a pre-ordained project without allowance for newly acquired knowledge of the precious metal veins. Similarly the use of geochemical analysis and sample preparation rather than fire assays lacking metallic sample-preparation may have down-graded the gold tenor of the eores.

In 1995 Westley Technologies Ltd. conducted an integrated program of soil sampling, trenching, and diamond drilling of the Wit prospect (Figs. 8,9,10), which extended the strike length of the mineralized zone from 250 m to 400 m, and indicates a revised potential for over 1 million tons to a depth of 250 m. The longitudinal drill section indicates three intersections averaging 3.2% Pb, 9.9% Zn, 18.4gm/ton Ag, and 0.85 gm/ton Au, and 18% barite with an average thickness of 4.15 m (Fig. 10). A multi-hole cross-section (Fig. 9) shows parallel zones of mineralization that could boost the potential tonnage and provide more working places for underground operations. At the time of writing there is insufficient information to ascribe a rake to the higher grade mineralization which,

together with the possibility of mineral zoning, remains to be tested by deeper drilling.

CONCLUSIONS AND RECOMMENDATIONS

This review of exploration of the Chuchi Lake property in the Omineca Mining Division, of central B. C., concludes that the little explored precious metal and base metal prospects of these claims occur in epithermal, mesothermal and porphyry styles of mineralization. Some of these prospects show similarities with economic gold and silver deposits of Tertiary volcanic centres in Colorado, so that their economic potential requires further investigation in conjunction with the exploration of newly acquired claims.

Geological and geophysical criteria suggest that the various styles of mineralization are related to the southern structural boundary of an arcuate fracture system composed of radial and concentric faults belonging to a caldera-like down-sag of probable Mesozoic age. This structure is reflected in the concave-north outline of Chuchi Lake which covers part of a fault system that is responsible for the structural repetition of a marker sedimentary member of the Chuchi Lake formation. The most prospective mineralized zones may be related to vein-openings and breccias near the intersection of the radial and concentric fractures of the Chuchi Lake fault system, which is mostly covered by lake sediments and glacial overburden in excess of 50 m . This scenario applies particularly to the eastern part of the claims, where several multielement geochemical anomalies have been identified in soils covering the strike continuation of the main concentric fault zone and its `down-ice' glacial tail.

Aside from the Wit prospect, previous drilling was dedicated to geophysical targets that were due to barren pyrite mineralization. Although the veins and breccias were shown to contain precious metal values at the time, these new targets received limited drilling. Further work is now justified on the basis of new geological ideas derived from productive or past productive properties in similar geological environments elsewhere in the Quesnel belt, and from a world-wide association of epithermal deposits with volcanic centres and block faulting.

The first priority is for further integrated exploration of the Wit prospect, to consists of 1600 m of Bq diamond drilling designed to establish a higher grade core to the previously established Pb-Zn-Ag mineralization, and to investigate the possibility of precious metal enrichment due to mineral zoning at depth. Emphasis

should be placed on 100% core recovery, the determination of the wall-rock structure, and gathering information on veins parallel or oblique to the main zone. At least one portion of the Wit geochemical anomaly may be unrelated to the known vein, so that further trenching is required to search for discrete or branch veins, followed, if warranted, by 200 m of additional drilling.

Mineral zoning may also apply on a property-wide scale, utilizing the proposed volcanic centre, in the sense that the Chuchi Lake formation is tilted southward at an angle steeper than the plateau surface. Assuming a Jurassic (volcanic) age for mineralization, deeper seated mineral deposits are to be expected north of the proposed ring-fracture, near the centre of the volcanic complex as evinced by the Digger prospect; whereas (shallower) epithermal mineralization is more likely to have escaped erosion further to the south, near Chuchi Lake itself. However if any of the mineralization is found to be of Tertiary age, topographic criteria should also incorporated into target selection.

It is concluded that the Skook West Zone is a mesothermal precious-metal sulphide vein system with the potential for over 1 million ounces of both gold and silver, comparable to the vein deposits of the Rossland mining district of southern B. C.. A thorough re-examination of this prospect, based on a 50 m grid, should include an integrated program of geological mapping, ground geophysical surveys (magnetic and EM), soil sampling, followed by up to 250 m of diamond drilling. This work is justified to further define the known gold-bearing veins (or vein-system) together with their envelope of low-grade copper mineralization. The latter may indicate proximity to a faulted porphyry Cu-Au target at relatively shallow depth.

It is concluded that the Rig breccia, the South Zone, and CLL prospects are epithermal gold-bearing prospects in the central part of the Chuchi Lake property. Using similar exploration methods recommended above for the Skook West Zone, the intersections of east-to-west (concentric) and north to north-westerly (radial) block-faults indicated by the airborne survey are recommended as favourable targets. The main emphasis should be on further trenching in association with diamond drilling (250m).

Since the Wit prospect is located on an east-west striking (concentric) fault-zone other east-west striking faults of the Chuchi Lake merit further exploration, particularly where supported by related geochemical anomalies. Aside from the Skook West Zone noted above, such a fault is probably indicated by the airborne geophysieal results in the south-central part of the property, near glacially dispersed soils with anomalous in Ba near the shore of Chuchi Lake. Overburden drilling, sampling and analysis may help decide which, if any, of the nearby airborne conductors should be drill-tested . The location of these conductors should be established prior to diamond drilling by limited ground geophysical coverage.

The easternmost claims (Skook # 29, 31,and 32), for which there is little geological information and considerable geochemical justification, should be further explored by soil sampling in conjunction with overburden drilling of a gold anomaly on Skook claims #10 and #14. Samples of overburden cuttings or cores should be at 2.5 m intervals, and analysis done by Fire Assay/ICP using 30 gm samples, including trial determinations for +150 Mesh material. Overburden drilling is necessary to confirm a bedrock source for transported gold anomalies, as indirectly suggested by the known glacial dispersion of stable elements elsewhere on the property, and by the nearby intersection of the strike-continuation of the Chuchi Lake fault system and inferred northwesterly striking faults and dikes. Thus a phased program is recommended to include initial drilling, with the a second phase of drilling to be contingent on the results of the first phase program as follows:

BUDGET PROPOSAL

Phase 1

Line Cutting 300 line km @$250		75,000
Geophysical Surveys		
Ground Magnetic survey 100 line/km @ $150		15,000
Electromagnetic survey 100 line/km @ $300		30,000
Trenching 30 days @ $1000		30,000
Overburden Drilling 1000 m @ $50/m		50,000
Diamond drilling 22,000 m @ $100		220,000
Mobilization		10,000
Assays and analytical costs		4,000
Transportation, Travel		10,000
Personnel		
Snr. Geol. 64 days @$425	= 25,500	
Geol. 40 days @ $300	= 12,000	
Asst. 40 days @ $200	= 8,000	
	45,500	45,500
Camp costs		
300 man days @ $50	= 15,000	
Supplies & equipment...	= 3,500	
	18,500	18,500
Communications		2,000
Reclamation allowance for trenching		3,000
Contingency		27,000
	Total	550,000

Signed ----------

Roy V. Beavon, B.Sc., Ph.D., P. Geo.

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CERTIFICATE

I, Roy Vernon Beavon, of the City of Richmond in the Province of British Columbia, do hereby certify that:

(1) I am a consulting geologist and a principal in Beavon Consulting Limited, with offices located at 8720, Millmore Road, B.C., V7C 1S9.

(2) I am a graduate of the University of Wales (U.K.) with the degree of B.Sc. (1957) and Ph.D. (1960).

(3) I have been practising my profession continuously for the past 35 years, and in a supervisory capacity for 25 years.

(4) I am registered as a Professional Geoscientist (P.Geo.) by the Association of Professional Engineers and Geoscientists of British Columbia (Registration Number: 19699), a Fellow of the Geological Association of Canada (FGAC) and the Geological Society of America, and a member of the Society of Economic Geologists, and the Association of Prospectors and Developers.

(5) I have based this document titled "Exploration proposals for the Chuchi Lake properties of Nation River Resources Ltd., Omineca Mining Division, B.C" upon a thorough review of information and data supplied by Nation River Resources Ltd., upon the sources listed in the references, and upon a personal examination of the Project site on July 13, 1990.

(6) I am the author of the titled report, and the recommendations herein are solely the responsibility of the author.

(7) I have not received, nor do I expect to receive, any direct or indirect interest in the Subject mineral claims.

(8) I have not received, nor do I expect to receive, any direct or indirect interest or securities in Nation River Resources Ltd. or in any associated companies.

(9) I consent to the use of this report and my name, by Nation River Resources Ltd. in the Company's Prospectus, Statement of Material Facts, or other public documents, and grant permission to for the filing this report as a listing document with the Vancouver Stock Exchange.

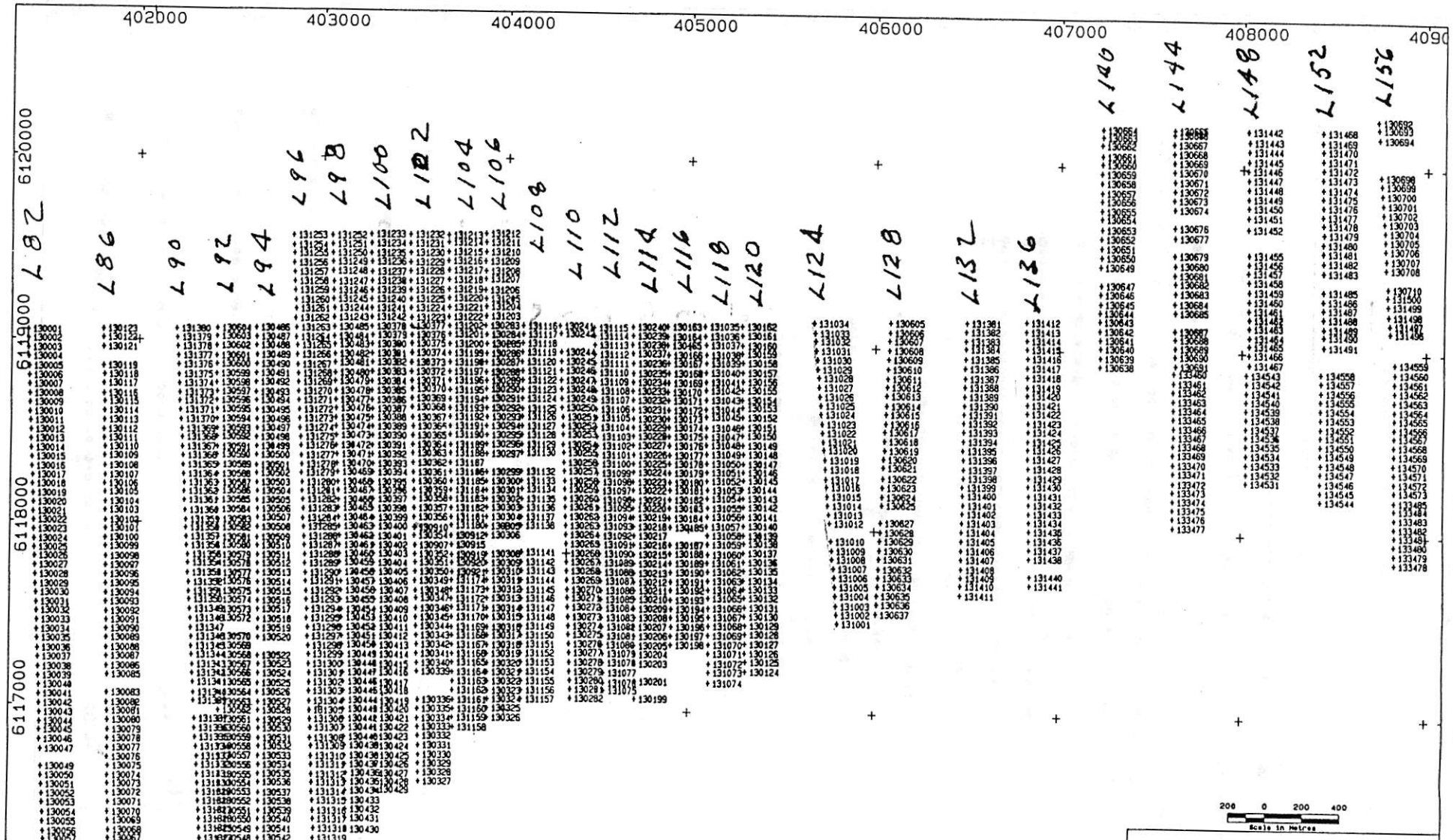
DATED at Richmond, B.C. this th day of February 1997.

Roy V. Beavon, B.Sc. Ph.D., P.Geo.

DISCLAIMER

This report contains information that is intended solely to characterize the geologic conditions, potential, and other aspects of the subject properties, and is intended only for display. Any other use, or reliance, is to be considered a misuse. The facts, findings, opinions, judgements, and conclusions contained in this report are presented on a best-efforts basis, and includes the best available information, as observed in the field, obtained through generally accepted professional practices, and as reviewed by other qualified personnel. Economic projections and estimates contained are subject to revision at any time. No investment decisions should be made without additional third party review. Due to the nature of geologic investigation, and to the potential existence of unknown, unknowable, concealed, or otherwise unreported conditions or facts in, on, or under the property, some conditions other than those reported may, in fact exist. Therefore no warranty of any kind, either expressed or implied, is included herewith.

APPENDIX A - Soil Geochemical Maps



SKOOK GRID

NATION RIVER OPTION (SKOOK CLAIMS) - B.C.

1991 SOIL SURVEY

SAMPLE LOCATION MAP

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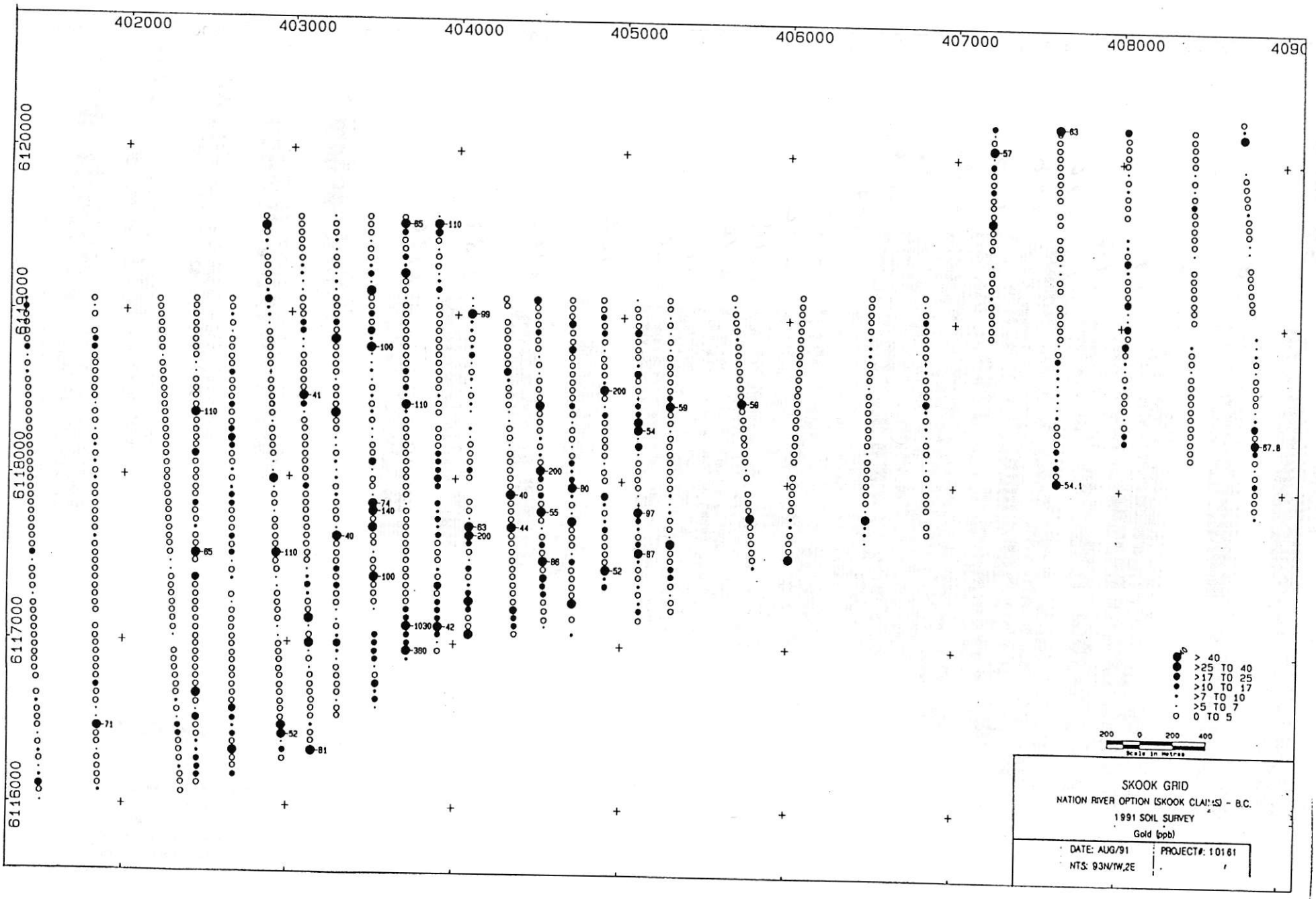
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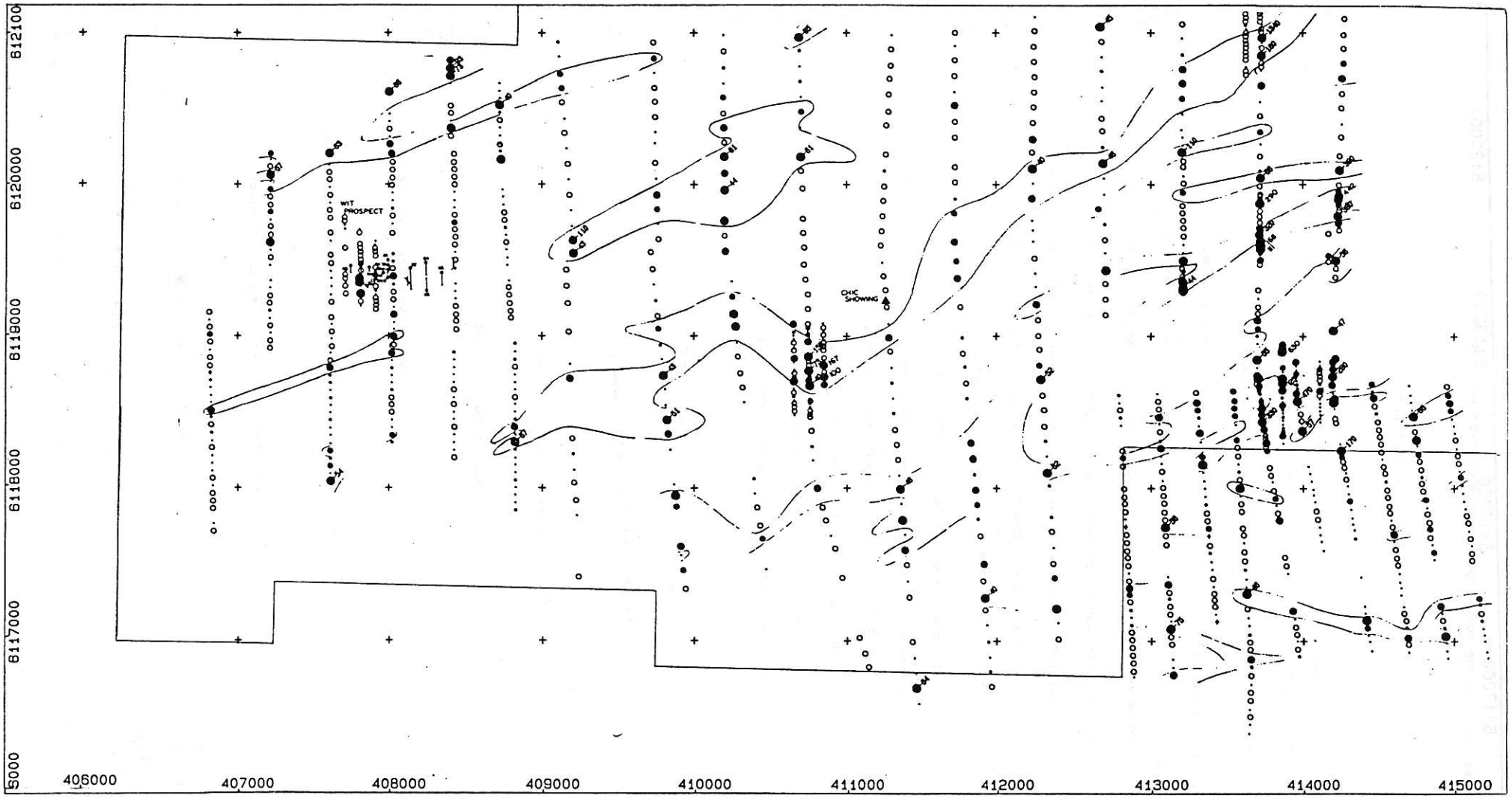
>17 TO 25
>10 TO 17
>7 TO 10
>5 TO 7
0 TO 5
200 0 200 400
Scale in metres
SKOOK GRID
NATION RIVER OPTION (SKOOK CLAIMS) - B.C.
1991 SOIL SURVEY
Gold (ppb)
DATE: AUG/91
NTS: 93N/1W,2E
PROJECT#: 10161



200 0 200 400

Scale in metres

- > 40
- >25 TO 40
- >15 TO 25
- >10 TO 15
- >7 TO 10
- >3 TO 7
- 0 TO 3
- DRILL HOLE
- TRENCH

WIT – FAR EAST – KLAW GRID		
NATION RIVER RESOURCES		
1991 SOIL SURVEY		
Gold (ppb)		
DATE: MARCH 1995	PROJECT#: A	
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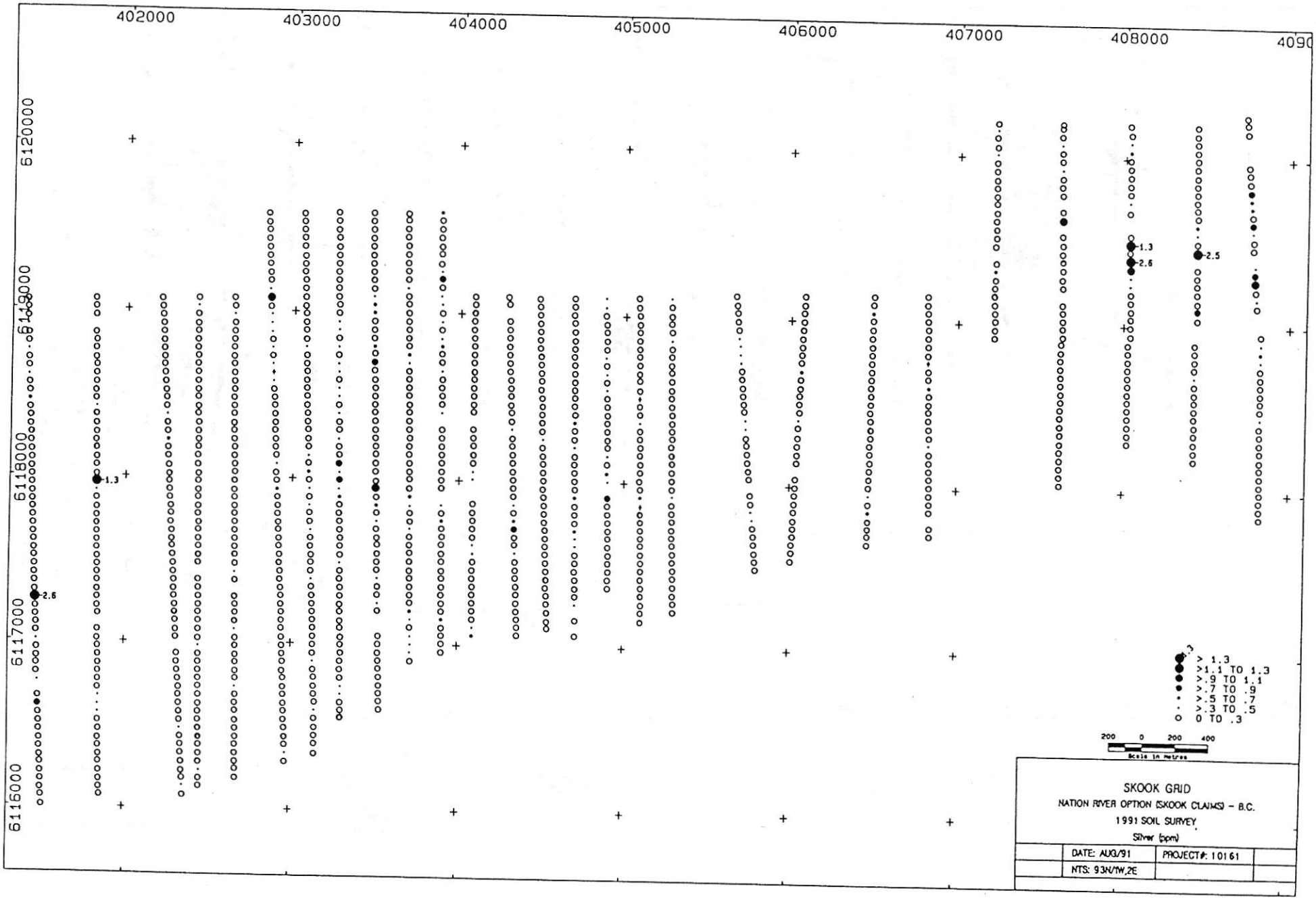
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0 TO .3
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Scale in Metres
SKOOK GRID
NATION RIVER OPTION (SKOOK CLAIMS) - B.C.
1991 SOIL SURVEY
Silver (ppm)
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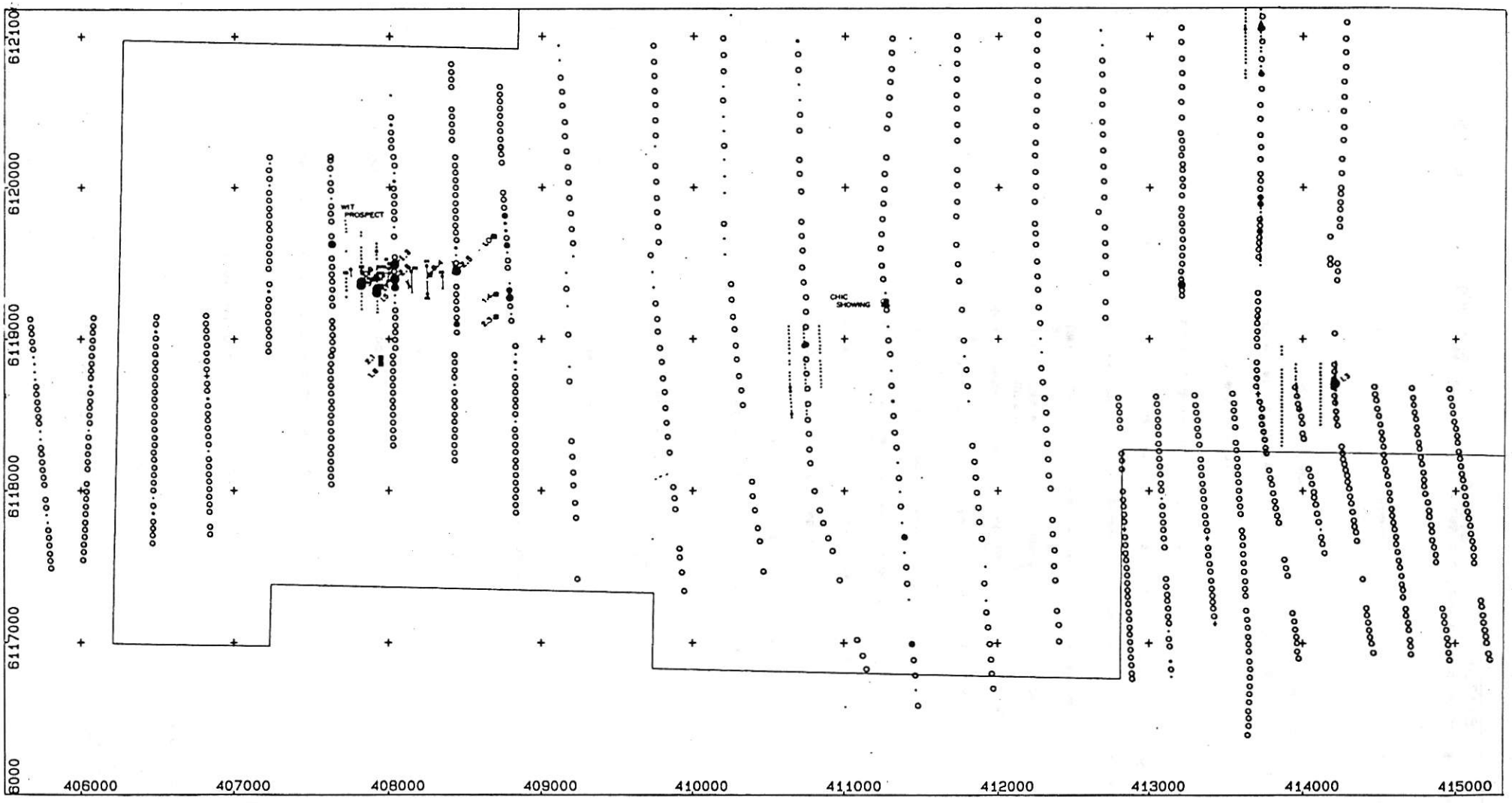

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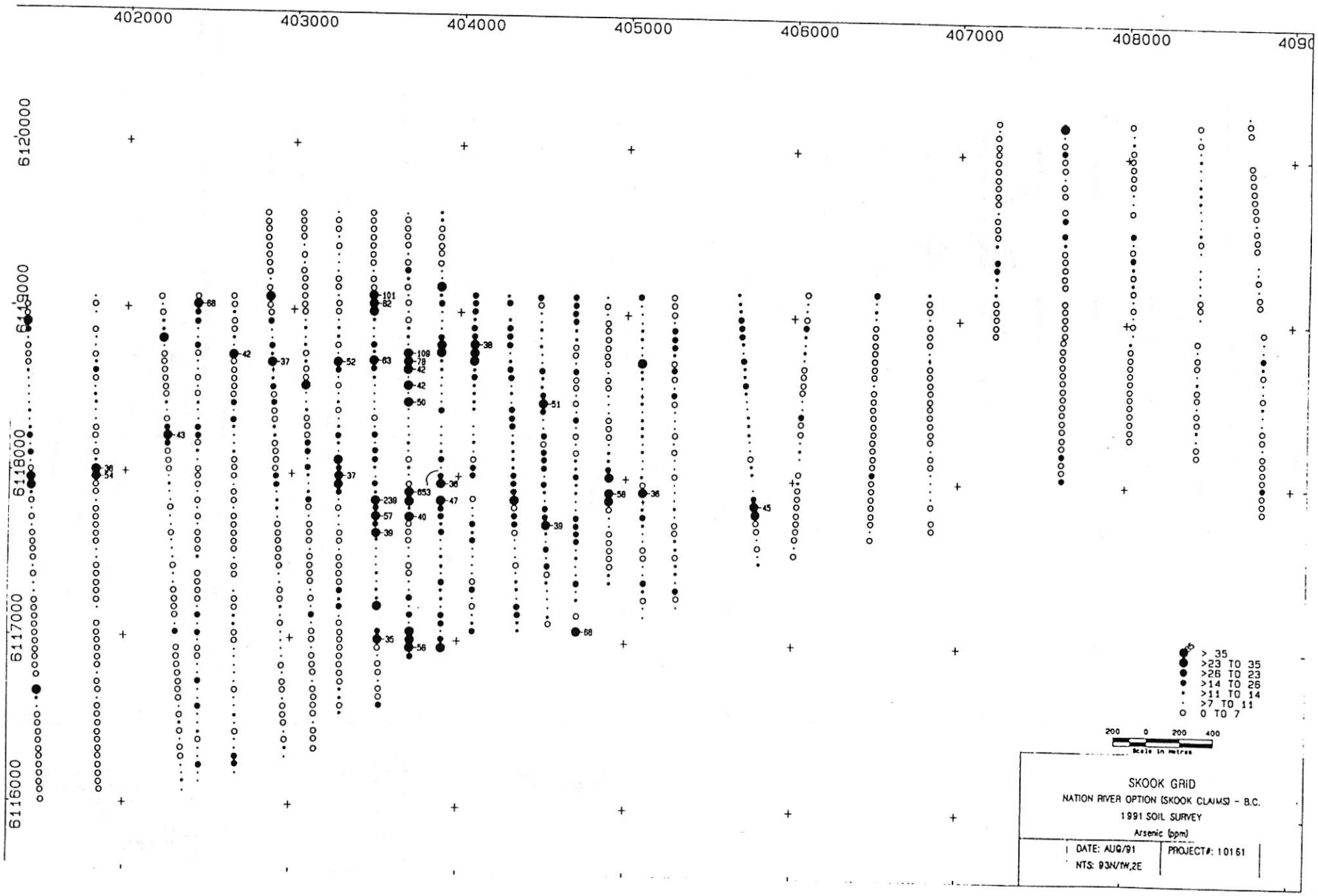
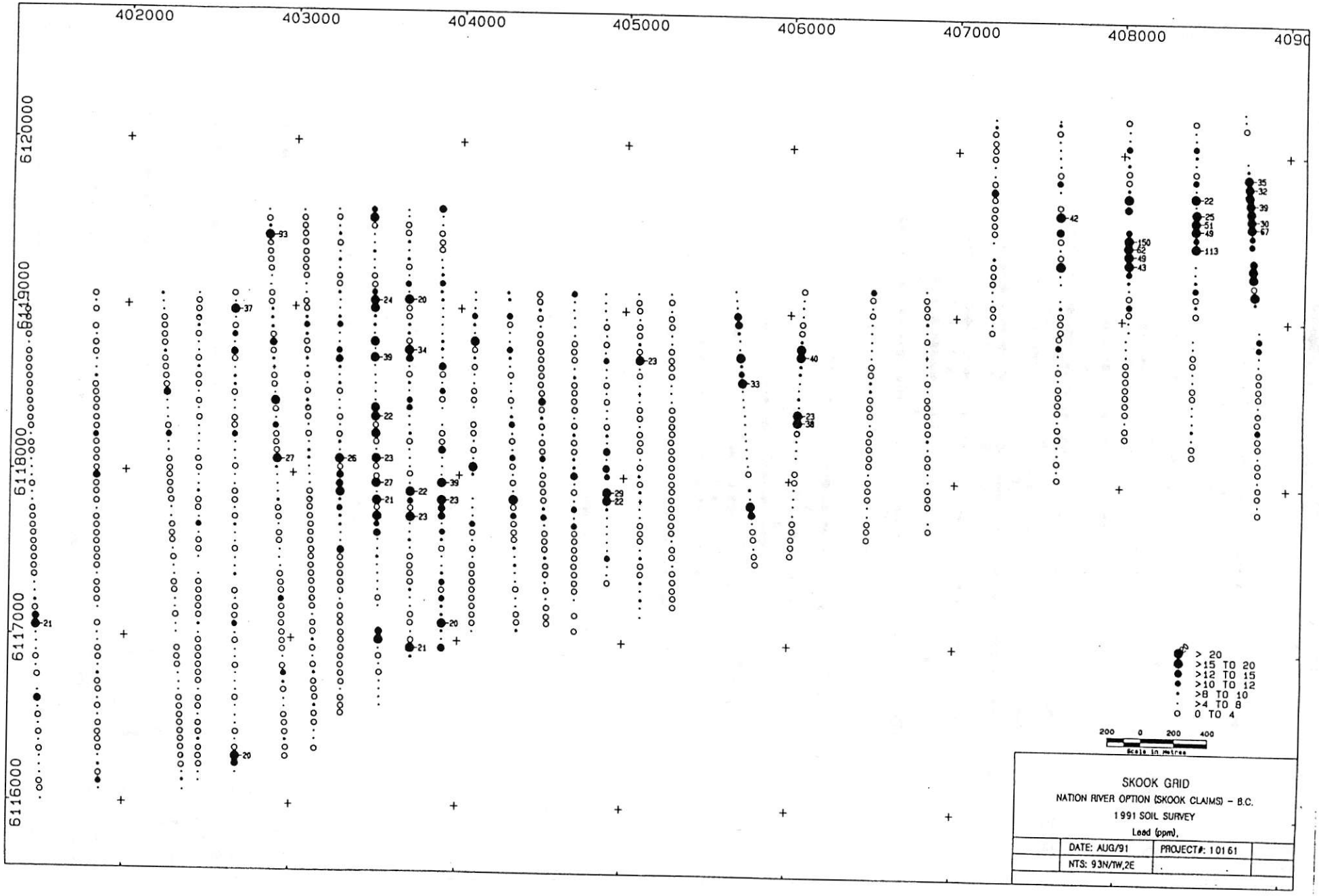
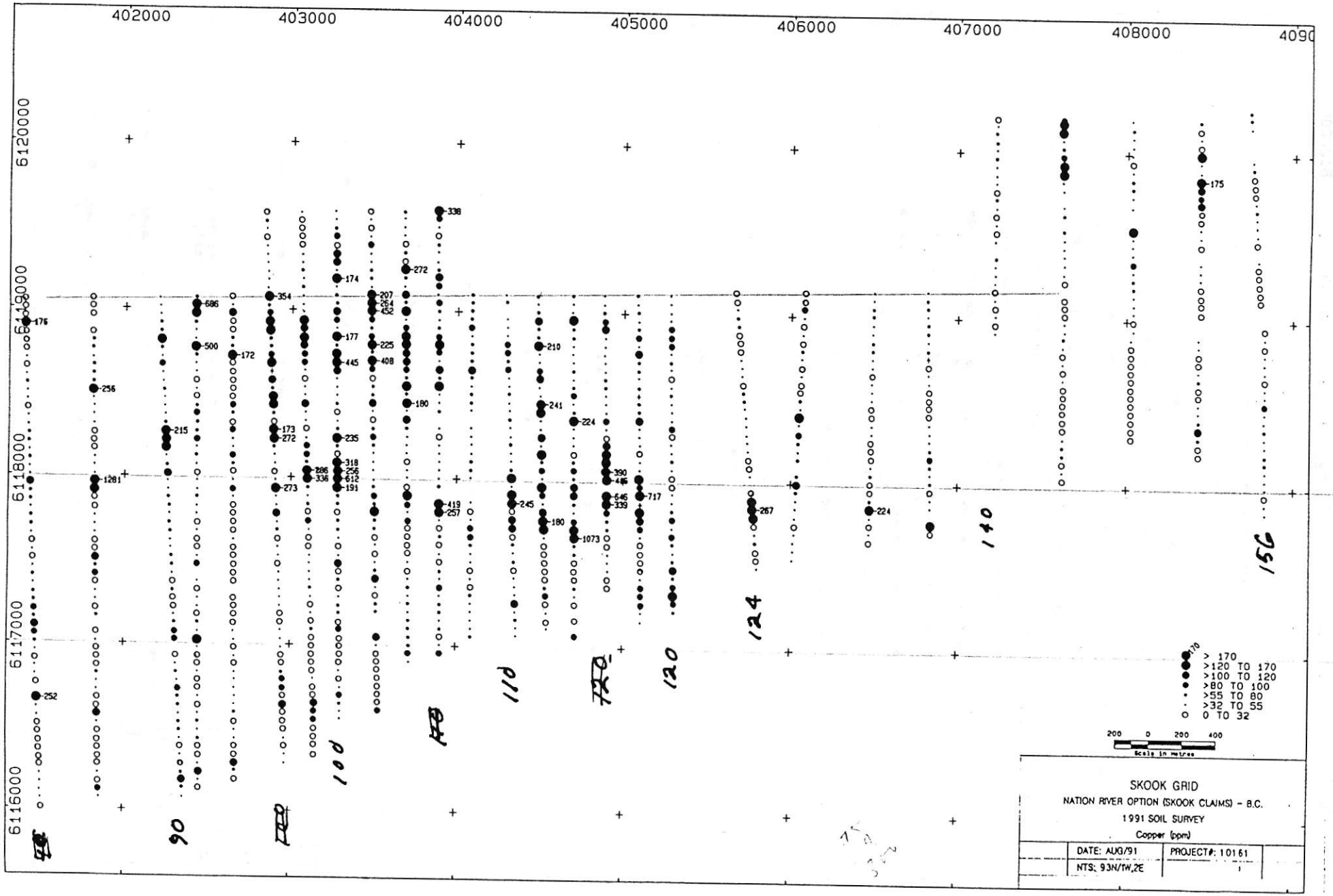
>1.1 TO 1.3
>.9 TO 1.1
>.7 TO .9
>.5 TO .7
>.3 TO .5
0 TO .3
DRILL HOLE
TRENCH
>1.0 (Triton Resources)

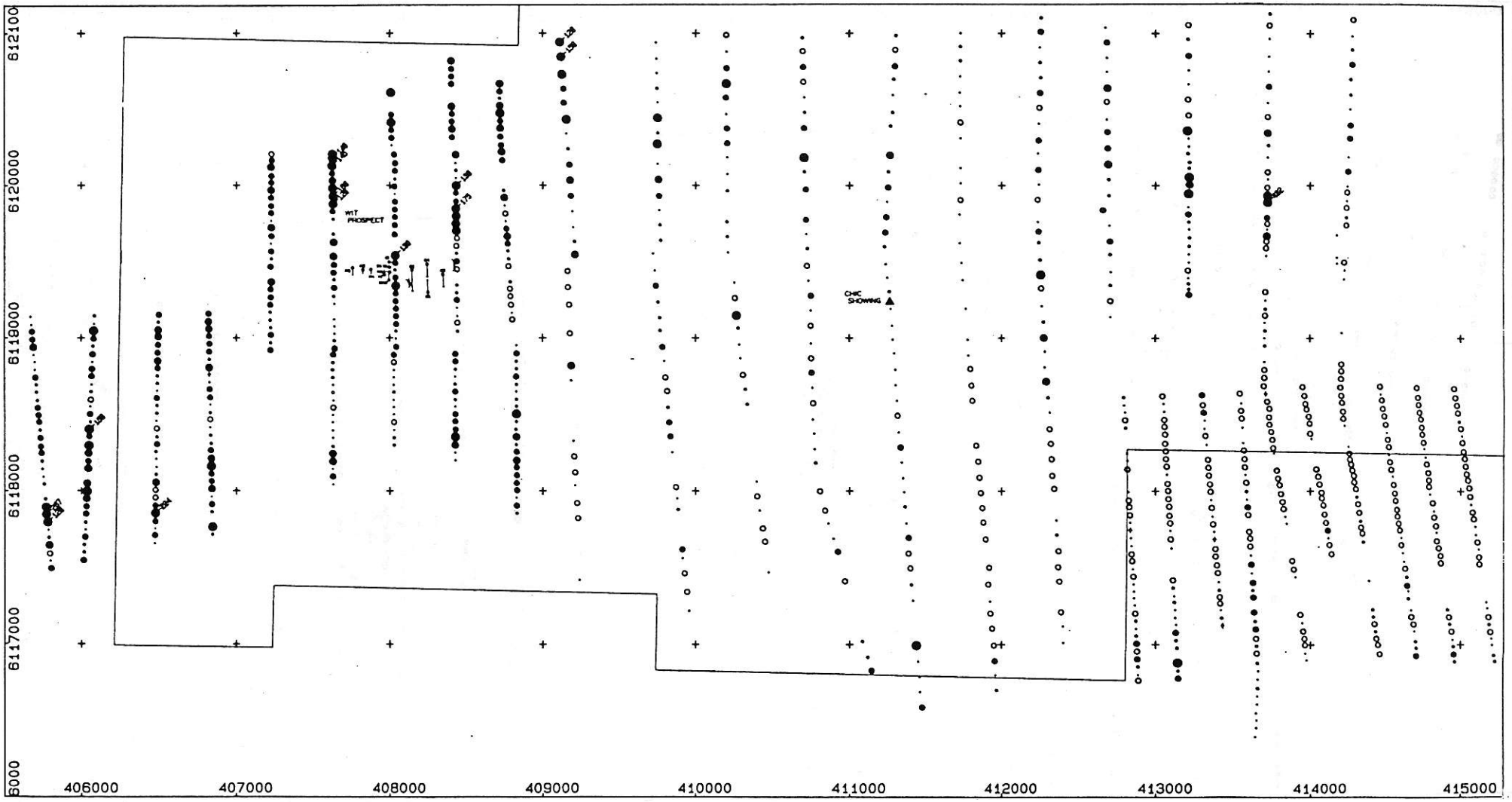
WIT - FAR EAST - KLAW GRID
NATION RIVER RESOURCES
1991 SOIL SURVEY
Silver (ppm)

DATE: MARCH 1991	PROJECT#: A	
NTS: 93N/7W,2E	SCALE	


402000
403000
404000
405000
406000
407000
408000
6120000
6119000
6118000
6117000
6116000
> 35
>23 TO 35
>26 TO 23
>14 TO 26
>11 TO 14
>7 TO 11
0 TO 7
200 0 200 400
Scale in Metres
SKOOK GRID
NATION RIVER OPTION (SKOOK CLAIMS) - B.C.
1991 SOIL SURVEY
Arsenic (ppm)
DATE: AUG/91
NTS: 93N/1W,2E
PROJECT#: 10161


402000
403000
404000
405000
406000
407000
408000
6120000
6119000
6118000
6117000
6116000
> 20
>15 TO 20
>12 TO 15
>10 TO 12
>8 TO 10
>4 TO 8
0 TO 4
200 0 200 400
Scale in metres
SKOOK GRID
NATION RIVER OPTION (SKOOK CLAIMS) - B.C.
1991 SOIL SURVEY
Lead (ppm).
DATE: AUG/91
PROJECT#: 10161
NTS: 93N/7W,2E

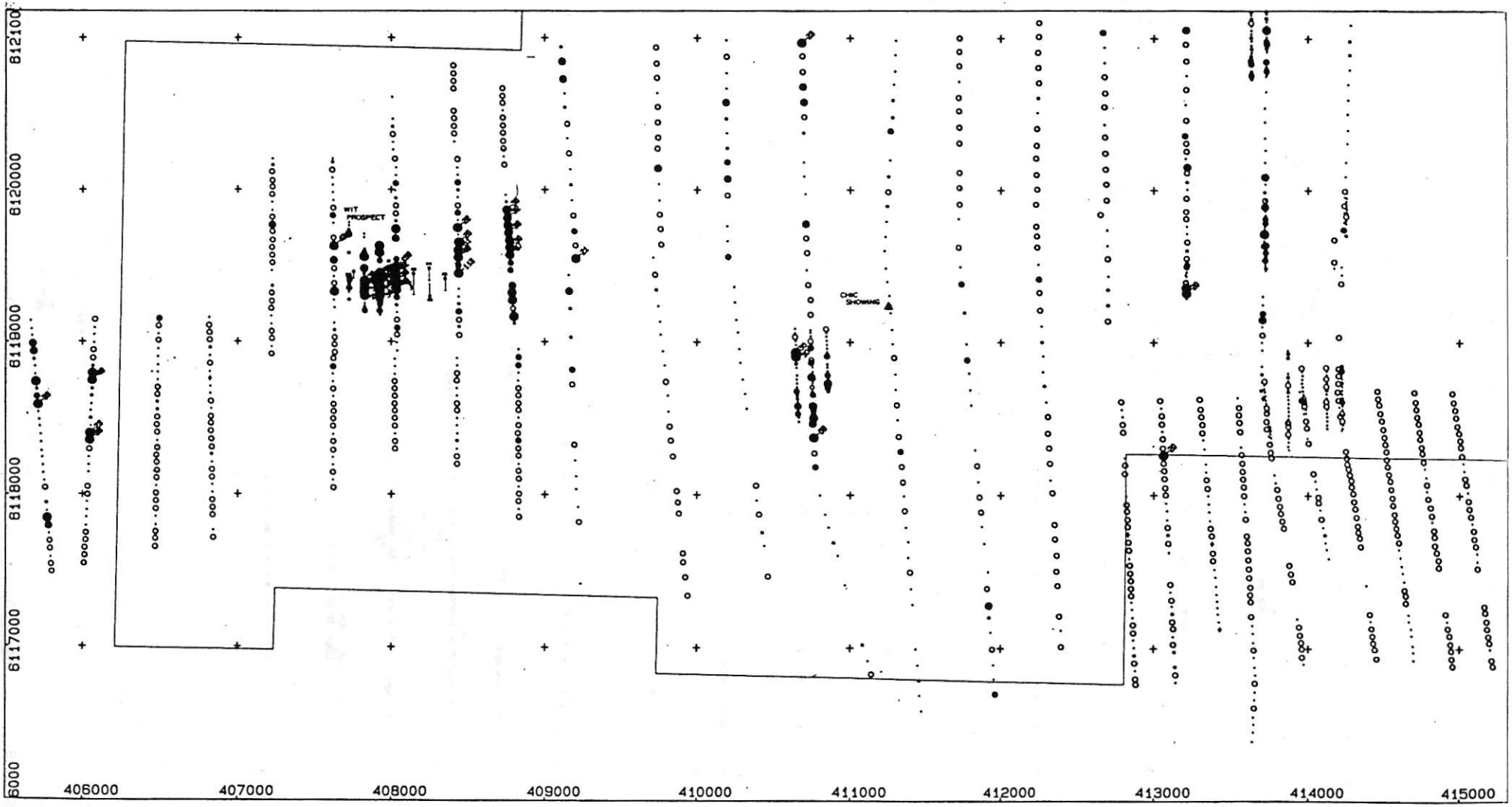

402000
403000
404000
405000
406000
407000
408000
6120000
6118000
6117000
6116000
> 170
>120 TO 170
>100 TO 120
>80 TO 100
>55 TO 80
>32 TO 55
0 TO 32
200 0 200 400
Scale in Metres
SKOOK GRID
NATION RIVER OPTION (SKOOK CLAIMS) - B.C.
1991 SOIL SURVEY
Copper (ppm)
DATE: AUG/91
PROJECT#: 10161
NTS: 93N/1W,2E



200 0 200 400
Scale in metres

> 125
>80 TO 125
>60 TO 80
>40 TO 60
>30 TO 40
>20 TO 30
0 TO 20
DRILL HOLE
TRENCH

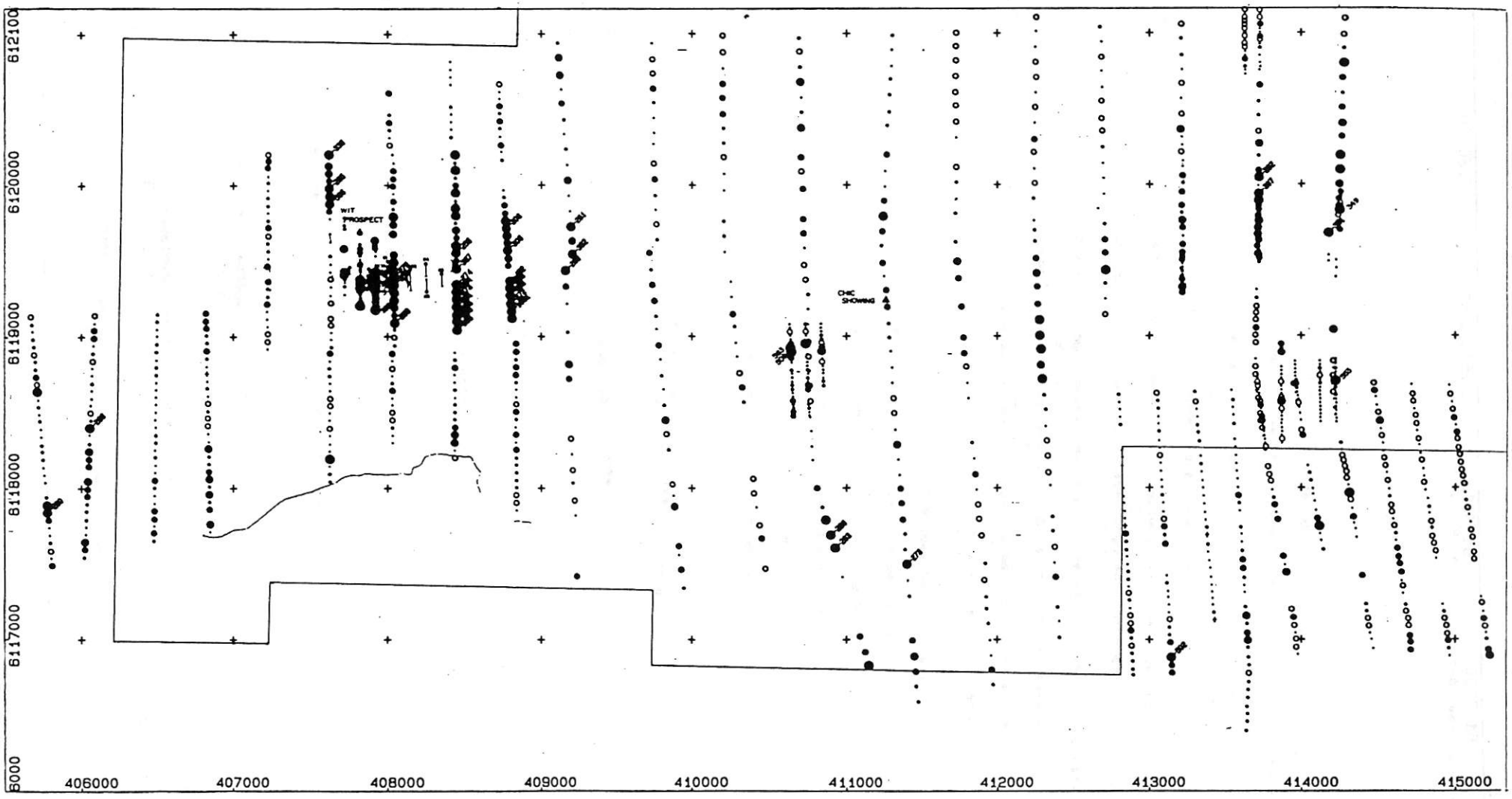
WIT - FAR EAST - KLAW GRID		
NATION RIVER RESOURCES		
1991 SOIL SURVEY		
Copper (ppm)		
	DATE: MARCH 1991	PROJECT#: A
	NTS: 93N/1W,2E	SCALE



> 20
>15 TO 20
>12 TO 15
>10 TO 12
>8 TO 10
>4 TO 8
0 TO 4
DRILL HOLE
TRENCH

WIT - FAR EAST - KLAW GRID
NATION RIVER RESOURCES
1991 SOIL SURVEY
Lead (ppm)

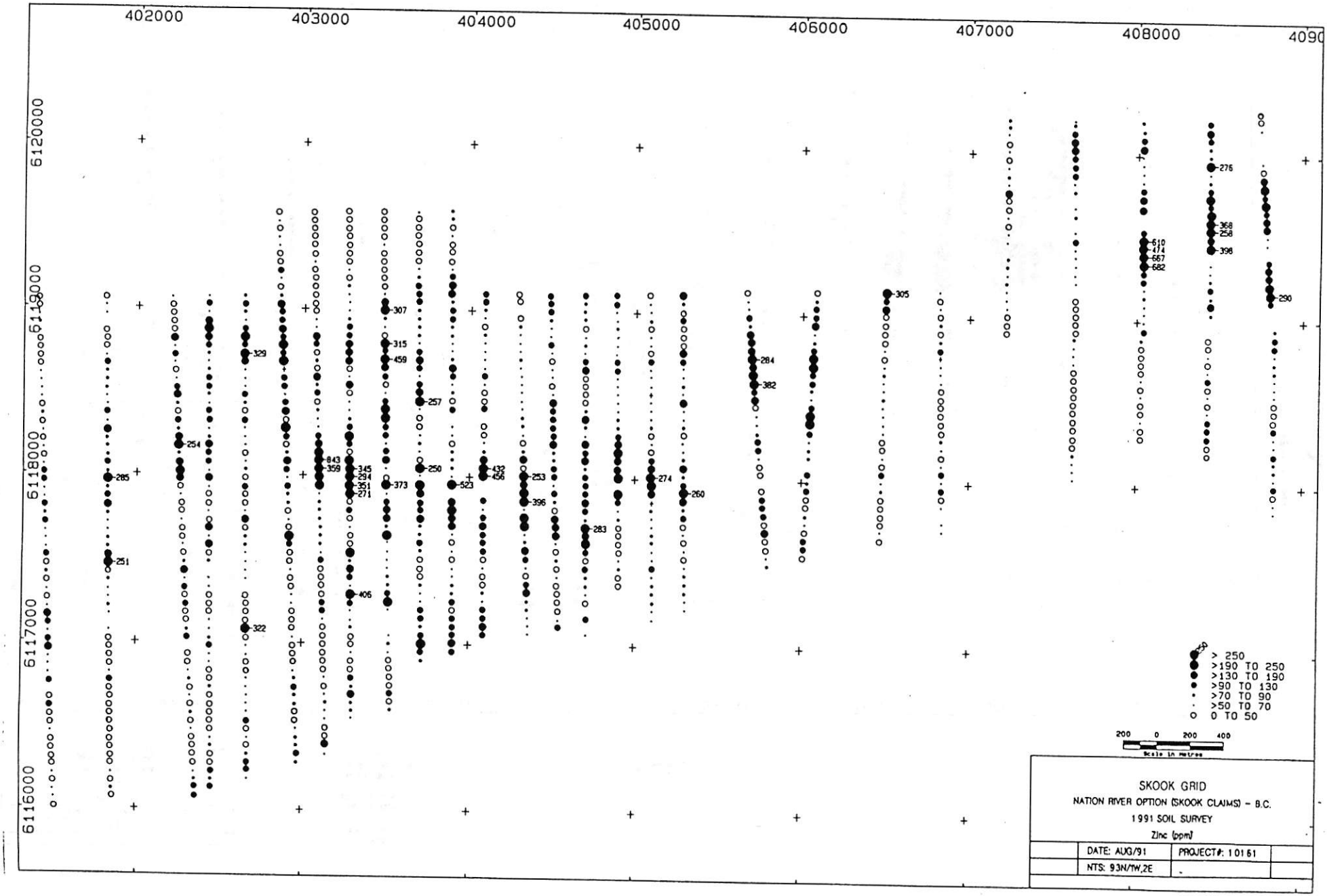
	DATE: MARCH 1995	PROJECT#: A
	NTS: 93N/W,E	SCALE

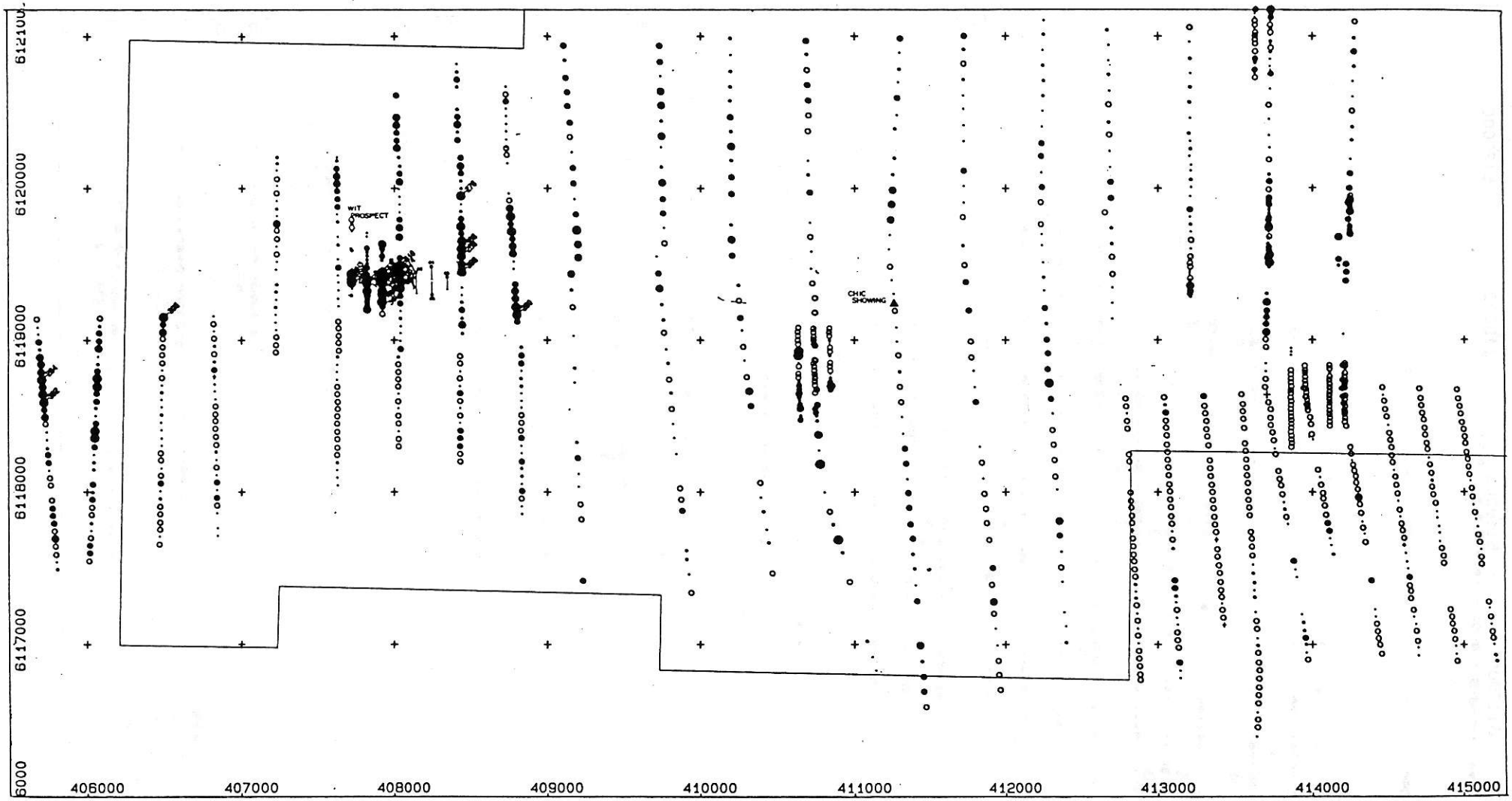


> 250
>200 TO 250
>160 TO 200
>120 TO 160
>95 TO 120
>75 TO 95
0 TO 75
DRILL HOLE
TRENCH

WIT - FAR EAST - KLAW GRID
NATION RIVER RESOURCES
1991 SOIL SURVEY
Barium (ppm)

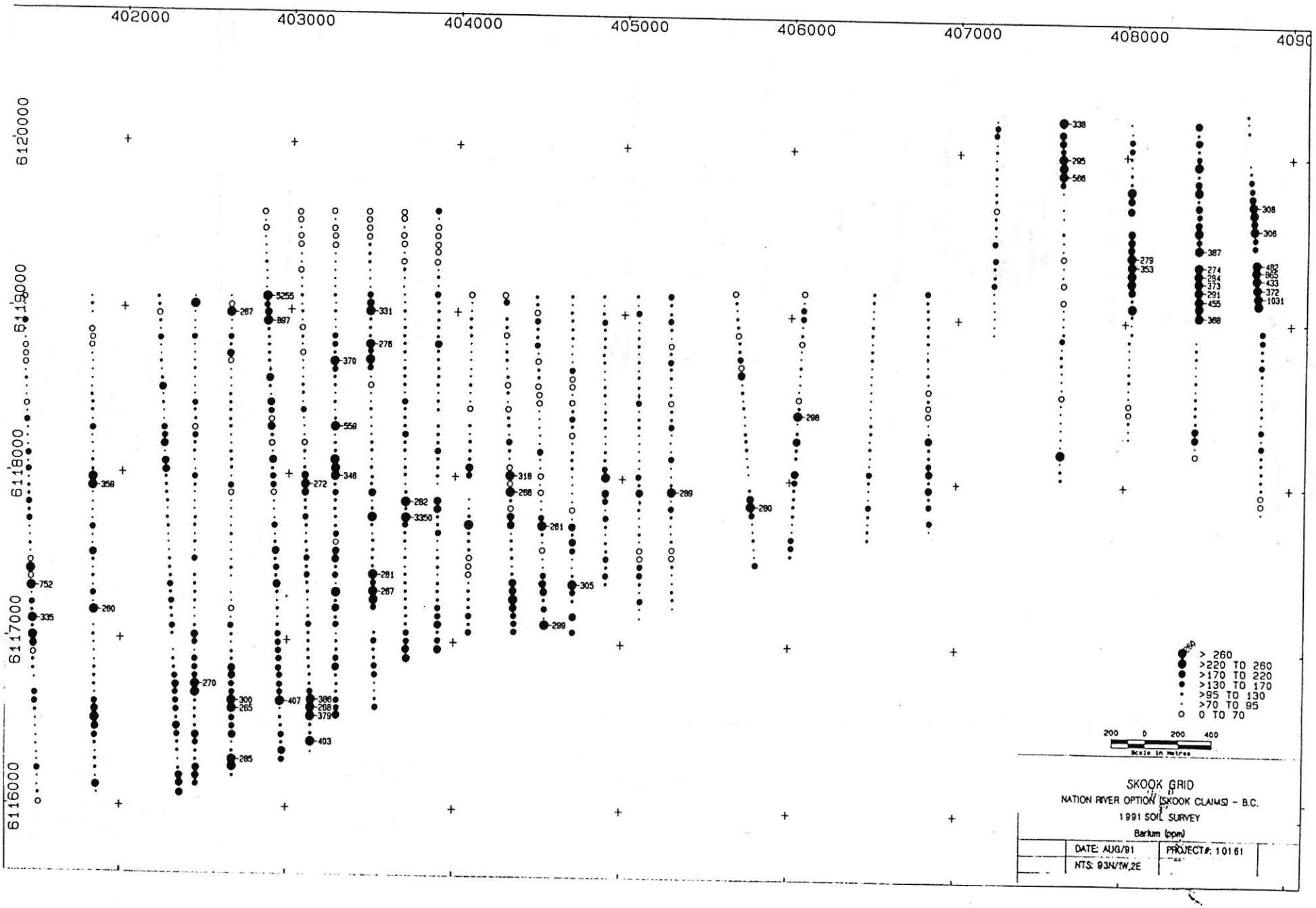
	DATE: MARCH 1995	PROJECT#: A
	NTS: 93N/7W,2E	SCALE

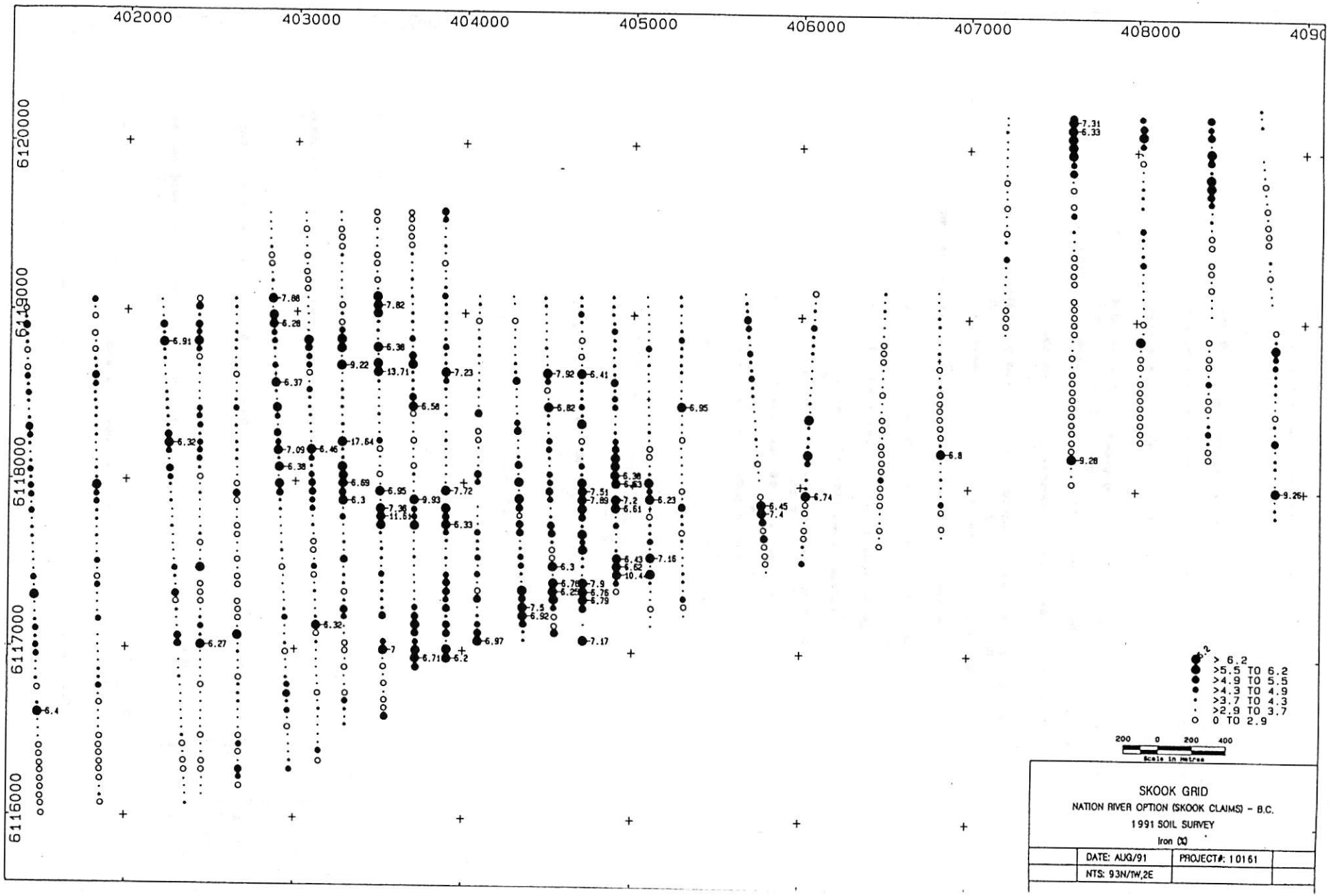

402000
403000
404000
405000
406000
407000
408000
6120000
6119000
6118000
6117000
6116000
> 250
>190 TO 250
>130 TO 190
>90 TO 130
>70 TO 90
>50 TO 70
0 TO 50
200 0 200 400
Scale in metres
SKOOK GRID
NATION RIVER OPTION (SKOOK CLAIMS) - B.C.
1991 SOIL SURVEY
Zinc (ppm)
DATE: AUG/91
PROJECT#: 10161
NTS: 93N/1W,2E



> 250
>190 TO 250
>130 TO 190
>90 TO 130
>70 TO 90
>50 TO 70
0 TO 50
DRILL HOLE
TRENCH

WIT - FAR EAST - KLAW GRID		
NATION RIVER RESOURCES		
1991 SOIL SURVEY		
Zinc (ppm)		
DATE: MARCH 1995	PROJECT#: A	
NTS: 93N/W,2E	SCALE	


402000
403000
404000
405000
406000
407000
408000
6120000
6119000
6118000
6117000
6116000
> 260
>220 TO 260
>170 TO 220
>130 TO 170
>95 TO 130
>70 TO 95
0 TO 70
200 0 200 400
Scale in Metres
SKOOK GRID
NATION RIVER OPTION (SKOOK CLAIMS) - B.C.
1991 SOIL SURVEY
Barium (ppm)
DATE: AUG/91
PROJECT#: 10161
NTS: 93N/1W,2E



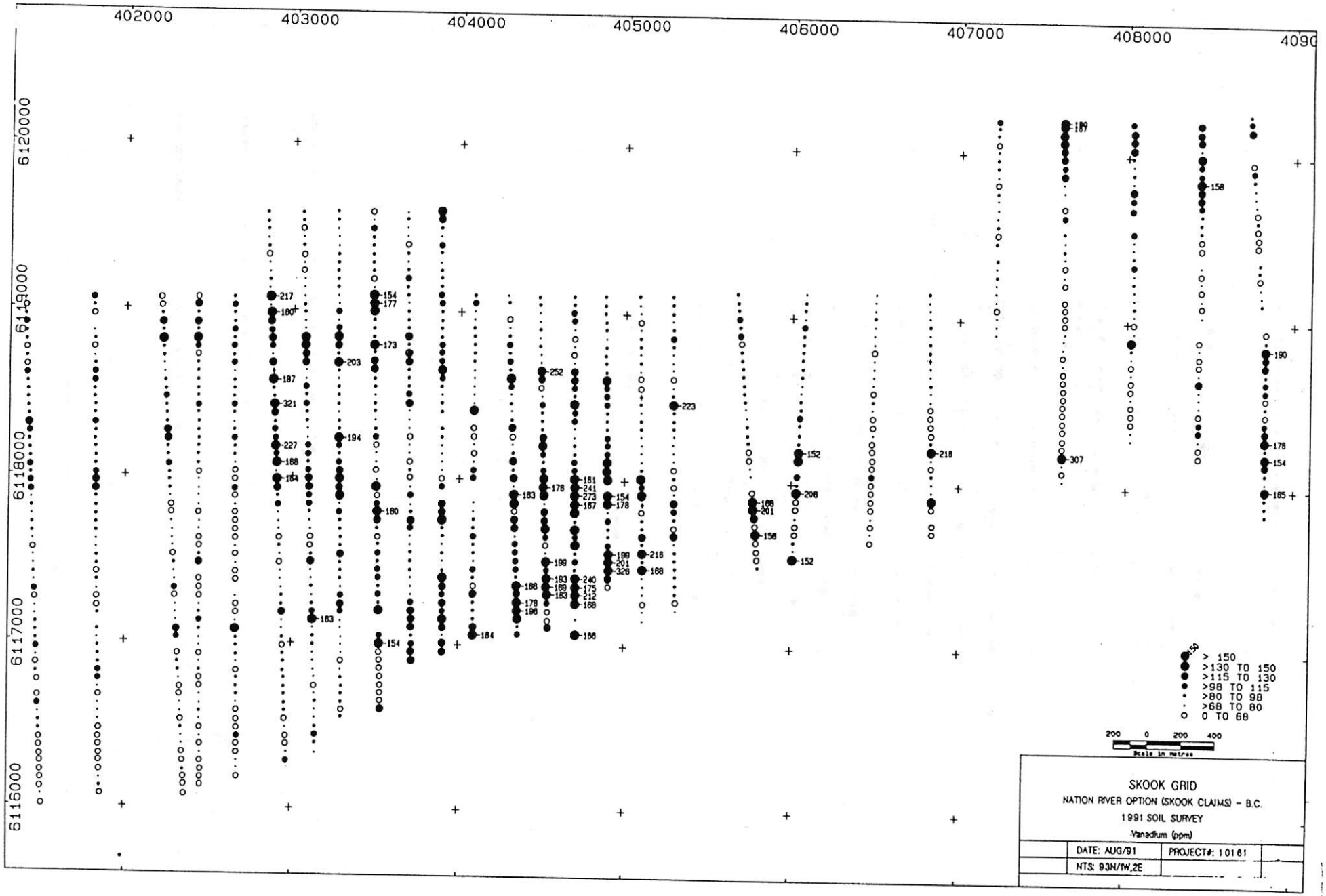
SKOOK GRID

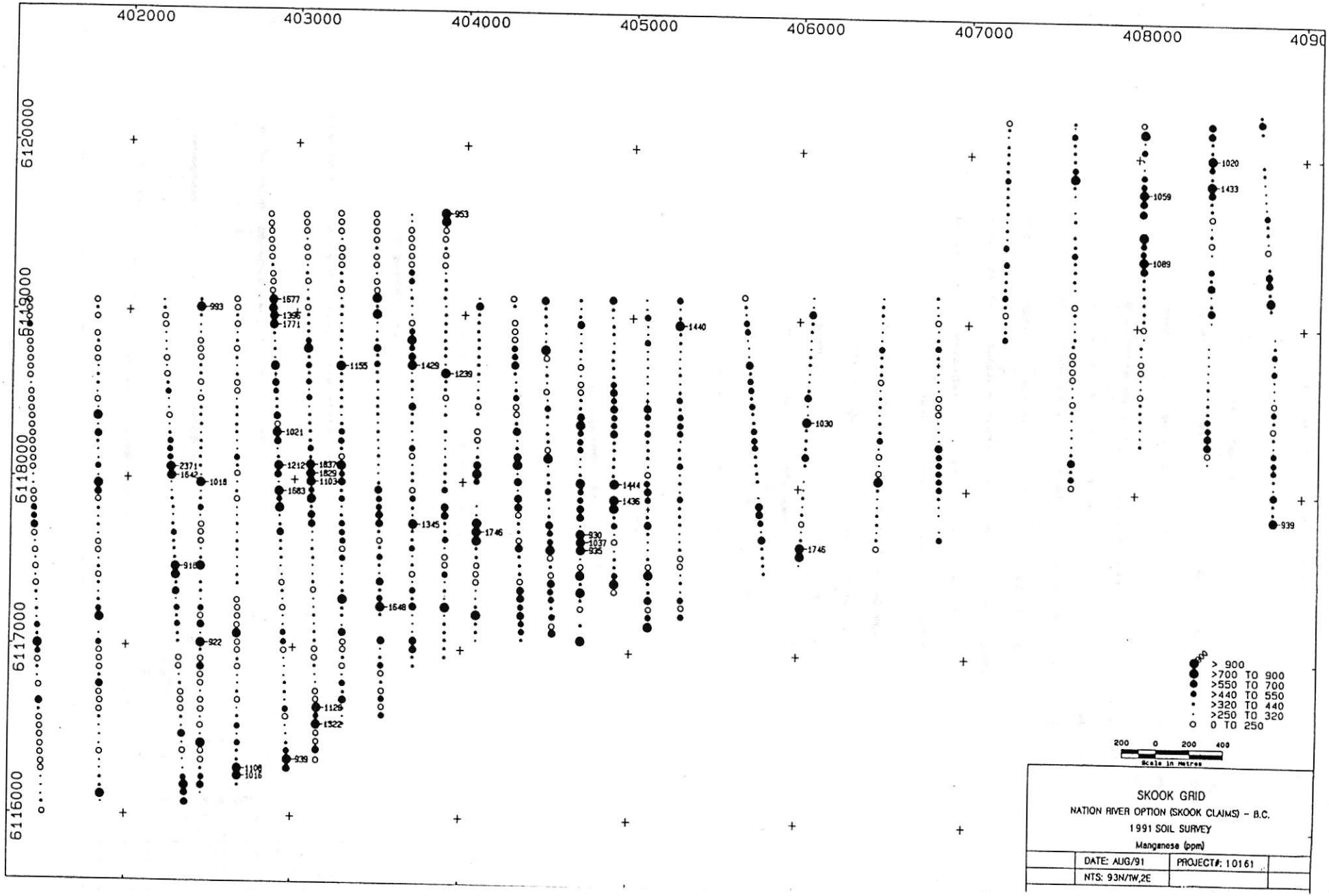
NATION RIVER OPTION (SKOOK CLAIMS) - B.C.

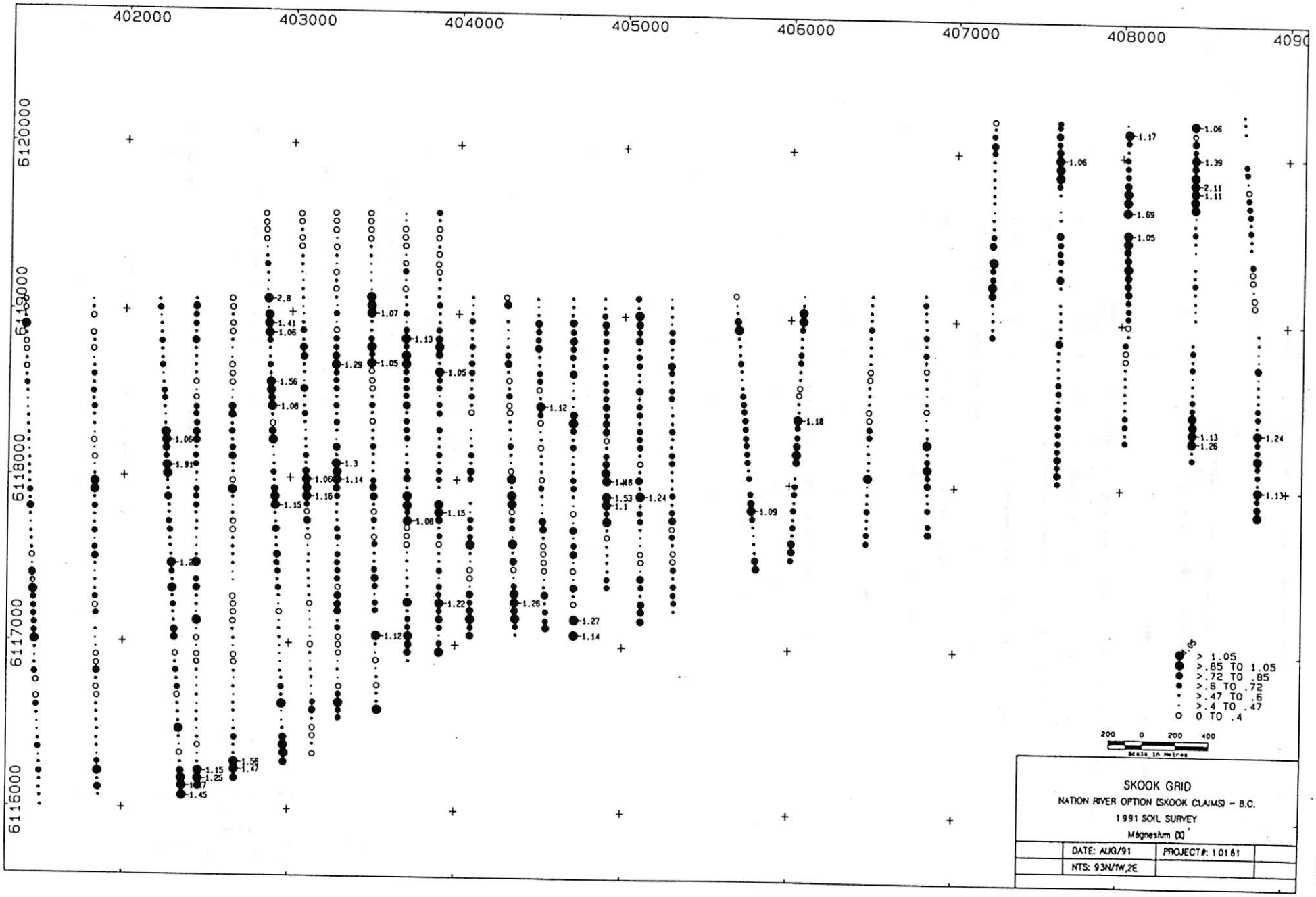
1991 SOIL SURVEY

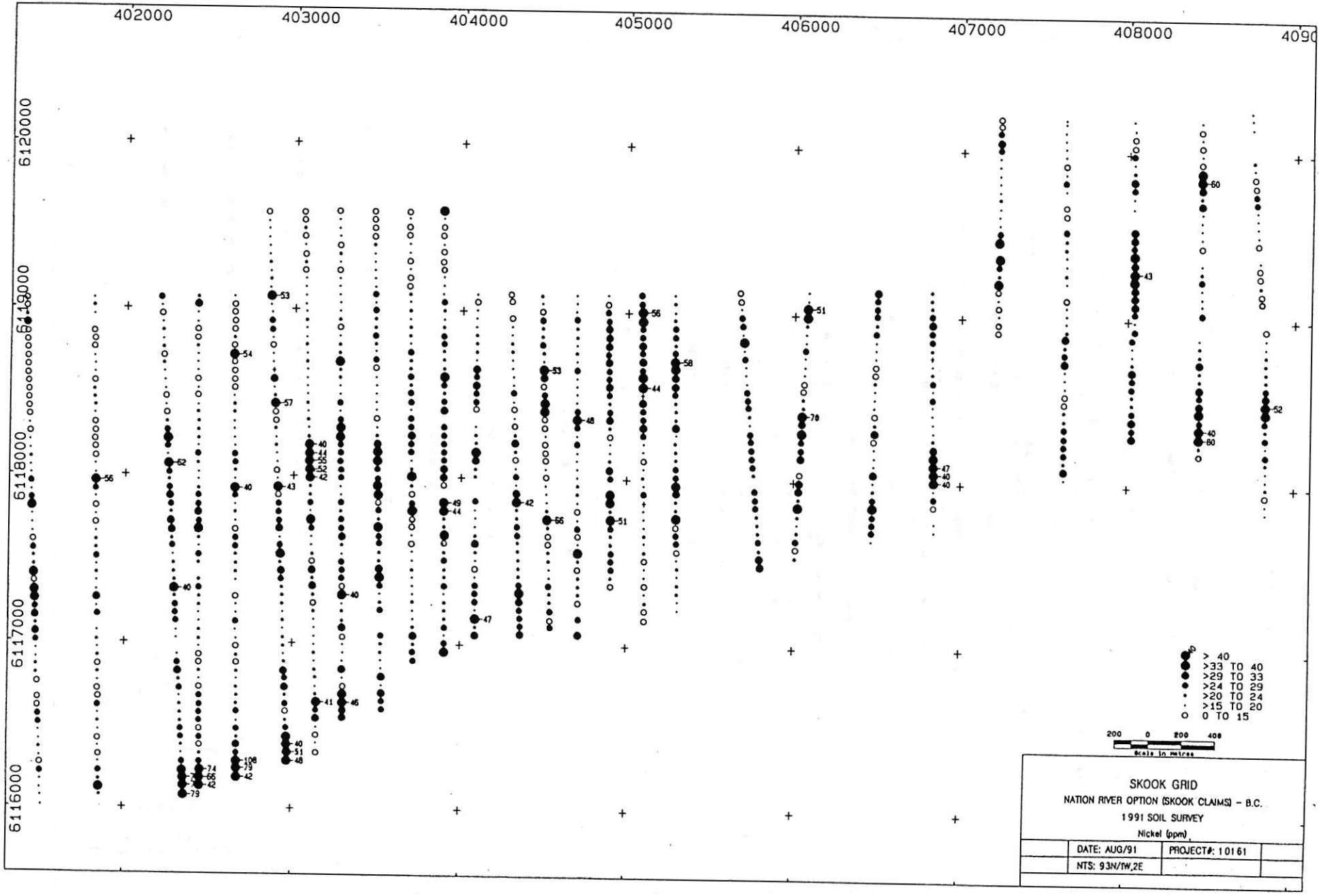
Iron (%)

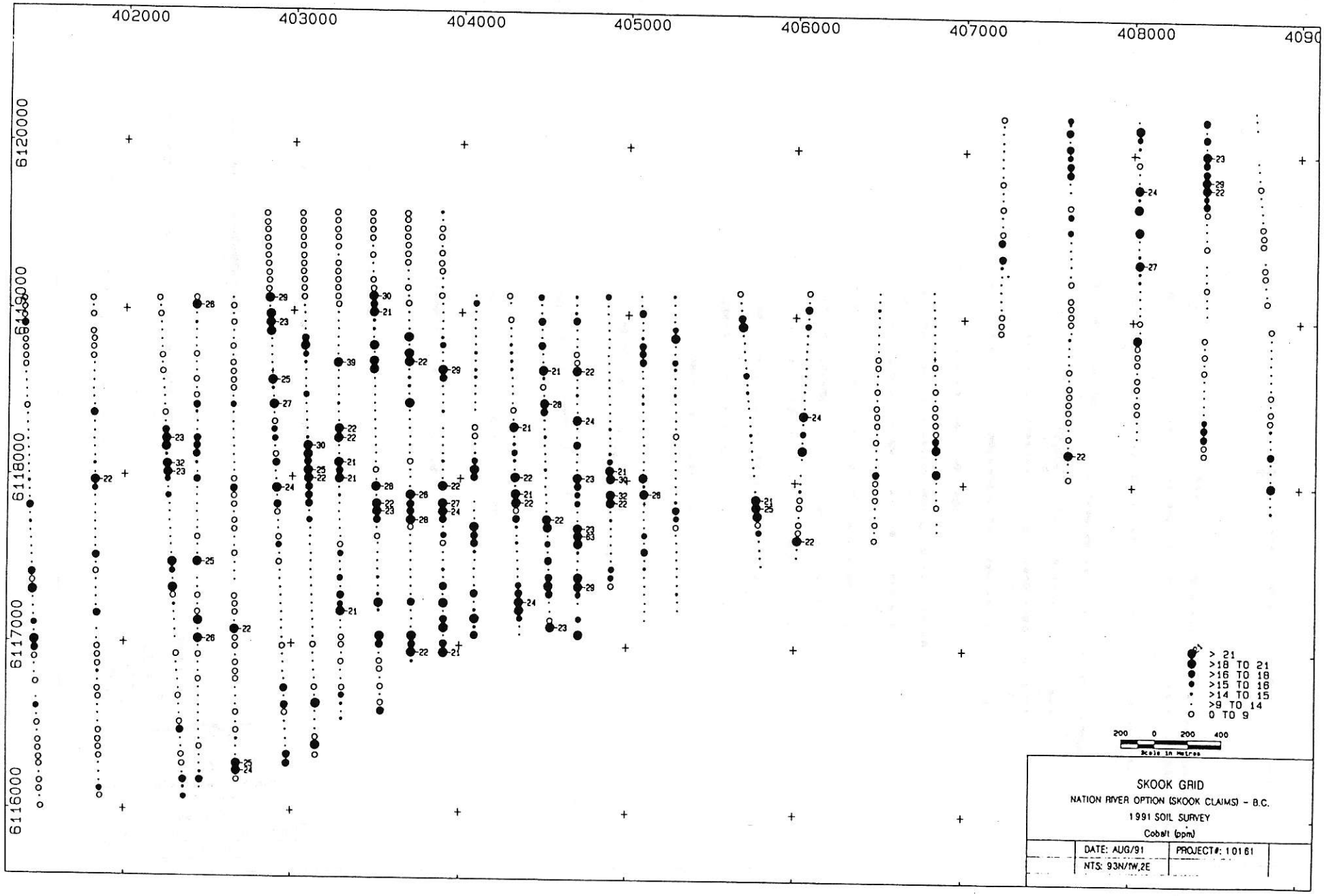
	DATE: AUG/91	PROJECT#: 10161
	NTS: 93N/1W,2E	

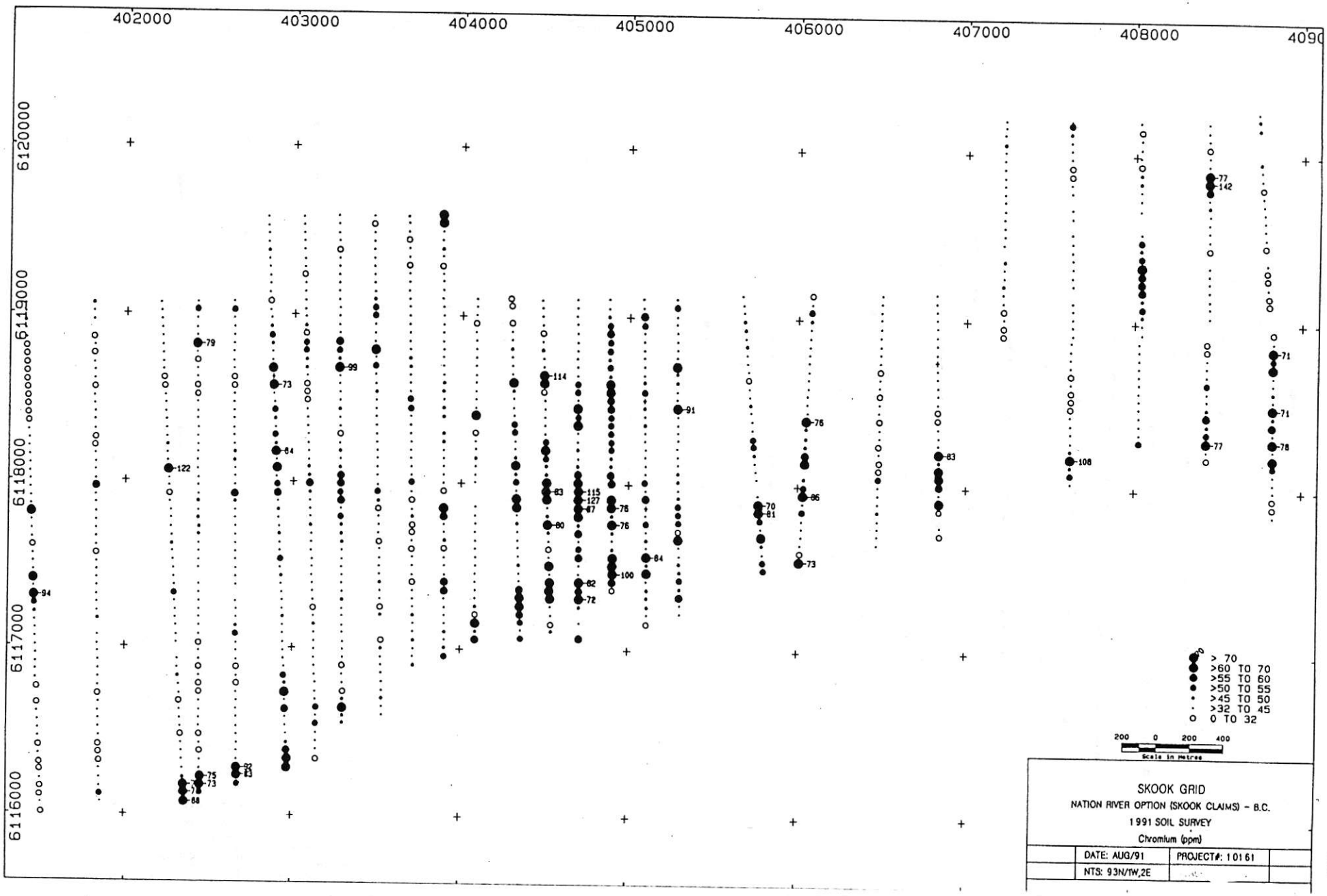

402000
403000
404000
405000
406000
407000
408000
6120000
6119000
6118000
6117000
6116000
> 150
>130 TO 150
>115 TO 130
>98 TO 115
>80 TO 98
>68 TO 80
0 TO 68
200 0 200 400
Scale in Metres
SKOOK GRID
NATION RIVER OPTION (SKOOK CLAIMS) - B.C.
1991 SOIL SURVEY
Vanadium (ppm)
DATE: AUG/91
PROJECT#: 10161
NTS: 93N/1W,2E


402000
403000
404000
405000
406000
407000
408000
6120000
6119000
6118000
6117000
6116000
> 900
>700 TO 900
>550 TO 700
>440 TO 550
>320 TO 440
>250 TO 320
0 TO 250
200 0 200 400
Scale in Metres
SKOOK GRID
NATION RIVER OPTION (SKOOK CLAIMS) - B.C.
1991 SOIL SURVEY
Manganese (ppm)
DATE: AUG/91
PROJECT#: 10161
NTS: 93N/1W,2E


402000
403000
404000
405000
406000
407000
408000
6120000
6119000
6118000
6117000
6116000
> 1.05
>.85 TO 1.05
>.72 TO .85
>.6 TO .72
>.47 TO .6
>.4 TO .47
0 TO .4
200 0 200 400
Scale in Metres
SKOOK GRID
NATION RIVER OPTION (SKOOK CLAIMS) - B.C.
1991 SOIL SURVEY
Magnesium (0)
DATE: AUG/91
PROJECT#: 10161
NTS: 93N/1W,2E


402000
403000
404000
405000
406000
407000
408000
6120000
6119000
6118000
6117000
6116000
> 40
>33 TO 40
>29 TO 33
>24 TO 29
>20 TO 24
>15 TO 20
0 TO 15
200 0 200 400
Scale in Metres
SKOOK GRID
NATION RIVER OPTION (SKOOK CLAIMS) - B.C.
1991 SOIL SURVEY
Nickel (ppm)
DATE: AUG/91
PROJECT#: 10161
NTS: 93N/1W,2E


402000
403000
404000
405000
406000
407000
408000
6120000
6119000
6118000
6117000
6116000
> 21
>18 TO 21
>16 TO 18
>15 TO 16
>14 TO 15
>9 TO 14
0 TO 9
200 0 200 400
Scale in Metres
SKOOK GRID
NATION RIVER OPTION (SKOOK CLAIMS) - B.C.
1991 SOIL SURVEY
Cobalt (ppm)
DATE: AUG/91
PROJECT#: 10161
NTS: 93N/1W,2E



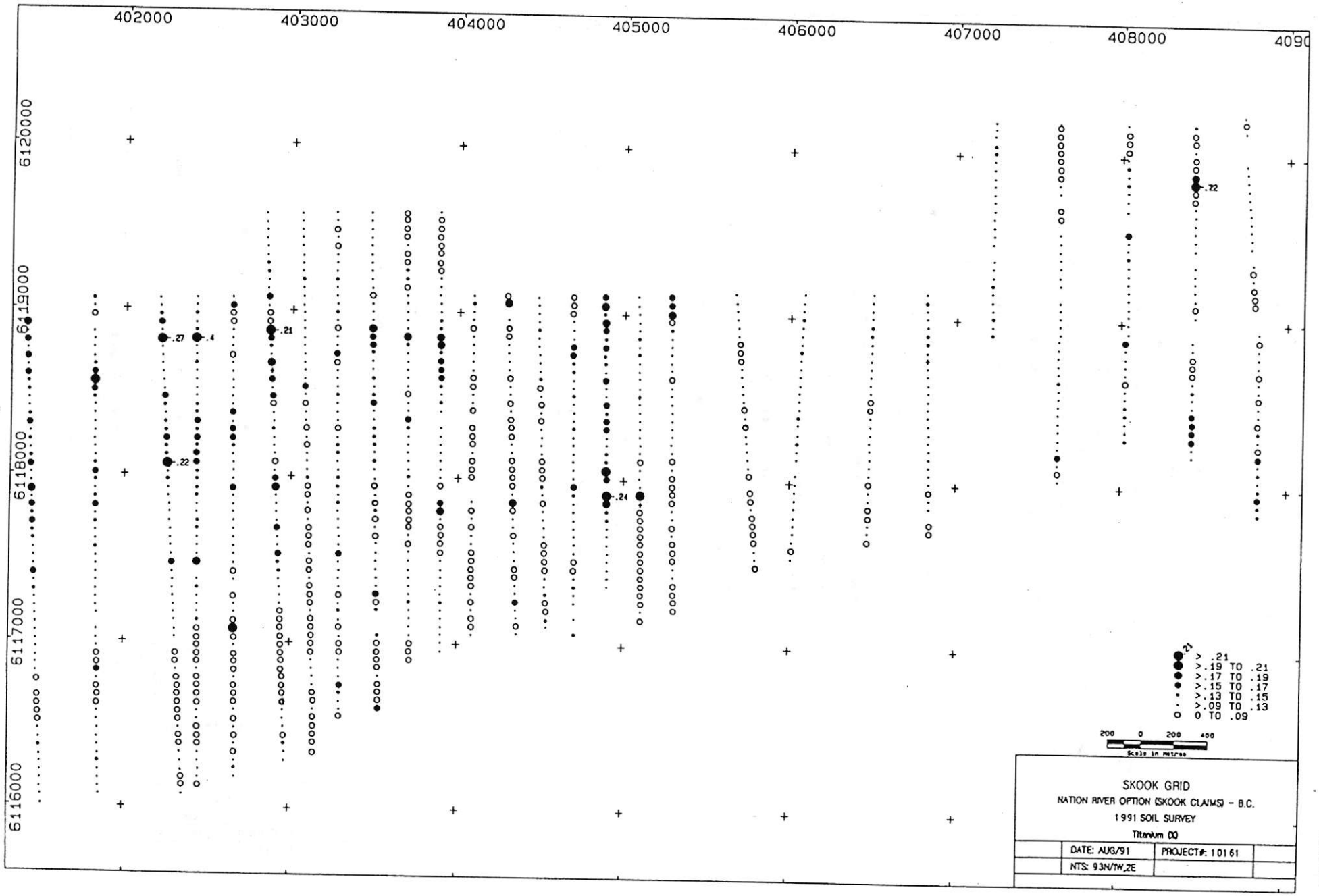
SKOOK GRID

NATION RIVER OPTION (SKOOK CLAIMS) - B.C.

1991 SOIL SURVEY

Chromium (ppm)

DATE: AUG/91	PROJECT#: 10161
NTS: 93N/1W,2E	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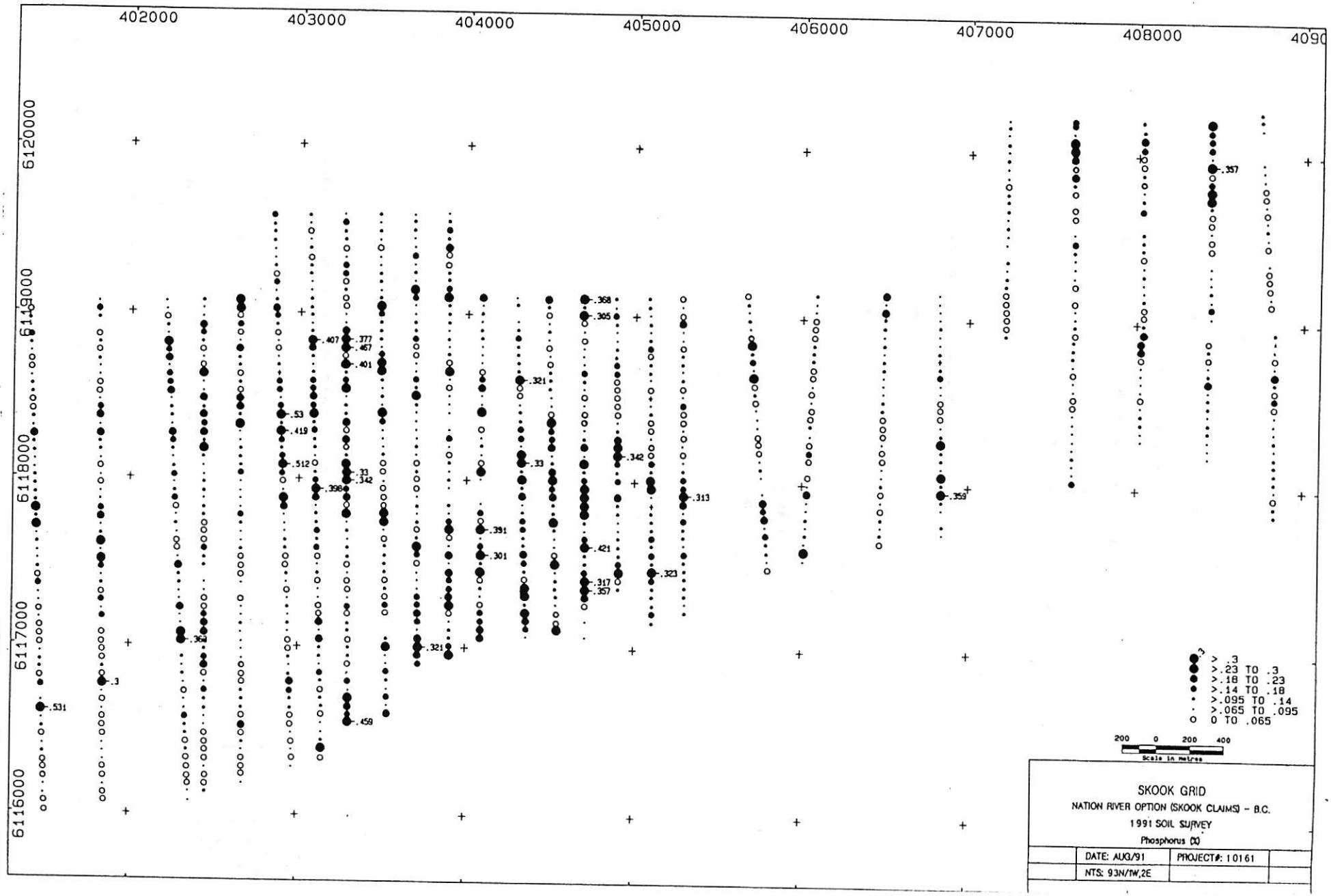
403000
404000
405000
406000
407000
408000
6120000
6119000
6118000
6117000
6116000
.27
.4
.21
.22
.24
.22
.21
> .21
>.19 TO .21
>.17 TO .19
>.15 TO .17
>.13 TO .15
>.09 TO .13
0 TO .09
200 0 200 400
Scale in metres
SKOOK GRID
NATION RIVER OPTION (SKOOK CLAIMS) - B.C.
1991 SOIL SURVEY
Titanium (X)
DATE: AUG/91
PROJECT#: 10161
NTS: 93N/1W,2E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405000
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407000
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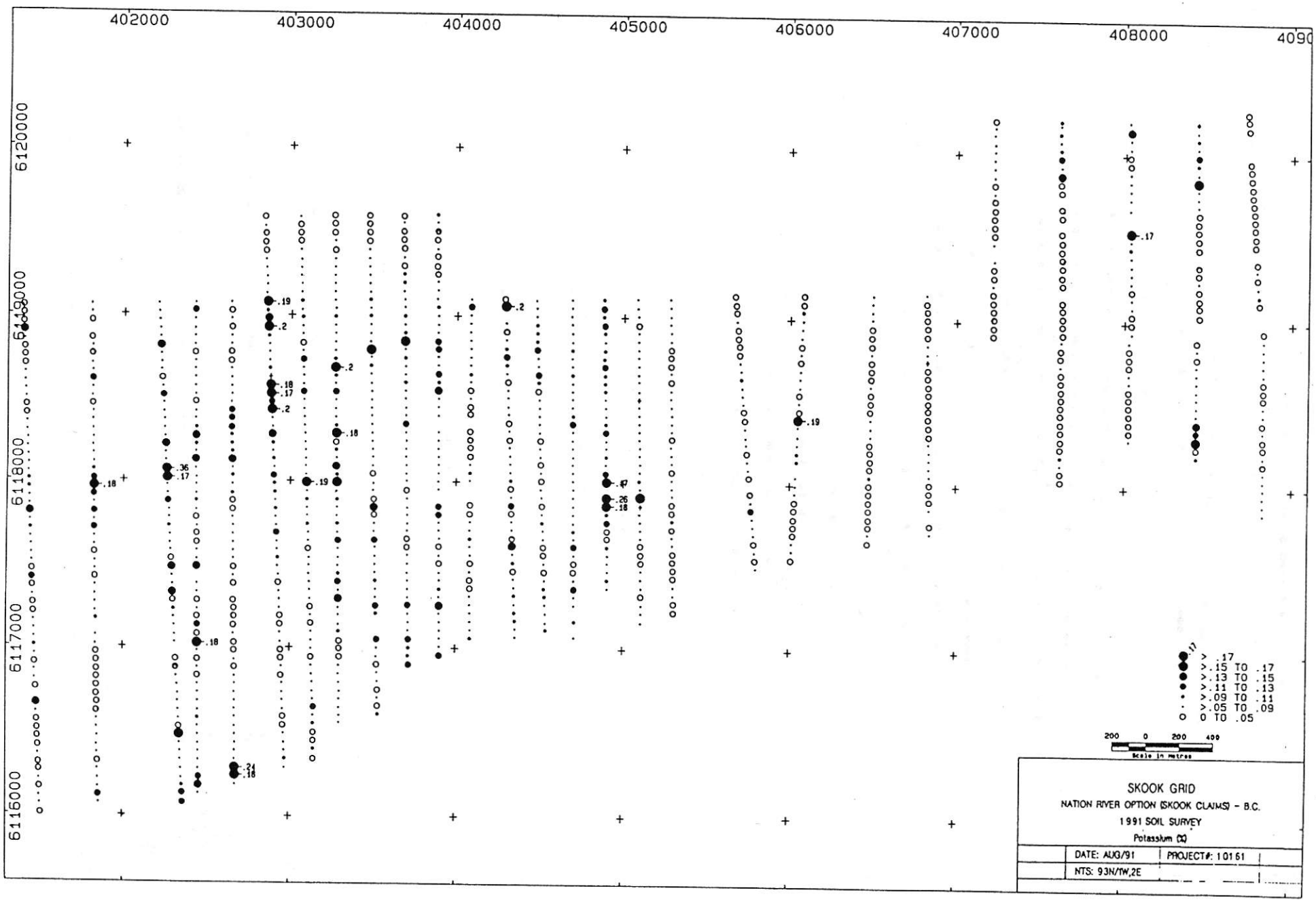
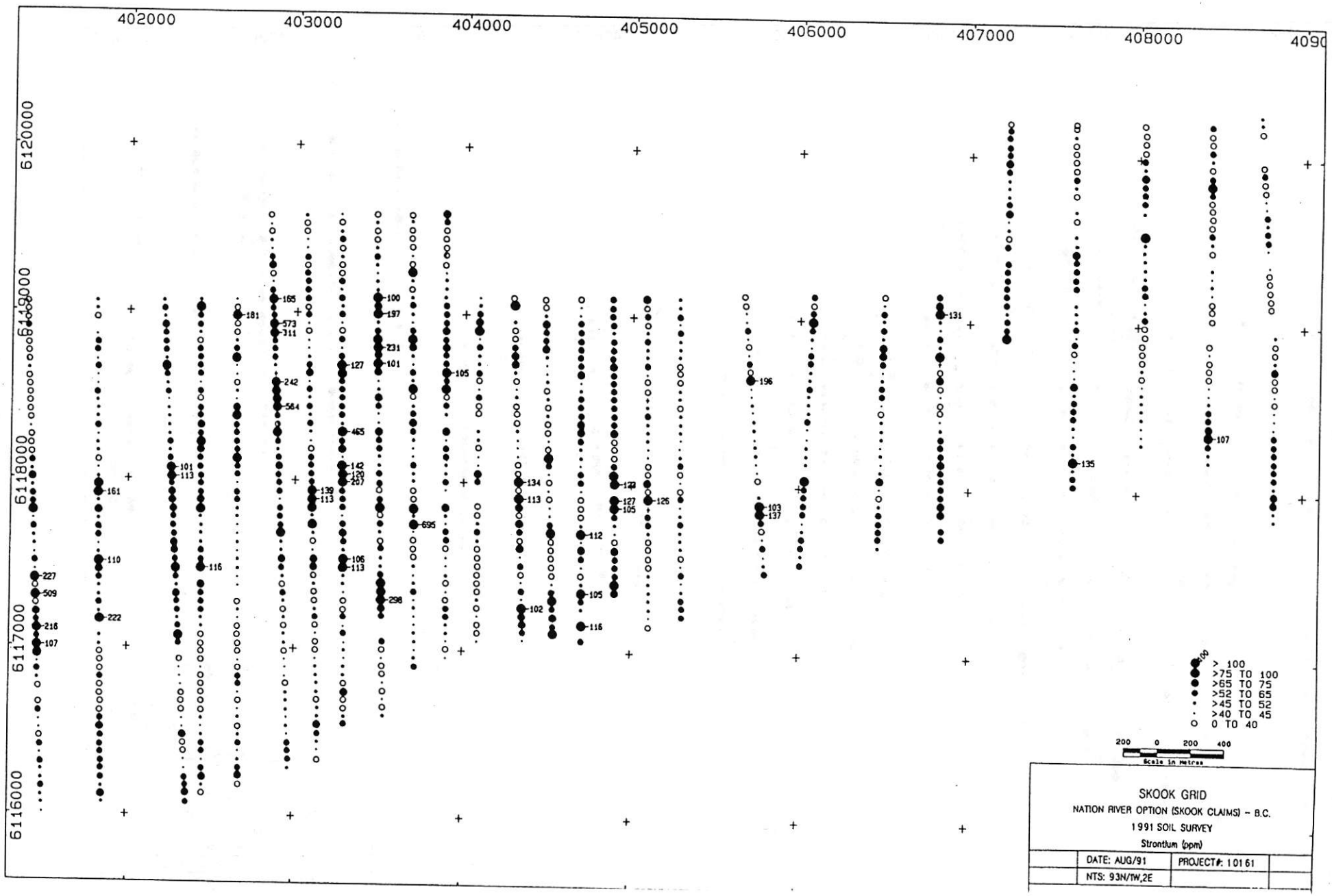
6120000
6119000
6118000
6117000
6116000
.531
.3
.364
.53
.419
.512
.398
.407
.377
.467
.401
.33
.342
.459
.321
.391
.301
.321
.33
.368
.305
.342
.421
.317
.357
.313
.323
.359
.357
> .3
>.23 TO .3
>.18 TO .23
>.14 TO .18
>.095 TO .14
>.065 TO .095
0 TO .065
200 0 200 400
Scale in Metres
SKOOK GRID
NATION RIVER OPTION (SKOOK CLAIMS) - B.C.
1991 SOIL SURVEY
Phosphorus (%)
DATE: AUG/91
PROJECT#: 10161
NTS: 93N/1W,2E


402000
403000
404000
405000
406000
407000
408000
6120000
6119000
6118000
6117000
6116000
> .17
>.15 TO .17
>.13 TO .15
>.11 TO .13
>.09 TO .11
>.05 TO .09
0 TO .05
200 0 200 400
Scale in metres
SKOOK GRID
NATION RIVER OPTION (SKOOK CLAIMS) - B.C.
1991 SOIL SURVEY
Potassium (%)
DATE: AUG/91
PROJECT#: 10161
NTS: 93N/1W,2E



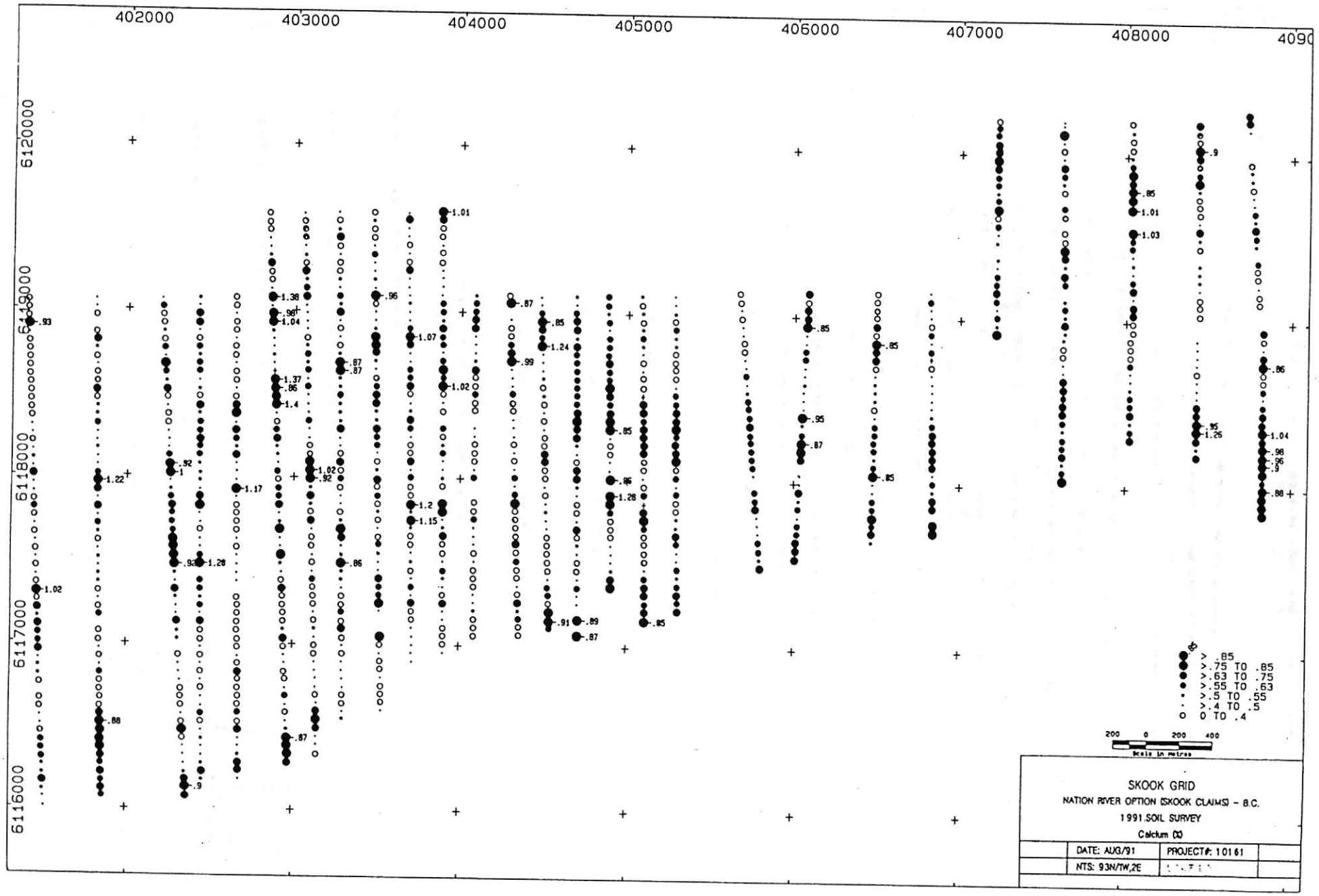
SKOOK GRID

NATION RIVER OPTION (SKOOK CLAIMS) - B.C.

1991 SOIL SURVEY

Strontium (ppm)

	DATE: AUG/91	PROJECT#: 10161
	NTS: 93N/1W,2E	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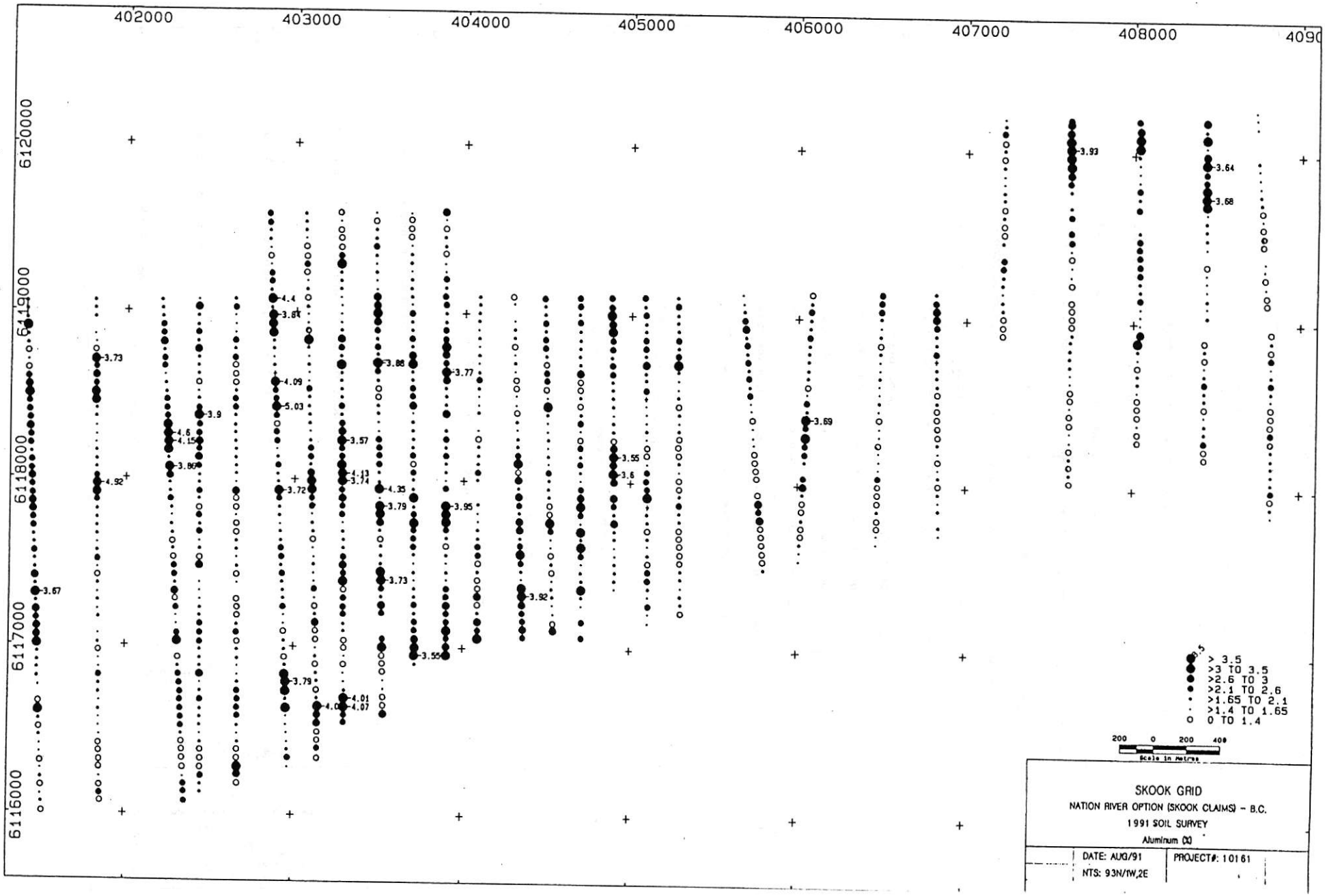
403000
404000
405000
406000
407000
408000
6120000
6119000
6118000
6117000
6116000
> .85
>.75 TO .85
>.63 TO .75
>.55 TO .63
>.5 TO .55
>.4 TO .5
0 TO .4
200 0 200 400
Scale in metres
SKOOK GRID
NATION RIVER OPTION (SKOOK CLAIMS) - B.C.
1991 SOIL SURVEY
Calcium (Ca)
DATE: AUG/91
PROJECT#: 10161
NTS: 93N/7W,2E



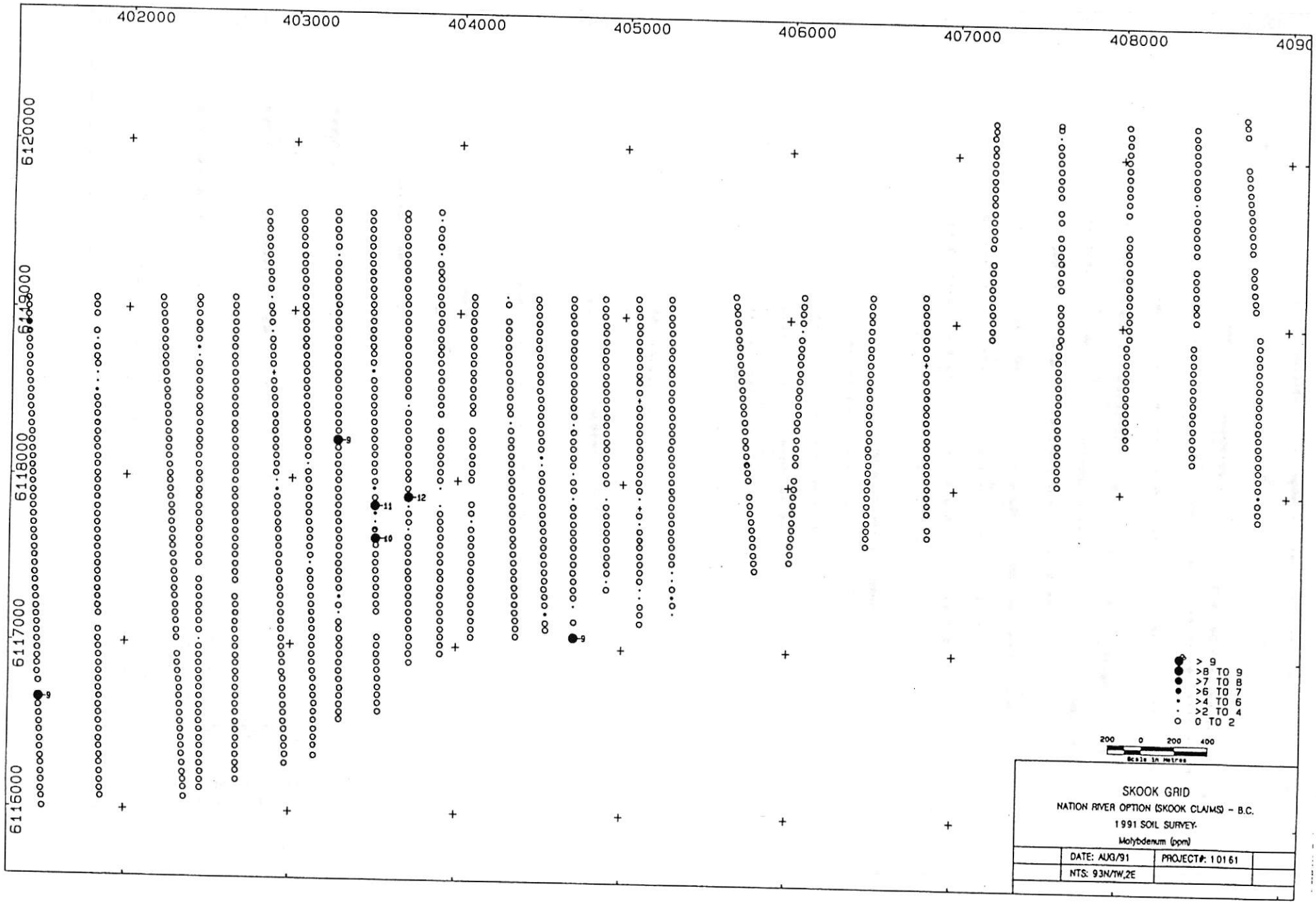
SKOOK GRID

NATION RIVER OPTION (SKOOK CLAIMS) - B.C.

1991 SOIL SURVEY

Aluminum (%)

DATE: AUG/91	PROJECT#: 10161
NTS: 93N/1W,2E	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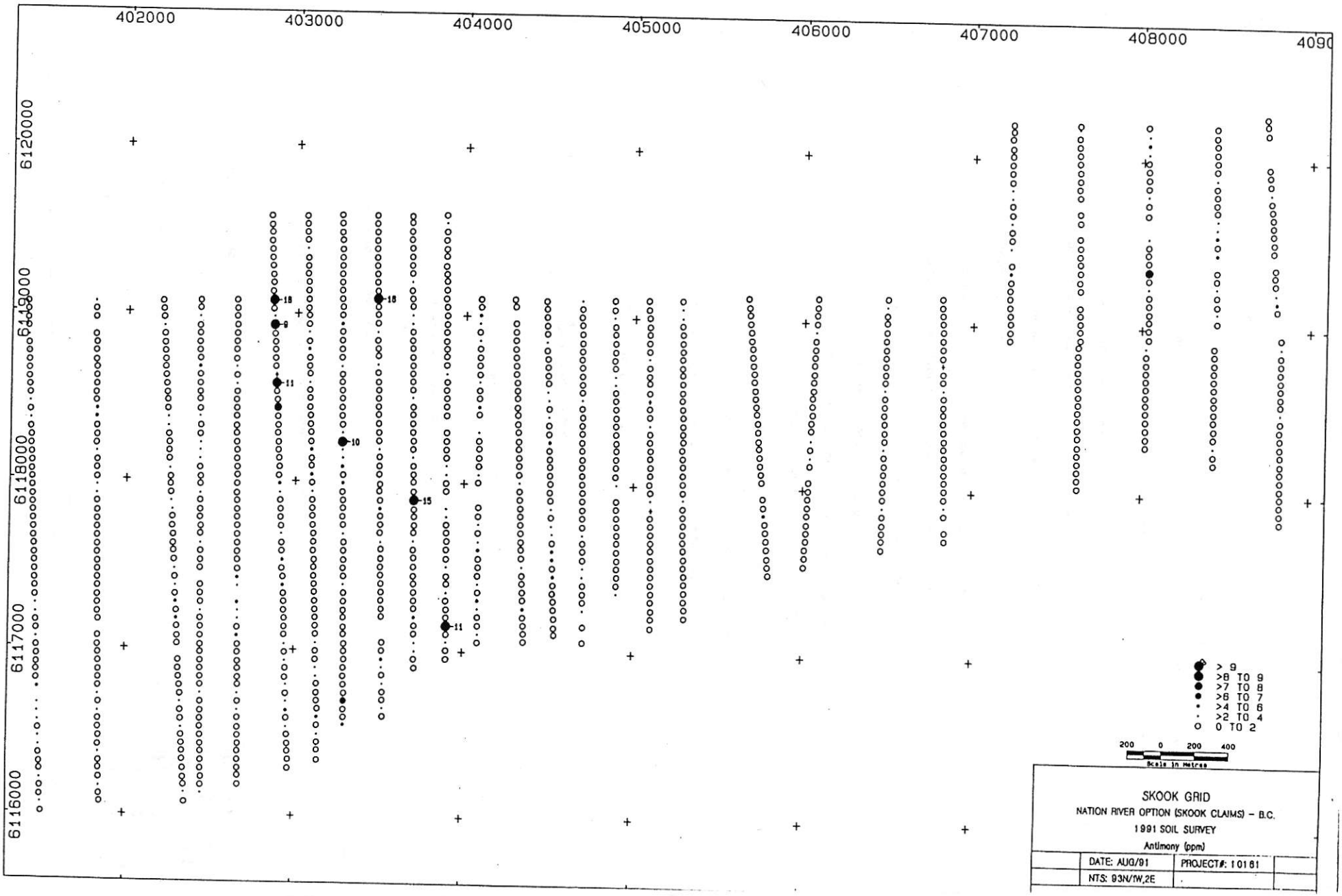
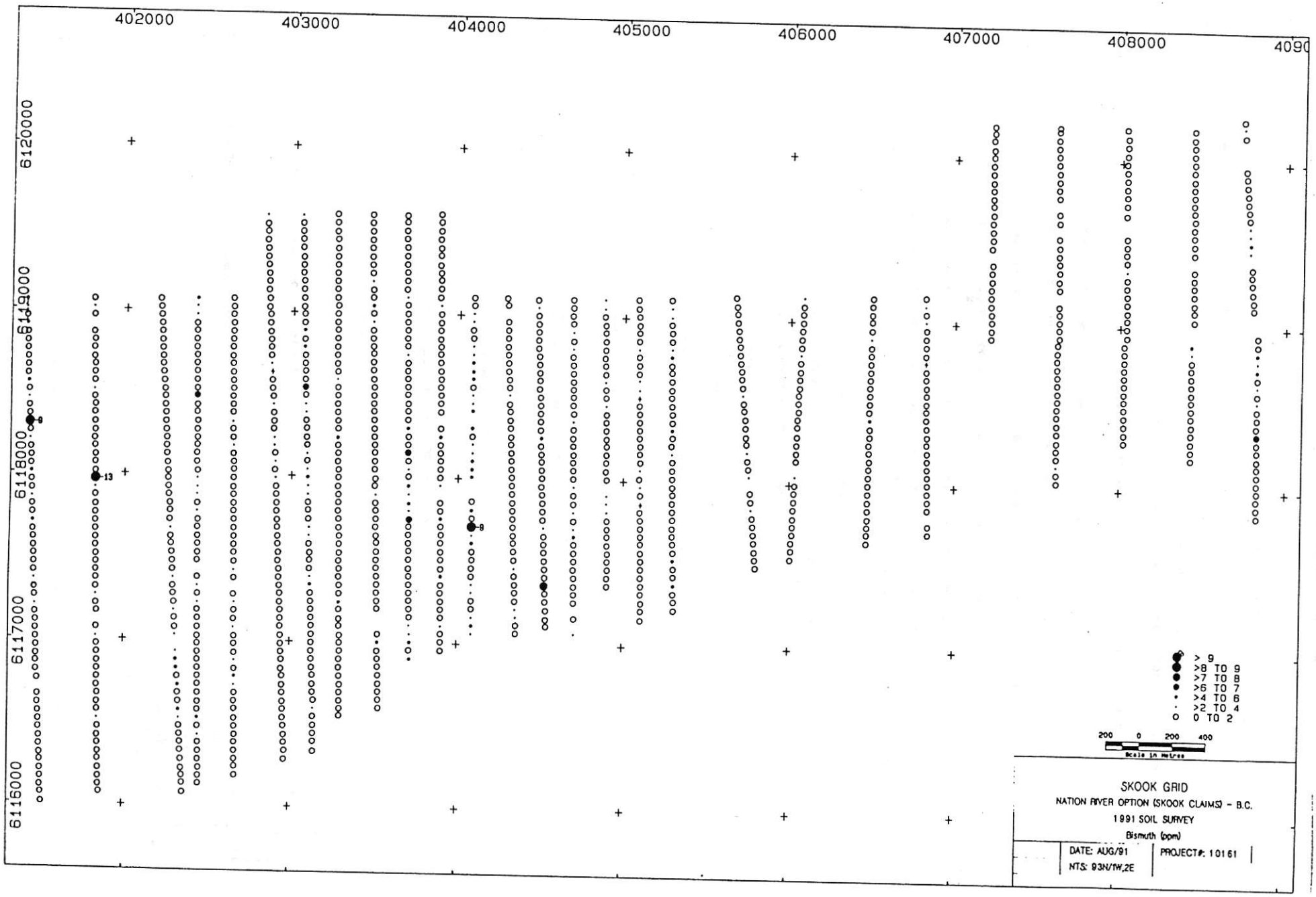
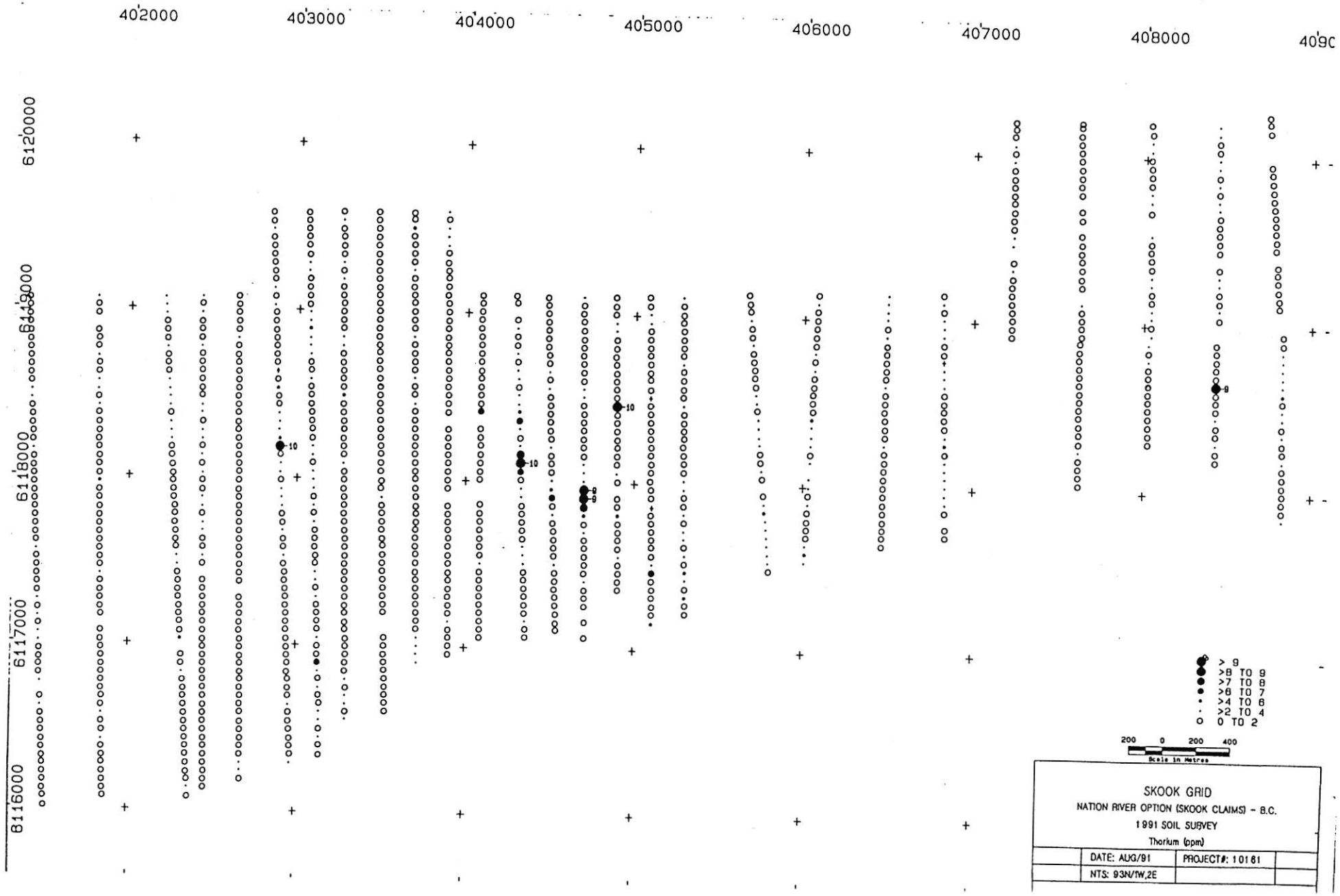
403000
404000
405000
406000
407000
408000
6120000
6119000
6118000
6117000
6116000
> 9
>8 TO 9
>7 TO 8
>6 TO 7
>4 TO 6
>2 TO 4
0 TO 2
200 0 200 400
Scale in Metres
SKOOK GRID
NATION RIVER OPTION (SKOOK CLAIMS) - B.C.
1991 SOIL SURVEY.
Molybdenum (ppm)
DATE: AUG/91
PROJECT#: 10161
NTS: 93N/7W,2E


402000
403000
404000
405000
406000
407000
408000
6120000
6119000
6118000
6117000
6116000
> 9
>8 TO 9
>7 TO 8
>6 TO 7
>4 TO 6
>2 TO 4
0 TO 2
200 0 200 400
Scale in Metres
SKOOK GRID
NATION RIVER OPTION (SKOOK CLAIMS) - B.C.
1991 SOIL SURVEY
Antimony (ppm)
DATE: AUG/91
PROJECT#: 10161
NTS: 93N/1W,2E


402000
403000
404000
405000
406000
407000
408000
6120000
6119000
6118000
6117000
6116000
> 9
>8 TO 9
>7 TO 8
>6 TO 7
>4 TO 6
>2 TO 4
0 TO 2
200 0 200 400
Scale in Metres
SKOOK GRID
NATION RIVER OPTION (SKOOK CLAIMS) - B.C.
1991 SOIL SURVEY
Bismuth (ppm)
DATE: AUG/91
NTS: 93N/1W,2E
PROJECT#: 10161


402000
403000
404000
405000
406000
407000
408000
6120000
6119000
6118000
6117000
6116000
> 9
>8 TO 9
>7 TO 8
>6 TO 7
>4 TO 6
>2 TO 4
0 TO 2
200 0 200 400
Scale in Metres
SKOOK GRID
NATION RIVER OPTION (SKOOK CLAIMS) - B.C.
1991 SOIL SURVEY
Thorium (ppm)
DATE: AUG/91
PROJECT#: 10161
NTS: 93N/1W,2E

APPENDIX B - Soil Analytical Results

ACME A[illegible]YTICAL LABORATORIES LTD. 852 E. HASTINGS ST. [illegible]OUVER B.C. V6A 1R6 PHONE(604)253-3158 FA[illegible])253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

BP Resources Canada Ltd. PROJECT LOC-10161 File # 91-1730 Page 1

700 - 890 W. Pender St., Vancouver BC V6B 4W3

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
130001	1	20	6	42	.3	15	8	164	3.18	8	5	ND	2	35	.5	2	5	76	.37	.079	8	38	.33	69	.10	2	1.91	.01	.05	1	9
130002	1	22	5	49	.2	13	8	176	2.79	6	5	ND	2	31	.4	2	3	61	.30	.061	8	36	.40	71	.10	2	1.93	.01	.05	1	11
130003	2	23	2	64	.1	21	9	240	4.14	4	5	ND	2	32	.2	2	2	91	.34	.120	9	49	.50	95	.10	2	1.89	.01	.05	1	5
130004	7	176	4	73	.4	30	18	505	5.04	30	5	ND	2	58	.2	2	5	112	.93	.072	12	39	.92	161	.18	4	3.24	.03	.15	1	5
130005	2	29	2	54	.3	13	9	219	4.12	16	5	ND	2	40	.3	3	2	93	.44	.151	8	34	.48	86	.13	4	1.68	.01	.07	1	5
130006	1	16	2	48	.2	12	8	160	3.84	10	5	ND	2	33	.2	2	2	97	.27	.110	6	31	.40	78	.16	2	1.66	.01	.05	1	5
130007	2	13	5	50	.4	11	6	144	2.81	7	5	ND	2	30	.3	2	2	66	.26	.083	7	29	.25	51	.10	2	1.17	.01	.04	1	12
130008	2	43	2	46	.1	15	9	208	2.95	4	5	ND	2	31	.2	2	2	82	.26	.019	7	31	.55	43	.16	2	1.64	.01	.04	1	6
130009	2	27	2	42	.2	7	5	136	2.27	3	5	ND	1	47	.2	2	2	64	.29	.039	7	18	.25	65	.11	2	1.12	.01	.06	1	3
130010	2	43	4	55	.4	14	11	217	4.49	12	5	ND	2	33	.2	2	2	106	.31	.070	6	30	.52	82	.16	3	2.30	.01	.07	1	9
130011	2	66	2	56	.2	13	11	251	3.85	9	5	ND	2	39	.3	2	6	85	.40	.127	8	30	.63	99	.14	3	2.78	.02	.09	1	5
130012	1	46	2	57	.2	15	12	218	4.40	11	5	ND	3	34	.2	2	2	97	.34	.121	7	31	.56	83	.15	2	3.30	.02	.08	1	4
130013	2	38	2	53	.6	13	10	180	4.18	9	5	ND	3	34	.2	3	3	89	.36	.055	6	31	.44	83	.12	3	2.37	.01	.05	1	3
130014	1	30	2	39	.2	11	9	156	3.56	9	5	ND	1	33	.2	2	2	92	.38	.053	5	32	.41	67	.13	2	2.19	.02	.05	1	3
130015	2	37	2	77	.2	13	10	216	3.84	13	5	ND	2	34	.4	3	2	90	.36	.111	6	30	.49	91	.14	2	2.53	.02	.07	1	3
130016	1	51	3	50	.1	18	14	231	5.43	11	5	ND	1	43	.2	2	9	128	.43	.066	7	43	.60	139	.16	2	2.63	.02	.07	1	4
130017	1	56	2	53	.1	14	11	232	4.34	13	5	ND	2	36	.2	2	2	102	.41	.207	6	35	.60	76	.13	2	2.34	.02	.07	1	1
130018	1	66	7	48	.1	20	12	192	3.73	15	5	ND	2	37	.2	2	3	91	.40	.112	6	38	.49	76	.14	2	2.54	.02	.07	1	4
130019	1	39	2	63	.2	16	11	193	3.51	8	5	ND	3	39	.2	2	2	89	.46	.123	6	34	.44	83	.13	5	1.83	.02	.06	1	1
130020	1	62	4	44	.1	21	14	223	3.83	15	5	ND	2	54	.3	2	2	92	.52	.078	7	36	.57	132	.14	2	2.31	.02	.09	1	1
130021	1	40	5	63	.1	16	11	208	4.67	9	5	ND	2	46	.2	2	2	108	.45	.084	6	35	.51	87	.17	2	2.24	.02	.08	1	4
130022	1	51	5	98	.1	16	12	272	3.97	2	6	ND	1	74	.2	2	6	91	.70	.119	5	33	.55	154	.13	2	2.61	.01	.10	1	1
130023	1	107	7	111	.1	26	15	286	4.36	28	5	ND	2	52	.2	2	2	101	.50	.104	6	40	.60	86	.13	2	2.40	.02	.10	1	4
130024	1	57	2	55	.3	16	11	230	4.67	32	5	ND	2	53	.2	2	2	102	.50	.098	6	35	.65	112	.18	2	2.43	.02	.08	1	1
130025	1	60	8	64	.1	27	14	223	3.70	12	5	ND	2	58	.2	2	4	78	.40	.105	6	40	.56	113	.13	4	2.90	.02	.08	1	1
130026	1	50	6	99	.1	37	18	471	4.57	6	5	ND	1	95	.2	2	2	89	.61	.239	5	67	.79	155	.17	2	2.95	.02	.14	1	1
130027	1	56	2	75	.2	18	14	454	3.51	11	5	ND	2	45	.2	2	2	77	.38	.127	6	35	.49	101	.14	4	2.31	.02	.07	1	1
130028	1	73	2	99	.1	20	15	587	3.92	6	5	ND	1	53	.2	2	5	86	.45	.243	5	34	.45	155	.17	2	2.60	.01	.11	1	3
130029	1	44	2	51	.1	19	13	242	3.73	8	5	ND	1	46	.3	2	2	91	.40	.075	6	35	.49	78	.15	2	1.96	.02	.07	1	1
130030	1	30	2	66	.2	15	12	253	3.59	6	5	ND	2	46	.3	2	2	80	.44	.133	6	31	.48	87	.14	2	1.95	.02	.07	1	1
130031	1	48	2	52	.1	28	12	232	3.35	7	5	ND	3	41	.2	2	2	66	.31	.077	9	41	.55	103	.13	2	2.49	.01	.06	1	3
130032	1	27	2	94	.1	21	13	256	3.32	7	5	ND	2	53	.2	2	2	72	.46	.080	8	38	.40	86	.12	2	1.70	.01	.06	1	16
130033	1	42	4	48	.1	22	10	193	3.51	5	5	ND	2	42	.2	2	2	73	.36	.127	7	39	.42	65	.12	2	1.99	.01	.05	1	6
130034	1	77	2	89	.3	35	17	268	4.72	10	5	ND	2	227	.2	2	2	98	.50	.061	7	65	.79	225	.16	2	2.78	.01	.13	1	2
130035	1	42	4	46	.1	15	7	175	3.40	4	5	ND	2	38	.2	2	3	77	.29	.159	7	41	.34	67	.12	4	2.03	.01	.03	1	5
130036	1	66	5	54	.3	34	19	424	5.56	10	5	ND	2	509	.2	2	2	110	1.02	.094	5	94	.92	752	.14	2	3.67	.05	.09	1	3
RE 130031	2	48	3	53	.3	29	13	243	3.39	9	5	ND	4	42	.3	2	2	66	.31	.078	9	42	.56	105	.14	4	2.52	.02	.07	1	3
STANDARD C/AU-S	19	56	38	132	7.3	73	31	1062	4.01	41	17	7	39	53	18.9	14	21	56	.50	.093	40	60	.91	180	.10	34	1.98	.06	.15	11	46
STANDARD C	18	56	38	132	6.9	70	32	1034	3.96	38	20	6	38	52	17.9	17	22	56	.48	.090	37	58	.88	176	.09	33	1.89	.06	.15	12	-

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: SOIL AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

DATE RECEIVED: JUN 12 1991 DATE REPORT MAILED: June 17/91 SIGNED BY. D. Toye D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

ACME ANALYTICAL

BP Resources Canada Ltd. PROJECT LOC-10161 FILE # 91-1730

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
130037	1	57	5	45	2.6	38	10	253	3.21	8	5	ND	3	40	.4	3	2	67	.35	.095	10	54	.65	94	.11	2	2.05	.01	.05	1	7
130038	1	97	9	54	.1	29	12	378	3.44	6	5	ND	2	70	.4	3	4	73	.70	.044	10	46	.66	165	.10	2	2.66	.02	.05	2	1
130039	1	76	4	145	.1	30	11	303	3.85	7	5	ND	3	58	.2	2	2	72	.53	.093	11	43	.71	96	.10	2	2.57	.01	.06	1	1
130040	1	108	13	94	.2	23	16	456	4.67	5	5	ND	2	216	.3	2	2	94	.70	.044	10	35	.64	335	.10	2	2.70	.02	.08	1	2
130041	1	82	21	62	.3	31	13	437	3.97	7	5	ND	3	58	.2	4	2	85	.62	.040	10	45	.61	127	.11	2	2.74	.01	.07	1	4
130042	1	65	6	124	.5	29	19	754	4.31	7	5	ND	3	107	.2	2	2	83	.58	.057	10	43	.86	240	.13	2	3.01	.02	.11	1	2
130043	1	40	6	136	.3	16	17	483	4.56	5	5	ND	2	82	.3	2	2	103	.70	.093	8	41	.57	172	.10	2	2.01	.01	.09	1	3
130044	1	23	7	55	.1	20	9	197	3.41	3	7	ND	1	43	.2	2	2	72	.45	.119	7	35	.42	69	.10	2	1.78	.01	.05	1	3
130045	1	44	2	64	.1	24	11	337	3.27	2	5	ND	2	53	.2	2	2	68	.53	.110	7	34	.57	127	.11	2	1.99	.01	.06	1	1
130046	1	48	6	54	.2	23	11	302	3.76	6	5	ND	1	51	.2	2	2	87	.55	.057	6	34	.63	103	.11	2	1.98	.02	.08	1	1
130047	1	16	4	95	.4	13	9	234	2.68	6	5	ND	3	38	.5	5	2	65	.39	.153	7	31	.29	76	.09	2	1.54	.01	.04	1	3
130049	9	252	7	40	.2	5	10	573	3.85	28	7	ND	1	15	.2	3	2	33	.19	.082	2	9	.09	152	.01	2	.69	.01	.14	1	5
130050	1	50	14	103	.8	14	16	354	6.40	13	5	ND	3	61	.2	3	2	115	.38	.531	6	37	.63	162	.07	2	3.37	.01	.07	1	8
130051	1	33	5	34	.2	27	10	233	3.06	8	5	ND	2	43	.2	3	2	73	.41	.084	8	42	.48	124	.09	2	1.69	.02	.05	1	2
130052	1	24	2	36	.1	26	9	210	3.52	4	5	ND	1	43	.2	2	2	81	.48	.112	9	43	.44	89	.08	2	1.37	.01	.05	1	1
130053	1	25	6	57	.1	18	11	229	3.58	7	6	ND	1	39	.4	3	2	83	.40	.062	9	44	.41	80	.10	2	2.04	.02	.05	2	2
130054	1	28	4	33	.1	16	9	226	2.17	4	5	ND	2	53	.2	3	2	53	.60	.081	9	27	.53	91	.12	2	1.41	.02	.05	1	7
130055	1	27	5	46	.1	21	8	216	2.25	2	13	ND	2	43	.2	2	2	53	.58	.103	12	35	.68	90	.14	2	1.55	.02	.06	1	1
130056	1	23	3	29	.1	19	7	230	2.11	2	5	ND	1	53	.2	2	2	55	.59	.050	9	29	.46	74	.13	2	1.04	.03	.05	1	9
130057	1	22	6	42	.1	13	7	206	1.87	3	5	ND	1	48	.2	2	2	49	.52	.039	8	24	.55	75	.13	3	1.52	.02	.05	1	5
130058	1	47	5	70	.3	28	12	319	2.88	5	5	ND	2	49	.2	3	2	63	.51	.057	9	38	.63	134	.10	2	2.05	.02	.07	1	6
130059	1	37	5	38	.1	19	8	274	2.27	2	5	ND	2	56	.2	2	2	58	.64	.082	11	31	.58	92	.11	2	1.39	.03	.05	1	10
130060	1	36	2	53	.1	20	9	265	2.70	2	7	ND	1	50	.3	2	2	66	.55	.067	8	31	.55	90	.11	3	1.46	.02	.06	1	21
130061	1	44	4	65	.2	20	10	380	2.89	5	5	ND	1	50	.4	3	2	69	.50	.064	8	36	.56	101	.10	2	1.70	.02	.06	1	5
130062	1	28	6	40	.1	19	6	210	2.01	3	5	ND	1	42	.3	2	2	52	.43	.033	8	30	.54	62	.12	3	1.26	.02	.04	1	7
130063	1	38	6	39	.1	23	9	308	2.70	4	5	ND	2	51	.3	2	2	65	.57	.060	12	42	.57	75	.12	2	1.07	.03	.06	1	9
130064	1	83	12	89	.3	38	16	873	3.91	3	9	ND	2	71	.4	2	2	84	.75	.056	11	51	.85	185	.11	2	2.23	.03	.12	1	3
130065	1	28	2	47	.1	22	11	354	3.04	2	5	ND	2	51	.2	3	2	75	.59	.072	10	41	.60	75	.12	3	1.20	.02	.06	1	2
130066	1	39	10	68	.1	27	11	363	2.79	2	14	ND	2	57	.2	2	2	62	.67	.047	9	44	.88	119	.13	3	1.63	.02	.08	1	1
130067	1	28	7	48	.1	17	10	299	2.59	3	5	ND	2	56	.2	2	2	64	.62	.024	8	33	.63	98	.14	2	1.38	.03	.06	1	1
130068	1	17	4	30	.1	14	8	277	2.47	2	5	ND	1	59	.2	2	2	66	.69	.079	10	31	.47	83	.12	3	1.02	.03	.05	1	6
130069	1	17	3	33	.2	17	7	246	2.20	2	5	ND	2	61	.2	3	2	55	.79	.092	10	32	.53	109	.12	2	1.21	.03	.06	2	4
130070	1	29	4	34	.1	15	8	269	2.56	2	5	ND	3	60	.2	2	2	66	.77	.070	10	31	.51	137	.13	2	1.27	.03	.07	1	2
130071	1	18	2	37	.1	18	8	261	2.73	2	5	ND	1	64	.2	2	2	67	.81	.042	9	35	.53	210	.12	3	1.42	.04	.07	1	71
130072	1	40	5	36	.2	21	10	300	3.07	3	5	ND	2	70	.2	2	3	75	.88	.041	11	37	.57	236	.13	2	1.52	.05	.08	1	6
130073	1	119	4	50	.4	19	10	378	3.02	4	5	ND	3	58	.4	2	2	75	.72	.041	10	39	.49	171	.11	2	1.63	.03	.07	1	7
RE 130056	1	21	2	26	.4	17	6	216	1.97	4	5	ND	4	51	.4	2	2	52	.54	.047	10	27	.42	75	.12	3	.97	.03	.04	1	5
STANDARD C/AU-S	20	62	41	136	7.3	75	32	1112	4.05	38	15	8	40	54	18.8	18	22	60	.51	.098	40	60	.95	183	.09	31	2.00	.07	.15	11	46
STANDARD C	19	60	36	133	7.3	72	31	1059	3.98	37	22	7	40	53	18.7	15	18	56	.48	.090	40	60	.88	178	.09	34	1.89	.06	.15	13	-

ACME ANALYTICAL

BP Resources Canada Ltd. PROJECT LOC-10161 FILE # 91-1730

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
130074	1	25	6	46	.4	28	11	226	3.38	8	5	ND	2	37	.5	3	2	70	.32	.070	8	45	.51	132	.09	2	1.98	.01	.05	2	3
130075	1	15	2	48	.4	15	9	205	2.88	2	5	ND	2	37	.2	2	2	63	.32	.062	7	33	.38	79	.09	2	1.56	.01	.05	1	3
130076	1	44	2	46	.3	13	9	236	3.16	7	5	ND	1	33	.5	3	2	69	.30	.077	7	31	.33	129	.09	3	1.69	.01	.04	2	11
130077	1	39	9	99	.2	16	14	618	4.63	9	5	ND	2	36	.5	2	2	104	.33	.300	7	38	.48	126	.10	2	1.96	.01	.05	1	2
130078	1	75	7	54	.2	22	15	321	4.14	7	5	ND	1	58	.3	2	2	108	.57	.050	6	40	.85	124	.17	2	2.39	.03	.05	1	5
130079	1	15	3	50	.1	12	9	210	3.72	2	5	ND	1	36	.2	2	2	88	.44	.107	6	37	.32	75	.08	2	1.48	.01	.05	1	3
130080	1	23	2	23	.1	22	8	159	3.13	6	5	ND	1	34	.2	2	2	82	.35	.051	6	35	.30	73	.09	3	1.41	.01	.03	1	1
130081	1	21	5	27	.2	18	9	197	3.35	2	5	ND	1	39	.2	2	2	85	.44	.051	5	39	.41	73	.10	2	1.31	.02	.04	1	3
130082	1	42	5	48	.2	23	12	529	3.27	5	5	ND	1	50	.2	2	4	74	.37	.042	7	39	.47	105	.11	2	1.82	.01	.08	1	2
130083	1	17	2	52	.3	19	11	253	3.38	6	5	ND	2	50	.3	2	2	82	.40	.042	6	42	.49	77	.12	2	1.45	.01	.06	1	4
130085	1	61	8	70	.2	25	17	852	4.44	8	5	ND	1	222	.7	2	2	91	.60	.169	6	48	.61	260	.11	2	1.99	.01	.11	1	2
130086	1	24	2	78	.3	16	11	467	3.04	2	5	ND	2	52	.2	2	2	68	.39	.075	10	38	.39	94	.12	2	1.48	.01	.06	1	5
130087	1	39	2	53	.1	32	12	332	3.32	7	5	ND	2	58	.5	2	4	68	.47	.161	9	43	.63	140	.10	2	1.93	.02	.06	1	3
130088	1	39	3	62	.1	20	11	267	3.28	3	5	ND	1	49	.2	2	2	76	.36	.042	8	35	.59	91	.12	2	1.62	.01	.06	1	4
130089	1	26	7	81	.1	20	13	338	4.34	6	5	ND	1	52	.2	2	2	92	.54	.139	8	42	.56	97	.10	2	1.81	.02	.06	1	3
130090	1	91	2	32	.2	23	8	210	2.42	6	5	ND	3	64	.2	2	2	55	.55	.092	12	36	.46	77	.10	2	1.33	.02	.04	1	3
130091	1	64	2	251	.1	19	14	397	3.55	10	5	ND	1	71	.8	2	2	82	.46	.150	7	38	.53	102	.10	2	1.57	.02	.08	1	5
130092	1	109	3	149	.1	29	17	304	4.52	8	5	ND	1	110	.8	2	2	98	.52	.259	6	44	.76	212	.11	2	2.55	.02	.08	1	3
130093	1	32	2	73	.2	21	14	203	3.44	3	5	ND	2	47	.2	2	2	74	.49	.087	7	31	.65	92	.14	2	2.10	.02	.05	1	2
130094	1	30	4	77	.1	22	10	230	3.28	3	5	ND	2	44	.2	2	2	69	.39	.231	7	38	.44	81	.10	2	1.60	.01	.06	1	9
130095	1	40	2	65	.2	20	12	293	3.74	6	5	ND	1	60	.2	2	2	84	.52	.124	7	33	.62	162	.13	2	2.02	.02	.09	1	1
130096	1	43	4	65	.3	14	14	420	3.53	2	5	ND	2	62	.4	2	2	82	.62	.093	7	35	.57	84	.15	2	2.07	.02	.12	1	1
130097	1	33	5	71	.1	20	13	302	4.03	3	5	ND	1	51	.2	2	2	85	.46	.216	7	38	.54	91	.12	2	1.66	.02	.08	1	3
130098	1	27	2	182	.2	15	14	356	4.12	9	5	ND	1	66	.3	2	2	93	.68	.145	7	35	.66	93	.16	2	2.06	.02	.13	1	2
130099	1	29	2	91	.2	19	11	206	4.44	7	5	ND	2	49	.2	2	2	97	.41	.069	7	37	.50	95	.15	6	2.53	.01	.07	1	1
130100	1	163	3	78	.5	25	16	579	4.61	4	5	ND	1	161	.4	3	3	120	.68	.077	6	42	.88	359	.13	2	3.18	.01	.12	1	2
130101	2	1281	15	285	1.3	56	22	813	5.69	54	5	ND	5	94	.2	4	13	118	1.22	.056	19	59	.89	239	.14	2	4.92	.03	.18	1	8
J102	1	49	4	78	.1	18	14	305	4.23	36	5	ND	1	52	.2	2	2	103	.61	.080	5	36	.57	106	.16	2	2.11	.02	.12	1	2
J103	1	41	2	96	.1	17	15	499	3.76	13	5	ND	1	45	.2	2	2	96	.44	.051	5	36	.44	99	.15	2	1.80	.02	.11	1	10
130104	1	38	3	85	.2	13	11	265	3.53	5	5	ND	2	40	.2	2	2	85	.43	.084	6	35	.36	75	.12	4	1.89	.02	.06	1	3
130105	1	30	3	81	.1	13	12	271	3.53	9	5	ND	1	50	.2	3	2	87	.52	.111	6	34	.42	83	.13	5	1.70	.01	.07	1	9
130106	1	28	4	83	.1	13	11	373	3.42	5	5	ND	2	46	.2	2	2	82	.44	.100	6	30	.38	83	.12	2	1.54	.01	.08	1	3
130107	1	28	3	156	.3	11	12	617	3.80	6	5	ND	1	42	.5	2	2	88	.46	.183	6	32	.41	147	.12	4	1.51	.01	.09	1	6
130108	1	43	3	70	.2	14	11	270	4.11	9	5	ND	1	54	.2	2	2	103	.56	.093	6	36	.51	86	.12	2	1.52	.02	.08	1	1
130109	2	52	2	104	.2	19	17	755	3.91	9	5	ND	1	50	.5	5	2	92	.52	.184	7	37	.56	113	.11	4	1.71	.02	.09	2	4
130110	1	55	2	62	.5	22	12	252	4.06	14	5	ND	3	51	.2	5	2	94	.54	.149	8	37	.61	111	.12	2	1.89	.02	.08	1	7
RE 13080	1	26	2	25	.1	22	9	166	3.34	4	7	ND	2	33	.2	2	4	86	.36	.056	5	36	.33	61	.10	2	1.39	.01	.04	1	4
STANDARD C/AU-S	19	53	38	129	6.9	69	33	1076	3.83	40	15	7	38	52	18.5	16	17	54	.45	.083	37	55	.84	156	.09	32	1.81	.06	.14	11	47
STANDARD C	18	60	39	132	7.4	70	32	1049	3.97	39	17	7	39	52	19.0	15	18	56	.48	.090	39	58	.87	179	.09	36	1.88	.06	.15	12	-

ACME ANALYTICAL

BP Resources Canada Ltd. PROJECT LOC-10161 FILE # 91-1730

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
130111	2	49	3	57	.1	23	13	231	4.05	14	5	ND	2	46	.3	2	2	87	.37	.074	6	38	.55	104	.14	3	3.09	.02	.05	2	1
130112	5	256	2	83	.1	24	13	296	3.88	10	5	ND	3	65	.6	2	4	81	.65	.035	10	37	.68	94	.17	3	3.01	.02	.07	1	1
130113	3	65	10	71	.1	15	12	333	4.48	7	5	ND	3	43	.7	2	2	109	.39	.054	8	32	.54	82	.20	2	2.43	.02	.07	1	1
130114	4	76	6	87	.1	19	12	378	5.05	15	5	ND	2	45	.7	2	2	111	.40	.083	8	34	.64	93	.17	3	2.97	.01	.12	2	5
130115	2	57	5	120	.1	17	10	313	4.09	13	5	ND	1	54	1.5	2	2	82	.50	.075	8	35	.53	87	.14	2	2.40	.02	.06	1	3
130116	1	50	3	51	.1	20	9	224	4.12	5	5	ND	3	42	.4	2	2	80	.37	.132	8	39	.47	80	.12	2	3.73	.02	.06	1	1
130117	2	61	4	26	.2	13	9	185	2.03	9	5	ND	1	59	.3	2	2	53	.53	.055	8	25	.40	54	.10	2	1.39	.02	.04	1	14
130118	3	71	7	41	.1	15	9	329	3.36	11	5	ND	2	62	.4	2	2	86	.66	.098	11	35	.52	59	.12	2	1.55	.02	.06	1	14
130119	2	24	2	29	.1	10	5	193	2.78	4	5	ND	2	44	.4	2	2	71	.40	.049	8	31	.31	62	.12	2	1.45	.01	.05	1	3
130121	1	18	4	58	.1	18	7	178	2.49	9	5	ND	2	40	.4	2	2	55	.39	.100	8	33	.33	75	.09	2	1.66	.02	.04	1	2
130122	1	32	6	64	.3	22	13	396	3.62	4	5	ND	2	50	.5	2	3	82	.45	.170	9	43	.52	123	.11	2	1.96	.02	.08	1	6
130123	1	27	2	37	.2	18	8	209	4.44	8	5	ND	3	51	.5	4	2	100	.47	.080	10	46	.44	94	.14	2	2.10	.01	.06	1	3
130566	1	15	2	46	.1	16	9	227	3.96	8	5	ND	2	52	.5	2	2	81	.48	.160	7	40	.43	85	.11	3	1.83	.01	.05	1	1
130567	1	38	3	50	.2	21	14	516	3.38	5	5	ND	1	54	.8	3	4	73	.56	.059	8	39	.58	123	.12	2	1.94	.03	.07	1	1
130568	1	40	3	43	.1	24	9	268	2.62	7	5	ND	2	55	.3	2	2	57	.51	.065	10	35	.48	98	.11	2	1.49	.02	.05	1	4
130569	1	24	3	58	.2	26	10	397	2.60	4	5	ND	2	63	.2	2	3	57	.62	.079	10	38	.78	96	.14	2	1.57	.02	.07	1	3
130570	1	33	6	61	.2	21	10	429	2.42	4	5	ND	2	70	.2	2	2	52	.62	.070	12	37	.70	123	.13	2	1.55	.02	.07	1	19
130572	2	82	6	81	.1	24	25	854	6.00	13	5	ND	2	116	1.4	2	2	121	1.28	.107	6	42	.99	145	.18	2	2.96	.03	.14	1	3
130573	1	36	2	35	.2	28	12	354	3.45	6	6	ND	3	62	.3	2	2	83	.57	.117	9	38	.52	81	.11	2	1.35	.01	.08	1	65
130574	1	20	3	163	.1	18	11	286	3.08	5	5	ND	2	55	.4	2	2	59	.44	.155	8	33	.43	112	.11	2	1.80	.01	.07	1	4
130575	1	20	7	66	.1	21	8	228	2.66	6	5	ND	2	50	.2	3	2	58	.42	.062	9	36	.44	85	.13	2	1.59	.01	.05	1	1
130576	1	41	11	138	.1	38	12	247	3.88	9	5	ND	3	49	.2	2	2	77	.38	.051	10	49	.54	104	.14	2	2.21	.01	.05	1	8
130577	1	29	6	50	.1	29	11	250	3.36	7	5	ND	3	52	.6	2	2	70	.43	.056	11	47	.52	101	.14	2	2.06	.02	.06	1	1
130578	1	34	4	59	.1	31	11	267	3.66	10	5	ND	2	49	.5	2	3	67	.43	.106	11	50	.55	80	.12	2	2.16	.01	.05	1	3
130579	1	45	3	36	.1	28	12	444	3.20	7	5	ND	3	88	.6	2	2	71	.80	.108	13	45	.63	92	.13	2	1.40	.02	.08	1	13
130580	2	67	9	41	.1	26	12	406	3.52	9	5	ND	3	75	.6	2	4	74	.64	.066	12	47	.62	87	.14	2	1.71	.02	.10	2	1
130581	1	33	7	59	.1	24	12	292	3.89	4	5	ND	2	61	.6	3	3	78	.48	.106	9	43	.62	104	.15	2	2.17	.02	.08	1	1
130582	1	33	5	144	.1	16	18	1018	3.42	4	5	ND	2	57	.8	2	3	71	.53	.116	6	33	.45	138	.15	2	1.73	.02	.09	1	3
130583	1	31	3	68	.1	18	10	262	2.90	3	5	ND	3	59	.4	2	2	64	.53	.091	8	33	.53	87	.15	2	1.72	.01	.09	1	2
130584	1	50	4	99	.2	21	15	350	4.30	9	5	ND	2	63	.7	2	2	94	.55	.080	5	44	.67	78	.17	2	2.18	.02	.09	1	1
130585	1	63	7	103	.2	29	17	370	4.50	13	5	ND	3	64	.2	4	2	96	.60	.106	7	44	.72	108	.17	3	2.61	.03	.15	1	24
130586	1	34	6	175	.1	20	18	335	4.80	7	5	ND	2	66	.8	3	2	92	.57	.269	8	41	.58	109	.14	3	2.43	.02	.09	1	4
130587	1	82	7	88	.1	22	17	397	4.41	18	5	ND	3	83	.7	4	2	94	.68	.122	8	38	.82	137	.17	3	2.62	.03	.11	1	1
130588	1	60	7	67	.2	23	14	320	4.19	16	5	ND	3	64	.4	2	2	92	.62	.220	8	34	.75	70	.15	2	2.28	.02	.14	1	4
130589	1	61	2	97	.1	23	14	325	4.42	9	5	ND	2	67	.6	2	2	95	.58	.157	6	34	.69	98	.17	2	2.47	.02	.10	1	1
130590	1	89	5	91	.1	24	15	331	4.70	9	5	ND	4	59	.4	3	2	95	.55	.221	9	37	.71	113	.15	2	3.90	.02	.09	1	110
RE 130570	1	35	5	61	.1	24	10	435	2.49	4	5	ND	3	73	.7	3	2	53	.62	.074	12	37	.72	125	.13	2	1.59	.02	.07	1	23
STANDARD C/AU-S	21	63	39	141	7.5	76	33	1085	4.01	42	19	8	41	51	17.8	18	22	60	.53	.099	40	60	1.00	183	.10	35	2.00	.07	.16	11	45
STANDARD C	19	62	40	132	7.5	71	32	1066	3.97	37	15	7	40	52	18.8	16	18	55	.48	.090	39	58	.88	177	.09	32	1.94	.06	.16	12	-

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
130591	1	66	2	57	.2	20	17	435	4.37	13	5	ND	3	61	.3	2	2	99	.69	.125	8	37	.66	161	.14	2	2.12	.02	.08	1	5
130592	1	28	5	80	.2	13	8	224	3.47	3	5	ND	2	39	.2	2	7	83	.37	.218	7	34	.33	76	.11	2	2.00	.02	.05	1	3
130593	1	50	3	113	.1	17	10	281	3.43	9	5	ND	2	54	.2	2	2	84	.53	.080	7	32	.43	84	.12	3	1.48	.02	.07	1	1
130594	1	25	2	110	.2	12	8	223	3.67	5	5	ND	1	45	.3	2	2	91	.42	.075	7	32	.39	81	.12	2	1.40	.02	.06	1	1
130595	1	44	10	80	.2	16	12	337	3.56	8	5	ND	2	53	.2	2	2	81	.57	.255	8	34	.53	110	.10	2	1.82	.02	.06	1	7
130596	1	50	2	60	.2	19	11	322	3.92	8	5	ND	1	63	.4	5	2	82	.57	.065	11	41	.56	74	.14	3	1.68	.03	.06	1	6
130597	3	67	6	79	.1	19	9	228	2.89	6	5	ND	2	54	.4	2	2	66	.53	.074	9	32	.54	88	.11	3	1.82	.02	.07	1	2
130598	5	500	6	106	.2	23	11	203	4.76	18	5	ND	3	58	.2	2	2	106	.57	.041	17	43	.51	73	.13	4	2.65	.02	.05	1	2
130599	2	38	2	190	.1	10	10	180	5.98	10	5	ND	1	35	.7	2	2	134	.37	.110	3	79	.78	164	.40	2	1.80	.02	.09	1	3
130600	2	44	9	207	.1	15	11	268	4.37	8	5	ND	2	48	.3	2	2	89	.43	.172	7	35	.49	85	.14	5	2.15	.02	.06	1	5
130601-1	2	94	2	167	.1	19	13	318	4.94	16	5	ND	2	58	.2	2	2	115	.64	.172	9	42	.70	92	.12	2	2.00	.02	.06	1	3
130601-2	2	80	2	175	.1	19	15	320	5.11	15	5	ND	2	58	.2	2	2	123	.64	.186	9	44	.71	90	.13	2	1.91	.02	.06	1	1
130602	1	121	4	60	.2	18	12	326	3.73	23	5	ND	3	60	.2	3	4	98	.65	.069	9	36	.62	81	.14	3	1.70	.03	.08	1	2
130603	2	686	3	126	.4	30	26	993	5.10	68	5	ND	1	86	1.0	2	3	117	.45	.079	10	51	.81	230	.13	4	2.65	.02	.12	1	1
130604	1	65	8	69	.1	21	9	358	2.88	2	7	ND	3	47	.2	2	6	60	.52	.099	11	33	.57	71	.12	2	1.60	.02	.07	1	1
130605	1	31	2	36	.1	17	8	253	2.66	7	5	ND	1	53	.2	2	4	72	.73	.108	8	31	.46	59	.10	3	.95	.02	.03	1	1
130606	1	27	5	82	.1	20	11	269	3.68	11	5	ND	3	39	.2	2	2	86	.35	.084	7	41	.50	78	.13	4	2.00	.02	.05	1	1
130607	1	94	8	111	.1	51	17	577	4.21	9	5	ND	2	59	.2	2	2	84	.73	.091	13	55	.96	153	.10	2	2.41	.02	.10	1	2
130608	1	44	7	112	.1	37	13	432	3.68	7	5	ND	2	78	.2	2	2	73	.70	.056	10	50	.90	156	.14	4	2.10	.02	.07	1	2
130609	3	31	4	153	.2	22	16	388	4.32	18	5	ND	1	57	.2	4	2	102	.85	.054	7	45	.69	92	.11	2	1.85	.02	.06	1	1
130610	2	53	2	70	.1	17	11	284	3.84	12	5	ND	1	48	.2	2	2	91	.50	.065	10	37	.53	96	.12	2	2.15	.04	.06	1	1
130611	1	28	10	74	.1	19	11	291	4.00	9	5	ND	2	45	.3	2	2	96	.49	.130	7	41	.51	68	.13	2	1.83	.02	.05	1	1
130612	1	56	17	120	.3	25	14	380	4.14	13	5	ND	3	58	.2	2	3	97	.59	.121	9	42	.66	89	.14	2	2.09	.02	.06	1	2
130613	1	44	40	202	.1	17	11	366	3.39	8	5	ND	2	55	.6	2	2	81	.61	.108	10	36	.61	79	.12	3	1.88	.02	.05	1	3
130614	1	29	10	246	.6	18	11	277	3.42	5	6	ND	3	46	.2	2	2	82	.44	.058	9	34	.56	101	.12	3	1.95	.02	.06	1	3
130615	1	35	9	111	.3	20	11	298	3.39	7	5	ND	2	51	.2	2	2	83	.48	.058	10	39	.52	87	.12	3	1.85	.02	.06	1	1
130616	1	17	5	127	.2	15	11	425	3.07	4	5	ND	1	56	.3	2	2	79	.51	.084	7	39	.38	94	.11	6	1.34	.02	.06	1	1
130617	1	22	8	84	.1	13	13	633	2.99	3	5	ND	2	47	.4	2	2	77	.46	.050	9	36	.31	85	.10	4	1.44	.02	.05	1	2
618	1	60	10	65	.1	24	11	296	3.76	11	5	ND	2	46	.2	2	2	89	.46	.069	7	40	.58	62	.12	4	2.36	.02	.07	1	1
130619	1	34	5	116	.1	23	13	261	3.68	8	5	ND	2	48	.4	2	2	88	.47	.053	7	42	.54	96	.13	6	1.99	.02	.05	1	2
130620	1	158	23	198	.4	70	24	1030	5.81	15	5	ND	6	60	.3	2	2	112	.95	.053	25	76	1.18	298	.14	2	3.69	.04	.19	1	3
130621	1	44	38	209	.2	31	13	356	3.86	4	5	ND	3	45	.5	2	2	83	.52	.118	10	47	.69	86	.11	2	2.41	.02	.07	1	1
130622	1	83	2	109	.3	36	16	389	3.86	7	5	ND	3	45	.2	4	2	85	.56	.084	10	48	.64	96	.11	9	3.17	.02	.08	1	2
130623	1	70	6	51	.1	28	12	393	3.74	8	5	ND	3	52	.2	2	2	91	.87	.064	11	48	.77	171	.14	4	2.19	.03	.09	1	1
130624	1	50	5	83	.2	28	20	628	5.61	12	5	ND	2	47	.2	4	2	152	.79	.156	9	60	.95	126	.13	6	2.16	.03	.11	1	1
130625	1	63	5	79	.1	32	13	395	4.89	8	5	ND	3	51	.2	2	2	131	.71	.045	9	66	.79	130	.13	3	2.02	.03	.10	1	1
RE 130610	1	50	3	66	.1	17	10	272	3.64	10	5	ND	1	47	.4	2	3	88	.48	.062	9	36	.50	87	.13	5	2.03	.04	.07	1	1
STANDARD C/AU-S	20	60	35	136	6.9	70	32	1077	4.03	40	18	8	39	53	18.7	16	17	59	.51	.093	40	59	.93	182	.09	33	2.01	.07	.15	11	46
STANDARD C	18	59	36	133	6.9	72	33	1047	3.99	38	16	6	39	52	18.6	18	18	55	.48	.093	39	58	.89	177	.09	31	1.88	.07	.15	13	-

ACME ANALYTICAL

BP Resources Canada Ltd. PROJECT LOC-10161 FILE # 91-1730

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
130627	2	63	2	100	.1	15	13	306	3.84	5	5	ND	3	87	.2	2	3	105	.48	.063	8	48	.57	179	.12	5	2.55	.02	.06	2	4
130628	2	114	3	80	.1	33	14	314	3.77	12	5	ND	4	57	.4	2	2	88	.46	.085	8	52	.69	148	.11	2	2.69	.02	.07	2	3
130629	2	66	6	93	.1	30	15	417	6.74	6	5	ND	2	64	.2	2	2	206	.65	.181	11	86	.72	121	.11	2	1.66	.02	.07	1	4
130630	1	43	5	42	.2	24	8	314	2.55	5	5	ND	3	56	.4	2	2	57	.55	.088	12	44	.56	110	.11	4	1.00	.02	.04	1	4
130631	1	42	5	42	.1	36	9	364	2.67	4	5	ND	2	57	.2	2	2	55	.60	.095	12	53	.66	104	.10	2	1.00	.02	.04	1	4
130632	1	33	5	88	.1	22	11	240	3.35	4	5	ND	1	44	.2	2	2	75	.48	.122	8	40	.53	120	.10	2	1.70	.02	.04	1	9
130633	1	21	2	63	.1	20	7	262	2.29	3	5	ND	2	48	.3	2	2	54	.56	.076	11	39	.62	93	.11	5	1.10	.02	.05	1	10
130634	1	42	2	45	.1	23	9	343	2.54	6	5	ND	2	57	.2	2	2	58	.59	.104	11	41	.60	92	.10	4	1.01	.02	.04	1	2
130635	2	39	3	118	.2	25	22	1746	3.83	3	5	ND	3	54	.6	2	2	91	.71	.095	8	44	.80	166	.12	6	1.69	.03	.09	1	1
130636	1	37	3	130	.1	15	14	739	3.55	8	7	ND	5	49	.3	2	2	72	.69	.231	8	25	.79	149	.09	5	1.49	.03	.09	1	1
130637	1	52	2	50	.2	22	11	310	4.86	7	5	ND	4	63	.2	2	2	152	.72	.067	13	73	.63	104	.13	2	1.55	.02	.04	2	38
130638	1	41	2	44	.1	14	9	454	2.97	6	5	ND	2	83	.5	2	2	79	.83	.125	12	32	.63	93	.14	2	1.13	.02	.04	2	3
130639	1	32	7	50	.1	12	9	379	2.72	5	5	ND	1	65	.2	2	2	74	.54	.031	7	32	.56	74	.12	4	1.24	.02	.05	2	2
130640	1	51	2	48	.2	16	9	334	2.68	6	5	ND	2	65	.4	2	2	70	.62	.042	9	36	.50	75	.14	2	1.14	.02	.04	2	4
130641	1	31	2	56	.1	15	10	242	2.69	4	5	ND	2	52	.3	2	2	66	.45	.057	8	31	.43	83	.12	3	1.81	.01	.03	1	1
130642	1	37	7	55	.2	17	11	338	2.97	7	5	ND	1	59	.4	2	2	74	.56	.049	10	35	.53	93	.11	2	1.75	.02	.04	1	4
130643	2	31	6	61	.1	14	11	531	3.43	14	6	ND	2	56	.6	2	2	80	.65	.060	9	38	.83	86	.12	2	1.56	.02	.05	1	9
130644	1	45	2	73	.2	37	13	385	3.38	11	5	ND	2	63	.2	2	2	74	.58	.106	11	49	.91	132	.15	2	1.98	.02	.06	1	2
130645	1	53	2	63	.1	24	12	390	3.66	13	5	ND	2	64	.2	2	2	84	.61	.106	10	40	.66	99	.13	8	1.89	.02	.05	1	2
130646	1	49	4	72	.6	25	15	339	3.64	16	5	ND	3	62	.2	5	2	79	.42	.082	9	40	.68	117	.13	5	2.39	.02	.05	2	4
130647	1	76	9	85	.1	35	17	462	4.35	25	5	ND	2	63	.5	2	2	85	.54	.100	9	47	.89	134	.12	4	2.42	.02	.07	1	7
RE 130630	1	45	3	40	.2	26	10	327	2.60	4	5	ND	3	57	.2	2	2	58	.57	.092	12	45	.59	98	.11	2	1.03	.02	.04	2	4
130649	1	47	6	64	.2	37	17	460	3.95	14	5	ND	3	59	.3	3	2	90	.51	.094	9	45	.81	141	.13	2	2.05	.02	.06	1	5
130650	1	31	2	54	.2	25	9	251	2.15	2	5	ND	3	37	.2	2	2	45	.48	.068	12	34	.62	78	.13	2	1.28	.02	.03	1	1
130651	1	47	3	36	.1	18	11	389	3.02	7	5	ND	2	51	.2	2	2	82	.57	.111	11	37	.52	98	.12	2	1.21	.02	.04	1	5
130652	1	30	2	55	.2	18	12	260	3.34	7	5	ND	2	41	.5	3	2	80	.38	.095	9	41	.48	96	.12	2	1.95	.02	.05	2	29
130653	1	45	2	35	.1	17	9	331	2.82	10	5	ND	2	66	.2	2	2	76	.78	.126	11	36	.47	70	.12	2	.95	.03	.04	1	2
130654	1	63	3	45	.1	24	13	359	3.16	4	7	ND	2	58	.2	2	2	80	.61	.113	10	40	.59	126	.12	3	1.69	.02	.04	1	2
130655	1	28	13	153	.3	20	13	373	3.62	7	5	ND	2	48	.5	3	2	85	.51	.109	8	40	.60	116	.12	4	1.84	.02	.06	2	5
130656	1	41	2	57	.2	18	9	323	2.40	2	5	ND	2	51	.3	3	2	58	.57	.033	9	33	.54	88	.13	7	1.57	.02	.04	1	14
130657	1	41	5	75	.2	17	11	530	3.06	2	5	ND	1	47	.2	2	2	74	.60	.093	7	33	.54	116	.10	3	1.65	.01	.07	1	2
130658	1	51	8	60	.2	20	13	348	3.25	7	6	ND	1	53	.3	2	2	82	.68	.068	8	36	.60	119	.13	3	1.88	.02	.06	1	3
130659	1	62	4	46	.1	19	11	420	3.17	7	5	ND	4	71	.5	2	2	87	.84	.117	11	38	.53	88	.13	2	1.16	.03	.06	1	15
130660	1	44	2	54	.4	25	13	344	3.23	7	5	ND	2	65	.2	2	2	77	.68	.080	10	42	.69	97	.14	5	1.70	.02	.07	1	6
130661	1	57	4	48	.3	31	12	387	2.96	5	5	ND	3	57	.2	2	2	66	.65	.096	16	48	.78	87	.14	4	1.40	.02	.06	1	57
130662	1	75	2	60	.2	25	12	273	3.79	5	5	ND	2	60	.4	2	2	87	.58	.095	9	39	.70	136	.13	5	2.20	.02	.09	1	3
130663	1	50	9	79	.4	14	12	409	3.31	8	5	ND	2	60	.4	2	2	86	.59	.109	9	35	.55	142	.13	2	1.75	.02	.07	1	6
STANDARD C/AU-S	19	60	36	129	7.3	65	33	1004	3.92	38	25	8	40	52	17.3	16	20	55	.48	.087	38	58	.84	175	.09	33	1.86	.06	.14	11	48
STANDARD C	19	58	35	132	7.4	70	33	1050	3.97	37	22	7	39	53	18.4	14	20	56	.48	.092	39	58	.88	173	.09	34	1.88	.06	.15	11	-

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
130664	1	20	8	85	.1	12	8	202	3.26	4	5	ND	1	35	.2	2	2	101	.38	.094	6	35	.32	74	.12	2	1.63	.02	.04	1	11
130665	1	94	8	66	.2	19	16	368	5.41	13	5	ND	2	30	.2	2	2	160	.47	.146	6	45	.65	338	.12	5	2.28	.01	.10	1	63
130666	2	146	9	74	.3	18	15	319	7.31	33	5	ND	2	32	.2	3	2	187	.43	.172	7	55	.67	104	.09	2	2.80	.01	.09	1	4
130667	3	145	2	93	.2	19	17	508	6.33	11	5	ND	1	51	.3	2	2	146	.81	.092	10	46	.85	193	.06	2	2.72	.02	.10	1	5
130668	1	53	5	136	.4	17	14	331	5.98	6	5	ND	2	36	.4	2	2	144	.49	.274	6	41	.68	189	.05	2	3.06	.01	.09	1	3
130669	2	71	7	132	.2	18	17	398	6.06	19	5	ND	2	23	.2	2	2	123	.29	.253	6	35	.76	146	.02	3	3.93	.01	.10	1	2
130670	1	94	5	125	.1	19	16	425	5.66	3	5	ND	1	27	.4	2	2	130	.49	.210	6	34	1.06	295	.02	2	3.40	.01	.12	1	5
130671	1	168	6	103	.4	14	17	534	4.82	5	5	ND	1	37	.5	2	2	113	.64	.064	15	23	.93	240	.01	2	3.47	.01	.09	1	1
130672	1	128	4	103	.1	18	17	739	5.33	10	5	ND	2	53	.5	2	2	125	.57	.206	10	30	.90	566	.06	2	2.99	.02	.15	1	5
130673	1	53	12	51	.1	29	13	331	3.18	6	5	ND	1	51	.2	2	2	77	.51	.096	9	38	.64	139	.12	2	2.20	.02	.05	1	1
130674	1	33	6	77	.2	20	10	266	2.79	4	5	ND	1	36	.2	2	2	73	.36	.060	8	37	.51	86	.12	2	1.82	.01	.05	1	1
RE 130689	1	28	2	38	.1	18	8	269	1.86	4	5	ND	1	45	.2	2	2	53	.53	.076	9	32	.49	82	.09	3	1.18	.02	.03	1	3
130676	1	33	4	61	.1	14	8	318	2.33	4	5	ND	1	52	.2	2	2	62	.63	.058	8	33	.43	95	.08	2	1.73	.02	.04	1	3
130677	2	64	42	86	1.0	15	16	370	4.90	21	5	ND	1	31	.5	2	2	104	.24	.053	7	35	.54	86	.08	2	2.54	.01	.05	1	4
130679	1	75	14	65	.1	25	16	379	3.77	25	5	ND	2	48	.4	2	2	87	.37	.084	8	39	.79	114	.13	2	2.38	.02	.05	1	3
130680	1	53	2	95	.1	21	12	343	3.62	13	5	ND	2	52	.5	2	2	80	.38	.145	9	42	.68	85	.12	2	2.45	.01	.04	1	2
130681	1	53	6	57	.1	22	11	463	3.06	7	5	ND	1	71	.2	2	2	85	.76	.113	10	41	.71	94	.11	3	1.47	.03	.04	1	4
130682	1	34	2	53	.2	18	10	365	2.59	7	5	ND	1	59	.2	2	2	75	.70	.087	9	34	.69	67	.13	5	1.30	.02	.04	1	6
130683	1	43	18	51	.2	19	10	339	2.47	4	5	ND	1	57	.2	2	2	67	.55	.085	10	35	.59	89	.11	3	1.59	.02	.03	1	6
130684	1	37	6	55	.2	23	10	368	2.63	4	5	ND	2	60	.2	2	2	69	.69	.078	11	42	.74	85	.12	4	1.43	.03	.04	1	4
130685	1	25	6	68	.1	17	9	307	2.33	5	5	ND	1	53	.2	2	2	68	.56	.058	9	34	.53	59	.11	2	1.14	.02	.03	1	2
130687	1	23	8	35	.1	15	9	248	2.02	3	5	ND	4	51	.2	2	2	61	.53	.058	9	33	.49	62	.11	4	1.11	.02	.03	1	2
130688	1	28	10	40	.2	18	9	322	2.28	5	5	ND	2	52	.2	2	2	62	.59	.076	9	37	.57	74	.11	4	1.14	.02	.03	1	5
130689	1	29	2	38	.1	19	8	266	1.95	3	5	ND	1	46	.2	2	2	53	.54	.076	9	35	.50	89	.10	2	1.19	.02	.03	1	2
130690	1	37	3	38	.2	16	8	317	2.43	2	5	ND	1	53	.2	2	2	67	.64	.100	10	35	.54	89	.11	2	1.09	.02	.04	1	4
130691	1	42	4	41	.3	22	10	334	2.67	4	5	ND	2	45	.2	2	2	69	.53	.058	10	36	.54	101	.10	3	1.68	.02	.04	1	2
130692	1	60	5	49	.2	19	11	437	3.91	8	5	ND	1	52	.2	2	2	86	.67	.096	10	42	.58	121	.10	3	1.58	.02	.05	1	1
130693	1	64	6	47	.2	16	11	567	3.61	5	5	ND	1	49	.2	2	3	105	.74	.109	13	48	.57	94	.09	2	1.48	.02	.04	1	9
130694	1	51	2	55	.1	19	13	393	3.93	5	5	ND	2	36	.2	2	2	116	.44	.087	8	49	.49	110	.12	2	1.53	.01	.05	1	35
130698	1	35	6	69	.1	22	12	333	2.99	6	5	ND	1	33	.2	2	2	67	.29	.093	9	46	.62	93	.11	2	2.01	.01	.04	1	6
130699	1	71	9	50	.1	18	12	373	3.40	7	5	ND	2	55	.2	2	2	103	.54	.083	12	43	.61	114	.12	3	1.54	.02	.05	1	4
130700	1	29	35	168	.3	13	10	304	3.09	7	5	ND	1	37	.2	2	2	84	.54	.083	7	34	.47	137	.10	3	1.57	.02	.03	1	4
130701	1	20	32	207	.8	9	7	258	2.31	5	5	ND	1	33	.2	3	2	69	.31	.044	7	25	.38	149	.11	4	1.53	.01	.04	1	3
130702	1	30	17	129	.7	26	11	302	3.23	6	5	ND	2	44	.2	2	2	75	.42	.056	10	42	.67	209	.13	4	1.88	.02	.04	1	3
130703	1	43	39	211	.6	25	11	283	3.21	6	5	ND	1	45	.2	2	2	80	.50	.069	9	33	.61	308	.12	3	2.10	.02	.04	1	9
130704	1	74	19	100	.3	18	10	529	2.38	3	5	ND	1	57	.2	2	2	64	.58	.047	14	36	.62	247	.13	3	1.32	.02	.04	1	5
130705	1	53	30	163	.8	19	11	376	3.36	8	5	ND	1	52	.2	2	3	81	.54	.082	12	36	.59	192	.10	5	1.64	.02	.04	1	3
STANDARD C/AU-S	20	63	42	133	7.4	71	32	1104	4.01	38	20	7	38	52	18.0	15	23	59	.48	.092	39	60	.91	178	.09	34	1.96	.06	.15	11	46
STANDARD C	19	63	37	133	7.3	70	32	1069	4.00	38	17	7	37	52	17.0	15	21	57	.48	.090	38	58	.90	177	.09	33	1.90	.07	.15	11	-

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
130706	1	35	67	140	.4	16	8	421	2.54	6	5	ND	2	59	.5	2	4	61	.69	.105	11	34	.63	306	.12	5	1.19	.02	.03	1	5
130707	1	37	11	60	.1	20	8	301	2.49	3	5	ND	2	53	.3	2	5	58	.62	.076	11	35	.56	168	.11	4	1.21	.02	.03	1	6
130708	1	13	12	67	.1	13	6	244	1.84	4	5	ND	1	45	.3	2	4	47	.53	.033	8	26	.56	160	.10	3	1.34	.02	.02	2	6
130710	1	35	13	92	.5	17	10	413	3.77	10	5	ND	2	45	.2	2	2	86	.58	.095	8	42	.64	482	.11	4	1.60	.01	.04	1	4
130711 (standard)	33	100	35	163	.7	86	27	1203	5.67	54	5	ND	3	455	.5	2	2	47	3.18	.112	17	116	2.61	143	.03	2	1.54	.03	.22	1	250
131329	1	67	3	44	.1	22	9	270	2.99	4	5	ND	2	42	.2	3	4	64	.39	.116	8	37	.51	118	.09	3	2.58	.01	.05	1	7
131330	1	48	3	75	.1	24	11	393	3.38	10	5	ND	2	44	.2	2	5	71	.44	.151	9	40	.51	146	.09	5	2.17	.02	.06	2	4
131331	1	69	4	46	.1	24	10	247	3.17	4	5	ND	2	37	.3	2	2	70	.38	.090	8	37	.48	142	.09	3	2.29	.02	.07	1	9
131332	1	60	6	57	.1	19	8	249	3.00	5	5	ND	2	32	.2	4	2	59	.32	.077	9	30	.39	151	.06	4	2.45	.01	.06	1	1
131333	1	94	5	41	.1	28	10	248	3.22	4	5	ND	2	40	.2	2	5	65	.40	.057	9	39	.61	208	.09	4	2.58	.02	.06	1	2
131334	1	44	8	86	.1	21	10	323	3.68	5	5	ND	1	42	.2	2	2	74	.42	.074	8	38	.58	162	.09	2	2.13	.01	.06	1	5
131335	1	65	3	55	.3	32	12	277	4.21	7	5	ND	3	42	.2	2	5	85	.41	.105	11	47	.61	113	.10	2	2.44	.01	.06	1	2
131336	1	33	3	34	.1	26	10	223	3.64	5	5	ND	2	44	.2	2	5	83	.41	.078	9	38	.51	100	.09	2	1.71	.01	.05	1	1
131337	1	23	2	24	.1	16	7	169	2.94	2	5	ND	1	34	.2	2	3	67	.37	.108	8	33	.35	79	.08	2	1.37	.02	.03	1	5
131339	1	81	5	103	.3	20	14	370	5.31	22	5	ND	5	58	.5	2	3	114	.55	.363	8	39	.74	126	.12	2	3.11	.02	.08	1	6
131340	1	81	5	84	.1	18	14	379	5.32	9	5	ND	2	87	.3	2	2	121	.54	.273	7	42	.76	143	.11	2	2.51	.02	.09	1	4
131341	1	60	3	37	.2	29	10	464	3.20	5	5	ND	1	58	.2	2	2	70	.65	.079	12	44	.59	101	.10	2	1.58	.02	.06	1	3
131342	1	43	6	34	.1	29	11	412	3.19	4	5	ND	2	50	.3	5	4	69	.50	.091	7	42	.56	97	.10	2	1.48	.01	.08	1	1
131343	1	30	5	92	.3	26	15	509	4.11	7	5	ND	2	57	.2	2	2	73	.48	.206	8	40	.61	148	.10	2	2.11	.02	.11	1	2
131344	1	25	2	39	.1	21	8	279	2.33	4	5	ND	1	55	.2	5	2	52	.51	.069	10	33	.56	102	.12	2	1.24	.02	.04	1	3
131345	1	78	2	92	.1	40	19	617	5.04	8	5	ND	1	69	.3	2	2	102	.72	.089	9	51	1.01	163	.13	2	2.93	.03	.14	1	4
131346	1	29	5	61	.1	22	11	329	3.55	8	5	ND	2	52	.5	4	3	72	.47	.135	7	39	.50	99	.10	2	1.79	.01	.06	1	2
131347	1	51	5	169	.1	23	16	827	4.21	5	5	ND	1	55	.7	2	2	79	.52	.124	8	39	.67	108	.12	3	2.26	.02	.09	1	6
131348	1	74	2	75	.1	24	19	916	4.49	9	5	ND	4	84	.6	3	2	88	.92	.193	8	37	1.27	120	.16	3	2.32	.05	.14	1	6
131349	1	60	6	37	.2	19	10	440	2.97	8	5	ND	3	65	.3	2	2	60	.78	.087	13	38	.54	79	.11	2	1.27	.02	.05	1	2
131350	2	50	2	53	.2	28	12	350	3.34	11	5	ND	1	69	.2	2	2	69	.84	.043	9	43	.58	91	.11	2	1.71	.02	.08	1	4
131351	2	45	2	48	.1	22	12	414	3.41	7	5	ND	1	68	.3	2	2	70	.77	.032	10	46	.55	82	.11	2	1.39	.03	.06	1	1
131352	1	70	3	50	.1	31	13	509	3.64	11	5	ND	2	61	.2	2	3	71	.60	.095	11	45	.63	112	.12	2	1.90	.02	.07	1	4
131353	2	69	5	60	.2	31	14	438	3.84	11	5	ND	2	56	.2	2	2	72	.58	.106	10	41	.61	111	.12	2	2.09	.02	.10	1	2
131354	1	46	5	34	.1	24	10	298	3.00	6	5	ND	2	63	.2	2	2	63	.60	.092	10	38	.59	81	.12	2	1.49	.02	.06	1	3
131355	1	63	2	32	.3	25	11	335	3.27	9	5	ND	1	71	.2	3	2	66	.70	.052	9	38	.60	109	.10	2	1.72	.02	.06	1	1
131356	1	79	2	61	.1	32	16	438	4.13	8	5	ND	1	68	.2	3	2	80	.58	.163	7	41	.78	127	.13	2	2.38	.02	.12	1	1
131357	1	48	2	42	.1	25	11	261	3.42	14	5	ND	1	67	.2	2	2	81	.51	.105	6	32	.54	106	.11	2	2.00	.02	.08	1	1
131358	1	33	2	131	.1	21	16	319	4.09	11	5	ND	2	56	.4	2	2	84	.48	.066	7	40	.55	106	.14	2	2.00	.02	.08	1	1
131359	1	106	3	192	.3	27	23	1642	4.70	6	5	ND	1	113	1.2	2	2	96	1.00	.143	6	45	.90	208	.13	2	2.88	.03	.17	1	2
131360	1	59	2	180	.3	62	32	2371	5.50	7	5	ND	1	101	1.6	3	2	109	.92	.105	4	122	1.91	220	.22	2	3.86	.01	.36	1	4
RE 131349	1	59	2	40	.1	21	11	475	3.08	11	5	ND	3	67	.7	2	2	63	.79	.095	14	40	.57	82	.11	2	1.33	.02	.06	2	2
STANDARD C/AU-S	21	59	38	130	7.3	70	32	1127	4.00	42	18	7	40	53	17.3	17	18	57	.49	.092	41	58	.90	174	.09	32	2.00	.06	.14	12	45
STANDARD C	20	62	39	133	7.3	70	32	1064	3.94	40	18	7	40	52	19.0	15	20	54	.48	.091	39	58	.88	176	.09	32	1.93	.06	.16	11	-

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
131361	2	45	5	71	.1	20	15	509	3.50	5	5	ND	1	63	.2	2	2	81	.56	.092	7	37	.62	92	.14	6	1.87	.02	.08	1	2
131362	2	134	7	254	.2	26	19	510	4.82	16	5	ND	2	52	.3	2	2	93	.47	.117	7	39	.76	176	.15	5	3.36	.02	.09	1	1
131363	2	144	11	133	.6	34	23	468	6.32	43	12	ND	3	58	.4	2	2	122	.48	.178	7	49	1.06	166	.17	5	4.15	.03	.14	1	1
131364	2	215	2	82	.2	26	18	395	5.34	16	5	ND	4	51	.2	2	2	117	.41	.198	8	45	.92	131	.15	4	4.60	.02	.08	1	2
131365	1	69	5	120	.1	21	11	281	4.25	3	5	ND	3	46	.2	3	2	84	.39	.085	8	40	.57	91	.15	4	3.33	.02	.07	1	1
131366	1	50	6	40	.4	15	9	228	3.94	10	5	ND	2	47	.2	3	2	94	.40	.120	8	36	.46	83	.13	3	2.31	.02	.06	1	4
131367	1	50	7	89	.1	16	12	269	3.79	12	5	ND	3	52	.2	2	2	91	.46	.098	8	37	.57	97	.14	4	2.32	.02	.08	1	2
131368	1	33	13	139	.1	15	10	254	3.85	2	6	ND	3	44	.3	2	2	107	.40	.069	7	40	.62	79	.16	2	2.51	.02	.07	1	1
131369	1	69	2	107	.2	20	13	491	4.06	7	5	ND	3	65	.5	2	2	94	.66	.184	10	38	.70	182	.13	2	2.00	.03	.12	1	3
131370	1	49	3	56	.1	19	11	333	3.63	6	5	ND	3	50	.2	2	2	89	.53	.162	10	31	.54	102	.13	3	2.00	.02	.09	1	4
1371	1	45	3	42	.2	19	9	231	2.94	5	5	ND	2	55	.2	2	2	71	.60	.143	9	31	.45	89	.10	2	1.61	.02	.05	1	4
131372	2	82	3	53	.1	22	13	318	3.67	4	5	ND	1	80	.2	2	2	75	.78	.082	9	38	.64	123	.12	2	2.30	.03	.07	1	3
131373	2	40	10	103	.2	15	8	250	3.72	6	5	ND	2	46	.2	2	2	81	.47	.228	8	35	.50	92	.12	2	2.13	.02	.08	1	6
131374	1	60	4	64	.1	22	11	296	3.88	9	5	ND	3	55	.6	2	2	92	.58	.147	11	38	.60	88	.13	2	1.99	.02	.08	1	1
131375	2	158	2	185	.2	17	13	302	6.91	27	8	ND	2	61	.4	2	2	135	.40	.240	7	41	.70	135	.27	3	2.69	.02	.15	1	5
131376	1	75	3	34	.1	21	11	252	3.81	13	5	ND	2	65	.2	2	2	86	.51	.094	10	40	.57	83	.13	2	2.34	.02	.06	1	2
131377	2	63	2	42	.1	17	10	242	5.49	14	5	ND	2	73	.2	3	2	125	.37	.102	7	45	.50	110	.17	2	2.33	.02	.07	1	3
131378	2	53	6	35	.3	12	8	201	3.47	6	13	ND	3	51	.3	2	2	82	.36	.059	10	33	.45	66	.14	2	1.89	.02	.06	1	1
131379	1	55	7	48	.1	20	11	378	3.15	8	5	ND	3	60	.2	2	2	66	.60	.073	14	38	.62	99	.12	2	1.84	.02	.07	1	3
131380	1	43	9	62	.1	25	9	309	3.19	6	5	ND	4	48	.2	2	2	59	.45	.074	16	37	.60	102	.12	2	1.68	.02	.08	1	1
131381	1	41	11	305	.1	30	13	313	4.21	21	5	ND	3	34	1.3	2	2	79	.33	.202	8	42	.56	106	.12	2	2.55	.02	.07	1	2
131382	1	40	2	104	.1	28	12	368	3.69	9	5	ND	3	42	.2	3	2	74	.36	.082	9	44	.54	113	.11	2	2.40	.01	.06	1	1
131383	2	69	6	144	.6	26	15	379	3.75	12	5	ND	4	53	.4	2	2	79	.40	.195	10	44	.53	88	.12	2	2.44	.02	.06	1	2
131384	1	62	4	47	.2	26	13	278	3.60	8	7	ND	3	46	.2	2	2	86	.39	.111	9	43	.54	92	.13	2	2.02	.02	.07	1	1
131385	1	45	6	43	.1	21	12	319	2.93	3	5	ND	2	64	.4	2	2	73	.65	.096	12	37	.66	106	.14	3	1.57	.02	.05	1	4
131386	1	55	5	49	.1	27	12	296	3.13	6	5	ND	4	48	.2	2	3	69	.38	.091	10	40	.60	113	.14	2	2.06	.02	.04	1	9
131387	1	65	7	43	.1	16	10	491	2.87	4	5	ND	1	73	.5	2	2	72	.85	.106	12	35	.57	86	.11	2	1.31	.02	.04	1	9
131388	1	60	5	56	.3	19	11	349	2.85	5	5	ND	1	69	.5	2	2	67	.69	.073	12	33	.59	102	.12	3	1.78	.02	.06	1	9
389	1	37	7	50	.1	16	9	340	2.76	7	5	ND	2	64	.2	2	2	76	.68	.126	10	33	.59	99	.13	2	1.45	.02	.04	1	1
.390	1	34	3	64	.2	13	9	325	3.01	6	5	ND	1	42	.2	2	2	74	.38	.118	7	32	.33	77	.11	2	1.55	.02	.04	1	5
131391	1	28	3	72	.1	15	10	239	3.47	5	5	ND	2	46	.2	2	2	80	.43	.093	9	35	.39	86	.11	3	1.80	.02	.04	1	3
131392	1	46	9	58	.1	21	10	308	3.09	10	5	ND	3	53	.2	3	2	75	.54	.090	9	35	.54	87	.12	2	1.63	.01	.06	1	6
131393	1	39	10	57	.2	17	9	340	2.64	5	5	ND	2	56	.5	2	2	68	.55	.092	10	32	.55	82	.11	2	1.42	.02	.05	1	4
131394	1	37	4	72	.2	20	12	345	3.29	4	5	ND	1	42	.2	2	2	81	.54	.099	9	37	.49	90	.09	2	1.68	.01	.05	1	1
131395	1	24	4	55	.1	17	9	296	2.91	5	7	ND	2	38	.2	2	2	70	.35	.109	8	34	.37	86	.09	2	1.44	.01	.05	1	4
131396	1	17	4	70	.1	12	9	363	2.37	3	5	ND	1	47	.8	2	5	61	.43	.042	8	29	.39	77	.11	2	1.29	.01	.06	1	3
RE 131387	1	65	9	43	.3	16	10	493	2.90	6	5	ND	1	74	.2	2	2	73	.87	.098	11	36	.57	98	.12	2	1.33	.03	.05	1	9
STANDARD C/AU-S	20	64	38	133	7.4	74	33	1145	4.01	36	22	8	41	53	19.0	16	19	60	.49	.090	40	60	.92	179	.10	34	2.04	.07	.17	11	46
STANDARD C	20	62	40	132	7.3	70	32	1081	3.94	38	23	7	39	53	18.7	18	22	57	.48	.088	39	58	.88	176	.09	35	1.92	.06	.15	12	-

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
131397	1	38	7	55	.2	22	9	433	2.61	2	5	ND	1	50	.2	2	2	63	.61	.051	10	39	.62	104	.11	2	1.49	.02	.06	1	4
131398	1	44	2	60	.3	30	12	459	3.20	2	5	ND	2	51	.2	2	2	78	.63	.063	11	44	.65	117	.11	2	1.58	.02	.06	1	5
131399	1	32	2	30	.1	12	7	254	2.03	4	5	ND	3	45	.2	3	2	54	.63	.083	10	28	.47	81	.11	2	1.13	.02	.03	1	3
131400	1	24	3	40	.2	19	10	226	2.18	5	5	ND	2	49	.2	2	2	56	.60	.055	9	34	.58	99	.11	2	1.48	.02	.04	1	6
131401	1	23	2	51	.1	16	10	297	2.31	2	5	ND	1	44	.3	2	2	68	.53	.055	8	29	.56	88	.12	2	1.57	.02	.04	1	4
131402	1	33	2	44	.2	18	10	250	2.27	2	6	ND	1	47	.2	2	2	56	.59	.082	9	32	.54	95	.10	2	1.45	.02	.05	1	4
131403	1	65	5	111	.2	30	17	740	4.51	24	5	ND	1	71	.4	2	2	104	.85	.076	8	55	.92	133	.10	2	2.20	.03	.10	1	2
131404	1	19	2	51	.2	16	8	372	2.07	4	5	ND	1	43	.4	2	2	43	.46	.101	9	37	.45	99	.08	2	1.09	.02	.05	1	2
131405	1	13	2	89	.4	21	8	289	2.09	2	5	ND	2	38	.2	2	2	44	.42	.063	9	37	.52	88	.10	2	1.26	.01	.05	1	2
131406	1	59	2	37	.2	27	8	297	2.50	4	5	ND	2	50	.2	3	2	59	.63	.095	14	44	.57	79	.11	2	.94	.02	.04	1	4
131407	1	224	7	49	.7	34	10	413	3.10	4	5	ND	1	55	.2	2	2	62	.63	.051	15	49	.64	141	.07	2	1.71	.02	.05	1	6
131408	1	45	7	45	.1	29	10	379	3.05	6	5	ND	1	64	.2	2	2	76	.77	.130	11	43	.60	121	.08	5	1.29	.02	.05	1	26
131409	1	25	2	37	.2	26	8	299	2.23	3	5	ND	2	55	.2	2	2	51	.61	.095	11	40	.57	94	.11	2	.96	.02	.04	1	8
131410	1	50	3	51	.2	29	11	380	3.18	10	5	ND	2	63	.3	2	2	76	.69	.103	10	43	.63	123	.10	2	1.58	.02	.06	1	10
131411	1	25	3	42	.2	18	7	215	2.03	2	5	ND	1	49	.2	2	2	50	.51	.039	8	39	.70	106	.07	2	1.43	.02	.04	1	7
131412	1	41	7	69	.1	24	13	377	3.68	13	5	ND	1	63	.2	2	2	86	.50	.072	8	38	.60	138	.13	2	2.07	.02	.06	1	3
131413	1	73	3	46	.1	22	11	303	3.24	7	5	ND	3	68	.2	2	4	74	.61	.075	11	38	.64	128	.15	2	2.27	.03	.04	1	7
131414	1	66	4	59	.2	21	12	298	3.58	4	5	ND	2	131	.2	2	2	79	.47	.087	9	38	.56	122	.13	2	2.64	.02	.04	1	3
131415	1	53	2	44	.2	25	11	249	3.78	8	5	ND	3	51	.3	2	4	80	.48	.086	9	40	.55	110	.13	2	2.64	.02	.04	1	11
131416	1	57	10	72	.2	31	14	255	3.93	5	5	ND	3	41	.3	2	2	85	.38	.101	9	43	.52	98	.12	4	2.57	.02	.04	1	3
131417	1	56	5	50	.2	27	12	363	3.35	7	5	ND	3	64	.2	2	2	80	.60	.081	10	43	.62	121	.14	2	2.00	.02	.05	1	4
131418	1	37	3	78	.2	28	13	488	3.68	5	5	ND	2	51	.2	2	2	86	.49	.085	8	41	.60	101	.14	3	2.09	.02	.06	1	3
131419	1	74	5	129	.1	24	14	330	3.75	9	5	ND	2	82	.7	2	2	83	.56	.102	10	42	.63	91	.12	2	2.28	.02	.07	1	3
131421	1	29	8	58	.2	18	9	258	2.88	2	5	ND	3	40	.2	2	2	69	.37	.098	9	38	.35	78	.10	2	1.71	.02	.03	1	8
131422	1	51	5	64	.2	24	11	255	3.46	3	5	ND	3	67	.2	2	2	76	.46	.160	8	38	.49	96	.11	2	2.08	.01	.05	1	5
131423	1	49	4	55	.6	29	13	259	3.73	6	5	ND	4	40	.2	3	2	94	.42	.085	7	43	.56	91	.11	2	1.87	.02	.05	1	4
131424	1	21	8	47	.3	17	9	225	2.71	2	5	ND	2	42	.2	2	2	71	.43	.076	8	35	.44	60	.11	5	1.26	.02	.04	1	5
131425	1	32	2	42	.1	25	11	208	2.79	2	5	ND	2	40	.2	2	2	69	.41	.061	8	38	.49	96	.11	2	1.88	.02	.04	1	21
426	1	16	2	28	.2	16	7	191	2.46	2	5	ND	2	37	.2	2	2	61	.46	.060	8	28	.39	61	.11	3	1.12	.01	.04	1	8
131427	1	21	2	30	.2	16	8	259	2.15	2	5	ND	2	44	.2	2	2	54	.53	.063	9	29	.45	68	.11	4	1.05	.02	.03	1	3
131428	1	33	2	32	.1	20	9	275	2.48	2	5	ND	1	49	.2	2	2	64	.62	.067	9	34	.50	85	.11	2	1.25	.02	.04	1	10
131429	1	34	2	29	.1	19	8	291	2.50	2	5	ND	3	62	.2	2	2	61	.67	.113	11	34	.51	85	.11	3	1.07	.02	.03	1	7
131430	1	48	9	78	.4	23	18	584	4.11	4	5	ND	5	62	.6	2	2	98	.67	.261	10	45	.86	176	.11	2	1.86	.03	.09	1	2
131431	2	75	8	60	.1	33	19	486	6.80	10	5	ND	2	64	.5	2	2	216	.64	.108	10	83	.58	117	.12	2	1.51	.02	.07	1	5
131432	1	100	2	46	.2	38	13	493	3.32	6	5	ND	4	69	.4	2	2	75	.68	.120	14	50	.71	103	.11	2	1.30	.03	.06	1	6
131433	1	56	3	65	.3	47	13	500	3.51	4	5	ND	3	61	.2	2	2	68	.64	.088	14	63	.88	143	.11	2	1.57	.03	.08	1	6
RE 131415	1	47	4	40	.2	21	10	227	3.43	6	5	ND	2	47	.2	2	2	73	.44	.080	8	37	.49	102	.13	5	2.30	.02	.04	1	11
STANDARD C/AU-S	19	58	38	132	7.6	74	34	1069	4.01	37	20	7	40	53	18.9	16	22	58	.49	.094	40	58	.90	182	.09	34	2.02	.07	.16	11	47
STANDARD C	19	60	38	133	7.5	72	33	1053	3.99	36	18	7	41	52	18.3	15	21	56	.48	.090	39	58	.88	176	.09	34	1.91	.06	.15	12	-

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
131434	1	47	8	119	.2	40	19	535	3.92	8	5	ND	3	61	.4	2	2	88	.47	.238	9	62	.72	177	.10	2	2.10	.02	.06	1	3
131435	1	70	6	52	.1	40	14	545	3.27	8	5	ND	3	60	.2	2	2	76	.63	.096	15	59	.74	118	.12	2	1.26	.02	.05	1	6
131436	1	26	2	95	.3	19	13	381	3.61	9	5	ND	3	54	.2	2	2	80	.54	.359	9	43	.53	198	.08	2	1.66	.02	.05	1	1
131437	1	55	2	48	.2	25	14	308	4.86	10	5	ND	4	66	.8	3	2	145	.73	.139	11	63	.58	98	.11	2	1.42	.02	.05	1	1
131438	1	33	3	61	.1	15	9	302	2.58	2	5	ND	1	71	.7	2	2	61	.66	.082	8	31	.69	142	.11	2	1.89	.02	.07	1	1
131440	1	121	8	65	.1	17	10	282	2.21	4	5	ND	1	62	.5	2	2	59	.79	.109	17	39	.63	168	.06	2	1.90	.02	.05	1	4
131441	2	31	2	55	.1	16	12	442	3.41	6	5	ND	2	61	.2	2	2	68	.76	.089	7	24	.81	88	.09	2	1.42	.04	.07	1	1
131442	1	46	2	76	.1	18	13	244	4.73	5	5	ND	1	37	.6	2	2	113	.36	.113	5	42	.45	87	.10	2	2.24	.01	.06	1	20
131443	1	58	6	71	.1	17	19	744	5.40	9	5	ND	2	32	.4	3	2	126	.51	.106	5	28	1.17	95	.06	2	2.62	.02	.14	1	1
131444	1	44	5	121	.4	14	16	319	5.52	13	5	ND	3	27	.4	5	2	124	.27	.226	7	39	.62	142	.04	2	3.33	.01	.09	1	3
131445	1	36	12	131	.6	14	15	535	4.77	7	5	ND	4	28	.3	4	2	116	.32	.146	7	38	.60	150	.04	2	3.13	.01	.09	1	2
131446	1	41	7	62	.1	25	11	299	2.98	5	5	ND	1	57	.4	2	2	82	.52	.039	9	39	.70	124	.12	3	2.03	.02	.05	1	3
131447	1	26	10	56	.1	16	9	288	2.46	2	5	ND	1	50	.2	2	2	74	.63	.059	8	30	.62	91	.15	3	1.53	.02	.05	1	6
131448	1	46	4	62	.1	24	13	487	3.32	7	5	ND	2	66	.5	2	2	87	.82	.123	14	46	.71	124	.13	4	1.64	.02	.06	1	5
131449	1	56	2	62	.1	30	13	510	3.12	4	5	ND	2	65	.3	2	2	70	.73	.063	13	46	.81	113	.15	3	1.60	.03	.06	1	8
131450	2	58	9	95	.2	27	24	1059	4.14	11	5	ND	3	58	.6	3	2	127	.85	.083	12	45	.92	240	.13	2	2.20	.02	.06	1	3
131451	1	48	18	158	.4	18	15	674	3.98	10	5	ND	3	59	.6	2	2	99	.83	.105	12	41	.86	189	.10	2	1.79	.02	.08	1	4
131452	1	45	13	176	.1	16	19	646	4.19	2	5	ND	2	52	.2	2	2	102	1.01	.160	10	43	1.69	177	.11	5	2.58	.02	.09	1	1
131455	1	130	11	116	.1	31	20	866	4.57	16	5	ND	3	90	.9	3	2	111	1.03	.127	13	45	1.05	190	.17	2	2.03	.04	.17	1	8
131456	1	47	150	610	1.3	30	14	494	3.71	11	5	ND	2	51	1.1	2	2	79	.58	.130	10	54	.92	208	.13	6	2.37	.02	.06	1	9
131457	1	33	62	474	.1	27	13	532	3.59	6	5	ND	2	47	.7	2	2	78	.61	.127	10	49	.83	188	.11	5	2.47	.01	.10	1	2
131458	1	46	49	667	2.6	34	15	1089	3.92	15	5	ND	2	52	1.3	2	2	85	.50	.053	10	54	.80	279	.15	2	2.21	.02	.07	1	18
131459	1	81	43	682	1.0	33	27	637	4.36	12	5	ND	1	46	1.4	8	4	105	.55	.090	9	64	.86	353	.13	4	2.48	.01	.07	1	8
131460	1	47	11	115	.5	43	15	393	3.67	7	5	ND	3	48	.4	2	2	73	.46	.125	10	60	.80	239	.13	2	2.57	.01	.06	1	1
131461	1	60	10	94	.4	39	15	427	3.67	12	5	ND	3	55	.3	4	2	81	.56	.091	11	59	.84	223	.13	6	2.08	.02	.06	1	2
131462	1	56	7	68	.1	33	12	379	3.41	7	5	ND	2	59	.2	2	2	76	.72	.085	16	56	.75	181	.13	4	1.77	.02	.05	1	4
131463	1	47	4	83	.1	32	14	386	3.57	10	5	ND	2	43	.3	2	2	75	.41	.112	9	50	.70	127	.12	2	2.28	.01	.06	1	21
131464	1	55	12	60	.2	30	12	346	3.63	7	5	ND	4	49	.3	2	2	82	.68	.043	18	53	.67	259	.12	2	1.55	.02	.06	1	7
131465	1	34	3	61	.3	29	11	362	3.24	8	5	ND	3	58	.2	2	2	74	.66	.028	11	48	.68	120	.13	4	1.53	.02	.05	1	7
131466	1	21	5	62	.1	16	8	203	2.70	4	5	ND	1	35	.3	2	2	64	.31	.106	7	34	.35	74	.11	3	1.56	.01	.04	1	18
131467	1	46	7	91	.3	29	13	271	3.70	10	5	ND	4	35	.2	2	2	77	.35	.192	9	45	.59	116	.12	7	2.63	.01	.06	1	3
131468	1	65	2	110	.1	20	18	604	5.41	7	5	ND	3	59	.4	2	2	125	.71	.254	7	40	1.06	201	.14	2	2.62	.03	.11	1	1
131469	1	24	8	174	.2	13	11	616	4.54	9	5	ND	3	30	.3	2	2	119	.33	.149	10	37	.38	100	.09	2	1.82	.01	.07	1	2
131470	1	39	7	104	.1	19	17	400	5.46	3	5	ND	2	33	.7	2	2	129	.34	.162	6	42	.74	211	.04	2	3.16	.01	.11	1	2
131471	1	27	12	72	.1	13	11	390	3.26	8	5	ND	2	62	.2	2	2	79	.90	.149	11	25	.71	120	.11	3	1.62	.02	.06	1	2
131472	2	138	9	85	.1	18	23	1020	5.75	14	5	ND	3	46	.2	2	2	140	.75	.085	13	35	1.39	157	.09	6	2.97	.03	.12	1	2
RE 131463	1	47	8	83	.1	33	14	388	3.54	10	5	ND	2	43	.2	2	2	75	.40	.109	9	53	.68	116	.13	7	2.25	.02	.06	1	18
STANDARD C/AU-S	21	62	35	136	7.4	72	32	1079	3.89	39	17	8	40	52	19.0	18	19	61	.50	.096	40	61	.97	187	.09	35	1.95	.07	.16	11	45
STANDARD C	17	57	36	132	7.0	70	32	1028	3.91	40	18	7	39	52	17.7	14	19	56	.45	.083	38	58	.79	180	.09	34	1.85	.06	.15	13	-

ACME ANALYTICAL

BP Resources Canada Ltd. PROJECT LOC-10161 FILE # 91-1730

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
131473	1	45	5	276	.1	14	17	488	5.24	8	5	ND	3	26	.5	2	2	115	.32	.357	6	38	.73	240	.03	4	3.64	.01	.10	1	6
131474	1	43	4	61	.1	36	17	383	4.14	10	5	ND	2	63	.2	3	2	102	.57	.046	8	77	1.00	112	.19	7	2.14	.02	.07	1	4
131475	1	175	12	80	.1	60	29	1433	6.13	12	5	ND	3	96	.4	2	2	158	.78	.151	11	142	2.11	206	.22	7	2.30	.02	.16	1	6
131476	1	107	8	112	.1	32	22	672	5.52	14	5	ND	1	55	.2	2	2	120	.53	.232	7	56	1.11	239	.08	6	3.03	.01	.08	1	2
131477	3	92	22	211	.1	21	16	427	5.29	12	6	ND	3	33	.5	2	2	119	.32	.241	8	41	.92	117	.08	2	3.68	.01	.06	1	15
131478	1	104	6	111	.1	31	17	376	4.64	10	5	ND	3	34	.4	2	2	102	.40	.100	8	50	.96	188	.10	2	3.20	.01	.07	1	3
131479	1	15	25	243	.2	17	9	221	3.37	10	5	ND	2	35	.7	3	2	81	.36	.041	7	40	.45	145	.11	2	1.61	.01	.04	1	2
131480	1	19	51	368	.7	16	11	265	3.71	10	5	ND	1	40	.7	3	2	89	.45	.054	6	41	.49	202	.11	7	1.74	.01	.04	1	1
131481	1	40	49	258	.5	20	13	392	3.44	14	5	ND	2	53	.8	6	2	90	.64	.071	8	41	.66	256	.11	6	1.91	.02	.05	1	4
131482	1	41	12	177	.1	19	11	248	2.90	6	5	ND	1	47	.4	2	2	67	.53	.041	7	39	.51	142	.11	2	1.95	.02	.04	1	1
483	1	17	113	398	2.5	15	7	288	2.13	8	5	ND	2	40	.8	5	2	53	.39	.045	8	31	.47	387	.11	5	1.51	.01	.04	1	6
131485	1	35	8	63	.2	18	10	527	2.67	9	5	ND	1	47	.2	2	2	69	.52	.077	9	36	.51	274	.10	3	1.37	.02	.04	1	4
131486	1	40	7	63	.3	24	10	327	2.89	10	5	ND	3	43	.4	2	2	68	.54	.082	10	39	.55	284	.10	6	1.47	.01	.05	1	4
131487	1	47	9	82	.2	26	11	559	3.10	11	5	ND	3	50	.2	3	2	74	.54	.092	11	38	.63	373	.11	5	1.53	.02	.06	1	4
RE 131483	1	19	114	418	2.5	17	8	300	2.21	7	5	ND	2	42	.8	2	2	55	.40	.046	8	32	.49	407	.11	4	1.58	.01	.04	1	4
131488	1	25	11	102	.3	18	9	309	2.88	9	5	ND	2	41	.2	2	2	66	.45	.096	9	36	.56	291	.11	5	1.60	.01	.04	1	3
131489	1	25	3	89	.2	18	12	377	3.55	5	5	ND	1	39	.2	2	2	79	.37	.087	7	36	.60	455	.10	2	1.73	.01	.05	1	2
131490	1	16	10	162	.9	16	10	666	2.99	4	5	ND	3	29	.3	3	2	65	.31	.145	8	33	.45	255	.09	3	1.53	.01	.05	1	1
131491	1	32	2	72	.3	27	11	282	3.15	8	7	ND	2	36	.2	2	2	73	.37	.072	7	39	.56	368	.10	2	1.89	.01	.05	1	2
131496	1	11	9	125	.1	10	8	425	3.10	2	5	ND	1	26	.2	2	2	86	.31	.038	5	31	.23	238	.09	3	1.14	.01	.04	1	1
131497	1	21	16	290	.5	15	12	860	3.44	7	9	ND	2	33	.2	5	2	75	.36	.083	7	28	.38	1031	.07	2	1.30	.01	.10	1	1
131498	1	20	4	196	.3	22	10	385	3.23	8	5	ND	2	31	.4	4	2	73	.43	.053	6	35	.45	372	.06	2	1.47	.01	.08	1	3
131499	1	13	16	175	1.1	10	8	686	2.61	2	5	ND	1	33	.2	2	2	65	.36	.061	7	27	.31	433	.10	4	1.09	.01	.05	1	1
131500	1	15	16	162	.8	9	9	669	3.38	9	5	ND	2	32	.5	2	2	87	.34	.058	7	21	.35	865	.09	4	1.50	.01	.06	1	2
STANDARD C/AU-S	19	59	38	133	7.6	73	34	1075	4.01	36	24	7	39	53	18.8	17	18	57	.49	.095	39	59	.91	186	.09	34	1.95	.06	.15	11	53
STANDARD C	18	61	38	132	7.4	70	31	1048	3.97	38	22	7	40	53	18.1	17	19	55	.48	.090	39	58	.88	175	.09	34	1.89	.06	.15	13	-

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

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700 - 890 W. Pender St., Vancouver BC V6B 4W3

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
130124	3	67	2	63	.1	17	11	469	3.35	10	5	ND	2	55	.2	2	2	75	.64	.115	17	39	.57	85	.09	2	1.35	.02	.05	1	3
130125	2	93	2	52	.1	18	10	238	2.57	4	5	ND	2	60	.2	2	2	59	.56	.089	14	36	.71	98	.09	4	1.80	.02	.05	1	2
130126	5	135	4	73	.2	23	15	481	4.46	16	8	ND	5	55	.2	2	2	93	.65	.119	23	58	.67	98	.09	2	1.94	.02	.06	1	6
130127	2	90	3	79	.1	21	10	284	3.20	9	5	ND	2	50	.2	2	6	92	.63	.132	14	48	.63	88	.09	2	1.60	.02	.06	1	4
130128	3	72	2	77	.2	17	12	377	3.77	13	5	ND	4	42	.2	2	2	95	.55	.137	13	51	.56	94	.10	3	1.68	.01	.05	1	17
130129	3	109	5	66	.1	23	12	320	3.78	13	5	ND	6	53	.2	2	2	85	.61	.121	14	48	.62	102	.10	2	1.71	.02	.05	1	15
130130	1	72	2	44	.1	16	11	237	3.44	6	5	ND	2	43	.2	2	5	97	.48	.112	7	46	.40	64	.08	3	.93	.01	.05	1	1
130131	1	45	2	59	.1	13	11	249	3.37	14	5	ND	3	36	.2	2	2	86	.42	.154	7	42	.33	62	.07	3	1.03	.01	.04	1	1
130132	1	58	5	48	.3	29	11	389	3.09	12	5	ND	2	51	.2	2	2	76	.60	.085	10	44	.56	122	.08	3	1.20	.02	.07	1	27
130133	2	82	2	51	.1	26	11	263	3.83	7	5	ND	4	47	.2	2	2	118	.70	.133	12	66	.65	84	.12	3	1.16	.02	.09	1	6
130134	1	35	2	30	.2	15	9	272	2.28	6	5	ND	3	48	.2	2	2	55	.53	.098	9	32	.39	73	.07	2	.85	.01	.04	1	2
130135	1	84	3	115	.2	36	16	376	4.14	10	5	ND	2	54	.2	2	2	91	.54	.145	7	53	.74	108	.10	2	1.80	.01	.11	1	5
130136	1	57	2	77	.2	24	18	388	3.98	12	5	ND	3	52	.2	2	2	102	.35	.092	7	52	.65	134	.10	2	2.07	.01	.05	1	8
130137	1	55	2	148	.1	21	15	346	4.97	10	5	ND	2	42	.2	2	2	122	.34	.223	7	52	.49	95	.09	2	2.45	.01	.05	1	6
130138	1	44	2	260	.5	32	14	444	3.67	8	5	ND	2	54	1.0	4	2	69	.58	.313	9	50	.70	289	.08	2	1.91	.01	.09	1	10
130139	1	29	2	91	.1	36	10	268	2.55	8	5	ND	3	35	.2	2	2	54	.47	.143	9	40	.59	102	.08	4	1.40	.01	.06	1	1
130140	1	27	2	84	.1	28	11	348	3.51	3	5	ND	3	44	.2	2	2	91	.61	.141	8	47	.55	73	.08	2	1.22	.01	.07	1	1
130141	1	35	2	160	.3	28	10	316	2.96	9	5	ND	2	34	.3	2	2	54	.37	.128	8	47	.52	80	.10	3	1.42	.01	.05	1	1
130142	2	78	2	77	.1	22	12	531	3.14	11	5	ND	1	58	.2	2	2	70	.77	.078	12	45	.62	136	.09	3	1.78	.02	.06	1	4
130143	1	50	2	55	.1	21	10	376	3.04	7	5	ND	1	46	.2	2	3	78	.66	.063	9	42	.61	79	.12	2	1.37	.02	.06	1	3
130144	1	39	2	54	.2	21	11	405	3.17	8	5	ND	1	43	.3	2	2	80	.65	.067	7	40	.59	87	.10	2	1.39	.02	.06	1	2
130145	1	27	2	39	.1	20	9	287	2.74	3	5	ND	1	44	.2	2	2	69	.61	.057	8	41	.54	79	.11	2	1.17	.02	.05	1	5
130146	1	89	3	82	.2	31	12	542	3.67	9	5	ND	1	51	.3	2	6	83	.78	.073	11	44	.72	132	.10	2	1.86	.02	.08	1	7
130147	1	42	2	68	.1	23	13	510	3.54	9	5	ND	1	47	.2	2	2	88	.64	.039	6	39	.60	104	.11	2	1.55	.02	.06	1	1
130148	1	44	2	64	.1	23	12	457	3.51	11	5	ND	1	50	.4	2	2	84	.75	.064	8	40	.60	100	.11	5	1.68	.03	.07	1	2
130149	1	33	6	149	.1	22	14	334	6.95	7	5	ND	3	39	.2	2	2	223	.59	.143	9	91	.42	53	.11	2	1.11	.01	.06	1	59
RE 130145	1	30	2	39	.1	18	9	278	2.71	6	5	ND	1	44	.2	2	2	70	.61	.057	7	38	.52	80	.11	2	1.15	.02	.05	1	5
130150	1	67	5	70	.1	27	15	479	3.68	16	5	ND	1	50	.3	2	2	88	.63	.073	9	42	.67	100	.12	2	1.72	.02	.08	1	12
51	1	53	5	71	.2	31	13	334	3.30	10	5	ND	2	46	.2	2	2	77	.49	.053	8	42	.63	93	.11	5	1.62	.02	.06	1	1
130152	1	29	3	66	.2	31	11	258	3.25	6	5	ND	2	37	.2	2	2	66	.35	.113	9	49	.55	99	.09	2	1.50	.01	.05	1	3
130153	1	45	2	58	.1	36	15	329	3.73	16	5	ND	1	37	.6	2	2	77	.35	.089	8	47	.66	116	.10	2	2.10	.01	.06	1	1
130154	1	62	4	93	.1	58	16	308	4.11	6	5	ND	3	31	.2	2	2	73	.24	.132	10	63	.77	132	.10	3	3.11	.01	.05	1	1
130155	1	37	3	136	.1	27	13	316	3.88	12	5	ND	2	46	.8	2	5	80	.37	.105	8	42	.57	108	.11	2	2.22	.01	.05	1	1
130156	2	85	5	45	.1	21	14	280	3.94	16	5	ND	1	47	.4	2	4	89	.53	.052	9	37	.51	70	.12	2	1.77	.02	.05	1	6
130157	1	88	5	46	.4	27	19	332	4.60	19	5	ND	1	50	.5	2	2	108	.55	.085	7	41	.63	95	.13	5	2.19	.02	.07	1	4
130158	1	85	2	36	.1	26	16	335	3.87	25	5	ND	1	55	.2	2	2	96	.56	.087	7	40	.65	120	.14	2	2.05	.02	.07	1	6
130159	1	40	3	95	.1	23	13	1440	3.30	8	5	ND	1	42	.6	2	2	77	.40	.213	7	39	.41	156	.09	2	1.68	.01	.06	1	1
STANDARD C/AU-S	19	58	30	132	7.9	73	36	1037	4.03	37	6	8	41	57	19.2	19	19	56	.48	.096	40	60	.89	180	.08	31	1.92	.06	.13	11	51
STANDARD C	18	62	37	132	7.3	67	31	1042	3.94	39	22	7	38	52	18.5	15	22	55	.48	.092	38	59	.87	178	.09	32	1.87	.06	.15	11	-

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: SOIL AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

DATE RECEIVED: MAY 29 1991 DATE REPORT MAILED: June 4/91. SIGNED BY..... D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

ACME ANALYTICAL

BP Resources Canada Ltd. PROJECT LCC-10161 FILE # 91-1480 Page 2

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
130160	1	44	7	50	.2	18	10	384	3.51	5	5	ND	1	55	.2	4	3	82	.53	.047	7	39	.57	119	.18	3	2.05	.06	.09	1	6
130161	1	44	3	78	.3	24	12	310	4.06	6	5	ND	2	47	.2	3	3	83	.49	.079	10	52	.57	103	.16	2	2.54	.04	.09	1	1
130162	1	35	5	133	.4	17	15	474	4.02	3	5	ND	3	47	.2	2	2	90	.44	.054	8	41	.44	143	.16	10	2.00	.04	.08	1	3
130163	1	51	6	103	.5	18	16	671	4.06	9	5	ND	1	55	.2	2	4	95	.59	.117	8	38	.50	101	.16	2	2.52	.04	.10	1	5
130164	1	37	5	100	.4	15	12	349	3.96	7	5	ND	1	54	.2	2	3	96	.58	.081	9	40	.48	86	.18	3	2.26	.04	.12	1	1
130165	1	80	6	70	.1	29	14	306	4.11	10	5	ND	2	57	.2	3	2	86	.52	.152	9	47	.67	118	.15	6	3.03	.04	.11	1	13
130166	1	92	7	55	.2	29	14	362	4.21	7	5	ND	3	55	.2	2	2	97	.57	.097	10	55	.75	148	.18	5	2.87	.07	.13	1	5
130167	1	110	4	72	.2	33	13	343	4.35	5	5	ND	3	49	.2	2	2	93	.45	.095	10	56	.71	124	.16	6	3.12	.04	.10	1	11
130168	1	46	8	66	.1	31	10	289	3.77	5	5	ND	1	54	.2	2	2	79	.57	.073	11	55	.64	123	.15	3	2.42	.05	.09	1	3
130169	1	53	4	58	.1	31	12	331	4.00	7	5	ND	1	63	.2	2	2	86	.61	.099	10	52	.70	114	.16	2	2.27	.06	.11	1	7
70	1	39	6	69	.4	26	12	410	3.62	4	5	ND	2	54	.2	2	2	83	.60	.130	9	49	.60	99	.14	4	1.99	.05	.10	1	5
71	1	55	11	94	.2	30	13	431	4.14	6	5	ND	1	67	.2	2	2	90	.74	.141	9	53	.64	117	.14	3	2.22	.05	.13	1	2
130172	1	36	5	128	.4	25	13	409	4.14	8	5	ND	2	54	.2	3	2	89	.60	.168	10	48	.53	73	.12	4	2.12	.03	.10	1	1
130173	1	71	7	65	.2	26	13	513	5.45	7	5	ND	2	56	.2	3	3	139	.58	.028	8	65	.66	86	.17	2	1.79	.04	.10	1	9
130174	1	73	3	65	.5	33	13	593	4.28	6	5	ND	1	60	.2	2	2	100	.76	.048	11	62	.71	119	.13	4	1.91	.05	.10	1	200
130175	1	47	6	67	.3	28	14	544	4.59	10	5	ND	1	57	.2	2	2	112	.68	.037	8	58	.64	109	.13	2	1.78	.05	.09	1	3
130176	1	41	4	62	.1	24	14	584	4.59	9	5	ND	10	58	.2	2	3	107	.63	.027	9	57	.77	95	.16	6	1.67	.08	.09	1	6
130177	1	40	5	55	.1	25	11	494	3.27	8	5	ND	1	59	.2	2	2	82	.66	.052	10	54	.66	99	.15	2	1.43	.08	.09	1	13
130178	1	84	5	84	.1	33	11	456	3.65	7	5	ND	2	64	.2	2	2	84	.77	.068	13	53	.81	130	.16	2	1.81	.08	.11	1	2
130179	1	53	4	74	.1	24	15	670	4.18	6	5	ND	2	68	.2	2	2	97	.85	.124	10	53	.77	123	.16	5	1.67	.06	.12	1	1
130180	1	28	9	107	.1	14	13	342	4.32	5	5	ND	2	39	.4	2	2	107	.45	.182	7	51	.40	89	.11	2	1.39	.03	.06	1	3
130181	1	115	5	138	.3	19	12	367	5.11	8	5	ND	1	37	.2	2	2	114	.37	.250	7	52	.52	85	.11	2	2.80	.02	.07	1	2
130182	1	129	13	224	.5	20	15	385	5.58	12	5	ND	1	39	.2	2	2	108	.35	.342	7	50	.65	111	.14	2	3.55	.03	.10	1	2
130183	1	157	8	174	.2	24	16	374	6.07	12	5	ND	1	65	.2	2	2	131	.41	.168	7	50	.79	122	.14	2	2.96	.02	.09	1	6
RE 130180	1	30	4	108	.2	14	12	341	4.30	4	5	ND	1	39	.2	2	2	110	.45	.181	7	49	.40	88	.12	2	1.38	.02	.06	1	5
130184	1	390	13	167	.6	31	21	425	6.38	17	5	ND	4	87	.2	2	2	146	.50	.108	5	59	1.02	143	.20	4	3.60	.02	.13	1	1
130185	1	416	12	224	.5	29	30	1444	6.53	32	5	ND	1	123	.7	3	2	143	.86	.156	9	58	1.18	235	.17	8	2.69	.03	.17	1	2
130187	3	646	29	232	.9	35	32	1436	7.20	58	5	ND	2	127	.6	2	4	154	1.28	.193	15	62	1.53	190	.24	3	2.61	.05	.26	1	24
130188	2	339	22	121	.2	36	22	767	6.61	32	5	ND	2	105	.2	2	4	178	.81	.122	9	76	1.10	151	.18	6	2.45	.03	.18	1	10
89	1	96	10	65	.2	22	10	323	3.45	7	5	ND	5	54	.2	2	3	75	.60	.134	10	46	.65	78	.15	6	1.81	.04	.11	1	3
130190	1	77	8	71	.2	51	15	442	4.74	9	5	ND	2	52	.2	2	2	111	.39	.069	10	76	1.02	169	.15	3	2.66	.06	.13	1	8
130191	1	67	7	38	.1	25	11	313	3.42	9	5	ND	2	44	.2	2	2	87	.35	.073	7	46	.55	115	.12	4	1.82	.02	.05	1	13
130192	1	18	5	50	.1	21	10	227	3.44	4	5	ND	1	37	.2	2	2	90	.29	.100	8	41	.36	72	.10	4	1.67	.02	.05	1	3
130193	1	32	7	37	.2	21	11	278	4.06	6	5	ND	1	75	.2	2	2	115	.48	.129	8	48	.53	126	.10	3	1.41	.02	.10	1	3
130194	1	36	6	44	.1	26	13	358	6.43	6	5	ND	3	55	.2	2	2	199	.47	.125	10	66	.52	108	.12	3	1.55	.02	.07	1	5
130195	1	37	12	65	.1	26	14	366	6.62	7	5	ND	1	65	.2	2	2	201	.46	.143	7	64	.53	146	.12	6	1.95	.02	.07	1	2
130196	1	38	6	74	.2	29	16	520	10.44	5	5	ND	2	56	.2	2	2	326	.52	.248	10	100	.50	127	.13	5	1.83	.02	.07	1	52
STANDARD C/AU-S	18	61	36	140	7.1	79	36	1033	4.01	39	18	8	41	61	18.9	18	17	63	.48	.090	42	58	.89	186	.11	35	1.88	.08	.19	11	45
STANDARD C	19	61	39	133	7.0	71	33	1044	4.03	36	15	6	38	53	18.6	14	18	57	.47	.089	40	59	.87	184	.09	33	1.89	.07	.15	13	-

ACME ANALYTICAL

BP Resources Canada Ltd. PROJECT LUC-10161 FILE # 91-1480

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
130197	3	27	6	47	.1	24	16	737	4.54	14	5	ND	1	87	.2	2	2	126	.66	.047	7	60	.66	148	.11	2	1.98	.05	.10	1	9
130198	1	21	4	43	.1	13	8	241	2.04	12	5	ND	1	69	.3	3	2	55	.78	.106	9	32	.62	120	.10	6	1.44	.04	.07	1	16
130199	9	91	4	66	.3	31	20	750	7.17	66	5	ND	2	65	.7	2	3	166	.87	.090	12	58	1.14	142	.14	2	2.42	.04	.08	1	8
130201	1	26	3	98	.1	26	16	406	3.20	2	5	ND	1	116	.2	2	2	75	.89	.073	7	41	1.27	203	.10	2	2.56	.05	.11	1	5
130203	4	21	7	34	.4	15	10	209	5.06	14	5	ND	1	48	.4	3	2	168	.41	.052	5	47	.24	128	.13	2	1.55	.03	.08	1	28
130204	1	37	2	70	.1	21	16	395	6.79	10	5	ND	2	65	.9	2	2	212	.48	.224	9	72	.53	147	.10	2	2.06	.02	.06	1	5
130205	1	62	2	79	.2	23	29	840	6.76	20	5	ND	1	105	.5	2	2	175	.62	.357	7	57	.85	305	.14	2	3.28	.04	.13	1	5
130206	2	23	2	77	.3	24	19	393	7.90	8	5	ND	3	48	.2	2	2	240	.46	.317	7	82	.44	115	.10	2	1.93	.02	.07	1	3
130207	1	15	4	119	.3	14	13	753	3.31	11	5	ND	1	40	.9	4	2	85	.32	.171	7	35	.31	93	.08	3	1.97	.02	.05	1	2
130208	1	26	2	38	.1	21	11	240	3.82	13	5	ND	2	45	.2	4	2	110	.39	.115	7	44	.43	82	.09	3	1.41	.02	.05	1	15
09	1	60	2	122	.3	38	15	289	3.95	11	5	ND	2	53	.4	2	2	85	.43	.130	9	58	.73	137	.11	4	2.50	.04	.09	1	7
1..210	2	76	2	197	.4	20	20	935	5.54	15	5	ND	2	75	.8	2	2	133	.53	.421	7	53	.69	202	.12	2	3.28	.03	.12	1	2
130211	1	1073	3	168	.4	15	63	1037	4.50	19	5	ND	1	42	.7	2	6	109	.40	.171	6	44	.42	104	.11	2	1.92	.03	.08	1	3
130212	2	166	11	283	.7	29	23	930	5.81	21	5	ND	3	112	1.2	4	4	148	.70	.094	10	60	.84	214	.13	2	3.48	.03	.10	1	4
130213	1	87	5	84	.1	19	12	311	3.78	17	5	ND	2	50	.3	2	2	96	.49	.119	8	49	.47	92	.10	6	1.61	.03	.06	1	32
130214	2	43	11	117	.1	12	12	670	4.96	10	5	ND	6	30	.2	2	3	135	.33	.255	8	67	.32	58	.11	2	2.32	.02	.06	1	6
130215	1	69	6	163	.3	17	16	658	5.72	8	5	ND	8	29	.5	2	2	167	.34	.268	9	87	.42	73	.12	3	3.36	.02	.07	1	2
130216	3	103	2	102	.6	22	16	459	7.89	13	5	ND	9	37	.8	2	2	273	.41	.232	8	127	.54	75	.14	2	2.87	.02	.08	1	10
130217	1	111	6	120	.1	22	17	441	7.51	13	5	ND	9	42	.5	2	4	241	.53	.244	10	115	.67	78	.16	2	2.34	.03	.08	1	80
130218	2	80	15	107	.3	17	23	817	5.71	15	5	ND	3	61	.9	2	2	161	.72	.152	11	68	.61	90	.11	2	1.61	.02	.07	1	14
130219	3	88	10	81	.1	17	13	402	4.29	14	5	ND	3	61	.7	2	2	109	.67	.122	19	57	.60	97	.11	3	1.82	.02	.08	1	8
130220	1	58	9	132	.2	19	14	257	4.79	13	5	ND	4	41	.3	2	2	110	.40	.236	7	48	.49	97	.10	2	2.50	.02	.06	1	16
130221	1	23	4	110	.1	19	12	288	3.35	4	5	ND	1	50	.7	2	2	81	.45	.092	7	40	.43	99	.13	3	1.80	.03	.07	1	5
130222	1	40	2	148	.4	27	18	514	4.01	9	5	ND	2	52	.8	2	2	92	.51	.199	8	47	.64	92	.12	2	2.33	.03	.08	1	7
130223	1	38	9	51	.1	17	11	466	2.87	6	5	ND	1	56	.5	2	2	73	.65	.097	9	37	.49	65	.11	2	1.16	.03	.06	1	2
130224	1	48	2	75	.1	25	13	512	3.12	8	5	ND	1	72	.5	2	2	79	.73	.079	11	43	.68	107	.14	2	1.58	.05	.09	1	1
130225	3	224	5	159	.6	48	24	872	5.53	24	5	ND	2	68	1.1	2	4	109	.77	.051	16	66	.93	167	.11	3	2.49	.04	.12	1	6
130226	2	72	3	86	.2	26	14	645	4.13	9	5	ND	2	62	.7	2	2	106	.69	.044	11	55	.73	105	.13	3	1.93	.04	.10	1	5
130227	1	47	3	46	.1	19	12	337	4.80	7	5	ND	1	53	.2	2	2	143	.60	.070	9	67	.43	63	.11	4	1.09	.02	.06	1	14
128	1	87	2	49	.2	18	15	376	4.02	9	5	ND	4	60	.4	3	2	96	.59	.039	10	44	.59	76	.14	4	1.76	.03	.09	1	2
130229	1	57	4	42	.1	17	11	245	4.08	4	5	ND	3	49	.3	2	2	113	.56	.093	9	53	.45	62	.11	3	1.38	.02	.07	1	2
130230	1	51	9	39	.1	16	11	245	4.07	7	5	ND	2	45	.6	2	2	117	.56	.097	8	53	.44	61	.11	6	1.24	.02	.07	1	3
130231	2	80	5	150	.3	26	22	319	6.41	21	5	ND	2	68	.7	2	2	128	.60	.164	10	45	.75	144	.14	2	2.86	.03	.11	1	1
130232	1	38	2	94	.1	20	9	242	3.30	8	5	ND	1	58	.2	2	2	73	.57	.069	9	40	.52	79	.15	3	1.82	.03	.08	1	2
130233	1	40	4	55	.1	21	8	272	2.54	5	5	ND	1	65	.4	2	2	60	.60	.068	11	38	.68	84	.17	3	1.68	.04	.08	1	4
130234	1	48	2	85	.2	19	12	328	3.15	5	5	ND	1	62	.3	2	4	73	.66	.069	10	42	.70	89	.16	2	2.09	.03	.10	1	18
STANDARD C/AU-S	17	56	37	131	7.2	70	31	1034	3.94	37	18	7	39	52	18.9	15	19	54	.48	.089	38	58	.87	177	.09	34	1.86	.06	.15	12	45

ACME ANALYTICAL

BP Resources Canada Ltd. PROJECT LOC-10161 FILE # 91-1480

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
130235	1	56	6	69	.1	21	12	287	2.85	12	5	ND	1	59	.2	2	2	66	.54	.057	7	37	.73	98	.10	2	1.78	.03	.08	1	3
130236	1	59	8	49	.1	23	13	289	3.22	12	5	ND	1	65	.2	2	4	75	.66	.067	7	35	.69	111	.10	2	1.78	.03	.08	1	3
130237	1	137	5	79	.2	25	17	558	4.24	15	5	ND	2	62	.2	2	2	100	.75	.059	9	43	.74	115	.12	5	2.37	.03	.09	1	23
130238	1	39	7	90	.3	19	15	322	4.46	22	7	ND	1	43	.4	2	2	103	.57	.305	6	38	.56	103	.09	3	2.08	.02	.09	1	2
130239	1	43	8	75	.1	19	13	264	4.22	18	5	ND	2	44	.3	2	2	97	.44	.110	7	37	.55	75	.09	3	2.25	.02	.06	1	1
130240	1	65	12	126	.1	20	15	352	4.21	15	5	ND	3	40	.3	4	2	98	.52	.368	8	38	.54	124	.08	2	2.46	.02	.07	1	3
130241	3	34	9	40	.1	9	8	155	3.15	12	5	ND	1	31	.4	2	2	69	.38	.091	7	30	.28	41	.06	5	1.12	.01	.03	1	2
130242	1	68	9	41	.1	15	12	393	3.27	18	5	ND	2	93	.2	2	2	83	.87	.126	9	30	.76	134	.18	3	1.52	.10	.20	1	4
130244	1	42	12	49	.3	13	9	227	2.70	14	5	ND	2	47	.2	2	2	67	.44	.079	7	26	.48	115	.11	2	1.48	.03	.06	1	5
130245	1	37	3	76	.2	18	13	220	3.43	22	5	ND	3	39	.3	2	2	75	.34	.129	5	34	.43	110	.09	7	2.01	.02	.05	1	2
[illegible]46	1	55	5	61	.1	17	13	233	3.47	18	5	ND	1	35	.5	2	2	82	.37	.168	5	38	.42	69	.08	4	1.66	.02	.06	1	1
1[illegible]47	1	86	7	52	.1	23	15	447	3.70	18	5	ND	2	55	.2	2	2	101	.62	.137	10	47	.55	85	.10	4	1.34	.03	.10	1	3
130248	1	97	11	58	.1	21	15	515	3.44	11	5	ND	3	71	.2	2	2	87	.69	.119	11	38	.68	116	.11	2	1.42	.04	.12	1	5
130249	1	75	10	71	.1	20	15	591	3.98	12	5	ND	2	69	.2	2	2	99	.99	.121	11	41	.77	113	.10	5	1.74	.03	.11	1	5
130250	1	81	5	58	.1	20	15	362	3.74	16	5	ND	4	49	.2	2	2	91	.49	.099	10	44	.60	90	.11	5	1.63	.02	.08	1	25
130251	1	39	4	56	.1	17	13	254	5.05	15	5	ND	4	33	.2	2	2	145	.47	.321	8	65	.38	100	.07	2	1.38	.01	.04	1	9
130252	2	36	7	59	.1	18	12	431	3.56	9	5	ND	2	42	.2	2	2	106	.45	.048	7	46	.56	61	.11	4	1.33	.02	.06	1	1
130253	1	69	8	62	.2	25	14	511	3.07	12	5	ND	3	49	.2	2	3	74	.57	.049	9	40	.71	97	.12	2	1.59	.03	.07	1	3
130254	1	35	2	64	.2	19	12	229	3.54	11	13	ND	3	35	.2	2	2	88	.38	.087	7	40	.38	72	.08	5	1.43	.02	.08	1	3
130255	2	35	5	65	.2	14	8	224	3.22	16	7	ND	6	37	.2	2	2	79	.36	.102	6	39	.37	62	.10	2	1.02	.02	.07	1	6
130256	4	73	10	84	.1	16	13	426	4.53	18	5	ND	7	37	.2	2	2	98	.42	.111	11	54	.52	110	.09	3	1.83	.02	.05	1	6
130257	2	51	11	87	.4	15	21	620	4.97	21	8	ND	3	48	.3	2	2	119	.49	.163	7	55	.57	108	.09	2	1.42	.02	.07	1	4
130258	1	40	5	52	.1	22	12	303	3.20	11	8	ND	2	45	.2	2	2	68	.42	.144	7	36	.47	95	.09	3	1.66	.02	.05	1	1
130259	1	61	4	44	.1	31	15	336	3.33	13	5	ND	3	44	.2	2	2	72	.35	.085	9	44	.68	145	.11	2	1.88	.02	.07	1	7
130260	1	50	8	82	.3	23	16	689	4.07	13	5	ND	8	43	.2	2	2	95	.44	.278	8	50	.55	114	.10	2	2.34	.02	.07	1	2
130261	2	53	12	187	.3	15	15	726	5.07	13	5	ND	10	28	.2	2	2	124	.33	.330	8	66	.46	85	.09	2	3.40	.01	.07	1	2
130262	1	72	3	41	.1	16	10	255	3.25	13	5	ND	7	32	.2	2	2	84	.44	.125	9	46	.39	60	.08	3	1.21	.01	.06	1	5
130263	1	130	6	253	.3	29	22	606	5.75	24	5	ND	2	134	.3	3	2	129	.56	.245	6	53	.91	316	.09	10	2.98	.02	.10	1	1
130264	1	41	4	179	.3	20	14	311	3.59	18	5	ND	3	33	.2	2	2	78	.43	.096	7	34	.49	62	.08	2	1.93	.02	.04	1	2
[illegible]65	1	141	6	220	.2	31	21	554	6.12	22	5	ND	3	113	.3	2	2	163	.61	.192	6	64	.88	266	.12	2	2.66	.02	.09	1	40
131001	1	45	4	71	.1	33	11	328	3.32	12	5	ND	2	57	.2	2	2	84	.64	.043	6	53	.85	144	.09	2	1.85	.03	.08	1	9
131002	1	29	2	51	.1	33	11	359	2.78	10	5	ND	3	46	.2	2	2	55	.55	.093	10	53	.79	95	.10	2	1.19	.03	.05	1	1
131003	1	20	5	47	.1	23	10	324	2.32	6	19	ND	3	44	.2	2	2	49	.56	.099	10	38	.59	75	.11	4	.95	.03	.06	1	1
131004	1	71	3	37	.2	25	10	323	2.73	10	5	ND	4	56	.3	2	2	63	.58	.105	12	46	.56	106	.09	7	1.05	.03	.05	1	1
RE 131001	1	41	2	66	.2	30	11	320	3.22	8	5	ND	2	55	.2	2	2	81	.63	.040	6	52	.83	138	.08	2	1.83	.03	.08	1	3
131005	1	39	2	134	.2	21	16	582	5.28	6	5	ND	3	41	.2	2	2	156	.46	.175	8	61	.45	91	.08	2	1.31	.01	.06	1	3
131006	1	22	8	48	.2	23	9	266	2.27	7	5	ND	3	40	.2	2	2	47	.41	.083	10	38	.53	83	.09	2	1.08	.03	.06	1	3
STANDARD C/AU-S	21	63	40	139	7.3	82	39	1074	4.04	42	21	8	42	61	20.8	19	24	59	.52	.104	41	67	.96	184	.08	36	2.05	.07	.15	11	52
STANDARD C	18	59	44	134	7.3	74	31	1053	4.00	37	25	7	39	52	18.6	15	19	56	.49	.094	39	60	.87	178	.09	33	1.90	.06	.15	11	-

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
131007	1	128	13	123	.4	23	19	484	5.28	32	5	ND	3	64	.2	2	2	127	.44	.220	6	55	.63	149	.09	5	2.80	.01	.07	3	29
131008	2	267	17	112	.4	28	25	688	7.40	45	5	ND	6	137	.2	5	4	201	.68	.165	9	81	1.09	280	.12	4	2.51	.02	.12	2	2
131009	1	124	8	127	.2	26	21	592	6.45	20	5	ND	4	103	.2	2	2	168	.56	.230	8	70	.82	204	.09	2	2.93	.02	.09	2	3
131010	1	32	9	50	.1	28	11	290	2.71	11	5	ND	1	48	.2	2	2	58	.59	.087	10	41	.70	109	.09	2	1.36	.02	.05	1	3
131012	1	35	2	49	.1	22	10	323	2.94	12	5	ND	2	38	.2	2	3	72	.50	.069	8	38	.61	81	.09	4	1.34	.02	.05	1	3
131013	1	28	7	43	.1	26	10	351	3.08	14	5	ND	3	42	.2	2	2	76	.61	.112	10	41	.59	94	.10	3	1.32	.02	.06	2	6
131014	1	21	7	55	.1	26	10	389	2.80	7	5	ND	2	44	.2	2	2	67	.60	.095	11	44	.69	90	.11	3	1.25	.02	.06	1	3
131015	1	36	8	128	.1	25	12	436	2.94	10	5	ND	1	47	.2	2	3	66	.59	.062	9	47	.69	103	.11	5	1.21	.02	.05	1	1
131016	1	49	7	102	.3	28	14	539	3.52	11	5	ND	3	46	.2	2	2	83	.63	.026	10	51	.71	107	.10	2	1.50	.02	.06	1	2
131017	1	47	8	81	.2	25	15	462	4.00	12	5	ND	3	42	.2	2	2	95	.58	.041	11	52	.63	103	.10	2	1.55	.02	.06	1	1
18	1	50	5	66	.4	20	13	479	3.68	13	6	ND	4	47	.2	2	2	88	.69	.088	10	45	.62	93	.09	4	1.53	.02	.07	1	5
19	1	35	6	55	.4	21	12	403	3.26	14	5	ND	3	49	.2	2	2	78	.59	.078	9	44	.63	89	.11	4	1.36	.02	.05	1	5
131020	1	42	6	50	.1	25	11	405	3.08	10	5	ND	2	44	.2	2	2	76	.57	.070	10	41	.62	98	.09	2	1.46	.02	.05	1	4
131021	1	58	5	181	.1	26	13	502	3.64	10	5	ND	3	48	.2	2	2	83	.61	.058	11	50	.67	87	.11	3	1.53	.03	.06	1	59
131022	1	57	8	91	.2	27	15	366	3.72	14	5	ND	3	42	.4	2	3	88	.51	.115	9	43	.69	109	.10	4	2.19	.02	.07	1	2
131023	1	32	33	382	.2	18	14	517	3.80	17	5	ND	1	41	.9	2	2	88	.42	.065	5	37	.53	89	.10	2	1.90	.02	.07	1	4
131024	1	35	11	225	.3	16	16	473	4.47	12	5	ND	2	196	.6	2	2	98	.62	.272	5	32	.47	217	.11	2	2.51	.02	.11	2	1
131025	1	37	9	163	.3	20	12	349	3.81	12	5	ND	2	37	.3	2	2	87	.44	.087	6	42	.57	67	.11	3	1.96	.01	.06	1	3
131026	1	52	18	284	.5	26	12	578	4.18	16	5	ND	2	57	1.2	2	2	85	.43	.157	7	42	.67	139	.09	3	2.52	.02	.06	1	3
131027	1	28	7	133	.4	16	12	320	4.32	11	5	ND	2	45	.5	2	2	86	.32	.120	7	37	.48	111	.09	2	1.80	.02	.05	1	1
131028	1	25	6	159	.5	39	13	277	3.54	13	5	ND	4	30	.4	2	2	64	.38	.238	11	50	.60	100	.08	5	2.12	.01	.05	1	1
131029	1	27	9	161	.4	16	11	265	4.00	17	5	ND	1	45	.5	2	2	102	.45	.027	6	39	.48	56	.12	2	1.90	.02	.04	1	10
131030	1	68	15	74	.1	26	19	458	4.46	21	5	ND	1	57	.2	2	2	96	.43	.091	6	50	.91	98	.13	5	2.76	.02	.04	1	2
131031	1	57	13	106	.3	26	18	550	5.09	15	5	ND	3	42	.2	2	2	112	.40	.124	7	46	.74	102	.12	2	2.24	.02	.08	1	3
131032	2	42	8	51	.2	16	12	289	3.81	14	5	ND	1	43	.2	2	2	94	.47	.067	7	38	.56	78	.11	6	1.77	.02	.04	2	3
131033	1	26	8	54	.2	15	14	354	3.80	12	5	ND	2	40	.5	2	2	98	.37	.098	7	37	.46	103	.12	2	1.46	.02	.05	1	6
131034	1	23	5	48	.3	15	9	221	3.33	13	5	ND	1	35	.2	2	2	83	.34	.049	7	36	.38	70	.12	5	1.64	.02	.04	1	1
131035	1	80	6	41	.2	26	13	295	3.46	17	5	ND	2	67	.2	2	2	83	.52	.105	9	40	.67	119	.12	3	2.12	.02	.08	1	7
131036	1	34	4	57	.1	27	13	274	3.46	10	5	ND	1	37	.2	2	2	76	.40	.128	9	44	.51	85	.10	2	1.78	.01	.06	1	2
37	1	77	2	59	.1	56	17	523	3.67	11	5	ND	3	64	.2	2	2	76	.53	.083	11	58	.97	135	.13	2	2.21	.03	.09	1	3
131038	1	44	7	73	.1	37	11	289	3.54	8	5	ND	4	36	.2	2	2	68	.38	.105	13	52	.73	72	.11	2	2.08	.01	.05	1	1
131039	1	56	2	43	.1	26	14	308	3.28	13	5	ND	1	51	.2	2	2	78	.53	.091	9	43	.65	95	.12	2	2.02	.03	.06	1	21
RE 131035	1	85	2	46	.3	30	15	312	3.64	13	5	ND	2	75	.3	2	2	88	.56	.115	9	43	.73	125	.12	2	2.29	.02	.09	2	14
131040	1	85	3	56	.2	26	15	444	3.51	12	5	ND	2	53	.2	2	2	88	.57	.103	10	41	.76	107	.14	2	2.32	.02	.09	1	4
131041	1	43	10	65	.2	31	17	294	4.45	9	7	ND	2	46	.3	2	3	94	.52	.164	8	43	.60	119	.11	4	2.27	.02	.09	1	2
131042	1	101	2	36	.1	26	17	294	3.28	11	5	ND	2	50	.2	3	2	78	.47	.043	7	39	.61	75	.15	2	1.70	.03	.06	2	3
131043	1	66	23	106	.3	33	17	312	4.05	32	5	ND	2	60	.2	2	2	83	.39	.096	8	41	.61	107	.11	3	2.61	.01	.07	1	8
STANDARD C/AU-S	21	63	39	146	7.5	71	40	1108	3.93	42	17	8	41	61	21.0	19	21	61	.53	.091	42	65	1.00	196	.07	34	1.96	.07	.14	11	45
STANDARD C	19	60	38	131	7.2	70	34	1045	3.92	39	22	7	39	52	18.5	16	23	56	.47	.090	39	58	.88	173	.09	34	1.86	.06	.15	12	-

ACME ANALYTICAL

BP Resources Canada Ltd. PROJECT D[illegible]-10161 FILE # 91-1480

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
131044	1	66	6	60	.3	26	14	317	3.15	13	5	ND	1	43	.4	2	2	75	.44	.102	7	38	.54	92	.10	2	1.95	.01	.06	1	24
131045	1	40	2	63	.1	36	12	282	2.95	14	5	ND	1	37	.2	2	3	63	.35	.070	8	47	.60	102	.10	3	1.95	.02	.06	1	4
131046	1	62	8	62	.3	44	13	318	3.37	9	5	ND	1	40	.2	2	4	68	.35	.058	9	52	.76	106	.11	2	2.28	.02	.06	1	3
131048	1	75	6	60	.1	30	15	672	3.63	14	5	ND	1	51	.3	2	2	91	.71	.091	13	48	.68	133	.12	5	1.53	.03	.08	1	13
RE 131052	1	33	9	48	.1	23	12	407	3.04	11	5	ND	1	48	.2	2	2	76	.63	.085	9	39	.61	100	.11	2	1.39	.03	.06	1	6
131049	1	57	2	55	.2	26	12	461	3.16	9	5	ND	1	56	.2	2	2	79	.75	.114	11	41	.64	94	.12	2	1.47	.03	.08	1	13
131050	2	103	2	54	.4	28	13	383	3.62	13	5	ND	1	49	.2	4	2	90	.57	.045	10	47	.60	106	.10	4	1.61	.02	.07	1	38
131051	1	52	5	78	.2	30	14	488	3.84	14	5	ND	1	46	.3	2	2	88	.69	.035	7	43	.63	119	.10	3	1.80	.03	.08	1	54
131052	1	35	2	49	.3	25	12	415	3.10	12	5	ND	1	48	.2	2	2	77	.65	.086	9	41	.63	92	.12	2	1.43	.03	.06	1	7
131053	1	43	3	54	.1	20	10	375	2.77	11	5	ND	1	44	.2	2	2	70	.64	.061	9	38	.62	87	.11	2	1.36	.02	.06	1	24
[illegible]54	1	30	3	40	.1	16	10	377	2.88	12	5	ND	1	44	.2	2	2	73	.64	.058	8	40	.55	85	.11	4	1.22	.02	.06	1	7
1[illegible].055	1	43	7	112	.3	12	10	285	3.30	9	5	ND	1	31	.7	2	2	80	.34	.147	5	33	.36	71	.09	3	1.54	.01	.06	1	5
131056	2	37	2	148	.3	18	12	241	4.25	11	5	ND	1	31	.2	2	3	91	.30	.135	6	40	.48	92	.11	2	2.14	.01	.07	1	1
131057	2	133	10	274	.2	21	20	527	5.78	13	5	ND	1	74	.3	2	2	132	.42	.234	5	52	.81	144	.13	2	2.46	.02	.10	1	1
131058	1	86	3	232	.3	18	15	585	4.83	7	5	ND	1	40	.5	2	3	104	.36	.285	7	45	.55	100	.11	2	2.18	.01	.06	1	3
131059	3	717	10	165	.7	28	26	517	6.23	36	5	ND	1	126	.2	3	2	144	.57	.088	5	58	1.24	206	.20	2	3.29	.02	.16	1	6
131061	2	129	5	76	.1	17	10	353	2.75	12	5	ND	1	59	.4	2	2	65	.73	.119	14	44	.66	103	.09	5	1.66	.02	.06	1	97
131062	4	112	8	67	.1	18	14	643	4.14	19	5	ND	1	59	.3	2	2	86	.78	.112	23	53	.61	80	.08	2	1.82	.02	.07	1	14
131063	1	88	2	60	.1	17	12	383	3.73	13	5	ND	1	50	.2	2	2	98	.58	.126	7	41	.52	92	.09	2	1.24	.02	.06	1	8
131064	2	40	4	86	.1	22	16	282	4.71	8	5	ND	1	37	.2	2	2	121	.35	.149	6	50	.43	104	.09	2	1.83	.01	.06	1	3
131065	1	28	2	73	.2	18	11	296	3.34	9	5	ND	1	36	.2	2	2	85	.35	.133	6	38	.43	89	.08	2	1.44	.01	.05	1	12
131066	2	29	6	63	.1	23	18	361	7.16	7	5	ND	2	32	.2	2	2	216	.32	.171	7	84	.32	70	.09	2	1.71	.01	.05	1	87
131067	1	27	9	68	.1	14	10	216	3.51	6	5	ND	3	27	.2	2	2	90	.29	.124	4	47	.29	47	.08	2	1.31	.01	.05	1	9
131068	1	20	2	109	.3	16	15	702	5.89	8	5	ND	7	52	.5	2	2	168	.45	.323	5	63	.46	154	.08	2	2.43	.02	.06	1	5
131069	1	39	2	66	.1	17	11	368	3.75	8	5	ND	2	49	.2	2	2	80	.58	.149	5	37	.77	139	.09	2	2.19	.02	.07	1	2
131070	3	87	9	79	.2	15	12	359	3.05	15	8	ND	1	51	.3	2	2	79	.67	.119	19	50	.62	103	.08	2	1.71	.02	.06	1	9
131071	4	82	7	83	.1	17	12	573	3.31	13	5	ND	1	48	.7	2	2	73	.68	.115	17	47	.58	81	.08	3	1.62	.02	.05	1	1
131072	1	88	10	73	.1	24	11	249	2.44	4	5	ND	1	50	.2	2	2	53	.61	.109	19	49	.75	135	.09	2	2.17	.02	.07	1	9
131073	2	43	8	66	.1	15	13	486	3.62	11	5	ND	2	44	.4	2	2	76	.69	.144	7	33	.85	88	.11	3	1.51	.03	.08	1	16
74	2	43	5	51	.1	12	14	891	3.64	10	5	ND	5	39	.2	2	2	77	.85	.126	12	24	.77	79	.09	2	1.44	.03	.09	1	3
131075	2	41	2	105	.1	26	23	574	5.43	7	5	ND	1	78	.2	2	2	130	.58	.299	9	48	.75	299	.11	2	2.73	.02	.11	1	7
131076	2	17	2	55	.1	14	8	218	1.95	12	5	ND	1	64	.4	2	2	54	.91	.018	4	25	.61	85	.15	2	1.30	.02	.09	1	3
131077	5	33	2	45	.1	25	12	478	2.70	9	5	ND	1	69	.2	2	2	63	.81	.048	6	41	.63	136	.09	2	1.58	.02	.08	1	4
131078	1	25	6	38	.1	23	14	352	4.41	10	5	ND	1	53	.3	2	2	112	.40	.091	5	43	.53	125	.09	2	1.65	.01	.07	1	1
131079	2	93	4	45	.1	23	17	548	6.13	11	5	ND	2	80	.7	2	2	163	.58	.097	9	61	.74	171	.14	2	1.69	.02	.11	1	11
131080	2	56	6	44	.3	25	19	490	6.25	14	5	ND	2	61	.5	2	8	169	.57	.134	7	61	.59	182	.12	2	1.89	.02	.10	1	11
131081	2	19	3	57	.1	19	18	627	6.76	2	5	ND	1	42	.6	2	2	193	.41	.120	6	61	.42	142	.11	2	1.54	.01	.08	1	20
STANDARD C/AU-S	20	58	38	132	7.4	74	35	1099	4.03	37	18	7	37	55	20.7	17	13	57	.48	.091	38	60	.89	179	.09	30	1.91	.06	.14	11	48
STANDARD C	18	56	39	132	7.5	70	31	1031	3.96	38	15	7	36	47	18.8	15	18	56	.48	.090	37	58	.88	177	.09	34	1.88	.05	.15	13	-

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
131082	1	32	2	26	.1	20	10	193	3.49	17	5	ND	2	35	.2	5	2	104	.30	.071	6	41	.39	75	.07	4	1.06	.01	.03	1	3
131083	1	26	10	81	.1	23	17	398	6.30	10	5	ND	4	39	.3	2	2	199	.33	.286	7	68	.39	86	.07	7	1.79	.01	.06	1	86
131084	1	25	3	23	.3	23	10	169	2.68	15	5	ND	2	33	.2	6	2	73	.24	.062	5	33	.37	56	.07	3	1.13	.01	.04	1	5
131085	1	21	2	57	.2	15	16	865	2.45	10	5	ND	2	35	.2	5	2	58	.25	.081	6	32	.31	82	.07	5	1.42	.01	.04	1	11
131086	1	40	3	170	.1	13	13	461	4.13	14	5	ND	1	35	.7	2	2	108	.30	.086	5	38	.51	103	.10	4	1.63	.02	.06	1	1
131087	2	154	6	140	.2	23	20	499	5.16	39	5	ND	1	89	.3	4	3	135	.44	.101	5	47	.77	261	.12	3	2.49	.02	.09	1	6
131088	1	180	12	166	.3	66	22	586	5.05	26	5	ND	2	63	.5	4	2	117	.45	.271	7	80	.80	138	.11	8	3.02	.02	.10	1	5
131089	1	112	9	48	.1	22	13	377	4.10	20	5	ND	4	41	.2	2	2	121	.55	.132	10	50	.47	71	.10	2	1.15	.01	.07	1	55
131090	1	46	3	82	.1	19	11	289	2.98	11	5	ND	1	44	.2	3	2	78	.43	.097	7	38	.47	84	.08	4	1.20	.01	.04	1	3
131091	1	81	2	96	.1	17	14	349	4.49	12	5	ND	7	36	.4	2	2	136	.40	.230	8	63	.53	66	.10	5	2.04	.01	.06	1	16
[illegible]92	1	146	2	70	.1	18	14	482	5.29	15	5	ND	5	41	.3	2	2	176	.45	.159	12	83	.64	87	.14	3	2.01	.02	.09	1	4
1[illegible]093	2	37	4	130	.1	14	11	362	4.60	9	5	ND	4	23	.2	2	2	135	.25	.250	6	67	.34	54	.09	6	2.01	.01	.05	1	15
131094	2	86	8	106	.1	19	15	435	4.57	17	5	ND	1	43	.2	2	2	111	.32	.230	5	47	.52	84	.09	2	2.28	.01	.06	1	200
131095	3	80	11	77	.1	14	10	303	3.10	16	5	ND	1	56	.2	2	2	86	.69	.114	16	46	.54	77	.07	7	1.45	.02	.05	1	5
RE 131100	1	40	7	128	.1	12	11	274	4.00	11	5	ND	1	37	.5	3	2	95	.30	.256	5	37	.38	87	.08	2	1.52	.01	.05	1	3
131096	5	131	2	90	.1	11	12	757	4.21	18	5	ND	1	83	.2	2	2	104	.71	.087	24	51	.54	132	.10	2	1.93	.03	.07	1	8
131097	1	37	2	137	.1	8	11	241	4.73	4	5	ND	4	37	.4	2	2	144	.34	.206	7	64	.31	78	.11	2	1.56	.02	.07	1	2
131098	1	103	6	119	.5	17	15	347	4.76	15	5	ND	2	42	.4	5	6	130	.37	.174	5	52	.51	88	.10	7	1.72	.01	.05	1	10
131099	1	46	4	103	.1	14	10	408	3.65	9	5	ND	1	38	.2	2	2	93	.42	.147	6	35	.45	84	.13	4	1.48	.02	.07	1	3
131100	1	39	9	128	.1	12	11	272	4.01	11	5	ND	1	36	.3	2	2	94	.29	.258	4	36	.38	87	.08	2	1.52	.01	.06	1	1
131101	1	167	2	113	.1	34	17	424	3.73	16	5	ND	1	47	.2	3	2	85	.45	.052	7	42	.61	79	.11	6	1.81	.02	.06	1	5
131102	2	241	13	153	.2	39	28	524	6.82	51	5	ND	1	32	.4	2	2	104	.33	.073	5	41	1.12	48	.07	6	3.32	.01	.08	1	35
131103	1	42	2	63	.3	29	12	269	3.20	17	6	ND	1	51	.2	4	2	74	.51	.085	8	39	.55	55	.11	4	1.63	.02	.06	1	2
131104	1	46	2	40	.1	14	9	183	2.75	12	5	ND	3	39	.2	4	2	57	.37	.137	7	28	.35	38	.07	6	1.10	.01	.05	1	3
131105	1	104	4	56	.1	31	15	309	4.82	12	5	ND	1	47	.3	2	2	126	.51	.115	7	64	.68	112	.14	5	2.23	.02	.11	1	2
131106	2	93	2	70	.1	53	21	351	7.92	16	5	ND	3	42	.7	2	2	252	.50	.139	8	114	.70	110	.12	9	2.28	.01	.13	1	6
131107	1	41	2	48	.1	19	10	309	2.91	8	5	ND	1	43	.2	2	2	77	.45	.061	6	38	.57	67	.11	3	1.29	.02	.06	1	3
131108	1	48	2	60	.1	24	10	234	2.92	8	5	ND	1	49	.3	2	2	69	.47	.067	9	39	.56	83	.13	4	1.76	.02	.06	1	6
131109	1	210	2	100	.3	27	17	781	4.25	13	5	ND	1	66	.2	2	2	95	1.24	.059	8	49	.76	131	.11	7	2.26	.03	.12	1	3
10	1	66	4	63	.1	23	13	254	3.20	8	5	ND	1	65	.2	3	2	70	.58	.088	8	37	.63	123	.13	3	2.21	.02	.10	1	1
131111	1	62	6	60	.1	21	14	307	3.33	13	5	ND	1	56	.2	2	2	84	.70	.121	8	32	.63	103	.14	4	1.99	.03	.10	1	13
131112	1	114	2	86	.1	27	17	342	3.53	8	5	ND	1	71	.2	2	2	80	.85	.095	7	36	.74	159	.12	7	2.43	.03	.11	1	4
131113	1	62	9	127	.3	15	11	380	3.28	11	5	ND	2	46	.2	2	2	78	.56	.053	9	35	.53	64	.13	6	1.87	.02	.07	1	1
131114	2	47	4	115	.3	17	14	435	3.79	5	5	ND	1	39	.5	2	3	93	.49	.115	6	34	.46	98	.12	6	1.86	.02	.09	1	3
131115	1	56	2	95	.1	22	16	618	3.83	15	5	ND	1	38	.4	2	2	92	.42	.222	5	36	.59	111	.11	6	2.38	.02	.08	1	20
131116	1	61	5	102	.1	17	13	298	3.68	21	5	ND	1	45	.2	2	2	88	.51	.217	7	38	.50	69	.11	5	1.80	.02	.07	1	7
131117	2	60	8	122	.1	12	16	612	4.06	18	5	ND	1	46	.2	2	2	106	.62	.089	8	40	.43	88	.14	10	1.73	.02	.12	1	7
STANDARD C/AU-S	19	56	38	127	7.0	69	34	1078	3.88	37	19	7	39	52	18.5	17	17	55	.47	.090	38	57	.87	174	.08	37	1.83	.06	.15	11	47
STANDARD C	19	56	37	134	7.2	73	34	1067	4.03	37	17	6	38	52	18.5	16	19	56	.49	.095	39	59	.89	180	.09	36	1.91	.06	.15	13	-

ACME ANALYTICAL

BP Resources Canada Ltd. PROJECT LOC-10161 FILE # 91-1480

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
131118	1	70	8	71	.1	19	11	341	3.19	18	5	ND	1	59	.2	5	4	77	.62	.115	9	36	.60	95	.11	4	1.69	.02	.06	1	99
131119	1	69	11	62	.1	16	11	370	2.74	14	5	ND	1	67	.6	3	3	70	.66	.091	10	32	.61	99	.10	2	1.70	.02	.06	1	9
131120	1	89	9	48	.1	19	12	398	3.22	23	5	ND	2	81	.2	2	2	84	.67	.124	10	35	.58	128	.09	2	1.57	.03	.06	1	8
131121	1	45	8	86	.1	21	13	335	3.88	23	5	ND	2	43	.4	3	2	90	.41	.119	7	36	.56	104	.10	3	2.04	.02	.06	1	5
131122	1	57	17	62	.1	22	13	377	3.48	38	5	ND	2	54	.3	2	4	87	.48	.083	7	36	.63	80	.10	2	1.61	.02	.08	1	8
131123	1	70	4	62	.1	23	15	361	3.81	28	5	ND	2	46	.2	2	3	97	.48	.083	6	41	.57	73	.11	2	1.73	.02	.09	1	13
131124	1	70	10	64	.1	20	13	321	3.62	28	5	ND	2	50	.4	2	6	91	.52	.094	8	39	.63	75	.11	2	1.62	.02	.07	1	6
131125	1	104	2	61	.1	31	15	327	3.40	13	5	ND	1	65	.4	2	5	78	.68	.064	8	40	.72	87	.12	2	1.87	.02	.10	1	1
131126	1	65	8	99	.1	27	15	292	3.62	15	5	ND	2	37	.4	4	6	79	.39	.153	7	44	.59	90	.09	4	2.11	.02	.07	1	9
131127	1	50	6	59	.1	31	13	265	3.79	14	5	ND	2	43	.4	2	2	78	.40	.202	8	44	.59	103	.09	2	2.03	.02	.05	1	6
28	1	71	2	50	.1	25	10	356	3.10	14	5	ND	1	57	.2	2	4	75	.60	.083	9	40	.65	95	.11	3	1.55	.02	.06	1	2
1[illegible]129	1	60	2	39	.2	26	12	216	3.05	13	5	ND	2	40	.2	5	4	73	.35	.074	6	39	.51	75	.10	7	1.46	.02	.04	1	10
131130	2	52	7	104	.2	15	11	402	5.33	13	5	ND	7	24	.3	2	5	142	.30	.247	6	66	.39	57	.09	2	1.91	.01	.05	2	7
131132	1	39	2	38	.2	20	9	210	2.53	10	5	ND	1	47	.4	4	6	58	.50	.063	8	32	.47	112	.09	4	1.57	.02	.04	1	10
131133	1	39	2	31	.1	21	8	233	2.36	9	5	ND	1	47	.2	2	2	56	.43	.092	9	34	.41	92	.08	2	1.15	.01	.03	1	7
131134	1	33	7	63	.1	23	12	268	3.38	12	8	ND	1	38	.2	2	3	72	.30	.120	7	40	.54	122	.09	2	1.98	.02	.05	1	2
RE 131129	1	64	2	43	.1	29	12	231	3.14	10	5	ND	1	43	.2	2	2	77	.37	.081	7	42	.54	84	.10	2	1.57	.01	.04	1	3
131135	1	40	3	73	.1	35	13	325	3.03	9	5	ND	1	42	.3	2	3	61	.35	.089	9	47	.67	123	.10	2	1.99	.02	.05	1	3
131136	2	58	7	132	.3	30	16	638	3.29	7	5	ND	1	45	.2	2	5	70	.37	.063	7	38	.54	116	.08	2	1.86	.02	.06	1	4
131137	2	67	16	432	.4	23	19	773	5.11	19	5	ND	1	67	1.0	3	5	103	.46	.287	7	42	.75	218	.08	3	2.31	.02	.10	1	11
131138	2	36	9	456	.4	24	17	450	4.64	22	5	ND	1	55	.9	2	5	101	.62	.089	5	44	.68	143	.09	2	1.75	.01	.08	1	2
131141	2	34	5	99	.1	27	13	307	3.27	7	5	ND	1	33	.2	2	2	72	.33	.074	6	39	.52	91	.10	2	1.89	.02	.05	1	2
131142	1	32	6	61	.1	18	12	298	3.55	10	5	ND	1	30	.2	2	5	80	.31	.155	5	35	.42	92	.07	2	1.60	.01	.04	1	2
131143	3	46	5	113	.2	19	14	732	3.49	11	5	ND	1	50	.3	3	2	81	.59	.053	7	37	.63	109	.11	2	1.62	.02	.07	1	7
131144	2	82	12	153	.2	19	19	1746	4.54	17	5	ND	1	56	.8	2	9	98	.44	.391	6	42	.66	241	.09	2	2.02	.02	.09	1	63
131145	1	84	4	130	.2	23	17	732	3.99	14	5	ND	1	46	.8	3	3	103	.50	.074	5	36	.66	104	.11	2	1.72	.01	.11	2	200
131146	2	66	5	117	.4	33	17	429	4.23	17	5	ND	2	36	.2	5	5	93	.47	.155	7	40	.95	101	.11	5	2.34	.02	.08	1	13
131147	2	43	4	107	.5	21	15	425	4.76	10	5	ND	2	31	.5	2	2	93	.38	.301	7	36	.60	101	.09	4	2.16	.02	.07	1	4
131148	2	41	5	50	.1	19	11	220	3.32	9	7	ND	3	34	.2	2	2	75	.42	.128	6	33	.46	59	.09	2	1.40	.01	.05	1	6
49	2	18	2	69	.1	15	13	225	4.53	8	5	ND	1	28	.7	2	2	99	.27	.244	6	41	.29	58	.08	2	1.91	.01	.06	1	12
131150	1	42	3	35	.2	20	10	179	3.44	8	5	ND	2	33	.2	3	2	93	.30	.062	6	40	.36	54	.08	2	1.07	.01	.04	2	3
131151	1	32	3	44	.1	25	10	281	2.82	6	5	ND	1	31	.2	2	3	66	.32	.117	8	40	.42	78	.07	5	1.16	.01	.05	1	10
131152	2	72	3	78	.2	27	17	319	4.91	18	5	ND	1	51	.9	5	3	127	.47	.095	4	43	.78	125	.11	2	2.73	.02	.07	1	14
131153	2	33	2	57	.3	28	14	348	3.48	9	5	ND	2	40	.2	4	2	84	.47	.047	8	47	.63	99	.09	2	1.20	.02	.06	1	38
131154	1	34	2	119	.2	20	15	851	3.75	6	5	ND	1	41	.2	2	2	82	.51	.170	6	30	.83	109	.10	3	2.03	.03	.09	1	11
131155	1	47	2	103	.1	47	19	391	4.75	11	5	ND	1	29	.2	2	3	98	.26	.148	8	66	1.00	165	.07	2	2.91	.02	.09	1	4
131156	1	33	2	171	.5	24	15	373	5.33	13	5	ND	1	36	.8	3	5	122	.29	.213	6	47	.64	124	.08	2	2.34	.01	.08	1	4
STANDARD C/AU-S	20	62	42	131	7.3	75	32	1102	4.00	43	18	7	39	53	18.8	18	21	57	.47	.095	41	59	.88	182	.08	34	1.92	.07	.14	11	47
STANDARD C	19	61	37	130	7.2	70	33	1050	3.97	36	17	6	38	52	18.4	14	20	55	.48	.090	39	58	.88	179	.09	33	1.91	.06	.15	11	-

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
131157	1	70	6	97	.6	32	17	261	6.97	26	5	ND	2	43	.2	2	4	164	.40	.181	7	60	.80	157	.12	3	3.26	.02	.11	1	27
131158	1	44	9	71	.3	25	15	371	5.48	17	5	ND	3	58	.2	2	6	129	.44	.174	6	50	.58	186	.08	3	1.96	.01	.12	1	9
131159	1	93	21	95	.5	26	22	369	6.71	58	5	ND	3	48	.2	2	2	124	.41	.198	4	43	.84	219	.07	2	3.55	.02	.10	1	360
131160	1	76	2	203	.4	23	17	695	5.83	28	5	ND	3	42	.2	3	5	108	.42	.321	8	40	.75	168	.08	3	3.47	.02	.10	1	11
131161	1	74	6	126	.5	32	19	573	4.74	30	5	ND	3	50	.2	3	3	90	.48	.194	10	48	.89	162	.12	5	2.68	.02	.12	1	12
131162	1	57	2	83	.3	22	14	286	5.29	11	5	ND	1	47	.5	2	4	130	.43	.087	6	41	.70	129	.11	2	2.34	.02	.07	3	1030
131163	1	56	2	101	.4	19	14	317	5.80	22	5	ND	1	41	.3	2	2	126	.38	.164	5	38	.69	111	.13	2	2.27	.02	.08	2	13
131164	1	48	7	101	.7	18	13	304	5.12	10	5	ND	2	42	.4	6	2	122	.39	.210	7	46	.51	107	.11	5	1.83	.02	.08	3	15

ACME ANA ICAL LABORATORIES LTD. 852 E. HASTINGS ST. V OUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(253-1716

GEOCHEMICAL ANALY S CERTIFICATE

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700 - 890 W. Pender St., Vancouver BC V6B 4W3

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
130266	2	245	16	396	.4	42	22	601	5.28	30	5	ND	2	68	.6	2	2	135	.81	.080	7	66	1.01	126	.19	5	2.40	.05	.13	1	4
130267	1	23	3	59	.2	21	7	239	2.64	4	5	ND	1	36	.3	2	2	66	.30	.113	7	40	.37	65	.09	2	1.67	.03	.05	1	2
130268	1	108	11	200	.6	24	17	371	5.39	18	5	ND	2	67	.3	2	2	124	.35	.157	7	47	.72	214	.11	4	2.98	.03	.08	1	1
130269	1	107	2	233	.8	25	15	339	5.48	21	5	ND	2	56	.6	2	2	121	.38	.169	8	44	.68	171	.11	2	2.95	.02	.07	1	44
130270	1	31	2	66	.3	26	10	226	2.99	7	5	ND	1	34	.2	2	2	69	.29	.135	8	42	.46	88	.08	4	2.00	.02	.05	1	4
130271	1	67	2	80	.3	24	15	563	4.22	10	5	ND	3	73	.2	2	2	107	.65	.139	8	44	.88	123	.12	4	2.30	.04	.14	1	3
130272	1	45	9	171	.4	21	14	378	4.82	9	5	ND	4	41	.3	2	2	113	.32	.199	9	45	.59	115	.10	3	3.37	.02	.07	1	3
130273	1	66	8	102	.3	21	14	416	4.60	11	5	ND	3	56	.2	3	2	112	.59	.150	7	49	.76	110	.13	5	2.22	.04	.11	1	1
130274	1	32	9	58	.2	21	10	369	3.82	6	7	ND	2	38	.2	2	3	106	.35	.129	7	44	.39	86	.08	4	1.80	.02	.05	1	2
130275	1	34	7	32	.2	23	10	217	3.45	10	5	ND	2	43	.2	2	2	95	.34	.062	7	41	.43	116	.09	2	1.62	.02	.06	1	2
130276	1	43	6	94	.3	28	16	580	6.18	12	5	ND	1	65	.4	2	2	166	.41	.278	8	57	.63	178	.10	2	3.08	.02	.09	1	4
130277	2	35	4	136	.3	35	17	618	5.49	13	5	ND	2	45	.2	2	2	129	.39	.287	8	65	.90	200	.10	2	3.92	.03	.11	2	1
130278	2	119	8	73	.3	33	24	483	7.50	11	5	ND	1	102	.2	5	2	178	.68	.109	9	63	1.26	256	.17	2	2.97	.03	.09	1	1
130279	1	55	7	73	.3	27	19	641	6.92	22	5	ND	2	72	.2	2	3	196	.55	.241	8	59	.84	186	.12	2	2.58	.04	.11	1	24
130280	1	56	3	57	.3	27	16	536	5.46	16	5	ND	3	67	.2	2	4	140	.61	.195	8	52	1.04	169	.13	4	2.39	.05	.11	1	11
130281	1	35	4	56	.2	28	13	489	3.95	12	5	ND	2	58	.2	2	2	96	.37	.163	6	41	.65	155	.09	4	2.61	.02	.08	1	13
130282	2	45	10	56	.2	33	14	349	4.19	12	5	ND	2	45	.2	2	2	104	.35	.072	8	51	.60	152	.10	3	2.32	.02	.07	1	2
130283	1	44	10	146	.4	16	9	386	4.40	13	5	ND	1	46	.5	2	2	101	.49	.264	8	39	.48	151	.11	2	2.19	.03	.07	1	6
130284	1	90	10	82	.4	25	13	308	3.78	18	5	ND	1	54	.2	2	3	99	.57	.132	8	39	.61	101	.13	2	2.56	.03	.10	1	4
130285	1	63	6	95	.3	24	11	348	3.96	9	5	ND	2	55	.2	2	2	98	.57	.133	9	41	.58	127	.13	3	2.00	.03	.09	1	1
130286	1	52	5	101	.5	19	10	328	3.76	11	5	ND	2	59	.2	2	2	92	.55	.109	9	40	.55	117	.14	6	2.02	.03	.09	1	2
RE 130296	1	47	5	42	.3	28	12	294	3.50	9	5	ND	1	62	.2	2	3	88	.46	.070	7	46	.63	111	.14	2	2.01	.04	.09	1	2
130287	1	73	8	85	.2	21	11	339	3.53	10	5	ND	2	72	.2	2	2	82	.66	.093	11	38	.65	129	.15	2	2.35	.03	.08	1	3
130288	1	81	7	85	.4	26	15	376	4.25	23	5	ND	1	61	.2	2	2	98	.58	.099	9	45	.83	127	.18	2	2.47	.03	.13	1	2
130289	1	129	10	56	.6	28	16	409	4.48	32	5	ND	2	70	.2	2	2	110	.60	.095	8	43	.92	171	.18	4	3.22	.04	.12	1	1
130290	1	92	9	57	.2	23	13	360	4.10	29	5	ND	2	60	.2	2	2	102	.50	.096	7	45	.75	101	.14	2	2.62	.03	.07	1	1
130291	1	53	7	87	.2	23	13	295	4.02	12	5	ND	1	64	.3	2	2	104	.57	.059	6	42	.58	102	.16	2	2.25	.03	.08	1	2
292	1	106	13	187	.4	21	29	1239	7.23	14	5	ND	1	105	.5	3	2	148	.84	.231	6	34	1.05	99	.17	2	3.77	.02	.12	1	2
293	1	64	3	99	.3	35	17	411	4.39	9	5	ND	1	58	.2	2	2	104	.60	.073	6	47	.67	126	.17	2	2.94	.04	.11	1	1
130294	1	146	6	56	.3	29	12	401	3.87	10	5	ND	1	84	.2	2	2	94	1.02	.058	12	46	.69	127	.15	2	1.88	.06	.15	1	5
130295	1	33	11	75	.1	22	10	225	3.14	8	5	ND	1	39	.2	2	2	71	.30	.092	10	45	.44	85	.13	2	1.98	.02	.06	1	10
130296	1	45	2	40	.2	29	12	275	3.38	9	5	ND	2	60	.3	2	2	85	.45	.069	7	46	.61	106	.15	2	1.93	.04	.08	1	3
130297	1	71	7	95	.4	30	15	332	4.07	16	5	ND	2	48	.2	2	2	96	.38	.089	6	47	.61	117	.12	2	2.68	.03	.09	1	1
130299	1	42	7	61	.1	27	10	419	3.70	9	5	ND	1	68	.3	2	2	81	.62	.076	8	46	.65	105	.11	2	1.66	.03	.08	1	2
130300	1	31	2	61	.1	29	11	290	3.79	10	5	ND	1	44	.4	2	5	82	.38	.142	8	48	.52	120	.12	2	2.52	.03	.07	1	1
130301	1	52	3	49	.2	29	10	298	2.96	10	5	ND	2	64	.2	2	2	71	.51	.090	10	42	.58	128	.12	2	1.87	.03	.07	1	2
STANDARD C/AU-S	19	55	38	127	6.9	70	33	1065	3.92	38	15	7	40	52	18.4	17	17	58	.47	.089	39	60	.85	188	.09	33	1.95	.08	.16	11	46
STANDARD C	18	57	39	129	6.9	69	31	1043	3.88	38	16	8	38	52	18.7	16	19	54	.48	.090	37	57	.87	173	.09	31	1.86	.06	.15	13	-

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: SOIL AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

DATE RECEIVED: JUN 5 1991 DATE REPORT MAILED: June 11/91. SIGNED BY..... .D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
130302	1	51	13	75	.1	25	13	306	3.05	12	5	ND	1	59	.2	2	2	72	.59	.054	8	38	.64	161	.12	2	2.19	.02	.06	1	16
130303	1	34	7	82	.1	25	15	373	3.35	15	5	ND	2	48	.3	3	2	72	.44	.106	8	41	.54	110	.11	10	1.93	.02	.06	1	15
RE 130311	1	28	11	139	.1	26	13	335	4.64	12	5	ND	1	64	.3	2	2	90	.54	.281	8	45	.62	130	.09	6	2.45	.02	.07	1	9
130304	1	40	5	73	.1	31	11	326	3.19	11	5	ND	2	52	.2	4	2	70	.48	.066	9	43	.70	120	.13	3	1.96	.02	.07	1	13
130305	1	47	5	52	.1	30	12	440	3.07	16	5	ND	1	58	.2	2	2	68	.51	.099	8	43	.61	124	.11	2	1.62	.02	.07	1	20
130306	3	56	39	523	.1	13	22	486	7.72	36	5	ND	1	42	1.5	2	3	111	.35	.080	6	25	.53	87	.08	2	2.30	.01	.06	1	17
130308	3	419	23	155	.5	49	27	652	6.05	47	5	ND	2	72	.2	3	2	126	.79	.108	12	62	.96	195	.16	6	3.95	.03	.12	1	17
130309	2	257	14	214	.3	44	24	570	5.34	22	5	ND	1	49	.2	3	2	117	.82	.069	7	56	1.15	183	.19	3	3.37	.03	.12	1	8
130310	2	49	14	162	.7	24	18	376	6.33	23	5	ND	2	44	.6	2	5	140	.45	.176	6	39	.74	115	.13	2	3.03	.03	.09	1	11
130311	1	28	6	134	.1	21	14	324	4.52	14	5	ND	1	62	.2	2	2	88	.53	.266	7	43	.60	122	.09	2	2.31	.02	.07	1	8
130312	1	69	11	58	.1	34	16	543	4.24	18	5	ND	1	61	.2	2	2	91	.67	.063	10	49	.68	154	.09	6	2.08	.03	.06	1	16
130313	1	24	9	42	.1	14	9	260	3.15	11	5	ND	1	40	.2	2	2	76	.40	.075	6	31	.35	82	.09	3	1.23	.01	.04	1	5
130314	1	39	2	61	.1	21	12	246	4.03	11	5	ND	1	42	.2	2	2	93	.40	.214	6	41	.51	88	.09	4	1.72	.02	.06	1	5
130315	1	30	6	30	.1	28	10	227	2.97	12	5	ND	2	41	.2	3	2	73	.41	.072	7	38	.48	115	.10	8	1.50	.02	.04	1	4
130316	1	65	5	70	.1	23	15	485	4.44	14	5	ND	1	47	.2	2	2	93	.61	.187	6	36	.67	103	.10	2	1.88	.02	.08	1	8
130317	1	42	10	65	.1	23	12	265	5.24	10	5	ND	1	38	.2	2	5	143	.51	.169	10	58	.45	73	.11	2	1.43	.02	.08	1	3
130318	1	89	12	73	.2	29	17	436	5.06	16	5	ND	1	44	.2	3	2	123	.50	.149	7	56	.67	102	.13	2	2.29	.02	.10	1	18
130319	1	44	2	86	.1	20	14	263	4.71	13	5	ND	1	37	.3	2	2	111	.33	.187	6	41	.62	108	.10	3	2.26	.01	.07	1	2
130320	1	59	11	95	.1	22	20	779	5.24	12	5	ND	2	53	.2	2	2	125	.74	.293	7	35	1.22	123	.14	3	2.63	.04	.14	1	11
130321	2	68	9	49	.1	24	14	267	4.28	11	5	ND	1	53	.2	2	2	114	.50	.046	5	40	.61	164	.12	3	2.27	.02	.08	1	17
130322	1	41	10	106	.6	22	18	427	5.03	16	5	ND	3	49	.6	11	2	131	.45	.086	6	41	.74	149	.13	8	2.55	.02	.09	1	15
130323	1	60	20	100	.1	26	19	349	5.15	16	5	ND	2	46	.3	2	4	122	.31	.114	8	50	.71	171	.13	2	3.08	.02	.09	1	42
130324	1	26	10	102	.2	17	12	375	3.37	8	5	ND	2	42	.4	3	2	76	.38	.121	9	36	.46	107	.10	4	2.14	.02	.06	1	17
130325	1	49	7	137	.1	29	17	394	5.61	24	5	ND	1	40	.2	2	2	121	.36	.143	7	46	.69	133	.10	7	2.76	.02	.09	1	7
130326	1	83	13	123	.1	36	21	405	6.20	33	5	ND	1	45	.2	2	2	128	.41	.258	5	51	1.04	172	.11	2	3.31	.02	.13	1	3
130327	1	97	8	76	.1	25	17	477	4.94	24	5	ND	1	47	.2	2	2	118	.49	.225	7	45	.95	162	.16	2	2.98	.02	.11	1	6
130328	1	16	5	45	.1	29	8	200	2.38	7	5	ND	2	37	.2	3	2	51	.35	.079	7	43	.49	122	.09	7	1.37	.02	.04	1	14
130329	1	18	7	100	.1	30	12	486	2.87	6	5	ND	1	43	.2	2	2	58	.38	.157	8	48	.52	93	.09	3	1.32	.01	.07	1	10
130330	1	16	5	50	.1	16	9	209	2.91	9	8	ND	1	31	.2	2	2	65	.28	.083	7	36	.36	81	.09	5	1.49	.02	.05	1	24
130331	1	27	3	45	.2	31	11	332	2.88	3	5	ND	2	42	.3	3	2	65	.44	.109	10	42	.58	131	.10	2	1.44	.02	.06	1	3
130332	1	17	6	50	.1	20	9	215	2.95	7	7	ND	1	39	.4	2	2	65	.38	.161	7	37	.43	139	.08	4	1.35	.01	.06	1	6
130333	1	22	2	43	.1	17	9	457	2.59	9	5	ND	1	34	.2	3	2	60	.29	.079	6	35	.35	103	.08	2	1.16	.01	.04	1	17
130334	1	27	6	66	.1	24	13	359	2.94	7	5	ND	1	43	.2	5	2	62	.47	.086	8	39	.45	125	.08	5	1.40	.01	.07	1	12
130335	1	42	19	79	.1	22	17	317	7.00	35	5	ND	1	36	.2	2	6	154	.34	.272	6	47	.60	161	.08	2	3.02	.02	.07	1	13
130336	1	114	14	58	.1	26	19	680	4.45	15	5	ND	1	63	.5	2	2	100	.77	.129	7	32	1.12	98	.15	5	2.36	.05	.12	1	15
STANDARD C/AU-S	18	58	37	129	6.7	65	32	996	3.88	37	16	7	36	52	17.3	14	18	56	.45	.084	37	56	.80	172	.08	36	1.80	.06	.14	11	51
STANDARD C	18	58	36	130	6.9	69	31	1048	3.95	38	20	7	38	52	18.5	15	19	55	.48	.090	38	58	.88	178	.09	33	1.87	.06	.15	13	-

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
130339	2	79	6	68	.2	27	15	335	5.06	30	5	ND	1	53	.3	2	2	141	.45	.046	6	46	.72	132	.15	2	2.17	.02	.10	1	6
130340	1	69	4	197	.4	22	20	1648	3.88	12	5	ND	1	69	.4	2	2	89	.81	.157	8	30	.67	226	.09	2	2.63	.02	.13	1	4
130341	1	32	6	108	.2	18	15	493	4.03	12	5	ND	1	298	.5	2	2	102	.59	.049	7	33	.42	267	.16	2	2.09	.02	.08	2	3
130342	1	37	5	78	.2	26	13	417	4.02	9	5	ND	2	96	.8	2	2	96	.57	.140	7	40	.62	150	.10	2	2.15	.02	.09	1	2
130343	2	119	5	80	.4	35	15	627	4.16	12	5	ND	2	81	.3	2	2	101	.75	.056	19	50	.76	281	.11	2	3.73	.03	.11	1	100
130344	1	61	8	65	.1	31	13	302	4.42	10	5	ND	2	54	.4	2	2	104	.45	.107	6	45	.68	127	.13	2	3.26	.02	.08	1	5
130345	1	37	10	58	.2	23	12	379	3.62	9	5	ND	1	51	.2	2	2	93	.48	.118	5	41	.50	99	.11	2	1.73	.02	.08	1	1
130346	1	29	5	70	.1	22	13	538	4.06	11	5	ND	1	51	.5	2	2	101	.54	.115	8	40	.52	109	.11	2	1.72	.02	.08	1	6
130347	1	49	5	65	.2	25	13	423	3.82	12	5	ND	1	58	.2	2	2	93	.61	.118	7	38	.61	120	.12	4	1.74	.02	.09	1	2
130348	10	18	14	235	.3	29	8	153	3.03	39	5	ND	1	12	2.4	3	2	61	.15	.050	11	17	.10	93	.01	3	.95	.01	.13	1	3
130349	2	63	12	76	.3	37	14	329	4.02	21	6	ND	2	51	.9	2	2	90	.42	.072	7	44	.57	128	.12	2	2.00	.02	.07	2	30
130350	3	76	17	176	.4	22	18	599	5.78	57	5	ND	1	60	.8	2	2	118	.38	.250	6	41	.69	245	.07	2	2.79	.02	.09	1	5
130351	6	131	4	176	.2	26	23	619	11.61	26	5	ND	2	30	1.7	2	2	160	.51	.254	9	34	.36	103	.15	2	3.47	.02	.05	1	140
130352	11	67	21	120	.7	14	22	542	7.36	239	5	ND	1	92	.4	6	2	99	.19	.057	3	31	.53	95	.01	2	3.79	.01	.14	2	74
130353	2	77	2	65	.2	38	13	374	3.22	14	5	ND	1	61	.2	2	2	69	.56	.028	10	49	.67	185	.13	3	2.16	.03	.06	1	5
130354	5	56	27	373	1.1	34	28	662	6.95	24	5	ND	2	30	1.2	2	2	134	.34	.062	8	53	.75	116	.08	2	4.35	.01	.06	2	4
130355	1	34	6	124	.1	31	13	435	3.52	13	5	ND	1	54	.2	2	2	77	.43	.094	8	41	.53	115	.11	7	1.94	.02	.08	1	3
130356	1	36	2	52	.1	27	8	273	2.60	13	5	ND	1	63	.2	2	2	61	.54	.038	9	38	.52	115	.13	4	1.74	.03	.05	1	6
130357	2	45	23	168	.1	34	11	296	3.27	16	5	ND	1	47	.6	2	2	74	.36	.061	9	44	.56	78	.14	6	2.12	.02	.06	1	18
130358	1	45	5	97	.1	34	12	360	3.24	17	5	ND	1	46	.3	2	2	71	.42	.110	9	43	.58	98	.13	4	2.18	.02	.07	1	5
130359	1	63	2	60	.1	31	12	256	2.65	10	5	ND	1	58	.2	3	2	63	.57	.072	10	40	.64	129	.15	4	2.12	.03	.06	3	1
130360	2	100	18	109	.1	21	13	290	4.56	15	5	ND	2	58	.4	2	2	106	.61	.095	10	45	.53	81	.14	2	2.15	.02	.08	1	6
130361	1	60	4	108	.2	16	11	325	3.16	8	5	ND	1	68	.2	2	2	81	.70	.089	9	38	.59	79	.15	3	1.48	.03	.07	1	7
130362	1	24	22	227	.1	13	10	310	3.42	3	6	ND	1	45	.3	2	2	80	.51	.165	7	37	.37	94	.11	2	1.52	.02	.07	1	5
130363	1	40	16	215	.1	16	12	342	3.82	10	5	ND	1	45	.8	2	2	89	.51	.286	7	38	.48	118	.12	2	1.68	.02	.09	1	10
130364	1	105	6	111	.3	17	12	433	3.21	11	5	ND	1	62	.3	2	2	88	.67	.072	8	41	.61	93	.16	6	1.67	.03	.09	1	4
130365	1	59	5	62	.1	17	10	380	2.91	10	5	ND	1	70	.2	2	2	79	.71	.105	10	35	.56	87	.14	2	1.36	.03	.08	1	8
130366	1	61	8	36	.2	17	10	279	3.39	10	5	ND	1	49	.2	2	2	97	.57	.092	11	46	.38	56	.10	4	1.09	.02	.06	2	5
67	1	30	5	124	.2	20	12	382	4.01	12	5	ND	1	43	.7	2	2	88	.39	.139	8	36	.40	75	.14	5	1.82	.02	.06	2	6
130368	5	82	7	165	.2	13	19	346	13.71	22	5	ND	1	68	1.5	2	2	127	.41	.281	6	41	.32	142	.11	2	2.36	.03	.09	1	10
130369	2	408	39	459	.8	29	20	540	6.10	63	5	ND	2	101	1.1	4	2	117	.51	.297	9	54	1.05	231	.13	7	3.88	.01	.10	2	6
130370	1	63	8	117	.1	20	12	328	3.41	13	5	ND	1	69	.2	2	2	82	.70	.161	10	36	.67	135	.14	3	1.97	.03	.09	1	6
RE 130366	1	62	9	39	.1	16	9	284	3.47	9	5	ND	1	51	.3	2	2	98	.58	.092	11	45	.40	56	.10	3	1.12	.02	.07	1	2
130371	1	225	18	315	.6	23	20	622	6.38	18	5	ND	1	231	.9	2	2	173	.82	.087	6	68	.94	276	.17	2	2.53	.03	.16	1	100
130372	1	96	8	43	.2	26	14	391	3.45	11	5	ND	2	93	.2	2	2	87	.76	.116	11	38	.69	116	.17	2	1.85	.04	.08	2	9
130373	1	61	10	67	.1	24	15	294	4.07	11	5	ND	1	55	.6	3	2	95	.51	.103	6	37	.60	96	.18	4	2.21	.02	.09	1	24
STANDARD C/AU-S	18	56	35	128	6.6	69	32	1013	3.89	39	20	8	38	52	18.4	16	18	57	.47	.090	38	58	.84	181	.09	32	1.92	.06	.15	11	45
STANDARD C	18	56	39	129	7.0	70	33	1042	3.87	37	20	7	37	52	18.5	15	18	54	.49	.090	37	59	.87	174	.09	34	1.86	.06	.15	11	-

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
130374	1	100	10	76	.2	23	15	299	3.98	14	5	ND	2	47	.2	2	4	92	.44	.112	7	41	.57	108	.13	3	2.70	.03	.07	1	2
130375	2	452	17	307	.6	27	21	819	5.73	31	5	ND	2	197	.2	2	2	133	.48	.175	7	51	1.07	331	.10	3	3.22	.02	.10	1	11
130376	2	264	24	179	.6	19	17	430	7.82	82	5	ND	2	75	.2	2	6	177	.37	.250	5	55	.98	196	.12	4	2.93	.02	.07	1	5
130377	1	207	11	64	.5	26	30	814	6.11	101	5	ND	1	100	.2	16	2	154	.96	.112	9	47	.91	135	.08	6	2.81	.02	.10	1	3
130378	1	67	10	70	.1	19	9	256	2.98	9	5	ND	1	53	.2	2	2	78	.61	.062	8	36	.51	97	.11	4	1.59	.04	.08	1	4
130379	1	60	6	56	.2	17	8	372	2.73	6	5	ND	2	46	.2	2	2	70	.53	.046	8	37	.45	86	.11	2	1.41	.03	.07	1	3
130380	1	107	5	65	.3	20	12	408	3.81	7	5	ND	2	64	.2	2	2	103	.66	.084	8	45	.69	112	.14	4	1.63	.04	.11	1	2
130381	1	88	9	83	.4	22	10	264	2.89	11	5	ND	2	42	.2	5	2	76	.42	.093	9	41	.47	82	.11	2	1.41	.03	.09	1	11
130382	1	54	11	129	.4	14	10	434	4.42	12	7	ND	2	33	.2	2	2	101	.30	.217	6	42	.33	76	.08	7	1.89	.02	.07	1	3
130383	2	177	7	116	.3	18	13	415	5.68	12	5	ND	3	64	.2	2	2	133	.44	.377	8	57	.64	136	.11	4	2.68	.02	.08	1	34
[illegible]84	1	78	8	188	.5	21	14	311	5.71	5	5	ND	3	45	.2	2	2	117	.36	.467	8	54	.61	157	.11	3	2.57	.02	.09	1	5
130385	1	124	12	175	.3	24	13	428	3.38	9	5	ND	1	59	.2	2	2	84	.51	.045	10	46	.79	105	.17	3	1.91	.03	.10	1	4
130386	2	445	14	183	.5	39	39	1155	9.22	52	5	ND	1	127	.2	3	2	203	.87	.401	8	99	1.29	370	.07	6	3.03	.02	.20	1	1
130387	1	103	9	44	.4	24	13	341	3.54	20	5	ND	1	85	.2	2	2	83	.87	.103	9	35	.69	162	.12	2	2.03	.03	.10	1	2
130388	1	44	7	70	.3	21	11	341	3.52	8	5	ND	1	62	.2	2	3	79	.52	.149	8	38	.61	124	.13	5	1.92	.04	.09	1	7
130389	1	40	10	154	.4	20	14	386	3.88	6	5	ND	2	57	.2	2	2	83	.55	.263	9	38	.65	128	.13	4	2.01	.03	.12	1	4
130390	1	37	2	46	.5	17	12	338	3.97	11	7	ND	5	60	.2	2	2	97	.56	.069	8	40	.54	91	.14	6	1.83	.03	.09	1	1
130391	1	66	7	57	.3	25	15	328	3.81	12	5	ND	2	65	.2	2	2	87	.54	.119	6	46	.63	105	.13	5	2.24	.03	.09	1	1
130392	1	26	8	52	.4	19	12	264	3.44	2	7	ND	1	53	.2	2	2	77	.52	.132	6	40	.51	95	.11	4	1.78	.03	.09	1	32
RE 130388	1	42	8	70	.2	22	11	337	3.51	11	5	ND	2	61	.2	2	4	79	.53	.149	8	40	.62	121	.13	4	1.93	.05	.10	1	7
130393	1	48	2	78	.1	26	13	389	3.78	8	5	ND	1	52	.2	2	2	83	.52	.202	7	42	.65	106	.12	2	2.20	.03	.11	1	2
130394	2	72	8	110	.2	38	22	492	3.70	13	5	ND	1	465	.2	3	2	85	.74	.055	5	24	.53	559	.08	3	2.69	.03	.18	1	4
130395	9	235	3	237	.4	35	22	458	17.64	23	5	ND	2	58	.7	10	6	194	.46	.199	6	33	.47	94	.12	3	3.57	.02	.05	1	6
130396	1	69	9	115	.3	29	14	349	4.18	14	5	ND	1	68	.2	3	2	101	.50	.040	7	46	.73	109	.15	4	2.45	.03	.10	1	6
130397	1	28	7	35	.1	27	11	231	3.97	10	5	ND	1	44	.2	3	2	94	.34	.099	8	44	.49	112	.14	2	2.14	.02	.06	1	4
130398	1	318	26	203	.8	27	21	817	5.53	27	5	ND	3	142	.2	6	2	114	.73	.277	8	49	1.30	259	.13	4	3.24	.03	.15	1	9
130399	1	256	4	345	.4	27	18	518	5.97	24	5	ND	2	120	.2	2	2	125	.33	.330	8	57	.88	230	.12	4	4.13	.02	.10	1	6
130400	2	612	13	294	.8	28	21	631	6.69	37	5	ND	1	207	.2	5	2	142	.61	.342	8	58	1.14	346	.14	2	3.74	.02	.16	1	8
01	1	191	13	351	.5	19	14	389	5.20	28	5	ND	1	65	.4	2	2	116	.40	.152	7	52	.84	109	.15	2	2.45	.02	.08	2	5
1[illegible]402	2	76	18	271	.7	19	15	508	6.30	22	5	ND	1	64	.2	2	2	149	.45	.197	5	57	.70	150	.12	2	2.77	.02	.11	1	8
130403	1	64	9	48	.3	27	11	259	3.48	8	5	ND	1	57	.2	2	2	76	.42	.059	9	44	.59	123	.14	2	2.18	.03	.07	1	1
130404	1	26	11	92	.1	23	13	326	4.68	5	5	ND	2	42	.2	2	2	105	.36	.236	9	53	.55	100	.10	2	2.16	.02	.07	1	2
130405	1	75	10	49	.2	26	12	459	3.60	11	5	ND	1	57	.2	2	2	93	.52	.091	9	47	.60	101	.13	2	1.60	.03	.11	1	1
130406	1	61	9	61	.1	25	12	478	3.55	9	5	ND	1	67	.2	3	2	84	.78	.103	9	48	.66	123	.11	3	1.84	.04	.09	1	6
130407	1	48	6	50	.1	32	12	472	3.78	7	5	ND	1	57	.2	2	2	93	.66	.078	10	46	.72	150	.13	2	2.03	.04	.12	1	40
130408	1	23	8	30	.1	23	9	232	3.28	7	5	ND	1	47	.2	2	2	82	.48	.097	8	43	.46	70	.11	2	1.67	.03	.07	1	5
130409	1	44	13	244	.3	20	16	502	5.31	11	5	ND	1	106	.5	2	2	125	.52	.102	8	35	.67	180	.17	4	2.27	.03	.09	1	3
STANDARD C/AU-S	17	57	42	126	6.9	64	29	933	3.92	37	20	7	37	51	17.1	15	18	56	.46	.085	35	55	.75	174	.08	31	1.73	.07	.15	11	46
STANDARD C	18	58	41	130	6.9	68	32	1046	3.95	38	15	6	38	52	18.4	16	19	55	.48	.090	38	58	.88	176	.09	32	1.87	.06	.15	12	-

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
130410	2	107	2	75	.4	26	14	312	3.52	6	5	ND	2	113	.7	2	2	92	.86	.046	9	40	.65	211	.12	4	2.92	.04	.08	1	5
130411	1	30	2	137	.1	28	12	308	3.93	4	5	ND	1	49	.2	2	2	92	.51	.093	7	45	.62	127	.12	2	2.22	.04	.10	1	12
130412	2	71	2	129	.2	28	16	383	4.12	4	5	ND	2	48	.2	3	2	88	.52	.063	10	40	.64	155	.12	6	3.11	.03	.12	1	4
130413	1	17	2	61	.2	15	11	359	2.83	2	5	ND	1	42	.2	2	2	80	.43	.033	6	34	.32	76	.11	4	1.25	.03	.08	1	16
130414	5	49	4	406	.1	40	17	730	4.29	16	5	ND	1	37	2.1	2	2	103	.38	.077	9	50	.78	250	.04	4	2.21	.02	.15	1	2
130415	1	78	5	123	.1	19	16	375	5.33	13	5	ND	1	39	.2	2	6	127	.39	.150	6	39	.77	121	.11	8	2.45	.03	.08	1	5
130416	3	75	2	66	.1	24	21	358	4.60	22	5	ND	2	58	.2	2	2	108	.59	.065	7	37	.75	175	.15	5	2.45	.03	.08	1	7
130417	1	27	2	64	.2	22	11	254	3.38	10	5	ND	2	43	.2	2	2	77	.40	.103	8	42	.49	120	.11	4	1.74	.03	.06	1	7
130418	1	84	2	76	.1	33	14	568	3.50	7	5	ND	1	61	.2	2	2	77	.65	.103	11	44	.65	166	.08	2	2.10	.02	.10	1	5
130419	1	17	2	38	.3	12	8	208	2.80	5	5	ND	1	42	.2	2	2	78	.37	.057	7	33	.36	95	.11	2	1.20	.03	.05	1	8
130420	1	31	2	27	.2	17	9	220	2.86	7	5	ND	1	49	.2	2	2	77	.50	.117	8	36	.38	110	.09	6	1.03	.02	.05	1	24
130421	1	15	2	69	.1	18	11	324	3.05	2	5	ND	2	45	.2	2	2	77	.40	.140	8	39	.39	130	.09	2	1.55	.02	.05	1	8
130422	1	31	2	42	.3	17	8	237	2.11	2	5	ND	2	52	.3	2	2	58	.47	.053	9	31	.45	137	.11	4	1.39	.03	.06	1	7
130423	1	41	3	40	.1	32	12	284	3.06	5	5	ND	1	47	.2	2	2	76	.46	.082	9	44	.59	175	.11	3	1.56	.03	.07	1	4
130424	1	12	2	119	.2	18	13	448	3.46	2	5	ND	3	40	.2	2	2	83	.41	.149	8	42	.42	129	.10	7	1.45	.03	.08	1	1
130425	1	36	2	71	.4	10	9	424	2.78	2	5	ND	1	74	.4	2	2	86	.50	.090	9	25	.38	101	.16	2	1.96	.03	.06	1	1
130426	2	83	8	134	.4	35	16	630	4.52	12	5	ND	4	39	.2	7	2	93	.31	.287	8	49	.67	120	.15	7	4.01	.02	.07	1	3
130427	1	76	2	73	.1	46	15	323	4.18	12	5	ND	4	35	.3	2	2	86	.31	.197	9	68	.86	138	.10	8	4.07	.02	.09	1	6
130428	1	36	3	81	.1	31	12	311	3.01	4	5	ND	2	50	.2	2	2	64	.47	.156	9	49	.67	150	.10	6	2.31	.02	.08	1	2
130429	1	48	2	52	.3	33	15	376	3.99	13	5	ND	3	60	.2	5	2	88	.53	.459	7	46	.61	210	.09	7	2.48	.02	.08	1	2
130430	1	8	2	53	.1	11	7	132	2.68	5	5	ND	1	39	.2	2	2	74	.29	.057	5	32	.20	86	.08	6	1.33	.02	.04	1	81
130431	1	20	5	140	.1	17	19	586	4.42	6	5	ND	2	43	.2	2	2	95	.41	.295	8	41	.51	403	.07	3	2.29	.03	.11	1	3
130432	1	15	7	42	.1	13	9	219	3.47	5	5	ND	3	49	.2	2	2	103	.42	.100	7	39	.27	126	.08	8	.94	.02	.05	1	4
130433	1	20	2	36	.3	18	10	206	3.07	8	5	ND	2	57	.2	3	2	82	.65	.079	7	38	.38	108	.08	2	1.19	.02	.05	1	9
130434	1	85	2	68	.3	33	14	1322	3.49	7	5	ND	3	67	.2	2	2	75	.80	.068	18	52	.60	379	.09	3	2.73	.02	.10	1	5
130435	1	86	9	64	.4	25	13	532	3.11	5	5	ND	3	51	.2	6	3	76	.64	.053	11	42	.85	268	.12	5	2.62	.03	.08	1	3
130436	1	101	3	80	.1	41	20	1126	4.00	5	5	ND	2	50	.2	2	2	86	.49	.103	9	55	.66	386	.09	4	4.02	.02	.13	1	4
130437	1	29	2	52	.1	23	12	230	3.41	7	5	ND	2	39	.2	2	2	78	.34	.102	7	39	.46	141	.08	4	2.04	.02	.06	1	1
438	1	30	2	31	.2	17	9	226	2.30	9	5	ND	3	51	.2	2	2	61	.46	.062	9	33	.47	111	.11	2	1.38	.03	.06	1	3
130439	1	36	9	53	.1	24	11	283	3.14	7	5	ND	2	52	.2	2	2	80	.49	.110	8	38	.51	124	.11	6	1.69	.03	.08	1	2
130440	1	29	2	40	.1	23	11	266	3.47	7	5	ND	3	48	.2	3	2	80	.43	.171	8	39	.49	108	.10	5	1.73	.03	.06	1	6
130441	1	28	5	42	.5	16	11	362	3.18	7	5	ND	7	47	.2	4	2	80	.44	.095	8	38	.43	106	.10	9	1.33	.03	.06	1	4
RE 130438	1	30	6	30	.2	18	9	214	2.20	8	5	ND	3	46	.3	2	3	58	.42	.056	8	31	.45	108	.10	5	1.30	.03	.06	1	3
130442	1	23	2	46	.1	23	11	245	3.44	11	5	ND	1	41	.5	2	2	79	.40	.128	7	37	.48	127	.09	7	1.75	.02	.05	1	7
130443	1	21	9	50	.2	16	9	198	3.53	7	5	ND	2	39	.2	2	2	87	.37	.100	6	37	.36	102	.09	9	1.56	.02	.06	1	35
130444	1	16	2	48	.2	17	10	343	3.93	7	5	ND	3	39	.3	3	2	95	.42	.230	7	40	.42	107	.08	9	1.31	.02	.06	1	5
130445	1	73	4	31	.1	20	10	388	2.59	9	5	ND	2	44	.2	2	2	70	.53	.091	11	35	.44	134	.09	4	1.03	.03	.07	1	6
STANDARD C/AU-S	20	59	40	131	7.0	73	32	1079	4.04	38	17	8	39	53	18.6	17	19	60	.49	.092	40	60	.91	180	.10	39	1.99	.07	.16	13	45
STANDARD C	19	63	43	134	7.2	73	32	1062	4.01	40	19	7	40	52	18.6	14	22	57	.49	.089	39	59	.90	176	.09	33	1.89	.06	.15	11	-

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
130446	2	32	5	69	.1	17	13	256	6.32	19	5	ND	2	28	.2	2	2	163	.22	.200	5	49	.42	96	.09	2	2.69	.02	.05	1	31
130447	1	34	2	113	.1	23	14	375	3.72	9	5	ND	2	64	1.2	2	2	101	.42	.044	5	34	.47	82	.12	2	1.84	.02	.06	1	5
130448	1	18	2	93	.2	14	12	309	3.26	2	5	ND	1	50	.2	2	2	90	.34	.030	5	31	.30	80	.09	2	1.26	.02	.05	1	1
130449	1	42	2	37	.3	22	11	257	3.08	8	5	ND	3	36	.2	2	2	76	.33	.083	6	35	.49	100	.08	2	1.64	.02	.06	1	8
130450	1	62	4	48	.1	32	13	241	3.82	7	5	ND	2	37	.2	2	6	90	.35	.095	6	41	.54	113	.09	2	2.47	.02	.07	1	13
130451	1	45	2	42	.4	24	10	356	3.03	6	5	ND	3	51	.2	2	3	76	.60	.022	10	41	.53	147	.11	3	1.60	.04	.07	1	8
RE 130455	1	13	2	83	.1	17	10	335	2.68	4	5	ND	1	43	.2	2	2	56	.39	.178	7	38	.43	126	.07	3	1.44	.02	.05	1	2
130452	1	37	2	35	.3	30	11	283	2.89	7	5	ND	3	39	.2	2	2	69	.44	.098	10	42	.56	106	.09	2	1.48	.03	.07	1	6
130453	3	33	2	115	.2	14	14	288	4.66	6	5	ND	1	73	.2	2	2	119	.28	.071	7	34	.48	154	.05	2	1.77	.02	.06	1	5
130454	1	47	4	69	.3	21	13	417	3.45	11	5	ND	1	66	.3	2	2	88	.46	.064	6	33	.58	100	.11	2	1.62	.03	.09	1	3
130455	1	11	2	80	.3	18	10	332	2.61	5	5	ND	2	43	.2	2	2	55	.38	.173	8	36	.41	119	.08	2	1.42	.02	.05	1	5
130456	1	17	4	74	.3	16	10	300	2.70	4	7	ND	2	37	.3	2	4	58	.31	.132	7	34	.36	86	.08	4	1.37	.02	.06	1	4
130457	1	45	2	74	.4	28	12	281	3.47	4	5	ND	2	47	.2	2	4	76	.44	.177	8	38	.57	121	.09	2	1.75	.02	.07	1	5
130458	1	86	2	75	.3	38	16	693	3.80	10	5	ND	3	78	.2	2	2	80	.68	.108	12	47	.80	158	.11	4	1.78	.04	.10	1	4
130459	1	22	2	86	.1	17	14	656	3.67	7	5	ND	1	47	.2	2	2	87	.32	.124	6	35	.40	115	.09	2	1.42	.02	.07	1	4
130460	1	67	4	78	.4	27	18	389	4.62	16	5	ND	3	94	.2	2	2	102	.51	.083	8	38	.64	125	.10	3	2.60	.02	.07	1	2
130461	1	44	3	70	.3	23	18	777	4.40	12	5	ND	2	113	1.0	2	4	106	.67	.187	6	41	1.16	186	.09	5	2.31	.04	.11	1	3
130462	1	59	8	222	.5	24	17	533	5.46	11	5	ND	3	139	.4	4	4	120	.54	.398	6	49	.91	272	.05	2	3.19	.02	.09	1	12
130463	1	336	7	208	.1	42	22	1103	5.47	14	5	ND	3	60	.5	2	5	122	.92	.155	13	58	1.06	182	.14	2	3.12	.02	.19	1	5
130464	2	286	7	359	.7	52	25	1829	4.65	23	5	ND	3	65	1.5	5	3	106	1.02	.100	16	47	.80	129	.12	3	2.99	.04	.08	1	4
130465	3	75	10	843	.1	55	17	1837	3.96	8	5	ND	2	59	1.3	2	2	94	.83	.059	6	48	.57	88	.10	2	1.83	.03	.06	1	1
130466	2	83	9	232	.4	44	19	357	4.63	15	5	ND	3	53	.4	2	4	113	.37	.093	5	43	.64	116	.11	3	2.57	.02	.06	1	4
130467	2	81	5	157	.2	40	30	486	6.46	22	5	ND	3	36	.2	5	2	103	.38	.130	6	40	.49	65	.09	4	2.19	.02	.08	1	3
130468	1	43	2	129	.2	23	15	356	3.53	5	5	ND	2	43	.3	2	2	74	.45	.124	6	35	.53	79	.12	3	1.70	.02	.08	1	3
130469	1	22	7	67	.1	17	13	322	3.22	5	5	ND	1	49	.2	2	2	76	.46	.178	5	36	.43	90	.09	6	1.53	.02	.09	1	2
130470	1	46	3	69	.2	22	14	408	3.48	4	5	ND	2	59	.4	2	2	83	.56	.124	6	37	.52	91	.10	4	1.86	.02	.09	1	3
130471	1	36	3	77	.1	20	14	364	4.22	12	5	ND	1	52	.6	2	3	93	.47	.235	6	39	.62	165	.11	2	1.97	.03	.08	1	6
130472	1	117	9	39	.1	24	14	300	4.08	11	5	ND	2	53	.2	2	3	111	.50	.146	8	42	.57	93	.09	3	1.84	.02	.09	1	16
130473	1	43	2	93	.2	18	16	511	3.77	8	5	ND	2	47	.2	2	2	81	.42	.204	6	30	.52	116	.11	2	2.00	.02	.07	1	41
130474	2	52	6	82	.3	18	14	286	4.51	28	8	ND	2	57	.3	2	7	101	.58	.148	5	31	.73	116	.16	5	2.26	.03	.12	1	3
130475	1	21	4	150	.3	18	12	508	3.15	7	5	ND	3	43	.2	3	2	71	.43	.152	6	30	.45	82	.11	4	1.51	.02	.08	1	4
130476	1	40	7	47	.1	20	11	347	2.88	6	5	ND	1	67	.2	2	2	70	.63	.113	11	35	.57	93	.13	7	1.41	.03	.07	1	3
130477	2	94	10	77	.1	22	15	542	4.60	14	5	ND	1	60	.3	2	2	128	.53	.068	11	47	.48	92	.10	4	1.84	.02	.07	1	1
130478	1	95	2	50	.1	20	16	393	4.55	7	5	ND	3	51	.4	2	2	124	.59	.118	7	46	.77	68	.12	6	1.53	.04	.12	1	4
130479	1	113	4	92	.4	21	19	701	5.30	14	5	ND	4	45	.5	5	6	143	.54	.187	7	52	.82	73	.11	9	2.10	.03	.08	1	6
130480	1	150	9	140	.2	16	17	492	5.67	9	5	ND	3	44	.3	2	2	137	.30	.407	6	54	.51	101	.10	2	3.19	.01	.05	1	6
130481	2	104	11	53	.1	16	13	400	3.58	14	5	ND	6	35	.3	3	6	72	.44	.134	8	32	.62	70	.10	5	1.36	.03	.09	1	14
STANDARD C/AU-S	19	58	35	130	7.5	71	32	1064	3.97	37	20	7	39	52	18.4	17	22	56	.47	.093	38	58	.86	183	.08	34	1.84	.07	.14	11	46
STANDARD C	19	61	41	130	7.3	68	31	1060	3.90	38	20	7	40	53	18.8	15	22	56	.48	.092	39	57	.85	176	.09	34	1.87	.07	.15	12	-

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
130482	1	139	9	59	.1	21	10	343	3.43	8	5	ND	4	42	.2	2	2	75	.48	.092	15	46	.56	88	.13	2	1.56	.03	.07	1	16
130483	1	47	4	42	.3	16	11	393	3.24	4	7	ND	3	55	.2	2	2	83	.49	.121	8	36	.46	100	.10	2	1.42	.03	.10	1	5
130484	1	37	4	39	.1	18	11	207	3.64	6	5	ND	1	40	.3	2	2	87	.42	.123	9	39	.41	84	.10	2	1.91	.03	.07	1	4
130485	1	53	7	44	.2	19	9	369	3.00	7	5	ND	2	60	.3	2	2	80	.68	.107	11	38	.53	104	.11	2	1.21	.05	.11	1	5
130486	1	20	4	72	.2	17	10	197	4.03	4	5	ND	2	42	.2	2	2	92	.40	.276	7	40	.34	91	.10	2	1.85	.02	.08	1	4
130487	1	38	5	99	.2	11	6	152	4.27	3	5	ND	2	25	.2	2	2	113	.36	.287	8	52	.35	66	.16	2	2.47	.02	.04	1	4
130488	1	118	37	79	.5	11	10	438	3.69	12	5	ND	1	181	.3	2	2	98	.50	.063	5	34	.55	267	.09	4	1.54	.03	.07	1	9
130489	1	22	7	65	.1	12	6	176	3.59	6	5	ND	2	37	.2	2	2	95	.33	.169	6	36	.28	88	.09	2	1.55	.03	.05	1	3
130490	1	30	3	111	.3	15	10	271	3.72	5	5	ND	2	39	.5	2	2	104	.37	.061	8	41	.35	73	.12	2	1.51	.03	.07	1	7
130491	1	76	12	246	.2	21	11	345	4.07	14	5	ND	3	46	.5	2	2	83	.41	.068	11	38	.58	134	.10	3	2.60	.02	.07	1	3
,92	1	61	6	112	.3	14	7	220	4.15	10	5	ND	2	58	.2	2	2	106	.35	.197	6	39	.43	117	.10	2	2.07	.02	.05	2	1
130493	1	172	15	329	.2	54	11	327	3.18	42	5	ND	2	92	.2	2	2	86	.33	.112	6	34	.44	214	.09	2	2.46	.02	.05	1	2
130494	1	23	2	161	.2	13	9	261	3.85	7	5	ND	2	41	.2	3	2	110	.42	.123	6	39	.35	65	.10	2	1.15	.02	.06	1	1
130495	1	23	8	60	.3	8	6	345	2.62	3	5	ND	1	45	.2	2	2	75	.37	.043	7	27	.24	75	.12	2	1.28	.02	.06	1	14
130496	1	23	9	59	.1	12	6	210	3.10	7	5	ND	1	36	.2	3	2	86	.30	.111	6	32	.31	76	.12	2	1.39	.02	.07	1	5
130497	1	29	9	62	.1	14	9	229	3.69	7	5	ND	1	48	.2	2	2	91	.42	.060	7	35	.41	73	.12	5	1.68	.03	.06	1	3
130498	1	31	2	111	.1	19	10	251	4.07	7	5	ND	1	42	.2	2	2	90	.39	.201	7	37	.41	98	.11	2	2.15	.02	.08	1	5
130499	1	88	5	86	.2	24	16	427	4.54	15	5	ND	1	69	.2	2	2	104	.71	.186	8	45	.75	113	.13	2	2.32	.03	.12	1	12
130500	1	61	7	43	.2	22	11	413	3.39	8	5	ND	2	84	.2	2	2	83	.76	.096	10	40	.79	123	.17	3	1.91	.05	.13	1	3
130501	1	31	2	119	.3	20	13	362	3.71	16	5	ND	1	53	.2	2	3	77	.48	.241	8	37	.55	130	.12	2	2.08	.03	.12	1	1
130502	1	82	2	63	.2	19	12	385	3.31	13	5	ND	2	63	.2	2	2	86	.75	.070	10	36	.71	104	.16	2	1.90	.04	.10	1	12
130503	1	40	12	67	.3	20	11	304	4.06	10	5	ND	1	58	.2	2	2	100	.56	.073	6	41	.56	87	.16	4	1.75	.03	.11	1	21
130504	1	39	6	52	.3	20	12	309	4.03	9	5	ND	1	61	.2	2	4	97	.51	.125	7	46	.62	79	.15	2	2.05	.03	.11	1	11
130505	1	84	8	46	.2	26	14	491	3.75	13	5	ND	1	87	.2	2	2	89	.75	.123	8	48	.74	122	.13	5	2.02	.04	.15	1	2
130506	1	57	6	56	.2	29	12	328	3.24	7	5	ND	2	56	.2	2	2	76	.47	.133	8	42	.59	109	.12	2	1.80	.03	.08	1	2
130507	1	28	4	85	.1	21	11	244	3.03	2	5	ND	1	53	.2	2	2	64	.48	.178	8	36	.51	124	.11	3	1.69	.02	.11	1	9
130508	1	33	5	46	.2	17	9	306	2.64	6	5	ND	1	42	.2	2	2	59	.41	.078	6	35	.37	90	.11	2	1.42	.02	.08	1	5
130509	2	100	6	94	.3	40	18	423	5.27	9	5	ND	1	65	.2	2	2	109	1.17	.087	11	59	.91	165	.17	2	2.87	.03	.11	1	10
130505	1	87	4	48	.3	26	14	501	3.89	12	5	ND	1	91	.2	2	2	93	.78	.127	7	50	.77	130	.14	2	2.09	.04	.16	1	5
,510	1	35	3	36	.1	25	8	229	2.51	4	5	ND	1	53	.2	2	2	59	.49	.088	11	46	.58	70	.10	2	1.26	.03	.04	1	12
130511	1	22	4	45	.3	16	7	271	3.39	7	5	ND	1	49	.2	2	2	76	.36	.081	6	39	.42	77	.10	2	1.30	.02	.05	1	14
130512	1	28	6	62	.2	24	10	317	3.21	8	5	ND	2	47	.2	2	2	68	.39	.151	9	44	.50	89	.11	2	1.61	.02	.07	1	2
130513	1	13	2	137	.1	19	7	402	2.49	2	5	ND	1	41	.3	2	2	58	.35	.114	9	39	.38	72	.10	2	1.22	.02	.06	1	1
130514	1	14	9	47	.1	13	7	273	2.43	4	5	ND	1	45	.2	2	2	61	.38	.079	7	33	.29	82	.11	2	1.13	.03	.07	2	1
130515	1	41	6	82	.2	25	11	408	2.97	6	5	ND	1	52	.2	2	2	66	.50	.071	8	40	.52	100	.11	6	1.72	.02	.09	1	11
130516	1	31	5	90	.2	26	10	346	3.14	6	5	ND	1	41	.3	2	2	69	.35	.105	8	45	.54	78	.11	2	1.68	.02	.08	1	1
130517	1	32	4	55	.2	24	8	281	2.56	2	5	ND	1	51	.2	2	2	60	.45	.040	9	41	.56	87	.13	5	1.48	.03	.07	1	16
STANDARD C/AU-S	20	58	38	135	6.9	74	34	1083	4.05	43	22	8	41	53	18.5	18	19	59	.49	.094	40	61	.91	184	.09	34	2.03	.07	.16	12	45
STANDARD C	18	58	39	133	6.8	71	32	1047	3.99	37	17	8	38	52	18.5	15	18	55	.48	.091	38	60	.89	177	.09	34	1.89	.06	.15	11	-

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
130518	1	30	6	56	.1	21	12	286	3.30	11	6	ND	1	49	.2	2	2	71	.48	.049	7	39	.50	80	.10	4	1.69	.02	.05	1	6
130519	1	32	8	65	.4	21	10	399	2.46	4	7	ND	2	45	.2	6	3	62	.42	.053	8	35	.44	96	.09	3	1.38	.02	.07	2	2
130520	1	21	9	54	.1	18	11	347	2.73	6	5	ND	1	42	.2	3	2	63	.42	.078	7	39	.42	83	.10	3	1.47	.02	.05	1	10
130522	1	11	2	34	.2	14	7	159	2.79	11	5	ND	2	37	.2	5	2	69	.27	.050	6	37	.25	90	.09	4	1.37	.01	.02	2	4
130523	1	15	5	33	.2	17	7	248	2.17	7	5	ND	1	50	.2	4	4	50	.40	.077	10	37	.36	89	.10	2	1.24	.02	.04	1	6
130524	1	18	2	28	.1	16	7	174	2.39	7	5	ND	1	43	.2	3	2	57	.37	.085	9	41	.35	63	.10	4	1.12	.02	.03	1	1
130525	1	19	2	38	.1	29	13	196	3.11	12	5	ND	1	34	.2	2	2	69	.24	.109	7	48	.35	88	.09	2	1.80	.01	.04	1	5
130526	2	33	11	322	.5	18	22	871	5.75	14	5	ND	2	33	2.5	5	4	145	.33	.078	6	52	.52	165	.20	5	2.13	.01	.06	2	1
130527	1	46	5	36	.1	16	8	206	3.29	7	5	ND	1	37	.2	2	2	83	.40	.076	6	36	.51	98	.09	2	1.38	.02	.04	1	1
130528	1	24	2	58	.3	14	9	224	3.76	5	5	ND	2	39	.2	2	2	96	.29	.080	6	37	.44	78	.10	2	2.08	.01	.05	1	1
130529	1	39	6	58	.2	21	12	431	3.66	9	5	ND	1	41	.2	2	2	84	.42	.079	5	42	.40	121	.07	2	1.90	.02	.06	1	5
130530	1	26	7	37	.3	15	8	184	2.91	11	5	ND	1	33	.2	2	3	70	.31	.053	6	29	.31	98	.06	2	1.52	.02	.04	1	4
130531	1	35	4	34	.1	21	9	307	2.25	8	6	ND	1	64	.2	2	2	51	.73	.048	9	33	.55	205	.08	3	1.65	.03	.07	1	4
130532	2	34	7	60	.1	16	9	293	3.97	9	5	ND	1	64	.2	2	6	93	.35	.039	6	31	.44	171	.10	2	1.89	.02	.06	1	1
130533	1	42	7	56	.4	21	12	386	4.00	9	5	ND	2	43	.2	3	3	88	.35	.107	6	36	.53	136	.08	6	2.20	.01	.07	1	1
130534	1	36	7	55	.2	23	12	226	4.01	6	5	ND	1	39	.2	2	2	82	.38	.111	6	41	.43	170	.08	2	2.26	.02	.08	1	3
130535	1	42	2	56	.3	21	11	258	3.63	10	5	ND	2	43	.2	3	2	74	.39	.128	6	33	.49	300	.07	5	2.19	.01	.07	1	3
130536	1	68	6	57	.3	28	9	365	3.06	9	5	ND	1	48	.2	2	2	67	.61	.035	14	37	.60	265	.10	3	2.21	.02	.08	1	20
130537	1	24	7	95	.1	17	11	516	3.15	12	5	ND	1	35	.2	2	2	63	.36	.192	8	34	.43	144	.07	2	1.92	.02	.07	1	13
130538	1	41	5	46	.1	25	8	294	2.87	11	5	ND	1	50	.2	2	2	67	.67	.049	13	40	.56	165	.11	5	1.62	.03	.07	1	10
RE 130544	1	26	11	65	.1	43	12	460	2.75	8	5	ND	2	39	.2	2	2	50	.46	.077	12	56	.83	116	.12	5	1.29	.02	.08	1	5
130539	1	33	2	67	.3	21	15	470	4.58	7	5	ND	1	59	.3	2	2	103	.48	.111	6	42	.63	220	.08	6	1.73	.02	.08	1	12
130540	1	24	6	38	.1	30	11	330	2.82	9	5	ND	1	41	.2	2	2	64	.45	.079	9	40	.58	86	.11	2	1.17	.02	.07	1	3
130541	1	21	2	78	.1	28	11	332	3.00	9	5	ND	1	49	.2	2	2	66	.51	.059	9	44	.50	110	.09	4	1.19	.02	.08	1	30
130542	1	104	20	130	.3	108	25	1108	5.18	18	5	ND	3	63	.2	2	2	75	.66	.056	18	92	1.56	285	.13	2	3.04	.02	.24	1	1
130543	1	66	13	100	.2	79	24	1016	4.59	16	5	ND	3	73	.5	2	2	71	.67	.046	14	83	1.47	241	.14	5	2.75	.03	.18	1	5
130544	1	25	5	61	.1	42	9	437	2.58	10	5	ND	2	37	.2	2	2	47	.43	.068	12	53	.78	110	.12	2	1.23	.02	.08	1	17
130545	1	25	5	102	.1	42	12	319	2.92	8	5	ND	1	36	.2	3	2	59	.42	.096	10	52	.80	141	.09	2	1.78	.02	.06	1	1
546	1	38	6	86	.2	66	17	690	3.31	11	5	ND	2	49	.2	2	2	52	.55	.052	13	73	1.25	189	.13	3	1.99	.03	.14	1	14
130547	1	103	3	93	.5	74	15	493	3.53	16	5	ND	2	74	.5	2	2	60	.69	.042	14	75	1.15	219	.10	2	2.25	.03	.12	1	11
130548	1	38	3	42	.2	26	10	426	2.83	10	5	ND	1	54	.2	2	2	66	.54	.066	10	40	.58	114	.10	4	1.31	.02	.08	1	15
130549	1	26	4	31	.1	23	10	248	2.89	10	5	ND	1	41	.2	2	2	70	.44	.060	8	37	.47	101	.10	7	1.26	.02	.06	1	9
130550	1	20	9	80	.1	14	8	180	2.95	7	5	ND	1	54	.2	2	2	66	.46	.044	8	32	.37	135	.09	3	1.21	.01	.06	1	9
130551	1	73	3	58	.3	29	14	832	3.23	13	5	ND	1	60	.2	2	3	75	.55	.063	10	41	.51	203	.08	3	1.81	.02	.08	1	2
130552	1	35	2	40	.2	12	10	277	2.59	9	5	ND	1	48	.2	2	2	56	.50	.030	7	25	.47	117	.06	2	1.45	.02	.08	1	3
130553	1	61	7	43	.1	26	10	228	3.09	10	5	ND	1	42	.2	2	6	69	.40	.080	7	35	.49	130	.10	3	2.00	.02	.06	1	19
STANDARD C/AU-S	18	55	36	123	7.2	68	34	998	3.90	40	19	7	36	52	17.9	16	19	56	.45	.084	36	56	.83	172	.09	34	1.80	.06	.14	11	55
STANDARD C	18	56	40	132	7.5	70	32	1049	3.98	40	18	7	37	54	18.8	15	19	54	.48	.090	37	59	.89	175	.09	32	1.87	.06	.15	12	-

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
130554	1	55	2	38	.2	25	14	299	3.28	15	5	ND	1	48	.2	2	2	81	.59	.086	7	37	.56	124	.10	4	1.85	.04	.10	3	7
130555	1	25	2	37	.1	27	11	227	3.04	11	5	ND	1	40	.2	2	2	71	.42	.099	7	35	.43	130	.09	2	1.95	.04	.07	1	2
130556	1	43	5	46	.3	27	12	233	3.68	9	5	ND	2	39	.2	2	2	77	.49	.103	7	38	.53	249	.09	2	2.33	.03	.08	1	37
130557	1	28	4	72	.3	15	10	264	3.07	16	5	ND	2	28	.2	3	2	60	.37	.169	7	25	.41	270	.05	2	2.07	.02	.09	2	3
130558	1	29	2	37	.1	17	9	205	2.48	9	5	ND	1	40	.2	2	2	58	.45	.071	7	30	.42	132	.09	4	1.61	.03	.06	1	2
130559	1	49	2	44	.1	23	13	217	3.57	9	5	ND	1	37	.2	2	2	83	.38	.063	8	39	.51	169	.10	2	2.70	.02	.05	1	2
130560	1	24	2	70	.1	13	10	700	3.23	5	5	ND	1	44	.4	2	2	72	.42	.181	5	30	.36	154	.07	2	1.74	.02	.06	1	1
130561	1	18	2	68	.1	15	9	248	3.05	4	5	ND	1	33	.3	2	2	66	.36	.147	7	34	.31	92	.08	3	1.92	.02	.05	1	2
130562	1	38	3	104	.4	16	11	385	3.56	8	5	ND	2	35	.2	2	2	76	.44	.137	8	38	.46	141	.09	2	1.87	.02	.09	1	4
130563	3	154	7	85	.3	23	26	922	6.27	26	5	ND	1	36	.2	2	2	72	.37	.107	4	26	.40	179	.03	2	2.22	.02	.18	1	1
130564	1	35	10	60	.2	22	13	310	3.89	10	5	ND	2	34	.2	2	2	88	.32	.185	7	38	.42	96	.09	2	2.16	.02	.05	1	1
130565	1	57	3	69	.1	19	19	619	4.31	18	5	ND	1	49	.2	2	2	109	.75	.187	6	33	1.04	95	.14	2	2.23	.06	.13	1	2
131165	1	66	6	70	.1	23	18	578	4.55	24	5	ND	2	47	.2	2	2	115	.72	.166	6	36	.99	98	.14	3	2.13	.06	.13	1	3
131166	1	40	9	62	.2	20	14	329	3.14	11	5	ND	2	43	.2	2	2	69	.48	.158	7	34	.53	110	.10	2	2.00	.02	.08	1	4
131167	1	57	3	88	.2	20	11	494	2.97	9	5	ND	1	56	.2	2	2	71	.63	.066	10	33	.55	116	.11	2	1.78	.02	.08	1	1
131168	1	33	2	38	.1	17	10	258	3.16	3	5	ND	1	50	.2	2	2	80	.48	.075	8	32	.52	105	.12	2	1.41	.03	.06	1	1
131169	1	28	2	41	.1	21	11	218	3.57	6	5	ND	1	41	.3	2	2	84	.40	.086	7	36	.41	92	.10	3	1.73	.02	.06	1	1
131170	1	37	2	47	.1	19	12	415	3.13	10	5	ND	2	48	.2	2	2	82	.53	.042	9	36	.54	104	.12	4	1.55	.03	.08	1	2
RE 131182	1	31	2	46	.1	19	8	287	2.08	6	5	ND	1	59	.2	2	2	52	.65	.063	10	30	.58	88	.13	3	1.30	.04	.06	1	1
131171	1	18	7	80	.2	19	12	280	3.90	9	5	ND	1	40	.2	2	2	92	.42	.160	6	35	.47	93	.10	2	1.71	.02	.07	1	1
131172	1	25	9	111	.1	13	10	512	3.14	4	5	ND	1	35	.2	2	2	73	.36	.255	6	31	.38	99	.09	4	2.25	.02	.05	1	2
131173	1	31	6	77	.1	19	10	364	3.22	6	5	ND	2	33	.2	3	2	79	.38	.096	7	34	.40	101	.10	2	2.32	.02	.05	1	2
131174	3	24	6	71	.4	9	9	321	3.09	7	5	ND	1	41	.2	2	2	104	.51	.048	6	19	.33	142	.05	2	2.25	.01	.06	1	1
131175	5	274	81	222	.6	19	64	1452	9.22	102	5	ND	1	332	.8	2	9	176	.89	.117	21	19	.89	2427	.03	2	4.35	.02	.12	1	10
131176	2	61	6	127	.1	26	13	575	3.72	13	5	ND	1	39	1.0	2	2	93	.41	.058	7	41	.49	157	.09	2	1.76	.02	.08	1	1
131177	4	70	15	349	.4	25	21	400	5.34	35	5	ND	1	65	1.4	2	2	124	1.04	.060	7	39	.82	233	.09	5	2.78	.03	.10	1	9
131178	3	78	25	326	.8	13	28	565	8.80	285	6	ND	1	22	.8	2	2	166	.23	.072	3	30	1.21	243	.01	2	4.69	.01	.08	1	2
131179	1	28	2	177	.1	25	11	241	3.96	11	5	ND	1	39	.6	2	2	84	.31	.038	7	42	.52	102	.15	2	2.09	.02	.06	1	1
180	2	39	2	64	.1	39	11	398	3.08	9	5	ND	2	47	.2	2	2	61	.59	.048	11	53	.79	129	.14	3	1.79	.04	.08	1	1
131181	1	33	8	250	.1	24	13	367	3.86	12	5	ND	1	46	.4	2	3	81	.45	.135	8	41	.62	121	.11	2	2.44	.03	.09	1	1
131182	1	31	5	47	.1	19	8	289	2.11	3	5	ND	1	61	.2	2	2	53	.66	.064	10	33	.59	91	.13	2	1.34	.04	.06	1	1
131183	1	45	6	63	.2	26	11	250	3.15	11	5	ND	2	43	.2	4	7	70	.40	.078	8	41	.50	103	.13	4	2.19	.03	.06	1	1
131184	1	34	3	85	.1	25	12	531	3.26	13	5	ND	1	41	.2	2	2	74	.39	.106	8	41	.43	101	.10	2	1.77	.02	.08	1	1
131185	1	40	10	61	.1	32	11	289	2.87	11	5	ND	2	47	.2	2	2	61	.48	.088	9	44	.69	135	.13	3	1.94	.03	.08	1	1
131186	1	67	6	42	.1	28	11	292	3.01	9	8	ND	1	64	.2	2	5	74	.60	.084	9	40	.67	129	.14	2	1.83	.04	.08	1	1
131187	1	116	7	44	.1	29	12	350	3.30	9	5	ND	1	67	.2	2	2	80	.64	.092	10	44	.72	121	.16	2	1.97	.05	.12	1	1
131188	1	43	11	68	.1	19	11	339	2.88	10	5	ND	1	59	.2	2	2	73	.54	.080	8	35	.53	120	.11	3	1.65	.03	.08	1	8
STANDARD C/AU-S	18	58	37	127	7.1	66	32	1020	3.93	36	15	7	40	51	17.4	14	17	55	.46	.090	39	60	.86	177	.09	31	1.93	.07	.17	11	49
STANDARD C	19	59	42	133	7.1	70	33	1046	3.97	39	18	7	38	51	18.5	15	20	55	.48	.090	38	58	.88	177	.09	33	1.89	.06	.15	13	-

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
131189	4	180	12	257	.2	26	20	677	6.58	50	5	ND	3	52	.3	2	2	122	.43	.126	8	51	.78	148	.13	3	2.83	.02	.08	2	110
131190	1	73	5	156	.2	27	14	296	5.07	11	5	ND	2	40	.2	3	2	112	.40	.240	8	55	.62	91	.09	2	2.43	.02	.07	1	9
131191	1	122	9	129	.1	21	15	413	4.24	42	5	ND	1	76	.2	2	2	97	.64	.097	8	40	.71	121	.13	4	2.13	.03	.09	1	17
131192	1	69	4	66	.1	25	15	393	3.75	10	5	ND	3	52	.2	2	2	92	.61	.150	9	44	.67	106	.11	4	1.96	.02	.10	1	4
131193	1	90	7	110	.1	21	12	259	3.89	42	5	ND	1	54	.2	2	2	91	.62	.089	9	40	.62	97	.13	2	2.06	.03	.07	1	14
131194	1	109	14	180	.4	24	22	1429	6.13	78	5	ND	1	43	.2	2	2	128	.47	.085	6	50	1.01	91	.12	2	3.43	.01	.09	1	1
131195	1	113	34	123	.7	28	19	653	5.14	109	5	ND	1	49	.2	2	3	127	.50	.039	6	50	1.04	98	.13	4	2.71	.02	.10	1	2
131196	1	132	4	55	.2	20	13	537	3.56	9	5	ND	2	67	.2	2	2	87	.70	.056	10	42	.72	105	.14	6	1.91	.04	.09	1	4
131197	1	128	9	89	.1	22	20	818	4.86	12	5	ND	3	83	.2	2	2	116	1.07	.142	12	43	1.13	125	.18	2	2.39	.06	.16	1	4
131198	1	99	9	77	.1	21	12	512	3.48	13	5	ND	1	61	.2	2	2	87	.61	.138	7	39	.62	110	.10	3	2.02	.02	.10	1	2
199	1	40	3	75	.1	19	10	241	3.71	7	5	ND	2	41	.3	3	2	84	.41	.119	8	38	.46	85	.11	2	1.76	.02	.07	1	2
131200	1	132	2	83	.1	23	13	273	3.89	10	5	ND	2	52	.2	3	2	92	.49	.091	9	40	.65	111	.13	3	2.49	.02	.10	1	3
131201	1	79	20	105	.1	18	9	282	2.92	3	5	ND	2	55	.3	2	2	74	.55	.075	9	35	.58	81	.12	2	1.55	.02	.07	1	5
131202	1	108	8	127	.1	21	12	360	3.89	11	5	ND	2	48	.2	2	4	87	.48	.150	9	41	.57	92	.11	5	2.08	.02	.09	1	7
131203	1	97	12	174	.3	17	10	332	4.10	31	5	ND	1	47	.3	2	2	91	.49	.150	8	39	.49	93	.10	5	1.83	.02	.07	1	17
131204	1	119	10	117	.8	19	11	390	3.56	11	5	ND	2	46	.2	2	2	83	.41	.122	7	38	.52	99	.10	5	2.16	.02	.07	1	8
131205	1	70	7	59	.4	13	8	252	3.26	11	5	ND	2	42	.2	2	2	88	.48	.139	8	36	.37	71	.09	5	1.56	.02	.05	1	6
131206	1	37	5	43	.1	11	5	166	2.78	6	5	ND	1	38	.3	2	2	73	.32	.041	7	32	.29	62	.08	3	1.58	.02	.03	1	1
131207	3	51	2	38	.1	15	7	195	3.53	7	5	ND	1	40	.2	2	2	93	.33	.034	7	34	.40	70	.09	4	1.34	.02	.03	1	4
131208	1	69	2	50	.1	19	11	362	4.01	7	5	ND	4	39	.2	2	2	101	.48	.208	7	47	.60	60	.09	6	1.88	.03	.08	1	6
131209	1	24	4	58	.1	14	6	148	3.26	5	5	ND	3	23	.2	2	2	79	.23	.138	6	43	.28	59	.08	2	2.08	.01	.04	1	4
131210	1	38	7	24	.1	10	5	191	3.12	6	5	ND	3	31	.3	2	2	85	.36	.171	8	38	.30	44	.07	4	.91	.01	.03	1	18
131211	3	81	8	72	.2	17	13	841	4.49	14	5	ND	1	54	.2	3	2	122	.72	.131	16	66	.56	78	.08	2	1.63	.02	.07	1	110
RE 131206	1	39	6	45	.1	11	5	172	2.82	8	5	ND	1	38	.2	2	2	76	.33	.042	7	32	.30	63	.08	3	1.63	.02	.03	1	5
131212	1	338	13	75	.6	34	15	953	5.30	13	5	ND	3	69	.3	2	2	140	1.01	.093	21	64	.71	131	.10	4	2.82	.02	.11	1	7
131213	2	58	6	54	.1	13	8	276	2.78	10	5	ND	2	37	.3	2	2	70	.49	.093	11	43	.42	65	.08	6	1.42	.02	.05	1	3
131214	1	36	6	31	.1	17	9	280	2.82	6	5	ND	2	49	.2	2	2	82	.66	.125	10	35	.44	68	.09	3	.95	.03	.06	1	65
131215	1	33	2	25	.1	15	7	201	2.63	4	5	ND	5	38	.2	2	2	77	.44	.118	9	33	.38	84	.09	2	1.30	.02	.05	1	12
216	1	37	2	23	.1	11	5	172	2.59	5	5	ND	1	40	.2	2	2	75	.49	.092	10	31	.33	38	.07	4	.96	.02	.04	1	4
217	1	31	9	29	.1	18	8	179	2.60	4	5	ND	2	34	.2	2	2	67	.32	.078	7	37	.35	70	.10	5	1.45	.02	.04	1	5
131218	1	78	7	45	.1	18	9	236	3.91	10	5	ND	1	42	.2	2	2	97	.42	.154	8	39	.44	82	.09	2	1.93	.02	.06	1	16
131219	1	31	10	37	.3	11	5	150	2.99	5	5	ND	1	31	.3	2	2	74	.26	.076	6	29	.25	55	.09	2	1.67	.01	.04	1	8
131220	1	272	2	65	.2	18	11	467	3.48	15	5	ND	3	76	.2	2	2	91	.69	.110	12	44	.64	102	.14	3	1.54	.04	.10	1	26
131221	2	59	7	84	.3	13	11	464	4.20	12	5	ND	1	47	.5	3	2	105	.41	.070	7	37	.44	71	.14	2	1.77	.02	.10	1	5
131222	1	38	12	130	.4	15	9	292	3.62	5	5	ND	2	40	.3	2	2	82	.42	.240	7	34	.36	81	.09	5	1.99	.02	.07	1	5
131223	1	54	4	42	.1	18	8	235	2.92	5	5	ND	1	51	.2	2	2	74	.47	.071	8	36	.44	74	.11	2	1.47	.02	.06	2	26
131224	1	56	4	50	.1	18	7	237	2.72	5	5	ND	1	47	.2	2	4	66	.51	.098	9	35	.47	72	.11	2	1.53	.02	.06	1	6
STANDARD C/AU-S	21	62	40	142	7.4	75	32	1135	4.01	37	22	6	40	53	19.0	15	22	60	.51	.095	40	60	.92	184	.08	37	2.07	.07	.15	11	47
STANDARD C	18	60	38	134	7.1	70	33	1082	4.04	36	15	6	39	52	18.7	15	20	56	.49	.091	39	59	.87	179	.09	33	1.92	.06	.15	11	-

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
131225	1	63	5	44	.1	20	10	264	3.01	8	5	ND	2	45	.2	2	2	85	.45	.111	8	38	.43	91	.10	2	1.69	.03	.07	1	11
131226	1	48	5	38	.1	17	10	246	2.80	4	5	ND	2	46	.2	2	2	81	.41	.072	9	35	.41	99	.11	3	1.57	.03	.06	1	9
131227	1	46	9	44	.2	17	9	247	2.87	7	5	ND	1	61	.4	2	2	84	.58	.079	8	36	.48	97	.11	4	1.67	.03	.07	1	4
RE 131232	1	22	8	32	.1	11	6	167	2.38	3	5	ND	1	34	.2	2	2	69	.27	.123	9	33	.23	52	.10	2	1.55	.02	.04	1	9
131228	2	95	6	58	.1	22	10	352	3.08	7	5	ND	1	49	.2	2	2	81	.49	.064	10	37	.59	106	.12	2	2.39	.02	.08	1	3
131229	1	34	8	44	.2	13	8	196	3.27	5	5	ND	1	40	.2	2	2	83	.38	.089	9	37	.33	61	.10	2	1.91	.02	.05	1	6
131230	1	24	3	34	.1	9	6	213	3.60	7	5	ND	2	37	.2	2	2	102	.39	.118	7	39	.30	63	.10	2	1.81	.02	.04	1	4
131231	1	43	16	25	.1	13	6	183	2.37	5	5	ND	1	50	.2	2	2	70	.55	.094	10	31	.38	61	.10	2	1.17	.02	.04	1	2
131232	1	23	12	32	.2	10	5	162	2.33	4	5	ND	2	33	.3	2	2	67	.26	.121	9	33	.22	52	.10	2	1.53	.02	.03	1	5
131233	1	35	5	35	.1	14	6	189	2.96	8	5	ND	1	41	.2	2	2	89	.43	.087	7	35	.40	61	.11	2	1.28	.02	.05	1	7
131234	1	44	4	33	.1	17	8	208	3.03	7	5	ND	3	38	.3	2	2	87	.40	.172	9	41	.35	87	.10	2	1.56	.02	.05	1	5
131235	1	62	5	26	.1	17	7	185	2.51	6	5	ND	1	50	.3	2	2	71	.52	.096	10	35	.38	59	.09	2	1.33	.02	.04	1	3
131236	1	98	10	42	.1	16	9	295	2.74	9	5	ND	2	60	.2	2	2	78	.64	.115	13	36	.44	67	.10	3	1.33	.03	.06	1	9
131237	2	30	4	28	.1	10	5	151	2.52	4	5	ND	1	38	.2	2	2	79	.34	.033	7	29	.26	48	.09	3	1.24	.02	.04	1	7
131238	3	109	8	43	.2	21	10	226	3.71	10	5	ND	2	52	.2	2	2	96	.49	.083	9	39	.48	76	.13	3	2.12	.02	.06	1	5
131239	1	101	10	44	.1	20	9	236	3.70	8	5	ND	4	34	.2	2	2	91	.27	.147	9	43	.47	71	.13	5	3.34	.02	.07	1	3
131240	1	52	7	66	.2	15	8	424	3.18	9	5	ND	1	40	.3	2	2	83	.40	.152	6	35	.37	75	.12	4	2.08	.02	.06	1	7
131241	1	174	4	41	.2	20	9	335	3.01	6	5	ND	3	56	.2	2	2	81	.55	.063	10	41	.60	84	.14	2	1.92	.02	.08	1	8
131242	1	55	3	71	.1	17	9	206	3.27	6	5	ND	2	43	.4	2	2	85	.45	.117	8	34	.40	80	.11	2	1.85	.02	.06	1	6
131243	1	75	5	45	.1	19	8	308	2.75	7	5	ND	1	62	.2	2	2	71	.59	.095	10	36	.56	93	.13	2	1.68	.03	.08	1	7
131244	1	51	2	25	.1	17	8	250	2.68	7	5	ND	2	53	.2	2	2	76	.51	.086	11	36	.46	90	.14	2	1.50	.03	.07	1	7
131245	1	69	2	31	.1	12	7	402	2.07	2	5	ND	3	62	.2	2	2	65	.72	.114	13	31	.42	65	.13	2	1.04	.03	.06	1	8
131246	1	55	2	67	.1	23	9	251	3.25	10	5	ND	3	40	.2	2	2	80	.32	.129	9	43	.50	82	.13	5	2.51	.02	.07	1	10
131247	1	35	2	35	.1	15	7	214	2.37	7	5	ND	1	57	.2	2	2	66	.54	.064	10	33	.54	71	.13	2	1.39	.03	.06	1	5
131248	1	30	3	31	.2	17	7	178	3.00	10	5	ND	1	43	.2	3	2	83	.42	.126	9	36	.33	69	.10	2	1.38	.02	.06	1	1
131249	1	17	2	45	.2	14	7	267	3.05	2	5	ND	1	42	.2	2	2	80	.33	.084	7	35	.24	58	.11	3	1.42	.02	.05	1	1
131250	1	24	3	41	.1	23	7	190	2.80	5	5	ND	2	35	.2	2	2	63	.29	.043	10	45	.50	75	.10	4	1.91	.02	.04	1	5
131251	1	29	3	38	.1	13	6	172	3.20	2	5	ND	2	38	.2	2	2	85	.32	.069	7	36	.24	50	.11	2	1.79	.02	.03	1	5
252	1	35	5	43	.2	12	7	204	3.55	3	5	ND	2	46	.2	2	3	92	.43	.119	8	37	.39	66	.12	2	1.93	.02	.07	1	3
131253	1	29	6	46	.1	9	4	145	3.17	2	5	ND	2	30	.3	2	3	94	.27	.141	7	36	.30	61	.12	2	2.28	.02	.05	1	2
131254	1	63	2	56	.1	18	9	225	3.61	5	5	ND	2	44	.2	2	2	89	.40	.129	8	39	.38	82	.11	2	2.35	.02	.06	1	27
131255	1	44	9	40	.1	17	8	205	3.24	4	5	ND	3	38	.2	2	2	85	.37	.121	9	38	.33	63	.10	6	2.01	.02	.05	1	5
131256	1	30	93	53	.1	17	6	214	3.08	6	5	ND	1	47	.3	2	2	71	.43	.108	9	36	.40	81	.12	2	1.69	.02	.05	1	9
131257	1	33	4	68	.2	19	7	169	4.09	6	5	ND	1	41	.2	2	2	87	.42	.092	8	46	.42	71	.10	2	1.63	.02	.04	1	7
131258	1	53	2	38	.2	18	7	241	2.49	5	5	ND	1	55	.2	2	2	66	.55	.069	11	39	.49	88	.12	3	1.40	.03	.06	1	5
131259	1	42	2	35	.2	22	9	349	2.68	6	5	ND	2	68	.3	2	2	69	.70	.097	12	39	.67	104	.15	4	1.46	.04	.09	1	5
131260	1	55	2	101	.1	19	8	237	3.33	5	5	ND	2	36	.2	2	2	72	.34	.065	10	38	.50	83	.14	2	2.42	.02	.06	1	4
STANDARD C/AU-S	20	59	37	135	7.4	74	32	1115	4.01	38	21	7	40	54	18.9	17	22	61	.50	.093	39	61	.89	186	.09	33	1.99	.07	.15	11	46
STANDARD C	19	59	39	131	7.6	71	33	1061	3.91	38	17	6	40	52	18.5	14	21	56	.48	.090	40	58	.87	175	.09	34	1.85	.06	.15	13	-

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
131261	1	34	6	56	.3	22	9	219	4.01	8	5	ND	2	41	.2	2	2	93	.33	.145	9	41	.41	88	.13	2	2.53	.03	.06	1	5
131262	1	47	8	32	.4	17	8	223	3.04	7	5	ND	3	57	.2	2	2	76	.50	.078	9	39	.41	89	.13	5	1.77	.04	.08	1	9
131263	4	354	2	84	1.0	53	29	1677	7.88	28	5	ND	1	165	.2	18	2	217	1.38	.139	15	23	2.80	5255	.17	2	4.40	.03	.19	1	19
131264	1	72	2	149	.2	17	13	752	3.37	3	5	ND	3	58	.3	2	2	73	.48	.188	8	36	.45	136	.12	2	1.98	.03	.10	1	9
131265	1	83	10	114	.5	18	20	1396	6.01	7	5	ND	1	61	.2	3	2	160	.98	.142	6	36	.89	191	.09	2	3.84	.02	.15	1	8
131266	2	136	9	120	.5	28	23	1771	6.28	25	5	ND	1	573	.2	9	2	130	1.04	.113	15	47	1.41	897	.08	2	3.49	.02	.20	1	6
131267	3	159	9	131	.4	28	19	389	4.54	8	5	ND	2	311	.2	2	2	103	.55	.056	10	54	1.06	117	.21	2	3.12	.03	.10	1	3
131268	2	74	4	115	.2	16	11	319	4.65	11	5	ND	1	59	.2	2	2	128	.46	.070	5	49	.64	101	.17	2	2.00	.03	.07	1	2
131269	2	72	13	199	.5	15	10	333	4.12	16	5	ND	1	62	.9	2	2	115	.48	.061	7	45	.59	124	.15	2	1.81	.03	.06	1	2
131270	1	87	2	120	.1	18	10	268	3.07	14	5	ND	1	63	.2	2	2	78	.55	.084	7	35	.49	112	.13	2	1.63	.04	.07	1	5
131271	1	156	9	235	.4	19	14	741	4.89	37	5	ND	2	50	.6	2	3	127	.49	.133	7	63	.72	104	.18	2	1.81	.03	.10	1	4
131273	1	115	3	108	.4	33	25	584	6.37	12	5	ND	1	242	.2	11	2	187	1.37	.159	6	73	1.56	213	.17	2	4.09	.03	.18	1	3
131274	1	74	4	99	.2	20	15	518	4.10	15	5	ND	5	85	.2	2	2	86	.86	.180	9	43	1.04	113	.13	5	2.30	.05	.17	1	2
131275	1	136	6	52	.1	21	12	436	3.57	6	5	ND	2	84	.2	2	2	85	.80	.068	11	43	.76	95	.17	2	2.26	.06	.12	1	2
131276	1	139	16	96	.3	57	27	425	6.15	22	5	ND	1	564	.2	8	3	321	1.40	.142	4	54	1.08	205	.08	2	5.03	.04	.20	1	2
131277	1	60	2	183	.3	15	14	587	4.88	6	5	ND	3	56	.2	2	2	118	.49	.530	7	48	.57	164	.11	2	2.30	.02	.09	1	3
131278	1	18	5	45	.1	10	7	173	3.53	3	5	ND	3	35	.2	2	2	95	.31	.097	6	37	.24	61	.11	2	1.33	.02	.07	1	6
131279	1	173	12	227	.3	21	16	1021	5.04	12	5	ND	4	81	.2	2	2	115	.60	.419	9	51	.85	177	.14	2	2.58	.02	.14	1	2
131280	1	272	2	91	.1	20	16	572	4.56	12	5	ND	5	65	.2	2	3	108	.66	.173	7	47	.92	98	.13	5	2.19	.04	.11	1	2
RE 131289	1	109	5	31	.1	22	8	239	2.91	11	5	ND	2	57	.2	2	2	71	.48	.068	9	40	.52	80	.12	2	1.59	.03	.05	1	1
131281	1	78	3	36	.1	24	13	300	7.09	6	5	ND	10	48	.2	2	3	227	.51	.102	9	84	.42	65	.13	5	1.45	.02	.09	1	4
131282	1	39	4	88	.1	16	9	398	4.09	7	5	ND	2	59	.3	2	2	99	.53	.146	9	45	.45	95	.11	2	1.76	.03	.10	1	3
131283	1	39	27	185	.4	18	17	1212	6.38	5	5	ND	4	71	.2	2	3	168	.43	.512	7	64	.56	196	.09	2	2.46	.02	.08	1	6
131284	1	31	9	99	.1	14	13	569	3.58	4	5	ND	4	55	.2	2	2	73	.63	.149	7	33	.67	107	.11	6	1.91	.04	.13	1	6
131285	4	34	5	66	.1	17	12	305	5.81	25	5	ND	2	64	.2	5	3	164	.36	.038	7	51	.55	154	.16	3	2.01	.02	.11	1	39
131286	5	273	8	120	.7	43	24	1683	5.31	21	5	ND	4	59	.3	4	2	119	.62	.077	15	56	.78	134	.18	2	3.72	.03	.10	1	6
131287	1	35	7	81	.2	15	11	527	4.25	8	5	ND	3	44	.2	2	2	94	.62	.248	8	43	.92	69	.11	5	2.25	.04	.09	1	2
131288	1	37	9	83	.2	25	17	855	4.04	12	5	ND	3	55	.2	2	2	100	.73	.190	8	47	1.15	94	.12	8	2.04	.07	.11	1	2
131289	1	109	4	33	.1	25	8	251	2.97	12	5	ND	2	58	.2	2	2	72	.50	.072	10	40	.55	84	.13	2	1.66	.03	.06	1	7
131290	1	37	2	56	.1	27	10	339	3.23	10	5	ND	1	64	.2	2	2	76	.55	.091	8	42	.58	82	.11	6	1.63	.03	.09	1	4
131291	1	80	6	50	.1	33	13	592	3.65	7	5	ND	3	90	.2	4	2	80	.79	.092	13	50	.80	161	.16	2	1.75	.07	.13	1	4
131292	1	19	2	207	.1	20	9	355	3.08	3	5	ND	1	49	.9	2	2	66	.42	.109	9	41	.49	84	.12	2	1.72	.03	.08	1	2
131293	1	51	4	101	.3	27	16	394	4.03	5	5	ND	1	51	.4	2	2	82	.44	.118	8	39	.57	110	.12	3	2.51	.03	.07	1	3
131294	1	48	5	47	.2	37	11	433	3.53	7	5	ND	3	74	.2	5	2	77	.83	.029	14	55	.83	176	.16	4	2.21	.08	.11	1	110
131295	1	30	7	47	.1	22	9	277	2.52	3	5	ND	2	53	.2	2	2	61	.54	.036	11	39	.64	104	.15	2	1.80	.05	.07	1	4
131296	1	46	7	54	.1	31	11	281	3.49	4	5	ND	2	49	.2	2	2	73	.47	.096	9	48	.68	144	.14	2	2.48	.03	.09	1	2
STANDARD C/AU-S	21	62	42	137	7.4	73	32	1082	4.05	40	18	7	40	54	17.0	17	22	60	.50	.100	40	56	.99	187	.10	35	2.00	.08	.16	11	45
STANDARD C	17	57	37	133	6.6	70	32	1043	3.97	36	17	6	38	52	18.5	15	20	57	.48	.091	37	57	.89	177	.09	34	1.90	.06	.15	12	-

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
131297	1	36	3	38	.2	28	12	232	3.25	9	5	ND	2	39	.3	5	2	79	.34	.092	7	42	.48	110	.10	3	1.84	.02	.05	1	7
131298	1	51	2	46	.2	23	13	344	2.92	8	5	ND	1	53	.2	2	2	75	.67	.030	10	38	.67	173	.11	2	1.86	.04	.06	1	6
131299	1	39	4	57	.1	21	12	279	3.50	7	5	ND	1	49	.4	2	2	95	.38	.071	8	39	.57	119	.11	2	1.94	.02	.07	1	2
131300	1	33	11	65	.1	23	13	238	3.83	5	5	ND	1	35	.3	2	2	93	.28	.124	10	42	.44	94	.10	2	2.35	.02	.06	1	3
131301	1	25	3	50	.1	20	13	294	4.65	12	5	ND	1	47	.2	2	2	130	.37	.087	6	47	.38	124	.08	2	1.55	.02	.05	1	1
131302	1	28	2	45	.1	22	11	293	3.00	9	5	ND	1	35	.2	2	2	76	.31	.111	8	37	.43	91	.08	2	1.58	.02	.04	1	1
131303	1	44	2	47	.1	20	12	499	2.92	7	5	ND	1	48	.2	2	2	70	.54	.094	9	36	.59	126	.08	5	1.37	.02	.08	1	7
131304	1	50	3	63	.3	22	14	529	3.75	10	5	ND	1	52	.2	4	2	92	.64	.055	9	41	.52	156	.08	4	1.67	.02	.07	1	7
131305	1	48	2	40	.1	23	9	233	2.50	8	5	ND	1	36	.2	2	2	61	.37	.045	7	35	.45	134	.08	3	1.96	.02	.05	1	1
131306	1	31	2	39	.3	20	11	278	3.24	11	5	ND	1	41	.2	3	2	83	.44	.098	6	36	.45	140	.07	4	1.39	.02	.05	1	4
.307	1	27	7	45	.1	23	12	281	3.53	9	5	ND	1	42	.2	2	2	84	.46	.092	7	38	.47	152	.09	2	1.81	.02	.06	1	1
RE 131312	1	106	7	74	.1	32	18	464	4.37	12	5	ND	2	50	.3	5	2	87	.43	.133	8	57	.96	416	.05	4	3.23	.02	.08	1	2
131308	1	69	4	63	.2	30	13	254	4.15	2	5	ND	2	41	.2	2	2	90	.31	.124	7	54	.55	168	.08	2	3.04	.01	.04	1	4
131309	1	99	11	78	.1	26	14	332	4.44	8	5	ND	2	40	.2	4	2	98	.30	.183	6	50	.54	160	.09	6	3.79	.02	.06	1	1
131310	1	86	10	123	.1	32	17	321	5.20	3	5	ND	1	52	.2	2	2	98	.43	.179	7	63	.67	152	.06	3	3.15	.02	.07	1	1
131311	1	26	2	82	.1	22	14	292	4.05	7	5	ND	1	52	.2	4	2	91	.56	.126	7	37	.51	162	.09	3	1.88	.02	.07	1	1
131312	1	105	6	73	.1	29	17	453	4.34	10	5	ND	4	51	1.0	5	2	86	.44	.133	8	58	.94	407	.06	4	3.16	.02	.08	1	1
131313	1	20	5	42	.1	14	9	209	3.25	4	5	ND	1	42	.2	2	2	83	.40	.047	6	36	.42	91	.10	5	1.51	.02	.05	1	1
131314	1	26	2	46	.3	21	10	253	2.67	7	5	ND	1	52	.2	4	2	67	.47	.045	8	35	.46	120	.10	2	1.41	.02	.05	1	1
131315	1	25	4	53	.1	27	12	289	3.17	6	5	ND	1	42	.2	2	2	75	.51	.066	9	43	.58	112	.10	6	1.44	.02	.06	1	36
131316	1	48	2	77	.3	38	12	369	3.10	9	5	ND	2	60	.2	2	2	64	.87	.056	11	50	.75	136	.09	2	1.64	.03	.07	1	52
131317	1	28	10	72	.1	40	12	487	3.28	7	5	ND	1	61	.2	2	2	64	.80	.084	12	56	1.01	106	.14	2	1.69	.06	.08	1	6
131318	1	45	2	102	.4	51	18	939	4.08	13	5	ND	2	54	.3	2	2	78	.84	.057	10	62	.90	203	.10	5	2.18	.03	.11	1	14
131319	1	40	4	73	.3	48	17	554	4.56	9	5	ND	3	46	.2	2	2	108	.70	.084	11	63	.80	144	.10	4	1.62	.03	.09	1	3
131320	2	47	7	109	.1	79	16	644	3.89	10	5	ND	1	53	.6	2	2	64	.69	.069	13	88	1.45	173	.13	5	2.17	.03	.12	1	1
131321	1	74	9	92	.5	75	15	578	3.55	14	5	ND	3	69	.9	3	2	58	.90	.066	14	78	1.27	203	.09	7	2.12	.03	.12	1	2
131322	1	113	6	78	.3	71	18	787	3.70	11	11	ND	1	64	.2	2	2	61	.74	.037	14	73	1.01	206	.09	5	2.14	.03	.11	1	1
131323	1	66	2	55	.2	36	12	465	3.38	8	5	ND	1	53	.5	2	2	81	.55	.060	12	49	.75	120	.10	4	1.61	.03	.08	1	8
1324	1	27	2	35	.1	25	9	281	2.68	5	5	ND	1	41	.2	2	2	67	.47	.056	9	40	.50	94	.10	2	1.13	.02	.07	1	1
1325	1	37	3	44	.2	20	9	272	2.50	4	5	ND	1	43	.5	2	2	65	.42	.022	8	35	.39	129	.10	6	1.19	.02	.07	1	1
131326	1	28	2	46	.2	23	10	235	2.92	10	5	ND	1	38	.2	2	2	71	.47	.100	8	37	.42	107	.09	4	1.31	.02	.07	1	2
131327	1	39	2	37	.1	28	11	289	2.85	7	5	ND	1	40	.2	2	2	69	.40	.053	8	39	.53	144	.08	2	1.27	.02	.07	1	14
131328	1	71	2	52	.4	27	17	662	4.05	14	5	ND	2	66	.6	2	2	96	.84	.111	8	31	.99	188	.12	9	1.95	.06	.16	1	12
STANDARD C/AU-S	20	56	40	137	7.3	74	33	1094	3.89	42	19	8	40	52	18.6	18	19	61	.50	.094	40	59	.97	183	.08	32	1.95	.06	.14	11	45
STANDARD C	19	57	40	132	7.1	70	34	1054	3.89	38	16	7	38	52	18.4	16	20	55	.48	.088	38	59	.83	177	.09	34	1.87	.06	.15	11	-

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

BP Resources Canada Ltd. PROJECT LOC 10161 & 10159 File # 91-3233 Page 1

700 - 890 W. Pender St., Vancouver BC V6B 4W3

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
133454	1	26	6	141	.2	13	12	321	5.39	2	5	ND	5	27	.2	2	2	157	.29	.196	7	58	.30	68	.09	2	2.82	.01	.04	1	25.1
133455	1	55	8	97	.1	19	16	287	5.50	7	5	ND	2	46	.2	2	2	141	.44	.096	6	51	.56	90	.13	2	2.53	.02	.06	1	3.7
133456	1	56	4	116	.3	17	14	327	5.94	5	5	ND	4	32	.2	2	2	144	.34	.404	6	52	.53	99	.11	2	3.44	.01	.06	1	2.9
133457	1	92	9	163	.6	20	17	527	5.32	8	5	ND	4	44	.2	2	2	113	.42	.347	7	49	.83	154	.11	4	4.07	.02	.09	1	3.2
133458	2	57	7	169	.3	17	16	391	5.93	6	5	ND	5	33	.2	2	2	153	.32	.221	9	60	.60	100	.12	2	3.27	.01	.07	1	3.1
133459	2	92	8	94	.4	18	19	342	6.70	15	5	ND	2	34	.2	2	2	163	.40	.128	7	47	.68	129	.13	4	3.48	.02	.10	1	86.0
133460	1	56	4	72	.1	32	15	343	3.47	6	5	ND	2	57	.2	2	2	74	.55	.097	10	43	.78	140	.12	5	2.10	.02	.06	1	6.1
133461	2	39	11	61	.2	24	12	249	3.48	7	6	ND	2	38	.2	2	2	76	.34	.116	7	38	.48	95	.10	3	2.04	.01	.05	1	2.6
133462	1	32	7	67	.1	25	12	243	2.87	2	5	ND	1	44	.2	2	2	62	.39	.097	9	40	.57	106	.11	5	1.98	.01	.04	1	16.3
133463	1	38	7	56	.2	30	12	238	3.38	6	6	ND	2	41	.2	2	2	75	.49	.080	8	41	.57	110	.10	5	1.92	.02	.06	1	9.6
133464	1	28	3	43	.1	18	8	212	2.23	2	5	ND	1	45	.2	2	2	57	.48	.050	8	29	.52	85	.11	5	1.49	.02	.03	1	8.6
133465	1	36	6	41	.1	20	10	298	2.57	3	5	ND	2	67	.2	2	2	66	.68	.081	10	35	.65	95	.14	6	1.42	.02	.04	1	5.7
133466	1	25	2	39	.1	18	8	255	2.26	2	5	ND	1	52	.2	2	2	56	.67	.081	9	31	.61	71	.12	5	1.22	.02	.04	1	7.4
133467	1	19	4	39	.1	15	8	246	2.02	2	5	ND	1	54	.2	2	2	55	.61	.053	8	27	.55	67	.13	5	1.20	.02	.04	1	5.5
133468	1	21	4	46	.1	13	8	333	2.43	2	5	ND	1	54	.2	2	2	60	.64	.047	8	28	.68	81	.10	6	1.43	.02	.04	1	6.7
133469	1	27	3	44	.1	23	9	319	2.58	2	5	ND	2	53	.2	2	2	61	.68	.085	12	39	.68	84	.13	5	1.24	.02	.05	1	7.4
133470	1	26	5	46	.1	24	9	263	2.52	2	5	ND	2	47	.2	2	2	59	.61	.083	11	38	.68	72	.12	5	1.37	.02	.05	1	4.7
133471	1	27	4	49	.1	25	10	257	2.75	3	5	ND	1	45	.2	2	2	66	.54	.075	10	41	.66	83	.11	5	1.50	.02	.05	1	4.7
133472	1	34	4	47	.1	26	9	266	2.58	2	5	ND	2	53	.2	2	2	57	.59	.090	10	39	.66	84	.11	6	1.53	.02	.05	1	3.3
133473	1	67	5	39	.1	29	10	328	2.58	5	5	ND	3	49	.2	2	2	59	.58	.093	12	46	.66	76	.12	6	1.22	.02	.05	1	12.5
133474	2	75	5	89	.2	29	22	595	9.28	16	5	ND	2	135	.2	2	2	307	.73	.136	10	108	.84	225	.16	4	1.79	.02	.10	1	8.0
133475	1	23	4	58	.1	24	12	412	3.01	3	5	ND	1	46	.2	2	3	71	.54	.066	9	47	.61	76	.11	5	1.29	.02	.06	1	11.4
133476	1	49	5	65	.1	33	11	452	3.17	6	5	ND	1	53	.2	2	2	67	.62	.075	12	52	.73	112	.08	6	1.77	.02	.05	1	4.7
133477	1	25	4	51	.1	20	8	242	2.83	15	5	ND	2	59	.2	2	2	76	.84	.152	12	41	.65	106	.10	4	1.27	.02	.04	1	54.1
133478	1	37	3	62	.1	20	15	939	3.97	5	5	ND	3	49	.2	2	2	93	.78	.131	7	37	.89	95	.14	5	1.56	.03	.08	1	8.5
133479	1	42	6	53	.1	16	13	407	3.76	7	5	ND	2	49	.2	2	2	89	.76	.111	6	31	.82	67	.14	7	1.67	.03	.07	1	5.0
133480	1	22	2	47	.1	12	10	326	3.39	7	5	ND	1	69	.2	2	2	95	.84	.043	6	30	.71	65	.16	8	1.37	.03	.07	1	3.2
133481	6	49	3	99	.1	21	20	632	9.26	17	5	ND	2	67	.2	2	2	165	.88	.094	8	36	1.13	113	.14	2	2.22	.02	.07	1	3.2
133482	1	46	7	67	.1	16	10	261	2.98	2	5	ND	2	48	.2	2	2	74	.58	.099	8	36	.59	99	.12	6	2.04	.02	.06	1	10.8
133483	1	50	4	73	.1	19	12	341	3.12	2	5	ND	2	65	.2	2	2	92	.83	.105	11	41	.71	115	.14	6	1.67	.02	.06	1	4.6
133484	1	57	2	75	.1	21	14	505	4.19	5	5	ND	1	64	.2	2	2	116	.90	.120	13	54	.70	119	.12	6	1.77	.02	.05	1	5.3
RE 133480	1	21	2	44	.1	12	9	315	3.24	3	5	ND	1	67	.2	2	2	90	.80	.041	5	29	.68	64	.16	7	1.31	.03	.07	1	2.3
133485	1	65	7	96	.2	27	18	481	4.04	6	5	ND	3	64	.2	2	2	154	.96	.120	12	68	.93	111	.16	6	1.80	.02	.06	1	4.5
134513	1	49	7	104	.1	18	18	322	4.97	4	5	ND	4	36	.2	2	2	123	.39	.067	10	49	.48	120	.12	2	2.72	.01	.07	1	1.3
134514	1	64	3	89	.2	12	14	362	5.88	3	5	ND	2	27	.2	2	2	152	.31	.208	4	41	.41	95	.03	2	2.98	.01	.08	1	33.3
134515	1	50	3	163	.2	15	16	398	5.67	3	5	ND	3	27	.3	2	2	150	.35	.247	7	50	.51	92	.09	5	3.37	.01	.07	1	4.3
134516	1	47	4	108	.1	14	14	279	6.29	7	5	ND	3	24	.2	2	3	164	.26	.256	7	51	.51	76	.08	5	3.19	.01	.06	1	2.2
STANDARD C/AU-S	19	63	38	133	7.3	68	34	1045	3.99	41	16	6	39	53	18.4	15	18	58	.50	.089	39	58	.88	186	.10	36	1.97	.06	.15	13	49.2
STANDARD C	18	57	36	133	7.5	71	31	1048	3.99	41	18	7	39	52	18.4	16	20	55	.48	.091	38	58	.89	176	.09	33	1.89	.06	.15	11	-

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: SOIL AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE. Samples beginning 'RE' are duplicate samples.

DATE RECEIVED: AUG 7 1991 DATE REPORT MAILED: Aug 12/91. SIGNED BY ..... D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

ACME ANALYTICAL

BP Resources Canada Ltd. PROJECT LOC 10161 & 10159 FILE # 91-3233

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
134517	1	75	2	78	.1	10	19	799	3.96	2	5	ND	1	26	.2	2	2	212	.89	.148	11	23	1.48	106	.24	2	2.40	.01	.15	1	1.7
134518	1	57	2	81	.2	20	15	430	6.41	5	5	ND	2	33	.2	2	2	226	.42	.295	6	76	.51	84	.14	5	2.42	.01	.07	1	6.3
134519	1	46	4	110	.1	21	16	443	7.52	8	5	ND	2	30	.2	2	2	277	.35	.313	7	91	.46	85	.14	3	2.78	.01	.06	1	73.9
134520	1	57	4	86	.3	19	16	382	7.54	9	5	ND	2	38	.2	2	2	246	.51	.285	6	76	.58	95	.15	3	2.27	.02	.07	1	93.5
134521	1	64	3	53	.1	17	11	557	3.65	4	5	ND	1	57	.2	2	2	112	.82	.125	11	46	.59	91	.13	3	1.56	.02	.06	1	17.8
134522	1	39	2	57	.1	15	12	460	3.92	3	5	ND	1	48	.2	2	2	122	.59	.135	7	47	.48	98	.15	3	1.63	.02	.06	1	10.9
134523	1	54	3	54	.1	17	13	562	3.59	4	5	ND	1	57	.2	2	2	107	.76	.119	12	46	.58	81	.11	4	1.67	.02	.06	1	4.1
134524	1	68	4	57	.1	18	14	729	3.67	4	5	ND	1	59	.2	2	2	100	.75	.115	15	43	.59	100	.10	5	1.91	.02	.06	1	6.3
RE 134529	1	55	4	43	.1	16	12	386	3.36	2	5	ND	1	54	.2	2	2	104	.79	.127	9	37	.56	80	.15	3	1.63	.02	.05	1	3.9
134525	1	50	2	63	.1	18	16	477	4.47	5	5	ND	1	47	.2	2	2	143	.62	.122	9	53	.55	127	.14	3	1.68	.02	.06	1	2.9
1[illegible]26	1	103	3	52	.1	17	17	1206	3.44	3	5	ND	1	62	.2	2	2	98	.91	.105	12	37	.69	97	.16	2	1.58	.03	.07	1	7.4
134527	1	75	5	65	.1	16	14	418	5.24	8	5	ND	2	44	.2	2	2	161	.58	.195	9	48	.59	141	.10	2	1.83	.02	.07	1	40.0
134528	1	38	2	91	.1	16	10	318	3.75	4	5	ND	1	49	.2	2	2	114	.74	.138	9	39	.50	78	.14	2	1.62	.02	.05	1	6.4
134529	1	55	4	44	.1	16	12	381	3.38	2	5	ND	1	53	.2	2	2	104	.80	.133	9	37	.57	83	.15	2	1.63	.02	.05	1	5.8
134530	1	73	3	57	.1	17	12	436	2.76	2	5	ND	2	52	.2	2	2	77	.65	.035	11	38	.54	70	.18	3	1.59	.02	.05	1	6.7
134531	1	32	3	38	.1	30	10	321	2.85	5	5	ND	2	52	.2	2	2	75	.65	.066	13	51	.64	88	.14	2	1.21	.03	.06	1	10.2
134532	1	31	3	37	.1	29	11	319	2.90	5	5	ND	2	43	.2	2	2	75	.61	.085	10	44	.58	93	.11	3	1.32	.02	.04	1	14.7
134533	1	23	5	51	.1	33	11	270	2.80	2	5	ND	2	45	.2	2	2	66	.53	.134	11	44	.65	98	.11	4	1.51	.02	.05	1	4.5
134534	1	20	2	34	.1	25	9	340	2.40	2	5	ND	2	51	.2	2	2	59	.64	.097	13	43	.65	70	.15	3	1.07	.03	.05	1	5.2
134535	1	26	2	34	.1	22	9	341	2.37	2	5	ND	2	46	.2	2	2	67	.61	.080	12	40	.59	68	.14	2	1.08	.02	.04	1	2.4
134536	1	28	2	57	.1	24	10	355	2.54	2	5	ND	1	48	.2	2	2	71	.62	.060	10	42	.58	84	.12	2	1.33	.02	.05	1	1.0
134537	1	30	2	46	.1	28	9	238	2.39	2	5	ND	2	46	.2	2	2	60	.55	.088	12	39	.60	91	.12	2	1.46	.02	.05	1	1.4
134538	1	31	4	56	.1	27	9	265	2.60	2	5	ND	1	42	.2	2	2	62	.45	.084	10	41	.50	122	.09	2	1.92	.02	.06	1	8.3
134539	1	30	3	44	.1	31	11	263	3.01	5	5	ND	2	40	.2	2	2	70	.42	.085	9	43	.60	101	.11	4	1.84	.02	.06	1	3.2
134540	1	24	2	31	.1	21	8	231	2.16	2	5	ND	2	49	.2	2	2	58	.60	.075	12	33	.57	86	.12	2	1.26	.02	.04	1	5.2
134541	1	22	5	41	.1	18	9	189	2.78	3	5	ND	3	37	.2	2	2	77	.40	.047	8	37	.39	73	.11	2	1.54	.02	.04	1	8.8
134542	1	19	5	49	.2	18	9	253	3.47	4	5	ND	2	37	.2	2	2	87	.35	.208	8	41	.40	76	.10	2	1.76	.02	.05	1	3.3
134543	2	52	8	86	.3	27	19	332	5.99	13	5	ND	3	39	.2	3	2	132	.37	.227	9	44	.67	123	.16	3	3.12	.02	.07	1	21.6
[illegible]544	1	26	2	41	.1	13	9	297	2.85	5	5	ND	2	48	.2	2	2	64	.73	.083	6	21	.64	60	.13	4	1.19	.05	.10	1	.8
[illegible]45	1	22	3	29	.1	22	8	245	2.11	2	5	ND	2	46	.2	2	2	53	.54	.074	12	36	.55	78	.12	3	.93	.02	.05	1	4.2
134546	1	66	6	94	.1	80	17	665	4.03	11	5	ND	4	58	.2	3	2	71	.66	.067	15	77	1.26	199	.17	3	2.25	.03	.16	1	4.8
134547	1	107	9	110	.3	40	17	688	4.40	12	5	ND	2	107	.3	2	2	104	1.26	.120	13	55	1.13	171	.17	3	2.06	.04	.12	1	4.8
134548	1	57	6	114	.2	29	16	504	4.02	7	5	ND	1	71	.2	2	2	106	.95	.107	8	49	.92	122	.17	3	1.79	.03	.14	1	2.3
134549	1	45	6	51	.2	38	12	443	2.96	6	5	ND	3	56	.2	2	2	68	.73	.086	14	56	.88	107	.17	3	1.43	.03	.08	1	4.0
134550	1	51	6	40	.2	32	10	343	2.86	9	5	ND	2	59	.2	2	2	70	.74	.104	14	46	.64	112	.10	2	1.28	.02	.06	1	4.5
134551	1	25	2	61	.2	29	11	327	2.88	4	5	ND	2	48	.2	2	2	69	.50	.100	10	45	.67	100	.11	3	1.67	.02	.07	1	1.2
134552	1	32	4	44	.3	32	11	260	3.18	7	5	ND	2	41	.2	2	2	76	.42	.084	10	44	.59	84	.14	3	1.81	.02	.06	1	4.1
STANDARD C/AU-S	19	64	42	134	7.5	71	33	1089	4.01	42	20	8	41	53	19.0	18	18	60	.51	.093	39	59	.89	179	.10	35	1.99	.07	.17	11	46.7
STANDARD C	18	57	44	133	7.4	71	33	1049	3.99	43	19	7	38	52	17.0	16	18	60	.50	.089	39	58	.87	180	.09	34	1.90	.06	.15	12	-

Samples beginning 'RE' are duplicate samples.

ACME ANALYTICAL

BP Resources Canada Ltd. PROJECT LOC 10161 & 10159 FILE # 91-3233

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
134553	1	60	7	102	.1	21	12	369	4.74	12	5	ND	9	43	.2	2	2	122	.46	.224	7	51	.53	102	.10	2	2.24	.01	.07	4	2.3
134554	1	34	5	56	.4	23	8	262	3.29	10	5	ND	2	36	.2	2	2	75	.37	.118	8	43	.45	91	.08	2	1.85	.01	.06	1	3.7
RE 134558	1	44	5	29	.2	16	8	266	2.37	6	5	ND	2	39	.2	2	2	60	.47	.063	7	27	.48	79	.10	2	1.24	.01	.04	2	5.6
134555	1	26	3	45	.2	32	10	315	2.47	6	5	ND	2	34	.2	2	2	50	.42	.085	10	42	.63	95	.09	3	1.47	.01	.06	1	5.5
134556	1	31	4	53	.2	21	7	302	2.33	5	5	ND	2	35	.2	2	2	50	.50	.063	9	34	.49	125	.09	2	1.40	.01	.05	1	4.1
134557	1	45	6	48	.3	22	11	282	3.41	10	5	ND	2	45	.2	2	3	73	.43	.105	7	31	.67	114	.12	4	1.99	.01	.06	2	4.3
134558	1	43	5	29	.2	17	8	260	2.35	6	5	ND	2	37	.2	2	6	59	.47	.063	7	26	.49	77	.10	2	1.19	.01	.05	1	9.1
134559	1	24	8	72	.3	10	7	305	2.54	7	5	ND	2	49	.2	2	2	63	.71	.097	9	24	.53	145	.12	3	1.03	.02	.05	1	8.4
134560	1	42	11	126	.5	19	10	407	3.81	11	5	ND	2	35	.3	3	2	93	.39	.070	7	38	.54	158	.09	2	1.80	.01	.06	3	6.5
134561	1	32	12	94	.7	19	13	486	6.00	8	5	ND	3	40	.5	2	5	190	.46	.072	8	71	.43	112	.10	2	1.29	.01	.06	1	9.6
1[illegible]62	1	36	7	69	.4	23	12	272	4.72	15	5	2	4	50	.3	2	3	124	.65	.053	12	54	.44	122	.11	2	2.38	.02	.06	1	2.8
134563	1	53	6	78	.3	24	11	495	4.77	12	5	ND	4	68	.3	2	5	122	.86	.079	11	65	.77	152	.13	2	1.63	.02	.07	1	6.1
134564	1	35	4	79	.2	21	11	290	3.78	6	5	ND	3	35	.2	2	2	92	.35	.213	7	42	.45	102	.08	2	1.86	.01	.07	1	3.6
134565	1	29	2	62	.2	24	11	314	4.07	11	5	ND	3	34	.2	2	3	104	.34	.138	8	43	.52	76	.12	2	2.20	.01	.05	1	3.4
134566	1	38	4	57	.2	25	10	257	4.23	9	5	ND	6	43	.2	2	2	111	.61	.048	7	47	.53	93	.11	2	1.86	.01	.04	1	1.8
134567	1	40	2	51	.2	31	9	223	2.95	6	5	ND	2	34	.2	2	4	65	.42	.147	8	44	.52	73	.08	2	1.52	.01	.05	1	4.4
134568	1	95	6	48	.2	52	12	512	3.48	14	5	ND	3	43	.5	3	2	81	.57	.037	12	71	.70	124	.11	2	1.34	.02	.06	2	6.9
134569	1	36	4	45	.4	36	9	361	2.84	8	5	ND	3	43	.2	2	2	62	.66	.075	11	48	.70	96	.10	2	1.06	.02	.06	1	7.7
134570	1	36	3	39	.2	26	8	244	3.84	9	5	ND	2	42	.2	2	2	105	.66	.087	11	56	.54	85	.09	2	.83	.01	.04	1	19.3
134571	1	67	11	112	.3	23	15	380	3.52	6	5	ND	3	53	.4	2	7	117	1.04	.080	11	42	1.24	154	.14	2	2.16	.02	.07	2	4.0
134572	1	37	2	59	.2	27	11	282	5.36	7	5	2	2	59	.6	2	2	176	.74	.109	9	78	.63	91	.12	2	1.03	.01	.04	1	67.8
134573	1	44	4	55	.3	18	10	517	3.49	9	5	ND	1	55	.2	2	2	86	.98	.091	10	37	.67	135	.08	2	1.75	.02	.05	1	10.9
STANDARD C/AU-S	17	62	36	133	7.3	70	32	1039	3.90	44	21	7	41	52	18.4	16	21	56	.49	.086	39	58	.88	178	.09	33	1.92	.06	.15	11	48.5

Samples beginning 'RE' are duplicate samples.

A.[illegible]E ANA[illegible]ICAL LABORATORIES LTD. 852 E. HASTINGS ST. VA[illegible]VER BC V6A 1R6 PHONE(604)253-3158 FAX(604)[illegible] 1716

GEOCHEMICAL ANALYSIS CERTIFICATE

Westley Technologies Ltd. PROJECT WIT File # 95-2103 Page 1

900 - 475 Howe St., Vancouver BC V6C 2B3 Submitted by: Colin Campbell

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppm	Au** ppb
FE L140E 99+25N	1	20	7	71	<.3	14	8	248	3.78	3	<5	<2	3	51	.2	<2	<2	92	.48	.144	8	39	.44	135	.09	6	2.30	.01	.05	<2	<5	<1	5
FE L140E 99+00N	<1	30	11	36	<.3	21	8	223	3.24	5	<5	<2	2	43	.2	2	<2	83	.37	.080	7	39	.45	144	.09	<3	1.74	.01	.04	<2	<5	<1	2
FE L140E 98+75N	<1	21	9	36	<.3	15	6	165	2.80	2	6	<2	3	27	<.2	<2	<2	69	.31	.066	7	36	.34	93	.10	3	1.78	.01	.04	<2	<5	<1	11
FE L140E 98+50N	1	19	6	59	<.3	25	10	265	3.31	4	<5	<2	2	27	.2	<2	<2	82	.38	.142	8	45	.40	89	.09	4	1.80	.01	.04	<2	<5	<1	9
FE L140E 98+25N	<1	13	5	59	<.3	14	8	374	2.85	<2	5	<2	2	29	<.2	<2	<2	79	.41	.118	7	45	.32	111	.09	6	1.17	.01	.04	<2	<5	<1	13
FE L140E 98+00N	<1	23	6	42	.3	24	8	261	3.46	5	<5	<2	3	33	.2	<2	<2	89	.48	.134	8	52	.47	117	.09	7	1.61	.01	.06	<2	<5	<1	11
FE L140E 97+75N	1	30	7	50	.3	28	11	293	4.60	7	<5	<2	2	32	.2	4	<2	110	.53	.152	6	44	.60	136	.10	<3	2.21	.01	.07	<2	<5	<1	2
FE L140E 97+50N	<1	22	7	50	<.3	27	10	287	3.61	4	<5	<2	3	31	.2	<2	<2	80	.35	.087	8	42	.56	98	.10	<3	2.34	.01	.06	<2	<5	<1	7
FE L140E 97+25N	<1	46	5	55	<.3	22	10	336	4.47	18	<5	<2	3	33	.2	<2	<2	124	.46	.202	7	48	.53	88	.09	<3	2.17	.01	.07	<2	<5	<1	3
FE L140E 97+00N	1	38	9	112	<.3	22	15	360	7.87	9	<5	<2	<2	32	.5	8	<2	275	.45	.103	6	91	.53	117	.10	<3	1.98	.01	.07	<2	<5	4	74
FE L144E 116+50N	<1	32	5	79	<.3	15	9	302	4.51	<2	<5	<2	2	44	.3	<2	<2	102	.81	.223	6	25	.79	79	.15	<3	2.94	.02	.07	<2	<5	<1	10
FE L144E 116+25N	<1	42	3	62	<.3	22	10	372	4.39	<2	<5	<2	<2	56	<.2	2	<2	125	1.14	.067	6	33	1.31	54	.28	<3	2.93	.02	.08	<2	12	1	4
FE L144E 116+00N	<1	46	7	75	<.3	14	10	338	4.55	<2	<5	<2	2	38	.3	<2	<2	115	1.24	.099	8	20	.78	43	.15	4	2.94	.02	.09	<2	<5	<1	4
FE L144E 115+75N	2	46	8	97	<.3	16	13	526	4.48	<2	<5	<2	2	44	.3	<2	<2	114	1.11	.267	7	23	1.00	61	.15	<3	3.23	.02	.09	<2	<5	1	3
FE L144E 115+50N	<1	19	5	58	<.3	12	8	319	3.42	<2	<5	<2	<2	35	.2	2	<2	101	.71	.095	7	27	.47	56	.12	<3	1.72	.01	.05	<2	<5	<1	<2
FE L144E 115+25N	<1	18	8	59	<.3	11	8	322	3.59	<2	<5	<2	2	32	.2	<2	<2	103	.62	.123	6	33	.39	78	.11	6	1.60	.02	.05	<2	<5	<1	<2
FE L144E 115+00N	<1	37	3	43	<.3	13	10	444	3.92	2	<5	<2	<2	45	<.2	<2	<2	129	1.02	.080	6	16	.83	62	.19	<3	1.93	.02	.04	<2	<5	<1	<2
FE L144E 114+75N	1	17	6	38	<.3	7	4	186	2.52	<2	<5	<2	<2	41	<.2	<2	2	87	.67	.030	6	24	.33	38	.13	<3	1.23	.01	.04	<2	<5	3	4
FE L144E 114+50N	1	36	7	54	.5	13	9	537	3.15	<2	7	<2	2	38	<.2	<2	<2	88	.62	.097	10	31	.52	55	.12	5	1.92	.01	.05	<2	<5	<1	14
FE L144E 114+25N	<1	28	5	40	.3	14	7	397	3.22	<2	<5	<2	2	51	<.2	<2	<2	95	.85	.086	8	37	.55	56	.14	6	1.45	.02	.05	<2	<5	<1	8
RE FE L144E 114+25N	<1	30	4	43	<.3	16	7	415	3.38	2	<5	<2	2	54	<.2	<2	<2	102	.90	.088	8	32	.59	61	.14	<3	1.53	.02	.05	<2	<5	<1	4
FE L144E 114+00N	<1	14	8	45	<.3	9	5	491	3.25	<2	<5	<2	<2	47	<.2	<2	<2	107	.73	.046	6	39	.30	104	.14	6	1.26	.01	.04	<2	<5	<1	3
FE L144E 113+75N	<1	34	4	38	.3	14	7	352	2.94	2	8	<2	2	55	<.2	<2	<2	91	.74	.065	10	35	.60	63	.15	6	1.59	.02	.04	<2	<5	<1	3
FE L144E 113+50N	<1	31	6	43	<.3	17	9	370	3.29	<2	<5	<2	2	39	<.2	<2	<2	94	.73	.074	8	39	.48	72	.12	4	1.66	.01	.04	<2	<5	<1	3
FE L144E 113+25N	<1	18	8	61	<.3	13	6	244	3.56	4	5	<2	<2	33	.2	<2	<2	96	.49	.203	6	39	.36	65	.11	3	1.51	.01	.05	<2	<5	<1	2
FE L144E 113+00N	<1	18	7	43	<.3	11	5	286	2.91	<2	5	<2	<2	34	<.2	<2	<2	88	.50	.061	6	41	.31	51	.11	4	1.36	.01	.04	<2	<5	<1	<2
FE L144E 112+75N	<1	25	9	63	.3	13	7	334	3.89	4	<5	<2	2	26	.2	<2	<2	101	.39	.154	6	35	.40	75	.09	6	1.87	.01	.06	<2	<5	<1	3
FE L144E 112+50N	<1	29	11	104	<.3	16	9	261	4.26	3	<5	<2	2	29	.2	2	<2	107	.40	.104	8	33	.54	74	.12	3	2.11	.01	.06	<2	<5	<1	<2
FE L144E 112+25N	<1	36	11	83	<.3	17	11	486	4.58	4	<5	<2	<2	48	.4	2	<2	113	.84	.157	5	30	.55	144	.11	<3	2.06	.01	.08	<2	<5	<1	<2
FE L144E 111+75N	<1	55	9	100	.4	11	10	321	3.27	<2	6	<2	<2	85	.4	<2	<2	93	1.44	.102	9	26	.27	128	.06	6	2.51	.01	.04	<2	<5	<1	12
FE L144E 111+50N	1	16	10	59	<.3	7	4	388	3.23	<2	<5	<2	<2	34	.2	2	<2	121	.47	.041	6	33	.15	86	.11	<3	.94	.01	.06	<2	<5	1	3
FE L144E 111+25N	<1	22	9	43	<.3	11	6	330	2.46	3	<5	<2	<2	43	<.2	<2	<2	77	.57	.066	7	26	.47	86	.12	5	1.28	.01	.07	<2	<5	<1	4
FE L145E 116+50N	<1	38	7	53	<.3	22	12	328	4.69	2	<5	<2	<2	35	.2	<2	<2	134	.65	.056	6	30	.67	97	.17	<3	3.32	.02	.08	<2	<5	1	3
FE L145E 116+25N	1	15	7	62	<.3	10	7	522	3.56	<2	<5	<2	<2	28	<.2	<2	<2	105	.63	.152	4	24	.37	80	.13	<3	1.82	.01	.05	<2	<5	<1	2
FE L145E 116+00N	<1	28	7	76	<.3	15	8	336	3.82	3	<5	<2	<2	31	.3	2	<2	102	.57	.169	6	25	.52	60	.12	<3	2.19	.01	.07	<2	<5	<1	2
STANDARD C/AU-S	19	57	39	124	7.0	70	32	1094	4.03	38	19	6	37	50	18.3	15	20	59	.50	.093	40	62	.90	174	.08	29	1.92	.07	.17	10	<5	1	44

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL.
- SAMPLE TYPE: SOIL AU** ANALYSIS BY FA/ICP FROM 30 GM SAMPLE.
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUL 4 1995 DATE REPORT MAILED: July 11/95 SIGNED BY C. Leong .D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

18 Appendix 18

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppm	Au** ppb
FE L145E 115+75N	<1	41	8	131	<.3	13	12	1094	3.73	<2	<5	<2	<2	43	<.2	2	<2	102	1.02	.193	6	11	.81	141	.09	3	2.87	.02	.08	<2	<5	1	4
FE L145E 115+50N	<1	29	6	36	<.3	13	7	278	3.17	2	<5	<2	2	44	<.2	<2	<2	104	.69	.095	7	34	.49	56	.13	6	1.44	.02	.05	<2	<5	<1	4
FE L145E 115+25N	<1	40	9	42	<.3	18	8	291	3.54	4	<5	<2	<2	51	<.2	<2	<2	106	.78	.176	9	33	.59	72	.15	<3	1.91	.01	.05	<2	<5	<1	4
FE L145E 115+00N	<1	27	6	50	<.3	13	8	282	3.36	4	<5	<2	<2	44	<.2	<2	<2	98	.84	.078	6	30	.42	59	.12	<3	1.57	.01	.04	<2	<5	<1	2
FE L145E 114+75N	1	148	6	42	.7	24	9	644	3.56	4	<5	<2	<2	66	.4	2	<2	102	1.60	.054	14	36	.61	73	.10	6	1.76	.02	.05	<2	<5	<1	3
FE L145E 114+50N	1	224	14	80	.8	39	16	1842	5.27	8	<5	<2	<2	68	.6	<2	<2	129	1.53	.112	27	47	.84	152	.08	3	2.79	.02	.07	<2	<5	2	7
FE L145E 114+25N	1	23	7	45	<.3	14	6	184	3.32	6	<5	<2	<2	39	<.2	<2	<2	93	.60	.276	7	33	.41	79	.10	<3	1.60	.01	.04	<2	<5	<1	3
FE L145E 114+00N	<1	23	6	51	<.3	15	7	222	3.54	5	<5	<2	<2	37	<.2	<2	<2	104	.52	.164	7	41	.41	70	.12	4	1.33	.01	.05	<2	<5	<1	2
FE L145E 113+75N	1	115	10	59	.3	38	12	680	4.70	7	5	<2	<2	61	<.2	<2	<2	119	.97	.073	22	57	.75	140	.11	<3	2.85	.02	.10	<2	<5	<1	6
RE FE L145E 113+75N	<1	122	5	62	.5	40	13	713	4.84	11	8	<2	2	64	<.2	2	<2	122	1.02	.078	23	59	.79	148	.11	3	2.95	.02	.11	<2	<5	<1	9
FE L145E 113+50N	<1	28	7	69	<.3	13	8	761	3.17	<2	<5	<2	<2	39	<.2	<2	<2	96	.77	.054	9	34	.44	68	.12	7	1.52	.01	.05	<2	<5	<1	3
FE L145E 113+25N	1	81	9	47	<.3	18	7	416	3.66	3	<5	<2	<2	66	<.2	<2	<2	102	1.53	.057	8	36	.66	82	.10	<3	1.77	.02	.06	<2	<5	<1	5
FE L145E 113+00N	<1	66	4	72	<.3	17	10	392	4.42	6	<5	<2	<2	90	<.2	<2	<2	111	1.66	.091	10	26	.79	98	.10	<3	2.35	.02	.06	<2	<5	<1	<2
FE L145E 112+00N	<1	18	9	50	<.3	4	2	159	1.99	<2	<5	<2	<2	27	<.2	2	<2	74	.36	.028	7	17	.12	88	.09	<3	.69	.01	.05	<2	<5	<1	3
FE L145E 111+75N	2	25	11	69	<.3	17	5	245	3.47	5	<5	<2	<2	28	<.2	<2	<2	97	.34	.127	8	43	.48	92	.09	<3	1.95	.01	.05	<2	<5	<1	2
FE L145E 111+50N	<1	22	6	34	<.3	10	4	148	2.56	5	<5	<2	<2	36	<.2	<2	<2	83	.45	.050	8	27	.35	74	.10	<3	1.49	.01	.03	<2	<5	<1	8
WL L145E 116+50N	1	22	6	46	<.3	11	7	198	2.59	<2	5	<2	<2	32	<.2	<2	<2	77	.38	.047	6	21	.48	95	.08	4	1.49	.01	.07	<2	<5	<1	3
WL L145E 116+25N	1	41	7	78	<.3	18	13	432	3.28	5	<5	<2	<2	37	<.2	2	<2	89	.43	.067	8	27	.58	89	.11	<3	1.99	.02	.07	<2	<5	<1	4
WL L145E 116+00N	1	41	8	42	<.3	22	8	214	3.05	5	<5	<2	2	38	<.2	<2	2	82	.43	.064	9	38	.53	96	.12	<3	1.71	.02	.06	<2	<5	<1	7
WL L145E 115+75N	1	60	12	51	<.3	21	9	332	3.59	5	<5	<2	<2	43	<.2	<2	<2	95	.58	.054	11	34	.58	104	.09	<3	2.21	.02	.08	<2	<5	<1	5
WL L145E 114+50N	1	38	8	70	<.3	32	9	303	2.52	<2	<5	<2	2	55	<.2	<2	2	61	.66	.082	14	45	1.04	184	.13	<3	1.82	.02	.06	<2	<5	<1	4
WL L145E 113+00N	1	37	11	413	<.3	22	8	419	2.77	3	<5	<2	<2	55	2.2	<2	<2	70	.60	.062	10	36	.64	203	.10	<3	1.61	.02	.05	<2	<5	<1	5
WL L145E 112+75N	<1	24	11	890	<.3	16	7	249	4.07	7	<5	<2	<2	36	2.0	<2	<2	98	.34	.113	8	38	.52	176	.12	<3	2.02	.01	.05	<2	<5	<1	4
WL L145E 112+50N	1	34	9	253	<.3	19	8	285	4.70	9	<5	<2	<2	31	.7	<2	<2	103	.34	.277	8	42	.58	107	.09	<3	2.09	.01	.06	<2	<5	<1	<2
WL L146E 115+75N	<1	33	6	65	<.3	20	7	277	2.42	3	<5	<2	<2	36	<.2	2	<2	60	.45	.060	9	31	.59	86	.12	<3	1.57	.02	.05	<2	<5	<1	6
WL L146E 115+50N	<1	53	7	66	<.3	23	10	723	3.11	4	<5	<2	<2	42	<.2	<2	2	76	.48	.080	12	38	.63	148	.10	<3	2.01	.02	.06	<2	<5	<1	4
WL L146E 114+75N	<1	30	9	93	<.3	18	8	307	3.00	5	<5	<2	<2	30	.2	<2	<2	73	.40	.067	9	29	.51	104	.07	<3	1.78	.01	.06	<2	<5	<1	2
WL L146E 114+50N	1	19	10	89	<.3	9	6	258	3.68	4	<5	<2	<2	23	<.2	<2	<2	97	.28	.115	6	26	.38	142	.05	<3	1.82	.01	.06	<2	<5	<1	2
WL L146E 114+25N	1	59	18	84	<.3	27	14	401	4.79	11	<5	<2	<2	31	<.2	2	<2	111	.36	.096	7	51	.99	153	.08	<3	2.81	.01	.07	<2	<5	<1	3
WL L146E 114+00N	3	48	8	71	<.3	14	12	603	4.91	7	7	<2	<2	26	<.2	<2	<2	117	.44	.070	5	21	.94	103	.10	<3	2.59	.01	.12	<2	<5	<1	<2
WL L146E 113+75N	1	51	3	80	.3	6	15	1177	5.14	2	6	<2	<2	20	.2	<2	2	110	.53	.094	7	4	1.04	82	.01	<3	2.67	.01	.18	<2	<5	<1	<2
WL L146E 113+50N	3	36	18	114	<.3	13	12	992	4.47	5	<5	<2	<2	57	<.2	3	<2	91	.98	.060	5	24	.81	149	.02	<3	2.15	.01	.09	<2	<5	<1	2
WL L146E 113+00N	<1	16	6	146	<.3	12	4	235	1.77	2	<5	<2	<2	34	.2	<2	3	53	.45	.031	8	28	.42	95	.10	<3	1.49	.01	.03	<2	<5	<1	3
WL L146E 112+75N	<1	17	35	288	<.3	11	5	405	2.56	5	<5	<2	<2	29	.7	<2	<2	71	.32	.093	8	30	.39	101	.11	<3	1.63	.01	.04	<2	<5	<1	6
WL L146E 112+50N	4	24	601	1461	10.0	14	6	375	3.34	12	5	<2	<2	30	2.8	3	3	76	.37	.103	9	49	.48	431	.09	<3	2.03	.01	.04	<2	<5	1	84
STANDARD C/AU-S	19	60	36	128	7.2	73	30	1002	4.19	41	20	7	38	53	18.8	17	19	63	.52	.095	42	63	.91	177	.09	27	2.00	.07	.17	9	<5	1	50

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppm	Au** ppb
WL L147E 115+00N	1	60	17	143	.3	17	12	560	4.39	15	<5	<2	<2	27	.4	<2	<2	101	.48	.112	8	31	.86	180	.05	8	2.25	.01	.08	<2	<5	<1	5
WL L147E 114+75N	<1	51	14	101	<.3	24	13	397	3.94	8	<5	<2	<2	28	<.2	<2	<2	92	.35	.116	9	38	.81	153	.09	<3	2.37	.02	.06	<2	<5	<1	6
WL L147E 114+50N	1	41	15	89	.5	17	10	336	3.72	5	7	<2	4	24	<.2	<2	<2	94	.32	.128	7	41	.70	156	.06	14	2.26	.01	.05	<2	<5	<1	2
WL L147E 114+25N	3	43	7	102	<.3	15	11	686	3.24	3	<5	<2	<2	40	<.2	<2	<2	83	.67	.037	9	20	.50	70	.07	<3	2.75	.01	.04	<2	<5	<1	<2
WL L147E 114+00N	1	23	10	70	<.3	15	9	325	3.64	3	<5	<2	2	25	<.2	<2	<2	97	.31	.061	8	32	.58	83	.06	8	2.17	.01	.05	<2	<5	<1	<2
WL L147E 113+25N	<1	26	17	331	<.3	14	11	378	3.96	7	<5	<2	2	23	.5	<2	<2	100	.30	.052	7	35	.51	107	.07	6	2.02	.01	.05	<2	<5	<1	2
WL L147E 113+00N	<1	31	31	860	<.3	17	10	491	3.90	5	<5	<2	<2	27	1.3	<2	<2	100	.46	.132	8	33	.70	185	.10	3	2.19	.01	.05	3	<5	<1	10
WL L147E 112+75N	2	38	305	1295	.7	28	9	414	3.52	7	<5	<2	2	32	1.1	<2	<2	78	.47	.103	9	42	.76	220	.10	10	2.45	.01	.04	4	<5	<1	15
WL L147E 112+50N	<1	26	202	1310	<.3	21	11	717	3.72	7	<5	<2	<2	29	2.3	<2	<2	98	.44	.051	8	51	.61	289	.10	5	1.99	.01	.06	4	<5	<1	14
W-01	1	50	34	84	.9	14	13	389	4.53	23	<5	<2	<2	22	<.2	<2	<2	99	.23	.054	7	28	.47	86	.06	5	2.17	.01	.08	<2	<5	<1	8
W-02	<1	60	10	72	.3	23	11	421	4.74	15	<5	<2	<2	33	<.2	2	<2	109	.42	.089	9	45	.71	146	.07	5	1.91	.02	.08	<2	<5	<1	2
W-03	1	40	23	118	.3	21	10	375	3.52	7	<5	<2	2	47	<.2	<2	<2	96	.53	.083	12	39	.59	161	.11	9	1.65	.02	.04	<2	<5	<1	6
W-04	<1	39	26	89	<.3	19	10	526	3.36	7	<5	<2	<2	49	<.2	<2	<2	95	.59	.101	11	37	.55	158	.10	<3	1.34	.02	.04	<2	<5	<1	8
W-05	1	59	63	131	<.3	23	12	789	3.83	8	<5	<2	2	54	<.2	3	<2	120	.69	.120	12	39	.58	240	.11	<3	1.17	.02	.06	<2	<5	<1	9
RE W-05	1	58	64	129	<.3	22	12	766	3.72	7	<5	<2	<2	54	.2	2	2	116	.69	.121	13	40	.58	227	.10	<3	1.15	.02	.05	<2	<5	<1	8
W-06	<1	17	36	395	.4	19	10	443	3.43	5	8	<2	3	30	.9	2	2	93	.38	.072	8	39	.55	230	.10	7	1.65	.01	.06	<2	<5	<1	2
W-07	1	38	47	174	<.3	28	10	388	3.38	7	<5	<2	<2	39	.3	<2	<2	93	.53	.080	9	41	.64	225	.12	<3	1.63	.02	.06	<2	<5	<1	5
W-08	2	75	129	331	.3	32	13	840	3.84	10	<5	<2	2	47	.7	<2	<2	100	.66	.095	13	59	.85	337	.13	4	1.66	.02	.08	<2	<5	<1	8
STANDARD C/AU-S	17	55	37	122	7.0	74	32	1112	4.00	39	20	7	36	48	17.7	18	20	63	.49	.091	42	62	.88	180	.08	34	1.86	.06	.16	12	<5	2	45

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

Westley Technologies Ltd. PROJECT WIT File # 95-2197 Page 1

900 - 475 Howe St., Vancouver BC V6C 2B3 Submitted by: Colin Campbell

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppm	Au** ppb
C L114E 96+00N	1	30	4	37	.3	19	6	194	3.48	2	7	<2	3	34	.9	<2	4	128	.41	.076	7	41	.42	88	.10	<3	1.45	.01	.03	<2	<5	<1	47
C L114E 95+75N	1	31	7	44	<.3	14	8	246	3.73	5	6	<2	4	29	.8	<2	4	135	.44	.104	7	39	.36	73	.08	<3	1.34	.01	.05	<2	<5	<1	9
C L114E 95+50N	1	27	<3	28	<.3	15	5	189	2.60	2	8	<2	4	33	.2	<2	4	90	.42	.072	7	32	.38	65	.09	<3	1.13	.01	.04	<2	<5	<1	12
C L114E 95+25N	1	24	7	29	.3	13	6	224	2.75	5	6	<2	3	31	.5	<2	4	99	.38	.062	7	33	.34	70	.08	<3	1.31	.01	.03	<2	<5	<1	8
C L114E 95+00N	<1	31	7	33	.3	27	7	317	2.53	5	12	<2	3	38	.5	<2	2	76	.50	.081	10	42	.48	84	.10	<3	.94	.01	.06	<2	<5	<1	8
C L114E 94+75N	2	51	5	53	<.3	24	11	513	3.16	6	<5	<2	2	37	1.1	<2	3	93	.54	.037	6	38	.50	166	.07	<3	1.56	.01	.06	<2	<5	<1	3
C L114E 94+50N	2	145	35	201	.3	5	10	866	3.87	24	<5	<2	2	36	1.7	<2	<2	61	.74	.095	7	11	.09	583	<.01	<3	1.19	.01	.08	<2	<5	<1	9
C L114E 94+25N	2	131	30	216	.3	6	7	626	4.46	29	<5	<2	2	34	1.9	<2	3	56	.65	.178	9	11	.12	509	.01	3	1.21	.01	.10	<2	<5	<1	3
C L114E 93+75N	1	25	8	54	.3	34	11	290	4.66	5	<5	<2	4	28	.9	<2	4	146	.35	.208	6	57	.42	132	.08	<3	1.65	.01	.05	<2	<5	<1	34
C L114E 93+50N	1	21	6	46	.3	25	8	320	2.71	<2	6	<2	2	28	.6	<2	3	80	.36	.103	6	47	.39	73	.08	<3	1.17	.01	.07	<2	<5	<1	5
C L114E 93+00N	1	19	7	48	.3	13	4	223	1.81	3	<5	<2	<2	33	.4	<2	3	60	.38	.035	9	32	.32	99	.08	<3	1.04	.01	.04	<2	<5	<1	5
C L114E 92+75N	<1	37	5	43	.3	32	9	206	2.89	5	6	<2	3	27	.7	<2	2	82	.35	.097	7	46	.48	79	.08	<3	1.44	.01	.05	<2	<5	<1	4
C L114E 92+50N	2	58	7	71	.3	29	12	314	5.37	15	13	<2	13	32	.9	<2	2	159	.36	.229	7	52	.61	94	.11	<3	2.43	.01	.07	<2	<5	<1	15
C L114E 92+25N	1	28	7	126	.3	16	9	317	3.77	4	6	<2	5	27	.8	<2	3	106	.34	.231	8	41	.42	92	.08	<3	1.92	.01	.06	<2	<5	<1	72
C L114E 92+00N	1	40	11	129	.5	24	11	323	4.81	3	8	<2	6	32	1.0	<2	4	131	.41	.335	9	47	.63	122	.10	<3	2.52	.01	.07	<2	<5	<1	7
C L114E 91+75N	1	41	8	137	.6	22	14	371	5.17	11	8	<2	5	34	.6	<2	4	155	.39	.284	6	52	.57	123	.10	<3	2.61	.01	.07	<2	<5	<1	5
C L114E 91+50N	1	30	8	90	.3	24	11	345	4.33	5	<5	<2	4	29	.8	<2	2	126	.40	.248	7	50	.49	94	.09	<3	2.18	.01	.06	<2	<5	<1	<2
RE C L114E 91+50N	1	31	7	88	.4	23	11	334	4.23	9	<5	<2	4	28	.7	<2	<2	121	.38	.244	7	46	.47	95	.08	<3	2.13	.01	.05	<2	<5	<1	8
C L114E 91+25N	1	27	4	77	.3	18	9	345	4.45	6	<5	<2	2	27	.7	<2	3	137	.32	.166	7	46	.33	80	.08	<3	1.92	.01	.04	<2	<5	<1	10
C L114E 91+00N	1	33	13	122	.4	24	13	1198	5.18	10	5	<2	5	39	.7	<2	2	164	.40	.315	8	56	.54	140	.09	<3	2.49	.01	.06	<2	<5	<1	8
C L114E 90+75N	1	27	5	159	.4	20	14	370	4.60	6	<5	<2	5	28	1.2	2	2	122	.34	.281	8	44	.50	113	.09	<3	2.94	.01	.06	<2	<5	<1	4
C L114E 90+50N	1	36	11	60	.3	31	12	400	4.83	13	7	<2	4	31	.9	<2	2	156	.39	.200	8	56	.52	95	.10	<3	2.21	.01	.04	<2	<5	<1	3
C L114E 90+25N	2	104	7	88	.6	28	14	482	5.32	12	6	<2	2	58	.9	<2	2	173	.99	.089	21	50	.83	168	.14	<3	2.40	.02	.07	<2	<5	<1	<2
C L114E 90+00N	1	138	7	91	.4	34	10	366	3.31	12	6	<2	2	47	.6	<2	3	116	.80	.068	24	44	.64	138	.09	<3	2.05	.02	.05	<2	<5	<1	6
C L115E 96+00N	1	41	4	32	.3	15	4	156	2.60	3	<5	<2	<2	40	.7	<2	2	95	.61	.056	7	37	.35	100	.06	<3	1.21	.01	.02	<2	<5	<1	3
C L115E 95+75N	1	39	5	34	.3	15	5	162	2.14	2	<5	<2	<2	42	.4	<2	<2	78	.66	.049	7	35	.40	93	.06	<3	1.19	.01	.03	<2	<5	<1	17
C L115E 95+50N	<1	25	4	27	<.3	16	5	183	2.03	3	6	<2	<2	35	.5	<2	3	75	.50	.048	7	33	.45	65	.09	<3	.95	.01	.03	<2	<5	<1	7
C L115E 95+25N	1	18	<3	30	<.3	14	5	204	2.04	4	6	<2	<2	30	.3	<2	<2	71	.44	.037	7	34	.41	72	.08	<3	1.15	.01	.04	<2	<5	<1	15
C L115E 95+00N	<1	20	4	49	<.3	26	7	215	2.75	3	6	<2	3	27	.8	<2	2	82	.37	.062	7	46	.44	77	.09	<3	1.22	.01	.05	<2	<5	<1	4
C L115E 94+74N	3	117	8	68	.7	62	15	917	4.74	7	<5	<2	2	62	1.1	<2	2	103	1.07	.077	22	67	.69	258	.07	<3	3.28	.01	.09	<2	<5	<1	5
C L115E 94+00N	<1	36	3	37	<.3	28	9	386	2.57	3	7	<2	3	34	.4	<2	3	73	.48	.085	12	45	.54	86	.09	<3	.94	.02	.06	<2	<5	<1	15
C L115E 93+75N	1	16	7	42	<.3	21	7	173	2.83	2	<5	<2	2	22	.5	<2	2	78	.23	.104	8	41	.31	88	.08	<3	1.73	.01	.03	<2	<5	<1	<2
C L115E 93+50N	1	31	7	30	<.3	40	9	233	3.27	5	<5	<2	4	24	.6	<2	<2	104	.35	.078	6	53	.49	81	.08	<3	1.18	.01	.04	<2	<5	<1	3
C L115E 93+25N	1	20	5	40	<.3	23	11	332	4.26	4	<5	<2	3	26	.7	<2	2	122	.30	.251	5	54	.37	87	.09	<3	1.48	.01	.04	<2	<5	<1	<2
C L115E 93+00N	1	30	3	34	<.3	29	8	192	3.16	6	7	<2	2	24	.6	<2	2	95	.31	.068	6	41	.45	99	.09	3	1.54	.01	.04	<2	<5	<1	5
STANDARD C/AU-S	21	61	36	129	7.1	74	33	1118	4.03	42	23	7	40	52	19.5	15	19	69	.51	.093	44	60	.91	186	.08	28	1.87	.06	.15	11	<5	2	50

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL.
- SAMPLE TYPE: SOIL AU** ANALYSIS BY FA/ICP FROM 30 GM SAMPLE.
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUL 10 1995 DATE REPORT MAILED: July 15/95 SIGNED BY ..... D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppm	Au** ppb
C L115E 92+75N	1	26	<3	20	<.3	25	5	138	2.08	5	<5	<2	2	26	.3	<2	<2	60	.31	.055	6	39	.37	84	.07	<3	1.19	.01	.02	<2	<5	<1	9
C L115E 92+50N	1	31	4	43	<.3	16	8	309	2.72	3	6	<2	<2	32	.2	<2	3	94	.42	.045	3	34	.66	101	.11	<3	1.47	.01	.04	<2	<5	<1	20
C L115E 92+25N	<1	22	3	30	<.3	10	4	182	1.59	<2	<5	<2	2	30	.3	<2	2	51	.35	.028	3	21	.40	73	.07	<3	1.00	.01	.03	<2	<5	<1	25
C L115E 92+00N	1	41	7	51	<.3	20	10	299	3.73	7	<5	<2	2	40	.5	<2	<2	121	.42	.089	4	46	.50	140	.08	<3	1.49	.01	.07	<2	<5	<1	12
C L115E 91+75N	1	46	10	43	<.3	14	8	384	2.54	6	<5	<2	<2	48	.3	<2	2	91	.64	.023	8	32	.61	148	.08	<3	1.79	.02	.05	<2	<5	<1	4
C L115E 91+00N	1	42	13	72	<.3	16	10	392	3.63	7	5	<2	2	30	.4	<2	3	119	.33	.055	6	40	.45	73	.10	<3	1.28	.01	.05	<2	<5	<1	10
C L115E 90+75N	1	36	10	91	<.3	21	10	398	5.46	11	<5	<2	3	30	<.2	<2	4	169	.39	.207	8	58	.52	96	.09	<3	1.70	.01	.06	<2	<5	<1	10
C L115E 90+50N	1	27	10	96	<.3	15	9	996	3.86	7	<5	<2	3	31	.6	<2	<2	126	.35	.205	6	44	.32	113	.08	3	1.37	.01	.05	<2	<5	<1	10
C L115E 90+25N	2	42	14	83	<.3	19	7	255	4.79	20	<5	<2	5	27	.4	<2	<2	140	.34	.204	5	45	.52	89	.10	3	1.95	.01	.07	<2	<5	<1	2
C L115E 90+00N	1	17	8	61	<.3	8	4	175	2.49	3	<5	<2	3	22	.5	<2	<2	74	.25	.083	7	30	.26	71	.06	<3	1.34	.01	.05	<2	<5	<1	2
C L116E 96+00N	1	27	<3	18	<.3	9	3	137	1.72	<2	<5	<2	<2	29	.2	<2	2	66	.35	.014	5	27	.27	80	.07	<3	.91	.01	.02	<2	<5	<1	7
C L116E 95+75N	1	24	4	30	<.3	15	6	193	2.66	4	<5	<2	2	31	.4	<2	2	82	.45	.056	8	40	.35	81	.07	<3	1.16	.01	.03	<2	<5	<1	3
C L116E 95+50N	1	29	7	34	<.3	18	6	268	2.39	2	<5	<2	2	34	.2	<2	3	84	.51	.077	7	37	.52	77	.09	<3	1.10	.01	.05	<2	<5	<1	8
C L116E 95+25N	1	35	4	70	<.3	19	7	350	2.50	3	5	<2	2	32	.4	<2	3	77	.44	.066	7	34	.49	114	.08	<3	1.43	.01	.05	<2	<5	<1	4
C L116E 95+00N	1	36	6	66	<.3	19	8	431	2.53	2	6	<2	3	36	.4	<2	2	75	.49	.076	8	36	.62	111	.09	3	1.46	.01	.07	<2	<5	<1	6
C L116E 94+75N	<1	33	6	29	<.3	19	5	271	2.17	3	8	<2	2	36	.3	<2	3	65	.50	.064	7	37	.51	66	.10	7	.98	.01	.05	<2	<5	<1	3
C L116E 94+50N	1	26	6	38	<.3	16	7	293	2.88	3	<5	<2	<2	28	.3	<2	<2	100	.41	.061	5	43	.41	69	.08	3	.92	.01	.04	<2	<5	<1	4
C L116E 94+25N	2	100	11	79	<.3	36	11	677	3.91	8	<5	<2	<2	57	.6	<2	<2	115	.87	.046	18	51	.69	209	.07	4	2.61	.02	.09	<2	<5	<1	4
C L116E 93+75N	<1	35	7	31	<.3	23	6	274	2.33	4	5	<2	2	32	.2	<2	3	69	.44	.081	9	41	.45	76	.09	<3	.89	.01	.05	<2	<5	<1	4
C L116E 93+50N	1	22	7	38	<.3	20	6	179	3.37	4	<5	<2	2	20	.3	<2	3	107	.25	.097	6	54	.26	68	.08	<3	1.35	.01	.03	<2	<5	<1	10
C L116E 93+25N	<1	29	5	31	<.3	21	6	192	2.35	4	6	<2	2	25	<.2	<2	<2	71	.30	.069	7	40	.38	76	.09	<3	1.11	.01	.04	<2	<5	<1	167
C L116E 93+00N	1	36	11	69	<.3	11	8	374	4.51	9	5	<2	2	24	.2	<2	3	150	.30	.211	6	45	.32	77	.08	<3	1.40	.01	.05	<2	<5	<1	7
RE C L116E 93+00N	1	38	10	73	<.3	13	8	393	4.41	9	<5	<2	2	25	.4	<2	4	142	.30	.226	6	44	.34	83	.08	<3	1.50	.01	.05	<2	<5	<1	<2
C L116E 92+75N	1	33	6	70	<.3	9	6	527	4.13	5	<5	<2	3	24	.3	<2	2	149	.28	.090	5	40	.28	72	.09	<3	1.17	.01	.04	<2	<5	<1	2
C L116E 92+50N	1	36	13	110	<.3	16	9	394	4.51	6	7	<2	3	25	.3	<2	4	149	.30	.149	5	54	.49	89	.10	<3	1.39	.01	.06	<2	<5	<1	100
C L116E 92+25N	1	42	11	200	<.3	20	11	398	4.91	7	<5	<2	3	26	.6	<2	2	155	.35	.278	7	54	.47	108	.08	<3	2.22	.01	.06	<2	<5	<1	15
C L116E 92+00N	1	57	8	113	<.3	22	11	316	4.96	8	6	<2	4	32	.2	<2	4	162	.40	.236	7	56	.56	105	.09	<3	2.13	.01	.07	<2	<5	<1	30
STANDARD C/AU-S	20	63	39	124	6.5	68	32	1094	3.83	42	19	7	39	51	18.5	16	21	66	.51	.090	43	58	.89	185	.08	27	1.82	.06	.15	9	<5	2	51

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppm	Au** ppb
FE L145E 103+00N	1	79	5	78	.3	15	14	1247	4.14	4	16	<2	<2	201	.7	<2	<2	119	1.76	.122	10	17	.88	235	.12	8	2.55	.01	.11	<2	<5	<1	4
FE L145E 102+75N	1	75	5	111	<.3	17	15	877	5.35	7	55	<2	2	176	.3	<2	3	150	1.95	.075	5	14	1.38	245	.21	5	3.99	.02	.13	<2	<5	<1	<2
FE L145E 102+50N	1	89	5	89	<.3	17	8	411	2.91	3	10	<2	2	41	.6	<2	<2	84	.77	.027	13	31	.61	107	.09	5	2.02	.02	.05	<2	<5	<1	290
FE L145E 102+25N	2	54	5	72	<.3	20	13	319	5.50	7	8	<2	2	47	.7	<2	<2	186	.73	.061	7	45	.72	153	.10	3	2.52	.02	.06	<2	<5	<1	5
FE L145E 102+00N	1	53	5	70	<.3	20	8	270	2.55	<2	16	<2	2	56	.4	<2	2	79	1.00	.040	7	34	.81	143	.12	3	1.70	.02	.05	<2	<5	<1	3
FE L145E 101+75N	1	38	10	125	<.3	19	11	283	5.52	4	5	<2	4	34	.8	<2	<2	152	.52	.231	8	43	.56	124	.09	3	2.52	.01	.07	<2	<5	<1	<2
FE L145E 101+50N	1	41	10	103	<.3	15	10	307	4.91	3	<5	<2	4	38	.9	<2	<2	151	.57	.183	8	40	.54	130	.08	<3	1.98	.01	.07	<2	<5	<1	<2
FE L145E 101+25N	2	53	7	164	<.3	17	14	581	4.82	6	<5	<2	2	58	1.3	<2	<2	138	.76	.290	5	36	.68	193	.07	3	2.12	.01	.07	<2	<5	<1	9
FE L145E 101+00N	1	43	4	147	<.3	19	11	395	5.31	5	<5	<2	4	31	.7	<2	<2	170	.51	.380	6	48	.60	112	.08	3	2.28	.02	.06	<2	<5	<1	2
FE L145E 100+75N	2	149	9	67	.5	24	14	481	6.20	14	14	<2	7	67	.7	<2	<2	227	1.13	.114	26	57	.82	162	.11	<3	2.09	.02	.08	<2	<5	<1	7
FE L145E 100+50N	1	58	7	49	<.3	24	8	331	3.18	5	9	<2	3	57	.6	<2	2	95	.82	.066	11	40	.70	166	.09	3	1.61	.02	.06	<2	<5	<1	7
FE L145E 100+00N	1	102	12	68	<.3	22	16	1296	5.42	14	5	<2	3	50	.5	<2	<2	170	.58	.152	8	45	.67	204	.08	3	2.24	.01	.08	<2	<5	<1	56
FE L145E 99+75N	1	31	8	113	<.3	13	9	535	5.33	3	5	<2	3	60	.7	<2	<2	181	.37	.172	6	46	.37	123	.08	3	1.77	.01	.06	<2	<5	<1	168
FE L145E 99+50N	1	41	10	106	<.3	18	11	379	6.06	11	<5	<2	4	32	.7	<2	<2	189	.49	.244	7	48	.49	114	.06	3	2.13	.01	.06	<2	<5	<1	111
FE L145E 99+25N	1	26	8	144	<.3	12	10	352	4.68	8	<5	<2	3	26	.9	<2	<2	146	.34	.191	7	43	.40	122	.06	<3	1.89	.01	.06	<2	<5	<1	23
FE L145E 99+00N	1	19	11	114	<.3	9	7	458	4.86	4	<5	<2	2	38	.9	<2	3	194	.80	.054	3	52	.31	146	.07	<3	1.32	.01	.05	<2	<5	<1	7
FE L145E 98+75N	1	25	6	148	<.3	13	10	582	5.49	6	<5	<2	3	30	1.0	<2	2	205	.42	.197	6	59	.38	147	.06	3	1.49	.01	.06	<2	<5	<1	26
FE L145E 98+50N	1	22	8	77	<.3	9	9	653	4.31	3	<5	<2	3	26	.7	<2	<2	153	.37	.061	3	42	.28	108	.06	3	1.47	.01	.04	<2	<5	<1	3
FE L145E 91+00N	<1	20	<3	39	<.3	18	5	159	1.78	2	6	<2	3	28	.3	<2	<2	55	.32	.065	7	30	.42	73	.08	4	1.28	.01	.03	<2	<5	<1	5
FE L145E 90+75N	<1	26	6	25	<.3	21	6	200	1.90	2	9	<2	3	33	.3	<2	3	58	.40	.072	11	38	.47	85	.10	4	1.04	.01	.03	<2	<5	<1	50
FE L145E 90+50N	<1	24	4	24	<.3	20	5	184	1.91	<2	6	<2	3	29	.3	<2	3	59	.37	.082	9	37	.41	68	.08	3	1.13	.01	.03	<2	<5	<1	7
RE FE L145E 90+50N	<1	26	6	25	<.3	21	5	192	2.01	<2	5	<2	3	30	.3	<2	<2	62	.39	.088	10	38	.42	72	.09	3	1.19	.01	.03	<2	<5	<1	8
FE L145E 90+25N	<1	13	6	31	<.3	13	3	125	1.71	<2	<5	<2	<2	27	.3	<2	<2	59	.31	.063	8	33	.33	58	.07	4	1.40	.01	.03	<2	<5	<1	35
FE L145E 90+00N	<1	21	6	21	<.3	16	4	165	1.55	<2	6	<2	<2	31	.3	<2	2	50	.38	.063	10	32	.36	87	.08	4	1.12	.01	.03	<2	<5	<1	13
FE L145E 89+75N	1	20	5	29	<.3	20	5	156	1.88	2	7	<2	3	25	.4	<2	<2	53	.29	.057	8	33	.42	87	.08	3	1.24	.01	.03	<2	<5	<1	13
FE L145E 89+50N	1	20	5	29	<.3	21	5	163	1.85	<2	7	<2	3	25	<.2	<2	<2	52	.26	.047	7	34	.40	79	.09	3	1.16	.01	.03	<2	<5	<1	8
FE L145E 89+25N	<1	15	3	20	<.3	15	4	123	1.32	<2	7	<2	2	25	<.2	<2	2	42	.31	.047	7	25	.33	68	.08	<3	.93	.01	.02	<2	<5	<1	19
FE L145E 89+00N	<1	17	8	34	<.3	19	5	145	1.67	<2	7	<2	3	25	<.2	<2	3	48	.28	.044	8	33	.36	73	.08	<3	1.04	.01	.03	<2	<5	<1	15
FE L145E 88+75N	<1	18	5	22	<.3	16	4	176	1.60	<2	5	<2	3	32	.3	<2	<2	52	.42	.050	8	29	.38	73	.08	<3	.88	.01	.03	<2	<5	<1	31
FE L145E 88+25N	1	21	7	37	<.3	24	9	354	2.33	2	8	<2	2	37	.5	<2	<2	71	.54	.056	11	41	.48	134	.08	3	1.14	.02	.04	<2	<5	<1	16
FE L145E 88+00N	<1	18	8	23	<.3	20	5	184	1.87	2	7	<2	3	29	<.2	<2	<2	57	.37	.065	8	37	.44	67	.09	4	.93	.01	.03	<2	<5	<1	17
FE L145E 87+75N	1	17	8	26	<.3	19	4	161	1.84	2	5	<2	2	29	.4	<2	<2	55	.33	.049	9	34	.43	76	.09	<3	1.09	.01	.04	<2	<5	<1	<2
FE L145E 87+50N	<1	18	5	22	<.3	23	4	152	1.72	<2	9	<2	<2	28	<.2	<2	<2	53	.37	.070	9	34	.44	79	.09	<3	1.06	.01	.03	<2	<5	<1	24
FE L145E 87+25N	<1	16	7	23	<.3	16	4	131	1.55	<2	7	<2	2	25	<.2	<2	2	50	.32	.051	8	28	.36	73	.08	3	1.05	.01	.02	<2	<5	<1	11
FE L145E 87+00N	1	18	6	27	<.3	19	4	130	1.58	<2	7	<2	2	25	<.2	<2	<2	49	.28	.048	7	30	.35	72	.08	<3	1.13	.01	.03	<2	<5	<1	4
STANDARD C/AU-S	20	59	38	123	6.7	73	32	1063	3.85	46	21	6	37	51	18.7	15	20	67	.49	.087	43	56	.88	188	.08	29	1.84	.06	.14	11	<5	1	51

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppm	Au** ppb
FE L145E 86+75N	<1	18	7	29	<.3	22	4	164	1.76	<2	7	<2	3	29	.2	<2	<2	47	.37	.065	9	36	.47	74	.09	<3	1.08	.01	.03	<2	<5	<1	4
FE L145E 86+50N	1	17	7	30	<.3	20	4	151	1.64	<2	6	<2	2	26	.2	<2	2	44	.32	.058	7	34	.42	84	.08	3	1.27	.01	.04	<2	<5	<1	67
FE L145E 86+25N	1	21	6	26	<.3	21	4	152	1.84	<2	6	<2	3	25	<.2	<2	<2	46	.33	.066	9	37	.43	65	.08	4	1.14	.01	.03	<2	<5	<1	3
FE L145E 86+00N	1	21	3	41	<.3	23	6	322	2.58	4	5	<2	2	30	.7	<2	3	65	.38	.108	8	44	.43	72	.08	3	1.20	.01	.04	<2	<5	<1	15
FE L146E 93+00N	2	44	7	66	<.3	15	9	253	3.96	2	9	<2	4	34	.5	<2	3	121	.38	.106	6	45	.46	139	.10	3	2.53	.01	.05	<2	<5	<1	25
FE L146E 92+75N	3	50	9	64	<.3	19	9	348	8.03	6	27	<2	4	35	<.2	<2	3	308	.36	.179	4	113	.52	97	.14	<3	2.45	.01	.05	<2	<5	<1	26
FE L146E 92+50N	2	58	9	61	<.3	29	10	355	5.02	6	15	<2	4	44	.6	<2	2	159	.46	.156	4	65	.65	187	.13	4	2.97	.02	.07	<2	<5	<1	630
FE L146E 91+50N	<1	19	6	33	<.3	16	6	306	1.80	2	6	<2	2	35	.2	<2	2	60	.49	.062	8	29	.44	87	.08	3	1.17	.01	.03	<2	<5	<1	21
RE FE L146E 91+50N	<1	19	5	32	<.3	15	6	303	1.75	2	5	<2	2	35	.2	<2	<2	59	.47	.060	8	30	.42	85	.08	3	1.14	.01	.03	<2	<5	<1	6
FE L146E 91+25N	<1	21	8	32	<.3	17	6	246	2.02	<2	6	<2	2	35	.4	<2	2	61	.46	.078	9	34	.42	81	.08	4	.99	.01	.03	<2	<5	<1	6
FE L146E 91+00N	<1	24	5	25	<.3	18	6	297	1.98	5	8	<2	3	36	.3	<2	2	54	.48	.087	13	36	.42	83	.09	<3	.92	.01	.03	<2	<5	<1	9
FE L146E 90+75N	<1	23	3	21	<.3	16	4	177	1.63	<2	7	<2	3	36	.2	<2	3	46	.49	.082	12	31	.40	84	.09	3	.93	.01	.03	<2	<5	<1	52
FE L146E 90+50N	<1	15	4	23	<.3	14	3	168	1.60	<2	5	<2	2	31	<.2	<2	<2	48	.43	.073	9	30	.39	61	.08	4	.84	.01	.03	<2	<5	<1	125
FE L146E 90+25N	<1	19	8	24	<.3	15	5	202	1.67	<2	5	<2	2	34	.2	<2	2	47	.45	.071	10	32	.42	76	.08	4	.85	.01	.03	<2	<5	<1	7
FE L146E 90+00N	<1	18	5	26	<.3	15	4	181	1.69	2	7	<2	2	32	.3	<2	3	48	.39	.055	9	31	.41	72	.09	<3	.97	.01	.03	<2	<5	<1	92
FE L146E 89+75N	1	20	6	41	<.3	17	5	149	2.31	<2	5	<2	3	24	.5	<2	2	61	.24	.077	7	37	.31	83	.08	<3	1.55	.01	.03	<2	<5	<1	2
FE L146E 89+50N	<1	13	4	23	<.3	12	2	115	1.30	<2	8	<2	2	27	<.2	<2	<2	39	.29	.032	7	26	.26	63	.08	<3	1.12	.01	.02	<2	<5	<1	10
FE L146E 89+25N	1	21	5	41	<.3	25	8	389	2.35	4	<5	<2	2	50	.3	<2	<2	67	.82	.049	11	42	.55	183	.08	3	1.57	.02	.04	<2	<5	<1	8
FE L146E 89+00N	<1	19	4	25	<.3	15	4	185	1.69	<2	8	<2	2	30	.2	<2	3	48	.38	.056	9	31	.40	73	.09	3	.92	.01	.03	<2	<5	<1	30
FE L146E 88+75N	<1	18	5	25	<.3	17	4	173	1.72	<2	8	<2	<2	30	.2	<2	2	50	.38	.058	9	33	.41	68	.08	3	.93	.01	.03	<2	<5	<1	13
FE L146E 88+50N	<1	25	5	25	<.3	23	5	207	2.21	3	7	<2	3	30	.4	<2	2	59	.37	.076	9	43	.50	73	.09	4	1.01	.01	.03	<2	<5	<1	9
FE L146E 88+25N	<1	23	3	24	<.3	25	5	175	1.91	3	6	<2	3	29	<.2	<2	2	51	.35	.064	9	39	.49	84	.09	5	1.08	.01	.03	<2	<5	<1	13
FE L146E 88+00N	<1	22	3	25	<.3	23	6	233	2.10	<2	6	<2	3	37	.3	<2	3	58	.47	.070	11	39	.50	93	.09	3	.97	.01	.03	<2	<5	<1	5
FE L146E 87+75N	<1	15	7	23	<.3	15	4	166	1.51	<2	5	<2	2	32	.2	<2	2	45	.46	.070	10	30	.41	82	.08	<3	.99	.01	.03	<2	<5	<1	9
FE L146E 87+50N	<1	19	<3	23	<.3	23	4	150	1.62	<2	6	<2	3	27	.2	<2	3	45	.32	.057	9	35	.42	76	.08	<3	1.19	.01	.03	<2	<5	<1	11
FE L146E 87+25N	1	18	5	34	<.3	15	4	155	1.93	3	8	<2	2	27	.3	<2	<2	56	.28	.040	8	34	.39	81	.09	<3	1.30	.01	.03	<2	<5	<1	16
FE L146E 87+00N	<1	21	4	26	<.3	22	5	157	1.74	2	7	<2	2	26	.4	<2	2	45	.32	.063	7	34	.45	84	.08	3	1.10	.01	.03	<2	<5	<1	32
FE L146E 86+75N	1	17	5	30	<.3	16	3	141	1.69	2	<5	<2	2	26	<.2	<2	2	51	.32	.063	7	31	.38	67	.08	<3	1.24	.01	.03	<2	<5	<1	7
FE L146E 86+50N	1	21	4	30	<.3	24	4	163	1.91	2	5	<2	2	27	.3	<2	<2	50	.34	.064	8	38	.46	76	.08	3	1.24	.01	.04	<2	<5	<1	5
FE L147+50E 91+00N	1	21	3	35	<.3	15	4	161	2.28	<2	6	<2	3	27	.4	<2	<2	69	.29	.054	6	37	.37	80	.08	4	1.39	.01	.03	<2	<5	<1	46
FE L147+50E 90+75N	<1	16	7	28	<.3	16	4	140	1.84	<2	<5	<2	<2	28	<.2	<2	<2	54	.31	.059	8	34	.37	79	.08	<3	1.31	.01	.04	<2	<5	<1	5
FE L147+50E 90+50N	<1	20	4	24	<.3	20	5	185	2.00	2	6	<2	3	27	.3	<2	<2	55	.30	.047	10	36	.43	75	.09	3	.98	.01	.03	<2	<5	<1	6
FE L147+50E 90+25N	1	22	5	32	<.3	22	6	172	2.51	2	6	<2	3	25	.4	<2	2	66	.23	.066	10	43	.39	86	.09	4	1.39	.01	.03	<2	<5	<1	16
FE L147+50E 90+00N	1	20	7	28	<.3	24	6	177	2.35	4	6	<2	3	25	.5	<2	2	62	.24	.058	8	43	.42	83	.09	<3	1.28	.01	.04	<2	<5	<1	11
FE L147+50E 89+75N	1	21	5	31	<.3	23	6	186	2.41	<2	5	<2	2	26	.4	<2	<2	64	.25	.069	8	43	.44	81	.09	<3	1.31	.01	.04	<2	<5	<1	5
STANDARD C/AU-S	21	63	37	129	6.8	72	30	1111	3.99	43	22	7	39	53	19.0	14	20	63	.52	.092	45	59	.91	190	.09	33	1.90	.06	.16	11	<5	2	45

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppm	Au** ppb
FE L147+50E 89+75N-A	<1	41	4	33	<.3	28	7	327	2.68	5	9	<2	4	43	.3	<2	2	71	.55	.090	14	47	.55	108	.10	<3	.99	.02	.05	<2	<5	<1	7
FE L147+50E 89+50N	<1	17	6	22	<.3	17	4	170	1.48	<2	<5	<2	2	31	.3	<2	<2	43	.42	.062	9	28	.39	69	.08	3	.78	.01	.02	<2	<5	<1	11
FE L147+50E 89+25N	<1	21	5	24	<.3	14	4	215	1.75	<2	8	<2	2	34	.3	<2	2	48	.50	.078	11	32	.39	97	.08	<3	.99	.01	.03	<2	<5	<1	12
RE FE L147+50E 89+25N	<1	23	4	25	<.3	15	5	226	1.86	2	7	<2	2	36	.3	<2	2	50	.53	.079	11	35	.42	104	.09	<3	1.05	.01	.03	<2	<5	<1	11
FE L147+50E 89+00N	<1	21	3	32	<.3	20	6	233	2.00	3	7	<2	2	32	.2	<2	<2	56	.38	.061	10	37	.50	86	.09	4	1.03	.01	.03	<2	<5	<1	17
FE L147+50E 88+75N	1	22	3	27	<.3	20	5	170	2.03	<2	8	<2	3	26	.2	<2	<2	56	.29	.057	9	39	.45	76	.09	<3	1.06	.01	.03	<2	<5	<1	8
FE L147+50E 88+50N	<1	20	3	24	<.3	19	5	172	1.89	4	5	<2	2	29	.2	<2	3	55	.35	.062	10	36	.43	76	.09	<3	.91	.01	.02	<2	<5	<1	5
FE L147+50E 88+25N	<1	17	4	25	<.3	14	4	136	1.54	<2	6	<2	<2	25	.3	<2	2	47	.31	.054	7	28	.36	69	.08	3	1.12	.01	.02	<2	<5	<1	<2
FE L147+50E 88+00N	<1	16	5	24	<.3	14	4	142	1.43	<2	8	<2	2	29	<.2	<2	<2	43	.37	.051	9	27	.37	71	.08	<3	.93	.01	.02	<2	<5	<1	7
FE L149E 91+50N	1	25	<3	33	<.3	25	7	216	2.38	5	6	<2	3	29	.4	<2	2	63	.31	.069	9	44	.46	88	.09	<3	1.35	.01	.04	<2	<5	<1	6
FE L149E 91+25N	<1	21	4	27	<.3	18	5	164	1.84	5	9	<2	3	28	.2	<2	2	52	.32	.054	8	36	.42	72	.09	<3	1.08	.01	.04	<2	<5	<1	9
FE L149E 91+00N	1	18	4	51	<.3	21	7	219	2.76	3	11	<2	6	25	.3	<2	3	76	.24	.067	11	45	.39	98	.10	<3	1.46	.01	.04	<2	<5	<1	18
FE L149E 90+75N	1	21	3	43	<.3	22	7	194	2.81	4	10	<2	4	26	.2	<2	2	77	.23	.047	10	49	.42	94	.11	3	1.46	.01	.04	<2	<5	<1	3
FE L149E 90+50N	1	16	6	27	<.3	14	4	150	2.04	3	5	<2	2	24	<.2	<2	3	60	.25	.060	6	34	.33	67	.09	<3	1.22	.01	.03	<2	<5	<1	2
FE L149E 90+25N	1	18	3	28	<.3	18	5	144	1.83	3	5	<2	2	26	.3	<2	2	50	.29	.055	7	33	.36	75	.08	<3	1.13	.01	.02	<2	<5	<1	3
FE L149E 90+00N	1	22	8	34	<.3	14	6	297	1.79	<2	6	<2	2	33	.2	<2	<2	60	.46	.054	8	30	.45	115	.08	<3	1.29	.01	.03	<2	<5	<1	14
FE L149E 89+75N	1	18	5	33	<.3	14	4	151	1.83	2	5	<2	2	26	.3	<2	2	55	.28	.037	6	30	.34	86	.08	<3	1.33	.01	.03	<2	<5	<1	7
FE L149E 89+50N	<1	20	6	25	<.3	19	5	173	2.09	4	6	<2	3	27	.3	<2	<2	61	.30	.052	9	37	.40	83	.09	<3	.99	.01	.02	<2	<5	<1	30
FE L149E 89+25N	<1	19	3	25	<.3	19	6	180	1.94	4	5	<2	2	32	.2	<2	<2	55	.36	.052	10	35	.45	89	.09	<3	.99	.01	.03	<2	<5	<1	2
FE L149E 89+00N	<1	20	<3	23	<.3	20	6	199	1.88	3	6	<2	2	32	.5	<2	2	53	.43	.076	12	37	.44	85	.08	<3	.88	.01	.02	<2	<5	<1	5
FE L149E 88+75N	<1	16	5	22	<.3	13	4	157	1.69	3	7	<2	3	33	<.2	<2	2	56	.42	.052	8	28	.38	79	.09	<3	.96	.01	.02	<2	<5	<1	8
FE L149E 88+50N	<1	17	5	25	<.3	16	5	143	1.69	3	<5	<2	2	28	<.2	<2	2	52	.38	.058	8	31	.38	83	.08	<3	.93	.01	.02	<2	<5	<1	7
FE L149E 88+25N	<1	17	4	27	<.3	14	5	168	1.60	2	6	<2	2	30	<.2	<2	<2	52	.39	.044	9	30	.38	80	.09	<3	1.03	.01	.02	<2	<5	1	7
FE L149E 88+00N	<1	24	5	25	<.3	19	5	211	1.97	3	9	<2	3	34	.4	<2	2	56	.50	.090	11	37	.51	80	.09	<3	1.03	.01	.02	<2	<5	<1	6
FE L149E 87+75N	1	16	4	29	<.3	15	5	245	1.65	2	<5	<2	2	31	<.2	<2	<2	57	.44	.064	9	31	.45	71	.09	<3	.98	.01	.02	<2	<5	<1	6
FE L149E 87+50N	1	17	6	37	<.3	15	4	178	1.59	3	5	<2	<2	29	.2	<2	2	53	.38	.046	8	33	.43	79	.08	<3	1.11	.01	.02	<2	<5	<1	5
FE L150E 103+00E	1	80	6	49	<.3	20	11	648	3.84	4	22	<2	2	70	.5	<2	3	118	1.04	.094	11	38	.82	153	.14	<3	1.87	.02	.09	<2	<5	<1	3
FE L150E 102+75E	2	30	5	154	<.3	9	11	2583	3.76	<2	21	<2	2	33	.6	<2	4	110	1.05	.167	6	20	.54	124	.13	3	2.63	.01	.07	<2	<5	<1	442
FE L150E 102+50E	1	32	6	48	<.3	22	8	245	2.93	4	<5	<2	2	33	.2	<2	3	79	.44	.101	8	40	.48	85	.10	<3	1.76	.01	.04	<2	<5	<1	19
FE L150E 102+25E	1	30	5	45	<.3	18	6	257	2.52	2	9	<2	2	38	.3	<2	3	68	.67	.050	7	35	.61	62	.10	<3	1.65	.01	.05	<2	<5	<1	3
FE L150E 102+00E	1	33	8	132	<.3	5	11	1913	3.61	3	7	<2	<2	60	.8	<2	4	117	2.05	.106	4	8	.50	184	.10	4	2.60	.01	.09	<2	<5	1	2
FE L150E 101+75E	1	34	3	87	<.3	6	19	794	4.63	<2	<5	<2	2	522	1.0	<2	2	119	1.14	.205	4	5	1.46	349	.07	<3	4.19	.01	.22	<2	<5	1	<2
FE L150E 101+50E	1	20	4	44	<.3	22	8	339	2.59	4	<5	<2	3	32	.6	<2	4	73	.39	.106	8	43	.43	93	.09	<3	1.21	.01	.04	<2	<5	<1	10
FE L150E 101+25E	1	29	7	52	<.3	26	7	265	2.61	6	5	<2	3	34	.5	<2	3	74	.47	.081	7	39	.43	76	.10	<3	1.38	.01	.06	<2	<5	<1	4
FE L150E 101+00E	1	33	6	98	<.3	10	9	1032	4.31	6	<5	<2	2	26	.9	<2	3	153	.36	.186	4	46	.29	106	.08	<3	1.31	.01	.04	<2	<5	<1	18
STANDARD C/AU-S	21	60	38	127	6.9	72	33	1103	3.89	42	22	7	40	53	19.3	15	20	63	.52	.091	45	59	.91	188	.08	28	1.85	.06	.15	11	<5	5	46

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppm	Au** ppb
FE L150E 100+75N	2	33	6	100	.3	15	8	293	4.90	8	<5	<2	2	35	1.2	<2	6	155	.49	.152	7	49	.49	100	.10	<3	1.94	.01	.06	<2	<5	<1	13
FE L150E 100+50N	3	40	9	142	<.3	15	10	372	4.74	7	7	<2	3	38	1.3	<2	4	161	.51	.060	6	50	.49	147	.11	<3	2.41	.01	.06	<2	<5	<1	2
FE L150E 91+65N	1	26	8	45	<.3	25	8	271	3.25	7	<5	<2	3	32	.8	<2	<2	98	.37	.123	8	51	.44	84	.09	<3	1.55	.01	.04	<2	<5	<1	89
FE L150E 91+50N	1	25	9	36	<.3	33	8	225	2.94	8	<5	<2	3	29	.7	<2	2	85	.32	.092	8	50	.49	73	.09	<3	1.43	.01	.04	<2	<5	<1	13
FE L150E 91+25N	1	24	10	62	<.3	31	8	243	3.38	8	<5	<2	4	31	.6	<2	<2	86	.31	.119	8	53	.48	94	.10	<3	1.96	.01	.05	<2	<5	<1	14
FE L150E 91+00N	1	23	7	49	<.3	31	7	213	2.96	4	5	<2	3	31	.6	<2	3	83	.29	.083	10	52	.45	95	.10	<3	1.57	.01	.04	<2	<5	<1	35
FE L150E 90+75N	<1	19	5	32	<.3	20	4	166	2.09	4	6	<2	4	31	.5	<2	<2	60	.32	.070	8	38	.39	72	.10	<3	1.38	.01	.03	<2	<5	<1	7
FE L150E 90+50N	<1	26	9	27	<.3	27	5	220	2.09	4	8	<2	4	38	.4	<2	2	60	.44	.068	10	42	.53	86	.11	<3	1.11	.01	.03	<2	<5	<1	29
FE L150E 90+25N	6	144	4	107	1.3	124	25	1687	7.16	13	10	<2	4	62	1.5	<2	2	205	1.20	.160	25	110	1.59	553	.09	<3	5.06	.02	.12	<2	<5	1	9
FE L150E 90+00N	1	26	7	32	<.3	22	5	198	2.24	3	8	<2	3	33	.4	<2	2	70	.38	.057	9	43	.47	86	.11	<3	1.39	.01	.03	<2	<5	1	7
FE L150E 89+75N	1	34	6	51	<.3	31	10	294	4.96	9	6	<2	4	32	1.0	<2	3	157	.36	.149	7	66	.54	97	.10	<3	1.79	.01	.05	<2	<5	<1	8
RE FE L150E 89+75N	1	33	8	50	<.3	31	10	289	4.87	10	6	<2	4	31	.9	<2	4	152	.35	.149	7	65	.53	96	.10	<3	1.78	.01	.05	<2	<5	<1	<2
FE L150E 89+50N	1	18	8	36	<.3	13	4	166	2.25	2	<5	<2	3	30	.6	<2	3	69	.29	.078	9	38	.31	75	.10	<3	1.53	.01	.04	<2	<5	<1	2
FE L150E 89+25N	1	22	10	33	<.3	19	5	188	2.12	5	6	<2	2	36	.2	<2	3	69	.38	.043	8	38	.40	98	.10	<3	1.31	.01	.03	<2	<5	<1	5
FE L150E 89+00N	<1	20	5	25	<.3	18	4	172	1.84	<2	5	<2	4	37	.2	<2	<2	62	.50	.075	9	35	.45	86	.10	<3	1.08	.01	.03	<2	<5	<1	27
FE L150E 88+75N	<1	22	4	24	<.3	20	5	171	1.91	4	7	<2	2	37	.3	<2	<2	61	.48	.064	10	39	.45	89	.10	<3	1.06	.01	.03	<2	<5	<1	89
FE L150E 88+50N	<1	26	3	28	<.3	26	4	223	2.04	2	<5	<2	2	41	.7	<2	2	58	.56	.083	10	42	.55	88	.09	<3	.92	.02	.04	<2	<5	1	6
FE L150E 88+25N	<1	24	4	26	<.3	22	5	249	1.93	2	<5	<2	3	39	<.2	<2	2	58	.52	.084	11	39	.51	85	.10	<3	.96	.01	.03	<2	<5	<1	5
FE L150E 88+00N	<1	29	3	30	<.3	28	6	261	2.35	3	<5	<2	2	35	.4	<2	<2	65	.47	.084	8	45	.50	86	.09	<3	1.06	.01	.04	<2	<5	<1	5
FE L150E 87+75N	1	25	4	36	<.3	27	6	218	2.17	3	<5	<2	3	40	.4	<2	2	60	.53	.061	10	41	.53	90	.10	<3	1.13	.01	.05	<2	<5	<1	<2
FE L150E 87+50N	<1	28	7	31	<.3	25	6	316	2.40	2	<5	<2	3	39	.4	<2	2	70	.53	.085	10	45	.49	80	.09	<3	.87	.01	.05	<2	<5	<1	19
STANDARD C/AU-S	21	62	37	126	6.8	70	30	1084	3.80	41	16	7	39	54	19.4	15	20	64	.52	.090	40	57	.89	185	.09	28	1.84	.06	.16	11	<5	1	47

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

ACME AN[illegible]ICAL LABORATORIES LTD. 852 E. HASTINGS ST. V[illegible]UVER BC V6A 1R6 PHONE(604)253-3158 FAX(604[illegible]-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

Westley Technologies Ltd. PROJECT WIT File # 95-2494 Page 2

900 - 475 Howe St., Vancouver BC V6C 2B3 Submitted by: Colin CAMPBELL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppm	Au** ppb
L145E 112+25N	1	26	11	83	<.3	20	7	224	3.26	8	<5	<2	2	37	.3	<2	3	78	.33	.115	6	41	.53	82	.11	3	2.13	.02	.05	<2	<5	<1	5
L145E 112+00N	1	40	7	57	<.3	27	7	241	2.78	8	<5	<2	<2	41	<.2	<2	<2	70	.41	.075	7	41	.67	115	.12	<3	1.85	.02	.04	<2	<5	<1	4
L145E 111+50N	1	24	9	74	<.3	19	6	209	3.13	8	<5	<2	2	37	.3	2	2	78	.39	.148	7	41	.49	77	.11	<3	1.88	.01	.04	<2	<5	<1	3
L146E 112+25N	1	315	3484	14925	34.0	18	14	18495	3.67	22	<5	<2	3	46	65.0	6	<2	76	.69	.238	29	34	.28	4204	.03	<3	2.20	.01	.03	<2	21	5	1149
L146E 112+00N	1	32	21	249	<.3	23	5	401	2.42	7	<5	<2	<2	35	.3	<2	<2	68	.35	.032	7	38	.57	221	.12	<3	2.17	.01	.03	<2	5	<1	14
L146E 111+75N	1	47	18	154	<.3	34	14	713	4.87	12	<5	<2	<2	29	.5	2	2	124	.43	.045	6	77	.96	198	.09	<3	2.62	.01	.10	<2	<5	<1	5
L146E 111+50N	<1	24	7	95	<.3	14	5	213	2.97	6	<5	<2	<2	37	.5	2	<2	79	.40	.110	6	33	.46	120	.09	<3	1.54	.01	.05	<2	<5	<1	78
L146E 111+25N	<1	36	6	44	<.3	31	8	497	2.67	7	8	<2	<2	54	<.2	<2	2	66	.65	.086	11	49	.82	102	.14	<3	1.29	.02	.05	<2	6	<1	5
L146E 111+00N	1	29	8	49	<.3	26	8	227	2.85	5	<5	<2	2	43	<.2	<2	<2	76	.49	.067	7	39	.55	156	.11	<3	1.90	.01	.04	<2	<5	<1	3
L146E 110+75N	<1	42	10	172	<.3	20	9	787	2.74	6	<5	<2	<2	58	1.1	3	<2	75	.86	.084	9	39	.63	246	.10	<3	1.42	.02	.04	<2	5	<1	8
L147E 112+00N	1	40	75	343	1.7	20	13	389	4.03	47	5	<2	2	35	1.0	6	3	104	.43	.069	7	40	.66	410	.11	3	1.98	.01	.08	<2	<5	<1	3
L147E 111+75N	1	42	36	405	1.5	21	10	456	5.45	9	5	<2	<2	41	.6	3	2	145	.59	.072	8	50	.75	302	.12	3	2.87	.01	.08	<2	<5	<1	13
L147E 111+50N	<1	31	14	181	.3	24	10	345	4.38	10	<5	<2	<2	31	.6	4	<2	102	.43	.282	7	48	.67	186	.08	<3	2.21	.01	.08	<2	<5	<1	9
L147E 111+25N	1	30	11	361	<.3	28	11	421	3.85	9	<5	<2	<2	34	.5	2	<2	95	.49	.116	6	57	.76	186	.10	<3	2.20	.01	.04	<2	5	<1	<2
L147E 111+00N	<1	26	9	128	<.3	10	6	478	2.88	4	<5	<2	<2	30	.3	5	2	82	.51	.073	5	33	.36	187	.08	3	1.31	.01	.06	<2	<5	<1	2
L147E 110+75N	<1	37	10	66	<.3	17	11	624	3.72	7	<5	<2	<2	30	.5	3	<2	104	.41	.101	5	41	.98	203	.07	<3	2.02	.01	.05	<2	<5	<1	2
RE L147E 110+75N	<1	37	5	66	<.3	17	11	611	3.64	8	<5	<2	<2	30	.6	2	<2	101	.40	.100	6	41	.97	205	.07	<3	2.00	.01	.05	<2	<5	<1	7
L147E 110+50N	<1	26	5	49	<.3	23	7	492	2.86	5	<5	<2	<2	51	.4	2	2	75	.84	.025	8	42	.60	268	.10	<3	1.89	.02	.03	<2	6	<1	<2
STANDARD C/AU-S	20	58	37	121	6.8	72	29	1088	3.90	41	18	8	37	52	19.2	17	19	62	.51	.092	39	58	.91	184	.08	30	1.86	.07	.15	12	5	3	45

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL.
ASSAY RECOMMENDED FOR ROCK AND CORE SAMPLES IF CU PB ZN AS > 1%, AG > 30 PPM & AU > 1000 PPB
- SAMPLE TYPE: P1 ROCK P2 SOIL P3 TILL PULP AU** ANALYSIS BY FA/ICP FROM 30 GM SAMPLE.
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUL 24 1995 DATE REPORT MAILED: Aug 1/95 SIGNED BY. C. L. .D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

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ACME AN ICAL LABORATORIES LTD. 852 E. HASTINGS ST. V UVER BC V6A 1R6 PHONE(604)253-3158 FAX(604) -1716

GEOCHEMICAL ANALYSIS CERTIFICATE

Westley Technologies Ltd. PROJECT WIT File # 95-2726 Page 1

900 - 475 Howe St., Vancouver BC V6C 2B3

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppm
FE L147E 105+00N	1	24	5	93	.4	15	9	302	4.31	6	<5	<2	2	46	.8	<2	<2	130	.62	.193	6	43	.51	201	.11	5	1.98	.01	.07	<2	<5	<1
RE FE L147E 105+00N	1	26	4	95	.4	13	9	316	4.68	4	<5	<2	2	48	.5	<2	<2	147	.66	.178	7	46	.51	183	.11	6	1.95	<.01	.07	<2	<5	<1
FE L147E 104+75N	1	21	3	99	.4	10	11	521	4.94	9	<5	<2	2	70	.3	<2	<2	165	.72	.083	6	32	.51	156	.14	<3	1.92	<.01	.07	<2	<5	<1
FE L147E 104+50N	1	33	5	89	.6	11	16	808	4.51	7	<5	<2	2	62	1.1	<2	<2	128	.80	.151	6	26	.59	188	.14	4	2.48	.01	.07	<2	<5	<1
FE L147E 104+25N	1	35	<3	106	.4	15	12	388	5.54	16	<5	<2	2	54	.4	<2	<2	184	.67	.159	6	54	.63	136	.12	6	2.22	.01	.07	<2	<5	<1
FE L147E 104+00N	1	57	9	82	.5	20	13	533	5.19	14	<5	<2	3	66	.3	<2	<2	162	.85	.198	10	47	.71	156	.12	4	2.57	.01	.10	<2	<5	<1
FE L147E 103+75N	1	38	3	71	.3	15	10	1320	2.94	10	<5	<2	<2	54	.5	<2	<2	79	.69	.054	12	32	.55	186	.10	<3	1.83	<.01	.06	<2	<5	<1
FE L147E 103+50N	1	24	3	47	.5	13	8	379	2.47	5	<5	<2	<2	45	<.2	<2	2	76	.61	.042	9	30	.39	205	.09	3	1.38	.01	.04	<2	<5	<1
FE L147E 103+25N	1	23	<3	44	<.3	15	10	797	2.71	4	<5	<2	<2	47	<.2	<2	<2	81	.58	.061	9	33	.47	183	.10	5	1.30	<.01	.05	<2	<5	<1
FE L147E 103+00N	<1	27	4	41	<.3	19	7	483	2.76	6	<5	<2	2	46	.2	<2	5	84	.68	.092	12	39	.54	101	.13	<3	1.01	.01	.06	<2	<5	<1
FE L147E 102+75N	1	56	4	95	.4	28	12	1137	3.45	4	<5	<2	2	67	<.2	<2	<2	87	.85	.080	15	44	.74	234	.10	4	1.94	.01	.11	<2	<5	<1
FE L147E 102+50N	2	35	6	70	<.3	16	13	1668	4.92	2	<5	<2	<2	44	.3	<2	<2	174	.62	.043	6	54	.40	93	.12	4	1.31	.01	.08	<2	<5	<1
FE L148E 105+00N	<1	30	<3	74	.4	14	8	508	3.93	4	<5	<2	3	46	<.2	<2	<2	124	.68	.121	7	41	.49	85	.11	<3	1.62	.02	.05	<2	<5	1
FE L148E 104+75N	1	86	3	49	.3	16	11	634	4.36	13	<5	<2	3	83	1.8	<2	<2	134	1.13	.101	9	39	.96	109	.15	3	2.35	.01	.09	<2	<5	<1
FE L148E 104+50N	1	32	5	102	.3	11	11	1004	5.15	2	<5	<2	2	59	1.1	<2	<2	176	.80	.211	6	54	.50	137	.12	6	1.93	.02	.14	<2	<5	<1
FE L148E 104+25N	2	49	3	66	<.3	23	11	505	8.24	<2	<5	<2	5	43	.7	<2	<2	318	.62	.171	8	107	.51	104	.12	<3	1.63	.01	.06	<2	<5	<1
FE L148E 104+00N	2	88	6	56	.3	23	16	603	7.01	18	10	<2	2	80	.3	<2	6	252	.95	.107	9	80	.78	149	.15	4	2.14	.02	.10	<2	<5	<1
FE L148E 103+75N	1	50	5	62	.3	19	11	412	3.82	13	<5	<2	<2	65	.7	<2	<2	106	.67	.102	7	35	.67	137	.11	8	2.14	.01	.09	<2	<5	<1
FE L148E 103+50N	1	60	<3	63	.4	21	11	441	4.18	16	<5	<2	2	69	<.2	<2	<2	112	.69	.133	7	40	.75	229	.12	8	2.41	.01	.07	<2	<5	<1
FE L148E 103+25N	1	36	3	53	.3	18	9	456	3.05	3	<5	<2	2	48	<.2	<2	<2	93	.66	.047	11	34	.55	168	.10	<3	1.68	<.01	.05	<2	<5	<1
FE L148E 103+00N	1	49	11	49	<.3	25	9	608	3.14	<2	<5	<2	2	50	.4	<2	5	89	.73	.097	14	47	.68	146	.12	<3	1.22	.01	.07	<2	<5	<1
FE L148E 102+75N	1	41	3	59	.3	19	9	692	2.74	4	<5	<2	<2	51	1.0	<2	3	75	.86	.063	11	39	.59	182	.09	6	1.31	<.01	.13	<2	<5	<1
FE L148E 102+50N	1	48	<3	148	<.3	12	15	594	5.29	2	<5	<2	2	53	<.2	<2	<2	120	1.07	.383	6	20	.85	244	.13	6	3.09	.01	.11	<2	<5	<1
FE L149E 105+00N	1	43	<3	91	.6	16	10	378	5.43	<2	<5	<2	2	48	.8	<2	<2	148	.63	.372	5	41	.60	129	.11	<3	2.62	.01	.06	<2	<5	<1
FE L149E 104+75N	1	30	<3	96	<.3	10	7	275	4.94	7	6	<2	2	32	.7	<2	<2	145	.47	.320	7	48	.44	102	.10	<3	2.06	.01	.05	<2	<5	<1
FE L149E 104+50N	1	45	8	73	<.3	25	12	431	6.20	9	<5	<2	3	37	<.2	<2	<2	219	.56	.227	8	79	.53	104	.10	<3	1.94	.01	.06	<2	<5	<1
FE L149E 104+25N	1	54	7	81	.3	17	12	505	4.97	6	7	<2	2	53	1.2	<2	<2	142	.65	.287	7	48	.71	229	.11	3	2.32	.01	.08	<2	<5	<1
FE L149E 104+00N	1	56	4	79	.3	18	11	514	4.97	4	<5	<2	2	68	.8	<2	7	153	.84	.198	5	46	.75	166	.11	7	2.57	.01	.08	2	<5	<1
FE L149E 103+75N	1	39	12	59	.3	14	9	617	3.65	6	8	<2	<2	60	.6	<2	<2	114	.70	.124	6	35	.52	149	.11	6	1.76	<.01	.09	<2	<5	<1
FE L149E 103+50N	1	68	9	68	<.3	20	10	342	3.77	<2	<5	<2	<2	47	1.0	<2	<2	106	.57	.083	10	40	.61	192	.11	4	2.20	.01	.08	<2	<5	<1
FE L149E 103+25N	1	38	3	126	.3	18	10	467	3.95	9	10	<2	2	45	.7	<2	3	106	.64	.213	7	34	.64	184	.11	<3	2.18	.01	.09	<2	<5	<1
FE L149E 103+00N	<1	40	4	43	<.3	20	9	512	3.03	6	<5	<2	2	48	.5	<2	<2	91	.68	.081	12	44	.58	115	.12	3	1.18	.01	.06	<2	<5	<1
FE L149E 102+75N	<1	98	4	40	.4	21	8	390	2.65	3	<5	<2	<2	53	.3	<2	<2	77	.76	.021	16	37	.49	189	.09	<3	1.42	.01	.05	<2	<5	<1
FE L149E 102+50N	<1	38	3	18	<.3	12	2	141	1.53	<2	7	<2	<2	40	.6	<2	2	54	.56	.020	9	26	.31	63	.10	4	.83	.01	.03	<2	<5	<1
FE L150E 105+50N	1	29	5	79	<.3	11	12	1295	4.47	9	5	<2	<2	45	1.2	<2	<2	146	.60	.160	5	39	.44	205	.11	4	1.81	.01	.05	<2	<5	<1
STANDARD C	19	58	38	121	6.9	65	31	1099	3.84	42	19	7	36	52	18.2	18	18	61	.51	.093	43	60	.91	180	.08	31	1.80	.06	.15	10	<5	2

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL.
- SAMPLE TYPE: SOIL Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: AUG 8 1995 **DATE REPORT MAILED:** Aug 12/95 **SIGNED BY** ..... D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

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SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppm
FE L150E 105+25N	1	39	13	51	<.3	13	9	615	5.00	6	<5	<2	3	35	.6	<2	<2	180	.49	.230	5	58	.45	125	.09	3	1.57	.01	.06	<2	5	<1
FE L150E 105+00N	1	27	7	43	<.3	16	7	273	3.49	5	<5	<2	<2	34	<.2	<2	<2	113	.45	.102	5	39	.43	119	.08	3	1.60	.01	.04	2	5	<1
RE FE L150E 105+00N	1	29	4	42	<.3	16	7	262	3.50	5	<5	<2	<2	35	<.2	2	5	114	.45	.100	5	40	.43	113	.08	<3	1.62	.01	.04	<2	<5	<1
FE L150E 104+75N	1	13	8	45	<.3	10	5	199	3.35	3	<5	<2	<2	22	<.2	<2	<2	116	.34	.090	4	40	.25	75	.08	<3	1.21	.01	.03	<2	<5	<1
FE L150E 104+50N	1	36	8	84	<.3	17	10	334	5.01	12	<5	<2	<2	42	.5	<2	2	171	.53	.223	6	51	.48	135	.09	<3	2.23	.01	.05	2	5	1
FE L150E 104+25N	1	38	<3	68	<.3	13	8	369	4.05	6	<5	<2	<2	39	.2	<2	4	125	.49	.178	5	38	.48	108	.09	3	2.00	.01	.06	<2	<5	<1
FE L150E 104+00N	1	15	8	106	.3	8	5	243	3.55	6	<5	<2	<2	32	<.2	<2	<2	99	.44	.293	5	35	.33	146	.08	3	1.65	<.01	.06	<2	<5	<1
FE L150E 103+75N	1	29	5	52	<.3	15	7	266	3.32	11	7	<2	<2	32	.2	<2	6	107	.42	.114	6	39	.37	121	.08	<3	1.52	.01	.05	<2	<5	<1
FE L150E 103+50N	<1	50	6	38	<.3	15	8	428	3.18	5	<5	<2	<2	42	.2	<2	<2	98	.61	.090	9	36	.50	118	.10	3	1.41	.01	.05	<2	<5	<1
FE L150E 103+25N	1	25	<3	181	<.3	5	12	2562	3.38	6	5	<2	<2	37	<.2	<2	2	87	.64	.177	9	10	.54	231	.06	3	2.56	.01	.10	<2	7	<1
STANDARD C	18	55	36	121	6.5	63	31	1085	3.90	42	22	6	34	48	17.2	15	17	64	.49	.089	40	58	.88	179	.07	24	1.84	.06	.14	11	5	2

Sample type: SOIL. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

ME ANA CAL LABORATORIES LTD. 852 E. HASTINGS ST. VA VER BC V6A 1R6 PHONE(604)253-3158 FAX(604)2 716

ASSAY CERTIFICATE

Westley Technologies Ltd. PROJECT WIT File # 95-2291 Page 1

900 - 475 Howe St., Vancouver BC V6C 2B3 Submitted by: Colin Campbell

SAMPLE#	Cu %	Pb %	Zn %	Ag** oz/t	Au** oz/t
95-RF-1	.298	.02	.09	3.44	.001
95-RF-2	.010	<.01	.01	.05	.001
95-RF-3	.012	.05	<.01	.01	<.001
WT-1	.008	.10	.08	.17	.003
WT-2	.007	.01	.12	.06	.002
WT-3	.008	<.01	.08	.02	.001
WT-4	.001	<.01	.06	.01	.001
WT-5	.003	<.01	.06	.02	.001
WT-6	.005	<.01	.10	.02	.001
WT-7	.009	.04	.06	.05	.002
WT-8	.011	.05	.04	.03	.002
WT-9	.008	.01	.10	.24	.003
WT-10	.008	<.01	.08	.05	.003
RE WT-10	.008	<.01	.08	.06	.002
RRE WT-10	.008	<.01	.08	.06	.002
WT-11	.003	<.01	.10	.02	<.001
WT-12	.004	.08	.43	.07	.002
WT-13	.002	6.22	1.84	.74	.006
WT-14	.003	.20	.44	.10	.001
WT-15	.009	.05	.18	.17	<.001
WT-16	.010	.03	.04	.03	.001
WT-17	.011	.01	.02	.03	<.001
WT-18	.010	<.01	.02	.01	<.001
WT-19	.012	<.01	.02	.01	.001
WT-20	.013	<.01	.02	.01	.001
WT-21	.008	<.01	.03	.04	.002
RE WT-21	.007	<.01	.03	.04	.001
RRE WT-21	.007	<.01	.03	.05	.001
WT-22	.004	<.01	.08	.14	.001
WT-23	.004	<.01	.06	.06	<.001
WT-24	.002	<.01	.06	.05	<.001
WT-25	.003	<.01	.04	.04	.001
WT-26	.002	<.01	.04	.01	.002
WT-27	.002	<.01	.04	.02	.001
WT-28	.003	<.01	.04	.03	.001
WT-29	.005	<.01	.04	.01	<.001
WT-30	.008	<.01	.06	.01	.001
STANDARD R-1/AG-1/AU-1	.830	1.26	2.31	13.59	.103

6.22% Pb

.206 gpt Au, 25.38 gpt Ag, 1.84% Zn, 6.22% Pb, 1.84% [illegible], .74 gpt Ag

1 m

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1 GM SAMPLE LEACHED IN 50 ML AQUA - REGIA, DILUTE TO 100 ML, ANALYSIS BY ICP.
AG** & AU** BY FIRE ASSAY FROM 1 A.T. SAMPLE.
- SAMPLE TYPE: ROCK
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUL 13 1995 DATE REPORT MAILED: July 20/95 SIGNED BY..... D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

Westley Technologies Ltd. PROJECT WIT FILE # 95-2291 Page 2

SAMPLE#	Cu %	Pb %	Zn %	Ag** oz/t	Au** oz/t
WT-31	.010	.01	.06	.04	.002
WT-32	.005	.01	.07	.05	.001
WT-33	.008	.01	.07	.06	.001
WT-34	.002	.04	.27	.06	.001
RE WT-34	.003	.04	.26	.06	.001
WT-35	.002	1.58	1.25	.17	.003
WT-36	.012	.63	1.79	.20	.004
WT-37	.021	.04	.16	.12	.001
STANDARD R-1/AG-2/AU-1	.837	1.34	2.22	13.36	.102

0-12 gpt Au, 6-17 opt Ag, 1.52% Zn, 1.10% Pb

(1.10% Pb, 1.52% Zn, -18 opt Ag .0035 zm

Sample type: ROCK. Samples beginning 'RE' are Reruns and 'RRE' are Reject Rer

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)25[illegible]716

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ASSAY CERTIFICATE

Westley Technologies Ltd. PROJECT WIT File # 95-2360

900 - 475 Howe St., Vancouver BC V6C 2B3 Submitted by: Colin Campbell

SAMPLE#	Cu %	Pb %	Zn %	Ag** oz/t	Au** oz/t
WT-38 2m	.005	.27	1.33	.07	.005 2m
WT-39	.004	.18	.57	.04	.002
WT-40	.007	1.81	2.33	.22	.003
WT-41	.006	1.03	1.70	.24	.004
WT-42	.004	3.50	3.21	.53	.006
WT-43	.003	1.62	1.40	.24	.003
WT-44 2m	.007	1.81	1.66	.29	.010 2m
WT-45	.009	1.08	1.36	.36	.002
WT-46	.006	.30	1.00	.14	.003
WT-47 .88%Pb, 1.33% Zn, 0.36 opt Ag	.002	.37	1.06	.15	.001
RE WT-47 22m	.002	.37	1.05	.14	.002
RRE WT-47	~~.003~~	~~.33~~	~~1.05~~	~~.14~~	~~.002~~
WT-48	.002	.25	.60	.08	.001
WT-49	.003	1.89	2.16	.48	.010
WT-50	.002	.32	.78	.11	.007
WT-51	.003	.31	.65	.13	.011
WT-52	.011	.49	1.49	.24	.017
WT-53	.002	.14	.63	.10	.002
WT-54	.006	.30	1.12	1.67	.004
WT-55	.004	.47	2.06	.95	.007
WT-56	.002	.38	1.09	.99	.003
WT-57	.003	.39	1.20	.68	.003
RE WT-57	.003	.40	1.20	.68	.004
RRE WT-57	.004	.46	1.46	.75	.004
WT-58 2m	.009	.05	.21	.07	.001 2m
WT-59	.003	.03	.39	1.18	<.001
WT-60	.002	.05	.64	.89	<.001
WT-61	.011	.18	.41	7.88	<.001
WT-62	.015	.02	.06	.11	.001
WT-63	.003	.04	.42	1.10	.002
WT-64	.001	.09	.27	.56	<.001
STANDARD R-1/AG-2/AU-1	.834	1.24	2.21	13.55	.104

TR 147+50

.171 gpt Au, 13.03 gpt Ag, 1.90% Zn, 1.81% Pb
1.81% Pb, 1.90% Zn, .380 opt Ag, .005 Au
7m

Trench 150+00

1 GM SAMPLE LEACHED IN 50 ML AQUA - REGIA, DILUTE TO 100 ML, ANALYSIS BY ICP.
AG** & AU** BY FIRE ASSAY FROM 1 A.T. SAMPLE.
- SAMPLE TYPE: ROCK
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUL 17 1995 DATE REPORT MAILED: July 25/95 SIGNED BY C. Leong D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

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ACME AN[illegible]CAL LABORATORIES LTD. 852 E. HASTINGS ST. V[illegible]UVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)[illegible]1716

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ASSAY CERTIFICATE

Westley Technologies Ltd. PROJECT WIT File # 95-2385

900 - 475 Howe St., Vancouver BC V6C 2B3 Submitted by: Colin Campell

	SAMPLE#	Cu %	Pb %	Zn %	Ag** oz/t	Au** oz/t	
							oz/ton 34.3g/T
	WT-65	.013	.07	.27	.20	<.001	
	WT-66	.006	9.36	.97	.79	<.001	0.34 gpt Au, 22.9 gpt Ag, 3.43% Zn, 5.9[illegible]
	WT-67	.005	1.44	3.51	.33	.003	5.91% Pb, 3.43% Zn, .67 opt Ag, .018
TR 149	WT-68	.007	5.35	5.43	.91	.018	
	WT-69	.003	8.87	3.17	.62	.019	5M
	WT-70	.005	4.83	4.06	.70	.023	
	WT-71	.006	.83	1.94	.52	.007	
	WT-72	.003	.13	.51	.06	.001	
	WT-73	.012	.01	.06	.07	.001	
	WT-74	.012	.06	.34	.23	<.001	
	RE WT-74	.012	.07	.34	.25	<.001	
	RRE WT-74	.012	.06	.34	.23	<.001	
	WT-75	.022	.10	.90	.30	<.001	124.5 gpt Ag, 0.46% Zn, 0.20% Pb
	WT-76	.026	.13	.33	7.14	<.001	.20% Pb .46% Zn 3.62 opt Ag <.001 opt Au
	WT-77	.015	.17	.22	2.31	<.001	3M
TR 149+50	WT-78	.044	.31	.83	1.43	<.001	
	WT-79	.023	.07	.39	.91	<.001	
	WT-80	.024	<.01	1.64	.08	<.001	
	WT-81	.020	.02	1.61	.09	<.001	
	WT-82	.017	.29	.86	.91	.003	
	WT-83	.019	2.84	.52	3.29	.003 *	0.26 gpt Au, 87.2 gpt Ag, 0.6[illegible]
	WT-84	.007	4.46	.21	1.62	.008 *	6.6% Pb .64% Zn 2.56 opt Ag .0076 opt Au
	RE WT-84	.007	4.48	.21	1.59	.011	3M
	RRE WT-84	.006	4.46	.21	1.58	.008	
	WT-85	.006	12.50	1.19	2.77	.012 *	includes
	WT-86	.002	.09	.15	1.24	.001	12.5% Pb, 1.19% Zn 2.77 opt Ag, .012 Au
	WT-87	.005	.13	.44	.29	.004	[illegible] gpt Au, 95.0 gpt Ag, 1.19% Zn, 12.5% Pb
	WT-88	.009	.19	.14	.35	.001	

1 GM SAMPLE LEACHED IN 50 ML AQUA - REGIA, DILUTE TO 100 ML, ANALYSIS BY ICP.
AG** & AU** BY FIRE ASSAY FROM 1 A.T. SAMPLE.
- SAMPLE TYPE: ROCK
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUL 19 1995 DATE REPORT MAILED: July 27/95 SIGNED BY. C. L. .D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)

ASSAY CERTIFICATE

Westley Technologies Ltd. PROJECT WIT File # 95-2494 Page 1

900 - 475 Howe St., Vancouver BC V6C 2B3 Submitted by: Colin CAMPBELL

SAMPLE#	Cu %	Pb %	Zn %	Ag** oz/t	Au** oz/t	
WT-89	.010	.13	.50	.06	<.001	
WT-90	.009	.38	1.11	.16	.003	.123 gpt Au, 8.0 oz gpt Ag, 1.57% Zn, 0.69% Pb
WT-91	.003	.21	.66	.04	.002	5m
WT-92	.002	.31	1.03	.07	.001	
WT-93	.003	.45	1.81	.12	.001	
WT-94	.004	.89	1.06	.60	.002	
TR 147+75E WT-95	.002	1.22	2.18	.18	.009	
WT-96	.005	.18	.52	.78	.002	18.20
WT-97	.003	.20	.55	.41	.002	5.96
WT-98	.004	.22	.59	.22	.004	22.16
WT-99	.001	.01	.32	.03	<.001	
WT-100	.001	.02	.33	.02	<.001	
WT-101	.002	.07	.43	.03	<.001	
WT-102	<.001	.03	.37	.02	<.001	
RE WT-102	<.001	.03	.36	.01	<.001	
RRE WT-102	.001	.03	.37	.02	<.001	
WT-103	.001	.04	.61	.01	.001	
WT-104	<.001	.23	.97	.05	.012	
WT-105	.001	1.20	2.72	.17	.003	.085 gpt Au, 5.83 gpt Ag, 2.89% Zn, 1.15% Pb
WT-106	.004	1.11	3.07	.17	.002	2m
WT-107	.005	.28	.86	.10	.001	
WT-108	.013	.22	.45	.07	.001	
WT-109	.014	.08	.34	.04	<.001	
WT-110	.003	<.01	.03	<.01	<.001	
WT-111	.006	.04	.23	.02	.001	
WT-112	.009	.17	.74	.06	<.001	
WT-113	.021	.76	2.51	.15	.001	.103 gpt Au, 5.37 gpt Ag, 2.34% Zn, 1.24% Pb
WT-114	.026	.55	1.46	.11	.004	3m
WT-115	.012	2.42	3.05	.21	.004	
TR 147+25E WT-116	.019	.56	.66	.09	.007	
RE WT-116	.019	.57	.68	.10	.006	
RRE WT-116	.020	.57	.68	.11	.006	
WT-117	.015	.18	.82	.03	<.001	
WT-118	.006	.12	.63	.06	<.001	
WT-119	.007	.14	.83	.05	<.001	
STANDARD R-1/AG-2/AU-1	.830	1.23	2.24	13.45	.097	

1 GM SAMPLE LEACHED IN 50 ML AQUA - REGIA, DILUTE TO 100 ML, ANALYSIS BY ICP.
AG** & AU** BY FIRE ASSAY FROM 1 A.T. SAMPLE.
- SAMPLE TYPE: P1 ROCK P2 SOIL P3 TILL PULP
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: JUL 24 1995 DATE REPORT MAILED: Aug 1/95 SIGNED BY. . . . . .TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

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SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppm
WT-120	1	82	15	83	<.3	43	12	675	3.33	13	7	<2	3	79	1.3	<2	4	77	1.54	.109	11	43	.96	118	.12	3	1.26	.03	.10	<2	<5	<1
WT-121	1	80	16	81	<.3	44	13	727	3.33	11	<5	<2	2	80	1.1	<2	2	84	1.47	.097	9	43	.94	118	.12	<3	1.24	.02	.10	<2	<5	<1
WT-122	1	85	37	114	.3	34	11	586	3.30	12	5	<2	3	65	1.0	<2	<2	83	.83	.115	12	40	.81	188	.13	3	1.29	.03	.09	<2	<5	<1
WT-123	1	88	31	113	.3	39	13	761	3.57	12	<5	<2	3	67	1.1	<2	2	95	.82	.102	10	41	.88	192	.13	3	1.37	.03	.09	<2	<5	<1
WT-124	1	74	31	146	.3	31	9	490	3.01	9	<5	<2	3	54	1.0	<2	<2	78	.72	.109	11	39	.78	290	.12	<3	1.50	.02	.06	<2	<5	<1
WT-125	1	80	31	146	<.3	34	11	561	3.26	10	<5	<2	2	53	.8	<2	2	88	.69	.098	9	43	.83	294	.13	3	1.53	.02	.06	<2	<5	<1
RE WT-125	1	79	34	150	<.3	33	11	561	3.28	12	<5	<2	2	53	.9	<2	3	89	.70	.101	9	43	.83	295	.13	<3	1.53	.02	.07	<2	<5	<1
STANDARD C	19	65	39	122	6.7	75	31	1101	3.78	43	22	7	36	50	19.0	16	22	59	.49	.089	40	54	.88	173	.08	28	1.76	.06	.15	10	<5	<1

Sample type: TILL PULP. Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER BC V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

Westley Technologies Ltd. PROJECT WIT File # 95-3119

900 - 475 Howe St., Vancouver BC V6C 2B3

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Tl ppm	Hg ppm	Au** ppb
WT-126	2	133	584	2209	2.3	76	25	1987	5.28	12	<5	<2	2	37	2.7	<2	<2	176	.26	.117	4	137	2.02	145	<.01	<3	2.16	.01	.15	<2	<5	1	22
WT-127	3	396	1223	4955	7.1	21	6	491	3.86	20	<5	<2	<2	96	5.0	5	<2	125	.10	.064	4	63	.45	291	.01	3	.88	.01	.18	<2	<5	2	42
WT-128	4	93	22352	3832	46.5	10	2	430	.75	4	<5	<2	<2	169	18.4	23	<2	12	.04	.020	<1	11	.03	16	<.01	<3	.11	.01	.05	<2	<5	3	62
WT-129	3	77	1081	4194	15.4	10	7	6346	1.25	8	<5	<2	<2	106	15.3	9	<2	38	.07	.016	2	11	.05	1120	<.01	<3	.09	<.01	.01	<2	<5	3	276
WT-130	3	63	1547	3636	18.4	8	3	2546	.67	4	<5	<2	<2	116	11.0	8	<2	15	.04	.007	1	10	.01	1044	<.01	<3	.03	<.01	.01	<2	<5	4	326
WT-131	5	61	768	3783	26.7	11	3	4383	.84	5	<5	<2	<2	78	10.1	4	<2	10	.33	.011	3	13	.01	1231	<.01	3	.04	<.01	.01	<2	<5	3	299
WT-132	4	104	665	7121	19.5	12	3	3278	1.09	9	<5	<2	<2	180	21.8	3	<2	11	.93	.014	1	12	.03	410	<.01	<3	.09	<.01	.05	<2	<5	4	580
WT-133	3	148	1937	22411	27.1	7	4	3819	1.24	8	<5	<2	<2	138	71.7	5	<2	13	1.12	.017	<1	8	.03	56	<.01	<3	.08	<.01	.05	<2	<5	8	423
RE WT-133	3	156	2025	23703	27.3	7	4	3985	1.29	7	<5	<2	<2	145	76.3	4	<2	14	1.18	.017	1	9	.03	51	<.01	<3	.08	<.01	.06	<2	<5	8	483
RRE WT-133	3	153	1981	23259	27.2	9	4	3958	1.29	8	<5	<2	<2	142	73.9	5	<2	14	1.16	.017	<1	12	.03	52	<.01	4	.08	<.01	.06	<2	<5	8	450
WT-134	3	158	1152	7258	5.1	9	5	4272	2.30	13	<5	<2	<2	183	20.2	2	<2	25	2.74	.024	3	9	.42	204	<.01	<3	.55	<.01	.07	<2	<5	2	501
WT-135	5	60	188	524	8.7	17	12	255	5.03	15	<5	<2	2	23	2.5	3	<2	34	.13	.079	4	21	.17	10	<.01	3	.41	.01	.27	<2	<5	3	27
WT-136	6	76	1260	734	7.9	8	4	113	3.59	4	7	<2	<2	21	3.8	2	<2	42	.05	.090	7	12	.09	44	.01	3	.39	.02	.46	<2	<5	4	7
STANDARD C/AU-R	20	60	37	132	7.2	73	33	1126	4.08	44	16	7	39	53	18.4	17	18	62	.50	.097	41	59	.93	193	.08	27	1.90	.06	.16	10	<5	3	462

380 gpt Au
21.1 gpt Ag
0.82% Zn
0.12% Pb
5 oz.

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL.
ASSAY RECOMMENDED FOR ROCK AND CORE SAMPLES IF CU PB ZN AS > 1%, AG > 30 PPM & AU > 1000 PPB
- SAMPLE TYPE: ROCK AU** ANALYSIS BY FA/ICP FROM 30 GM SAMPLE.
Samples beginning 'RE' are Reruns and 'RRE' are Reject Reruns.

DATE RECEIVED: AUG 28 1995 DATE REPORT MAILED: Sept 1/95 SIGNED BY C. Leong .D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

32 oz ICP 6.70
Au 6.15
1.22
3.46
1.50

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APPENDIX C - Diamond Drill Logs, Assays, Trench samples

HOLE NO. SK91-04

INTERVAL FROM	INTERVAL TO	ROCK TYPE (composition, colour, texture, grain size)	ALTERATION	MINERALIZATION	Fr/m	STRUCTURE (Fractures, faults, folding, bedding, etc.)	Mineralization, type, age, relations
		hard (H=5-6) and "flinty". Some coarser grained sections contain silty clasts, 2-5mm, - rippied up siltstones. Core is blocky throughout with some strongly broken sections					
		4.6 - 30.0m Coarse asn tuff. Med. to light grey, 40% plag. clasts, 40% mafics (augite + hblde) 20% matrix, some siltstone fragments (5%). Siltstone interval at 14.4-14.8m	4.6 - 18.3 mod. K alt of matrix	4.6 - 16.9m py / FE / 2-4%		4.6 - 13.7 m very blocky core with rusty (weathered) fracture surfaces.	
			18.3-30.0 weak epidote alt, blebby and FE, v. weak K alt.	18.3-30.0 Py/D 4-9%, avg about 5%			
			Alteration best developed 19.0-27.2 where rock has a pinkish colour.	27.0 - 2.5cm wide qtz/calcite vein with galena 5%, minor cp. (1%)		Qtz/calcite vein at 68° to c.a.	
						27.2 - 29.7 Fault. Rubbly core, breccia, clay gouge.	
		30.0 - 53.3 Siltstone - med. to light grey, poorly to well bedded, fine grained, hard (H=5-6), dense, flinty - hornfels. Rock has a patchy, mottled light grey to pinkish grey	K alt is weak to moderate and patchy - as	Py / FE / 1-2% D / 1%		30.0 - 30.3 clay gouge zone	
			flooding with some FE. Epidote alteration is			33.8 bedding at 20° to c.a	
						40.0 bedding at 20° to c.a.	

DRILL HOLE NO. SK91-04

HOLE NO. SK91-04

DRILLING CO.	LOCATION SKETCH	DEPTH	TESTS DIP ANGLE	AZIMUTH		
Advanced Drilling Ltd.	- N -	COLLAR	-47°	003°	DATE STARTED: July 11, 1991	PROJECT: Skook Project
		100.6 m	-42°	003°	DATE COMPLETED: July 13, 1991	N.T.S.: 93 N/2
					COLLAR ELEV.:	LOCATION: North side of Chuchi Lake
					NORTHING: 6118100 (100+10 N)	
					EASTING: 403460 (102+00 E)	
					AZIMUTH: 003°	
					DEPTH: 100.6 m	DATE LOGGED: July 15, 1991
HOLE TYPE					CORE SIZE: NQ	LOGGED BY: E.R. Craigie

INTERVAL FROM	INTERVAL TO	ROCK TYPE (composition, colour, texture, grain size)	ALTERATION	MINERALIZATION	Fr/m	STRUCTURE (fractures, faults, folding, bedding, etc.)	REMARKS Mineralization, type, age relations
0	4.6m	Overburden					
4.6	100.6m	Volcaniclastic sediments: Unit varies from siltstones to greywackes (coarse ash tuffs). Colour is light to dark grey. Finer grained sections tend to be well-bedded, coarser grained sections are massive. Coarser sections are composed of 40% plag. crystals, 40% mafics (augite) 1-2mm in size, and 20% f.g. matrix. Clasts are mostly subrounded but good crystal forms do occur. Unit is hornfelsed and variably altered. Silty layers are	Alteration varies from weak to moderate. Bleaching is common, weak epidote and kalt. occur in some sections	Py is ubiquitous throughout unit. Avg. is about 2% mostly as fracture coatings but partly diss.		Late calcite filled fractures occur throughout the core.	

DRILL HOLE NO. SK91-04

HOLE NO. SK91-04

INTERVAL FROM	INTERVAL TO	ROCK TYPE (composition, colour, texture, grain size)	ALTERATION	MINERALIZATION	Fr/m	STRUCTURE (Fractures, faults, folding, bedding, etc.)	Mineralization, type, age, relations
		dense, fine grained, poorly to well bedded. Colour varies from dark grey to v. light brownish grey. Coarse ash tuff units occur from 72.1-73.2, 73.9-75.9, 81.5-84.4 and 89.6-90.6m. 82.3- large clast of siltstone, 1cm thick, 8cm long, occurs in ash tuff unit about 3cm above a siltstone bed. Rippel upcast- suggests rocks are sitting right way up.	across bedding. From 67.4 to 68.3 rock is bleached to light grey, is very hard (H=6) and mottled with pinkish grey patches - this is hornfelsed effed. Rock is only v. weakly K altered. 72.1-100.6 Kalt varies from weak to mod. in patchy sections. At 72.1-72.7 rock is strongly bleached but with no kalt- this is hornfelsed effed. At 88.4-88.8 rock is purplish coloured with weak K, chlorite and calcite as FE and FE alt.	72.1-73.8, Py /D / 4% FE / 1%		61.9-63.3 brecciated rubble with calcite veins and minor (2%) py. 88.0 beds at 25° to c.a. 89.6 Minor fault, 7cm wide, 75° to c.a., carbonate veins and clay gouge.	
		E.O.H. - 100.6m					

PAGE 4 OF 4

DRILL HOLE NO. SK91-04

HOLE NO. SK91-04

INTERVAL FROM	INTERVAL TO	ROCK TYPE (composition, colour, texture, grain size)	ALTERATION	MINERALIZATION	Fr/m	STRUCTURE (Fractures, faults, folding, bedding, etc.)	Mineralization, type, age, relations
		colouration, from alteration, in part fracture controlled, in part pervasive flooding - unit contains about 5% fine grained diss. biotite	generally weak as patchy blebs.				
			45.3-48.8 mod. to strong K alt, FE and pervasive flooding weak to mod. blebby epidote				
			50.6-51.2 well bedded unit strong K alt along beds.			50.9 bedding at 30° to c.a.	
		53.3-59.8 Coarse ash tuff: Plagioclase grains form 60% of rock, 1-3mm in size, in light grey, f.g., matrix. Mafics are less than 5%, mostly f.g. biotite	weak blebby epidote alt., mod to strong K alt., as pervasive flooding and FE.	Py / D / 1-2%			
		59.8 - 100.6 Siltstone unit with a few sections of coarse ash tuff. Similar to upper siltstones. Hard,	59.8 - 72.1 weak to mod, patchy K alt of siltstones alt is irregular, cuts	Py / D / 2% FE / minor		61.3 beds at 25° to c.a 69.5 beds at 20° to c.a.	

DRILL HOLE NO. SK91-04

SP 86.2

DRILL LOG sample data

SAMPLE					CORE RECOVERY		VISUAL ESTIMATES (% ORE MINERALS)	ASSAY RESULTS						
NUMBER	FROM	TO	TOTAL METRES	M.S.	%	AMT. LOST								
104182	56	58	2	.2	90	.2								
183	58	60	2	.2	85	.3								
184	60	62	2	.1	90	.2								
185	62	64	2	.3	95	.1								
186	64	66	2	.6	85	.3								
187	66	68	2	.2	85	.3								
188	68	70	2	.2	90	.2								
189	70	72	2	.3	95	.1								
190	72	74	2	.2	95	.1								
191	74	76	2	.2	90	.2								
192	76	78	2	.2	90	.2								
193	78	80	2	.3	65	.7								
194	80	82	2	.2	95	.1								
195	82	84	2	.1	90	.2								
196	84	86	2	.6	95	.1								
197	86	88	2	~~.9~~ .3	95	.1								
198	88	90	2	~~1.0~~ .4	85	.3								
199	90	92	2	.4	90	.2								
200	92	94	2	.3	75	.5								
201	94	96	2	.2	90	.2								
202	96	98	2	.1	80	.4								
203	98	100.6	2.6	.2	81	.5								
	EOH													

DRILL HOLE NO. _____

91-2880

DRILL LOG sample data

SAMPLE NUMBER	FROM	TO	TOTAL METRES	M.S.	CORE RECOVERY %	CORE RECOVERY AMT. LOST	VISUAL ESTIMATES (% ORE MINERALS)	ASSAY RESULTS						
104156	4.6	6.0m	1.4	.3	65	.5								
157	6.0	8.0	2	.4	40	1.2								
158	8.0	10.0	2	.2	65	.7								
159	10.0	12.0	2	.3	75	.5								
160	12.0	14.0	2	.5	75	.5								
161	14.0	16.0	2	.2	95	.1								
162	16.0	18.0	2	.2	70	.6								
163	18.0	20.0	2	.1	95	.1								
164	20.0	22.0	2	.1	70	.6								
165	22.0	24.0	2	.4	85	.3								
166	24.0	26.0	2	.1	90	.2								
167	26.0	28.0	2	.1	90	.2								
168	28.0	30.0	2	.1	80	.4								
169	30.0	32.0	2	.1	85	.3								
170	32.0	34.0	2	.3	90	.2								
171	34.0	36.0	2	.2	85	.3								
172	36.0	38.0	2	.3	90	.2								
173	38.0	46.0	2	.4	95	.1								
174	40.0	42.0	2	.2	90	.2								
175	42.0	44.0	2	.3	90	.2								
176	44.0	46.0	2	.1	85	.3								
177	46.0	48.0	2	.1	90	.1								
178	48.0	50.0	2	.3	85	.3								
179	50.0	52.0	2	.3	90	.1								
180	52.0	54.0	2	.5	90	.1								
181	54.0	56.0	2	.4	90	.1								

DRILL HOLE NO. SK-91-04

104200	92.0	94.0	151	5
104201	94.0	96.0	128	1
104202	96.0	98.0	154	12
104203	98.0	100.6	177	280

DRILLHOLE: SK91-04

ASSAY DATA

SAMPLE #	FROM	TO	Cu (ppm)	Au (ppb)
104156	4.6	6.0	152	1
104157	6.0	8.0	159	5
104158	8.0	10.0	141	3
104159	10.0	12.0	139	3
104160	12.0	14.0	168	1
104161	14.0	16.0	144	1
104162	16.0	18.0	130	1
104163	18.0	20.0	149	6
104164	20.0	22.0	158	6
104165	22.0	24.0	148	6
104166	24.0	26.0	110	3
104167	26.0	28.0	69	2
104168	28.0	30.0	91	2
104169	30.0	32.0	234	6
104170	32.0	34.0	114	8
104171	34.0	36.0	115	9
104172	36.0	38.0	118	4
104173	38.0	40.0	135	2
104174	40.0	42.0	61	1
104175	42.0	44.0	78	1
104176	44.0	46.0	73	1
104177	46.0	48.0	128	4
104178	48.0	50.0	113	3
104179	50.0	52.0	121	2
104180	52.0	54.0	108	3
104181	54.0	56.0	86	1
104182	56.0	58.0	53	3
104183	58.0	60.0	162	1
104184	60.0	62.0	104	1
104185	62.0	64.0	149	4
104186	64.0	66.0	166	7
104187	66.0	68.0	148	2
104188	68.0	70.0	119	1
104189	70.0	72.0	136	3
104190	72.0	74.0	132	2
104191	74.0	76.0	189	3
104192	76.0	78.0	165	13
104193	78.0	80.0	194	10
104194	80.0	82.0	194	22
104195	82.0	84.0	161	6
104196	84.0	86.0	172	9
104197	86.0	88.0	143	7
104198	88.0	90.0	141	5
104199	90.0	92.0	115	3

HOLE NO. SK91-07

INTERVAL FROM	INTERVAL TO	ROCK TYPE (composition, colour, texture, grain size)	ALTERATION	MINERALIZATION	Fr/m	STRUCTURE (Fractures, faults, folding, bedding, etc.)	Mineralization, type, age, relations
		in matrix of crowded plag. porph. Interval is 80% andesite, 20% plag. porph. monzonite.	chlorite alt; weak to mod, patchy K alt.	envelope. 35.5-42.3 cp/ D / 1% - should run 0.3t% Cu.	x	35.4-35.5 4cm qtz/epidote vein with 15% cp. at 45° 38.0 8cm zone of clay gouge with 5% cp. 38.3-38.9 clay gouge and breccia, with 5% cp. zone is subparallel to core axis	
42.3	45.2	Sediment - coarse ash tuff with some siltstone interbeds: coarse, crystal-rich sections look similar to plag. porphyry.	Mod. to str. FE and blebby epidote alt; mod. to str. pervasive chlorite alt; mod. pervasive K alt.	No significant sulphide mineralization		44.0-44.4 vuggy section, 10% open spaces	
45.2	61.4	Siltstone, fine ash tuff: light pinkish to salmon colour; v. fine grained, well bedded in some sections. Generally hard, dense, brittle rock - hornfelsed. Only weakly K altered.	Variable weak to mod. blebby and FE epidote; moderate FE chlorite alt; weak, patchy and FE K alt.	No significant sulphides. 54.7 minor (1-2%) blebs of black mineral, possibly sphalerite		Most pinkish coloured zones are a hornfelsed effect - not a result of K alteration. 47.4 1cm calcite veinlet 55° to c.a., 51.7 bedding at 40° to c.a. 56.2-61.0 v. blocky rubble zone	
61.4	108.0	Altered siltstone; with some coarse ash tuff units. From 101.0-108.0, coarse ash tuff unit, with 60-80% clasts of subrounded plagioclase	strong, pervasive chlorite alt; strong, blebby and FE epidote alt; weak to moderate	66.0-67.0 shear zone subparallel to c.a., with epidote calcite and 5% cp.		66.5-72.0 Breccia, gouge and rubble zone	

DRILL HOLE NO. SK91-07

HOLE NO. SK91-07

DRILLING CO.	LOCATION SKETCH	DEPTH	TESTS DIP ANGLE	AZIMUTH		
ADVANCED DRILLING LTD	-N-	COLLAR	-45°	183°	DATE STARTED: July 19, 1991	PROJECT: Skook Project
		152.4	-41°	183°	DATE COMPLETED: July 21, 1991	N.T.S.: 93N/2
					COLLAR ELEV.: 1003 m	LOCATION: North side of Chuchi Lake.
					NORTHING: 6119050	
					EASTING: 402370	
					AZIMUTH: 183°	
					DEPTH: 152.4 m	DATE LOGGED: July 22, 1991
HOLE TYPE					CORE SIZE: NQ	LOGGED BY: E.R. Craigie

INTERVAL FROM	INTERVAL TO	ROCK TYPE (composition, colour, texture, grain size)	ALTERATION	MINERALIZATION	Fr/m	STRUCTURE (fractures, faults, folding, bedding, etc.)	REMARKS Mineralization, type, age relations
0	3.0m	Overburden					
3.0	10.5	Plagioclase porphyritic monzonite: crowded to semi-crowded; medium to light grey; 80% plag phenos, 1-3mm, in f.g. matrix - contains patchy, purplish coloured zones with f.g. biotite (5-15%).	Moderate FE and blebby epidote, weak chlorite alt.	Cp. / D-blebs / 0.3% 9.0m - qtz/epidote vein, 7cm wide with 1% cp. 10.2m - 2cm qtz/epidote vein with 1% cp.		Late calcite filled fractures occur throughout core. Contact with lower andesite unit is diffuse, obscured by alteration.	
10.5	42.3	Andesite: dark greenish grey, fine grained. Contains zones of plagioclase porphyry, intruding volcanics. At 32.6 fragments of andesite occur	Moderate to strong FE and patchy blebs of epidote. Mod to strong, pervasive	11.8 m - 10cm qtz/epidote vein with 10-15% cp in vein and 5% in 6cm wide		Vein at 45° to c.a. 16.0-23.5 very blocky rubble zone with 10% clay gouge, minor hematite staining 34.8 1cm qtz/calcite vein, subparallel to c.a.	

DRILL HOLE NO. SK91-07

HOLE NO. SK91-07

INTERVAL FROM	INTERVAL TO	ROCK TYPE (composition, colour, texture, grain size)	ALTERATION	MINERALIZATION	Fr/m	STRUCTURE (Fractures, faults, folding, bedding, etc.)	Mineralization, type, age, relations
		matrix. Andesite unit is not strongly altered with ~~only~~ weak, pervasive chloritic alt. minor epidote and K-alt.					
121.5	148.9	Hybrid Unit; mix of plagioclase porphyritic monzonite and andesite. About equal proportions of intrusive and volcanic units, in irregular zones. Porphyry intrudes volcanics; volcanics are weakly contact metamorphosed - slightly re-cryst. with some purplish sections containing 5-10% f.g. biotite. Plag porph. is fairly matic with 20-30% of matrix, from assimilation of volcanic material. 139.9 - 145.2 agglomerate unit. angular to subrounded fragments up to lapilli size.	weak to mod K alt, primarily of matrix; mod to strong FE epidote and chlorite alt.	122.4 4cm qtz vein, minor cp 129.0 10cm wide shear/gouge zone with minor cp. 138.1 - 138.2 qtz/kspar veinlet with minor cp.		vein at 45° to c.a vein at 40° to c.a	
148.9	152.4	Plagioclase porphyritic monzonite: semi crowded to crowded plag. porph. with					

DRILL HOLE NO. SK91-07

HOLE NO. SK91-07

INTERVAL FROM	INTERVAL TO	ROCK TYPE (composition, colour, texture, grain size)	ALTERATION	MINERALIZATION	Fr/m	STRUCTURE (Fractures, faults, folding, bedding, etc.)	Mineralization, type, age, relations
		1-2mm. Interval has about 5% f.g. biotite and 10% chloritized augite ± hblde.	patchy K alt.	68.6 - 30cm with 0.5% cp		75.5 - 76.1 Fault zone - clay gouge and breccia.	
				75.6 - cp/1%/D over 0.3m.		80.2m bedding at 70°	
						85.4 - 91.1 Fault zone; rubble, clay gouge and breccia. From 87.7 to 91.1 zone consists of breccia with clasts of of variably altered fine ash tuffs	
				90.0 - 90.3 cp/D/0.5%			
				91.1, 98.2, 107.8 minor cp, py.		97.0 bedding at 65°	
						107.9 2cm wide calcite filled fracture, 15° to c.a.	
108.0	121.5	Andesite: augite porphyritic augite phenos from 1 to 5mm form 5-20% of rock in some sections. Rock is med to dark grey, v. fine grained. Contact with sediment at 108.0m is obscure. Chloritized seds are difficult to distinguish from andesite - seds have no augite phenos. Some sections of andesite have purplish tint from f.g. biotite. 121.5 - 122.6 fragments of volcani occur in plag porphyritic	weak, blebby epidote alt; weak pervasive chlorite alteration weak to mod., patchy K-alt of matrix.				

DRILL HOLE NO. SK91-07

DRILL LOG sample data

SAMPLE NUMBER	FROM	TO	TOTAL METRES	M.S.	CORE RECOVERY %	CORE RECOVERY AMT. LOST	VISUAL ESTIMATES (% ORE MINERALS)	ASSAY RESULTS						
1-4321	3.0	6.0m	3.0m	.1	55	.9								
322	6.0	8.0	2	.1	80	.4								
323	8.0	10.0	2	.1	90	.2								
324	10.0	12.0	2	.1	75	.5								
325	12.0	14.0	2	.1	90	.2								
326	14.0	16.0	2	0	70	.6								
327	16.0	18.0	2	0	35	1.3								
328	18.0	20.0	2	.1	50	1.0								
329	20.0	22.0	2	0	70	.6								
330	22.0	24.0	2	.1	50	1.0								
331	24.0	26.0	2	.1	90	.2								
332	26.0	28.0	2	.1	85	.3								
333	28.0	30.0	2	0	95	.1								
334	30.0	32.0	2	0	80	.4								
335	32.0	34.0	2	.1	80	.4								
336	34.0	36.0	2	0	90	.2								
337	36.0	38.0	2	.1	85	.3								
338	38.0	40.0	2	.1	80	.4								
339	40.0	42.0	2	0	85	.3								
340	42.0	44.0	2	0	40	.2								
341	44.0	46.0	2	0	90	.2								
342	46.0	48.0	2	0	85	.3								
343	48.0	50.0	2	.1	80	.4								
344	50.0	52.0	2	.1	95	.1								
345	52.0	54.0	2	0	80	.4								
346	54.0	56.0	2	0	95	.1								

DRILL HOLE NO. SK-91-07

HOLE NO. SK91-07

INTERVAL FROM	INTERVAL TO	ROCK TYPE (composition, colour, texture, grain size)	ALTERATION	MINERALIZATION	Fr/m	STRUCTURE (Fractures, faults, folding, bedding, etc.)	Mineralization, type, age, relations
		10% augite phenos. Contains					
		brownish purple, patchy				152.3 - 152.4 clay gouge seam.	
		sections with 5-10% f.g.					
		biotite					
		E.O.H. - 152.4 m					

DRILL HOLE NO. SK91-07

BP 54-2

DRILL LOG sample data

SAMPLE NUMBER	FROM	TO	TOTAL METRES	M.S.	CORE RECOVERY %	CORE RECOVERY AMT. LOST	VISUAL ESTIMATES (% ORE MINERALS)	ASSAY RESULTS						
104373	108	110	2	0	90	.2								
374	110	112	2	0	95	.1								
375	112	114	2	0	95	.1								
376	114	116	2	0	75	.5								
377	116	118	2	0	90	.2								
378	118	120	2	0	90	.2								
379	120	122	2	0	80	.4								
380	122	124	2	0	95	.1								
381	124	126	2	.1	95	.1								
382	126	128	2	0	90	.2								
383	128	130	2	0	95	.1								
384	130	132	2	0	95	.1								
385	132	134	2	0	95	.1								
386	134	136	2	0	90	.2								
387	136	138	2	.1	85	.3								
388	138	140	2	0	90	.2								
389	140	142	2	0	95	.1								
390	142	144	2	.1	85	.3								
391	144	146	2	0	90	.2								
392	146	148	2	0	95	.1								
393	148	150	2	0	95	.1								
394	150	152.4	2.4	0	88	.3								
EOH														

91-2997

BP 88-3

DRILL HOLE NO. SK-91-07

DRILL LOG sample data

SAMPLE NUMBER	FROM	TO	TOTAL METRES	M.S.	CORE RECOVERY %	AMT. LOST	VISUAL ESTIMATES (% ORE MINERALS)	ASSAY RESULTS						
104347	56	58	2	0	65	.7								
348	58	60	2	0	55	.9								
349	60	62	2	0	60	.8								
350	62	64	2	0	65	.7								
351	64	66	2	0	85	.3								
352	66	68	2	.1	90	.2								
353	68	70	2	0	80	.4								
354	70	72	2	.1	65	.7								
355	72	74	2	0	85	.3								
356	74	76	2	0	80	.4								
357	76	78	2	0	80	.4								
358	78	80	2	0	95	.1								
359	80	82	2	.1	85	.3								
360	82	84	2	0	85	.3								
361	84	86	2	0	80	.4								
362	86	88	2	0	85	.3								
363	88	90	2	.1	85	.3								
364	90	92	2	.1	85	.3								
365	92	94	2	.1	80	.4								
366	94	96	2	0	75	.5								
367	96	98	2	0	90	.2								
368	98	100	2	0	90	.2								
369	100	102	2	0	85	.3								
370	102	104	2	.1	80	.4								
371	104	106	2	0	85	.3								
372	106	108	2	0	90	.2								

DRILL HOLE NO. SK-91-07

DRILLHOLE: SK91-07

ASSAY DATA

SAMPLE #	FROM	TO	Cu (ppm)	Au (ppb)
104321	3.0	6.0	1308	1
104322	6.0	8.0	831	1
104323	8.0	10.0	1083	1
104324	10.0	12.0	3640	2
104325	12.0	14.0	1483	1
104326	14.0	16.0	612	3
104327	16.0	18.0	265	6
104328	18.0	20.0	147	3
104329	20.0	22.0	1261	2
104330	22.0	24.0	944	3
104331	24.0	26.0	203	2
104332	26.0	28.0	199	2
104333	28.0	30.0	170	3
104334	30.0	32.0	200	3
104335	32.0	34.0	284	3
104336	34.0	36.0	3002	13
104337	36.0	38.0	6387	320
104338	38.0	40.0	27107	1650
104339	40.0	42.0	14207	840
104340	42.0	44.0	147	5
104341	44.0	46.0	50	4
104342	46.0	48.0	198	9
104343	48.0	50.0	17	6
104344	50.0	52.0	18	16
104345	52.0	54.0	8	4
104346	54.0	56.0	10	5
104347	56.0	58.0	100	5
104348	58.0	60.0	113	4
104349	60.0	62.0	3872	1
104350	62.0	64.0	739	3
104351	64.0	66.0	4554	9
104352	66.0	68.0	1402	8
104353	68.0	70.0	876	2
104354	70.0	72.0	329	3
104355	72.0	74.0	83	3
104356	74.0	76.0	709	1
104357	76.0	78.0	202	1
104358	78.0	80.0	1077	1
104359	80.0	82.0	34	1
104360	82.0	84.0	11	1
104361	84.0	86.0	383	3
104362	86.0	88.0	37	2
104363	88.0	90.0	208	2
104364	90.0	92.0	926	1

1650
840
2490
2 1245

2.1%
1.4%
4.1 ÷ 2 = 2.05% cu

4m

104365	92.0	94.0	71	2
104366	94.0	96.0	326	1
104367	96.0	98.0	1425	1
104368	98.0	100.0	305	2
104369	100.0	102.0	19	4
104370	102.0	104.0	10	2
104371	104.0	106.0	22	1
104372	106.0	108.0	88	1
104373	108.0	110.0	1230	1
104374	110.0	112.0	220	1
104375	112.0	114.0	23	1
104376	114.0	116.0	12	3
104377	116.0	118.0	26	1
104378	118.0	120.0	5	1
104379	120.0	122.0	2998	2
104380	122.0	124.0	1293	2
104381	124.0	126.0	233	2
104382	126.0	128.0	163	2
104383	128.0	130.0	241	2
104384	130.0	132.0	289	9
104385	132.0	134.0	22	8
104386	134.0	136.0	19	4
104387	136.0	138.0	79	1
104388	138.0	140.0	98	4
104389	140.0	142.0	689	4
104390	142.0	144.0	64	2
104391	144.0	146.0	16	2
104392	146.0	148.0	8	2
104393	148.0	150.0	8	1
104394	150.0	152.4	76	1

HOLE NO. SK91-09

INTERVAL FROM	INTERVAL TO	ROCK TYPE (composition, colour, texture, grain size)	ALTERATION	MINERALIZATION	Fr/m	STRUCTURE (Fractures, faults, folding, bedding, etc.)	Mineralization, type, age, relations
21.8	32.8	Altered coarse ash tuff: - light greenish grey to near white. Rock is strongly brecciated with a few reddish coloured partly altered fragments 22.2-23.2 Breccia composed of qtz. vein fragments Unit is weakly calcareous (2-4%) until 29m, then contains about 10% calcite for rest of interval	Alteration of unit occurs as broad envelope of bleaching around quartz vein interval at 32.8-39.0. Alteration is pervasive with only a few volc. fragments retaining reddish cores.	22.2-24.6 Interval is brecciated with some qtz veins, 1-5% diss galena, sph. 10% barite + calcite, very irregular banding of calcite and barite		Contact with red unaltered ash tuff is sharp, sheared, marked by 30cm wide qtz vein 27.4-33.2 Clay gouge breccia. Fragments of green volcs and qtz veins in clay gouge matrix 28.4 - 4cm wide white qtz vein 29.0, 31.1 - 10cm wide sections of 75% calcite 30.5-31.0 pinkish coloured qtz vein with minor py and galena (< 1%).	
32.8	39.0	Quartz vein. Interesting rock. Quartz is brecciated and re-healed, chalcedonic with irregular thin bands in some sections. Colour varies from white to clear to pink and green. Some narrow sections (up to a few cms)		Minor diss. galena and sphalerite (<1%) occur throughout interval. Sphalerite is light brown (honey) colour		36.0m banding of quartz varies from 15° to 30° to c.a.	

DRILL HOLE NO. SK91-09

HOLE NO. SK91-09

DRILLING CO.	LOCATION SKETCH	DEPTH	TESTS DIP ANGLE	AZIMUTH		
ADVANCED DRILLING LTD	-N-	COLLAR	-46°	003°	DATE STARTED: July 23, 1991	PROJECT: Skook Project
					DATE COMPLETED: July 25, 1991	N.T.S.: 93N/1
					COLLAR ELEV.:	LOCATION:
					NORTHING: 6119340 (111+90N)	North side of Chuchi Lake
					EASTING: 407970 (147+70E)	- Wit Zone
					AZIMUTH: 003°	
					DEPTH: 59.4 m	DATE LOGGED: July 26, 1991
HOLE TYPE					CORE SIZE: NQ	LOGGED BY: E.R. Craigie

INTERVAL FROM	INTERVAL TO	ROCK TYPE (composition, colour, texture, grain size)	ALTERATION	MINERALIZATION	Fr/m	STRUCTURE (fractures, faults, folding, bedding, etc.)	REMARKS Mineralization, type, age relations
0	3.0 m	Overburden					
3.0	21.8	Coarse ash tuff: Brick red colour, very blocky and fractured. Strongly hematitic - impairs colour to unit. Coarse clasts vary from 1-3 mm with a few lapilli size fragments. Clasts are heterolithic - 25% mafic crystals (augite), 45% plagioclase crystals, 25% lithic fragments. Clasts form 40-80% of rock in f.g. matrix. Unit is strongly calcareous, 5-10% calcite		10.6 m - 5cm wide qtz vein with 10% cp.			

DRILL HOLE NO. SK91-09

HOLE NO. SK91-09

INTERVAL FROM	INTERVAL TO	ROCK TYPE (composition, colour, texture, grain size)	ALTERATION	MINERALIZATION	Fr/m	STRUCTURE (Fractures, faults, folding, bedding, etc.)	Mineralization, type, age, relations
55.5	59.4	No core recovered. Hole lost in bad ground at 59.4 m.					
		E.O.H. - 59.4 m.					

DRILL HOLE NO. SK91-09

HOLE NO. SK91-09

INTERVAL FROM	INTERVAL TO	ROCK TYPE (composition, colour, texture, grain size)	ALTERATION	MINERALIZATION	Fr/m	STRUCTURE (Fractures, faults, folding, bedding, etc.)	Mineralization, type, age, relations
		are massive calcite. Unit is a tectonized epithermal quartz vein.					
39.0	53.0	Plagioclase, augite porphyry Colour varies from dark reddish brown to dark greenish brown. Core is very blocky. Interval is strongly brecciated throughout. Fragments of porphyry are partly re-healed with qtz. Porphyry consists of about 10% phenocrysts, 1-3mm in size. Composition of phenos is 50% plag, 50% augite. Matrix is very fine grained.	Colour variations are a result of alteration. Red-brown unit is bleached to greenish colour, bleaching increases towards base of interval. Upper sections have fragments with brown cores, greenish rims; green colour is pervasive near base of interval.	Unit contains minor py Py / D / 1%.		39.0 - 39.6 rubble zone with 20% clay gouge	
		48.0 - 48.2 banded qtz veins					
53.0	55.5	Quartz veins. Very blocky core. Veins are brecciated and re-healed		1-2% diss. light brown coloured sphalerite			

DRILL HOLE NO. SK91-09

DRILLHOLE: SK91-9

ASSAY DATA

SAMPLE #	FROM	TO	Cu (ppm)	Au (ppb)
104469	3.0	6.0	39	8
104470	6.0	8.0	55	9
104471	8.0	10.0	56	9
104472	10.0	12.0	57	18
104473	12.0	14.0	8	6
104474	14.0	16.0	22	10
104475	16.0	18.0	26	11
104476	18.0	20.0	191	9
104477	20.0	22.0	61	30
104478	22.0	24.0	43	451
104479	24.0	26.0	24	62
104480	26.0	28.0	31	43
104481	28.0	30.0	23	40
104482	30.0	32.0	25	42
104483	32.0	34.0	49	148
104484	34.0	36.0	24	75
104485	36.0	38.0	46	152
104486	38.0	40.0	28	83
104487	40.0	42.0	88	67
104488	42.0	44.0	30	29
104489	44.0	46.0	45	16
104490	46.0	48.0	75	44
104491	48.0	50.0	28	59
104492	50.0	52.0	39	24
104493	52.0	54.0	38	127
104494	54.0	55.5	38	341

DRILL LOG sample data

SAMPLE NUMBER	FROM	TO	TOTAL METRES	M.S.	CORE RECOVERY %	CORE RECOVERY AMT. LOST	VISUAL ESTIMATES (% ORE MINERALS)	ASSAY RESULTS						
104469	2.0	6.0	3m	.5	110	1.8								
470	6.0	8.0	2	.4	45	1.1								
471	8.0	10.0	2	.3	50	1.0								
472	10.0	12.0	2	.3	45	1.1								
473	12.0	14.0	2	.2	85	0.3								
474	14.0	16.0	2	.6	85	0.3								
475	16.0	18.0	2	.3	80	0.4								
476	18.0	20.0	2	.7	70	0.6								
477	20.0	22.0	2	.6	95	0.5								
478	22.0	24.0	2	0	60	0.9								
479	24.0	26.0	2	0	65	0.7								
480	26.0	28.0	2	0	70	0.6								
481	28.0	30.0	2	0	45	1.1								
482	30.0	32.0	2	0.1	75	0.5								
483	32.0	34.0	2	0	70	0.6								
484	34.0	36.0	2	0	80	0.4								
485	36.0	38.0	2	0	75	0.5								
486	38.0	40.0	2	0.1	65	0.7								
487	40.0	42.0	2	0.2	85	0.3								
488	42.0	44.0	2	0.6	75	0.5								
489	44.0	46.0	2	2.5	65	0.7								
490	46.0	48.0	2	0.2	90	0.2								
491	48.0	50.0	2	0.1	80	0.4								
492	50.0	52.0	2	0.1	80	0.4								
493	52.0	54.0	2	0.2	40	1.2								
494	54.0	55.5	1.5	0.0	47	0.9								

PAGE 1 OF 1

DRILL HOLE NO. [illegible]-91-09

HOLE NO. SK91-10

INTERVAL FROM	INTERVAL TO	ROCK TYPE (composition, colour, texture, grain size)	ALTERATION	MINERALIZATION	Fr/m	STRUCTURE (Fractures, faults, folding, bedding, etc.)	Mineralization, type, age, relations
		greenish grey colour - sausseritic. Unit contains 5-10% calcite as diss, FF and filling vesicles. 27.4-32.6m Rock is dark greenish grey colour, gradational from red over 2m at upper contact, abrupt change back to red at lower contact.				55.7 - 57.6m Breccia zone with 30% clay gouge.	
57.6	74.4	Brecciated quartz vein - rock is light to dark grey, very blocky, composed of qtz vein fragments in sand, silt and clay matrix. Fragments make up 60% of rock and range in size from coarse sand to 10 cm. Most fragments are quartz - milky white to pink to grey, sometimes banded and zoned (calcedonic) Upper 1m contains greenish grey fragments of volcanics, lower 0.5m contains fragments of brownish grey coloured	Interval is strongly calcareous - 15-20% calcite	57.6-67.1 interval contains 2-3% sulphides, mostly sphalerite (2%) with minor py. and galena. Mineralization occurs mostly as fragments within breccia. No massive or banded zones. Interval might run 2% Zn+Pb.		Contact with upper volcanic is sharp 75° to C.A.	
				67.1-69.9 Contains 10-15% sulphides, mostly sphalerite (8-10%), with			

DRILL HOLE NO. SK91-10

HOLE NO. SK91-10

DRILLING CO.	LOCATION SKETCH	DEPTH	TESTS DIP ANGLE	AZIMUTH		
ADVANCED DRILLING LTD.	-N-	COLLAR	-46°	178°	DATE STARTED: July 25, 1991	PROJECT: Skook Project
					DATE COMPLETED: July 27, 1991	N.T.S.: 93N/1
		94.5m	-44°	178°	COLLAR ELEV.:	LOCATION:
					NORTHING: 6119430	North side of Churchi
					EASTING: 407970	Lake - Wit Zone
					AZIMUTH: 178°	
					DEPTH: 94.5m	DATE LOGGED: July 27, 1991
HOLE TYPE					CORE SIZE: NQ	LOGGED BY: E.R. Craigie

INTERVAL FROM	INTERVAL TO	ROCK TYPE (composition, colour, texture, grain size)	ALTERATION	MINERALIZATION	Fr/m	STRUCTURE (fractures, faults, folding, bedding, etc.)	REMARKS Mineralization, type, age relations
0	18.3m	Casing: Hole was cased down to 18.3m to prevent caving. Overburden depth is 3 metres.					
18.3	57.6	Plagioclase porphyritic latite (probable flow). Brick red colour - strongly hematitic. Phenocrysts form 30-40% of rock, are 1-5mm in size, in v.f.g. brick red matrix. About 5-10% of phenos are mafic's (augite ± hblde), dark green to black coloured, often hematite stained. Plag phenos are soft,				26-32 m very blocky core 29.9m 10cm zone of clay gouge.	

DRILL HOLE NO. SK91-10

HOLE NO. SK91-10

INTERVAL FROM	INTERVAL TO	ROCK TYPE (composition, colour, texture, grain size)	ALTERATION	MINERALIZATION	Fr/m	STRUCTURE (Fractures, faults, folding, bedding, etc.)	Mineralization, type, age, relations
		qtz vein, brown porphyry,					
		volcanics in f.g. rock		92.4 - 20%			
		flour matrix. About 40%		galena over			
		fragments, 60% matrix.		6 cm.			
		92.6-94.5 rubble zone					
		no good core, 2-6 cm		93.3 massive			
		fragments of rubble.		sphalerite +			
				galena over			
		Hole lost at 94.5m in		6 cm.			
		bad ground.					
		E.O.H. 94.5m.					

DRILL HOLE NO. SK91-10

HOLE NO. SK91-10

INTERVAL FROM	INTERVAL TO	ROCK TYPE (composition, colour, texture, grain size)	ALTERATION	MINERALIZATION	Fr/m	STRUCTURE (Fractures, faults, folding, bedding, etc.)	Mineralization, type, age, relations
		porphyry dike.		galena (2-4%) and minor py, cp. Some sections are well mineralized with 30% light brown sphalerite over 6cm. Sulphides occur as blebs (1-2cm), diss. and irregular (0.5cm wide) bands with calcite. Zone should run 8% combined Zn + Pb (6% Zn and 2% galena).			
				69.9 - 74.4 Contains 4-6% sulphides, about 2% py, 2% sph., minor py (< 1%) and cp (< 1%). Zone should run 2-3% Zn+Pb+Cu.			
74.4	88.6m	Brown porphyry dike (Syenite) Interval is extremely blocky, largest piece of core is 6cm, core consists of 40% porphyry fragments and 60% clay gouge. Phenos make up 10-15% of porphyry in v.f.g. brownish matrix. Phenos are 1-2mm, 50% altered plag., 50% mafics (augite + hblde).	Porphyry is altered to a med. to dk. grey but contains relic, unaltered brownish red sections. Interval is strongly chloritized, contains 5% calcite as FF.	Py/D/4-5% ~~93.4 20% galena over 6cm.~~ ~~93.3 massive sphalerite + galena over 6cm.~~		77.8 16cm wide banded qtz vein, brecciated and re-healed.	
88.6	94.5m	Clay gouge breccia: - mixed fragments of					

DRILL HOLE NO. SK91-10

BP 8A 2

DRILL LOG sample data

SAMPLE					CORE RECOVERY		VISUAL ESTIMATES (% ORE MINERALS)	ASSAY RESULTS						
NUMBER	FROM	TO	TOTAL METRES	M.S.	%	AMT. LOST								
104521	70	72		0	80	0.4								
522	72	74		0	60	0.8								
523	74	76		0.1	55	0.9								
524	76	78		0.7	60	0.8								
525	78	80		0.5	60	0.8								
526	80	82		0.2	70	0.6								
527	82	84		0.4	60	0.9								
528	84	86		0.1	65	0.7								
529	86	88		0.2	55	0.9								
530	88	90		0.1	85	0.3								
531	90	92		0	75	0.5								
532	92	92.5	2.5	0.1	64	0.9								

91-324

DRILL HOLE NO St. 91-10

DRILL LOG sample data

SAMPLE NUMBER	FROM	TO	TOTAL METRES	M.S.	CORE RECOVERY %	AMT. LOST	VISUAL ESTIMATES (% ORE MINERALS)	ASSAY RESULTS						
10449.5	17.7	20	2.3	0.1	91	0.2								
496	20	22		0.1	85	0.3								
497	22	24		0.2	75	0.5								
498	24	26		0.2	80	0.4								
499	26	28		0.2	65	0.7								
500	28	30		0.1	50	1.0								
501	30	32		2.1	80	0.4								
502	32	34		0.9	85	0.3								
503	34	36		0.4	80	0.4								
504	36	38		0.2	90	0.2								
505	38	40		0.1	90	0.2								
506	40	42		0.1	90	0.2								
507	42	44		0.1	95	0.1								
508	44	46		0.1	90	0.2								
509	46	48		0.5	85	0.3								
510	48	50		0.8	80	0.4								
511	50	52		0.3	85	0.3								
512	52	54		0.2	90	0.2								
513	54	56		0.9	75	0.5								
514	56	58		0.1	85	0.3								
515	58	60		0	55	0.9								
516	60	62		0	75	0.5								
517	62	64		0	70	0.6								
518	64	66		0	70	0.6								
519	66	68		0	80	0.4								
520	68	70		0	75	0.5								

DRILL HOLE NO. SK-91-10

BP88-3

HOLE NO. SK 91-11

DRILLING CO.	LOCATION SKETCH	DEPTH	TESTS DIP ANGLE	AZIMUTH			
ADVANCED DRILLING LTD.	- N -	COLLAR	-60°	0°	DATE STARTED: 23/09/91	PROJECT: SKOOK	
		151.8 m	-56°	0°	DATE COMPLETED: 25/09/91	N.T.S.: 93N/2	
					COLLAR ELEV.: 1045 m	LOCATION: Grid Coords:	
					NORTHING: 6118959 N	108+89 N	
					EASTING: 402258 E	90+38 E	
					AZIMUTH: 0°		
					DEPTH: 151.8 m	DATE LOGGED: SEPT. 24th-25th, 1991	
HOLE TYPE DDH					CORE SIZE: NQ	LOGGED BY: CTB	

INTERVAL FROM	INTERVAL TO	ROCK TYPE (composition, colour, texture, grain size)	ALTERATION	MINERALIZATION	Fr/m	STRUCTURE (fractures, faults, folding, bedding, etc.)	REMARKS Mineralization, type, age relations
0	3.0	OVERBURDEN					
3.0	29.6	SILTSTONE AND MONZONITE INTERCALATED: medium and fine grained, grey to light grey volcaniclastic siltstone (65%) and fine grained biotite hornblende plagioclase monzonite (35%) Non to slightly magnetic	BT/P/4 EP-BL/FF-DB/3 CB/FF/3			Broken core: 6.7-7.2, 12.2-12.8, 15.8-16.2, 21.7-22.3 Bedding 40° C.A. Fractures in multiple orientations; minor	
29.6	31.7	FAULT ZONE: altered siltstone and chlorite-carbonate-quartz-epidote rubble; Non-magnetic	EP-CH/P/7 CB-QTZ/FF/5	CPY-PY/V/1%		Broken core and rubble 31.0-31.8 Bedding 32° C.A.	

DRILL HOLE NO. SK 91-11

DRILLHOLE: SK91-10

ASSAY DATA

SAMPLE #	FROM	TO	Cu (ppm)	Au (ppb)
104495	17.7	20.0	7	15
104496	20.0	22.0	8	5
104497	22.0	24.0	9	2
104498	24.0	26.0	9	5
104499	26.0	28.0	17	6
104500	28.0	30.0	31	6
104501	30.0	32.0	103	3
104502	32.0	34.0	47	3
104503	34.0	36.0	35	6
104504	36.0	38.0	98	5
104505	38.0	40.0	253	5
104506	40.0	42.0	109	7
104507	42.0	44.0	15	3
104508	44.0	46.0	13	4
104509	46.0	48.0	24	3
104510	48.0	50.0	33	2
104511	50.0	52.0	150	4
104512	52.0	54.0	33	1
104513	54.0	56.0	114	10
104514	56.0	58.0	136	136
104515	58.0	60.0	20	1281
104516	60.0	62.0	32	620
104517	62.0	64.0	99	346
104518	64.0	66.0	44	200
104519	66.0	68.0	132	346
104520	68.0	70.0	182	588
104521	70.0	72.0	208	263
104522	72.0	74.0	57	315
104523	74.0	76.0	258	97
104524	76.0	78.0	46	75
104525	78.0	80.0	24	94
104526	80.0	82.0	39	123
104527	82.0	84.0	65	41
104528	84.0	86.0	40	38
104529	86.0	88.0	38	47
104530	88.0	90.0	46	62
104531	90.0	92.0	111	83
104532	92.0	94.5	164	220

HOLE NO. SK 91-11

INTERVAL FROM	INTERVAL TO	ROCK TYPE (composition, colour, texture, grain size)	ALTERATION	MINERALIZATION	Fr/m	STRUCTURE (Fractures, faults, folding, bedding, etc.)	Mineralization, type, age, relations
93.8	97.2	FAULT ZONE: rock flour, grit and angular pebble-sized fragments in quartz and calcite cement; unmineralized	CH-CB/P/5 EP/FF/3	PY/DB/tr		some broken core and rubble; generally moderately-well cemented, with 10-20% porosity	
97.2	100.0	MONZONITE: medium-grained hornblende monzonite dike (?); non-magnetic	CH-CB/P/6 EP-CB-GT/FF/4 BT/FF/4			Numerous hairline fractures, many orientations Hornblende only cumulate phase; like hornblende lamprophyres.	
100.0	105.9	SILTSTONE AND MONZONITE INTERCALATED: as above; skarn type alteration assemblage locally.	EP-GT/P/8 → EP/FF-DB/6 K-CH/P/4	→ 100.0-100.5 PY/DB-FF/tr.		Bedding 0-50° CA, variable	
105.9	116.0	FAULT ZONE: altered Siltstone and quartz vein material as broken core and rubble; 2-4% CPY over 45-cm intervals	CH/P/6 EP/FF/4 QTZ-CB/P-V/7 K/P/4 ↳ locally in siltstone	PY/DB-V/2% locally CPY/V/2% → 105.8-106.2 CPY/V/4% → 108.2-108.8		Predominantly broken core and rubble	

DRILL HOLE NO. SK 91-11

HOLE NO. SK 91-11

INTERVAL FROM	INTERVAL TO	ROCK TYPE (composition, colour, texture, grain size)	ALTERATION	MINERALIZATION	Fr/m	STRUCTURE (Fractures, faults, folding, bedding, etc.)	Mineralization, type, age, relations
31.7	41.7	SILTSTONE AND MONZONITE INTERCALATED: as above, with fracture-controlled metasomatic recrystallization of medium grained Siltstone gradational with medium grained hornblende Monzonite non to slightly magnetic	EP-CH/FF-P/3 K/P/3	PY/FF-BD/.2%	locally	Bedding 27° C.A. Monzonite non-porphyritic	
41.7	42.1	SULFIDE-QUARTZ VEIN in FAULT: 28% sulfide: 18% CPY, 10% PY as vein	CH/P/8 QTZ/P-V/6	CPY/P-V/18% PY/V/10%		Broken core and rubble; also one veinlet 0.2 cm thick at 40° to C.A.	
42.1	61.0	SILTSTONE AND MONZONITE INTERCALATED: as above, with grey medium-grained and pink fine-grained siltstone, and medium grained monzonite; slightly magnetic; trace MoS_2 locally	K/FF-BD/5 BT/P-FF/3 CH/DB/5 QTZ/BD/3 →	PY/FF/0.1% MoS_2/DB-FF/0.1% (56-59m)		Bedding undulating 30° to 0° C.A. K-flooding in pink siltstone with silica & MoS_2 → related to syenite-granite? - possible synchronous K-flooding and soft-sediment deformation at 56.0-59.0 m	
61.0	93.8	MONZONITE: fine grained, grey to maroon grey, hornblende biotite plagioclase monzonite; slightly magnetic with intercalated siltstone (25%); trace CPY locally	BT-K/P/4-8 EP-BL/FF/3-6 CH/P/3 CB/FF/3	PY/FF-DB/0.3% (81-85.0m) CPY/FF-DB/0.2% (82-83.0m)		Fault with chlorite rubble 69.4-70.0, 85.0-85.3 Broken core 91.7-93.8 PY+CPY associated with epidote, strong biotite alteration with 0.2% magnetite 88.5-91.8 m	

DRILL HOLE NO. SK 91-11

91-4810

DRILL LOG sample data

SAMPLE NUMBER	FROM	TO	TOTAL METRES	M.S.	CORE RECOVERY %	CORE RECOVERY AMT. LOST	VISUAL ESTIMATES (% ORE MINERALS)	ASSAY RESULTS						
	3.0	4.0	1.0	0.2	100	0								
	4	6	2	0.1	75	.5								
100076	6	8	2	0	65	.7								
100077	8	10	2	0	100	0								
	10	12	2	0	95	.1								
100078	12	14	2	.1	75	.5								
100079	14	16	2	.1	95	.1								
	16	18	2	.1	90	.2								
	18	20	2	.1	100	0								
	20	22	2	.1	100	0								
	22	24	2	.1	90	.2								
	24	26	2	.1	100	0								
	26	28	2	.1	100	0								
100080	28	30	2	.1	90	.2								
100081	30	32	2	.1	90	.2								
	32	34	2	0	100	0								
	34	36	2	.1	100	0								
	36	38	2	.1	100	0								
100082	38	40	2	.2	95	.1								
100083	40	42	2	.1	100	.2								
100084	42	44	2	0	95	.1								
	44	46	2	0	100	0								
100085	46	48	2	.3	80	.4								
	48	50	2	.1	100	0								
	50	52	2	.1	95	.1								
	52	54	2	.1	95	.1								

DRILL HOLE NO SK 91-11

HOLE NO. SK 91-11

INTERVAL FROM	INTERVAL TO	ROCK TYPE (composition, colour, texture, grain size)	ALTERATION	MINERALIZATION	Fr/m	STRUCTURE (Fractures, faults, folding, bedding, etc.)	Mineralization, type, age, relations
116.0	126.4	SILTSTONE: medium and fine grained grey siltstone, as above; with two 3 & 10 cm thick quartz-aplite dikes	EP/FF-P/4 QTZ-CB/FF/3 BL/FF/4	PY/FF-DB/.5-.8%		Bedding 15°-35° to C.A. Granite dikes 125.5, 125.9; 80°, 30° to C.A. respectively. PY associated with fractures & Quartz-Carbonate veinlet/fracture fillings	
126.4	128.8	MONZONITE: medium grained hornblende biotite plagioclase monzonite, slightly magnetic	CH-CB/FF/5 EP/FF/2			Fault zone with moderate chlorite and calcite alteration, brittle deformation at 127.9-128.4m	
128.8	147.0	SILTSTONE: very fine grained bedded ash tuffs, as above	EP/FF/4 K/P/3 CH/DB/4 locally	PY/DB-FF/.3% → 133.0-138.5 140.0-144.0 PY/DB-FF/1.0-5.0% 144-146.0		granitic dikes 1-3 cm thick at 138.6, 137.0 Soft sediment deformation breccia at 130.4-130.6, 131.5-131.8 Broken core: 128.8-130.3, 138.3-138.7, 139.7-140.0, 145.5-145.8	
147.0	151.8 EOH	MONZONITE: as above, medium and coarse grained hornblende biotite plagioclase monzonite, subporphyritic; slightly magnetic	CH-EP/FF-DB/3 BT/P/3 QTZ/FF/3	PY/DB-FF/0.3%		Metasomatized Siltstone 148.9-149.3m Granitic vein at 25° to C.A 151.6-151.7m	

DRILL HOLE NO. SK 91-11

BP 66.2

DRILL LOG sample data

SAMPLE NUMBER	FROM	TO	TOTAL METRES	M.S.	CORE RECOVERY %	CORE RECOVERY AMT. LOST	VISUAL ESTIMATES (% ORE MINERALS)	ASSAY RESULTS						
100096	106	108	2	.1	90	.2								
100097	108	110	2	0	75	.5								
100098	110	112	2	0	80	.4								
	112	114	2	0	90	.2								
	114	116	2	0	80	.4								
	116	118	2	0	95	.1								
	118	120	2	0	100	0								
	120	122	2	.1	100	0								
100099	122	124	2	.2	100	0								
100100	124	126	2	0	100	0								
	126	128	2	.1	100	0								
	128	130	2	0	75	.5								
100101	130	132	2	.1	100	0								
100102	132	134	2	.2	100	0								
100103	134	136	2	.1	100	0								
100104	136	138	2	.1	100	0								
100105	138	140	2	.1	75	.5								
	140	142	2	0	65	.7								
100106	142	144	2	.1	100	0								
100107	144	146	2	.1	95	.1								
	146	148	2	.1	100	0								
	148	150	2	.2	100	0								
	150	151.8	1.8	0	100	0								
	EOH													
		91-4810												

BP 88-3

DRILL HOLE NO SK91-11

DRILL LOG sample data

SAMPLE NUMBER	FROM	TO	TOTAL METRES	M.S.	CORE RECOVERY %	CORE RECOVERY AMT. LOST	VISUAL ESTIMATES (% ORE MINERALS)	ASSAY RESULTS						
	54	56	2	.2	100	0								
100086	56	58	2	.1	100	0								
	58	60	2	.1	100	0								
	60	62	2	.1	100	0								
	62	64	2	0	100	0								
	64	66	2	0	100	.1								
	66	68	2	0	100	0								
	68	70	2	.1	90	.2								
	70	72	2	.1	100	0								
	72	74	2	.1	100	0								
	74	76	2	.1	100	0								
	76	78	2	.1	90	.2								
	78	80	2	.2	100	0								
100087	80	82	2	.1	100	0								
100088	82	84	2	.1	100	0								
100089	84	86	2	.1	100	0								
	86	88	2	.1	95	.1								
	88	90	2	.1	95	.1								
	90	92	2	.5	100	0								
100090	92	94	2	.1	90	.2								
100091	94	96	2	0	95	.1								
100092	96	98	2	0	95	.1								
100093	98	100	2	.1	95	.1								
100094	100	102	2	0	100	0								
100095	102	104	2	0	95	.1								
107751	104	106	2	0	80	.4								

DRILL HOLE NO SK 91-11

BP 88-3

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

Skook | ANOM

BP Resources Canada Ltd. PROJECT 10161 File # 91-2880 Page 1

700 - 890 W. Pender St., Vancouver BC V6B 4W3

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
A 104156	3	152	2	20	.2	28	28	279	3.60	2	9	ND	1	61	.5	2	3	57	1.69	.158	3	36	.83	98	.13	9	1.67	.20	.22	1	1
RE A 104161	3	140	2	22	.2	29	18	192	3.22	2	6	ND	3	41	.6	2	2	52	1.82	.154	6	33	.46	72	.11	7	1.45	.14	.20	1	2
A 104157	3	159	2	21	.1	27	26	287	3.99	2	5	ND	1	62	.5	2	2	87	1.24	.157	6	26	.79	100	.14	4	1.26	.18	.24	1	5
A 104158	2	141	2	33	.1	22	17	245	3.32	2	5	ND	2	63	.6	2	6	72	1.53	.149	6	32	.57	88	.15	6	1.67	.17	.21	1	3
A 104159	2	139	2	24	.1	24	18	227	3.43	2	5	ND	2	59	.6	2	2	67	1.58	.152	5	34	.65	78	.14	7	1.68	.16	.20	1	3
A 104160	3	168	2	22	.1	24	22	229	3.62	2	7	ND	2	71	.7	2	2	57	1.82	.147	4	34	.61	90	.12	6	1.68	.17	.23	1	1
A 104161	3	144	2	23	.1	28	18	191	3.18	2	5	ND	2	40	.6	2	2	53	1.82	.151	6	32	.45	68	.12	9	1.44	.14	.17	1	1
A 104162	2	130	3	27	.1	26	17	254	3.34	2	5	ND	2	46	.7	2	2	74	1.84	.148	6	39	.69	59	.14	7	1.72	.11	.15	1	1
A 104163	1	149	2	14	.1	26	22	380	3.34	5	5	ND	1	66	.7	2	2	93	3.75	.149	2	53	1.69	24	.11	4	1.76	.14	.07	1	6
A 104164	1	158	2	13	.1	27	26	356	2.97	8	5	ND	1	120	.7	2	3	80	4.09	.149	2	46	1.60	43	.09	6	1.72	.15	.05	1	6
A 104165	1	148	27	13	.2	30	26	384	2.99	2	6	ND	1	87	.6	2	2	73	3.61	.151	2	42	1.48	25	.09	4	1.63	.16	.07	1	6
A 104166	1	110	6	21	.2	31	25	856	3.23	11	7	ND	1	164	.8	2	2	108	6.59	.140	2	55	2.06	57	.07	2	1.99	.13	.11	1	3
A 104167	1	69	42	74	.1	26	18	1554	3.73	25	5	ND	1	202	1.2	2	2	122	9.88	.131	2	66	2.30	79	.01	2	2.42	.06	.17	1	2
A 104168	1	91	17	63	.4	21	19	2076	4.28	26	5	ND	1	128	.8	2	2	66	10.85	.170	5	32	1.37	42	.01	4	2.09	.01	.36	1	2
A 104169	1	234	41	395	.3	22	22	988	4.90	33	5	ND	1	116	2.3	2	3	126	3.98	.163	7	28	1.31	89	.16	3	2.13	.13	.25	1	6
A 104170	2	114	5	91	.1	25	18	485	4.21	3	5	ND	2	103	1.0	2	2	131	2.78	.132	7	33	.98	102	.18	3	1.81	.18	.19	1	8
A 104171	3	115	4	73	.2	29	13	338	2.86	2	11	ND	7	92	.6	2	4	66	1.99	.112	13	29	.67	76	.13	3	1.13	.13	.14	1	9
A 104172	2	118	5	58	.1	22	18	391	3.87	7	9	ND	4	90	1.1	2	2	72	3.35	.128	8	19	.67	71	.14	10	2.11	.13	.18	1	4
A 104173	2	135	5	52	.1	25	20	315	4.36	4	7	ND	2	85	.6	2	2	77	3.11	.127	6	18	.56	79	.17	10	2.30	.16	.19	1	2
A 104174	4	61	4	49	.1	20	9	302	2.42	3	5	ND	6	72	.5	2	5	53	2.37	.082	10	14	.54	58	.11	4	1.15	.10	.16	1	1
A 104175	4	78	6	49	.1	25	14	342	3.53	7	5	ND	5	76	.6	2	8	74	2.04	.100	12	24	.77	57	.11	2	1.01	.09	.12	2	1
A 104176	4	73	4	49	.1	20	11	434	2.92	7	7	ND	5	128	.9	2	5	86	3.54	.112	11	19	1.02	43	.13	3	1.61	.15	.13	1	1
A 104177	4	128	3	50	.1	34	21	352	4.53	4	8	ND	2	91	.7	2	2	87	2.14	.146	5	16	.81	68	.17	3	1.60	.19	.18	1	4
A 104178	4	113	4	56	.2	26	17	582	3.86	7	7	ND	4	105	.8	2	2	91	3.84	.125	6	25	1.30	42	.10	2	1.74	.11	.15	1	3
A 104179	2	121	3	28	.1	32	20	399	3.84	5	5	ND	3	103	.6	2	7	84	2.66	.137	6	26	1.01	54	.15	4	1.64	.13	.15	1	2
A 104180	1	108	4	79	.1	29	19	648	3.68	6	5	ND	2	163	1.2	2	2	105	4.75	.136	5	60	1.41	79	.11	3	1.88	.12	.18	1	3
A 104181	1	86	2	29	.2	30	18	697	3.21	6	9	ND	2	145	.8	2	2	82	5.40	.129	4	59	1.45	73	.08	2	1.55	.05	.15	1	1
A 104182	2	53	5	501	.2	31	15	897	2.78	13	5	ND	3	87	2.9	5	2	62	6.33	.115	5	45	1.62	22	.03	6	1.95	.04	.22	1	3
A 104183	1	162	4	184	.2	17	9	1189	3.07	11	7	ND	2	133	1.2	5	2	77	8.90	.066	5	75	1.99	23	.02	4	2.31	.02	.22	1	1
A 104184	8	104	4	122	.1	35	20	855	4.23	15	5	ND	3	125	.9	5	2	102	4.05	.121	9	28	1.28	58	.09	3	1.90	.08	.18	1	1
A 104185	3	149	8	84	.1	30	17	1099	3.59	23	5	ND	1	110	.8	8	2	66	9.08	.119	8	19	1.02	21	.03	4	1.64	.03	.18	1	4
A 104186	6	166	2	65	.1	38	19	392	4.41	8	7	ND	2	58	.8	2	2	78	2.30	.127	5	22	.47	66	.14	6	1.84	.14	.17	1	7
A 104187	6	148	2	69	.1	39	22	484	5.14	12	5	ND	1	84	.5	2	2	85	2.69	.134	6	23	.50	57	.14	6	1.79	.18	.14	1	2
A 104188	8	119	4	79	.1	31	17	548	3.72	6	5	ND	2	114	.5	2	2	92	3.06	.128	7	28	.67	50	.14	2	1.41	.13	.12	1	1
A 104189	15	136	2	78	.1	38	19	535	4.24	52	5	ND	3	97	.9	2	2	84	3.05	.112	8	33	.61	74	.13	3	1.63	.16	.18	1	3
A 104190	3	132	2	53	.1	22	20	491	4.47	13	5	ND	2	85	.9	2	8	90	3.74	.131	3	18	.77	36	.15	11	2.57	.15	.16	1	2
A 104191	2	189	2	49	.1	20	23	422	4.40	10	5	ND	2	96	1.0	2	2	90	3.68	.125	2	14	.87	14	.15	10	2.55	.16	.10	1	3
STANDARD C/AU-R	18	62	38	129	7.0	71	33	1035	3.94	41	18	6	39	52	18.6	15	21	56	.51	.099	39	58	.88	182	.10	33	1.99	.07	.16	13	461
STANDARD C	18	59	36	132	7.1	69	34	1055	3.95	41	20	6	39	52	18.6	15	19	56	.48	.090	40	58	.87	177	.09	32	1.99	.06	.15	12	-

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: CORE AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

DATE RECEIVED: JUL 24 1991 DATE REPORT MAILED: July 31/91. SIGNED BY. C. Leong .D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

DRILLHOLE: SK91-11

ASSAY DATA

SAMPLE #	FROM	TO	Cu (ppm)	Au (ppb)
100076	6.0	8.0	34	78
100077	8.0	10.0	869	56
100078	12.0	14.0	2459	37
100079	14.0	16.0	414	15
100080	28.0	30.0	505	15
100081	30.0	32.0	2117	12
100082	38.0	40.0	645	8
100083	40.0	42.0	24085	3750
100084	42.0	44.0	3463	2
100085	46.0	48.0	943	7
100086	56.0	58.0	46	5
100087	80.0	82.0	304	5
100088	82.0	84.0	1241	27
100089	84.0	86.0	1098	10
100090	92.0	94.0	445	9
100091	94.0	96.0	557	8
100092	96.0	98.0	74	2
100093	98.0	100.0	19	6
100094	100.0	102.0	9	4
100095	102.0	104.0	194	1
107751	104.0	106.0	260	3
100096	106.0	108.0	152	4
100097	108.0	110.0	3546	5
100098	110.0	112.0	274	2
100099	122.0	124.0	831	3
100100	124.0	126.0	349	3
100101	130.0	132.0	566	5
100102	132.0	134.0	1937	5
100103	134.0	136.0	824	2
100104	136.0	138.0	534	3
100105	138.0	140.0	181	2
100106	142.0	144.0	49	2
100107	144.0	146.0	631	2

2m
2.4% Cu
3.7gm Au.

ACME ANALYTICAL

BP Resources Canada Ltd. PROJECT 10161 FILE # 91-2880

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
A 104228	3	245	2	25	.2	51	25	455	5.46	29	5	ND	1	108	.2	2	2	115	2.03	.128	4	114	1.44	80	.22	7	2.01	.20	.28	1	1
A 104229	1	165	2	43	.2	99	26	920	5.45	21	5	ND	1	166	.2	3	2	170	3.81	.103	5	358	2.30	172	.32	13	3.33	.35	.66	1	1
A 104230	1	133	3	38	.3	86	23	598	5.16	21	5	ND	1	167	.2	2	3	152	2.06	.103	5	322	1.82	150	.33	14	2.89	.38	.88	1	3
A 104231	3	137	2	33	.2	88	23	664	5.15	26	5	ND	1	163	.2	4	2	137	2.43	.101	5	314	2.04	139	.31	14	2.90	.33	.62	1	3
A 104232	2	425	4	28	.2	78	34	538	6.28	26	5	ND	1	138	.2	2	4	89	1.82	.110	4	126	1.69	45	.21	13	2.42	.27	.14	1	3
A 104233	1	162	4	75	.1	64	25	502	5.07	22	5	ND	1	217	.2	2	2	149	1.84	.103	4	234	1.71	142	.31	12	2.95	.36	.72	1	4
A 104234	3	166	4	39	.1	78	25	490	4.98	21	5	ND	1	250	.2	3	3	143	1.78	.103	4	317	1.77	151	.32	12	2.88	.35	.72	1	1
A 104235	1	223	3	26	.2	56	24	430	5.13	22	5	ND	1	152	.2	2	2	127	1.86	.109	4	171	1.55	90	.29	12	2.52	.29	.46	1	1
A 104236	2	308	3	21	.2	31	23	346	7.37	28	5	ND	1	52	.2	2	4	118	1.93	.137	5	49	1.44	37	.19	7	1.87	.13	.12	1	1
A 104237	2	83	4	20	.1	10	17	288	6.59	22	5	ND	1	34	.2	2	2	107	1.88	.151	5	17	1.21	33	.14	4	1.38	.07	.11	1	2
A 104238	2	26	2	16	.1	8	17	255	6.10	16	5	ND	1	33	.2	2	2	75	2.17	.146	5	12	.90	32	.16	11	1.55	.08	.11	1	1
A 104239	2	91	6	24	.1	7	15	252	5.70	21	5	ND	1	38	.2	2	2	70	2.46	.144	4	11	.99	28	.07	11	1.28	.07	.14	1	1
A 104240	2	69	4	17	.1	6	16	264	5.61	34	5	ND	1	68	.2	9	2	29	4.01	.144	4	11	.49	23	.01	10	1.10	.03	.34	1	1
A 104241	2	148	7	17	.1	12	22	330	6.11	50	5	ND	1	54	.2	2	2	63	3.69	.132	5	16	.89	26	.02	10	1.45	.06	.17	1	1
A 104242	1	188	2	18	.1	21	29	341	6.96	21	5	ND	1	49	.2	2	2	53	2.25	.134	3	17	.82	35	.08	15	1.98	.09	.10	1	1
A 104243	1	264	4	20	.2	18	34	355	8.47	24	5	ND	1	53	.2	2	2	85	1.51	.168	4	14	1.04	39	.11	8	1.80	.11	.09	1	1
A 104244	2	213	4	27	.1	25	27	533	6.06	22	5	ND	1	108	.2	2	3	105	2.59	.112	3	41	1.75	43	.17	8	2.43	.20	.12	1	1
A 104245	1	212	5	30	.1	25	26	498	5.56	23	5	ND	1	83	.2	2	2	97	2.34	.114	2	36	1.80	52	.18	8	2.45	.11	.11	1	1
A 104246	1	183	7	58	.2	25	25	533	5.61	22	5	ND	1	106	.2	3	2	127	2.72	.112	3	46	1.75	71	.21	9	2.82	.19	.13	1	1
A 104247	1	147	7	29	.2	24	23	603	5.68	17	5	ND	1	133	.2	2	3	142	3.04	.117	4	51	1.77	70	.20	6	2.77	.24	.13	1	2
A 104248	1	154	5	38	.2	21	23	983	6.45	31	5	ND	1	125	.2	2	2	170	4.72	.118	5	50	2.66	53	.03	2	3.14	.13	.15	1	2
A 104249	1	165	5	45	.2	21	23	1183	6.50	60	5	ND	1	128	.2	5	2	145	5.79	.103	5	43	2.47	45	.01	7	3.05	.08	.19	1	4
A 104250	1	176	5	144	.3	25	30	1312	6.28	52	5	ND	1	145	.6	5	2	132	7.05	.099	6	44	2.31	45	.03	4	2.95	.09	.19	2	1
A 104251	1	208	5	38	.1	25	32	838	7.05	34	5	ND	1	118	.2	5	2	140	4.14	.073	3	47	2.06	45	.03	3	2.68	.14	.13	1	1
A 104252	1	114	8	170	.2	23	28	1080	6.56	33	5	ND	1	125	.6	2	2	134	5.58	.103	5	41	2.42	50	.01	3	2.96	.05	.20	1	3
A 104253	1	233	8	425	.3	34	38	943	7.77	51	5	ND	1	119	1.9	4	2	131	5.52	.243	7	39	2.19	29	.01	3	2.63	.05	.15	2	4
A 104254	1	177	7	76	.1	28	31	798	6.45	25	5	ND	1	129	.2	2	2	135	4.90	.108	4	40	2.04	42	.03	3	2.61	.13	.19	1	2
A 104255	1	176	2	47	.1	28	26	909	6.34	35	5	ND	1	136	.2	3	2	142	6.05	.111	5	60	2.19	51	.02	3	2.51	.10	.16	1	1
A 104256	1	66	3	28	.1	26	20	704	5.06	18	5	ND	1	132	.2	2	2	150	4.22	.126	4	72	1.93	94	.12	5	2.49	.22	.15	1	2
A 104257	1	96	4	28	.1	28	26	714	5.19	22	5	ND	1	121	.2	2	2	144	4.03	.126	4	60	2.12	56	.11	6	2.35	.19	.11	1	2
A 104258	1	69	5	29	.1	28	25	792	5.16	25	5	ND	1	124	.2	2	2	159	4.26	.129	5	67	2.10	71	.18	6	2.29	.17	.11	1	3
A 104259	1	129	4	31	.1	31	27	702	5.16	26	5	ND	1	116	.2	2	3	133	3.57	.129	4	64	1.91	57	.17	5	2.20	.18	.09	1	1
A 104260	1	111	3	34	.1	26	28	760	6.21	29	5	ND	1	139	.2	3	2	151	4.48	.124	3	53	2.36	57	.12	7	2.54	.18	.08	1	1
A 104261	1	93	4	29	.1	25	27	797	6.29	24	5	ND	1	149	.2	3	2	150	4.83	.117	4	45	2.29	51	.02	5	2.43	.18	.10	1	1
RE A 104257	1	94	8	28	.1	28	25	705	5.19	22	5	ND	1	122	.2	2	2	144	4.01	.123	4	59	2.10	56	.11	6	2.32	.18	.11	1	1
A 104262	1	81	7	27	.1	24	27	751	5.65	24	5	ND	1	139	.2	2	2	137	5.15	.120	5	42	2.06	60	.02	8	2.04	.13	.19	1	1
A 104263	1	221	6	64	.1	21	18	1140	5.67	53	5	ND	1	252	.2	44	2	45	8.57	.078	4	14	2.34	67	.01	11	.68	.03	.28	2	1
STANDARD C/AU-R	19	57	35	131	6.7	71	31	1094	4.01	39	17	7	37	52	18.6	18	20	58	.50	.092	38	60	.92	176	.10	34	1.97	.07	.16	11	460
STANDARD C	19	58	37	131	6.6	69	34	1030	3.94	39	21	7	35	52	18.7	14	20	54	.48	.089	37	59	.86	176	.09	34	1.87	.06	.15	11	-

Samples beginning 'RE' are duplicate samples.

ACME ANALYTICAL

BP Resources Canada Ltd. PROJECT 10161 FILE # 91-2880

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
A 104192	7	165	5	110	.2	37	22	336	4.45	16	5	ND	1	51	.8	2	2	90	2.46	.195	5	24	.53	42	.18	13	2.38	.14	.12	3	13
A 104193	3	194	2	84	.3	33	25	570	5.81	13	5	ND	1	123	1.0	2	2	130	3.46	.193	5	34	1.04	43	.20	8	2.62	.18	.12	3	10
A 104194	2	194	6	67	.3	42	26	651	5.53	32	5	ND	1	129	.9	2	2	110	3.49	.171	6	35	1.04	60	.19	7	2.28	.14	.10	1	22
A 104195	1	161	2	41	.3	35	27	311	4.41	6	6	ND	2	34	.6	2	2	107	2.13	.173	4	60	1.15	30	.22	10	2.40	.08	.10	1	6
A 104196	4	172	4	44	.2	41	25	405	4.37	10	5	ND	1	97	.7	2	2	104	2.56	.178	5	30	.78	51	.20	11	2.26	.17	.12	3	9
A 104197	1	143	4	39	.3	31	23	394	4.11	11	5	ND	1	73	.6	2	2	112	2.83	.176	4	23	1.13	18	.23	13	2.53	.15	.09	5	7
A 104198	1	141	2	39	.2	47	25	784	4.41	16	5	ND	1	97	.7	4	2	114	3.38	.178	4	66	1.51	52	.24	14	2.56	.14	.27	6	5
A 104199	1	115	2	30	.2	32	16	468	3.37	13	5	ND	1	96	.3	2	2	105	3.85	.169	3	23	.88	22	.17	16	2.56	.15	.09	4	3
A 104200	1	151	2	24	.3	34	25	379	4.52	23	5	ND	1	41	.5	2	2	107	3.54	.174	3	20	.70	23	.18	17	2.99	.15	.09	3	5
A 104201	2	128	97	24	.1	36	21	373	4.70	25	5	ND	1	47	.3	2	2	140	3.27	.188	4	17	.72	28	.18	17	2.98	.18	.08	6	1
. 04202	2	154	3	18	.2	44	22	330	4.98	31	5	ND	1	46	.4	2	2	118	2.51	.177	6	20	.65	78	.18	9	2.30	.15	.19	4	12
A 104203	2	177	10	20	.1	44	24	396	4.87	38	5	ND	1	40	.5	2	4	107	2.75	.182	4	22	.77	39	.16	10	2.14	.13	.10	4	280
A 104204	1	115	17	80	.7	32	27	1513	5.66	62	5	ND	1	68	1.1	2	2	156	4.87	.154	5	72	2.51	50	.02	8	3.15	.06	.31	1	3
RE A 104208	1	162	2	37	.4	66	24	1282	5.11	34	5	ND	1	144	1.1	3	2	156	4.74	.133	4	212	2.67	71	.15	19	3.71	.26	.42	3	4
A 104205	1	176	19	82	.7	31	27	1145	5.72	62	5	ND	1	65	1.1	2	2	138	4.27	.134	3	55	2.38	41	.01	6	2.76	.08	.23	1	9
A 104206	1	206	123	250	1.4	28	26	1164	5.57	501	5	ND	1	57	1.8	2	2	98	3.99	.128	3	37	1.78	32	.01	6	2.31	.04	.30	1	180
A 104207	1	150	8	38	.4	56	23	1121	4.84	85	5	ND	1	101	.7	2	2	136	4.05	.120	3	163	2.49	96	.11	13	2.97	.16	.34	3	22
A 104208	1	143	2	34	.3	61	22	1158	4.59	32	5	ND	1	130	.7	7	2	142	4.32	.120	4	194	2.44	71	.14	19	3.39	.25	.38	6	5
A 104209	1	205	2	31	.3	29	22	833	4.74	27	5	ND	1	182	.6	2	2	142	3.39	.134	4	43	1.59	64	.15	21	3.42	.39	.40	1	5
A 104210	1	187	3	38	.7	27	24	1072	5.35	36	5	ND	1	118	.6	4	2	138	3.89	.122	4	43	1.81	61	.08	7	2.80	.16	.35	2	16
A 104211	1	190	10	35	.6	29	24	1041	5.34	26	5	ND	1	94	.7	2	2	154	4.31	.126	3	64	1.97	55	.09	7	2.98	.14	.40	1	2
A 104212	1	119	2	18	.4	20	22	644	4.95	26	5	ND	1	50	.6	2	2	100	3.15	.157	3	19	1.50	31	.01	4	1.94	.05	.24	1	3
A 104213	1	160	2	22	.3	28	20	795	3.81	25	5	ND	1	79	.4	2	2	128	4.70	.133	6	63	1.57	58	.03	8	2.28	.07	.29	1	3
A 104214	1	157	9	17	.4	19	24	735	5.06	37	5	ND	1	60	.7	2	2	131	4.06	.150	3	19	1.71	51	.01	4	2.09	.05	.20	1	4
A 104215	1	136	18	111	.5	16	19	1146	5.37	42	5	ND	1	48	1.3	5	2	71	4.29	.122	3	11	1.73	35	.01	6	2.00	.03	.15	3	3
A 104216	3	60	5	14	.2	12	18	437	5.31	25	5	ND	1	37	.7	2	2	54	2.52	.137	2	13	1.25	32	.01	8	1.27	.06	.15	1	1
A 104217	2	91	4	18	.3	11	19	467	5.48	28	5	ND	2	46	.7	2	2	68	2.45	.138	3	6	1.38	33	.01	5	1.63	.06	.18	1	1
A 104218	2	109	4	17	.1	10	16	327	4.56	32	5	ND	1	172	.2	2	2	90	1.86	.140	4	6	1.15	36	.07	5	1.32	.08	.13	1	2
. 04219	3	141	5	16	.2	9	15	350	5.12	39	5	ND	1	105	.3	2	2	80	2.04	.129	3	16	1.13	41	.06	7	1.19	.09	.12	1	4
. 04220	1	167	3	18	.3	11	17	336	5.74	42	5	ND	1	55	.3	2	2	95	1.74	.142	3	9	1.18	38	.13	7	1.25	.11	.13	1	3
A 104221	2	209	3	18	.3	11	17	316	5.74	36	7	ND	2	53	.5	2	4	87	1.61	.133	3	8	1.26	36	.12	6	1.35	.12	.14	1	4
A 104222	4	146	3	17	.2	13	17	330	5.72	35	5	ND	1	83	.3	4	2	90	1.81	.140	3	19	1.22	33	.11	8	1.29	.10	.10	2	3
A 104223	1	78	5	14	.3	8	16	286	5.25	23	5	ND	2	184	.2	2	2	93	1.85	.139	3	7	1.03	40	.15	6	1.34	.10	.12	1	5
A 104224	1	69	2	15	.3	11	16	358	5.20	25	5	ND	1	94	.6	2	2	94	2.14	.127	4	8	1.19	29	.10	4	1.30	.09	.12	2	4
A 104225	2	97	2	15	.2	11	16	368	5.76	31	5	ND	1	40	.6	2	2	97	1.85	.128	3	17	1.25	23	.09	5	1.20	.08	.11	1	1
A 104226	1	85	2	20	.2	10	16	348	5.71	25	5	ND	1	49	.2	2	2	104	1.98	.135	4	7	1.26	27	.11	8	1.27	.12	.10	2	1
A 104227	1	151	3	27	.2	14	20	400	6.55	35	5	ND	1	52	.7	2	2	104	1.79	.144	4	8	1.17	33	.14	8	1.55	.12	.12	3	4
STANDARD C/AU-R	19	59	38	141	7.0	72	32	1121	4.05	42	22	6	40	53	19.0	16	21	60	.50	.096	39	60	.96	180	.09	33	1.96	.07	.17	11	450
STANDARD C	17	60	36	132	6.8	68	33	1051	3.87	42	19	7	39	52	18.5	15	18	55	.47	.090	39	57	.88	173	.09	31	1.90	.06	.15	11	-

ACME ANALYTICAL

BP Resources Canada Ltd. PROJECT 10161 FILE # 91-2997

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
A 104313	2	143	6	53	.3	20	24	750	5.53	15	5	ND	1	133	.2	2	2	111	2.28	.125	5	37	1.45	53	.19	8	2.22	.12	.13	1	1
A 104314	3	154	9	64	.5	12	25	1306	6.88	47	5	ND	1	123	.2	2	3	137	4.07	.138	5	30	1.97	43	.20	7	2.20	.10	.13	1	1
A 104315	2	136	3	62	.3	16	24	652	6.18	5	5	ND	1	93	.2	2	3	167	1.77	.146	5	34	1.17	65	.28	5	1.75	.14	.24	1	6
A 104316	2	187	5	66	.3	15	23	570	6.38	3	5	ND	1	89	.2	2	2	178	1.75	.154	5	32	1.16	66	.29	9	1.90	.14	.21	1	1
A 104317	1	106	4	49	.3	11	21	691	6.17	8	5	ND	1	59	.2	2	2	163	2.52	.146	5	23	1.14	48	.26	14	2.10	.12	.17	1	6
A 104318	2	95	3	62	.3	11	21	1323	6.80	12	5	ND	1	96	.2	2	2	170	3.32	.147	5	24	1.78	43	.25	9	2.31	.11	.16	1	1
A 104319	2	97	4	76	.4	10	21	1908	7.48	22	5	ND	1	69	.2	2	2	167	3.58	.146	4	24	2.46	27	.24	5	2.70	.12	.11	1	1
A 104320	1	103	2	59	.4	11	22	985	6.39	16	5	ND	1	99	.2	2	2	163	2.89	.151	5	26	1.55	51	.25	13	2.22	.13	.17	1	1
A 104321	1	1308	2	54	.4	6	20	484	3.12	14	5	ND	1	70	.3	2	4	73	1.57	.155	3	18	.98	34	.21	9	1.89	.17	.09	1	1
A 104322	3	831	6	40	.2	10	17	599	2.55	8	5	ND	1	98	.3	2	3	67	1.51	.164	4	27	1.13	54	.19	8	1.74	.17	.09	1	1
A 323	2	1083	8	47	.2	8	19	631	2.90	7	5	ND	1	130	.2	2	2	68	2.14	.158	3	18	1.36	74	.15	4	1.89	.10	.07	1	1
A 104324	2	3640	2	80	.8	28	29	970	5.00	13	5	ND	1	89	.4	2	5	104	1.72	.156	4	64	1.99	60	.25	3	2.35	.12	.08	1	2
A 104325	1	1483	2	125	.5	21	39	1963	9.87	2	5	ND	1	69	.2	2	4	106	1.30	.134	3	90	3.02	39	.21	3	4.07	.07	.08	1	1
A 104326	2	612	2	113	.4	23	39	1626	8.24	2	5	ND	1	63	.2	4	3	98	1.10	.131	3	59	3.51	66	.20	2	4.19	.08	.05	1	3
A 104327	2	265	30	108	1.0	17	33	1641	8.83	210	5	ND	1	64	.2	9	2	89	2.53	.111	4	66	2.78	45	.09	2	4.04	.04	.15	1	6
A 104328	1	147	2	120	.5	15	49	2573	11.74	18	5	ND	1	37	.2	4	2	109	1.80	.114	5	55	3.15	40	.11	4	4.85	.03	.12	1	3
A 104329	1	1261	7	98	.6	13	27	1672	4.85	65	5	ND	1	91	.3	2	2	61	5.90	.118	6	36	2.50	35	.07	3	2.79	.05	.12	1	2
A 104330	1	944	2	95	.5	26	26	1598	5.80	8	5	ND	1	95	.2	2	4	94	2.67	.120	4	89	3.21	97	.23	3	3.36	.06	.11	1	3
A 104331	1	203	3	47	.4	19	31	588	4.84	18	5	ND	2	67	.2	3	2	107	1.68	.141	6	50	2.05	97	.34	5	2.26	.12	.19	1	2
A 104332	1	199	5	47	.3	20	30	468	4.84	11	5	ND	1	82	.2	2	2	104	1.78	.139	5	41	2.27	69	.34	3	2.32	.09	.14	1	2
A 104333	1	170	4	46	.4	30	28	501	4.71	15	5	ND	1	75	.2	2	2	121	1.86	.134	5	66	2.27	78	.36	3	2.44	.11	.16	1	3
A 104334	1	200	4	49	.3	36	22	658	3.14	16	5	ND	1	67	.2	2	2	79	1.51	.136	4	120	2.10	85	.25	2	2.05	.09	.12	1	3
A 104335	1	284	2	45	.1	21	11	703	2.35	4	5	ND	1	99	.2	2	3	46	1.90	.136	4	64	1.63	48	.17	2	1.77	.09	.07	1	3
A 104336	1	3002	3	103	1.0	28	18	1386	6.05	10	5	ND	1	178	.4	2	7	109	2.49	.124	4	54	2.32	180	.10	2	3.10	.09	.09	1	13
A 104337	1	6387	13	216	1.7	34	39	1914	16.85	57	5	ND	1	14	.9	2	10	158	.71	.112	3	195	3.67	10	.04	2	5.90	.01	.03	1	320
A 104338	1	27107	44	941	7.1	34	73	1972	16.96	317	5	2	1	44	6.1	7	9	147	1.63	.105	3	151	3.05	33	.06	2	4.83	.03	.06	1	1650
A 104339	1	14207	33	508	3.8	27	54	2300	16.09	147	5	ND	1	22	2.6	2	17	137	1.18	.100	4	118	3.12	11	.06	2	5.42	.01	.09	1	840
A 104340	3	147	2	67	.2	13	19	1077	2.83	5	5	ND	1	127	.2	2	2	61	2.12	.122	4	38	2.00	121	.19	2	2.27	.09	.05	1	5
RE 104336	1	2995	3	104	1.1	28	18	1371	5.96	9	5	ND	1	181	.5	2	4	110	2.51	.121	4	55	2.31	182	.10	4	3.08	.10	.09	1	11
A .341	2	50	2	47	.1	17	17	771	2.01	5	5	ND	1	84	.2	2	2	51	1.69	.106	4	33	1.76	88	.13	2	1.66	.08	.08	1	4
A 104342	5	198	2	45	.2	21	26	781	2.09	15	5	ND	1	90	.2	2	2	53	2.03	.127	5	33	1.83	58	.13	2	1.77	.09	.06	1	9
A 104343	2	17	6	55	.1	20	19	873	2.26	7	5	ND	1	135	.2	2	2	59	2.50	.117	3	29	1.59	82	.12	2	1.70	.08	.02	1	6
A 104344	2	18	2	27	.1	15	9	538	1.36	6	5	ND	1	116	.2	2	2	47	2.13	.143	4	26	.86	28	.15	2	1.11	.12	.04	1	16
A 104345	1	8	2	59	.2	16	18	849	2.55	5	5	ND	1	99	.2	2	2	63	1.82	.127	4	49	1.75	20	.18	2	1.66	.10	.03	1	4
A 104346	2	10	2	39	.1	17	12	637	1.81	7	5	ND	1	135	.2	2	2	61	2.27	.130	3	30	1.09	69	.17	2	1.40	.08	.06	1	5
A 104347	4	100	4	19	.2	11	5	351	.92	5	5	ND	6	83	.5	5	2	28	1.55	.071	6	22	.46	49	.11	2	.66	.09	.06	2	5
A 104348	4	113	3	20	.1	11	6	354	1.13	3	5	ND	9	56	.2	2	2	17	.79	.033	4	21	.55	20	.09	2	.74	.10	.03	3	4
STANDARD C/AU-R	18	59	42	138	6.9	70	32	1073	4.05	40	21	7	37	54	19.0	17	19	57	.51	.096	37	59	.88	179	.10	32	1.97	.06	.17	11	480
STANDARD C	18	59	36	134	7.0	71	32	1046	3.99	40	20	7	36	52	18.0	16	19	56	.49	.092	37	59	.87	178	.09	32	1.90	.06	.15	11	-

Samples beginning 'RE' are duplicate samples.

ACME ANALYTICAL

BP Resources Canada Ltd. PROJECT 10161 FILE # 91-2880

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
A 104264	1	158	5	34	.2	19	20	1068	4.86	46	5	ND	1	243	.2	32	2	41	7.88	.091	4	14	2.02	49	.01	17	.68	.03	.31	1	1
A 104265	1	69	4	25	.1	23	17	902	5.31	21	5	ND	1	167	.2	3	2	101	5.76	.105	5	37	1.80	65	.02	12	1.78	.10	.26	1	2
A 104266	1	140	8	30	.1	26	25	793	5.92	25	5	ND	1	106	.2	6	2	142	4.48	.110	4	55	1.97	48	.04	8	2.43	.17	.14	1	1
A 104267	1	177	13	55	.2	29	33	743	6.27	36	5	ND	1	109	.2	3	2	139	3.94	.108	5	49	1.96	47	.01	6	2.23	.08	.21	1	1
A 104268	1	137	5	29	.1	27	25	774	6.06	31	5	ND	1	119	.2	3	2	132	5.07	.106	6	52	1.91	38	.01	10	2.17	.07	.22	1	2
A 104269	1	196	8	40	.2	48	35	900	6.95	49	5	ND	1	134	.2	5	2	97	5.71	.101	5	106	2.09	30	.01	9	2.24	.04	.23	1	1
A 104270	1	128	6	29	.2	31	22	1132	4.85	32	5	ND	1	182	.2	5	2	43	9.36	.087	5	26	1.90	35	.01	11	1.05	.03	.27	1	1
A 104271	1	124	2	25	.1	26	20	713	5.45	31	5	ND	1	136	.2	4	2	139	4.93	.101	5	60	2.27	56	.05	8	2.33	.12	.20	1	1
A 104272	1	123	3	30	.1	30	22	668	4.57	43	5	ND	1	136	.2	3	2	93	4.58	.109	4	42	1.66	63	.07	10	1.74	.13	.20	1	1
A 104273	1	221	4	28	.3	71	31	512	5.92	37	5	ND	1	99	.2	4	2	104	1.89	.108	3	158	1.99	43	.22	9	2.27	.20	.10	1	1
. 4274	1	91	5	25	.1	27	22	504	5.10	26	5	ND	1	105	.2	2	3	145	2.50	.127	4	64	1.64	85	.24	15	2.74	.16	.12	1	1
A 104275	1	101	10	24	.2	26	27	494	5.09	27	5	ND	1	78	.3	2	3	139	3.00	.115	4	43	1.55	82	.21	19	2.77	.12	.09	1	2
A 104276	1	94	5	28	.3	24	26	687	6.24	38	5	ND	1	110	.2	2	2	144	4.03	.102	4	42	1.89	46	.17	11	2.81	.13	.17	1	1
STANDARD C/AU-R	17	58	39	133	6.9	70	33	1032	3.93	40	18	8	38	51	18.6	15	18	55	.48	.090	38	57	.89	175	.09	34	1.88	.06	.15	11	480

ACME ANALYTICAL

BP Resources Canada Ltd. PROJECT 10161 FILE # 91-2997

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
A 104385	1	22	2	65	.2	56	25	822	3.80	13	5	ND	2	115	.5	2	2	94	1.44	.143	5	165	2.06	48	.20	2	2.44	.06	.20	1	8
A 104386	1	19	2	67	.2	55	21	883	3.95	7	5	ND	3	183	.3	4	2	82	1.92	.158	5	126	2.18	55	.17	2	2.70	.05	.09	1	4
A 104387	1	79	2	66	.1	70	19	729	3.62	6	5	ND	2	106	.3	2	2	83	1.46	.114	3	191	2.33	31	.19	2	2.51	.06	.07	1	1
A 104388	1	98	3	79	.2	76	22	975	3.81	11	5	ND	1	228	.5	3	2	76	2.06	.098	2	204	2.39	42	.16	2	2.90	.08	.06	1	4
A 104389	1	689	5	84	.4	28	18	762	3.27	18	5	ND	3	156	.2	5	2	75	2.33	.124	4	64	1.51	45	.19	2	2.68	.11	.08	3	4
A 104390	1	64	2	43	.3	11	12	648	2.80	7	5	ND	3	131	.2	2	2	74	2.15	.142	6	13	1.27	20	.20	2	2.06	.10	.06	1	2
A 104391	1	16	2	41	.3	18	13	656	2.59	12	5	ND	2	180	.2	2	2	66	2.75	.116	4	65	1.31	27	.17	2	1.84	.08	.06	1	2
A 104392	1	8	2	41	.2	45	13	622	2.95	7	5	ND	1	98	.2	4	2	74	1.37	.082	3	182	1.77	29	.20	2	2.09	.07	.08	1	2
A 104393	1	8	2	33	.2	21	11	524	2.49	5	5	ND	2	95	.3	2	2	71	1.43	.118	4	58	1.38	27	.18	3	1.94	.10	.07	1	1
A 104394	1	76	2	41	.2	18	14	654	3.19	11	5	ND	3	109	.3	2	2	83	1.98	.137	5	45	1.23	41	.22	4	2.10	.08	.11	1	1

ACME ANALYTICAL

BP Resources Canada Ltd. PROJECT 10161 FILE # 91-2997

ACME ANALYTICAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
A 104349	4	3872	5	51	1.4	19	23	785	3.16	41	5	ND	4	76	.8	2	3	35	1.31	.068	2	26	1.54	10	.06	2	1.64	.05	.02	1	1
A 104350	1	739	2	62	.2	32	30	917	3.58	21	5	ND	1	128	.6	2	2	59	1.81	.124	3	25	1.70	7	.09	2	1.93	.10	.01	1	3
A 104351	1	4554	5	58	.9	20	51	1017	4.03	47	5	ND	1	147	.9	5	4	48	2.72	.099	2	19	1.80	22	.07	2	2.01	.05	.01	1	9
A 104352	1	1402	2	62	.5	23	26	855	4.20	9	7	ND	1	199	.7	2	2	55	1.41	.106	3	20	1.60	88	.09	2	2.14	.06	.04	1	8
A 104353	1	876	3	88	.1	24	23	1217	5.65	7	5	ND	1	155	1.3	8	2	72	2.90	.109	3	24	1.92	35	.08	2	3.01	.03	.10	3	2
A 104354	1	329	13	177	.3	20	26	1712	8.59	10	8	ND	1	238	1.8	2	2	101	1.91	.111	4	24	2.14	129	.05	2	4.33	.05	.16	1	3
A 104355	1	83	2	71	.2	28	23	1201	5.12	3	5	ND	2	211	.9	2	2	75	2.04	.100	3	76	2.52	101	.14	2	3.24	.05	.07	1	3
A 104356	1	709	2	81	.4	30	27	1369	5.16	8	8	ND	2	329	1.2	2	2	84	2.63	.098	3	74	2.11	163	.14	2	2.91	.05	.05	1	1
A 104357	1	202	2	94	.4	32	24	1523	5.21	5	8	ND	2	361	.9	2	2	82	3.02	.099	2	80	2.08	165	.15	2	2.86	.02	.05	1	1
A 104358	1	1077	5	63	.3	25	24	695	2.37	25	5	ND	1	364	.6	2	2	62	2.71	.106	2	30	.99	164	.11	2	1.69	.07	.05	1	1
A 104359	2	34	4	48	.2	30	23	807	2.82	20	5	ND	2	258	.7	2	2	64	2.52	.112	4	42	1.22	104	.13	2	1.61	.06	.05	1	1
A 104360	1	11	3	53	.2	18	16	886	2.96	6	5	ND	2	215	.5	2	2	63	2.79	.105	4	51	1.45	81	.15	2	1.72	.05	.06	1	1
A 104361	1	383	2	106	.3	34	31	1724	7.09	7	5	ND	3	132	.9	2	2	94	1.63	.102	3	98	2.54	84	.13	2	3.46	.02	.06	1	3
A 104362	2	37	2	86	.2	14	36	1969	8.71	11	5	ND	3	302	1.3	2	2	82	.85	.086	4	18	2.02	266	.05	2	4.10	.03	.17	1	2
A 104363	6	208	2	85	.5	16	30	1849	7.42	12	5	ND	3	502	1.0	2	2	68	1.12	.076	5	18	2.07	336	.04	2	3.85	.03	.14	1	2
A 104364	4	926	3	122	1.5	12	28	1930	8.04	105	5	ND	3	191	1.7	2	2	73	2.21	.107	6	20	2.24	139	.06	3	4.08	.03	.16	1	1
A 104365	3	71	2	56	.2	14	19	1215	4.62	13	5	ND	2	224	.7	2	2	76	2.33	.144	5	23	1.82	131	.15	2	2.45	.04	.07	1	2
A 104366	6	326	2	54	.3	12	15	1076	5.06	8	5	ND	4	124	.9	2	2	65	1.50	.128	7	27	1.62	100	.14	2	2.50	.04	.14	1	1
A 104367	1	1425	5	43	.3	32	9	608	2.47	14	5	ND	1	101	.3	2	4	66	2.09	.147	4	35	.83	25	.10	2	1.16	.07	.05	1	1
A 104368	3	305	4	46	.2	26	10	933	3.40	8	5	ND	1	183	.6	2	2	78	2.58	.144	3	51	1.35	57	.13	2	1.86	.08	.06	1	2
A 104369	2	19	5	46	.3	19	17	956	3.65	11	5	ND	2	256	.6	3	3	59	1.78	.117	3	33	1.54	90	.14	2	2.16	.05	.07	1	4
A 104370	3	10	3	65	.1	16	26	1381	5.68	14	5	ND	1	204	1.0	3	2	65	1.28	.122	2	18	1.93	62	.12	2	3.10	.07	.04	1	2
A 104371	2	22	3	49	.2	16	18	841	3.17	12	5	ND	1	159	.7	2	2	53	1.69	.129	2	11	1.46	73	.12	2	1.97	.07	.07	1	1
A 104372	1	88	2	56	.2	12	19	943	3.68	9	5	ND	2	143	.5	3	2	53	1.67	.130	3	10	1.70	78	.11	2	2.29	.05	.07	1	1
A 104373	1	1230	5	92	.4	24	25	1383	5.73	10	5	ND	2	469	1.1	2	2	95	2.22	.107	2	103	2.12	134	.15	2	3.18	.05	.09	1	1
A 104374	1	220	18	51	.2	29	20	946	3.91	11	5	ND	1	178	.6	2	2	85	1.88	.098	3	104	1.81	49	.19	2	2.24	.05	.06	1	1
A 104375	1	23	3	44	.1	28	15	789	2.92	8	5	ND	1	138	.5	2	2	65	1.56	.124	4	92	1.55	51	.14	2	1.87	.06	.08	1	1
A 104376	1	12	2	70	.1	24	27	1134	4.60	9	5	ND	1	330	.7	2	2	71	1.72	.114	2	85	2.29	77	.12	2	2.73	.04	.05	1	3
A 104377	2	26	3	49	.1	29	19	823	3.30	9	5	ND	1	217	.3	2	3	77	1.59	.089	2	79	1.70	65	.18	2	2.20	.05	.06	1	1
A 104378	1	5	7	33	.1	6	8	543	1.59	4	5	ND	1	226	.3	2	2	34	3.00	.107	2	15	.75	37	.10	2	1.28	.07	.03	1	1
RE A 104374	1	220	18	52	.1	29	20	963	3.97	11	5	ND	1	183	.8	3	2	87	1.90	.100	3	105	1.83	52	.19	2	2.28	.06	.06	2	1
A 104379	1	2998	5	77	.9	24	16	864	3.62	12	5	ND	1	230	1.0	4	2	73	2.16	.096	3	83	1.50	58	.16	3	2.63	.10	.08	2	2
A 104380	1	1293	2	101	.4	30	22	1197	5.08	5	5	ND	2	92	1.2	3	3	86	1.33	.105	3	131	2.05	34	.17	2	2.66	.04	.06	1	2
A 104381	2	233	4	46	.2	16	28	574	2.49	34	5	ND	3	154	.6	2	3	60	1.69	.104	3	35	1.00	63	.17	2	1.83	.08	.11	1	2
A 104382	1	163	4	27	.1	19	18	406	2.26	13	5	ND	1	160	.3	2	2	72	1.15	.122	5	50	.73	66	.17	2	1.70	.10	.17	1	2
A 104383	2	241	9	143	.1	45	21	1316	4.60	24	5	ND	1	167	1.2	2	2	83	1.99	.116	3	149	1.84	61	.16	2	2.93	.08	.32	1	2
A 104384	1	289	2	98	.2	51	24	1218	4.71	16	5	ND	2	148	1.0	3	2	91	1.51	.148	5	132	2.15	50	.19	2	2.95	.06	.20	1	9
STANDARD C/AU-R	19	60	39	135	7.3	70	31	1083	3.99	42	22	6	40	50	18.8	20	21	58	.51	.092	40	57	.90	183	.09	33	1.99	.08	.16	11	520
STANDARD C	18	62	40	132	7.3	70	33	1053	3.95	44	19	7	40	52	18.9	15	18	55	.48	.089	39	58	.88	176	.09	32	1.93	.06	.16	11	-

Samples beginning 'RE' are duplicate samples.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
A 104503	2	35	18	100	.2	16	17	1193	5.18	6	5	ND	1	71	.2	2	2	119	2.57	.149	8	38	1.96	114	.23	9	2.17	.15	.27	1	6
A 104504	1	98	7	89	.3	15	17	1127	5.36	11	5	ND	1	55	.2	2	2	122	2.19	.158	6	33	1.63	67	.23	14	2.06	.12	.24	1	5
A 104505	1	253	6	85	.5	16	17	1252	5.06	19	5	ND	1	64	.2	2	2	129	2.23	.150	4	39	1.64	82	.27	15	2.30	.16	.22	1	5
A 104506	1	109	6	100	.3	17	18	1365	5.35	15	5	ND	1	60	.2	2	2	132	1.92	.146	5	43	2.05	88	.26	12	2.23	.13	.25	1	7
A 104507	1	15	8	95	.2	16	19	1237	5.35	12	5	ND	1	63	.2	2	2	124	2.26	.142	7	37	2.03	115	.23	10	1.99	.14	.30	1	3
A 104508	1	13	7	85	.1	15	17	1167	5.07	7	5	ND	1	61	.2	2	2	123	2.88	.139	6	40	1.98	89	.25	10	1.96	.13	.33	1	4
A 104509	1	24	4	84	.2	16	18	1197	5.06	8	5	ND	1	63	.2	2	2	113	2.56	.140	6	45	2.07	222	.23	7	1.97	.14	.24	1	3
A 104510	1	33	6	81	.1	17	17	1122	5.04	4	5	ND	1	56	.2	2	2	114	2.31	.136	4	40	2.05	101	.23	7	1.93	.13	.24	1	2
A 104511	1	150	4	77	.4	16	17	1046	4.93	3	5	ND	1	64	.2	2	2	115	2.61	.135	7	42	1.70	328	.23	7	1.90	.16	.28	2	4
A 104512	1	33	6	75	.1	15	18	1166	4.59	2	5	ND	1	120	.2	2	2	109	2.96	.133	8	35	1.60	3094	.19	8	1.98	.15	.28	1	1
A 104513	2	114	10	119	.4	18	21	1793	5.20	5	5	ND	1	144	.2	2	4	130	2.83	.143	7	33	1.62	1513	.08	6	2.52	.21	.23	1	10
A 104514	3	136	649	4340	1.4	12	15	5796	4.41	24	5	ND	1	126	19.7	2	2	92	7.19	.096	12	24	1.65	221	.03	4	2.22	.06	.17	1	136
A 104515	2	20	89	1610	5.6	6	3	15106	1.43	38	5	2	1	243	5.9	2	2	19	19.92	.010	7	10	.39	167	.01	2	.49	.01	.01	1	1281
A 104516	7	32	631	10044	11.3	5	4	11076	1.95	48	5	ND	1	164	41.5	3	2	17	13.54	.007	7	14	.32	134	.01	2	.39	.01	.01	1	620
A 104517	7	99	334	5028	10.6	8	7	7429	2.78	71	5	ND	1	88	19.2	2	2	38	7.55	.026	6	23	1.02	81	.01	3	.99	.01	.04	1	346
RE A 104514	3	122	629	4026	1.4	11	13	5224	3.96	24	5	ND	1	108	19.0	2	2	79	6.19	.092	10	23	1.55	141	.03	4	1.87	.05	.16	1	154
A 104518	5	44	143	1451	16.8	4	4	12397	1.12	61	5	ND	1	164	4.2	2	2	16	13.75	.016	6	15	.20	121	.01	2	.30	.03	.01	1	200
A 104519	9	132	618	29969	9.0	3	2	10150	.72	32	5	ND	1	165	183.1	2	2	9	12.28	.005	8	11	.18	89	.01	2	.17	.01	.01	1	346
A 104520	13	182	1577	39477	21.1	5	5	4071	1.69	63	5	ND	1	64	242.2	5	2	19	4.28	.007	3	15	.35	48	.01	2	.36	.01	.01	1	588
A 104521	3	208	1499	4955	97.0	9	6	2639	2.24	49	5	ND	1	40	25.4	11	2	32	2.47	.025	2	22	.92	134	.01	3	.76	.01	.04	1	263
A 104522	10	57	738	11977	21.5	9	6	6014	2.24	71	5	ND	1	70	55.7	6	2	17	6.44	.003	6	26	.18	80	.01	2	.19	.01	.01	1	315
A 104523	3	258	835	1633	54.5	10	17	2692	4.93	58	5	ND	1	31	10.7	7	6	126	1.13	.094	4	16	2.60	161	.02	5	2.52	.02	.15	1	97
A 104524	1	46	105	921	7.1	10	18	3346	5.63	81	5	ND	1	37	1.9	2	2	150	1.30	.129	7	18	2.56	120	.02	4	2.81	.02	.24	1	75
A 104525	1	24	47	1028	2.9	10	20	2320	5.32	270	5	ND	1	32	2.8	5	3	102	.82	.105	6	18	2.40	81	.02	3	2.20	.01	.21	1	94
A 104526	1	39	30	2762	1.6	11	21	3108	6.19	72	5	ND	1	34	8.6	2	3	162	.71	.135	7	14	2.93	113	.02	5	3.06	.02	.21	1	123
A 104527	1	65	35	912	2.8	10	19	2576	5.45	35	5	ND	1	35	2.0	2	7	157	.67	.141	7	14	2.44	218	.04	8	2.51	.04	.27	1	41
A 104528	1	40	22	1034	1.6	10	21	2442	5.82	87	7	ND	1	34	2.3	4	2	147	.52	.134	6	15	2.49	105	.03	5	2.56	.04	.28	1	38
A 104529	1	38	19	727	1.9	8	20	2247	5.07	214	5	ND	1	37	1.7	6	13	97	.77	.126	6	16	2.58	90	.02	2	2.36	.01	.25	1	47
A 104530	1	46	304	1604	1.8	8	18	2962	5.57	154	5	ND	1	39	4.4	2	2	123	1.30	.121	6	10	2.94	60	.02	4	2.63	.01	.23	1	62
A 104531	2	111	2023	5934	5.2	10	17	3258	5.54	129	5	ND	1	66	23.5	3	8	107	1.79	.093	3	16	1.65	78	.01	3	1.68	.01	.11	1	83
A 104532	6	164	18627	14638	32.3	8	10	2009	3.28	52	6	ND	1	58	117.0	22	6	57	1.13	.056	2	12	1.05	86	.02	3	.88	.01	.07	1	220
STANDARD C/AU-R	19	59	38	133	7.3	73	33	1024	3.96	40	15	8	37	53	17.3	18	21	60	.50	.096	38	56	.80	176	.09	31	1.93	.09	.17	12	462
STANDARD C	20	64	41	137	7.2	75	33	1078	4.10	42	22	8	41	52	18.2	18	19	62	.53	.096	40	60	.98	183	.10	37	1.97	.09	.15	11	-

Samples beginning 'RE' are duplicate samples.

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
A 104467	4	174	5	40	.3	11	18	366	1.70	19	5	ND	1	90	.2	2	3	55	2.47	.152	5	21	.60	43	.17	9	1.86	.12	.07	1	4
A 104468	3	172	2	35	.2	10	16	339	2.10	8	5	ND	1	112	.2	2	4	63	2.28	.152	4	22	.85	53	.19	6	1.77	.10	.10	1	10
A 104469	1	39	533	774	.6	21	25	1925	6.08	9	5	ND	1	68	1.9	22	2	150	1.47	.144	10	33	1.98	873	.18	7	1.56	.01	.17	3	8
A 104470	1	55	64	314	.2	17	22	2302	6.08	10	5	ND	1	81	.2	21	2	169	2.90	.141	9	18	1.87	1586	.19	7	1.72	.03	.19	1	9
A 104471	3	56	1355	1382	2.1	30	37	1746	5.79	17	5	ND	1	67	3.9	19	2	140	1.00	.134	7	56	2.10	92	.10	5	1.66	.01	.17	5	9
A 104472	3	57	1729	2591	2.1	25	29	1807	5.62	21	5	ND	1	106	8.5	22	2	129	1.26	.126	8	52	1.83	120	.09	4	1.44	.02	.16	10	18
A 104473	1	8	32	201	.4	59	27	2470	6.49	8	5	ND	1	84	.2	16	2	170	3.43	.125	8	85	2.56	1728	.09	6	1.88	.03	.15	1	6
A 104474	1	22	28	147	.6	62	27	2386	6.50	12	5	ND	1	75	.2	20	2	162	4.00	.109	8	96	2.35	1300	.11	6	1.81	.04	.18	1	10
A 104475	1	26	47	267	.9	23	30	2057	6.56	13	5	ND	1	57	.3	20	2	197	2.23	.106	8	39	2.08	1197	.11	6	1.79	.01	.52	1	11
A 104476	1	191	128	424	1.1	14	27	2336	6.56	9	5	ND	1	46	1.0	40	2	189	3.04	.115	8	24	1.98	605	.13	7	1.63	.01	.23	1	9
A 104477	1	61	435	540	1.1	14	24	1917	6.44	10	5	ND	1	60	.6	20	2	163	2.60	.136	9	7	1.43	1180	.10	7	1.59	.01	.32	2	30
A 104478	1	43	8870	25531	6.1	8	9	7391	3.96	36	17	ND	1	137	149.1	18	3	41	9.49	.022	5	5	3.34	331	.01	10	.55	.03	.02	1	451
A 104479	2	24	2045	7633	2.6	11	14	5776	5.59	41	5	ND	1	102	39.2	7	2	71	6.02	.059	5	17	2.42	118	.01	5	1.10	.01	.03	15	62
A 104480	2	31	1510	5751	2.8	11	19	3537	6.64	198	5	ND	1	73	22.4	18	2	95	2.56	.091	5	19	2.19	70	.01	4	1.98	.01	.06	20	43
A 104481	1	23	21649	8425	6.9	7	13	5429	6.03	114	5	ND	1	76	35.7	17	2	84	5.02	.071	6	9	3.75	87	.03	4	2.65	.01	.06	11	40
A 104482	2	25	1229	3570	4.2	8	12	6273	5.06	149	5	ND	1	78	13.2	8	2	65	6.63	.054	6	18	3.06	41	.01	2	2.02	.01	.06	17	42
A 104483	3	49	6009	16078	20.6	10	6	8264	2.63	72	7	ND	1	99	95.2	8	2	28	12.45	.016	8	15	.95	40	.01	2	.67	.01	.02	1	148
A 104484	1	24	1460	5229	10.3	6	4	10676	1.71	41	6	ND	1	297	26.6	4	2	21	15.83	.010	11	7	.57	69	.01	3	.45	.01	.01	24	75
A 104485	3	46	1075	7893	14.0	8	5	13023	2.03	45	5	ND	1	279	37.4	5	2	21	16.99	.009	12	17	.54	75	.01	2	.42	.01	.01	18	152
A 104486	2	28	1353	2821	4.5	8	10	7636	4.01	61	5	ND	1	156	10.4	7	2	62	9.52	.047	7	19	2.06	69	.01	2	1.56	.01	.06	14	83
A 104487	1	88	468	2978	1.7	10	19	2306	5.35	109	5	ND	1	53	12.9	6	2	97	.90	.103	6	13	3.36	93	.06	2	2.28	.01	.17	14	67
A 104488	2	30	130	1186	1.3	10	21	2138	5.52	101	5	ND	1	32	3.8	7	2	111	.96	.131	8	18	2.72	69	.08	3	1.97	.01	.18	4	29
A 104489	1	45	74	827	1.4	11	27	2261	5.73	96	5	ND	1	31	1.4	10	2	155	.86	.156	9	12	3.02	65	.04	5	2.35	.02	.21	3	16
A 104490	2	75	79	1148	2.6	12	22	2607	5.70	182	5	ND	1	31	3.0	12	2	146	.88	.134	7	19	3.36	58	.01	5	2.46	.01	.15	4	44
RE A 104487	1	97	475	3058	1.8	9	20	2309	5.57	116	5	ND	1	53	13.3	7	2	101	.84	.107	6	11	3.46	124	.06	3	2.34	.01	.18	15	65
A 104491	1	28	91	756	2.9	12	26	2169	5.77	200	5	ND	1	28	1.7	12	2	165	.54	.141	7	19	3.39	68	.02	4	2.47	.01	.19	3	59
A 104492	1	39	67	602	4.8	12	26	2547	6.09	93	5	ND	1	28	1.4	12	2	162	.47	.150	7	15	3.79	66	.01	2	2.92	.02	.16	2	24
A 104493	1	38	40	6008	1.8	12	22	2591	5.69	66	5	ND	1	48	22.2	9	2	148	.66	.138	7	13	3.47	172	.02	4	2.71	.02	.17	22	127
A 104494	5	38	135	10772	6.7	10	12	2203	3.85	73	5	ND	1	53	45.9	8	2	74	1.02	.040	3	26	1.95	84	.01	4	1.58	.01	.05	1	341
A 104495	1	7	12	132	.2	16	19	1020	5.30	5	5	ND	1	47	.2	7	2	102	3.32	.151	10	34	1.85	101	.18	5	1.59	.04	.18	1	15
A 104496	1	8	8	119	.2	16	20	1010	5.33	5	5	ND	1	58	.2	5	2	105	2.95	.160	11	34	2.05	93	.16	6	1.77	.05	.21	1	5
A 104497	2	9	7	103	.2	16	18	978	5.40	4	5	ND	1	54	.2	6	2	102	2.77	.157	10	37	2.01	62	.20	5	1.69	.05	.15	1	2
A 104498	1	9	9	109	.2	16	17	984	5.23	4	5	ND	1	58	.2	5	2	103	3.47	.150	10	44	1.73	72	.20	4	1.45	.04	.17	1	5
A 104499	2	17	8	90	.2	15	15	995	4.98	5	5	ND	1	54	.2	4	2	86	3.16	.144	9	37	1.32	48	.20	4	1.20	.03	.16	1	6
A 104500	1	31	8	179	.1	13	17	1248	4.75	5	5	ND	1	78	.3	5	2	95	3.41	.146	9	34	2.09	125	.09	4	1.97	.04	.13	1	6
A 104501	1	103	5	110	.3	10	16	1078	5.11	2	5	ND	1	164	.2	6	2	128	2.63	.155	10	26	2.20	116	.22	4	2.45	.07	.10	1	3
A 104502	1	47	3	90	.3	10	16	1042	4.92	5	5	ND	1	90	.2	4	2	114	2.28	.158	9	27	2.13	60	.26	5	1.86	.07	.13	1	3
STANDARD C/AU-R	19	60	36	140	7.3	73	32	1140	4.04	40	18	6	39	53	18.7	20	21	61	.51	.094	40	61	.94	183	.10	32	2.07	.07	.17	13	462
STANDARD C	19	56	38	133	7.0	70	32	1040	3.97	40	15	6	37	52	18.8	17	19	57	.48	.091	37	58	.88	177	.09	32	1.89	.07	.15	13	-

Samples beginning 'RE' are duplicate samples.

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

BP Resources Canada Ltd. PROJECT LOC-10161 File # 91-4810

700 - 890 W. Pender St., Vancouver BC V6B 4W3 Submitted by: C.T. BARRIE

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
D 100076	5	34	13	46	.5	12	4	394	1.11	3	5	ND	14	65	.3	2	2	23	.87	.047	7	34	.42	99	.06	3	.71	.09	.16	2	78
D 100077	2	869	21	450	.3	17	10	1585	4.94	6	5	ND	7	107	1.4	2	3	70	1.64	.064	4	43	1.08	77	.07	2	2.49	.15	.09	1	56
D 100078	1	2459	207	508	1.4	22	29	2460	11.99	165	5	ND	1	40	2.1	2	2	169	1.06	.079	2	50	2.49	38	.08	2	5.42	.04	.12	1	37
D 100079	1	414	3	100	.2	23	21	1420	5.23	2	5	ND	1	84	.7	2	2	115	1.70	.113	2	65	1.77	36	.14	3	2.77	.11	.08	1	15
D 100080	4	505	5	57	.2	21	30	574	2.95	15	5	ND	1	115	.6	2	2	85	2.61	.126	2	35	.93	35	.13	7	2.10	.17	.09	2	15
D 100081	11	2117	22	121	.4	24	42	1407	6.91	16	5	ND	1	56	1.0	2	2	98	1.50	.081	2	50	1.52	26	.06	2	3.07	.07	.08	1	12
D 100082	3	645	2	53	.6	34	34	449	2.15	23	5	ND	3	80	.2	2	2	46	2.15	.107	3	39	.52	33	.09	6	1.41	.20	.06	1	8
D 100083	5	24085	120	794	16.7	22	58	984	7.65	2550	5	7	4	41	3.5	7	68	63	1.45	.050	2	36	.86	44	.04	2	2.05	.10	.11	1	3750
D 100084	4	3463	9	160	1.0	23	21	1240	5.22	47	5	ND	5	70	.2	2	2	76	1.68	.066	4	32	.82	50	.08	2	2.17	.07	.11	1	2
D 100085	4	943	19	143	.3	28	25	1187	3.85	21	5	ND	5	116	.3	2	2	50	1.98	.059	3	33	.88	83	.06	2	1.80	.08	.10	1	7
D 100086	64	46	2	13	.2	7	2	206	.62	4	5	ND	6	44	.2	2	2	21	1.15	.078	3	25	.19	56	.09	3	.52	.12	.08	1	5
D 100087	2	304	5	37	.1	11	20	449	3.54	6	5	ND	1	77	.2	2	2	85	1.86	.111	2	18	1.00	77	.20	8	2.40	.17	.15	1	5
D 100088	7	1241	56	571	.9	15	33	1667	10.13	17	5	ND	1	51	2.9	2	2	105	1.86	.086	2	15	1.82	28	.10	2	4.59	.04	.14	1	27
D 100089	5	1098	9	168	.2	30	30	1995	8.44	2	5	ND	1	111	1.1	2	2	108	2.37	.092	2	67	2.04	53	.10	2	4.02	.05	.17	1	10
D 100090	8	445	2	109	.3	38	31	2109	8.95	3	5	ND	4	62	1.0	2	2	105	1.25	.075	2	115	2.39	17	.11	2	3.96	.06	.03	1	9
D 100091	1	557	2	86	.2	30	27	1549	6.34	6	5	ND	1	115	.7	2	2	89	3.79	.072	2	106	1.71	68	.11	2	4.19	.13	.07	1	8
D 100092	1	74	3	42	.1	25	14	744	2.94	2	5	ND	1	344	.3	2	2	75	2.62	.125	4	63	1.35	173	.15	4	2.63	.14	.11	2	2
D 100093	2	19	3	34	.3	31	15	594	2.63	6	5	ND	2	287	.2	2	2	75	1.95	.095	3	69	1.24	138	.17	5	2.02	.10	.09	1	6
D 100094	1	9	2	31	.1	42	17	679	2.52	14	5	ND	1	293	.5	2	2	62	2.69	.090	2	82	1.35	105	.12	5	1.79	.10	.05	1	4
D 100095	2	194	2	23	.3	37	14	451	1.66	12	5	ND	1	242	.2	3	2	42	1.90	.131	3	31	.70	85	.09	3	1.38	.14	.04	2	1
D 100096	6	152	2	102	.1	18	41	2360	10.44	6	5	ND	1	149	1.3	2	2	124	1.00	.102	2	40	2.32	117	.08	2	4.82	.04	.12	1	4
D 100097	30	3546	2	150	3.0	25	51	2533	13.18	9	5	ND	1	21	1.7	2	7	138	.63	.054	2	79	2.70	11	.05	2	5.46	.02	.01	1	5
D 100098	3	274	9	70	.4	32	29	1440	5.85	4	5	ND	2	118	.2	2	2	109	2.58	.136	2	71	1.29	35	.09	2	2.54	.09	.04	1	2
D 100099	3	831	2	31	.2	58	49	219	3.32	29	5	ND	1	84	.2	2	2	31	1.82	.141	4	22	.25	42	.08	2	1.43	.14	.03	1	3
D 100100	2	349	4	26	.1	40	30	325	2.77	8	5	ND	1	79	.7	2	2	53	2.10	.129	4	48	.62	36	.11	4	1.51	.13	.03	1	3
D 100101	7	566	7	34	.3	22	16	431	2.76	7	10	ND	1	124	.4	3	2	42	1.38	.123	3	31	.61	117	.06	3	1.24	.11	.12	2	5
D 100102	5	1937	5	67	.3	43	41	240	1.94	54	5	ND	1	64	.2	2	2	30	1.34	.133	3	26	.28	46	.09	3	.82	.16	.05	1	5
D 100103	5	824	2	34	.2	30	18	247	1.59	21	5	ND	1	66	.4	2	2	33	1.48	.136	4	30	.27	60	.07	3	.75	.15	.07	1	2
RE D 100100	2	328	6	23	.2	38	29	313	2.65	9	5	ND	1	75	.2	2	2	51	2.02	.123	3	47	.60	36	.11	4	1.43	.13	.03	1	1
D 100104	5	534	6	34	.2	23	12	342	1.98	12	5	ND	1	93	.2	2	2	46	1.66	.131	5	36	.50	114	.07	3	.98	.12	.08	1	3
D 100105	6	181	9	28	.1	20	10	427	2.13	2	5	ND	1	67	.2	2	2	32	1.52	.107	2	32	.75	41	.05	2	.92	.09	.03	1	2
D 100106	5	49	2	4	.2	14	4	136	.82	5	5	ND	1	43	.2	2	2	13	.84	.094	6	28	.14	149	.05	2	.48	.10	.18	1	2
D 100107	7	631	10	21	.5	32	26	195	1.81	29	5	ND	2	62	.2	4	2	25	.93	.122	5	30	.19	140	.07	3	.70	.10	.14	2	2
STANDARD C/AU-R	20	64	42	131	7.4	72	32	1087	4.05	42	22	8	40	53	18.9	18	20	62	.48	.092	40	60	.92	182	.08	34	1.93	.07	.15	11	480
STANDARD C	20	62	43	133	7.3	73	32	1033	3.99	44	16	8	40	53	18.6	19	18	60	.45	.088	41	59	.84	178	.08	34	1.90	.06	.14	11	-

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
ASSAY RECOMMENDED FOR ROCK AND CORE SAMPLES IF CU PB ZN AS > 1%, AG > 30 PPM & AU > 1000 PPB
- SAMPLE TYPE: CORE AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE. Samples beginning 'RE' are duplicate samples.

DATE RECEIVED: SEP 30 1991 DATE REPORT MAILED: Oct 2/91. SIGNED BY. C. Leong .D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

Chemex Labs Ltd.

Analytical Chemists * Geochemists * Registered Assayers

212 Brooksbank Ave., North Vancouver
British Columbia, Canada V7J 2C1
PHONE: 604-984-0221 FAX: 604-984-0218

To: WESTLEY TECHNOLOGIES LTD.

900 - 475 HOWE ST.
VANCOUVER, B.C.
V6C 2B3

Project : WIT
Comments: ATTN: VICTOR JONES CC: COLIN CAMPBELL

Certificate Date: 22-FEB-95
Invoice No. : I9511965
P.O. Number :
Account : AF

CERTIFICATE OF ANALYSIS A9511965

SAMPLE	PREP CODE		Pb %	Zn %	Ba %							
W95-211	244	--	1.27	1.60	1.5							
W95-212	244	--	-----	2.50	0.9							

CERTIFICATION:_____

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(AF) - WESTLEY TECHNOLOGIES LTD.

Project: WIT
P.O. # :

Samples submitted to our lab in Vancouver, BC.
This report was printed on 9-JAN-97.

SAMPLE PREPARATION

CHEMEX CODE	NUMBER SAMPLES	DESCRIPTION
244	2	Pulp; prev. prepared at Chemex

ANALYTICAL PROCEDURES

CHEMEX CODE	NUMBER SAMPLES	DESCRIPTION	METHOD	DETECTION LIMIT	UPPER LIMIT
312	1	Pb %: Reverse Aqua-Regia digest	AAS	0.01	100.0
316	2	Zn %: Reverse Aqua-Regia digest	AAS	0.01	100.0
351	2	Ba %: Carbonate fusion	GRAVIMETRIC	0.1	100.0

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V6C 2B3

Project : WIT
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Certificate Date: 09-FEB-95
Invoice No. : I9511454
P.O. Number :
Account : AF

CERTIFICATE OF ANALYSIS A9511454

SAMPLE	PREP CODE		Mo ppm	Na %	Ni ppm	P ppm	Pb ppm	Sb ppm	Sc ppm	Sr ppm	Ti %	Tl ppm	U ppm	V ppm	W ppm	Zn ppm
W95-238	205	226	< 1	< 0.01	2	160	3240	< 2	2	354	< 0.01	< 10	< 10	36	< 10	8230
W95-239	205	226	< 1	0.02	13	1280	52	< 2	18	136	0.11	< 10	< 10	246	< 10	320
W95-240	205	226	< 1	0.02	10	1260	40	< 2	17	196	0.14	< 10	< 10	228	< 10	264
W95-241	205	226	1	0.01	11	1290	28	2	18	84	0.15	< 10	< 10	216	< 10	304
W95-300	205	226	< 1	< 0.01	10	1400	10	< 2	12	175	< 0.01	< 10	< 10	69	< 10	62
W95-301	205	226	< 1	< 0.01	10	1310	10	< 2	12	143	< 0.01	< 10	< 10	69	< 10	52
W95-302	205	226	1	< 0.01	< 1	1580	12	< 2	4	138	< 0.01	< 10	< 10	36	< 10	78
W95-303	205	226	< 1	0.01	4	1620	16	6	9	84	< 0.01	< 10	< 10	84	< 10	188
W95-304	205	226	6	< 0.01	4	60	2140	6	< 1	197	< 0.01	< 10	< 10	12	< 10	3030
W95-305	205	226	6	< 0.01	4	70	442	4	< 1	116	< 0.01	< 10	< 10	14	< 10	2720
W95-306	205	226	2	0.01	7	570	328	8	3	337	< 0.01	< 10	< 10	31	< 10	2210
W95-307	205	226	1	< 0.01	2	160	1420	18	2	349	< 0.01	< 10	< 10	21	< 10	1910
W95-308	205	226	1	< 0.01	2	400	950	4	6	363	< 0.01	< 10	< 10	73	< 10	2550
W95-309	205	226	< 1	< 0.01	6	530	568	4	9	166	< 0.01	< 10	< 10	82	< 10	1660
W95-310	205	226	< 1	< 0.01	5	550	152	< 2	8	294	< 0.01	< 10	< 10	48	< 10	2390
W95-311	205	226	< 1	< 0.01	4	350	1050	4	6	219	< 0.01	< 10	< 10	47	< 10	4800
W95-312	205	226	< 1	< 0.01	8	830	606	4	8	110	0.01	< 10	< 10	86	< 10	2850
W95-313	205	226	2	0.01	37	1500	236	< 2	16	184	0.01	< 10	< 10	190	< 10	904
W95-314	205	226	< 1	0.02	26	1210	24	2	8	230	< 0.01	< 10	< 10	95	< 10	206
W95-315	205	226	1	0.03	66	1960	14	2	13	227	0.01	< 10	< 10	134	< 10	152
W95-316	205	226	< 1	0.01	34	1350	114	2	11	139	0.03	< 10	< 10	136	< 10	736
W95-317	205	226	< 1	< 0.01	7	840	348	2	8	181	< 0.01	< 10	< 10	81	< 10	1360
W95-318	205	226	1	< 0.01	5	1050	274	4	8	142	0.02	< 10	< 10	120	< 10	1710
W95-319	205	226	1	< 0.01	4	1400	146	4	11	98	0.07	< 10	< 10	163	< 10	734
W95-320	205	226	1	0.01	7	1400	230	4	11	71	0.06	< 10	< 10	155	< 10	1730
W95-321	205	226	< 1	0.01	11	1210	204	4	11	155	0.02	< 10	< 10	129	< 10	684

CERTIFICATION:

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Account : AF

CERTIFICATE OF ANALYSIS A9511454

SAMPLE	PREP CODE		Au ppb FA+AA	Ag ppm	Al %	As ppm	Ba ppm	Be ppm	Bi ppm	Ca %	Cd ppm	Co ppm	Cr ppm	Cu ppm	Fe %	Ga ppm	Hg ppm	K %	La ppm	Mg %	Mn ppm
W95-238	205	226	< 5	27.6	0.56	< 2	70	< 0.5	2	2.04	57.5	6	118	42	1.31	< 10	6	0.01	< 10	0.90	2910
W95-239	205	226	< 5	1.2	2.48	< 2	370	0.5	4	2.91	< 0.5	23	37	132	5.49	< 10	2	0.14	< 10	3.13	3850
W95-240	205	226	< 5	0.6	2.62	< 2	960	0.5	< 2	3.41	< 0.5	20	33	128	5.15	< 10	1	0.11	< 10	2.99	4130
W95-241	205	226	< 5	< 0.2	2.26	< 2	180	0.5	< 2	2.52	< 0.5	22	41	118	5.47	10	1	0.20	< 10	2.93	3240
W95-300	205	226	< 5	< 0.2	2.33	6	130	< 0.5	< 2	5.87	< 0.5	23	14	91	4.47	< 10	1	0.40	< 10	1.15	2560
W95-301	205	226	< 5	0.4	2.06	18	90	< 0.5	2	5.17	< 0.5	23	17	66	4.32	< 10	1	0.39	< 10	1.25	2620
W95-302	205	226	< 5	< 0.2	2.05	20	200	< 0.5	2	4.39	< 0.5	10	9	22	3.67	< 10	< 1	0.35	10	0.97	2230
W95-303	205	226	< 5	0.6	1.13	8	280	0.5	< 2	2.16	< 0.5	16	21	120	3.90	< 10	1	0.47	< 10	0.77	1995
W95-304	205	226	5	45.4	0.13	4	300	< 0.5	< 2	3.33	11.5	2	147	22	1.22	< 10	14	0.03	< 10	1.27	3820
W95-305	205	226	10	17.8	0.10	118	400	< 0.5	2	4.82	8.0	2	135	19	1.58	< 10	17	0.04	< 10	1.77	5400
W95-306	205	226	< 5	68.2	0.82	12	150	< 0.5	2	4.46	9.5	7	98	85	2.25	< 10	6	0.16	< 10	1.30	2710
W95-307	205	226	< 5	174.5	0.48	8	120	< 0.5	2	3.61	7.5	4	139	80	1.45	< 10	6	0.02	< 10	1.87	2890
W95-308	205	226	< 5	55.0	1.98	2	140	0.5	2	3.97	8.0	9	84	53	3.27	< 10	9	0.01	< 10	4.34	3160
W95-309	205	226	< 5	4.4	2.42	2	460	0.5	2	3.51	4.0	12	120	39	3.79	< 10	6	0.03	< 10	4.79	2760
W95-310	205	226	< 5	0.6	1.50	< 2	290	0.5	2	7.08	6.0	9	70	11	3.94	< 10	9	0.19	< 10	4.59	3550
W95-311	205	226	5	4.6	1.21	4	170	0.5	4	6.37	21.5	8	91	37	3.30	< 10	20	0.04	< 10	3.71	5080
W95-312	205	226	< 5	10.6	2.17	< 2	490	1.0	4	4.50	12.5	12	73	64	4.43	< 10	17	0.11	< 10	4.79	3140
W95-313	205	226	< 5	0.4	1.89	8	270	0.5	4	2.78	1.5	23	128	105	4.54	10	2	0.16	< 10	2.51	1295
W95-314	205	226	< 5	< 0.2	0.92	6	1550	0.5	4	8.57	< 0.5	13	73	139	3.10	< 10	1	0.12	< 10	3.44	2050
W95-315	205	226	< 5	< 0.2	2.17	32	770	1.0	2	4.50	< 0.5	22	186	170	4.34	< 10	2	0.27	< 10	2.54	1695
W95-316	205	226	< 5	1.6	2.10	6	1050	0.5	4	5.59	1.5	19	113	113	4.39	10	4	0.17	< 10	2.24	3440
W95-317	205	226	< 5	1.6	1.44	44	110	0.5	2	6.26	4.5	13	34	40	4.06	< 10	9	0.25	< 10	2.43	4600
W95-318	205	226	15	0.4	1.70	60	130	0.5	4	3.68	7.0	15	17	34	4.60	< 10	6	0.19	< 10	2.49	3490
W95-319	205	226	< 5	< 0.2	1.62	24	580	0.5	4	2.05	1.5	12	38	13	5.21	< 10	2	0.24	< 10	1.72	2830
W95-320	205	226	< 5	0.2	1.60	6	1120	0.5	4	2.63	6.0	15	22	37	5.03	< 10	3	0.30	< 10	1.54	2970
W95-321	205	226	< 5	1.0	2.03	56	240	0.5	2	2.83	2.0	20	26	84	4.79	< 10	4	0.16	< 10	2.07	2300

CERTIFICATION:

Chemex Labs Ltd.

Analytical Chemists * Geochemists * Registered Assayers

212 Brooksbank Ave., North Vancouver
British Columbia, Canada V7J 2C1
PHONE: 604-984-0221 FAX: 604-984-0218

To: WESTLEY TECHNOLOGIES LTD.

900 - 475 HOWE ST.
VANCOUVER, B.C.
V6C 2B3

Project : WIT
Comments: ATTN: VICTOR JONES CC: COLIN CAMPBELL

Certificate Date: 09-FEB-95
Invoice No. : I9511454
P.O. Number :
Account : AF

CERTIFICATE OF ANALYSIS A9511454

SAMPLE	PREP CODE		Mo ppm	Na %	Ni ppm	P ppm	Pb ppm	Sb ppm	Sc ppm	Sr ppm	Ti %	Tl ppm	U ppm	V ppm	W ppm	Zn ppm
W95-163	205	226	< 1	< 0.01	4	2250	10	2	4	81	< 0.01	< 10	< 10	114	< 10	124
W95-164	205	226	< 1	0.02	70	1600	4	4	15	219	< 0.01	< 10	< 10	126	< 10	120
W95-165	205	226	< 1	0.01	25	1120	20	14	9	135	0.02	< 10	< 10	100	< 10	192
W95-200	205	226	< 1	< 0.01	12	1280	270	2	17	83	0.06	< 10	< 10	220	< 10	1050
W95-201	205	226	< 1	< 0.01	18	1230	112	< 2	17	103	0.04	< 10	< 10	186	< 10	728
W95-202	205	226	< 1	0.01	16	1010	214	< 2	14	120	0.03	< 10	< 10	155	< 10	1010
W95-203	205	226	1	< 0.01	7	550	650	< 2	8	128	0.01	< 10	< 10	85	< 10	3750
W95-204	205	226	< 1	< 0.01	< 1	130	642	< 2	1	261	< 0.01	< 10	< 10	21	< 10	5830
W95-205	205	226	< 1	< 0.01	1	100	2030	4	< 1	191	< 0.01	< 10	< 10	14	< 10	8980
W95-206	205	226	< 1	0.01	47	1860	36	2	14	168	0.01	< 10	< 10	144	< 10	220
W95-207	205	226	< 1	0.01	11	260	242	< 2	3	214	< 0.01	< 10	< 10	50	< 10	1255
W95-208	205	226	1	< 0.01	3	60	318	< 2	< 1	199	< 0.01	< 10	< 10	15	< 10	1570
W95-209	205	226	< 1	< 0.01	3	50	240	< 2	< 1	349	< 0.01	< 10	< 10	13	< 10	2900
W95-210	205	226	1	< 0.01	4	10	1540	< 2	< 1	248	< 0.01	< 10	< 10	7	< 10	2960
W95-211	205	226	2	< 0.01	6	620	>10000	4	5	120	< 0.01	< 10	< 10	83	60	>10000
W95-212	205	226	1	< 0.01	3	540	1865	2	5	116	< 0.01	< 10	< 10	77	40	>10000
W95-214	205	226	10	< 0.01	8	960	1110	4	6	58	< 0.01	< 10	< 10	89	< 10	4140
W95-215	205	226	20	< 0.01	7	1400	412	12	8	46	< 0.01	< 10	< 10	133	< 10	1000
W95-216	205	226	5	< 0.01	10	1080	490	4	6	37	< 0.01	< 10	< 10	87	< 10	1220
W95-217	205	226	3	< 0.01	12	1400	90	6	6	46	< 0.01	< 10	< 10	87	< 10	220
W95-218	205	226	3	0.01	13	1430	374	< 2	6	42	< 0.01	< 10	< 10	104	< 10	744
W95-219	205	226	4	< 0.01	10	1250	388	2	4	49	< 0.01	< 10	< 10	81	< 10	2120
W95-220	205	226	4	< 0.01	12	1240	280	2	6	64	< 0.01	< 10	< 10	86	< 10	592
W95-221	205	226	5	< 0.01	9	940	700	2	4	68	< 0.01	< 10	< 10	63	< 10	1830
W95-222	205	226	5	< 0.01	8	720	1135	6	2	65	< 0.01	< 10	< 10	33	< 10	1690
W95-223	205	226	2	< 0.01	18	1080	880	2	6	111	0.02	< 10	< 10	80	< 10	1330
W95-224	205	226	< 1	0.01	10	890	1060	2	11	65	0.18	< 10	< 10	160	< 10	1065
W95-225	205	226	< 1	0.01	14	1190	82	2	9	54	0.08	< 10	< 10	141	< 10	1040
W95-226	205	226	1	0.06	8	1270	14	< 2	12	187	0.18	< 10	< 10	166	< 10	138
W95-227	205	226	< 1	0.01	13	1110	20	< 2	20	153	0.20	< 10	< 10	213	< 10	220
W95-228	205	226	< 1	< 0.01	23	1030	20	2	26	106	0.26	< 10	< 10	243	< 10	380
W95-229	205	226	< 1	0.01	16	1090	14	2	20	88	0.24	< 10	< 10	255	< 10	206
W95-230	205	226	< 1	0.01	13	980	8	< 2	14	95	0.18	< 10	< 10	193	< 10	192
W95-231	205	226	< 1	0.03	12	1130	8	2	15	192	0.16	< 10	< 10	188	< 10	130
W95-232	205	226	< 1	0.02	9	1170	10	4	11	163	0.09	< 10	< 10	145	< 10	126
W95-233	205	226	2	< 0.01	3	320	832	< 2	2	223	< 0.01	< 10	< 10	40	< 10	2100
W95-234	205	226	< 1	< 0.01	12	1100	176	8	14	113	< 0.01	< 10	< 10	121	< 10	460
W95-235	205	226	< 1	0.01	12	820	176	8	10	134	< 0.01	< 10	< 10	78	< 10	638
W95-236	205	226	1	< 0.01	10	1290	388	2	13	119	0.01	< 10	< 10	138	< 10	1125
W95-237	205	226	< 1	< 0.01	8	1260	228	< 2	12	95	0.04	< 10	< 10	180	< 10	1270

CERTIFICATION: _____

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Project : WIT
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Certificate Date: 09-FEB-95
Invoice No. : I9511454
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Account : AF

CERTIFICATE OF ANALYSIS A9511454

SAMPLE	PREP CODE		Au ppb FA+AA	Ag ppm	Al %	As ppm	Ba ppm	Be ppm	Bi ppm	Ca %	Cd ppm	Co ppm	Cr ppm	Cu ppm	Fe %	Ga ppm	Hg ppm	K %	La ppm	Mg %	Mn ppm
W95-163	205	226	25	0.6	2.54	96	250	0.5	< 2	2.36	< 0.5	17	16	53	4.03	< 10	< 1	0.64	10	1.78	1860
W95-164	205	226	< 5	< 0.2	1.36	2	400	0.5	4	6.69	< 0.5	25	175	115	4.25	< 10	1	0.17	< 10	2.89	1930
W95-165	205	226	< 5	< 0.2	0.97	30	1550	0.5	2	5.32	< 0.5	18	74	42	3.58	< 10	2	0.28	< 10	1.91	1500
W95-200	205	226	< 5	3.0	2.69	24	110	1.0	4	2.42	2.5	24	48	113	5.79	10	2	0.12	< 10	3.98	3990
W95-201	205	226	< 5	4.6	2.84	14	360	0.5	4	1.97	0.5	24	93	79	5.38	< 10	2	0.08	< 10	4.96	3380
W95-202	205	226	< 5	2.6	2.75	< 2	370	1.0	2	2.30	2.5	17	107	81	4.41	10	2	0.05	< 10	5.27	3620
W95-203	205	226	5	3.4	1.85	14	50	0.5	4	4.91	17.5	12	95	52	3.46	< 10	3	0.03	< 10	3.88	5190
W95-204	205	226	15	7.2	0.60	8	40	< 0.5	4	>15.00	23.0	3	50	9	1.84	< 10	1	< 0.01	< 10	1.20	>10000
W95-205	205	226	25	11.4	0.27	38	60	< 0.5	4	13.05	45.0	3	60	14	1.55	< 10	3	< 0.01	< 10	1.36	8780
W95-206	205	226	< 5	< 0.2	1.96	4	1660	1.0	4	5.97	0.5	19	161	160	4.34	< 10	2	0.16	< 10	2.66	2710
W95-207	205	226	< 5	2.2	0.47	14	170	< 0.5	4	7.24	5.0	8	106	29	2.18	< 10	2	0.02	< 10	3.23	3570
W95-208	205	226	< 5	3.6	0.14	14	110	< 0.5	2	4.48	6.5	2	152	26	1.37	< 10	2	< 0.01	< 10	2.05	4470
W95-209	205	226	10	5.6	0.08	4	110	< 0.5	2	3.33	12.5	1	190	18	1.19	< 10	1	< 0.01	< 10	1.57	3660
W95-210	205	226	15	5.4	0.02	6	150	< 0.5	< 2	3.20	15.0	2	205	14	0.99	< 10	3	< 0.01	< 10	1.30	4170
W95-211	205	226	80	41.4	2.14	60	40	0.5	4	4.35	>100.0	13	68	71	4.34	10	15	0.04	< 10	2.31	4160
W95-212	205	226	95	9.6	1.55	58	30	< 0.5	4	4.19	>100.0	13	46	49	4.19	< 10	26	0.03	< 10	2.59	3950
W95-214	205	226	50	3.2	2.06	112	80	0.5	2	1.33	23.0	17	74	41	3.98	< 10	14	0.21	< 10	1.86	1535
W95-215	205	226	105	2.6	2.51	300	70	0.5	< 2	0.96	4.5	20	39	110	4.98	10	3	0.25	< 10	2.20	1445
W95-216	205	226	345	2.6	1.67	204	40	< 0.5	2	1.10	5.5	14	87	84	4.05	< 10	3	0.21	< 10	1.61	1505
W95-217	205	226	100	2.2	1.71	154	70	< 0.5	4	1.20	0.5	13	66	339	3.65	< 10	2	0.27	< 10	1.40	1565
W95-218	205	226	165	2.8	2.02	138	80	< 0.5	2	0.82	3.5	18	68	100	4.03	< 10	1	0.22	< 10	1.77	1455
W95-219	205	226	350	2.2	1.52	284	60	< 0.5	< 2	1.69	10.0	13	65	72	3.64	< 10	2	0.22	< 10	1.33	1680
W95-220	205	226	265	1.8	1.56	230	60	< 0.5	< 2	1.77	3.0	14	74	59	3.95	< 10	2	0.26	< 10	1.22	1585
W95-221	205	226	295	1.8	1.16	200	110	< 0.5	< 2	2.47	10.0	11	96	86	3.41	< 10	5	0.20	< 10	0.79	1455
W95-222	205	226	400	4.2	0.96	180	80	< 0.5	< 2	1.73	8.0	13	83	122	3.23	< 10	5	0.16	< 10	0.50	915
W95-223	205	226	280	1.6	1.28	84	190	0.5	2	3.96	6.0	16	84	78	3.73	< 10	3	0.31	< 10	0.85	2000
W95-224	205	226	20	0.6	1.02	20	90	< 0.5	2	4.06	3.5	12	53	73	3.85	< 10	1	0.14	< 10	1.12	1705
W95-225	205	226	20	0.2	1.85	62	140	< 0.5	< 2	0.94	3.0	21	42	32	4.91	10	1	0.11	< 10	2.30	1865
W95-226	205	226	< 5	< 0.2	1.95	< 2	2240	0.5	< 2	2.71	< 0.5	15	29	58	4.90	10	2	0.14	10	2.04	2120
W95-227	205	226	< 5	< 0.2	2.18	< 2	270	0.5	16	2.54	< 0.5	20	45	94	5.24	10	1	0.10	< 10	2.74	2250
W95-228	205	226	< 5	< 0.2	2.22	6	130	0.5	16	2.26	< 0.5	25	93	41	5.80	< 10	1	0.11	< 10	3.30	2230
W95-229	205	226	< 5	< 0.2	1.97	4	70	< 0.5	12	3.05	< 0.5	23	66	7	5.61	10	< 1	0.12	< 10	2.71	2090
W95-230	205	226	< 5	< 0.2	1.44	4	60	< 0.5	10	5.40	< 0.5	20	36	17	5.05	10	1	0.12	< 10	2.01	2400
W95-231	205	226	< 5	< 0.2	2.05	< 2	2560	< 0.5	8	3.93	< 0.5	20	33	113	4.84	10	2	0.14	< 10	2.39	2410
W95-232	205	226	< 5	1.4	1.92	< 2	1620	0.5	6	4.25	< 0.5	18	23	338	4.35	< 10	1	0.24	< 10	2.22	2620
W95-233	205	226	< 5	8.2	0.81	8	70	< 0.5	< 2	8.35	12.5	8	85	50	1.99	< 10	7	0.01	< 10	0.98	4150
W95-234	205	226	< 5	4.6	1.44	20	180	0.5	2	4.52	1.0	20	54	98	4.47	< 10	5	0.21	< 10	1.87	2930
W95-235	205	226	< 5	12.8	0.94	38	140	0.5	2	5.76	2.0	22	35	121	3.96	< 10	4	0.20	< 10	2.23	3010
W95-236	205	226	< 5	16.8	1.18	70	20	0.5	2	3.54	3.5	23	29	117	4.68	< 10	3	0.14	< 10	1.40	3720
W95-237	205	226	< 5	7.0	2.10	< 2	100	0.5	4	2.28	4.0	19	40	124	4.76	10	2	0.16	< 10	3.23	4800

CERTIFICATION: Hart Bachlaw

Chemex Labs Ltd.

Analytical Chemists * Geochemists * Registered Assayers

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A9511454

Comments: ATTN: VICTOR JONES CC: COLIN CAMPBELL

CERTIFICATE A9511454

(AF) - WESTLEY TECHNOLOGIES LTD.

Project: WIT
P.O. # :

Samples submitted to our lab in Vancouver, BC.
This report was printed on 9-JAN-97.

SAMPLE PREPARATION

CHEMEX CODE	NUMBER SAMPLES	DESCRIPTION
205	66	Geochem ring to approx 150 mesh
226	66	0-5 lb crush and split
229	66	ICP - AQ Digestion charge

* NOTE 1:

The 32 element ICP package is suitable for trace metals in soil and rock samples. Elements for which the nitric-aqua regia digestion is possibly incomplete are: Al, Ba, Be, Ca, Cr, Ga, K, La, Mg, Na, Sr, Ti, Tl, W.

ANALYTICAL PROCEDURES

CHEMEX CODE	NUMBER SAMPLES	DESCRIPTION	METHOD	DETECTION LIMIT	UPPER LIMIT
983	66	Au ppb: Fuse 30 g sample	FA-AAS	5	10000
2118	66	Ag ppm: 32 element, soil & rock	ICP-AES	0.2	200
2119	66	Al %: 32 element, soil & rock	ICP-AES	0.01	15.00
2120	66	As ppm: 32 element, soil & rock	ICP-AES	2	10000
2121	66	Ba ppm: 32 element, soil & rock	ICP-AES	10	10000
2122	66	Be ppm: 32 element, soil & rock	ICP-AES	0.5	100.0
2123	66	Bi ppm: 32 element, soil & rock	ICP-AES	2	10000
2124	66	Ca %: 32 element, soil & rock	ICP-AES	0.01	15.00
2125	66	Cd ppm: 32 element, soil & rock	ICP-AES	0.5	100.0
2126	66	Co ppm: 32 element, soil & rock	ICP-AES	1	10000
2127	66	Cr ppm: 32 element, soil & rock	ICP-AES	1	10000
2128	66	Cu ppm: 32 element, soil & rock	ICP-AES	1	10000
2150	66	Fe %: 32 element, soil & rock	ICP-AES	0.01	15.00
2130	66	Ga ppm: 32 element, soil & rock	ICP-AES	10	10000
2131	66	Hg ppm: 32 element, soil & rock	ICP-AES	1	10000
2132	66	K %: 32 element, soil & rock	ICP-AES	0.01	10.00
2151	66	La ppm: 32 element, soil & rock	ICP-AES	10	10000
2134	66	Mg %: 32 element, soil & rock	ICP-AES	0.01	15.00
2135	66	Mn ppm: 32 element, soil & rock	ICP-AES	5	10000
2136	66	Mo ppm: 32 element, soil & rock	ICP-AES	1	10000
2137	66	Na %: 32 element, soil & rock	ICP-AES	0.01	5.00
2138	66	Ni ppm: 32 element, soil & rock	ICP-AES	1	10000
2139	66	P ppm: 32 element, soil & rock	ICP-AES	10	10000
2140	66	Pb ppm: 32 element, soil & rock	ICP-AES	2	10000
2141	66	Sb ppm: 32 element, soil & rock	ICP-AES	2	10000
2142	66	Sc ppm: 32 elements, soil & rock	ICP-AES	1	10000
2143	66	Sr ppm: 32 element, soil & rock	ICP-AES	1	10000
2144	66	Ti %: 32 element, soil & rock	ICP-AES	0.01	5.00
2145	66	Tl ppm: 32 element, soil & rock	ICP-AES	10	10000
2146	66	U ppm: 32 element, soil & rock	ICP-AES	10	10000
2147	66	V ppm: 32 element, soil & rock	ICP-AES	1	10000
2148	66	W ppm: 32 element, soil & rock	ICP-AES	10	10000
2149	66	Zn ppm: 32 element, soil & rock	ICP-AES	2	10000

Chemex Labs Ltd.

Analytical Chemists * Geochemists * Registered Assayers

212 Brooksbank Ave., North Vancouver
British Columbia, Canada V7J 2C1
PHONE: 604-984-0221 FAX: 604-984-0218

To: WESTLEY TECHNOLOGIES LTD.

900 - 475 HOWE ST.
VANCOUVER, B.C.
V6C 2B3

Project :
Comments: ATTN: VICTOR JONES CC: COLIN CAMPBELL

Certificate Date: 09-FEB-95
Invoice No. : I9511433
P.O. Number :
Account : AF

CERTIFICATE OF ANALYSIS A9511433

SAMPLE	PREP CODE		Pb %	Zn %	Ba %
W95-115	244	--	-----	3.64	0.7
W95-161	244	--	0.56	2.29	12.4
W95-162	244	--	1.03	3.47	11.9
W95-106	244	--	-----	-----	0.3
W95-107	244	--	-----	-----	0.4
W95-108	244	--	-----	-----	0.2
W95-109	244	--	-----	-----	0.9
W95-110	244	--	-----	-----	0.5
W95-111	244	--	-----	-----	1.0
W95-112	244	--	-----	-----	1.6
W95-113	244	--	-----	-----	1.6

CERTIFICATION:

Chemex Labs Ltd.

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V6C 2B3

A9511433

Comments: ATTN: VICTOR JONES CC: COLIN CAMPBELL

CERTIFICATE A9511433

(AF) - WESTLEY TECHNOLOGIES LTD.

Project:
P.O. # :

Samples submitted to our lab in Vancouver, BC.
This report was printed on 9-JAN-97.

SAMPLE PREPARATION

CHEMEX CODE	NUMBER SAMPLES	DESCRIPTION
244	11	Pulp; prev. prepared at Chemex

ANALYTICAL PROCEDURES

CHEMEX CODE	NUMBER SAMPLES	DESCRIPTION	METHOD	DETECTION LIMIT	UPPER LIMIT
312	2	Pb %: Reverse Aqua-Regia digest	AAS	0.01	100.0
316	3	Zn %: Reverse Aqua-Regia digest	AAS	0.01	100.0
351	11	Ba %: Carbonate fusion	GRAVIMETRIC	0.1	100.0

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VANCOUVER, B.C.
V6C 2B3

Project :
Comments: ATTN: VICTOR JONES CC: COLIN CAMPBELL

Certificate Date: 02-FEB-95
Invoice No. : I9511177
P.O. Number :
Account : AF

CERTIFICATE OF ANALYSIS A9511177

SAMPLE	PREP CODE		Mo ppm	Na %	Ni ppm	P ppm	Pb ppm	Sb ppm	Sc ppm	Sr ppm	Ti %	Tl ppm	U ppm	V ppm	W ppm	Zn ppm
W95-150	205	226	1	< 0.01	21	1410	54	< 2	4	83	< 0.01	< 10	< 10	84	< 10	164
W95-151	205	226	7	< 0.01	16	1190	326	< 2	8	67	< 0.01	< 10	< 10	129	< 10	568
W95-152	205	226	8	0.01	15	1300	928	< 2	9	69	0.02	< 10	< 10	153	< 10	1585
W95-153	205	226	19	< 0.01	17	1470	2790	4	7	66	< 0.01	< 10	< 10	132	< 10	6760
W95-154	205	226	12	< 0.01	10	1420	556	< 2	11	53	< 0.01	< 10	< 10	193	< 10	1075
W95-155	205	226	9	< 0.01	13	1310	284	< 2	10	104	< 0.01	< 10	< 10	177	< 10	920
W95-156	205	226	19	< 0.01	16	990	1685	2	8	58	< 0.01	< 10	< 10	140	< 10	3200
W95-157	205	226	45	< 0.01	17	1160	1620	6	7	63	< 0.01	< 10	< 10	134	< 10	2600
W95-158	205	226	25	0.01	11	1590	346	4	11	70	< 0.01	< 10	< 10	187	< 10	1325
W95-159	205	226	28	< 0.01	12	1400	1850	2	8	50	< 0.01	< 10	< 10	150	< 10	3810
W95-160	205	226	30	< 0.01	11	1130	554	6	7	78	< 0.01	< 10	< 10	125	< 10	2850
W95-161	205	226	1	< 0.01	41	770	5120	14	12	78	0.12	< 10	< 10	115	< 10	>10000
W95-162	205	226	2	< 0.01	59	340	9820	24	4	116	0.01	< 10	< 10	54	< 10	>10000

CERTIFICATION: _____

Chemex Labs Ltd.

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V6C 2B3

Project :
Comments: ATTN: VICTOR JONES CC: COLIN CAMPBELL

Certificate Date: 02-FEB-95
Invoice No. : I9511177
P.O. Number :
Account : AF

CERTIFICATE OF ANALYSIS A9511177

SAMPLE	PREP CODE		Au ppb FA+AA	Ag ppm	Al %	As ppm	Ba ppm	Be ppm	Bi ppm	Ca %	Cd ppm	Co ppm	Cr ppm	Cu ppm	Fe %	Ga ppm	Hg ppm	K %	La ppm	Mg %	Mn ppm
W95-150	205	226	145	1.2	2.60	146	230	0.5	2	4.48	< 0.5	12	25	115	3.88	10	< 1	0.39	< 10	2.40	3870
W95-151	205	226	170	5.0	2.24	178	110	< 0.5	< 2	4.54	3.0	16	62	136	3.89	10	1	0.16	< 10	2.20	4040
W95-152	205	226	440	4.0	2.36	146	170	< 0.5	< 2	2.79	9.5	20	42	185	4.30	< 10	2	0.21	< 10	2.11	2900
W95-153	205	226	700	6.0	2.03	198	70	< 0.5	< 2	3.14	58.0	21	60	369	3.81	< 10	6	0.25	< 10	1.71	2910
W95-154	205	226	115	4.6	3.20	220	40	0.5	2	1.02	7.5	25	41	80	5.99	10	1	0.21	< 10	3.02	2590
W95-155	205	226	100	4.6	2.90	188	40	< 0.5	2	2.25	4.0	23	54	84	5.10	10	1	0.21	< 10	2.67	3190
W95-156	205	226	490	51.8	1.99	328	30	< 0.5	< 2	3.44	15.5	21	135	249	5.01	< 10	3	0.18	< 10	1.82	3510
W95-157	205	226	455	84.8	1.88	266	30	< 0.5	< 2	2.72	10.5	19	124	182	4.27	10	2	0.25	< 10	1.75	3090
W95-158	205	226	85	7.2	2.91	206	50	0.5	2	2.29	4.5	23	44	206	5.29	10	1	0.31	< 10	2.45	3340
W95-159	205	226	170	7.8	2.03	244	30	< 0.5	< 2	1.51	14.0	24	71	256	4.72	< 10	2	0.31	< 10	1.85	2300
W95-160	205	226	205	10.2	1.66	310	20	< 0.5	< 2	1.98	12.0	22	75	329	4.20	< 10	2	0.21	< 10	1.41	2380
W95-161	205	226	60	4.6	1.74	410	10	< 0.5	< 2	0.36	75.5	42	114	88	6.54	< 10	9	0.09	< 10	2.42	1195
W95-162	205	226	405	12.0	1.14	420	20	< 0.5	< 2	1.02	>100.0	18	222	122	3.71	< 10	7	0.02	< 10	1.47	1415

CERTIFICATION: [illegible]

Chemex Labs Ltd.

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To: WESTLEY TECHNOLOGIES LTD.

900 - 475 HOWE ST.
VANCOUVER, B.C.
V6C 2B3

A9511177

Comments: ATTN: VICTOR JONES CC: COLIN CAMPBELL

CERTIFICATE A9511177

(AF) - WESTLEY TECHNOLOGIES LTD.

Project:
P.O. # :

Samples submitted to our lab in Vancouver, BC.
This report was printed on 9-JAN-97.

SAMPLE PREPARATION

CHEMEX CODE	NUMBER SAMPLES	DESCRIPTION
205	13	Geochem ring to approx 150 mesh
226	13	0-5 lb crush and split
229	13	ICP - AQ Digestion charge

* NOTE 1:

The 32 element ICP package is suitable for trace metals in soil and rock samples. Elements for which the nitric-aqua regia digestion is possibly incomplete are: Al, Ba, Be, Ca, Cr, Ga, K, La, Mg, Na, Sr, Ti, Tl, W.

ANALYTICAL PROCEDURES

CHEMEX CODE	NUMBER SAMPLES	DESCRIPTION	METHOD	DETECTION LIMIT	UPPER LIMIT
983	13	Au ppb: Fuse 30 g sample	FA-AAS	5	10000
2118	13	Ag ppm: 32 element, soil & rock	ICP-AES	0.2	200
2119	13	Al %: 32 element, soil & rock	ICP-AES	0.01	15.00
2120	13	As ppm: 32 element, soil & rock	ICP-AES	2	10000
2121	13	Ba ppm: 32 element, soil & rock	ICP-AES	10	10000
2122	13	Be ppm: 32 element, soil & rock	ICP-AES	0.5	100.0
2123	13	Bi ppm: 32 element, soil & rock	ICP-AES	2	10000
2124	13	Ca %: 32 element, soil & rock	ICP-AES	0.01	15.00
2125	13	Cd ppm: 32 element, soil & rock	ICP-AES	0.5	100.0
2126	13	Co ppm: 32 element, soil & rock	ICP-AES	1	10000
2127	13	Cr ppm: 32 element, soil & rock	ICP-AES	1	10000
2128	13	Cu ppm: 32 element, soil & rock	ICP-AES	1	10000
2150	13	Fe %: 32 element, soil & rock	ICP-AES	0.01	15.00
2130	13	Ga ppm: 32 element, soil & rock	ICP-AES	10	10000
2131	13	Hg ppm: 32 element, soil & rock	ICP-AES	1	10000
2132	13	K %: 32 element, soil & rock	ICP-AES	0.01	10.00
2151	13	La ppm: 32 element, soil & rock	ICP-AES	10	10000
2134	13	Mg %: 32 element, soil & rock	ICP-AES	0.01	15.00
2135	13	Mn ppm: 32 element, soil & rock	ICP-AES	5	10000
2136	13	Mo ppm: 32 element, soil & rock	ICP-AES	1	10000
2137	13	Na %: 32 element, soil & rock	ICP-AES	0.01	5.00
2138	13	Ni ppm: 32 element, soil & rock	ICP-AES	1	10000
2139	13	P ppm: 32 element, soil & rock	ICP-AES	10	10000
2140	13	Pb ppm: 32 element, soil & rock	ICP-AES	2	10000
2141	13	Sb ppm: 32 element, soil & rock	ICP-AES	2	10000
2142	13	Sc ppm: 32 elements, soil & rock	ICP-AES	1	10000
2143	13	Sr ppm: 32 element, soil & rock	ICP-AES	1	10000
2144	13	Ti %: 32 element, soil & rock	ICP-AES	0.01	5.00
2145	13	Tl ppm: 32 element, soil & rock	ICP-AES	10	10000
2146	13	U ppm: 32 element, soil & rock	ICP-AES	10	10000
2147	13	V ppm: 32 element, soil & rock	ICP-AES	1	10000
2148	13	W ppm: 32 element, soil & rock	ICP-AES	10	10000
2149	13	Zn ppm: 32 element, soil & rock	ICP-AES	2	10000

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To: WESTLEY TECHNOLOGIES LTD.

900 - 475 HOWE ST.
VANCOUVER, B.C.
V6C 2B3

Project :
Comments: ATTN: VICTOR JONES CC: COLIN CAMPBELL

Certificate Date: 02-FEB-95
Invoice No. : I9511173
P.O. Number :
Account : AF

CERTIFICATE OF ANALYSIS A9511173

SAMPLE	PREP CODE		Mo ppm	Na %	Ni ppm	P ppm	Pb ppm	Sb ppm	Sc ppm	Sr ppm	Ti %	Tl ppm	U ppm	V ppm	W ppm	Zn ppm
W95-111	205	226	18	< 0.01	8	1450	434	4	8	50	< 0.01	< 10	< 10	141	< 10	1220
W95-112	205	226	8	< 0.01	10	1270	4090	< 2	10	60	< 0.01	< 10	< 10	161	< 10	5100
W95-113	205	226	< 1	< 0.01	10	590	2770	< 2	9	122	0.01	< 10	< 10	106	< 10	5480
W95-114	205	226	< 1	< 0.01	18	1000	716	< 2	16	118	0.01	< 10	< 10	147	< 10	3920
W95-115	205	226	< 1	< 0.01	20	1000	1400	< 2	10	120	0.01	< 10	< 10	118	< 10	>10000
W95-117	205	226	1	0.01	25	1430	1305	10	12	96	0.06	< 10	< 10	181	< 10	6970
W95-118	205	226	< 1	0.03	63	2140	24	< 2	11	127	0.16	< 10	< 10	181	< 10	364
W95-119	205	226	< 1	0.05	68	2110	28	< 2	10	169	0.17	< 10	< 10	178	< 10	190
W95-120	205	226	< 1	0.01	18	1450	296	< 2	12	85	0.09	< 10	< 10	210	< 10	1750
W95-121	205	226	1	< 0.01	19	1750	968	16	15	51	0.23	< 10	< 10	229	< 10	2760
W95-122	205	226	1	< 0.01	18	1410	4410	4	12	47	0.22	< 10	< 10	162	< 10	9300
W95-123	205	226	< 1	< 0.01	18	1520	706	2	16	43	0.25	< 10	< 10	181	< 10	2010
W95-124	205	226	< 1	< 0.01	18	1380	946	2	14	46	0.23	< 10	< 10	178	< 10	2360
W95-125	205	226	2	< 0.01	23	1530	1205	24	14	38	0.19	< 10	< 10	188	< 10	5360
W95-126	205	226	1	< 0.01	19	1620	710	12	14	44	0.22	< 10	< 10	193	< 10	3720
W95-127	205	226	< 1	< 0.01	19	1570	760	2	14	43	0.25	< 10	< 10	219	< 10	2650
W95-128	205	226	1	< 0.01	17	1470	748	2	15	49	0.24	< 10	< 10	221	< 10	2610
W95-129	205	226	1	< 0.01	20	1630	530	4	17	60	0.15	< 10	< 10	283	< 10	2570
W95-130	205	226	< 1	< 0.01	23	1680	726	2	18	59	0.19	< 10	< 10	288	< 10	2380
W95-131	205	226	3	< 0.01	19	1230	594	34	12	33	0.19	10	< 10	180	< 10	2300
W95-132.5	205	226	1	0.02	53	1740	90	< 2	14	222	0.21	< 10	< 10	185	< 10	356
W95-133.5	205	226	< 1	< 0.01	76	1030	404	< 2	20	90	0.21	< 10	< 10	157	< 10	1285
W95-134.5	205	226	< 1	< 0.01	80	1020	476	< 2	20	93	0.22	< 10	< 10	149	< 10	1530
W95-135.5	205	226	< 1	< 0.01	76	1010	620	< 2	20	86	0.22	< 10	< 10	161	< 10	2500

CERTIFICATION: _____

Chemex Labs Ltd.

Analytical Chemists * Geochemists * Registered Assayers

212 Brooksbank Ave., North Vancouver
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To: WESTLEY TECHNOLOGIES LTD.

900 - 475 HOWE ST.
VANCOUVER, B.C.
V6C 2B3

Project :
Comments: ATTN: VICTOR JONES CC: COLIN CAMPBELL

Certificate Date: 02-FEB-95
Invoice No. : I9511173
P.O. Number :
Account : AF

CERTIFICATE OF ANALYSIS A9511173

SAMPLE	PREP CODE		Au ppb FA+AA	Ag ppm	Al %	As ppm	Ba ppm	Be ppm	Bi ppm	Ca %	Cd ppm	Co ppm	Cr ppm	Cu ppm	Fe %	Ga ppm	Hg ppm	K %	La ppm	Mg %	Mn ppm
W95-111	205	226	120	5.6	1.76	218	30	< 0.5	< 2	1.40	6.0	24	30	184	3.79	10	1	0.26	< 10	1.51	1960
W95-112	205	226	150	4.4	2.77	172	40	0.5	2	1.08	28.5	22	23	95	4.93	10	2	0.18	< 10	2.88	2520
W95-113	205	226	195	2.4	2.05	28	170	< 0.5	2	2.42	24.5	11	97	15	4.13	< 10	2	0.03	< 10	3.13	3460
W95-114	205	226	70	1.6	3.12	42	120	0.5	2	1.30	12.0	26	92	12	6.26	10	1	0.04	< 10	4.47	3770
W95-115	205	226	200	2.8	2.06	74	20	< 0.5	< 2	4.07	>100.0	20	49	88	5.89	< 10	9	0.07	< 10	2.03	3510
W95-117	205	226	55	3.8	2.22	324	20	0.5	2	1.72	27.5	29	80	109	5.88	< 10	2	0.17	< 10	2.57	1845
W95-118	205	226	< 5	< 0.2	2.20	4	570	0.5	< 2	3.60	1.0	22	213	195	4.50	10	1	0.12	< 10	2.84	2180
W95-119	205	226	< 5	< 0.2	2.43	6	1070	0.5	< 2	3.32	< 0.5	22	229	192	4.95	< 10	< 1	0.17	< 10	3.20	2060
W95-120	205	226	25	2.2	2.31	90	30	0.5	2	1.18	5.5	25	40	88	5.71	< 10	2	0.15	< 10	3.23	1490
W95-121	205	226	25	2.2	1.96	196	30	< 0.5	< 2	0.85	8.5	28	42	174	6.57	10	3	0.21	< 10	2.43	1370
W95-122	205	226	30	2.4	1.32	118	30	< 0.5	< 2	0.88	40.0	20	46	66	5.19	< 10	5	0.22	< 10	1.48	885
W95-123	205	226	10	1.4	1.97	48	40	< 0.5	4	0.84	6.0	22	44	45	5.69	10	3	0.24	< 10	2.33	1305
W95-124	205	226	5	1.4	1.75	62	40	< 0.5	< 2	0.83	8.0	20	52	43	5.14	10	3	0.18	< 10	1.98	1150
W95-125	205	226	40	3.4	2.05	536	10	0.5	< 2	0.97	23.5	42	31	68	8.03	10	6	0.24	< 10	2.28	1450
W95-126	205	226	15	2.0	1.97	250	40	< 0.5	< 2	0.62	13.5	27	36	46	6.72	10	4	0.22	< 10	2.15	1435
W95-127	205	226	5	1.4	1.96	12	100	< 0.5	< 2	0.67	10.0	22	42	79	5.94	10	3	0.20	< 10	2.16	1595
W95-128	205	226	10	1.6	2.05	30	90	0.5	6	0.68	9.5	24	41	47	5.84	10	2	0.17	< 10	2.47	1665
W95-129	205	226	20	2.2	2.63	88	120	0.5	2	0.58	6.0	32	34	94	6.56	10	2	0.15	< 10	3.41	2180
W95-130	205	226	30	2.4	2.60	78	110	0.5	6	0.60	5.5	39	35	77	6.75	10	3	0.18	< 10	3.29	2060
W95-131	205	226	40	4.2	1.87	766	10	< 0.5	< 2	0.55	8.5	41	40	39	8.34	< 10	3	0.15	< 10	2.21	1155
W95-132.5	205	226	< 5	0.6	2.42	44	110	0.5	8	2.47	0.5	30	166	153	5.13	10	< 1	0.15	< 10	2.63	2080
W95-133.5	205	226	< 5	3.4	2.63	16	130	0.5	< 2	1.93	3.5	31	173	139	5.26	10	< 1	0.13	< 10	3.48	2650
W95-134.5	205	226	< 5	3.6	2.73	14	160	0.5	2	2.02	3.5	30	190	138	5.47	10	1	0.16	< 10	3.81	2730
W95-135.5	205	226	< 5	2.4	2.52	18	90	0.5	< 2	1.10	10.0	34	182	89	5.16	10	2	0.12	< 10	3.64	2300

CERTIFICATION: _____

Chemex Labs Ltd.

Analytical Chemists * Geochemists * Registered Assayers

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To: WESTLEY TECHNOLOGIES LTD.

900 - 475 HOWE ST.
VANCOUVER, B.C.
V6C 2B3

A9511173

Comments: ATTN: VICTOR JONES CC: COLIN CAMPBELL

CERTIFICATE A9511173

(AF) - WESTLEY TECHNOLOGIES LTD.

Project:
P.O. # :

Samples submitted to our lab in Vancouver, BC.
This report was printed on 9-JAN-97.

SAMPLE PREPARATION

CHEMEX CODE	NUMBER SAMPLES	DESCRIPTION
205	24	Geochem ring to approx 150 mesh
226	24	0-5 lb crush and split
229	24	ICP - AQ Digestion charge

* NOTE 1:

The 32 element ICP package is suitable for trace metals in soil and rock samples. Elements for which the nitric-aqua regia digestion is possibly incomplete are: Al, Ba, Be, Ca, Cr, Ga, K, La, Mg, Na, Sr, Ti, Tl, W.

ANALYTICAL PROCEDURES

CHEMEX CODE	NUMBER SAMPLES	DESCRIPTION	METHOD	DETECTION LIMIT	UPPER LIMIT
983	24	Au ppb: Fuse 30 g sample	FA-AAS	5	10000
2118	24	Ag ppm: 32 element, soil & rock	ICP-AES	0.2	200
2119	24	Al %: 32 element, soil & rock	ICP-AES	0.01	15.00
2120	24	As ppm: 32 element, soil & rock	ICP-AES	2	10000
2121	24	Ba ppm: 32 element, soil & rock	ICP-AES	10	10000
2122	24	Be ppm: 32 element, soil & rock	ICP-AES	0.5	100.0
2123	24	Bi ppm: 32 element, soil & rock	ICP-AES	2	10000
2124	24	Ca %: 32 element, soil & rock	ICP-AES	0.01	15.00
2125	24	Cd ppm: 32 element, soil & rock	ICP-AES	0.5	100.0
2126	24	Co ppm: 32 element, soil & rock	ICP-AES	1	10000
2127	24	Cr ppm: 32 element, soil & rock	ICP-AES	1	10000
2128	24	Cu ppm: 32 element, soil & rock	ICP-AES	1	10000
2150	24	Fe %: 32 element, soil & rock	ICP-AES	0.01	15.00
2130	24	Ga ppm: 32 element, soil & rock	ICP-AES	10	10000
2131	24	Hg ppm: 32 element, soil & rock	ICP-AES	1	10000
2132	24	K %: 32 element, soil & rock	ICP-AES	0.01	10.00
2151	24	La ppm: 32 element, soil & rock	ICP-AES	10	10000
2134	24	Mg %: 32 element, soil & rock	ICP-AES	0.01	15.00
2135	24	Mn ppm: 32 element, soil & rock	ICP-AES	5	10000
2136	24	Mo ppm: 32 element, soil & rock	ICP-AES	1	10000
2137	24	Na %: 32 element, soil & rock	ICP-AES	0.01	5.00
2138	24	Ni ppm: 32 element, soil & rock	ICP-AES	1	10000
2139	24	P ppm: 32 element, soil & rock	ICP-AES	10	10000
2140	24	Pb ppm: 32 element, soil & rock	ICP-AES	2	10000
2141	24	Sb ppm: 32 element, soil & rock	ICP-AES	2	10000
2142	24	Sc ppm: 32 elements, soil & rock	ICP-AES	1	10000
2143	24	Sr ppm: 32 element, soil & rock	ICP-AES	1	10000
2144	24	Ti %: 32 element, soil & rock	ICP-AES	0.01	5.00
2145	24	Tl ppm: 32 element, soil & rock	ICP-AES	10	10000
2146	24	U ppm: 32 element, soil & rock	ICP-AES	10	10000
2147	24	V ppm: 32 element, soil & rock	ICP-AES	1	10000
2148	24	W ppm: 32 element, soil & rock	ICP-AES	10	10000
2149	24	Zn ppm: 32 element, soil & rock	ICP-AES	2	10000

Chemex Labs Ltd.

Analytical Chemists * Geochemists * Registered Assayers

212 Brooksbank Ave., North Vancouver
British Columbia, Canada V7J 2C1
PHONE: 604-984-0221 FAX: 604-984-0218

To: WESTLEY TECHNOLOGIES LTD.

900 - 475 HOWE ST.
VANCOUVER, B.C.
V6C 2B3

Project :
Comments: ATTN: VICTOR JONES CC: COLIN CAMPBELL

Certificate Date: 31-JAN-95
Invoice No. : I9511125
P.O. Number :
Account : AF

CERTIFICATE OF ANALYSIS A9511125

SAMPLE	PREP CODE		Pb %	Zn %
W95-106	244	--	-----	2.25
W95-107	244	--	-----	2.30
W95-108	244	--	-----	1.58
W95-109	244	--	-----	2.66
W95-110	244	--	1.11	12.20
W95-111	244	--	2.33	7.19
W95-112	244	--	7.58	15.30
W95-113	244	--	4.90	13.50

CERTIFICATION: Hart Bichlen

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V6C 2B3

A9511125

Comments: ATTN: VICTOR JONES CC: COLIN CAMPBELL

CERTIFICATE A9511125

(AF) - WESTLEY TECHNOLOGIES LTD.

Project:
P.O. # :

Samples submitted to our lab in Vancouver, BC.
This report was printed on 9-JAN-97.

SAMPLE PREPARATION

CHEMEX CODE	NUMBER SAMPLES	DESCRIPTION
244	8	Pulp; prev. prepared at Chemex

ANALYTICAL PROCEDURES

CHEMEX CODE	NUMBER SAMPLES	DESCRIPTION	METHOD	DETECTION LIMIT	UPPER LIMIT
312	4	Pb %: Reverse Aqua-Regia digest	AAS	0.01	100.0
316	8	Zn %: Reverse Aqua-Regia digest	AAS	0.01	100.0

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900 - 475 HOWE ST.
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V6C 2B3

Project :
Comments: ATTN: VICTOR JONES CC: COLIN CAMPBELL

Certificate Date: 25-JAN-95
Invoice No. : I9510817
P.O. Number :
Account : AF

CERTIFICATE OF ANALYSIS A9510817

SAMPLE	PREP CODE		Mo ppm	Na %	Ni ppm	P ppm	Pb ppm	Sb ppm	Sc ppm	Sr ppm	Ti %	Tl ppm	U ppm	V ppm	W ppm	Zn ppm
W95-101	255	295	< 1	0.02	14	1340	56	4	11	98	< 0.01	< 10	< 10	115	< 10	218
W95-102	255	295	< 1	0.02	12	1330	42	4	11	132	< 0.01	< 10	< 10	113	< 10	190
W95-103	255	295	< 1	0.02	10	1390	12	4	11	105	< 0.01	< 10	< 10	136	< 10	198
W95-104	255	295	< 1	0.03	7	1580	2	< 2	10	134	0.01	< 10	< 10	151	< 10	102
W95-105	255	295	3	0.01	4	1140	206	4	8	65	< 0.01	< 10	< 10	119	< 10	7500
W95-106	255	295	6	< 0.01	5	740	290	8	7	46	< 0.01	< 10	< 10	105	< 10	>10000
W95-107	255	295	1	< 0.01	4	700	394	< 2	9	35	0.01	< 10	< 10	133	< 10	>10000
W95-108	255	295	2	< 0.01	6	350	498	8	6	26	< 0.01	< 10	< 10	86	< 10	>10000
W95-109	255	295	6	< 0.01	6	130	1295	16	2	22	< 0.01	< 10	< 10	28	< 10	>10000
W95-110	255	295	1	< 0.01	6	440	9150	< 2	7	22	0.01	< 10	< 10	100	< 10	>10000
W95-111	255	295	< 1	0.01	4	320	>10000	8	5	78	< 0.01	< 10	10	60	< 10	>10000
W95-112	255	295	1	< 0.01	3	170	>10000	< 2	2	35	< 0.01	< 10	< 10	48	< 10	>10000
W95-113	255	295	< 1	< 0.01	5	430	>10000	< 2	8	39	< 0.01	< 10	< 10	100	< 10	>10000

CERTIFICATION: [illegible]

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To: WESTLEY TECHNOLOGIES LTD.

900 - 475 HOWE ST.
VANCOUVER, B.C.
V6C 2B3

Project :
Comments: ATTN: VICTOR JONES CC: COLIN CAMPBELL

Certificate Date: 25-JAN-95
Invoice No. : I9510817
P.O. Number :
Account : AF

CERTIFICATE OF ANALYSIS A9510817

SAMPLE	PREP CODE		Au ppb RUSH	Ag ppm	Al %	As ppm	Ba ppm	Be ppm	Bi ppm	Ca %	Cd ppm	Co ppm	Cr ppm	Cu ppm	Fe %	Ga ppm	Hg ppm	K %	La ppm	Mg %	Mn ppm
W95-101	255	295	< 5	0.6	2.51	12	70	< 0.5	< 2	2.25	0.5	26	65	95	4.97	10	< 1	0.34	< 10	1.80	985
W95-102	255	295	< 5	0.4	2.80	2	80	< 0.5	< 2	3.35	0.5	25	49	108	4.94	10	< 1	0.30	< 10	2.02	1155
W95-103	255	295	< 5	< 0.2	2.89	10	160	< 0.5	< 2	2.98	< 0.5	25	42	81	5.21	10	< 1	0.35	< 10	2.05	1220
W95-104	255	295	< 5	< 0.2	2.48	2	210	< 0.5	< 2	2.95	< 0.5	21	17	125	5.40	10	< 1	0.33	< 10	1.58	1220
W95-105	255	295	170	2.0	2.57	58	60	< 0.5	< 2	2.20	43.0	16	38	498	5.23	10	< 1	0.20	< 10	2.21	2620
W95-106	255	295	390	3.4	2.27	88	100	< 0.5	6	1.91	>100.0	15	67	413	4.95	10	< 1	0.12	< 10	2.42	2940
W95-107	255	295	345	4.8	3.42	120	110	< 0.5	6	0.53	96.5	19	55	613	7.19	10	1	0.05	< 10	3.91	2850
W95-108	255	295	515	8.4	1.85	104	90	< 0.5	2	0.91	66.5	18	119	92	4.74	< 10	3	0.01	< 10	2.24	1830
W95-109	255	295	715	36.4	0.49	110	10	< 0.5	6	1.46	>100.0	9	151	503	4.25	< 10	5	0.01	< 10	0.93	1240
W95-110	255	295	2810	7.6	1.86	124	20	< 0.5	10	0.80	>100.0	19	59	159	6.74	10	14	0.02	< 10	1.43	2490
W95-111	255	295	665	11.6	1.05	18	40	< 0.5	2	6.15	>100.0	10	62	145	3.62	< 10	13	0.01	< 10	3.27	4680
W95-112	255	295	740	51.0	0.76	14	20	< 0.5	16	1.51	>100.0	8	66	105	2.74	< 10	16	< 0.01	< 10	0.83	1800
W95-113	255	295	550	22.6	1.37	16	20	< 0.5	20	1.64	>100.0	10	75	59	4.10	< 10	24	0.01	< 10	1.07	1890

CERTIFICATION: Hart Bichan

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o: WESTLEY TECHNOLOGIES LTD.

900 - 475 HOWE ST.
VANCOUVER, B.C.
V6C 2B3

A9510817

Comments: ATTN: VICTOR JONES CC: COLIN CAMPBELL

CERTIFICATE A9510817

(AF) - WESTLEY TECHNOLOGIES LTD.

Project:
P.O. # :

Samples submitted to our lab in Vancouver, BC.
This report was printed on 9-JAN-97.

SAMPLE PREPARATION

CHEMEX CODE	NUMBER SAMPLES	DESCRIPTION
255	13	RUSH Geo ring to approx 150 mesh
295	13	RUSH Crush and split (0-5 lbs)
229	13	ICP - AQ Digestion charge

* NOTE 1:

The 32 element ICP package is suitable for trace metals in soil and rock samples. Elements for which the nitric-aqua regia digestion is possibly incomplete are: Al, Ba, Be, Ca, Cr, Ga, K, La, Mg, Na, Sr, Ti, Tl, W.

ANALYTICAL PROCEDURES

CHEMEX CODE	NUMBER SAMPLES	DESCRIPTION	METHOD	DETECTION LIMIT	UPPER LIMIT
991	13	Au ppb: Fuse 30 g sample	FA-AAS	5	10000
2118	13	Ag ppm: 32 element, soil & rock	ICP-AES	0.2	200
2119	13	Al %: 32 element, soil & rock	ICP-AES	0.01	15.00
2120	13	As ppm: 32 element, soil & rock	ICP-AES	2	10000
2121	13	Ba ppm: 32 element, soil & rock	ICP-AES	10	10000
2122	13	Be ppm: 32 element, soil & rock	ICP-AES	0.5	100.0
2123	13	Bi ppm: 32 element, soil & rock	ICP-AES	2	10000
2124	13	Ca %: 32 element, soil & rock	ICP-AES	0.01	15.00
2125	13	Cd ppm: 32 element, soil & rock	ICP-AES	0.5	100.0
2126	13	Co ppm: 32 element, soil & rock	ICP-AES	1	10000
2127	13	Cr ppm: 32 element, soil & rock	ICP-AES	1	10000
2128	13	Cu ppm: 32 element, soil & rock	ICP-AES	1	10000
2150	13	Fe %: 32 element, soil & rock	ICP-AES	0.01	15.00
2130	13	Ga ppm: 32 element, soil & rock	ICP-AES	10	10000
2131	13	Hg ppm: 32 element, soil & rock	ICP-AES	1	10000
2132	13	K %: 32 element, soil & rock	ICP-AES	0.01	10.00
2151	13	La ppm: 32 element, soil & rock	ICP-AES	10	10000
2134	13	Mg %: 32 element, soil & rock	ICP-AES	0.01	15.00
2135	13	Mn ppm: 32 element, soil & rock	ICP-AES	5	10000
2136	13	Mo ppm: 32 element, soil & rock	ICP-AES	1	10000
2137	13	Na %: 32 element, soil & rock	ICP-AES	0.01	5.00
2138	13	Ni ppm: 32 element, soil & rock	ICP-AES	1	10000
2139	13	P ppm: 32 element, soil & rock	ICP-AES	10	10000
2140	13	Pb ppm: 32 element, soil & rock	ICP-AES	2	10000
2141	13	Sb ppm: 32 element, soil & rock	ICP-AES	2	10000
2142	13	Sc ppm: 32 elements, soil & rock	ICP-AES	1	10000
2143	13	Sr ppm: 32 element, soil & rock	ICP-AES	1	10000
2144	13	Ti %: 32 element, soil & rock	ICP-AES	0.01	5.00
2145	13	Tl ppm: 32 element, soil & rock	ICP-AES	10	10000
2146	13	U ppm: 32 element, soil & rock	ICP-AES	10	10000
2147	13	V ppm: 32 element, soil & rock	ICP-AES	1	10000
2148	13	W ppm: 32 element, soil & rock	ICP-AES	10	10000
2149	13	Zn ppm: 32 element, soil & rock	ICP-AES	2	10000

INDATA RESOURCES LTD. **DRILL LOG** sample data

SAMPLE					CORE RECOVERY		VISUAL ESTIMATES (% ORE MINERALS)	ASSAY RESULTS						
NUMBER	FROM	TO	TOTAL METRES	M.S.	%	AMT. LOST		Au (ppb)	Ag (ppm)	Pb (ppm)	Zn (ppm)			
W95-300	35	36.5	1.5		100			<5	<.2	10	62			
-301	36.5	38	1.5		"			<5	0.4	10	52			
-302	38	39.5	1.5		90			<5	<.2	12	78			
-303	62.2	63.7	1.5		30			<5	0.6	16	188			
-304	63.7	65.2	1.5		18			5	45.4	2140	3030			
-305	65.2	66.7	1.5		38			10	17.8	442	2720			
-306	66.7	68.2	1.5		12			<5	68.2	328	2210			
-307	68.2	69.7	1.5		65			<5	174.5	1420	1910			
-308	69.7	71.2	1.5		100			<5	55.0	950	2550			
-309	71.2	72.7	1.5		12			<5	4.4	568	1660			
-310	72.7	74.2	1.5		75			<5	0.6	152	2390			
-311	74.2	75.7	1.5		100			<5	4.6	1050	4800			
-312	75.7	77.2	1.5		30			<5	10.6	606	2850			
-313	52	53.5	1.5		100			<5	0.4	236	904			
-314	53.5	55	1.5		"			<5	<0.2	24	206			
-315	55	56.5	1.5		90			<5	<0.2	14	152			
-316	83.5	85	1.5		80			<5	1.6	114	736			
-317	85	86.5	1.5		30			<5	1.6	348	1360			
-318	86.5	88	1.5		60			15	0.4	274	1710			
-319	88	89.5	1.5		15			<5	<0.2	146	734			
-320	89.5	91	1.5		15			<5	0.2	230	1730			
-321	91	92.5	1.5		50			<5	1.0	204	684			

INDATA RESOURCES LTD.

HOLE NO. W95-05

DRILLING CO FALCON	LOCATION SKETCH	DEPTH	TESTS DIP ANGLE	AZIMUTH	DATE STARTED: JAN. 24, 1995	PROJECT:
	N	COLLAR	-45	180	DATE COMPLETED: JAN 28, 1995	N.T.S.:
					COLLAR ELEV.: 932	LOCATION:
					NORTHING: 11230	
					EASTING: 15125	
					AZIMUTH: 180	
					DEPTH: 120.4	DATE LOGGED: JAN 30
HOLE TYPE					CORE SIZE:	LOGGED BY: C. J. CAMPBELL

INTERVAL FROM	INTERVAL TO	ROCK TYPE (composition, colour, texture, grain size)	ALTERATION	MINERALIZATION	Frlm	STRUCTURE (fractures, faults, folding, bedding, etc.)	REMARKS Mineralization, type, age relations
3.7	16	Cored till - Brn rusty - cased to 70 m - 10 m casing left in hole					
	18	Blk f.g. volc. - ground as pebbles					
18	22	As above - but better recovery					
22	35	"Polymictic" agglomerate	minor Cb v's			Gouge at 26.5 m	
35	39.5	Grey-green gouge	Clay - chlorite ?	minor py ?		Sampled at 1.5 m intervals	
39.5	44.5	Red porphyry ?? ⇒ fragmented	Str. Hematite				
44.5	62.2	Hb Porphyry	Cb v's at 47m & 46 m				
		Purple ⇒ Red volc. nearer vein at 62.2					
62.2	77.2	a.v's breccia Py -	Chlorite - clay	Galena - Sphalerite			
		Galena Sphalerite					
52	53.5	Chlorite rich blk alt. rock				Sampled	
53.5	55	Qv's + Cb	Py + ?	minor sulphide		"	
55	56.5	Chlorite rich - blk Alt.				some light green gouge - sampled	
77	83.5	Andesitic Porphyry	minor Cb. v's at	80m 30° to	C.A.		
83.5	92.5	Chlorite - Hem gouge	minor Py			Sampled at 1.5 m intervals	
92.5	106.4	Sheared Blk ves. volc.					
106.4	120.4	Red Porphyry	Hem. stained			Fractured minor Cb veinlets	E.O.H.

DRILL HOLE NO W95-05

INDATA RESOURCES LTD.

HOLE NO. W95-04

DRILLING CO FALCON	LOCATION SKETCH	DEPTH	TESTS DIP ANGLE	AZIMUTH	DATE STARTED: JAN 22, 1995	PROJECT: WIT
	- N -	COLLAR	-45°	180°	DATE COMPLETED: JAN 24, 1995	N.T.S.:
		39			COLLAR ELEV.: 945	LOCATION:
					NORTHING: 11300	
					EASTING: 15025	
					AZIMUTH: 180	
					DEPTH: 120.4	DATE LOGGED: JAN 24, 1995
HOLE TYPE					CORE SIZE:	LOGGED BY: C. J. CAMPBELL

INTERVAL FROM	INTERVAL TO	ROCK TYPE (composition, colour, texture, grain size)	ALTERATION	MINERALIZATION	Fr/m	STRUCTURE (fractures, faults, folding, bedding, etc.)	REMARKS Mineralization, type, age relations
0	9.1 m	Cased					
9.1	10.5	Boulders					
10.5	49	Polymictic agglomerate?	Fresh				
					27.3	Cb v's 10cm breccia minor Cpy v's @ 45° C.A.	
						Fragments angular 20cm to v. fine 20% rd/br feldspar	
						porph. - 20% rd. k-spar altered fragments generally	
						2 cm, rd and white chert fragments in f.g.	
						gry-grn matrix	
					39.5-40	Intense Cb - sheared zone (Hematite)	
					45-49	Intense Cb - green sheared zone - no sulphides	
49	57	Fresh vesicular Andesite	Cb in vesiculars			highly magnetic	
57	62.7	"Poly Agglomerate"	Chlorite - grn gouge	minor py		not magnetic	
62.7	67	"Fresh" vesicular Andesite	minor shearing				
67	73	"Poly Agglomerate"				Gouge at 72.→72.5	
73	95	Vesicular Basalt? (Andesite)	Green & white amygdule filling			Green looks like epidote!	
95	110	" "	Fresh			magnetic	
110	111	Poly Agglomerate					
116	120.5	vesicular Basalt	Fresh			magnetic E.O.H.	

DRILL HOLE NO W95-04

INDATA RESOURCES LTD. **DRILL LOG** **sample data**

SAMPLE					CORE RECOVERY		VISUAL ESTIMATES (% ORE MINERALS)	ASSAY RESULTS						
NUMBER	FROM	TO	TOTAL METRES	M.S.	%	AMT LOST		Au (ppb)	Ag (ppm)	Pb (ppm)	Zn (ppm)			
W95-224	9.2	10.7	1.5		42			20	.6	1060	1065			
-225	13.4	14.9	1.5		89			20	.2	82	1040			
-226	14.9	16.4	1.5		100			<5	<.2	14	138			
-227	16.4	17.9	1.5		"			<5	<.2	20	220			
-228	17.9	19.4	1.5		"			<5	<.2	20	380			
-229	19.4	20.9	1.5		97			<5	<.2	14	206			
-230	20.9	21.4	0.5		200			<5	<.2	8	192			
-231	21.4	22.9	1.5		100			<5	<.2	8	130			
-232	22.9	24.4	1.5		"			<5	1.4	10	126			
-233	45.5	45.8	0.3		"			<5	8.2	832	2100			
-234	47	48.5	1.5		"			<5	4.6	176	460			
-235	48.5	50	1.5		"			<5	12.8	176	638			
-236	50	51	1		150			<5	16.8	388	1125			
-237	68	69.5	1.5		100			<5	7.0	228	1270			
-238	72.3	72.5	0.2		"			<5	27.6	3240	8230			
-239	77.5	79	1.5		"			<5	1.2	52	320			
-240	79	80.5	1.5		"			<5	0.6	40	264			
-241	80.5	82	1.5		"			<5	<0.2	28	304			

DRILL HOLE NO. W95-03

INDATA RESOURCES LTD. **DRILL LOG** sample data

SAMPLE					CORE RECOVERY		VISUAL ESTIMATES (% ORE MINERALS)	ASSAY RESULTS						
NUMBER	FROM	TO	TOTAL METRES	M.S.	%	AMT. LOST		Au (ppb)	Ag (ppm)	Pb (ppm)	Zn (ppm)	Pb %	Zn %	
W-95-200	88	89	1					<5	3.0	270	1050			
-201	89	90	1					<5	4.6	112	728			
-202	90	91	1					<5	2.6	214	1010			
-203	91	92	1					5	3.4	650	3750			
-204	92	93	1					15	7.2	642	5830			
-205	93	94	1					25	11.4	2030	8980			
-206	99	100	1					<5	<0.2	36	220			
-207	100	101	1		50			<5	2.2	342	1255			
-208	101	102	1		32			<5	3.6	318	1570			
-209	102	103	1		38			10	5.6	240	2900			
-210	103	105	2		10			15	5.4	1540	2960			
-211	105	106	1		70			80	41.4	>10 000	>10 000	1.27	1.6	
-212	106	107	1					95	9.6	1865	>10 000			
-214	107	108	1					50	3.2	1110	4140	.73	2.05	
-215	108	109	1					105	2.6	412	1000			
-216	109	110	1					345	2.6	490	1220			
-217	110	111	1					100	2.2	90	220			
-218	111	112	1					165	2.8	374	744			
-219	112	113	1					350	2.2	388	2120			
-220	113	114	1					265	1.8	280	592			
-221	114	115	1					295	1.8	700	1830			
-222	115	116	1					400	4.2	1135	1690			
-223	116	117	1					280	1.6	880	1330			

INDATA RESOURCES LTD.

HOLE NO. W95-03

INTERVAL FROM	INTERVAL TO	ROCK TYPE (composition, colour, texture, grain size)	ALTERATION	MINERALIZATION	Fr/m	STRUCTURE (Fractures, faults, folding, bedding, etc.)	Mineralization, type, age, relations
71.6	72.3	-				15 cm Q-Cb zone minor py.	
72.6	78.0	Lt. grey volc. Fspar porphry	Fresher	minor pyrite			
78	87	Lt grey volc. Fspar	Hematite at	85.6 - 86 m	77.5-79	Sulphide py Cb alteration Q v's	
					79-80.5	Frac. green volcanics py	
					80.5-82	hematite stained Calcedonic Q v's	
87	94	Sheared altered volc.			88-89	green alt. volc. + py	
					89-90	" "	
					90-91	" "	
					91-92	20 cm Qtz-Cb-Ba in green sheared volc.	
					92-93	Qtz Ba -py (5%) - t.g. grey sulphides	
					93-94	" " "	
94	99	Lt grey Fspar	Cb-			Cb vs @ 97 m	
			Chl-Cb	Py ⇒ 5%	99-100	alt. sheared volc.	
100	105	Q v's + Cb + Ba? grey sulphides					
105			Clay + Chlorite?		105-106	Green sheared zone + py.	
			"		106-107	"	
			"		107-108	"	
			"		108-109	"	
			"		109-110	"	
			"		110-111	"	
			"		111-117	As above sampled at 1m interval H.S. @ 110 m	
117	120.5	Red alt. volcanics	Hematite	minor Py	⇒	fresher andesite	
	121.9	EOH					

DRILL HOLE NO W95-03

INDATA RESOURCES LTD.

HOLE NO. W95-03

DRILLING CO. FALCON	LOCATION SKETCH	DEPTH	TESTS DIP ANGLE	AZIMUTH	DATE STARTED: JAN 19, 1995	PROJECT: WIT
	N	COLLAR	-45°	360°	DATE COMPLETED: JAN 21, 1995	N.T.S.:
					COLLAR ELEV.: 930	LOCATION:
					NORTHING: 11 112	
					EASTING: 15025	
					AZIMUTH: 360°	
					DEPTH: 121.9	DATE LOGGED:
HOLE TYPE					CORE SIZE:	LOGGED BY: C.J. CAMPBELL

INTERVAL FROM	INTERVAL TO	ROCK TYPE (composition, colour, texture, grain size)	ALTERATION	MINERALIZATION	F/m	STRUCTURE (fractures, faults, folding, bedding, etc.)	REMARKS Mineralization, type, age relations
0	3	Casing in till					
3	5	till plus volc. boulders					
5	7	Red cherty agglomerate	Hematite	minor py		Badly fractured and weathered	
7	9.3	Blk · Kspar (white)?	(basaltic) (Could be BP's "syenite" dike)			minor Carbonate veinlet's 10° to CA	
9.3	10.7	Red porph - Qtz flooding	Hematite	Py grey sulphides	v.f.g.	only .6 m of core sampled	
10.7	11.3	Blk gouge and ground pebbles				.1 m recovered	
11.3	12.8	No core recovered					
12.8	13.4	Red hem. altered pebbles	Hematite			.2m pebbles of red porphry then gouge	
13.4	14.9	Gry · grn gouge	Clay + Chlorite?				
14.9	26	Rd. Brn gouge - Some more competent sections Cb. v's - minor py - grey sulphides					
26	35.5	as above hematite alt.	Hematite			very fractured ⇒ gouge	
35.5	47	Cb altered + Grey - Blk volcanics - fragmentals		Sheared slickensides		‖ to C.A. striae at 90° to 60° to C.A.	
						Kspar - grey dike 35.6 – 36.2 m	
47	51	Crushed zone - silicified plus	vtg. sulphides				
51	62	Fragmentals grey to red near	sheared sections - breccia zone at			54.5 to 55 → bleached with Hem. near sheers	
						Cb v's @ 58.5 m.	
62	65	L. gry - volc. - pink - white vesicules	no sulphide				
65	71.6	Rd. alteration of fragmental hematite		py.	68-69.5	more brecciated plus sulphides	

DRILL HOLE NO. W95-03

INDATA RESOURCES LTD. **DRILL LOG** **sample data**

SAMPLE					CORE RECOVERY		VISUAL ESTIMATES (% ORE MINERALS)	ASSAY RESULTS						
NUMBER	FROM	TO	TOTAL METRES	M.S.	%	AMT LOST		Au (ppb)	Ag (ppm)	Pb (ppm)	Zn (ppm)	Pb %	Zn %	Ba %
W95-111A	111	112	1					120	5.6	414	1220			
-112A	112	113	1					150	4.4	4090	5100			
-113A	113	114	1					195	2.4	2770	5480			
-114	114	115	1					70	1.6	716	3920			
-115	115	116	1					200	2.8	1400	>10 000		3.64	0.7
-116	116	117	1		-W95-162-			405	12.0	9820	>10 000	1.03	3.47	11.9
-117	117	118	1					55	3.8	1305	6970			
-118	118	119	1					<5	<.2	24	364			
-119	119	120	1					<5	<.2	28	190			
-120	120	121	1					25	2.2	296	1750			
-121	121	122	1					25	2.2	968	2760			
-122	122	123	1					30	2.4	4410	9300			
-123	123	124	1					10	1.4	706	2010			
-124	124	125	1					5	1.4	946	2360			
-125	125	126	1					40	3.4	1205	5360			
-126	126	127	1					15	2.0	710	3720			
-127	127	128	1					5	1.4	760	2650			
-128	128	129	1					10	1.6	748	2610			
-129	129	130	1					20	2.2	530	2570			
-130	130	131	1					30	2.4	726	2380			
-131	131	131.7	0.7					40	4.2	594	2300			
-131.7	131.7	132.5	0.8	Sent out	as	W95-161		60	4.6	5120	>10 000	0.56	2.29	12.4
-132.5	132.5	133.5	1					<5	.6	90	356			
-133.5	133.5	134.5	1					<5	3.4	404	1285			
-134.5	134.5	135.5	1					<5	3.6	476	1530			
-135.5	135.5	136	0.5					<5	2.4	620	2500			

INDATA RESOURCES LTD. **DRILL LOG** **sample data**

SAMPLE					CORE RECOVERY		VISUAL ESTIMATES (% ORE MINERALS)	ASSAY RESULTS						
NUMBER	FROM	TO	TOTAL METRES	M.S.	%	AMT LOST		Au(PPB)	Ag(PPM)	Pb(PPM)	Zn(PPM)	Pb %	Zn %	Ba %
W95-150	100	101	1		100			145	1.2	54	164			
-151	101	102	1		"			170	5.0	326	568			
-152	102	103	1		"			440	4.0	928	1585			
-153	103	104	1		"		-25 cm H.S.	700	6.0	2790	6760			
-154	104	105	1		73			115	4.6	556	1075			
-155	105	106	1		100			100	4.6	284	920			
-156	106	107	1		"			490	51.8	1685	3200			
-157	107	108	1		"			455	84.8	1620	2600			
-158	108	109	1		"		-22 cm H.S.	85	7.2	346	1325			
-159	109	110	1		80			170	7.8	1850	3800			
-160	110	111	1					205	10.2	554	2850			
-161	131.7	132.5	.8					60	4.6	5120	>10,000	.56	2.29	12.4
-162	116	117	1					405	12.0	9820	>10,000	1.03	3.47	11.9
-163	99.2	100	.8					25	0.6	10	124			
-164	177	178	1		100%			<5	<0.2	4	120			
-165	180	181			85%			<5	<0.2	20	192			

DRILL HOLE NO. W95-02

INDATA RESOURCES LTD.

HOLE NO. W95-02

INTERVAL FROM	INTERVAL TO	ROCK TYPE (composition, colour, texture, grain size)	ALTERATION	MINERALIZATION	Frm	STRUCTURE (Fractures, faults, folding, bedding, etc.)	Mineralization, type, age, relations
132.5	133.8	Gouge				5% Py	
133.8	136.0	Sheared volcanic - grey-green					
136.0	136.7	F-spar Porphyry (orange) dike					
136.7	143.0	Hb F-spar porphyry	Fresh - hard			Shearing @ 144m dike as above 50cm @ 140 & 143	
143.0	152.0	Red to Grey volcanics					
152.0	161.5	Grey volcanics - increased shearing	Fresh			minor Py - Shearing increases with depth	
161.5	167.0	→ Red Hematite alt. volcanics				" "	
167.0	173.2	" "				Cb v's at 168 m - minor breccia	
173.2	177.0	green andesite porphyry	Epidote (f.g.)?			Cbv's at 70° & 45° to CA	
					177-178	Hematite stained breccia zone - minor sulphide CbQ v's	
178.0	180.0	green andesite porphyry				minor hematite on fractures	
					180-181	As 177-178	
181.0	189.0	green hornblende porphyry (Hb)	Epidote			Sheared ⇒ gouge @ 185 m	
189.0	197.0	Hematite stained "Red porphyry"				Stain diminishes to end of hole (Bill's Trout Rock)	
	197.0	EOH					

DRILL HOLE NO W95-02

INDATA RESOURCES LTD.

HOLE NO. W95-02

DRILLING CO.	LOCATION SKETCH	DEPTH	TESTS DIP ANGLE	AZIMUTH			
FALCON	N	COLLAR	-45	180	DATE STARTED: JAN 12, 1995	PROJECT: WIT	
					DATE COMPLETED: JAN 16, 1995	N.T.S.:	
					COLLAR ELEV.: 955	LOCATION:	
					NORTHING: 11262 N		
					EASTING: 14925E		
					AZIMUTH: 180°		
					DEPTH: 197	DATE LOGGED: JAN 19, 1995	
HOLE TYPE					CORE SIZE:	LOGGED BY: C.J. CAMPBELL	

INTERVAL FROM	INTERVAL TO	ROCK TYPE (composition, colour, texture, grain size)	ALTERATION	MINERALIZATION	Fr/m	STRUCTURE (fractures, faults, folding, bedding, etc.)	REMARKS Mineralization, type, age relations
0	3	CASING					
3	15.5	F.G. grey andesite	bleached, Cb	Cb + bx minor Cpy		Fragmental to bx random orientation open space	
						filled by Cb · Cb + malachite ore fracture 45° to C.A. at 10m	
15.5	28	Red and coarse feldspar porphyry	Strong hematite	minor Py		minor late fractures · some fragments to 21m	
28	33	Grey Bleached - some bx				50% Py at 32.5 to 32.7	
33	72	Coarse Red feldspar porphyry	bleaching, hematite			minor brecciation	
72	80	Bleached → Grey + coarser fragments					
80	90.5	Coarse red agglomerate	Hematite			fragments of above red porph.	
90.5	93.0	Bleached equiv. of above + silicification		minor Py at 91.5			
93	99.2	Red ash tuff	Hematite				
99.2		Strongly brecciated andesite	silicified, Cb.	Py.	99.2-100	Sampled Lt. grey 5% Py -	
		" "			100-106	As above sampled @ 1m - 110 - 113.4 Ground Qv's	
116	117	Qtz + Cb - Py HgS? at 116.2m	Qv's		116-117	5% Py - grey sulphides cinnibar?	
117	121	More basic - sheared	Chlorite			2-3% Py - sampled	
121	125	Red Porph?	Hematite			2-3% Py disseminated	
125	126	Sheared volc?	50% Py			Badly fractured and sheared - cemented by Py?	
126	131.7	Grey to Red volc	Hematite	Py		2-3%	
131.7	132.5	Sheared Qv's	Py Qv's		.8m	10-20% Py H.S. bonded Py, Pb Zn - 132.4 meters	

DRILL HOLE NO W95-02

APPENDIX

INDATA RESOURCES LTD. DRILL LOG sample data

SAMPLE					CORE RECOVERY		VISUAL ESTIMATES (% ORE MINERALS)	ASSAY RESULTS						
NUMBER	FROM	TO	TOTAL METRES	M.S.	%	AMT LOST		Au (ppb)	Ag (ppm)	Pb (ppm)	Zn (ppm)	Pb %	Zn %	
W95-101	119	120	1		90			<5	.6	56	218			
-102	120	121	1					<5	.4	42	190			
-103	121	122	1					<5	<.2	12	198			
-104	122	123	1					<5	<.2	2	102			
-105	123	124	1					170	2	206	7500			
-106	124	125	1					390	3.4	290	>10 000		2.25	
-107	125	126	1					345	4.8	394	>10 000		2.30	
-108	126	127	1					515	8.4	498	>10 000		1.58	
-109	127	128	1					715	36.4	1295	>10 000		2.66	
-110	128	129	1					2810	7.6	9150	>10 000	1.11	12.20	
-111	129	130	1					665	11.6	>10 000	>10 000	2.33	7.19	
-112	130	131	1					740	51	>10 000	>10 000	7.58	15.30	
-113	131	131.5	0.5					550	22.6	>10 000	>10 000	4.90	13.50	

INDATA RESOURCES LTD.

HOLE NO W95-01

INTERVAL FROM	INTERVAL TO	ROCK TYPE (composition, colour, texture, grain size)	ALTERATION	MINERALIZATION	Frlm	STRUCTURE (Fractures, faults, folding, bedding, etc.)	Mineralization, type, age, relations
17.3	173.5	-				40 cm. of pink Feldspar dike	
173.5	182	Hb. Andesite	Cbu's			Minor bx and shearing	
					179.5	30 cm. orange Feldspar dike	
185	186	Orange Feldspar dike					
186	192.8	Green to brown fragmental				sheared and altered?	
		E.O.H. - Green hornblende andesite	Chlorite			Carbonate v's at 196 metres	

PAGE 2 OF 2

DRILL HOLE NO W95-01

APPENDIX

INDATA RESOURCES LTD.

HOLE NO. W95-01

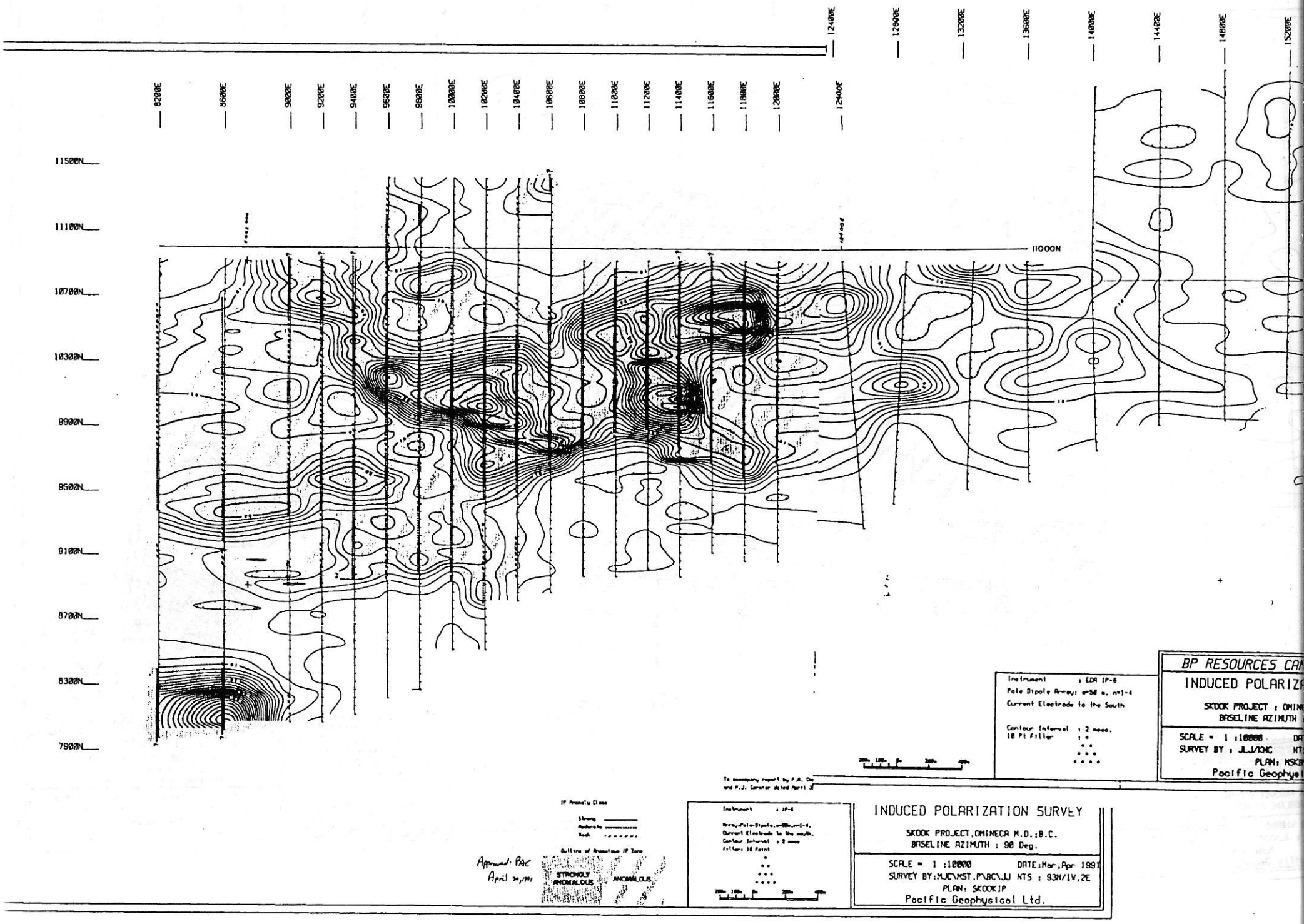
DRILLING CO.	LOCATION SKETCH	DEPTH	TESTS DIP ANGLE	AZIMUTH		
FALCON	N	COLLAR	-45°	180°	DATE STARTED: JAN 12, 1995	PROJECT:
					DATE COMPLETED: JAN 16, 1995	N.T.S.:
					COLLAR ELEV.: 935	LOCATION:
					NORTHING: 11315	
					EASTING: 14775	
					AZIMUTH: 180°	
					DEPTH: 197.8	DATE LOGGED: JAN 20/95
HOLE TYPE					CORE SIZE:	LOGGED BY: C. J. CAMPBELL

INTERVAL FROM	INTERVAL TO	ROCK TYPE (composition, colour, texture, grain size)	ALTERATION	MINERALIZATION	F/m	STRUCTURE (fractures, faults, folding, bedding, etc.)	REMARKS (Mineralization, type, age relations)
0	3	Casing in overburden and andesitic rubble					
3	89	Lt grey andesitic tuff	minor propyletic	Calcite on fractures		Oxidized to 11.9 m Calcite v's @ 10° to C.A.	
						at 4.5 m and 20° to C.A. at 12 m.	
89	90.5	Red to purple ash. tuff	Hematite				
90.5	119.2	Grey hornblende andesite				Somewhat magnetic increasing with depth	
119.2	124.0	Sheared green fragmental	Bleaching	Py + Gn + Sp (1-2% combined)			
124.0	125	Sheared quartz vein		"		50% Recovery	
125	126	Sheared green fragmental	Chlorite	"			
126	127	" " "	"	"			
127	128	Less shearing	"	"			
128	129	"					
129	130	Lighter green	" + Silicified				
130	131	"					
131	131.5	"					
131.5	134.0	Mixed green → Red fragmentals	Hem, Py	Py			
134	157	Red porphyry + fragmentals	Hematite		143.5 & 148 m	Sheared Cb and Quartz veins	
157	173	Hb Porph. Andesite				Some sections of "Red Porph"	

DRILL HOLE NO W95-01

APPENDIX D - Geophysical Maps (I.P.-Resistivity and

Calculated Magnetic Vertical Gradient Maps)



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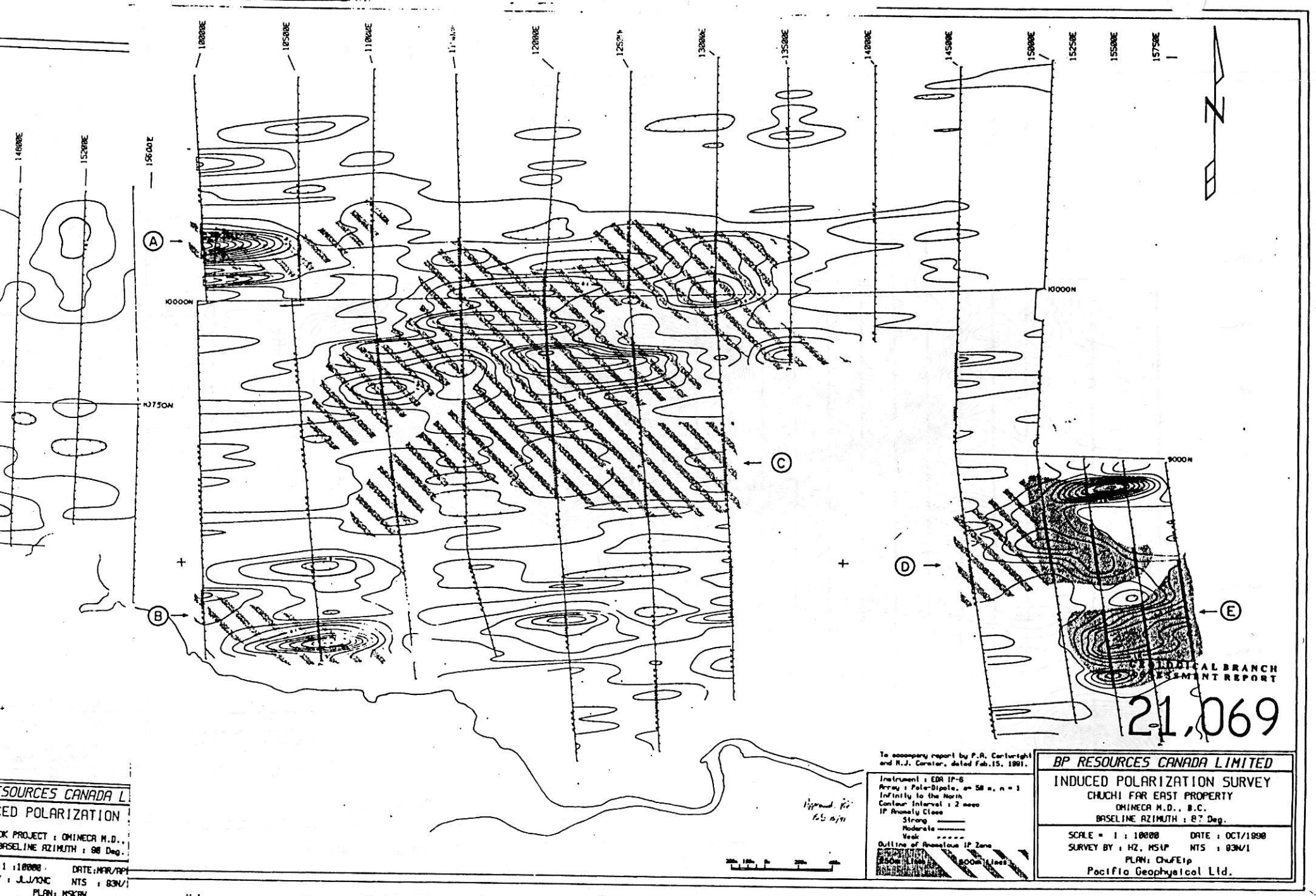
10300N
9900N
9500N
9100N
8700N
8300N
7900N
11000N
Instrument : EDA IP-6
Pole Dipole Array: a=50 m, n=1-4
Current Electrode to the South
Contour Interval : 2 msec.
10 Ft Filter
BP RESOURCES CA
INDUCED POLARIZ
SKOOK PROJECT : OMIN
BASELINE AZIMUTH
SCALE = 1 :10000
SURVEY BY : JLJ/KNC
PLAN: MSK
Pacific Geophys
IP Anomaly Class
Strong
Moderate
Weak
Outline of Anomalous IP Zone
Approved: BAC
April 30, 1991
STRONGLY ANOMALOUS
ANOMALOUS
Instrument : IP-6
Array: Pole-Dipole, a=50m, n=1-4.
Current Electrode to the south.
Contour Interval : 2 msec
Filter: 10 Point
INDUCED POLARIZATION SURVEY
SKOOK PROJECT, OMINECA M.D.; B.C.
BASELINE AZIMUTH : 90 Deg.
SCALE = 1 :10000
DATE: Mar, Apr 1991
SURVEY BY: MJC\MST.P\BC\JJ
NTS : 93N/1W,2E
PLAN: SKOOKIP
Pacific Geophysical Ltd.



SOURCES CANADA L
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BASELINE AZIMUTH : 98 Deg.
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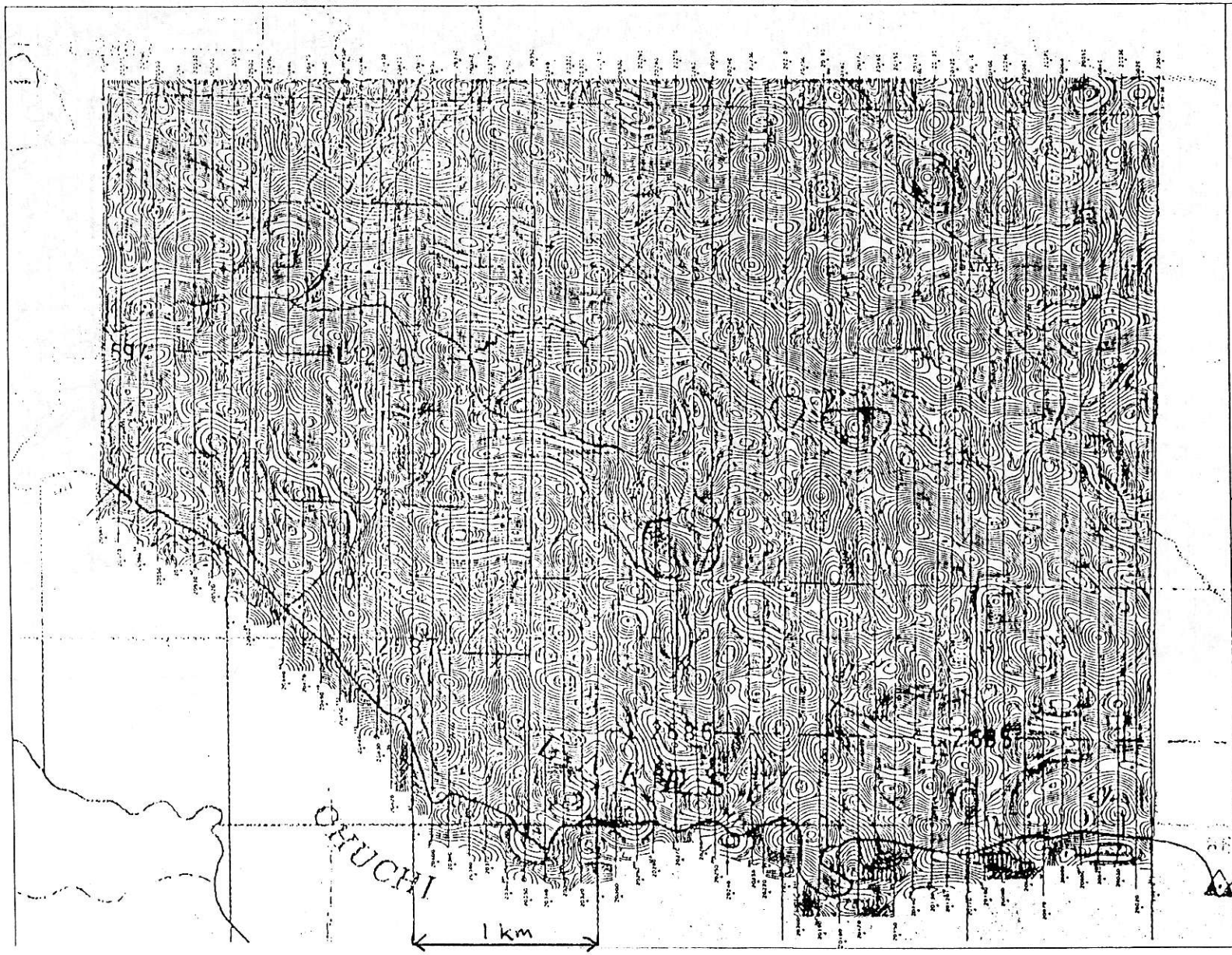
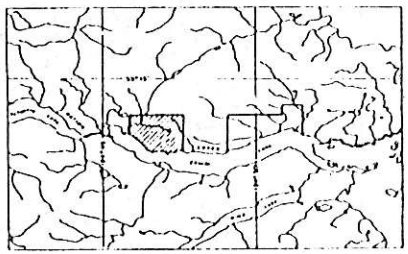
: JLJ/KNC
NTS : 93N/
PLAN: MSKBV
acific Geophysical Ltd.



N

Flight Path

Vertical Gradient



BP RESOURCES CANADA

CALCULATED VERTICAL MAGNETIC GRADIENT

ANOM BLOCK

BRITISH COLUMBIA

[redacted]

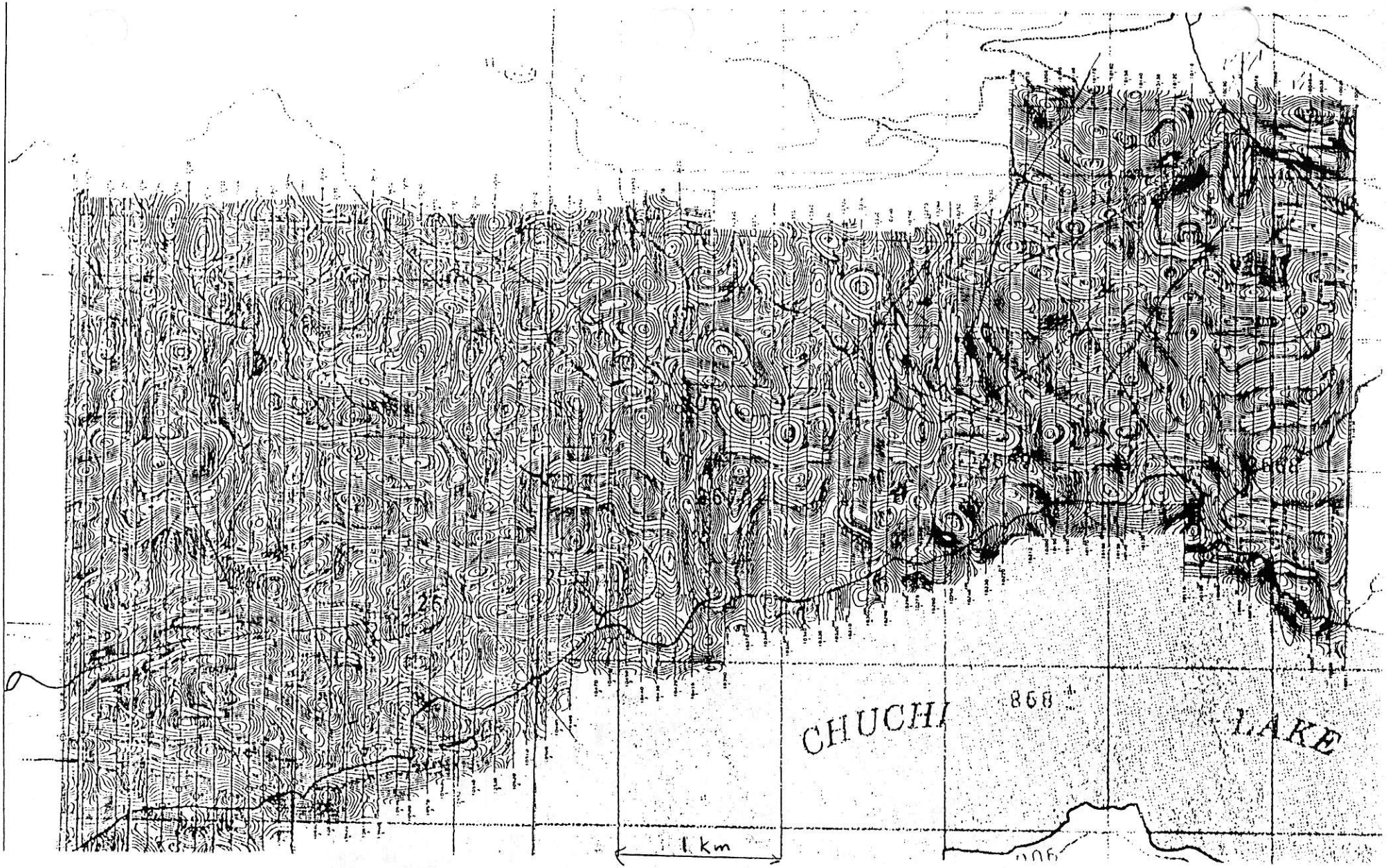
AERODAT LIMITED

DATE: DECEMBER 1990

NTS NO: 93 N

MAP NO: 4

JN085 - 1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LAKE
868
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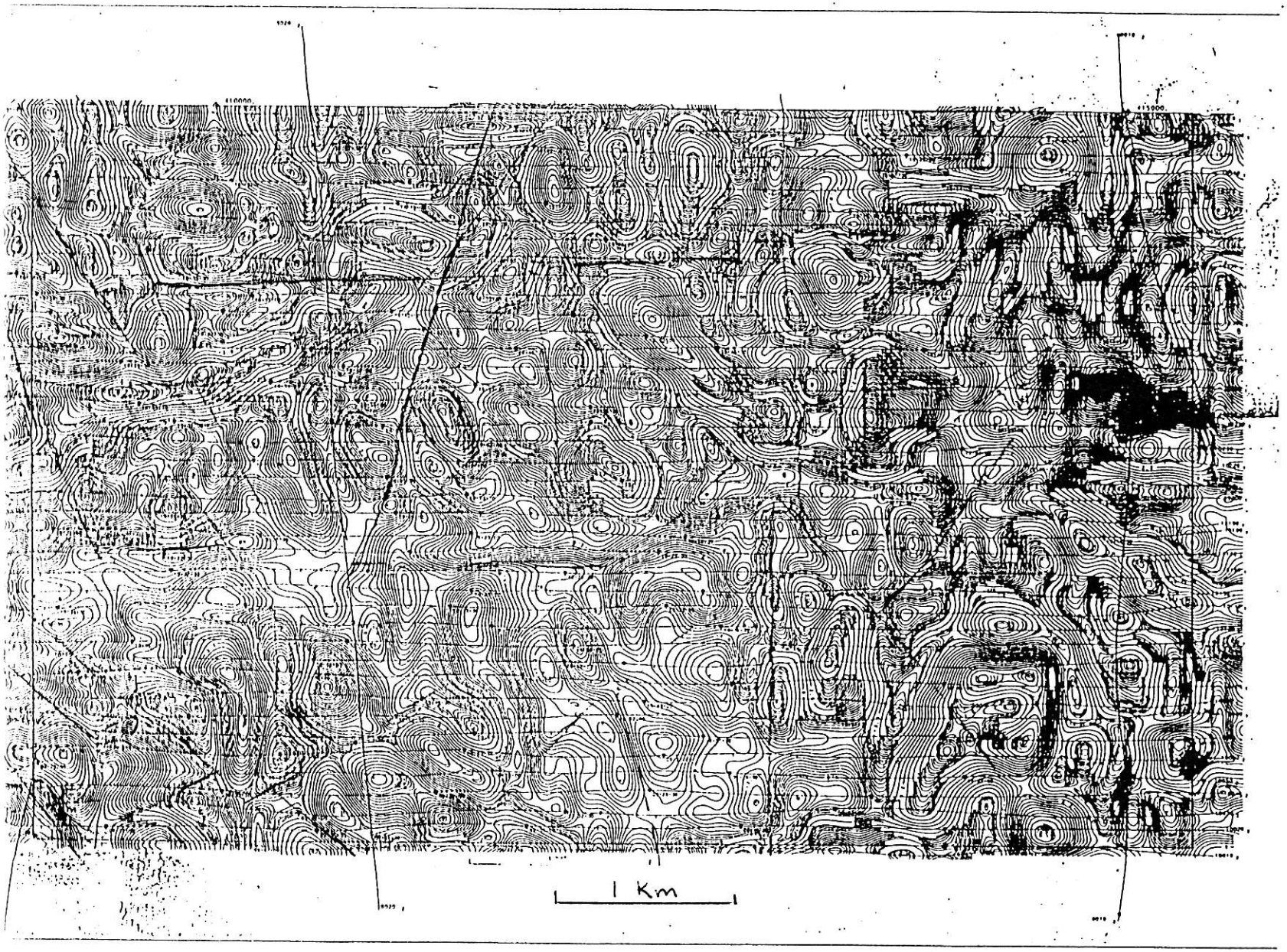
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