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# **CINOLA GOLD PROJECT**

## **STAGE II**

### **WORKSHOP RESPONSE REPORT**

### **APPENDICES**



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## **CITY RESOURCES (CANADA) LIMITED**

**CINOLA GOLD PROJECT**

**STAGE II REVIEW**

**WORKSHOP RESPONSE REPORT**

**APPENDICES**

Submitted by:

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File: 1-098-34.02

LIST OF APPENDICES

- 2.2.1-1 Predicted Seepage Through the Reclaimed Cinola Pit Backfill
- 2.2.3-1 Response to Supplemental Questions About the Geohydrology of the Proposed Cinola Pit
- 3.2.8-1 Summary of Kinetic Test Data Used in the Evaluation of Critical NNP Value for Acid Generation, Cinola Gold Project
- 4.2.2-1 High West Water Balance Spreadsheets
- 4.2.3-1 Baseflows from the Yakoun River Near Port Clements (080A003) Gauge and from Barbie and Florence Creeks
- 4.2.3-2 Linear Regression Plots for Concurrent Baseflow Discharge in the Study Area Creeks and the Yakoun River
- 4.2.6-1 Mine Area: Water Management Plan for Year of Wettest Precipitation
- 6.2.3-1 Commentary from Environment Canada on Mercury/Nutrients
- 7.2.2-1 Ferguson Bay Dock Impacts and Compensation: Hay & Company Response

**APPENDIX 2.2.1-1**  
**PREDICTED SEEPAGE THROUGH THE RECLAIMED**  
**CINOLA PIT BACKFILL**  
**(Page 1 to 50)**

REPORT TO  
CITY RESOURCES LIMITED

ON

PREDICTED SEEPAGE THROUGH THE  
RECLAIMED CINOLA PIT BACKFILL

QUEEN CHARLOTTE ISLANDS  
BRITISH COLUMBIA, CANADA

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Project 1100

May 5, 1989

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May 5, 1989

Steffen Robertson and Kirsten  
1030 West Georgia Street, Suite 801  
Vancouver, British Columbia  
Canada, V6E 2Y3

Attention: Mr. John Gadsby, P.E.

Re: Predicted Flow through the Reclaimed Cinola Pit Backfill

Dear John:

Please find attached my report on the above captioned matter. This report was requested as a result of the meetings with the Provincial and Federal reviewers of this project, which took place in Vancouver on May 5, 1989. The analysis performed is an extension of the work presented in our report on the geohydrology of the project, and evaluates the distribution of flow to the backfilled pit greater detail.

I trust that this report meets your needs at this time. Should you have any questions, please do not hesitate to call.

Respectfully submitted,  
ADRIAN BROWN CONSULTANTS INC



Adrian Brown, P.E., President

Att.

TABLE OF CONTENTS

1.0 INTRODUCTION	1
2.0 ANALYSIS METHOD	2
3.0 ANALYSIS RESULTS	4
3.1 Transverse Section	4
3.2 Longitudinal Section	9
3.3 Overall Results	14

FIGURES

Figure 1 - Site Plan	3
Figure 2 - Transverse Section - Heads (m)	5
Figure 3 - Transverse Section - Seepage through Backfill	6
Figure 4 - Transverse Section - Time for Plug Flow	7
Figure 5 - Transverse Section - Proportion of Plug Flow	8
Figure 6 - Longitudinal Section - Heads	10
Figure 7 - Longitudinal Section - Seepage through Backfill	11
Figure 8 - Longitudinal Section - Time for Plug Flow	12
Figure 9 - Longitudinal Section - Proportion of Plug Flow	13
Figure 10 - Distribution of Seepage Flow Rates through Backfill	15
Figure 11 - Distribution of Times for Plug Flow	16
Figure 12 - Proportions of Plug Flow in Backfill Seepage	17

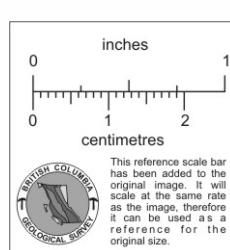
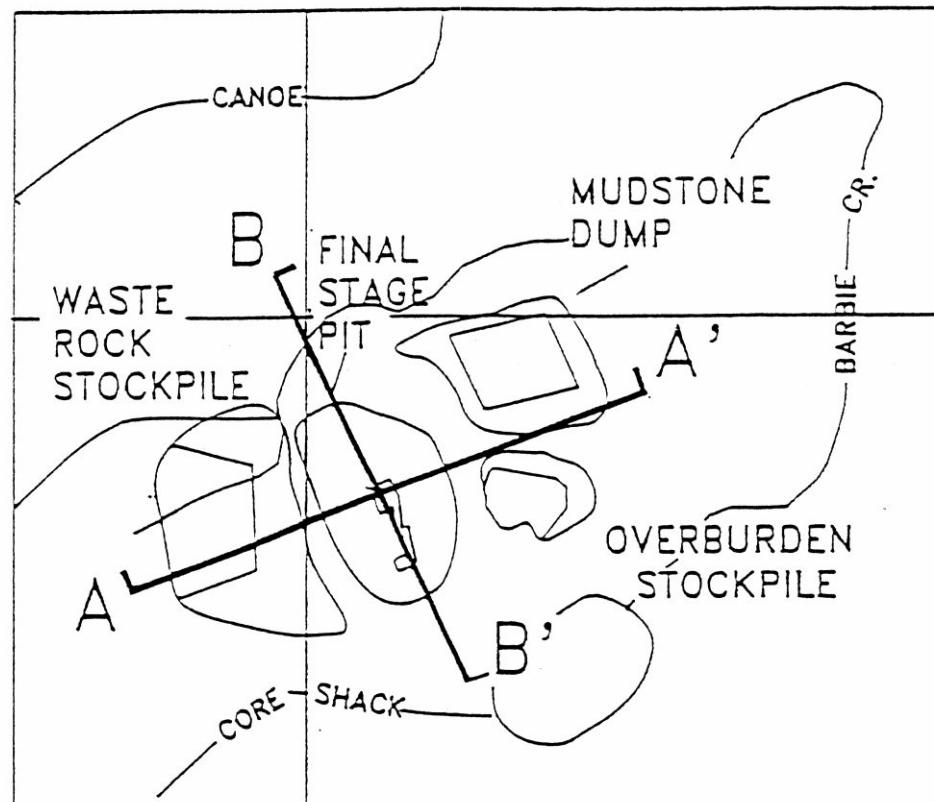
## 1.0 INTRODUCTION

City Resources Limited proposes to develop an open pit gold mine to exploit the Cinola orebody, located in the Queen Charlotte Islands. As some of the waste rock to be mined is potentially acid generating, it is proposed to partially backfill the pit with this rock, and to resaturate this material to prevent acid generation. This report presents a detailed evaluation of the seepage of groundwater through the backfill material after the reclamation of the mine.

## 2.0 ANALYSIS METHOD

The analysis involved the evaluation of the flow conditions through the backfill for both a transverse and a longitudinal section through the pit (Figure 1). The approach used is to refine the analyses performed in the geohydrology report ("The Geohydrology of the Cinola Gold Project", ABC, March, 1989). The flow heads were computed, which allowed a computed time for plug flow at different locations over the reclaimed surface. This plug flow time was used to establish the total plug flow rates versus time for each condition, and then to compute the proportion of plug flow in the total seepage that passes through the backfill as a function of time. The plug flow is expected to remove the bulk of the available chemical mass that may exist in the backfill material, so this proportion indicates the extent to which the quality of this seepage has been modified by contact with the backfill.

The two sets of analysis were then used to estimate an effective overall condition. The detailed information on those analyses is attached as a data appendix; a discussion of the results is provided below.



0            1            2  
SCALE IN KM.

Figure 1 - Site Plan

### 3.0 ANALYSIS RESULTS

#### 3.1 Transverse Section

This analysis evaluated an east-west section through the deepest part of the pit. The results are as follows:

1. Heads. Heads are shown on Figure 2. The flow through the backfill material is in this section all upwards through the backfill.
2. Rate of flow per unit area. The rate of flow per unit area of the reclaimed surface of the pit was computed, and is illustrated in Figure 3. As expected the flow rate around the edges of the reclaimed area are much higher than the rates in the center of the pit.
3. Time taken for backfill to flush. The time taken for plug flow (that is the displacement of the first pore volume of porewater from the backfill material) was computed using an assumed porosity of 30%, and the results are presented in Figure 4. This shows that the edges of the reclaimed pit area flush quickly (in less than a year), because they are subject to high gradients and the depth of backfill material is small. The center of the pit takes up to 160 years to flush.
4. Estimated plug flow seepage. The estimated proportion of plug flow in the total seepage that passes through the backfill (that is the proportion of "first flush" water in of the backfill seepage) is plotted for this section on Figure 5. This shows that the plug flow drops to 75% of the total seepage in the first 2 years, to 50% of the total seepage in the first 10 years, and ends after 160 years.

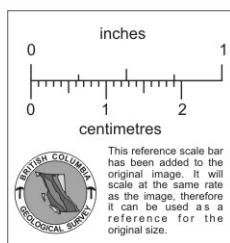
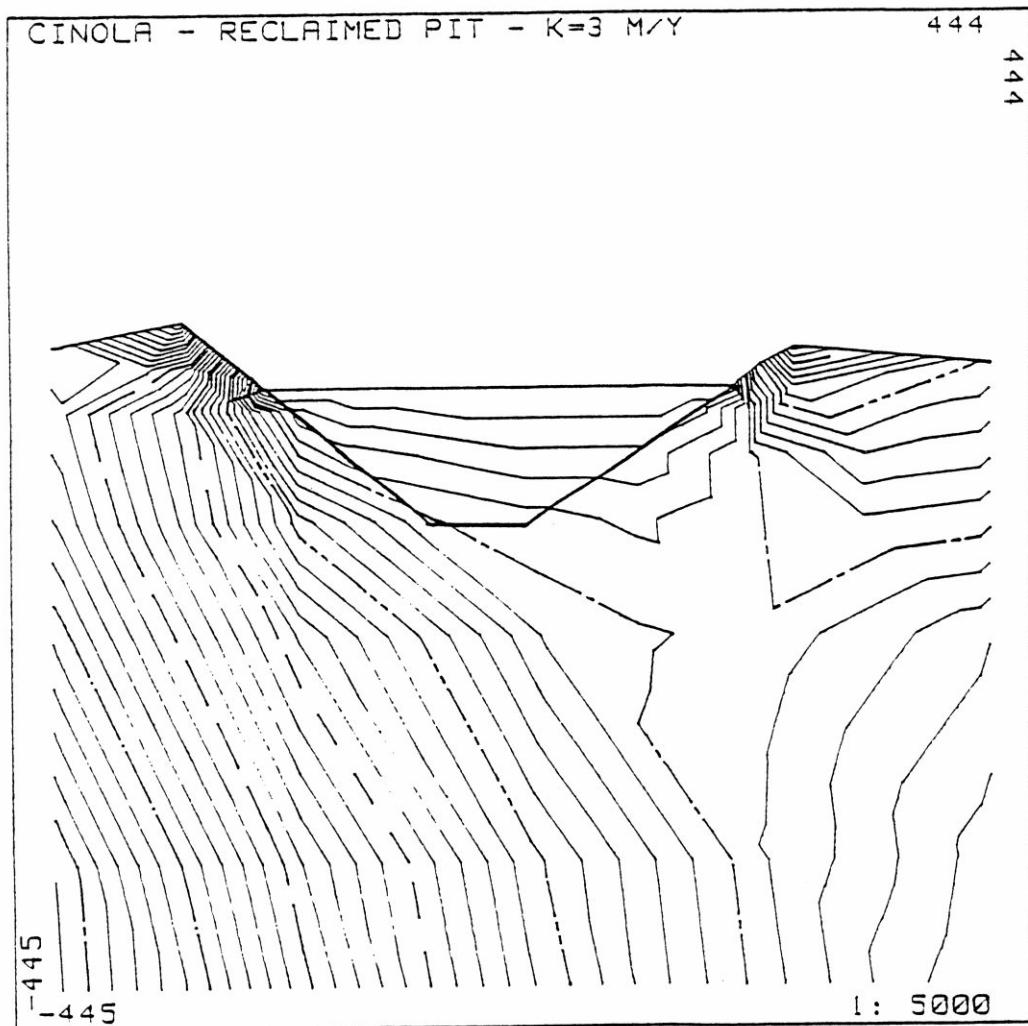


Figure 2 - Transverse Section - Heads (m)

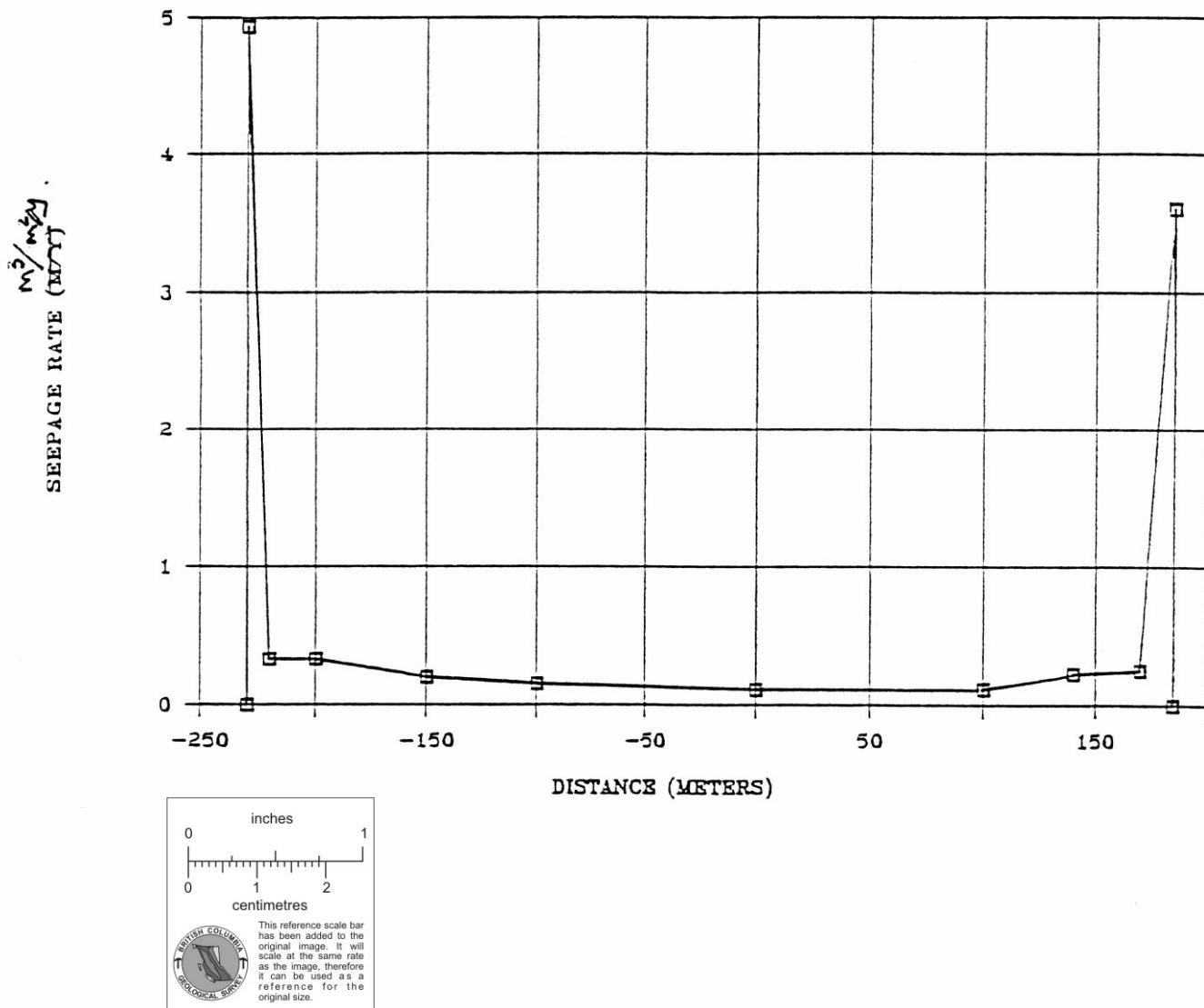


Figure 3 - Transverse Section - Seepage through Backfill ( $\text{m}^3/\text{m}^2/\text{y}$ )

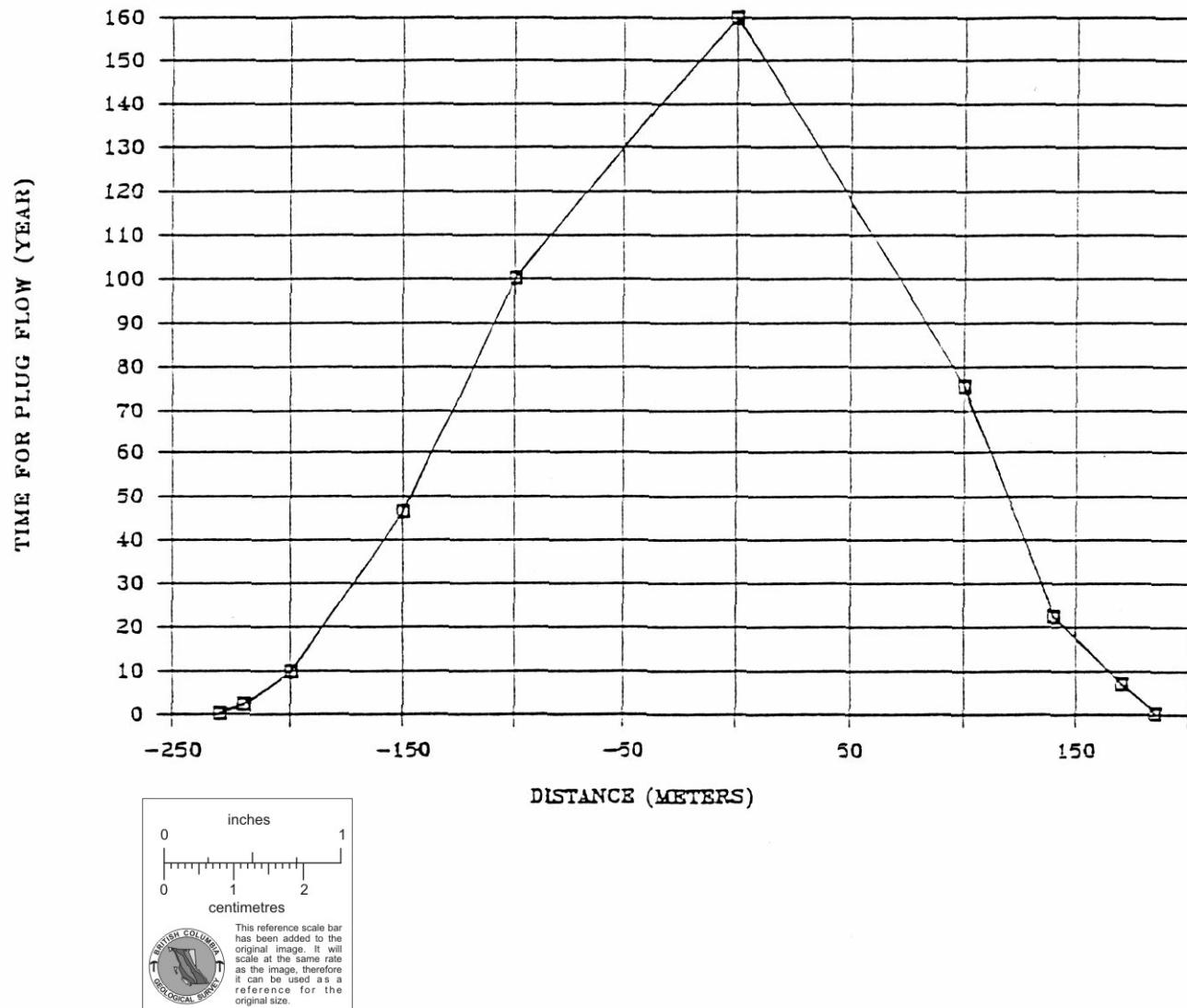


Figure 4 - Transverse Section - Time for Plug Flow (y)

Figure 5 - Transverse Section - Proportion of Plug Flow (%)

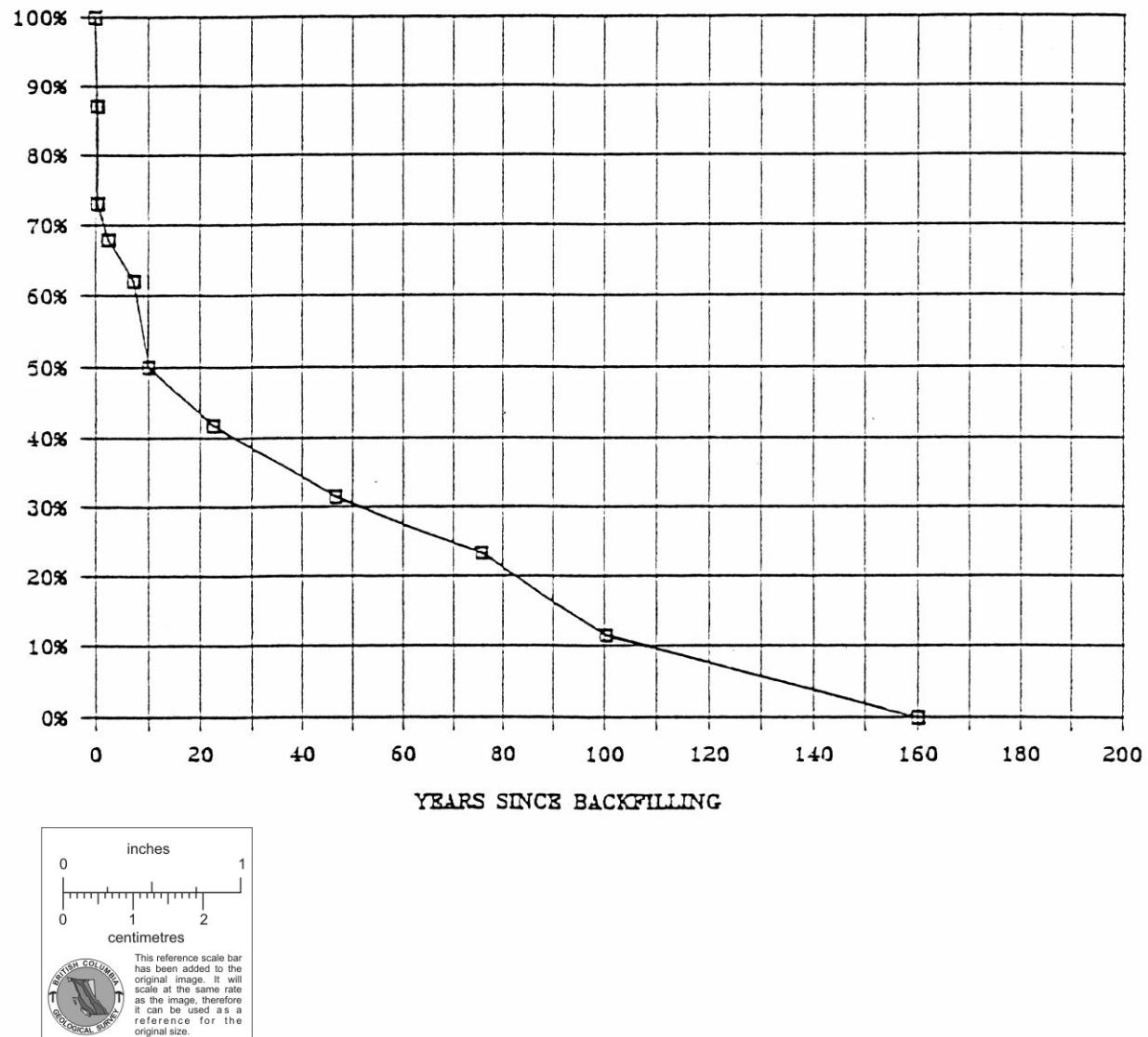


Figure 5 - Transverse Section - Proportion of Plug Flow (%)

### 3.2 Longitudinal Section

A similar analysis was performed using the longitudinal section presented in the geohydrology report (ABC, 1989). This analysis evaluated a north-south section through the deepest part of the pit. The results are as follows:

1. Heads. Heads are shown on Figure 6. The flow through the backfill material is upwards to the north of the section, and downwards to the south.
2. Rate of flow per unit area. The rate of flow per unit area of the reclaimed surface is illustrated in Figure 7. As before, the flow rate around the edges of the reclaimed area are much higher than the rates in the center of the pit. Also, in this section, the flow rate is downward to the south, and upward to the north.
3. Time taken for backfill to flush. The time taken for plug flow was computed using an assumed porosity of 30%, and the results are presented in Figure 8. This again shows that the edges of the reclaimed pit area flush quickly, while the stagnation point in the center south of the pit takes up to 400 years to flush.
4. Estimated plug flow seepage. The estimated proportion of the seepage through the backfill that is plug flow (that is comes from the "first flush" of the backfill) is plotted for this section on Figure 9. This shows that the plug flow drops somewhat less quickly than for the transverse section, but that the upward plug flow seepage reduces to 50% of the total seepage in the first 50 years. Note that the downward plug flow percentages drop off more quickly.

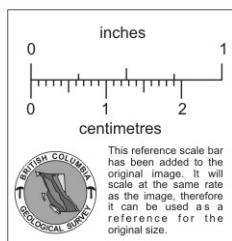
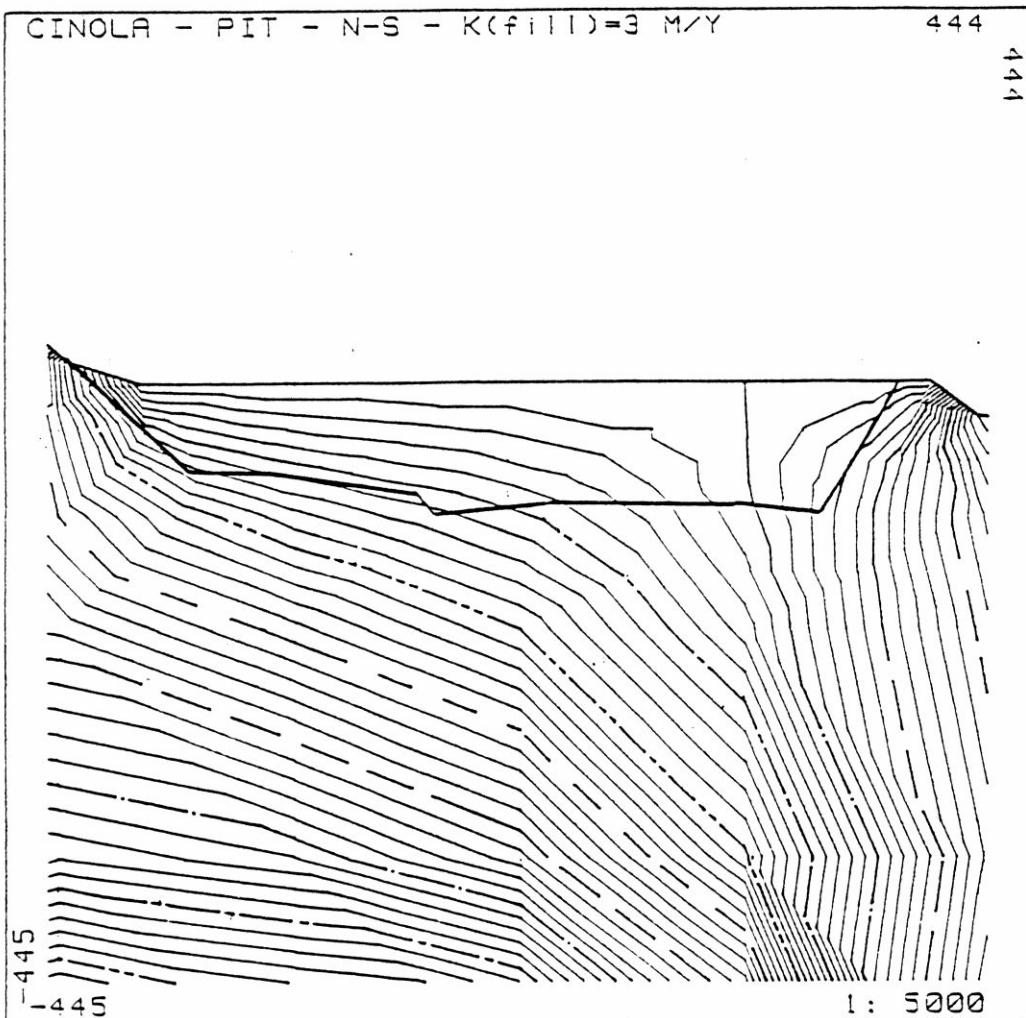


Figure 6 - Longitudinal Section - Heads (m)

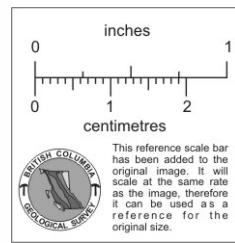
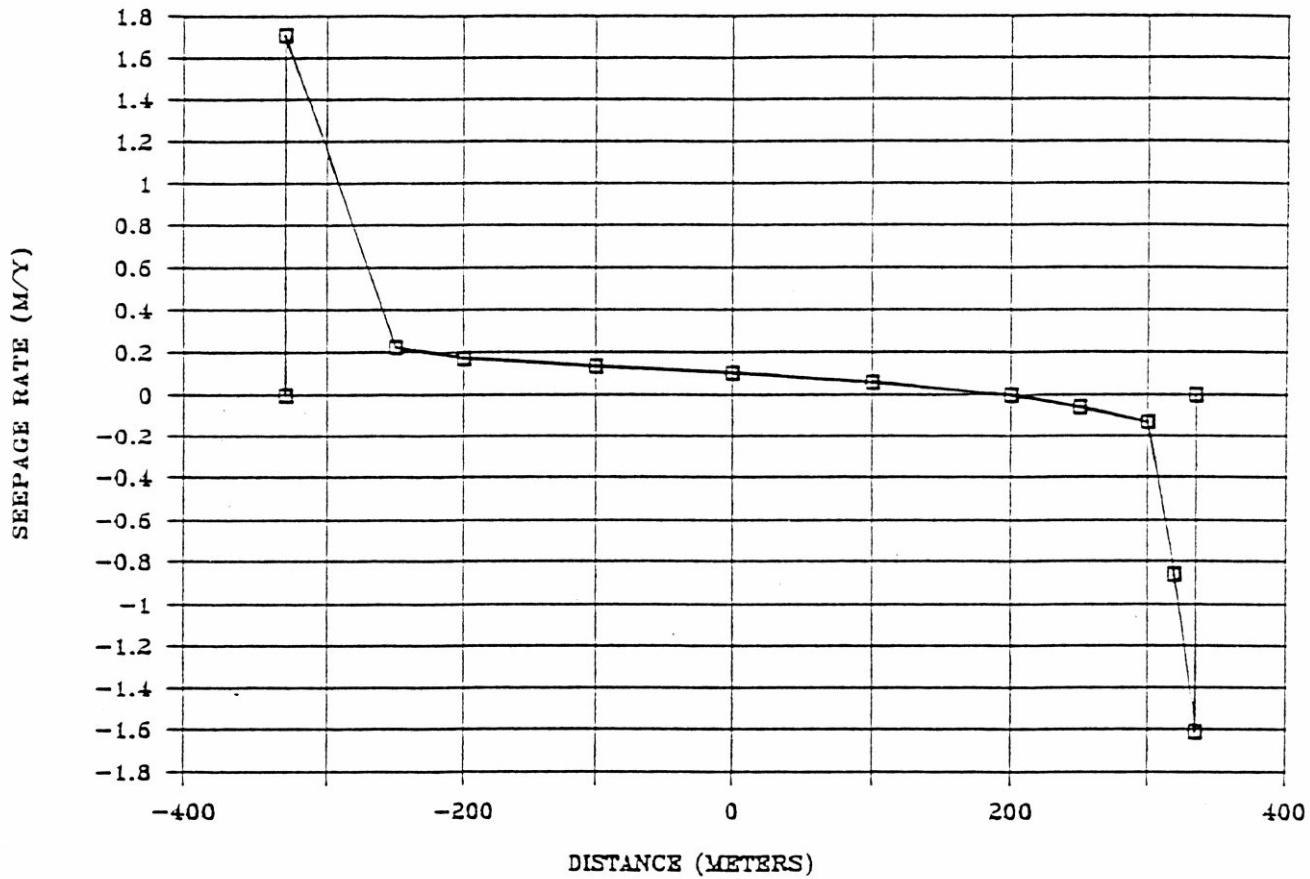


Figure 7 - Longitudinal Section - Seepage through Backfill ( $\text{m}^3/\text{m}^2/\text{y}$ )

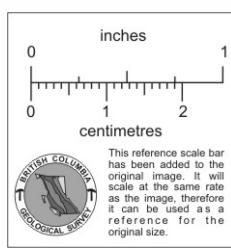
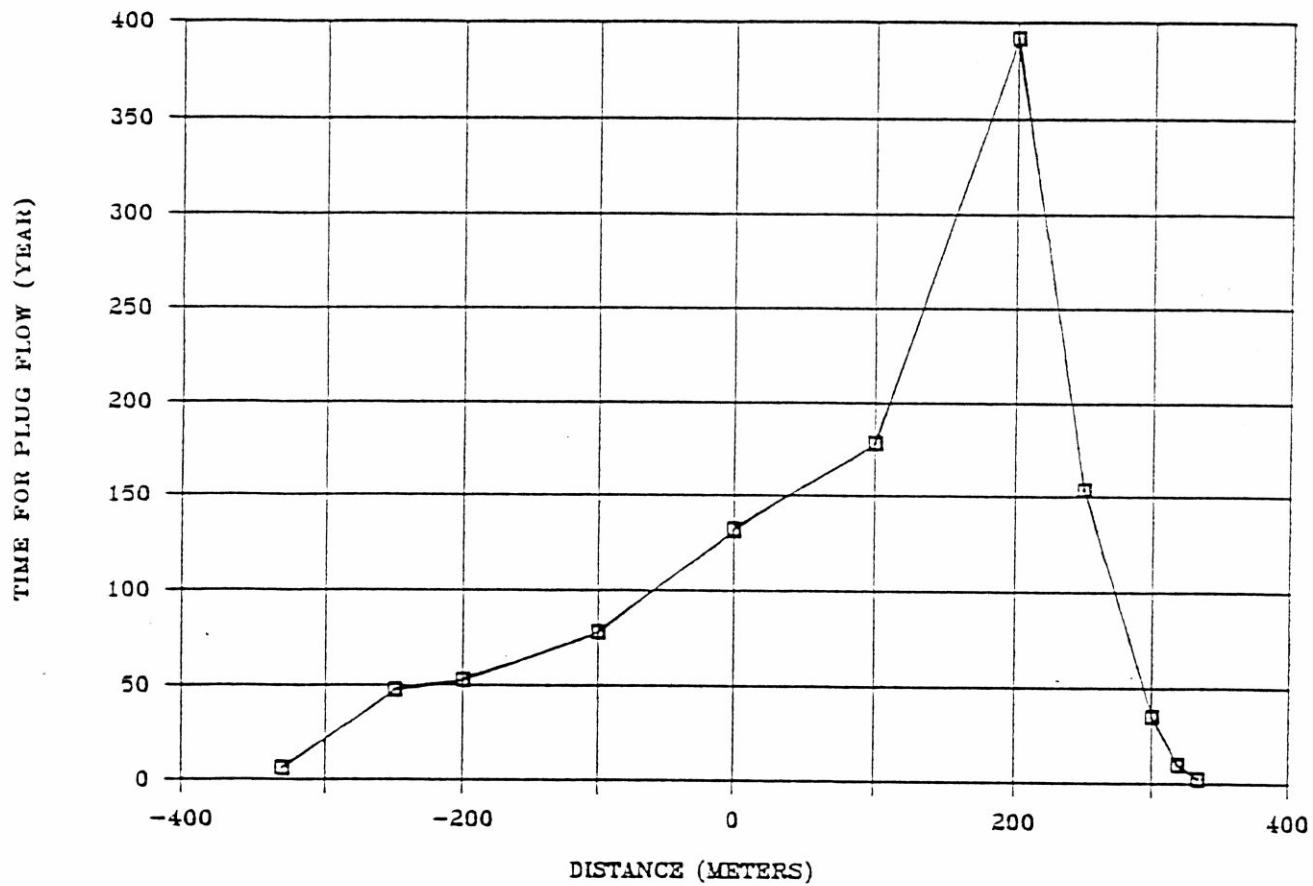


Figure 8 - Longitudinal Section - Time for Plug Flow (y)

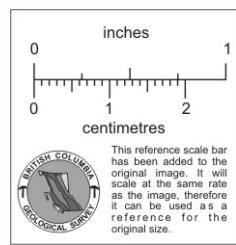
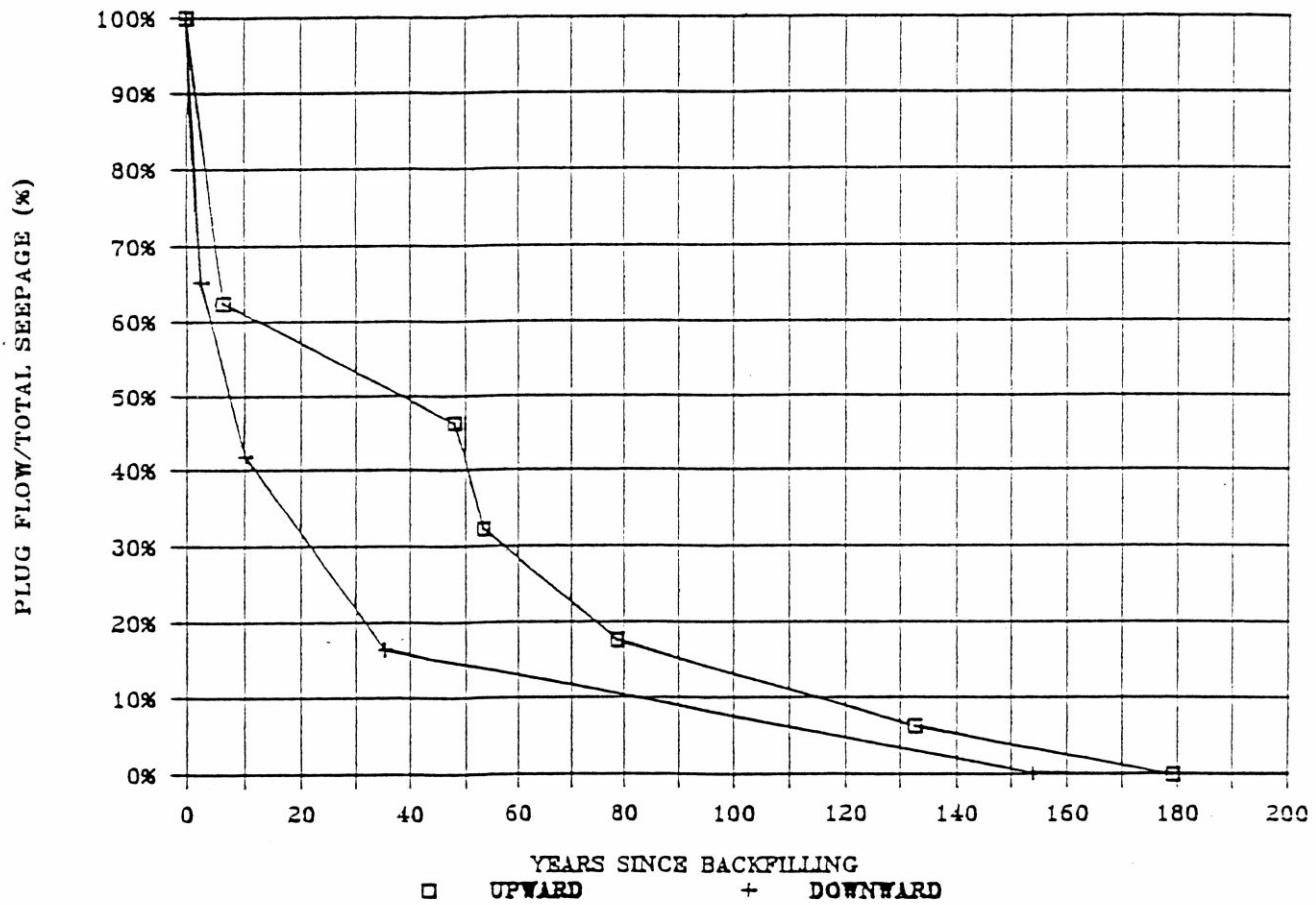


Figure 9 - Longitudinal Section - Proportion of Plug Flow (%)

### 3.3 Overall Results

The above results are taken for sections around the perimeter. An estimate of the combined effect of the seepage system can be obtained by combining these analyses, recognizing that the transverse section situation holds over perhaps a few hundred meters of the pit, and that the longitudinal section situation holds over a narrower portion of the pit. This is shown in two sketch plans of the reclaimed pit:

1. Rate of flow to the pit. Figure 10 shows the rate of flow to the reclaimed pit floor. The "high" rate of flow is greater than 0.3 cubic meters per square meter per year (and averages about 1 cubic meter per square meter per year), the "moderate" rate of flow is 0.1 to 0.3 cubic meters per square meter per year, and the "low" rate of flow is less than 0.1 cubic meters per square meter per year. As expected, the high flow area is of relatively small size, and is located where the backfill material is thinnest. Further, the locations of upward flow and downward flow are identified on this figure.
2. Time for plug flow. Figure 11 shows the time for the first pore volume to flush as a function of location in the pit. As can be seen, and would be expected, the flush times increase as the backfill depth increases, and as the gradient in the backfill decreases. Note that the plug flow flush times are for upward flow in the northern portion of the pit, and for downward flow in the southern portion of the pit.
3. Rate of plug flow. Figure 12 shows the expected proportion of seepage that passes through the backfill that is plug flow. After the plug flow occurs, the quality of the groundwater flow would be expected to approach the quality of groundwater in the country rock. The percentages for both upward and downward flow are shown. The figure indicates that the quality of the seepage from the backfill will improve rapidly, with the proportion of plug flow in the total seepage through the backfill falling to 50% within a decade, and essentially ending within a century. Note that the seepage through the backfill will not change, only the proportion that is plug flow (that is the first pore volume).

In summary, the analysis indicates that the proportion of plug flow water in the backfill seepage halves in the first decade after backfilling of the pit, and drops to zero in the long term.

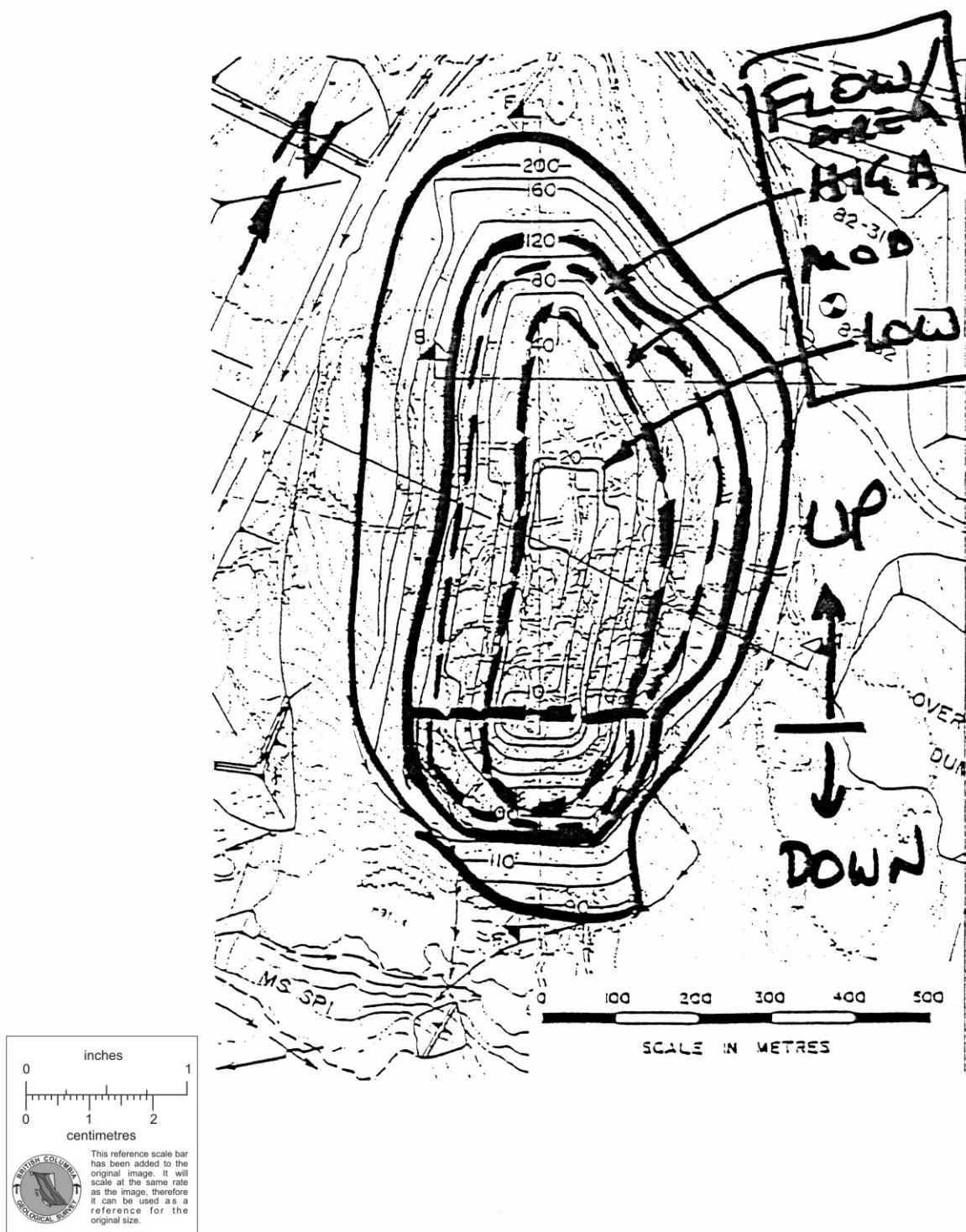


Figure 10 - Distribution of Seepage Flow Rates through Backfill

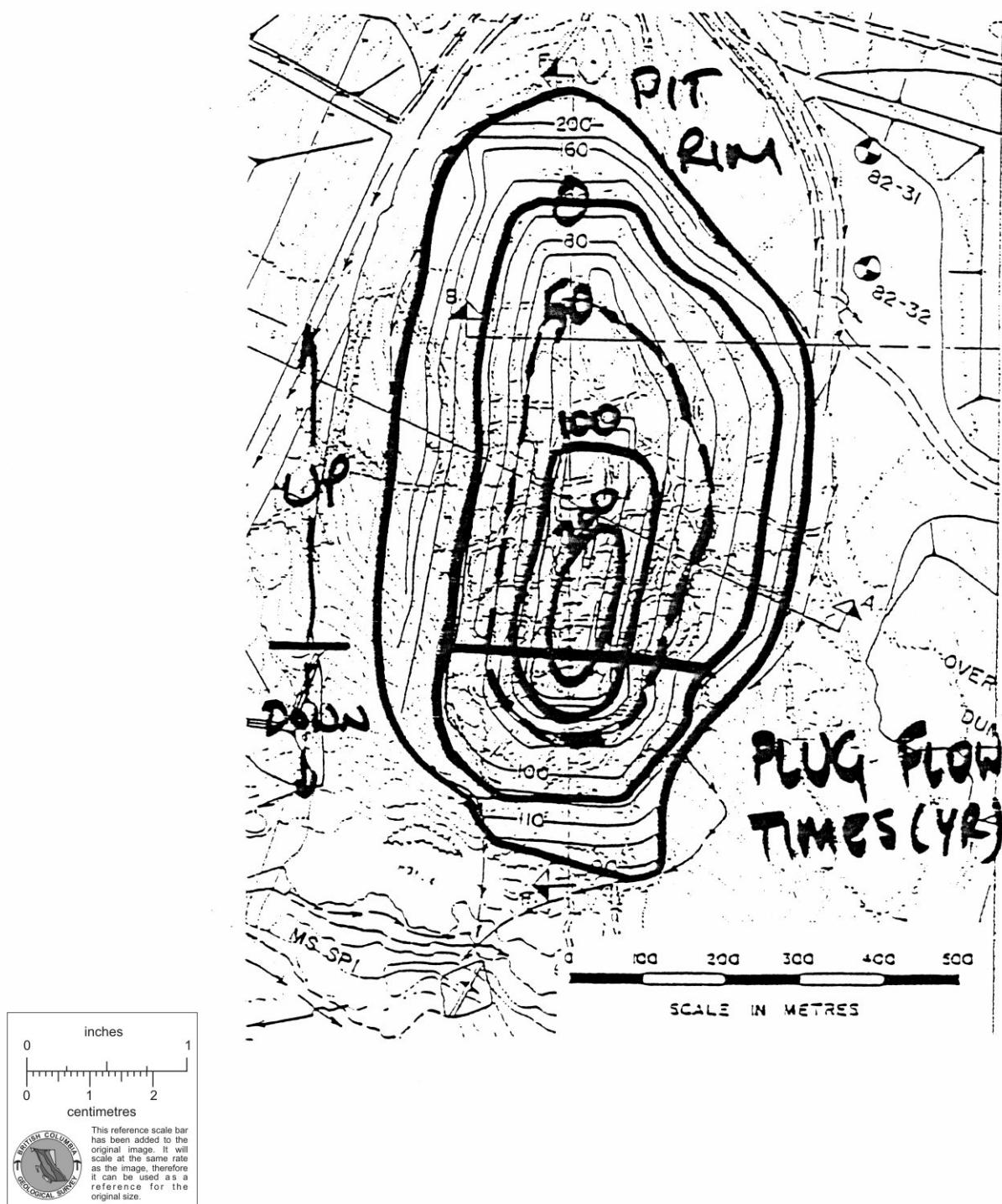


Figure 11 - Distribution of Times for Plug Flow (year)

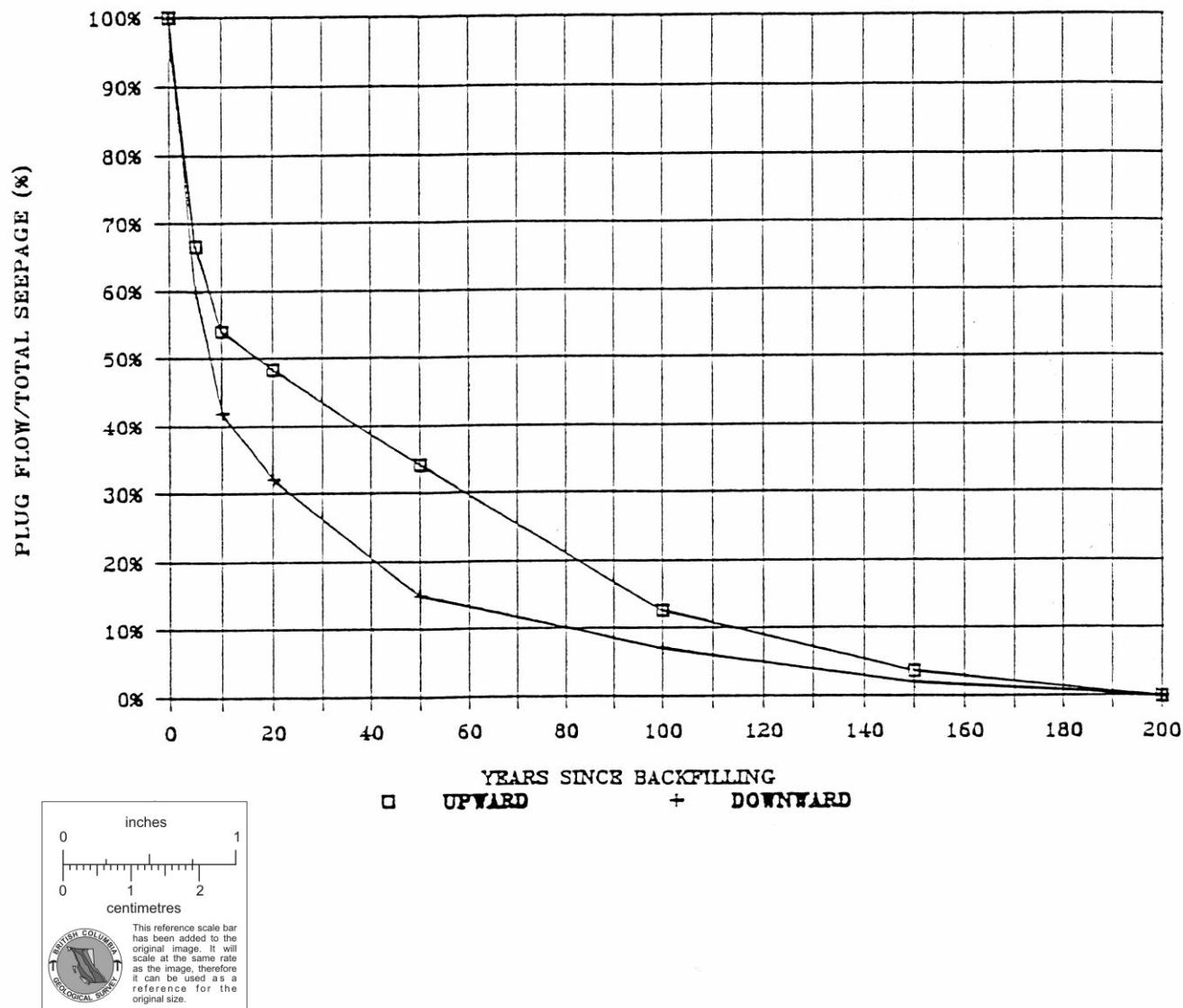


Figure 12 - Proportions of Plug Flow in Backfill Seepage

-----KEY ANALYSIS PARAMETERS-----

Number of nodes.....100  
Number of elements.....154  
Number of materials.....7  
Number of soils.....3

-----MATERIAL AND SOIL DATA-----

MATERIAL OR SOIL	HYDRAULIC CONDUCTIVITY [L/T]	SPECIFIC STORAGE [1/L]	SPECIFIC YIELD [-]	DISTRIBUTED INFLOW [L/T]
1	3.00E+00	1.00E-06	.0200	0.00E+00
2	2.00E+00	1.00E-06	.0500	0.00E+00
3	3.00E+00	1.00E-06	.0500	0.00E+00
4	3.00E+00	1.00E-06	.0200	
5	6.00E+00	1.00E-06	.0200	
6	3.00E+00	1.00E-06	.3000	
7	3.00E-01	1.00E-06	.0200	

## -----NODE AND FLOW DATA-----

-NODE DATA-		X-COORD [L]	Y-COORD [L]	BASE-EL [L]	MAX-EL [L]	INIT-W/T [L]	NEW-W/T [L]	BOUN DARY	FIXED-INF [L3/T]	INFILT_INF [L3/T]	STORE_INF [L3/T]	STREAM_INF [L3/T]	OUTFLOW [L3/T]	NODE #
##	LNK	INT												
1	0	0	-1400.0	-500.0	-1000.0	-500.0	320.0	320.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-2.410E-04	1
2	0	0	-1400.0	-300.0	-800.0	-300.0	320.0	320.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-4.915E-04	2
3	0	0	-1400.0	-100.0	-600.0	-100.0	320.0	320.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-5.200E-04	3
4	0	0	-1400.0	100.0	-400.0	100.0	320.0	320.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-5.933E-04	4
5	0	0	-1200.0	-500.0	-1000.0	-500.0	122.0	287.9 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	6.095E-02	5
6	0	0	-1200.0	-300.0	-800.0	-300.0	122.0	287.2 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.041E-01	6
7	0	0	-1200.0	-100.0	-600.0	-100.0	122.0	285.3 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	7.050E-02	7
8	0	0	-1200.0	100.0	-400.0	100.0	122.0	282.3 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.076E-02	8
9	0	0	-1000.0	-500.0	-1000.0	-500.0	122.0	257.0 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.150E-01	9
10	0	0	-1000.0	-300.0	-800.0	-300.0	122.0	255.7 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.982E-01	10
11	0	0	-1000.0	-100.0	-600.0	-100.0	122.0	251.3 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.330E-01	11
12	0	0	-1000.0	100.0	-400.0	100.0	122.0	244.5 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	5.369E-02	12
13	0	0	-800.0	-500.0	-1000.0	-500.0	122.0	223.6 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.676E-01	13
14	0	0	-800.0	-300.0	-800.0	-300.0	122.0	227.0 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.865E-01	14
15	0	0	-800.0	-100.0	-600.0	-100.0	122.0	221.5 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.923E-01	15
16	0	0	-800.0	100.0	-400.0	100.0	122.0	211.1 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	6.480E-02	16
17	0	0	-600.0	-500.0	-1000.0	-500.0	122.0	203.7 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.181E-01	17
18	0	0	-600.0	-300.0	-800.0	-300.0	122.0	201.9 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.732E-01	18
19	0	0	-600.0	-100.0	-600.0	-100.0	122.0	196.1 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.096E-01	19
20	0	0	-600.0	100.0	-400.0	100.0	122.0	170.1 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	6.450E-02	20
21	0	0	-400.0	-500.0	-1000.0	-500.0	122.0	182.1 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.596E-01	21
22	0	0	-400.0	-300.0	-800.0	-300.0	122.0	181.0 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.842E-01	22
23	0	0	-400.0	-100.0	-600.0	-100.0	122.0	170.7 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.054E-01	23
24	0	0	-400.0	100.0	-400.0	100.0	122.0	162.4 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	6.598E-02	24
25	0	0	-200.0	-500.0	-1000.0	-500.0	122.0	162.9 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.437E-01	25
26	0	0	-200.0	-300.0	-800.0	-300.0	122.0	159.1 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.797E-01	26
27	0	0	-200.0	-100.0	-600.0	-100.0	122.0	147.8 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.503E-01	27
28	-2	0	-200.0	120.0	-380.0	120.0	120.0	120.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.468E+04	28
29	0	0	0.0	-500.0	-1000.0	-500.0	122.0	143.7 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.674E-01	29
30	0	0	0.0	-300.0	-800.0	-300.0	122.0	140.3 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	4.633E-01	30
31	0	0	20.0	-100.0	-600.0	-100.0	122.0	131.5 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.007E+00	31
32	-1	0	0.0	120.0	-380.0	120.0	120.0	120.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.107E+04	32
33	0	0	200.0	-500.0	-1000.0	-500.0	122.0	130.2 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.025E-01	33
34	0	0	220.0	-300.0	-800.0	-300.0	122.0	127.8 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.134E+00	34
35	0	0	200.0	-100.0	-600.0	-100.0	122.0	129.5 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	6.936E-01	35
36	-2	0	185.0	120.0	-380.0	120.0	120.0	120.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.704E-04	36
37	0	0	420.0	-500.0	-1000.0	-500.0	122.0	118.5 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.248E-00	37
38	0	0	400.0	-300.0	-800.0	-300.0	122.0	121.2 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.095E-00	38
39	0	0	400.0	-100.0	-600.0	-100.0	122.0	124.7 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	4.348E-01	39
40	0	0	400.0	140.0	-360.0	140.0	140.0	140.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-2.994E+04	40
41	0	0	600.0	-500.0	-1000.0	-500.0	122.0	109.7 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	4.107E-01	41
42	0	0	600.0	-300.0	-800.0	-300.0	122.0	110.3 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	4.538E-01	42
43	0	0	600.0	-100.0	-600.0	-100.0	122.0	113.1 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.470E-01	43
44	0	0	600.0	120.0	-380.0	120.0	120.0	120.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-9.590E-03	44
45	0	0	900.0	-500.0	-1000.0	-500.0	90.0	90.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	9.362E-03	45
46	0	0	900.0	-300.0	-800.0	-300.0	90.0	90.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.033E+04	46
47	0	0	900.0	-100.0	-600.0	-100.0	90.0	90.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.200E+04	47
48	0	0	900.0	90.0	-410.0	90.0	90.0	90.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.550E+04	48
49	0	0	-1400.0	320.0	-180.0	320.0	320.0	320.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-2.735E+04	49
50	0	0	-1200.0	280.0	-220.0	280.0	280.0	280.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.743E+04	50

## -----NODE AND FLOW DATA-----

-NODE DATA-		X-COORD [L]	Y-COORD [L]	BASE-EL [L]	MAX-EL [L]	INIT-W/T [L]	NEW-W/T [L]	BOUN DARY	FIXED-INF [L3/T]	INFILT_INF [L3/T]	STORE_INF [L3/T]	STREAM_INF [L3/T]	OUTFLOW [L3/T]	---
#	LNK	INT												#
51	0	0	-950.0	230.0	-270.0	230.0	230.0	230.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.473E+04	51
52	0	0	0.0	0.0	0.0	0.0	0.0	0.0 XXXX	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	52
53	0	0	0.0	0.0	0.0	0.0	0.0	0.0 XXXX	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	53
54	0	0	0.0	0.0	0.0	0.0	0.0	0.0 XXXX	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	54
55	0	0	-400.0	160.0	-340.0	160.0	160.0	160.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.971E+03	55
56	0	0	-300.0	180.0	-320.0	180.0	180.0	180.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-3.144E+04	56
57	-1	0	-100.0	120.0	-380.0	120.0	120.0	120.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.132E+04	57
58	-1	0	100.0	120.0	-380.0	120.0	120.0	120.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	7.795E+03	58
59	0	0	240.0	155.0	-345.0	155.0	155.0	155.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-5.118E+04	59
60	0	0	-300.0	200.0	-300.0	200.0	200.0	200.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.574E+04	60
61	0	0	-600.0	155.0	-345.0	155.0	155.0	155.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	5.510E+04	61
62	0	0	-500.0	140.0	-360.0	140.0	122.0	166.7 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	5.155E-02	62
63	0	0	-500.0	100.0	-400.0	100.0	122.0	168.3 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.049E-01	63
64	0	0	-300.0	100.0	-400.0	100.0	122.0	151.3 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	6.390E-02	64
65	0	0	-300.0	0.0	-500.0	0.0	122.0	153.3 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.476E-01	65
66	0	0	-200.0	0.0	-500.0	0.0	122.0	137.0 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.540E-01	66
67	0	0	-160.0	60.0	-440.0	60.0	122.0	127.1 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.065E-01	67
68	0	0	-30.0	0.0	-500.0	0.0	122.0	130.1 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.991E-01	68
69	0	0	0.0	60.0	-440.0	60.0	122.0	124.4 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.048E-01	69
70	0	0	0.0	0.0	-500.0	0.0	122.0	128.8 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	4.922E-01	70
71	0	0	100.0	50.0	-440.0	60.0	122.0	124.5 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.044E-01	71
72	0	0	100.0	0.0	-500.0	0.0	122.0	127.6 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.697E-01	72
73	0	0	200.0	0.0	-500.0	0.0	122.0	129.7 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.590E-01	73
74	0	0	300.0	0.0	-500.0	0.0	122.0	131.9 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.826E-01	74
75	0	0	200.0	50.0	-440.0	60.0	122.0	129.3 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.115E-01	75
76	0	0	240.0	120.0	-380.0	120.0	122.0	143.9 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.434E-02	76
77	0	0	300.0	60.0	-440.0	60.0	122.0	136.1 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.226E-01	77
78	0	0	-300.0	140.0	-360.0	140.0	122.0	162.9 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.622E-02	78
79	0	0	-290.0	140.0	-360.0	140.0	122.0	157.3 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.937E-02	79
80	0	0	-500.0	0.0	-500.0	0.0	122.0	175.1 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.304E-01	80
81	0	0	-400.0	0.0	-500.0	0.0	122.0	165.5 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.345E-01	81
82	0	0	100.0	-100.0	-600.0	-100.0	122.0	130.2 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.209E+00	82
83	0	0	200.0	-200.0	-700.0	-200.0	122.0	123.6 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.766E+00	83
84	0	0	300.0	-300.0	-800.0	-300.0	122.0	125.1 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.049E+00	84
85	0	0	400.0	-400.0	-900.0	-400.0	122.0	120.6 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.052E+00	85
86	0	0	500.0	-500.0	-1000.0	-500.0	122.0	115.5 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	7.174E-01	86
87	0	0	-265.0	150.0	-350.0	150.0	150.0	150.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-1.107E+03	87
88	0	0	-240.0	130.0	-370.0	130.0	130.0	130.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	7.385E+03	88
89	-1	0	-220.0	120.0	-380.0	120.0	120.0	120.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	4.953E+03	89
90	-1	0	-200.0	120.0	-380.0	120.0	120.0	120.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.156E+04	90
91	-1	0	-150.0	120.0	-380.0	120.0	120.0	120.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.973E+03	91
92	-1	0	140.0	120.0	-380.0	120.0	120.0	120.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	7.391E+03	92
93	-1	0	170.0	120.0	-380.0	120.0	120.0	120.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	5.604E+03	93
94	0	0	190.0	125.0	-375.0	125.0	125.0	125.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	5.663E+03	94
95	0	0	210.0	140.0	-360.0	140.0	140.0	140.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-6.367E+03	95
96	0	0	200.0	100.0	-400.0	100.0	100.0	129.9 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	8.410E-02	96
97	0	0	180.0	100.0	-400.0	100.0	100.0	123.3 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	7.104E-02	97
98	0	0	-200.0	100.0	-400.0	100.0	100.0	124.4 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.973E-02	98
99	0	0	-240.0	100.0	-400.0	100.0	100.0	133.5 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	5.621E-02	99
100	0	0	-260.0	110.0	-390.0	110.0	110.0	139.8 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	4.295E-02	100

-----SINK FLOW DATA-----

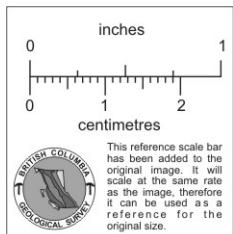
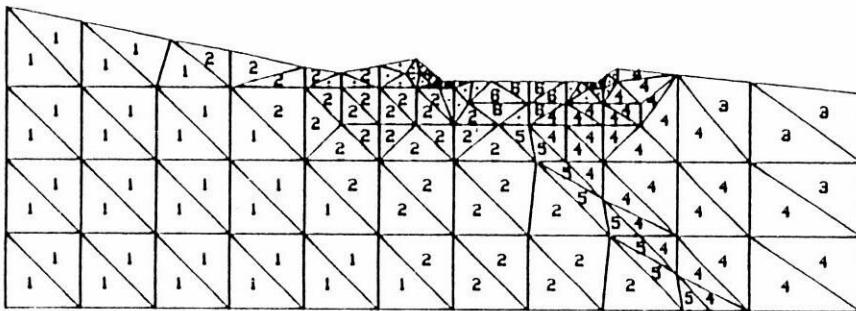
SINK	CONN	TOT_FLOW	SINK	CONN	TOT_FLOW	SINK	CONN	TOT_FLOW	SINK	CONN	TOT_FLOW	SINK	CONN	TOT_FLOW																														
#	#	[L3/T]	#	#	[L3/T]	#	#	[L3/T]	#	#	[L3/T]	#	#	[L3/T]																														
0	90	-1.2181E+05	1	8	7.0169E+04	2	2	5.1718E+04	3	0	0.0000E+00	4	0	0.0000E+00	5	0	0.0000E+00																											
6	0	0.0000E+00	7	0	0.0000E+00	8	0	0.0000E+00	9	0	0.0000E+00	10	0	0.0000E+00	11	0	0.0000E+00	12	0	0.0000E+00	13	0	0.0000E+00	14	0	0.0000E+00	15	0	0.0000E+00	16	0	0.0000E+00	17	0	0.0000E+00	18	0	0.0000E+00	19	0	0.0000E+00	20	0	0.0000E+00

-----ELEMENT DATA-----

CINOLA - RECLAIMED PIT - K=3 M/Y

1614

1318



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original size.

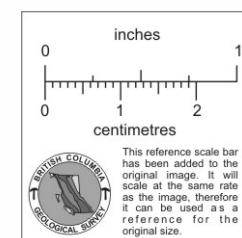
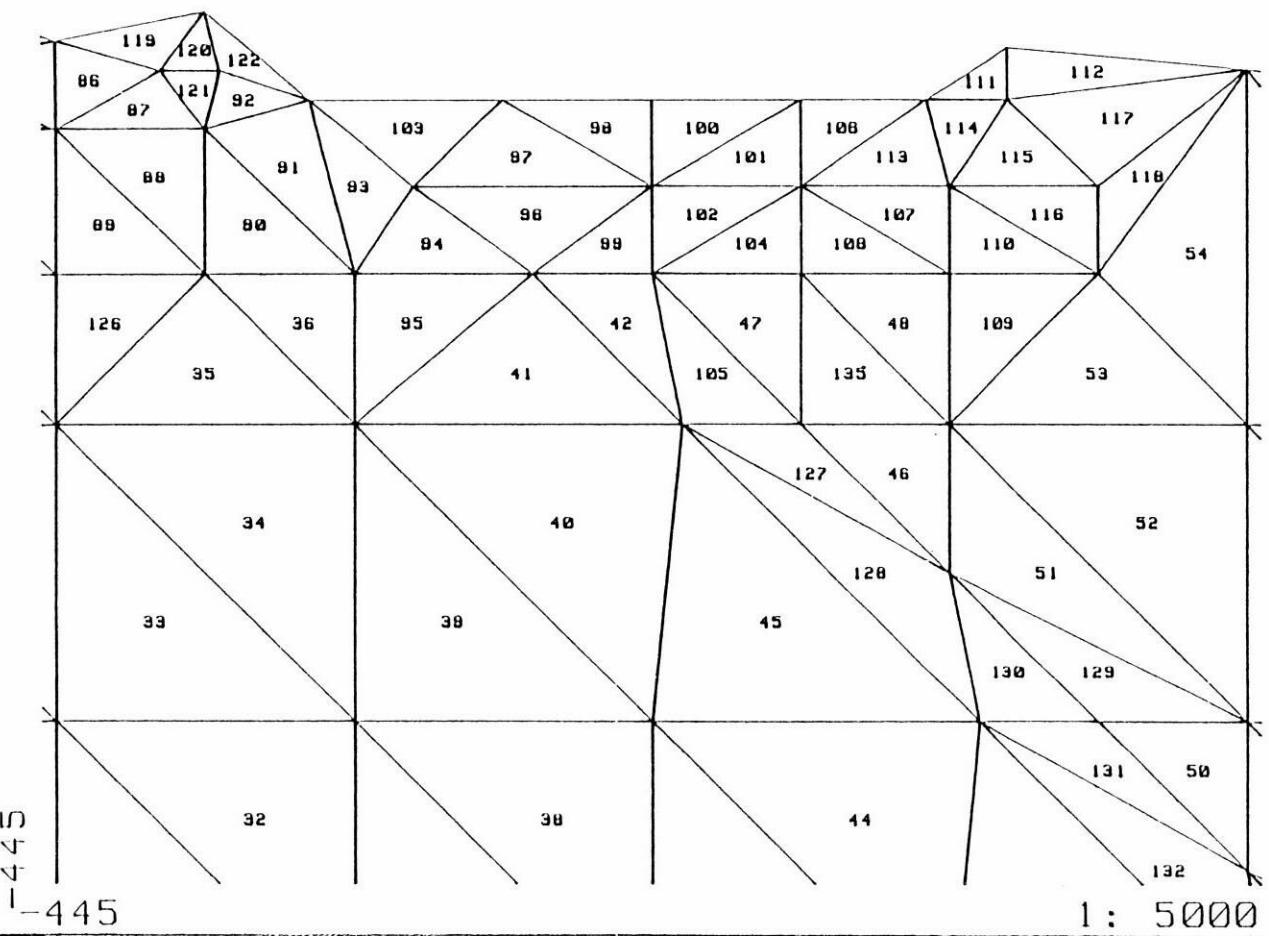
2238  
I-1943

1 : 20000

ELEMENTS  
MATERIALS

CINOLA - RECLAIMED PIT - K=3 M/Y

444



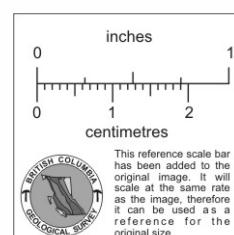
This reference scale bar  
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scale at the same rate  
as the image, therefore  
it can be used as a  
reference for the  
original size.

ELEMENTS  
NUMBERS

+<sub>55</sub>  
 +<sub>56</sub>  
 +<sub>24</sub> +<sub>78</sub> +<sub>79</sub> +<sub>28</sub> +<sub>57</sub> +<sub>32</sub> +<sub>58</sub> +<sub>36</sub> +<sub>76</sub> +<sub>59</sub>  
 +<sub>84</sub>  
 +<sub>67</sub> +<sub>69</sub> +<sub>71</sub> +<sub>75</sub> +<sub>77</sub>  
 +<sub>81</sub> +<sub>65</sub> +<sub>66</sub> +<sub>68</sub> +<sub>70</sub> +<sub>72</sub> +<sub>73</sub> +<sub>74</sub>  
 +<sub>23</sub> +<sub>27</sub> +<sub>31</sub> +<sub>82</sub> +<sub>35</sub> +<sub>83</sub>  
 +<sub>22</sub> +<sub>26</sub> +<sub>30</sub> +<sub>34</sub> +<sub>84</sub> +<sub>+</sub>

10  
44  
44  
1-445

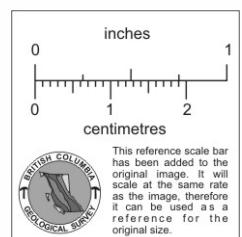
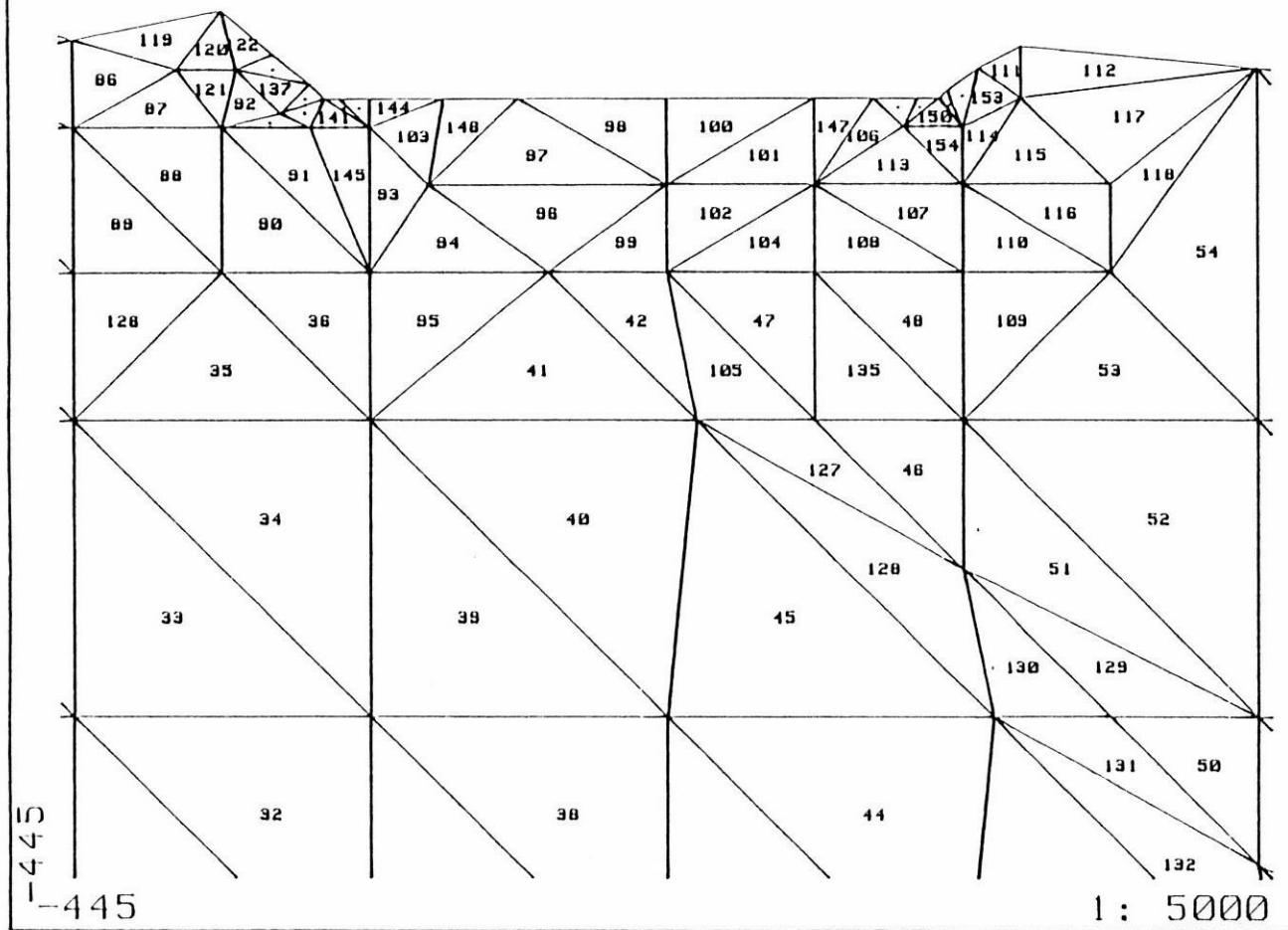
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NODES  
NUMBERS

CINOLA - RECLAIMED PIT - K=3 M/Y

444



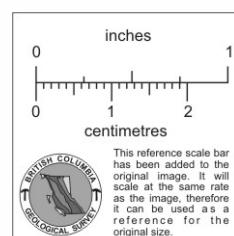
## ELEMENTS NUMBERS

CINOLA - RECLAIMED PIT - K=3 M/Y

444

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+<sub>24</sub>                    +<sub>78</sub> +<sub>79</sub> +<sub>87</sub>  
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+<sub>81</sub>                    +<sub>85</sub>                    +<sub>66</sub>                    +<sub>68</sub>                    +<sub>70</sub>                    +<sub>72</sub>                    +<sub>73</sub>                    +<sub>74</sub>  
+<sub>23</sub>                    +<sub>27</sub>                    +<sub>31</sub>                    +<sub>82</sub>                    +<sub>35</sub>  
+<sub>22</sub>                    +<sub>26</sub>                    +<sub>30</sub>                    +<sub>34</sub>                    +<sub>84</sub>                    +<sub>83</sub>  
+<sub>15</sub>  
+<sub>47</sub>  
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1 : 5000



NODES  
NUMBERS

CINOLA - RECLAIMED PIT - K=3 M/Y

177

+<sub>59</sub>

+<sub>95</sub>

+<sub>58</sub>      +<sub>92</sub>      +<sub>93</sub> +<sub>94</sub>  
                +<sub>96</sub>

+<sub>97</sub>      +<sub>98</sub>

+<sub>71</sub>

+<sub>75</sub>

+<sub>77</sub>

+<sub>72</sub>

+<sub>73</sub>

+<sub>74</sub>

+<sub>82</sub>

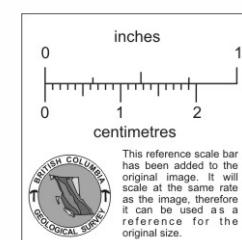
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22

-178

1 : 2000

377



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NODES  
NUMBERS

CINOLA - RECLAIMED PIT - K=3 M/Y

177

E2  
I

+<sub>87</sub>

+<sub>78</sub>

+<sub>79</sub>

+<sub>88</sub>

+<sub>28</sub> +<sub>89</sub> +<sub>90</sub>

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+<sub>57</sub>

+<sub>100</sub>

+<sub>84</sub>

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+<sub>65</sub>

+<sub>66</sub>

+<sub>68</sub>

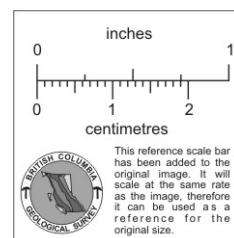
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37

1-178

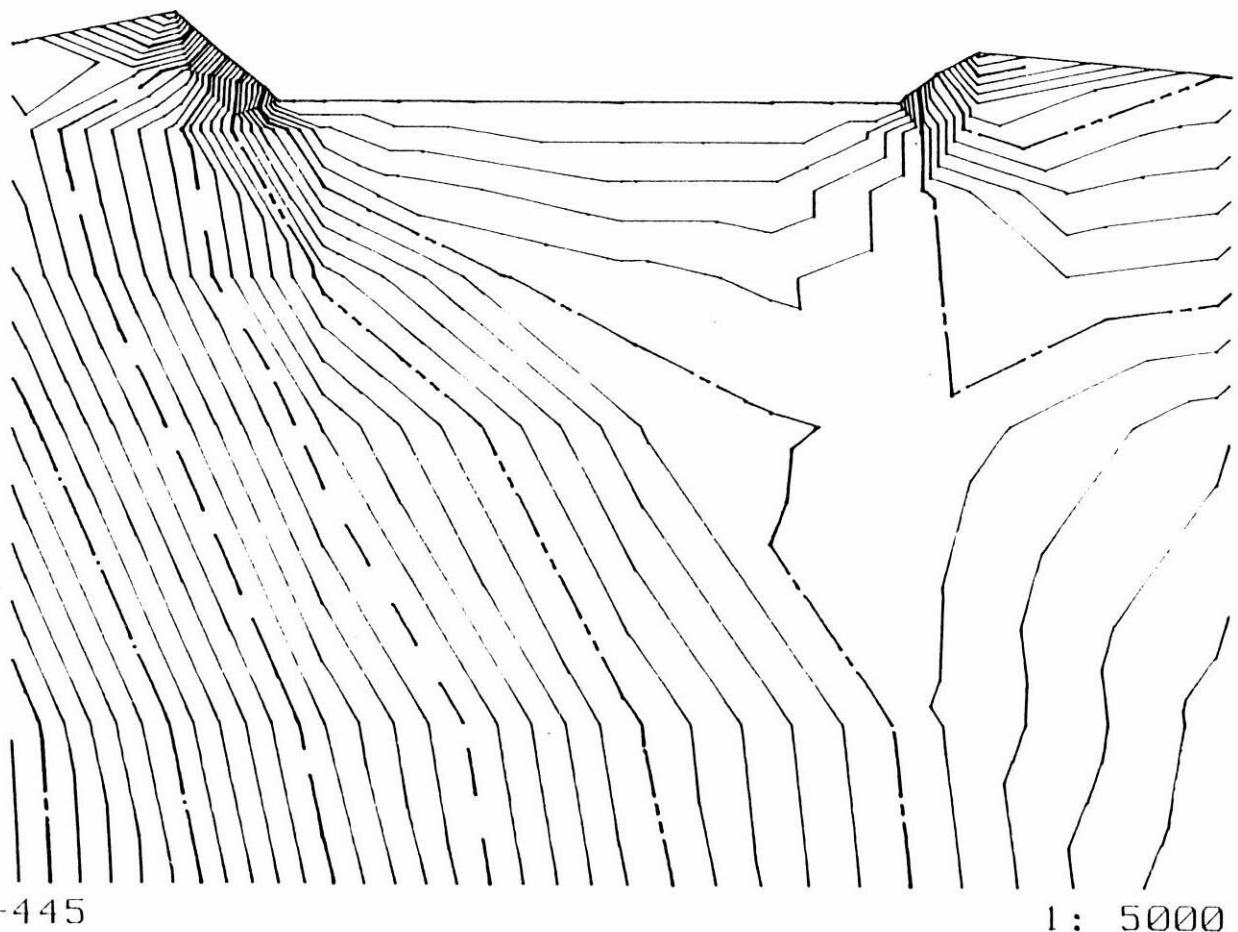
1 : 2000



NODES  
NUMBERS

CINOLA - RECLAIMED PIT - K=3 M/Y

444

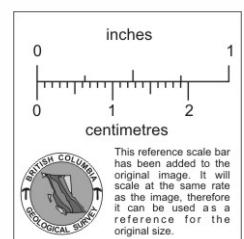


Legend:

- 110
- 120
- 130
- 140
- 150

(meters)

Interval:  
2 meter

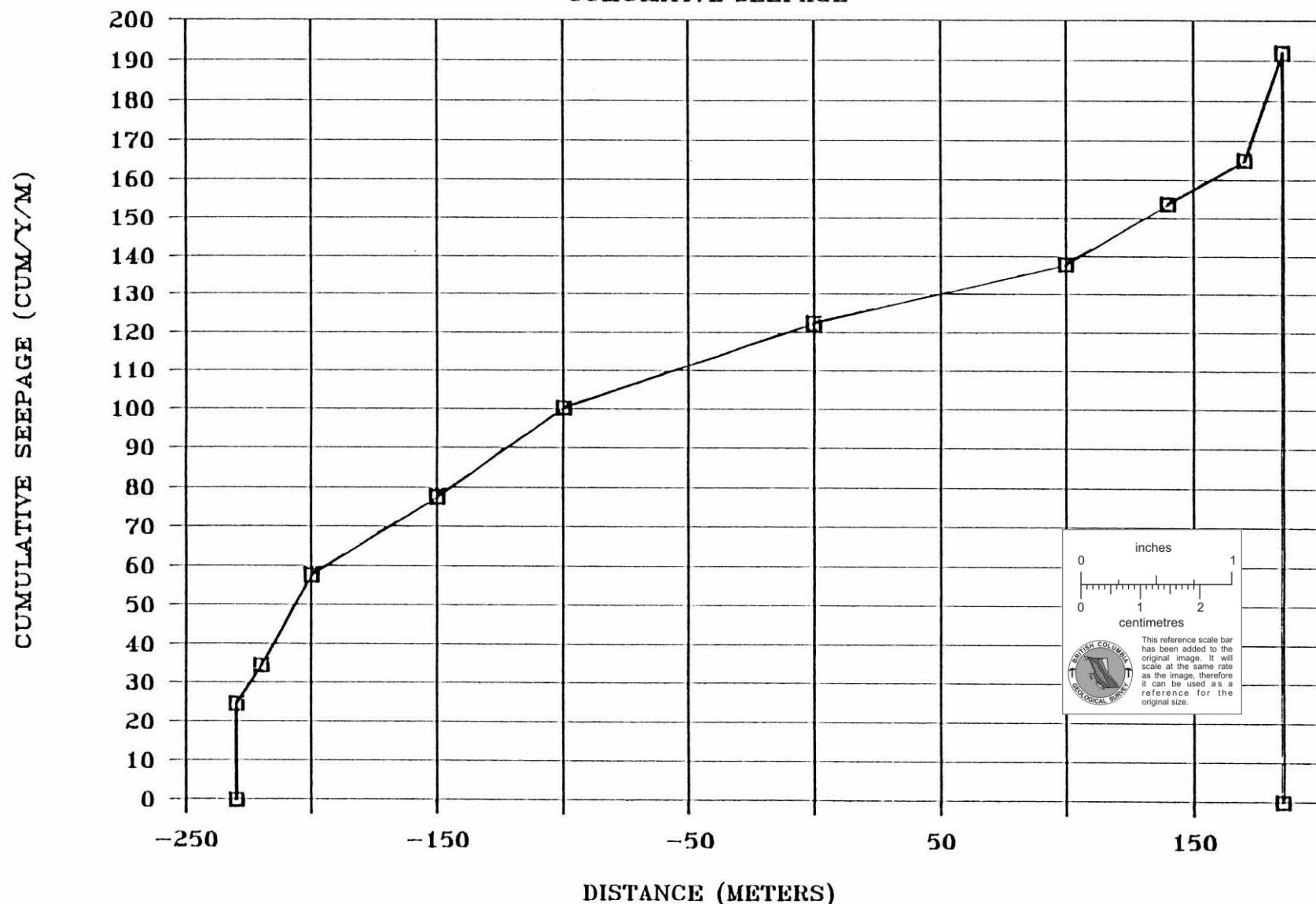


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reference for the  
original size.

HEADS  
CURRENT

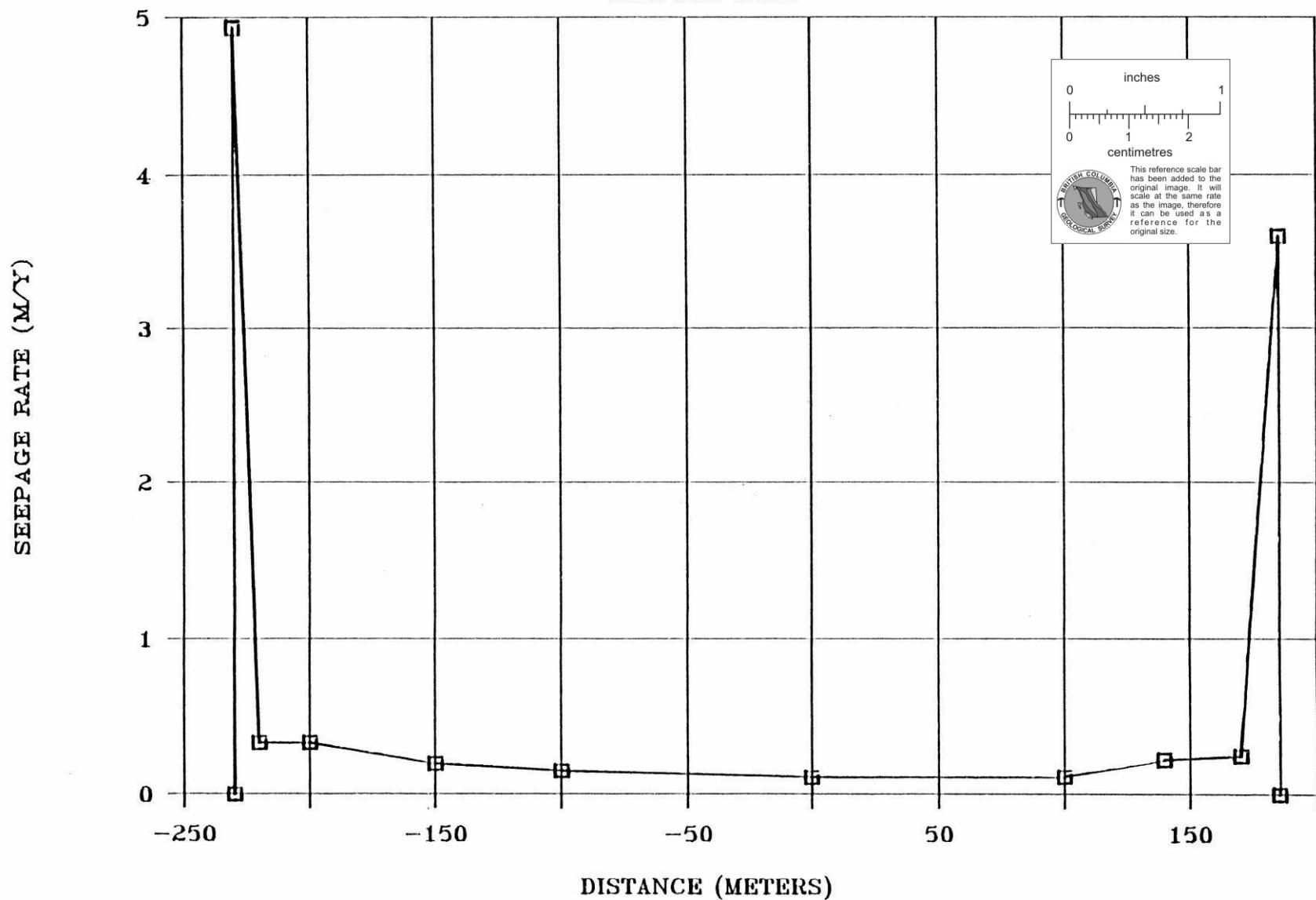
# RECLAIMED PIT SEEPAGE

## CUMULATIVE SEEPAGE



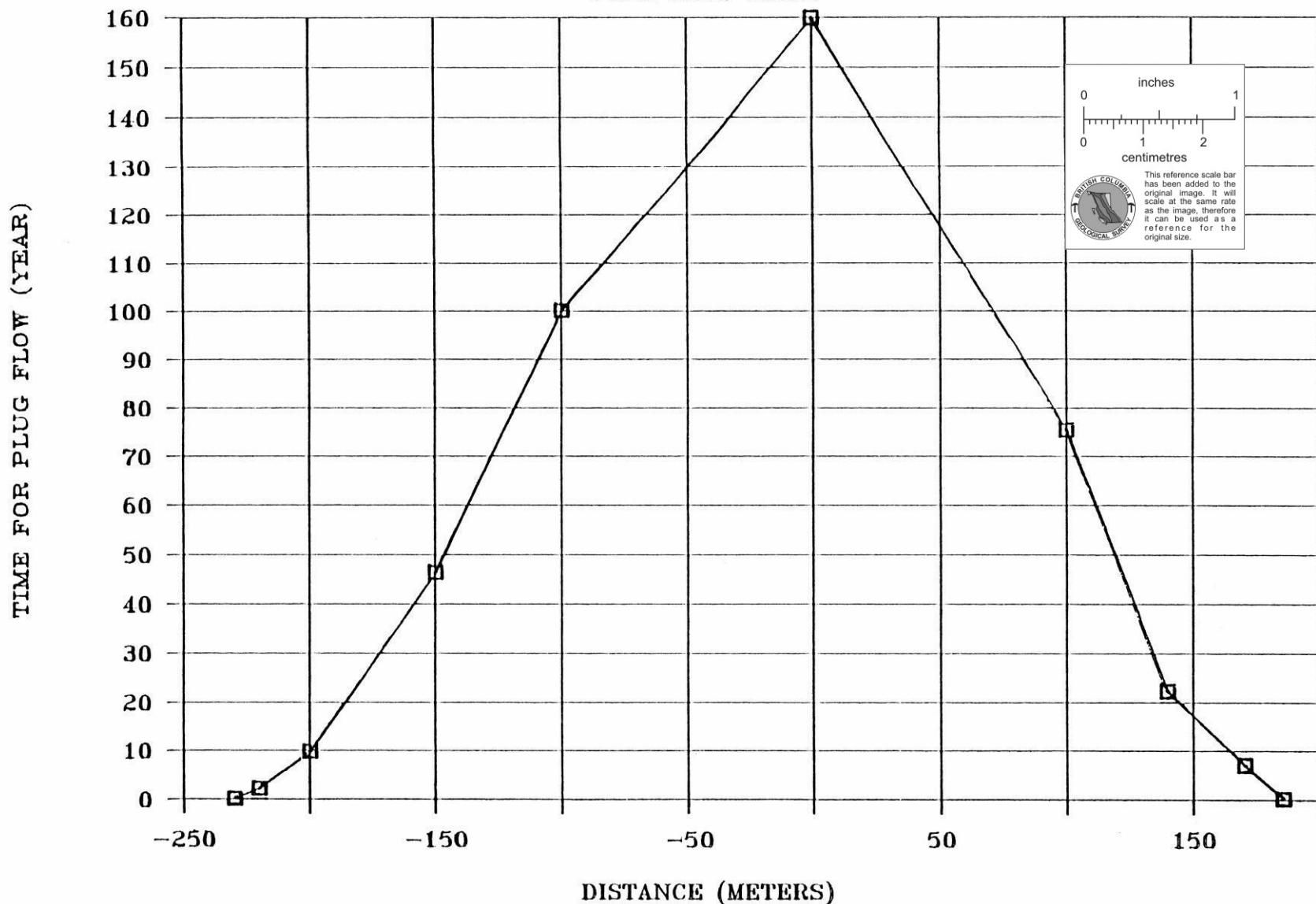
# RECLAIMED PIT SEEPAGE

## SEEPAGE RATE



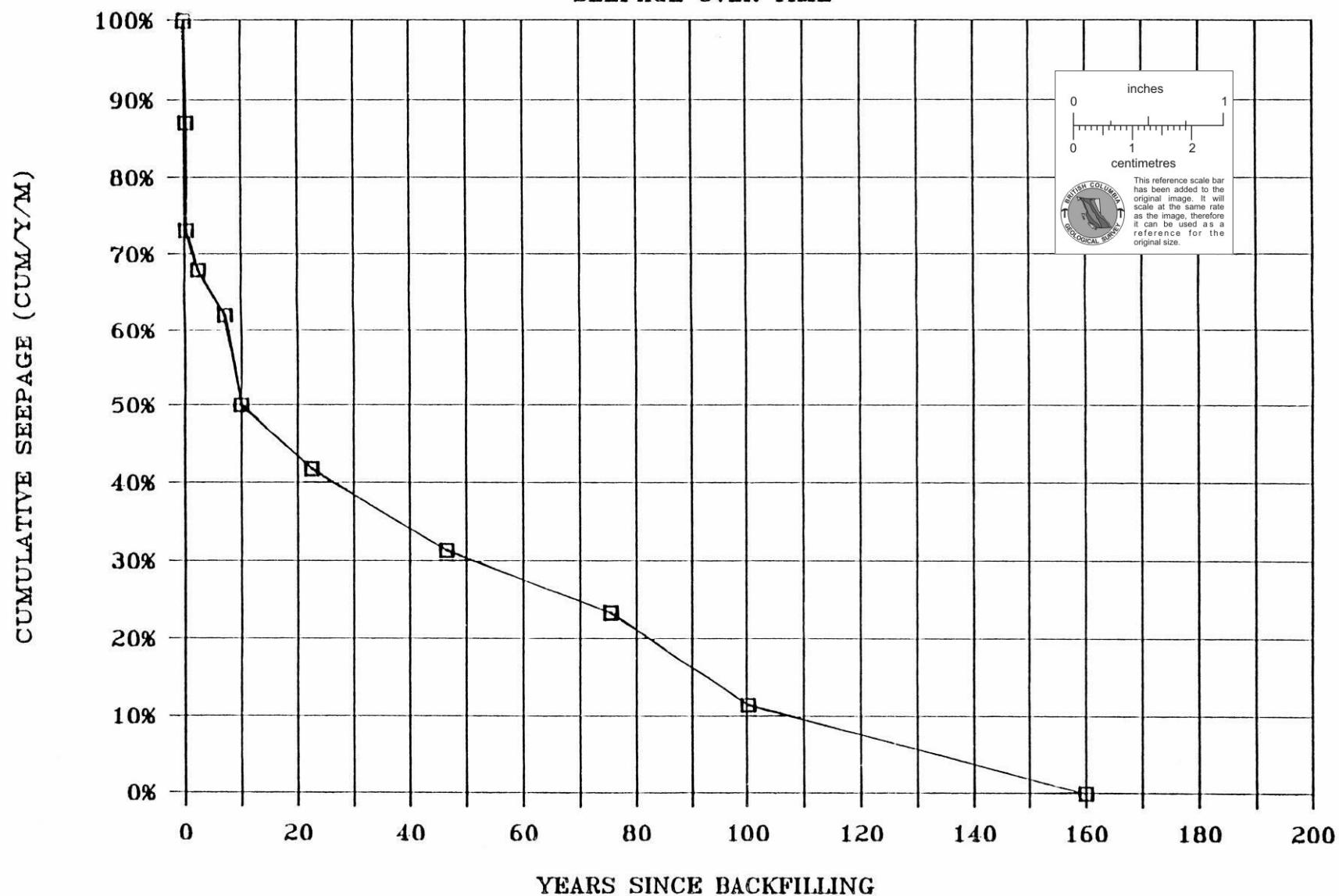
# RECLAIMED PIT SEEPAGE

## PLUG FLOW TIMES



# RECLAIMED PIT SEEPAGE

## SEEPAGE OVER TIME



-----KEY ANALYSIS PARAMETERS-----

Number of nodes.....130  
Number of elements.....219  
Number of materials.....5  
Number of soils.....6

-----MATERIAL AND SOIL DATA-----

MATERIAL OR SOIL	HYDRAULIC CONDUCTIVITY [L/T]	SPECIFIC STORAGE [1/L]	SPECIFIC YIELD [-]	DISTRIBUTED INFLOW [L/T]
1	3.00E+00	1.00E-01	.1000	0.00E+00
2	3.00E+00	1.00E-01	.1000	0.00E+00
3	3.00E+00	1.00E-01	.1000	0.00E+00
4	3.00E+00	1.00E-01	.1000	0.00E+00
5	3.00E+00	1.00E-01	.1000	0.00E+00
6				0.00E+00

-----NODE AND FLOW DATA-----

-NODE DATA-		X-COORD [L]	Y-COORD [L]	BASE-EL [L]	MAX-EL [L]	INIT-W/T [L]	NEW-W/T [L]	BOUN DARY	FIXED-INF [L3/T]	INFILT_INF [L3/T]	STORE_INF [L3/T]	STREAM_INF [L3/T]	OUTFLOW NODE [L3/T]	---
---	---	---	---	---	---	---	---	---	---	---	---	---	---	---
1	0	0	-1000.0	-500.0	-900.0	-500.0	170.0	170.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-1.800E+04	1
2	0	0	-1000.0	-300.0	-700.0	-300.0	170.0	170.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-1.289E+04	2
3	0	0	-1000.0	-100.0	-500.0	-100.0	170.0	170.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-1.577E+04	3
4	0	0	-800.0	-500.0	-700.0	-500.0	140.0	140.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	5.911E+04	4
5	0	0	-300.0	-300.0	-700.0	-300.0	150.0	159.3 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-3.140E-02	5
6	0	0	-800.0	-100.0	-500.0	-100.0	150.0	160.5 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-3.717E-02	6
7	0	0	-600.0	-500.0	-700.0	-500.0	170.0	170.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	5.835E+02	7
8	0	0	-600.0	-300.0	-700.0	-300.0	150.0	166.5 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-7.222E-02	8
9	0	0	-600.0	-100.0	-500.0	-100.0	150.0	160.6 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-7.147E-02	9
10	0	0	-400.0	-500.0	-900.0	-500.0	208.0	208.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	9.526E+04	10
11	0	0	-400.0	-300.0	-700.0	-300.0	150.0	176.1 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-1.336E-01	11
12	0	0	-400.0	-100.0	-500.0	-100.0	150.0	157.8 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-1.883E-01	12
13	0	0	-200.0	-500.0	-900.0	-500.0	210.0	201.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-3.219E+04	13
14	0	0	-200.0	-300.0	-700.0	-300.0	150.0	172.2 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-2.163E-01	14
15	0	0	-200.0	-100.0	-500.0	-100.0	150.0	148.9 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-3.548E-01	15
16	0	0	0.0	-500.0	-900.0	-500.0	198.0	198.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-5.736E+04	16
17	0	0	0.0	-300.0	-700.0	-300.0	150.0	162.7 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-2.392E-01	17
18	0	0	0.0	-100.0	-500.0	-100.0	150.0	140.0 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-6.998E-01	18
19	0	0	200.0	-500.0	-900.0	-500.0	170.0	170.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-6.044E+04	19
20	0	0	200.0	-300.0	-700.0	-300.0	150.0	140.6 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-2.901E-01	20
21	0	0	200.0	-100.0	-500.0	-100.0	150.0	125.0 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-7.648E-01	21
22	0	0	400.0	-500.0	-900.0	-500.0	100.0	100.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.274E+04	22
23	0	0	400.0	-300.0	-700.0	-300.0	150.0	104.8 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-1.347E-01	23
24	0	0	400.0	-100.0	-500.0	-100.0	150.0	99.7 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-3.384E-01	24
25	0	0	600.0	-500.0	-900.0	-500.0	75.0	75.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	7.527E+03	25
26	0	0	600.0	-300.0	-700.0	-300.0	150.0	78.3 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-3.042E-02	26
27	0	0	600.0	-100.0	-500.0	-100.0	150.0	76.0 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-3.776E-02	27
28	0	0	800.0	-500.0	-900.0	-500.0	55.0	55.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.113E+04	28
29	0	0	800.0	-300.0	-700.0	-300.0	150.0	59.3 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-2.649E-02	29
30	0	0	800.0	-100.0	-500.0	-100.0	150.0	58.3 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-2.405E-02	30
31	0	0	1000.0	-500.0	-900.0	-500.0	45.0	45.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	6.000E+03	31
32	0	0	1000.0	-300.0	-700.0	-300.0	45.0	45.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.713E+04	32
33	0	0	1000.0	-100.0	-500.0	-100.0	45.0	45.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.391E+04	33
34	0	0	-1000.0	170.0	-230.0	170.0	170.0	170.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-4.615E+03	34
35	0	0	-1000.0	100.0	-300.0	100.0	170.0	170.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-1.917E+04	35
36	0	0	1000.0	45.0	-355.0	45.0	45.0	45.0 HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	4.650E+03	36
37	0	0	-800.0	100.0	-300.0	100.0	150.0	145.8 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-1.162E-02	37
38	0	0	-600.0	100.0	-300.0	100.0	150.0	162.4 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-3.315E-02	38
39	0	0	-500.0	0.0	-400.0	0.0	150.0	158.6 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-1.117E-01	39
40	0	0	-400.0	0.0	-400.0	0.0	150.0	150.1 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-1.539E-01	40
41	0	0	-300.0	0.0	-400.0	0.0	150.0	141.9 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-2.574E-01	41
42	0	0	-200.0	0.0	-400.0	0.0	150.0	136.7 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-3.571E-01	42
43	0	0	-100.0	-20.0	-420.0	-20.0	150.0	135.6 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-5.670E-01	43
44	0	0	0.0	-50.0	-450.0	-50.0	150.0	134.9 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-6.365E-01	44
45	0	0	100.0	-50.0	-450.0	-50.0	150.0	129.2 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-6.336E-01	45
46	0	0	200.0	-50.0	-450.0	-50.0	150.0	122.5 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-6.367E-01	46
47	0	0	300.0	-50.0	-450.0	-50.0	150.0	111.7 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-6.150E-01	47
48	0	0	400.0	0.0	-400.0	0.0	150.0	96.7 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-2.541E-01	48
49	0	0	500.0	0.0	-400.0	0.0	150.0	82.4 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-1.246E-01	49
50	0	0	600.0	0.0	-400.0	0.0	150.0	72.9 CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-5.541E-02	50

-----NODE AND FLOW DATA-----

-NODE DATA-			X-COORD [L]	Y-COORD [L]	BASE-EL [L]	MAX-EL [L]	INIT-W/T [L]	NEW-W/T [L]	BOUN DARY	FIXED-INF [L3/T]	INFILT_INF [L3/T]	STORE_INF [L3/T]	STREAM_INF [L3/T]	OUTFLOW [L3/T]	NODE ##
##	LNK	INT													
51	0	0	700.0	0.0	-400.0	0.0	150.0	150.0	CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-2.744E-02	51
52	0	0	-870.0	150.0	-250.0	150.0	150.0	150.0	HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.800E+04	52
53	0	0	-770.0	135.0	-265.0	135.0	135.0	135.0	HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	4.379E+04	53
54	0	0	-600.0	170.0	-230.0	170.0	170.0	170.0	HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-1.551E+04	54
55	0	0	-480.0	200.0	-200.0	200.0	200.0	200.0	HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-6.072E+04	55
56	0	0	-390.0	140.0	-260.0	140.0	140.0	140.0	HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.058E+04	56
57	0	0	-330.0	120.0	-280.0	120.0	120.0	120.0	HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	3.422E+04	57
58	0	0	-250.0	120.0	-280.0	120.0	120.0	120.0	HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.460E+04	58
59	0	0	-200.0	120.0	-280.0	120.0	120.0	120.0	HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.295E+04	59
60	0	0	-100.0	120.0	-280.0	120.0	120.0	120.0	HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.329E+04	60
61	0	0	0.0	120.0	-280.0	120.0	120.0	120.0	HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.035E-04	61
62	0	0	100.0	120.0	-280.0	120.0	120.0	120.0	HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	5.798E-03	62
63	0	0	200.0	120.0	-280.0	120.0	120.0	120.0	HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-3.457E-01	63
64	0	0	250.0	120.0	-280.0	120.0	120.0	120.0	HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-2.844E+03	64
65	0	0	300.0	120.0	-280.0	120.0	120.0	120.0	HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-4.403E+03	65
66	0	0	319.0	120.0	-280.0	120.0	120.0	120.0	HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-4.073E+03	66
67	0	0	334.0	120.0	-280.0	120.0	120.0	120.0	HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-5.038E+03	67
68	0	0	360.0	120.0	-280.0	120.0	120.0	120.0	HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-1.510E+04	68
69	0	0	400.0	90.0	-310.0	90.0	90.0	90.0	HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	2.528E+04	69
70	0	0	500.0	75.0	-325.0	75.0	75.0	75.0	HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	1.861E+04	70
71	0	0	600.0	70.0	-330.0	70.0	70.0	70.0	HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	6.594E-03	71
72	0	0	800.0	55.0	-345.0	55.0	55.0	55.0	HEAD	0.000E+00	0.000E+00	0.000E+00	0.000E+00	9.536E+03	72
73	0	0	-470.0	150.0	-250.0	150.0	150.0	176.3	CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-3.157E-02	73
74	0	0	-400.0	100.0	-300.0	100.0	100.0	146.0	CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-5.963E-02	74
75	0	0	-350.0	50.0	-350.0	50.0	150.0	140.2	CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-1.422E-01	75
76	0	0	-360.0	118.0	-282.0	118.0	150.0	131.9	CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-3.021E-02	76
77	0	0	-325.0	80.0	-320.0	80.0	150.0	131.3	CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-1.159E-01	77
78	0	0	-290.0	40.0	-360.0	40.0	150.0	134.8	CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-2.748E-01	78
79	0	0	-300.0	90.0	-310.0	90.0	150.0	127.0	CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-9.521E-02	79
80	0	0	-250.0	90.0	-310.0	90.0	150.0	125.2	CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-1.169E-01	80
81	0	0	-270.0	60.0	-340.0	60.0	150.0	131.0	CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-2.023E-01	81
82	0	0	-220.0	60.0	-340.0	60.0	150.0	129.1	CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-3.015E-01	82
83	0	0	-220.0	40.0	-360.0	40.0	150.0	132.0	CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-3.566E-01	83
84	0	0	-200.0	90.0	-310.0	90.0	150.0	124.3	CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-1.678E-01	84
85	0	0	-250.0	118.0	-282.0	118.0	150.0	120.4	CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-5.777E-02	85
86	0	0	-200.0	118.0	-282.0	118.0	150.0	120.3	CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-3.222E-02	86
87	0	0	-330.0	118.0	-282.0	118.0	150.0	120.3	CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-4.166E-02	87
88	0	0	-100.0	118.0	-282.0	118.0	150.0	120.2	CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-1.603E-01	88
89	0	0	-100.0	70.0	-330.0	70.0	150.0	125.6	CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-3.408E-01	89
90	0	0	-150.0	50.0	-350.0	50.0	150.0	128.8	CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-4.706E-01	90
91	0	0	-150.0	30.0	-370.0	30.0	150.0	131.3	CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-4.396E-01	91
92	0	0	-85.0	20.0	-380.0	20.0	150.0	130.8	CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-5.559E-01	92
93	0	0	-80.0	40.0	-350.0	40.0	150.0	128.5	CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-5.275E-01	93
94	0	0	-30.0	70.0	-330.0	70.0	150.0	124.7	CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-2.907E-01	94
95	0	0	-60.0	20.0	-380.0	20.0	150.0	130.1	CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-6.244E-01	95
96	0	0	-70.0	0.0	-400.0	0.0	150.0	132.5	CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-6.399E-01	96
97	0	0	30.0	10.0	-390.0	10.0	150.0	128.3	CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-9.245E-01	97
98	0	0	30.0	30.0	-370.0	30.0	150.0	125.7	CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-7.306E-01	98
99	0	0	0.0	118.0	-282.0	118.0	150.0	120.2	CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-1.374E-01	99
100	0	0	100.0	118.0	-282.0	118.0	150.0	120.1	CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-1.757E-01	100

-----NODE AND FLOW DATA-----

-NODE DATA-		X-COORD	Y-COORD	BASE-EL	MAX-EL	INIT-W/T	NEW-W/T	BOUN	FIXED-INF	INFILT_INF	STORE_INF	STREAM_INF	OUTFLOW	NODE	
#	LNK	INT	[L]	[L]	[L]	[L]	[L]	DARY	[L3/T]	[L3/T]	[L3/T]	[L3/T]	[L3/T]	#	
101	0	0	100.0	70.0	-330.0	70.0	150.0	122.4	CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-3.795E-01	101
102	0	0	120.0	30.0	-370.0	30.0	150.0	123.7	CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-8.523E-01	102
103	0	0	120.0	10.0	-390.0	10.0	150.0	124.7	CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-8.341E-01	103
104	0	0	200.0	10.0	-390.0	10.0	150.0	120.5	CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-9.114E-01	104
105	0	0	200.0	70.0	-330.0	70.0	150.0	120.1	CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-4.038E-01	105
106	0	0	200.0	118.0	-282.0	118.0	150.0	120.0	CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-1.319E-01	106
107	0	0	250.0	118.0	-282.0	118.0	150.0	119.9	CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-1.138E-01	107
108	0	0	250.0	80.0	-320.0	80.0	150.0	116.1	CONT	0.000E+00	0.000E+00	0.000E+00	0.000E+00	-3.141E-01	108
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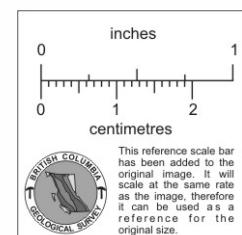
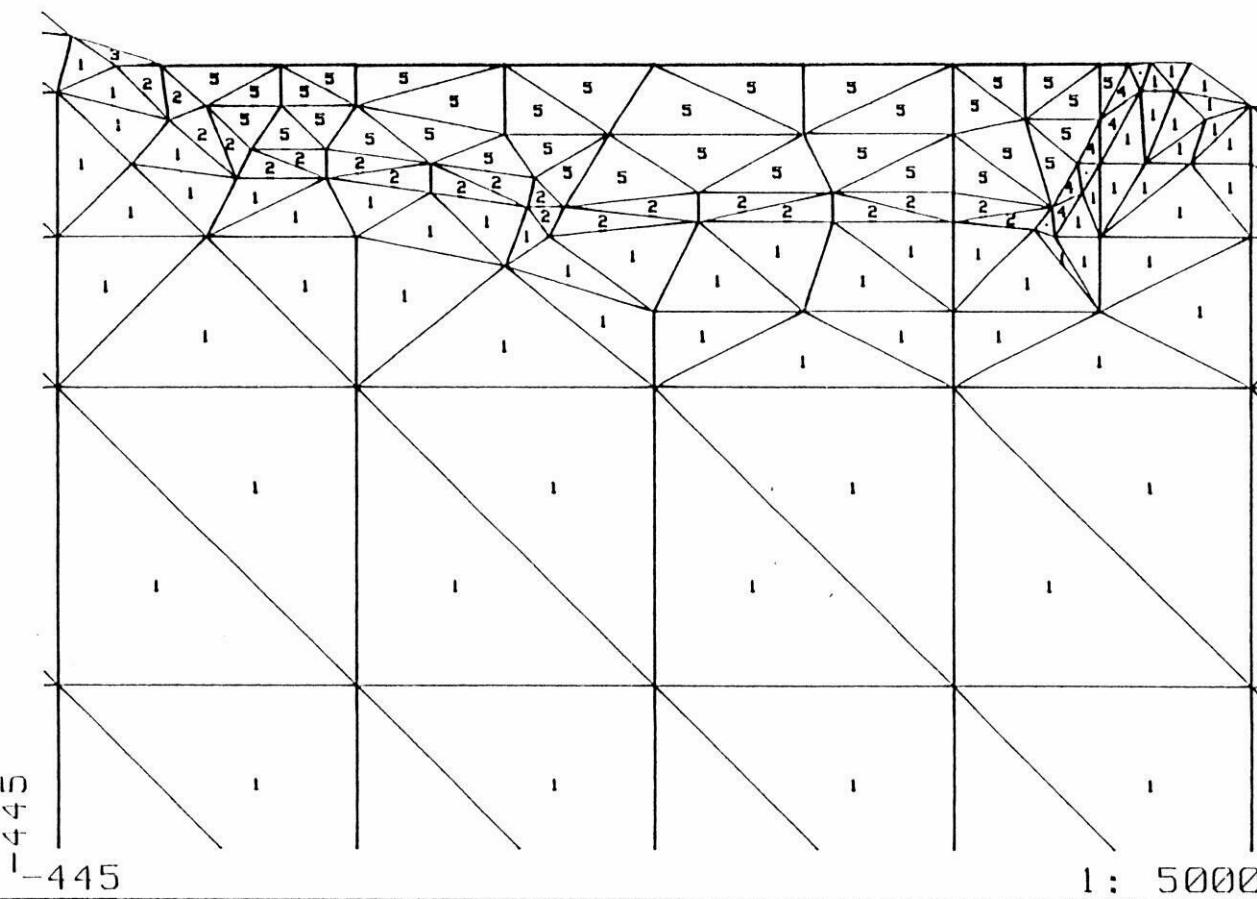
SINK	CONN	TOT_FLOW												
#	#	[L3/T]												
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-----ELEMENT DATA-----

-----ELEMENT DATA-----

CINOLA - PIT - N-S - K(f i l l)=3 M/Y

444

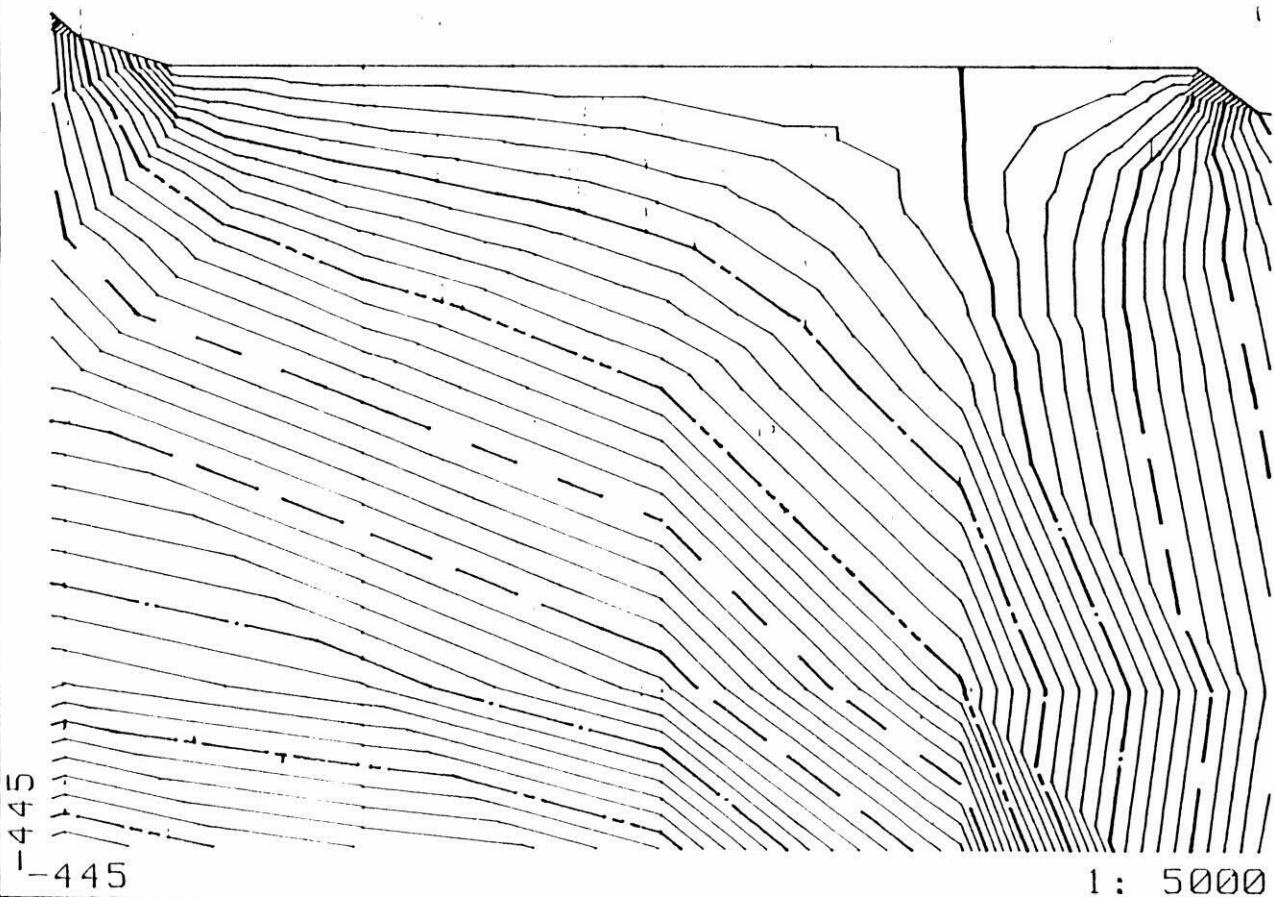


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ELEMENTS  
MATERIALS

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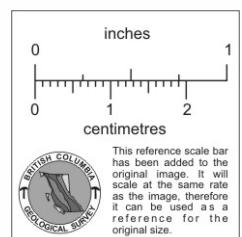
1 : 5000

Legend :

- 80
- 90
- 100
- 110
- 120

(meters)

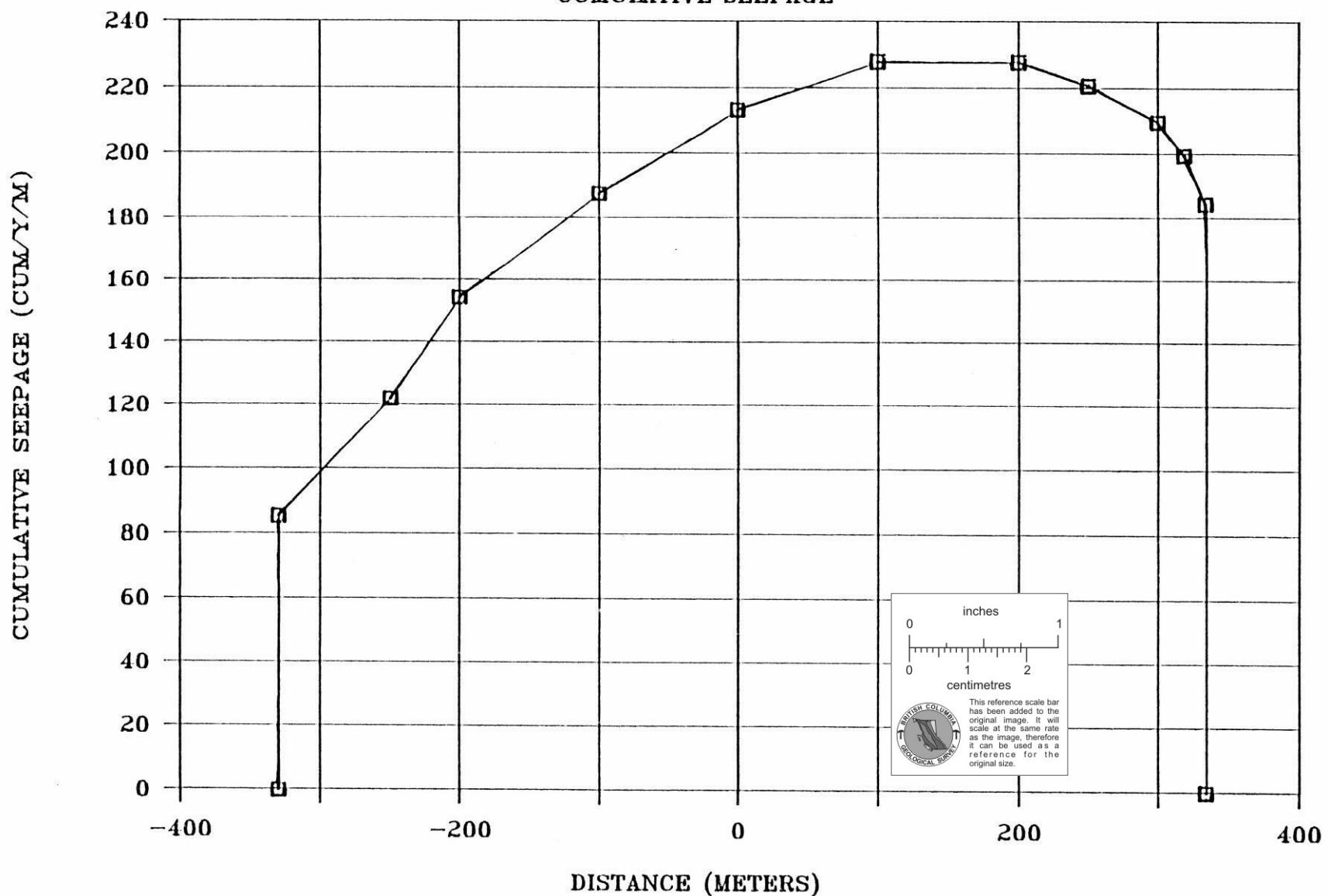
Interval :  
2 meters



HEADS  
CURRENT

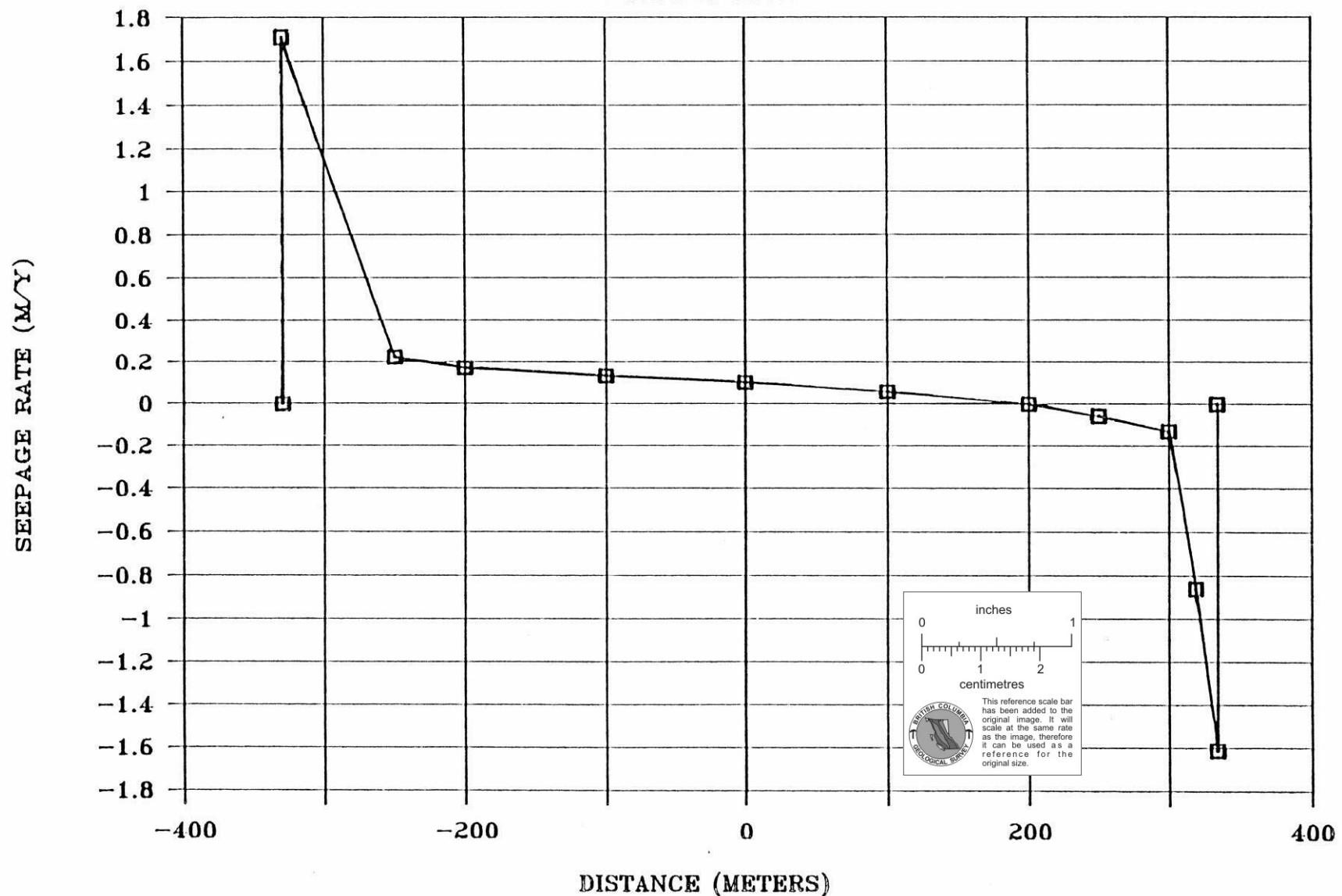
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## CUMULATIVE SEEPAGE



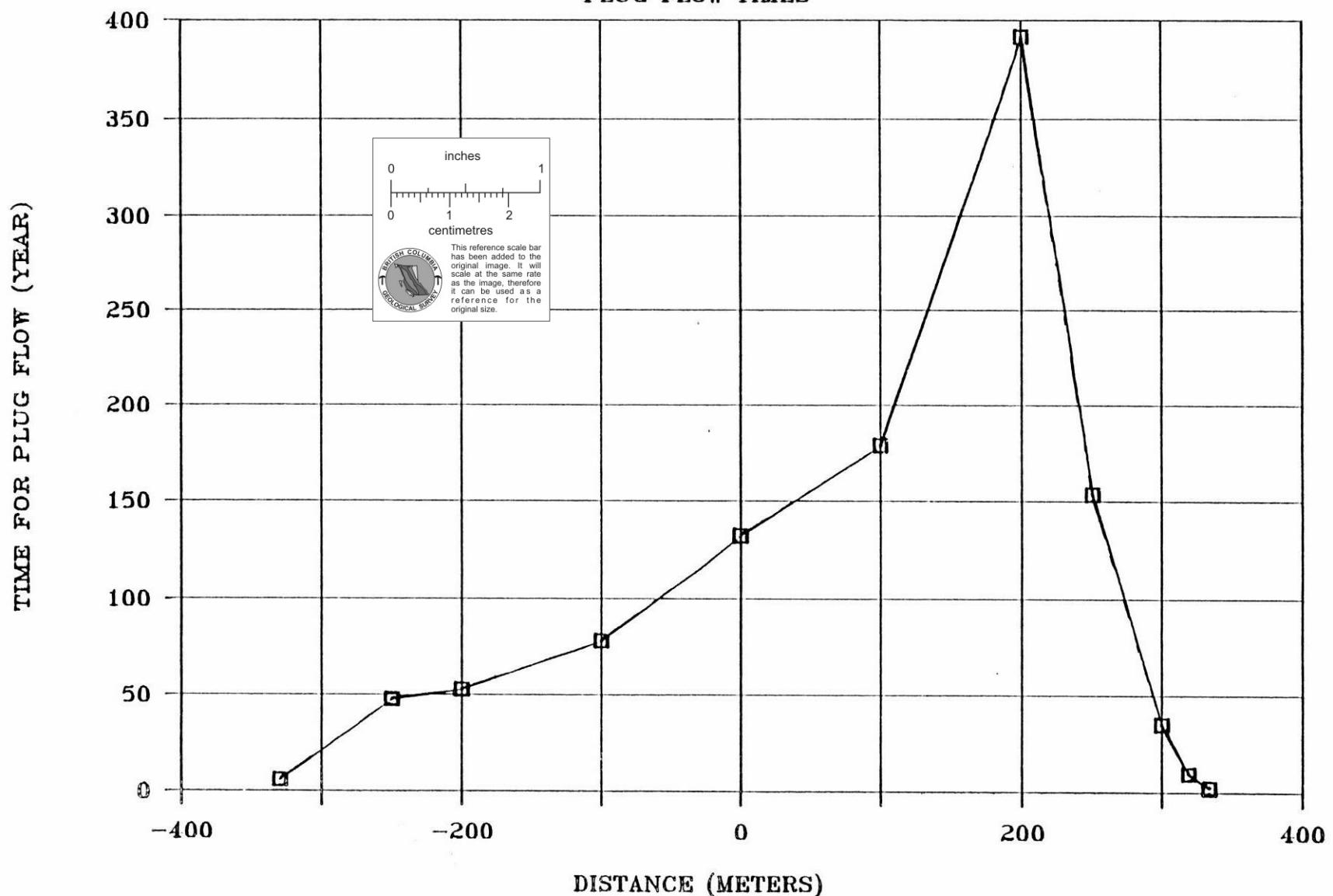
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## SEEPAGE RATE



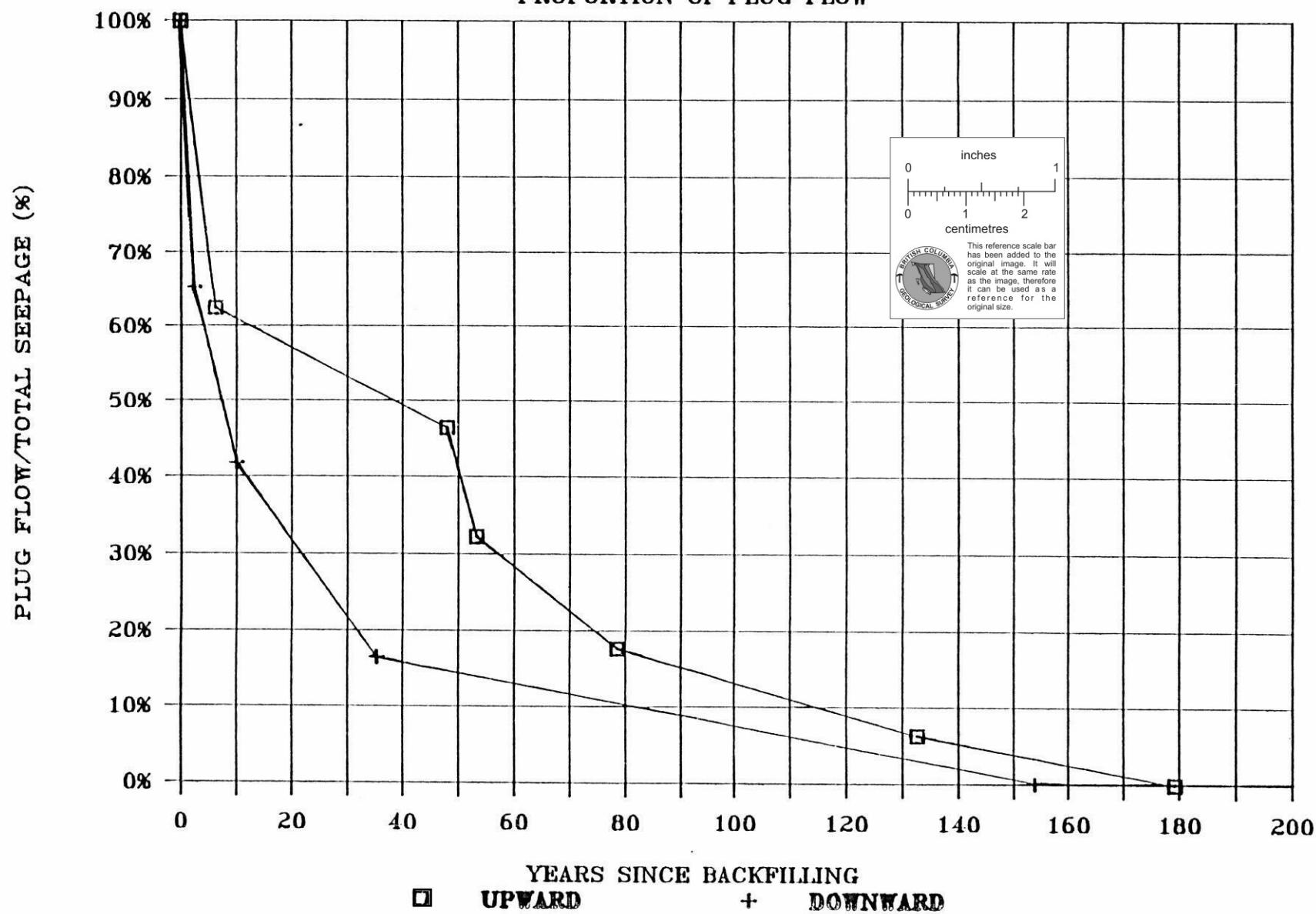
# RECLAIMED PIT SEEPAGE

## PLUG FLOW TIMES



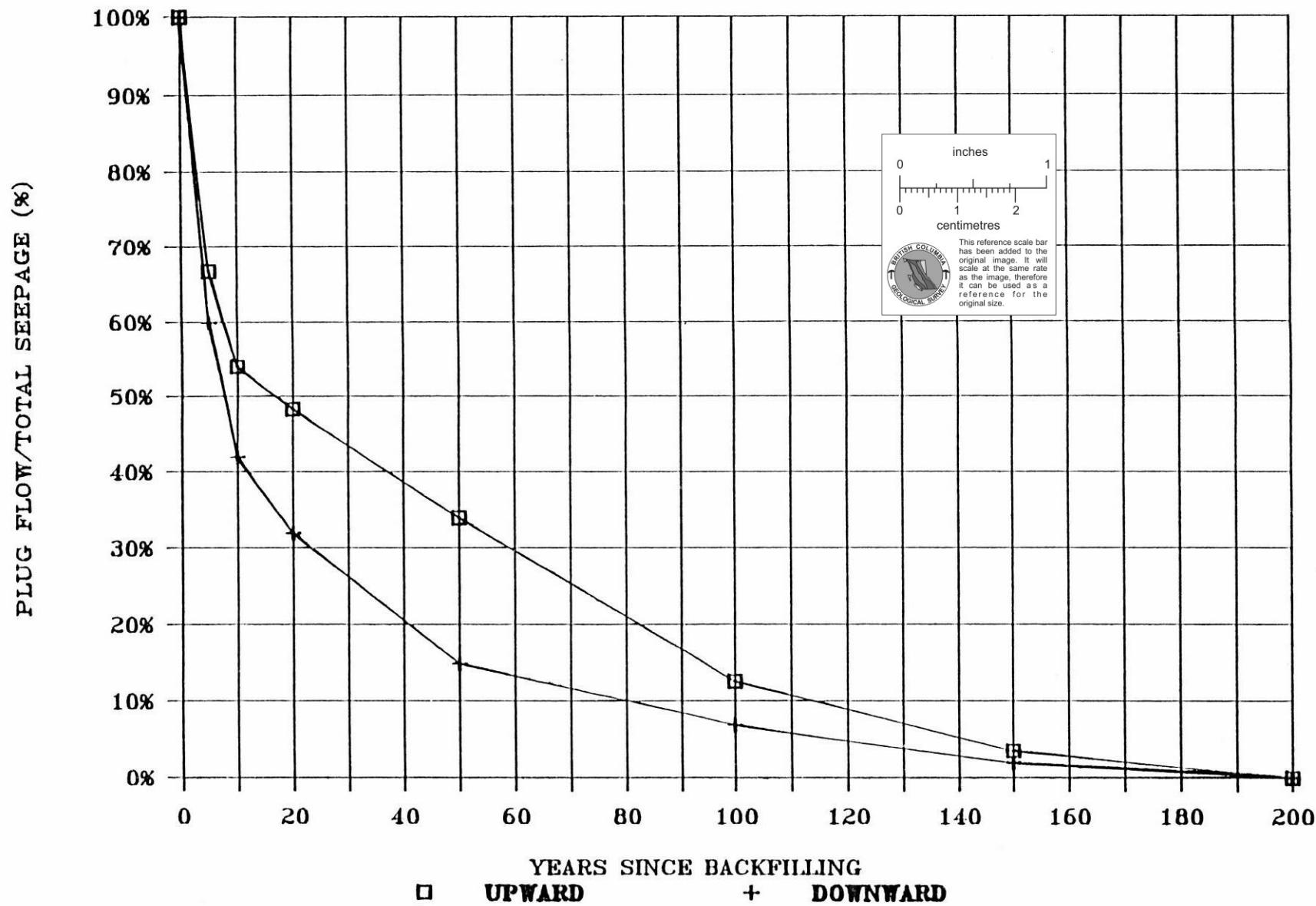
# RECLAIMED PIT SEEPAGE

## PROPORTION OF PLUG FLOW



# RECLAIMED PIT SEEPAGE

## SEEPAGE OVER TIME



**APPENDIX 2.2.3-1**

**RESPONSES TO SUPPLEMENTAL QUESTIONS ABOUT THE**

**GEOHYDROLOGY OF THE PROPOSED CINOLA PIT**

**(Pages 1 to 91)**

REPORT TO  
CITY RESOURCES LIMITED  
ON

RESPONSE TO SUPPLEMENTAL QUESTIONS  
ABOUT THE GEOHYDROLOGY OF THE  
PROPOSED CINOLA PIT

QUEEN CHARLOTTE ISLANDS  
BRITISH COLUMBIA, CANADA

Prepared by

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Denver, Colorado 80209  
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Project 1100  
May 18, 1989

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(303) 399-9630 FAX (303) 399-9701

May 18, 1989

Steffen Robertson and Kirsten Limited  
1030 West Georgia Street, Suite 801  
Vancouver, British Columbia  
Canada, V6E 2Y3

Attention: Mr. John Gadsby, P.E.

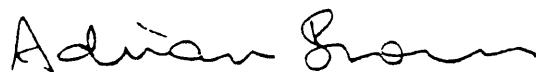
Re: Response to Questions about the Geohydrology of the Proposed  
Cinola Pit

Dear John:

Please find attached our report on the above captioned matter. This report was requested as a result of the meetings with the Provincial and Federal reviewers of this project, which took place in Vancouver on May 5, 1989. Several questions were asked on the behavior of the groundwater system in the vicinity of the proposed pit. These matters have been evaluated by further modeling of the area in and near the pit. This report sets out the results of the evaluations and activities have been performed to address these questions.

I trust that this report meets your needs at this time. Should you have any questions, please do not hesitate to call.

Respectfully submitted,  
ADRIAN BROWN CONSULTANTS INC



Adrian Brown, P.E., President

Att.

TABLE OF CONTENTS

- 1.0 INTRODUCTION
- 2.0 PRE-MINING HEAD/FLOW CONDITIONS INCLUDING ADIT EFFECTS
  - 2.1 AVAILABLE CALIBRATION INFORMATION
  - 2.2 ANALYSIS OF EFFECT OF ADIT
  - 2.3 CONCLUSIONS FROM THE POST-ADIT ANALYSES
- 3.0 EFFECT OF A POSTULATED HIGH CONDUCTIVITY FEATURE
  - 3.1 STATEMENT OF THE QUESTION
  - 3.2 ANALYSES PERFORMED
    - 3.2.1 Flow to the pit
    - 3.2.2 Impact on Barbie Creek
  - 3.3 CONCLUSIONS FROM THE ANALYSIS
- 4.0 PROOF OF ANALYSES AND RESPONSE TO VARIANCES
  - 4.1 METHODS OF CHECKING EVALUATION
  - 4.2 AVAILABLE REMEDIES
    - 4.2.1 Excessive pit inflow
    - 4.2.2 Excessive flow to the water treatment plant
    - 4.2.3 Excessive reduction in stream flow
    - 4.2.4 Excessive impact on stream quality
- 5.0 PARTITIONING OF PRECIPITATION
  - 5.1 CONCEPT
  - 5.2 QUANTITATIVE ESTIMATE OF FLOWS
  - 5.3 BASEFLOW
- 6.0 CROSS SECTIONS IN THE VICINITY OF THE PIT

TABLES

- Table 1 - Measured Water Levels - Proposed Pit Area  
Table 2 - Flow from the Adit

FIGURES

- Figure 1 - Drill Hole Locations - Pit Area  
Figure 2 - Water Levels and Water Table Contours - Pit Area  
Figure 3 - Computer Drawn Water Table Contours - Pit Area  
Figure 4 - Water Table - Standard Conditions with Adit  
Figure 5 - Water Table - High Conductivity Fault with Adit  
Figure 6 - Barbie Creek Baseflow -  $K(fault) = 30$  meters/year  
Figure 7 - Groundwater/Surface Water Concept  
Figure 8 - Groundwater/Surface Water Concept - Quantitative  
Figure 9 - Geological Cross Sections - Cincla Pit Area

1.0 INTRODUCTION

At the groundwater workshop held in Vancouver on May 2, 1989, several questions were asked by the Governmental Review Panel on the behavior of the groundwater system in the vicinity of the proposed pit. Our formulation of these questions were:

1. If the effects of the adit drainage are taken into account, does the computed groundwater table reasonably match the observed current groundwater table for the selected values of the hydraulic conductivity and infiltration?
2. If the Specogna fault and hydrothermal breccia hydraulic conductivity were in fact 30 meters per year, what would be the effect on inflow to the pit, and what would be the effect on the flow in Barbie Creek during and after mining?
3. If the evaluations made in the Phase II report about inflow to the pit, and flow after pit reclamation turn out to be wrong, when would that be identifiable, and what responses would be available to mitigate the effects of the inflow?
4. What is the partitioning of the precipitation that has been used in the analysis, and what is its basis?
5. Could lateral and longitudinal cross sections through the pit be provided, showing the geology and the pre-mining water table?

Responses to these questions have been developed, in part by the performance of further modeling of the area in and near the pit. This report sets out the results of evaluations and activities that we have performed to address these questions.

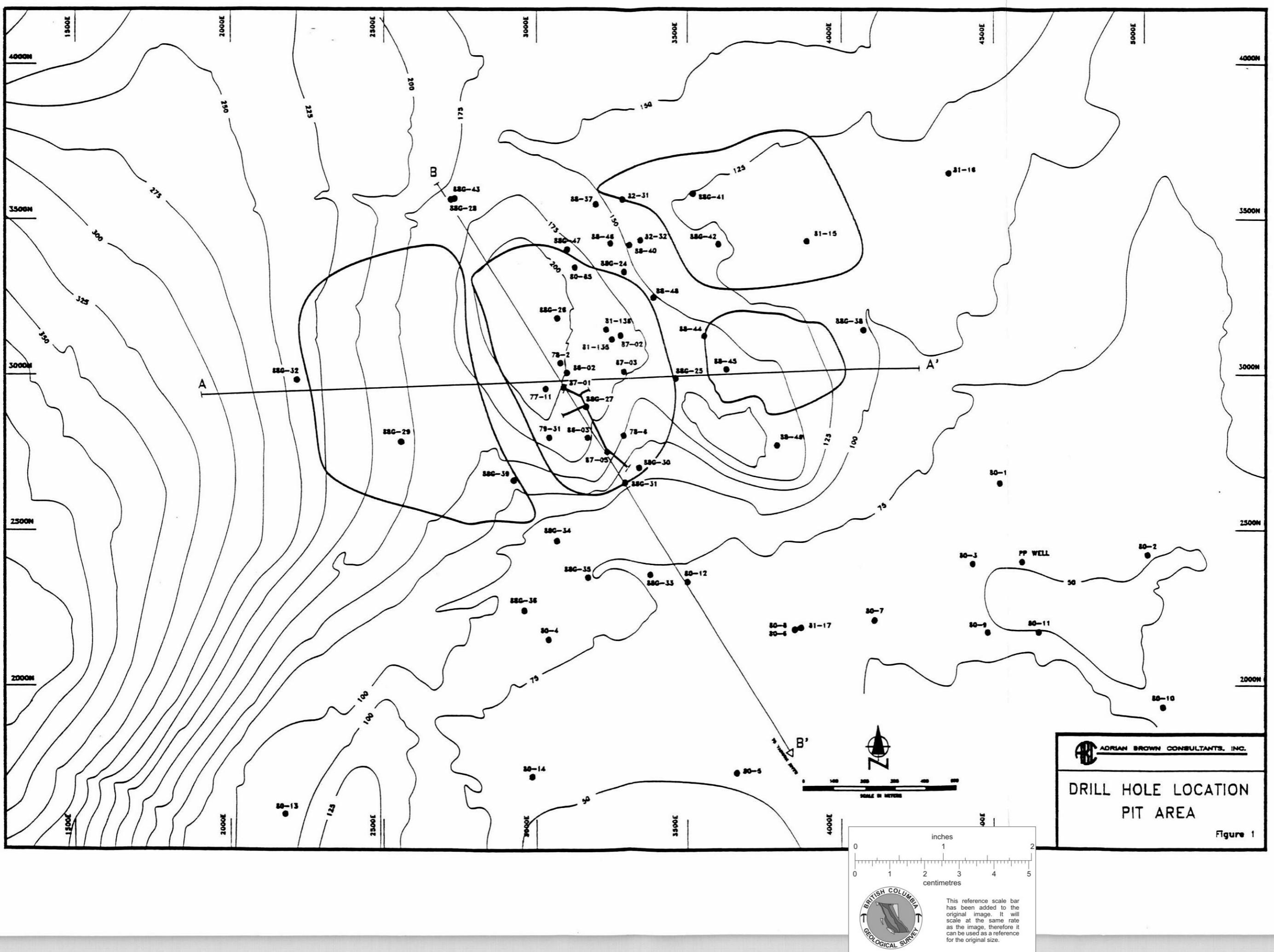
2.0 PRE-MINING HEAD/FLOW CONDITIONS INCLUDING ADIT EFFECTS

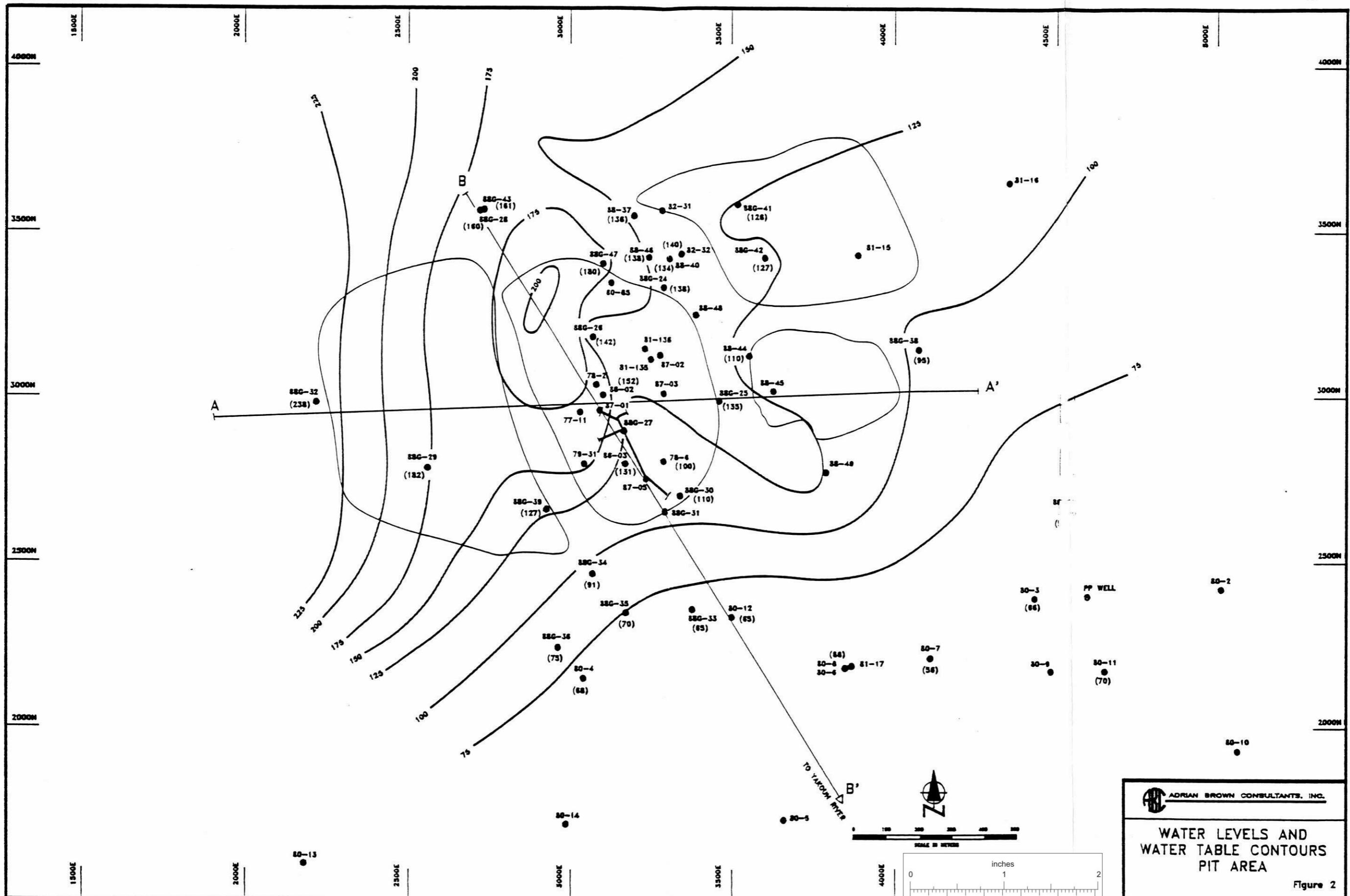
The Cinola exploration adit was installed in 1980, and extended in 1982. The collar elevation is about 117 meters above mean sea level, and the slope of the adit is about 1%. It would be expected to act as a drain in the groundwater system.

2.1 AVAILABLE CALIBRATION INFORMATION

A considerable amount of water level data is available in this area for this period, which allows reasonable calibration. This data has been collected in the drill holes and wells shown in Figure 1. The heads that currently exist in the area are indicated in Figure 2, which shows the values of the water levels used in the evaluation, and the resulting contours of the groundwater table. The raw information used for the preparation of this map are presented in Table 1. To assist in comparisons between computer generated results and the observed values of the groundwater table, a computer drawn version of the water table to the same scale as the computed results has been presented as Figure 3.

In addition, data exists on the flow from the adit: the four measurements are presented in Table 2. Based on these values, the recent flow from the adit appears to have been in the vicinity of about 200 cubic meters per day.

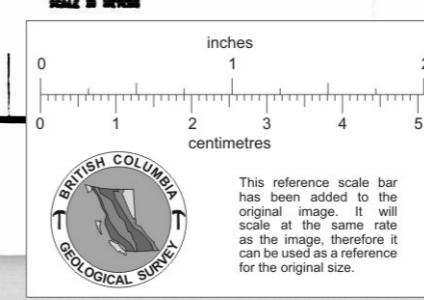




 ADRIAN BROWN CONSULTANTS, INC.

**WATER LEVELS AND  
WATER TABLE CONTOURS  
PIT AREA**

Figure 2



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May 18, 1989

Table 1 - Measured Water Levels in the Vicinity of the Proposed

Pit







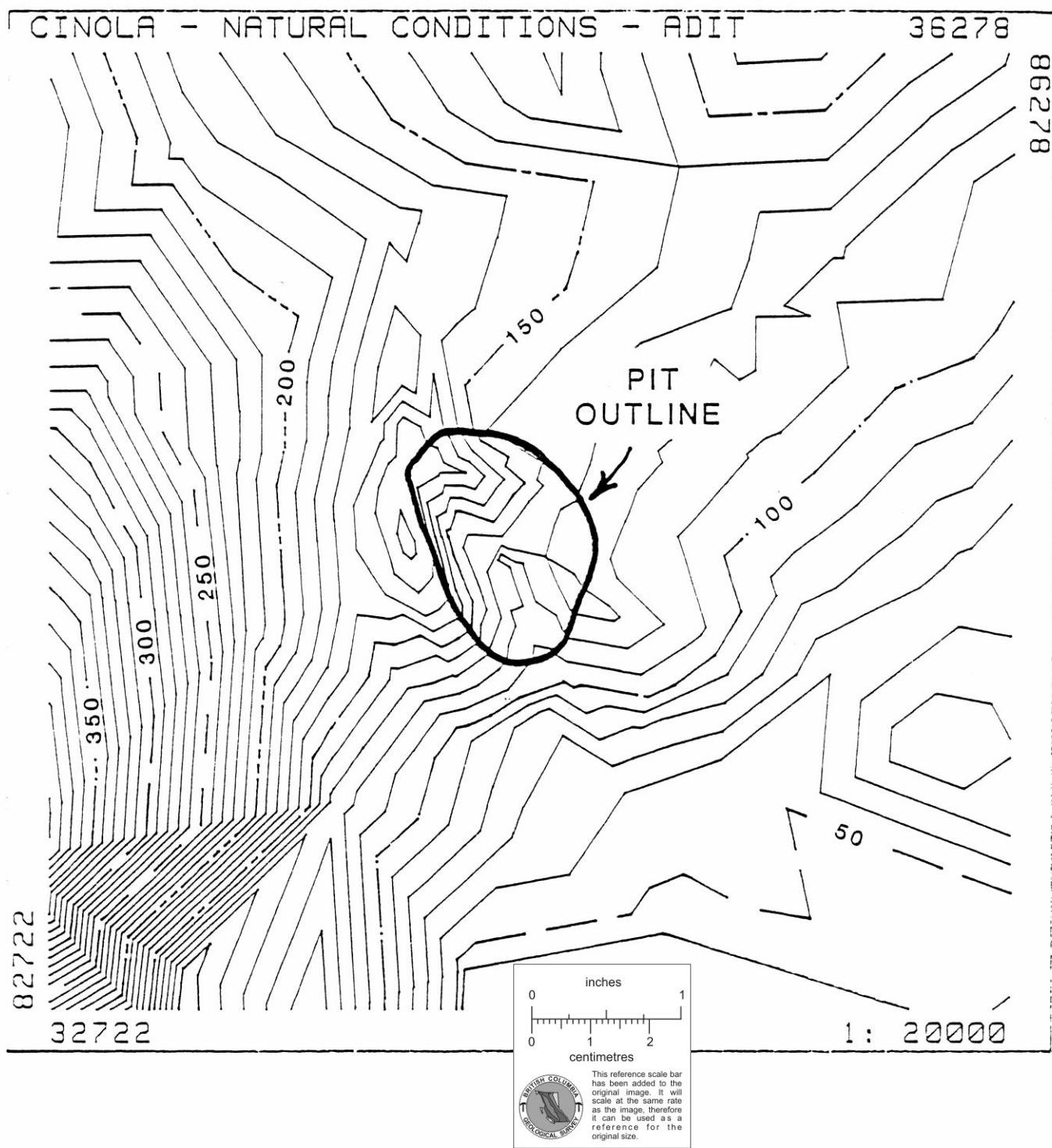


Figure 3 - Computer Drawn Water Table Contours - Pit Area

Table 2 - Flow from the Adit

Date	Adit Length (m)	Flow Rate (cum/d)	Comments
mid 1981	122	130	Flows became steady, vary with precipitation.
mid 1982	457	n/a	Adit extended to essentially its full length. Length includes spurs; actual distance from adit to most remote location is about 360 meters.
Aug 1988	457	97	Variations in flow due to precipitation considerably lower than when adit was shorter.
Nov 1988	457	242	After precipitation; variation with precipitation small.
Jan 1989	457	218	After precipitation.

2.2 ANALYSIS OF EFFECT OF ADIT

An analysis of the head and flow conditions in the vicinity of the pit was performed for the period after the adit had been installed, but prior to the development of the mine. The mesh used was essentially the same as for the aquifer analyses presented in Appendix C of the ABC Geohydrology Report. The mesh was modified to explicitly model the location and head effect of the adit. The results are attached to this report as Exhibit A.

The first analysis was a steady state simulation of the water table using the "standard" hydraulic conductivities for the area (see Appendix C, ABC Geohydrology Report). Specifically, the Specogna Fault and associated hydrothermal breccia was modeled

with an hydraulic conductivity of 6 meters per year, while the altered/silicified Skonun was modeled with an hydraulic conductivity of 1.5 meters per year. The resulting computed water table for the area is presented in Figure 4. It is similar to the measured values, in that the adit is clearly visible in the drawdown system, and the other water levels are higher to both the east and west. The analysis also allows a computation of the flow from the adit under these conditions; the flow was is computed to be 268 cubic meters per day, somewhat above the observed value of about 200 cubic meters per day.

The hydraulic conductivity of the Specogna fault was then raised to 30 meters per year (a sixfold increase) and the analysis re-run. The water table is as portrayed in Figure 5, and is similar to the values obtained in the earlier run. The drawdown around the fault is, however, much more marked, and is not consistent with the observed data. The computed flow from the adit has dropped to 135 cubic meters per year, somewhat below the measured flow from the adit. This drop in flow to the adit is a result of the adit losing the contest with the fault zone for the infiltrating local groundwater.

Accordingly, it would appear that the calibration of the system is best achieved with the Specogna fault at the measured hydraulic conductivity of 6 meters per year, although it is not inconceivable that the effective hydraulic conductivity may be

somewhat greater or less (say between 3 meters per year and 12 meters per year).

### 2.3 CONCLUSIONS FROM THE POST-ADIT ANALYSES

The conclusion of the evaluation is that, if the effects of the adit drainage are taken into account, the computed groundwater table does reasonably match the observed current groundwater table for the selected values of the hydraulic conductivity and infiltration.

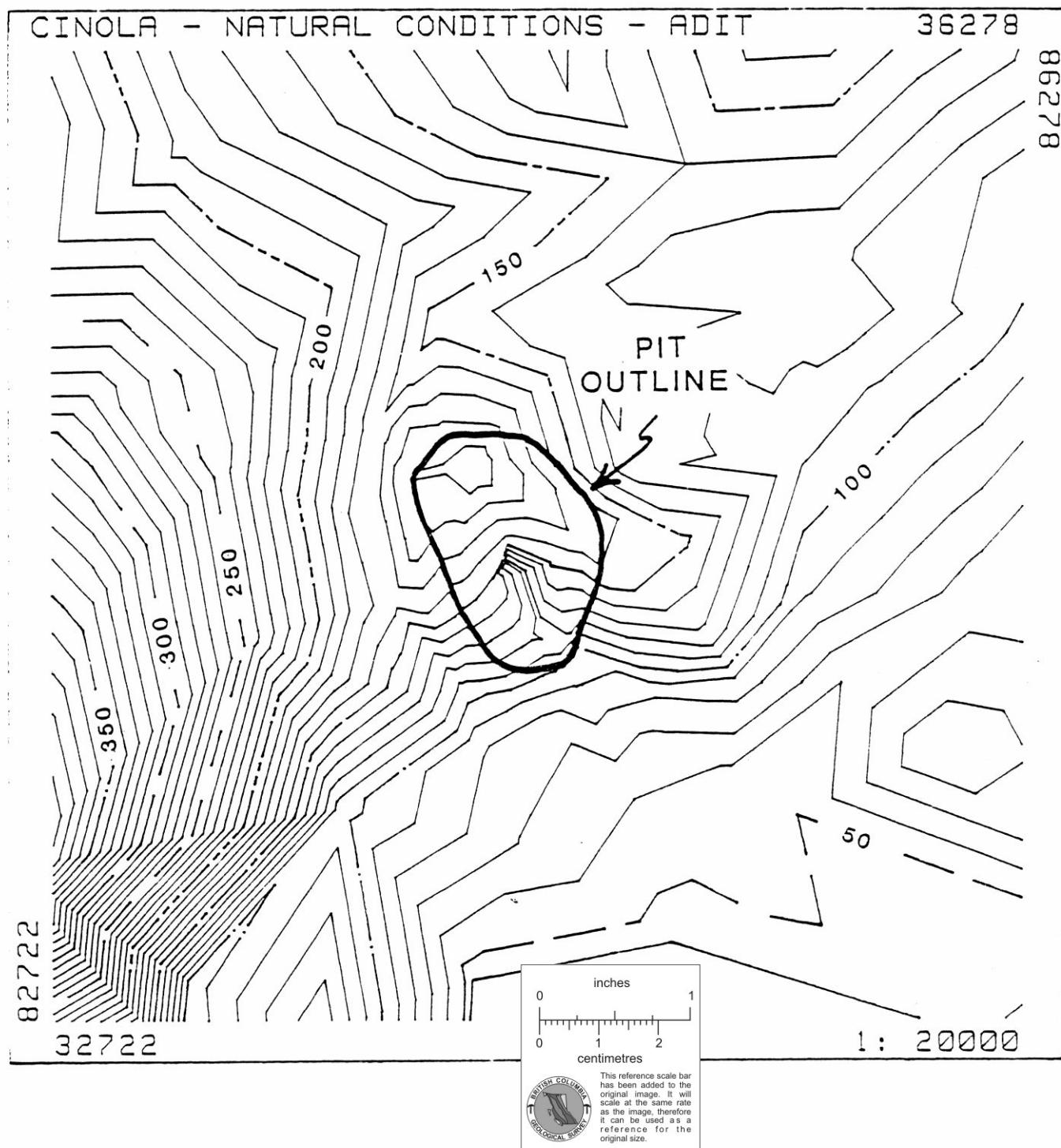


Figure 4 - Water Table - Standard Conditions with Adit Drainage

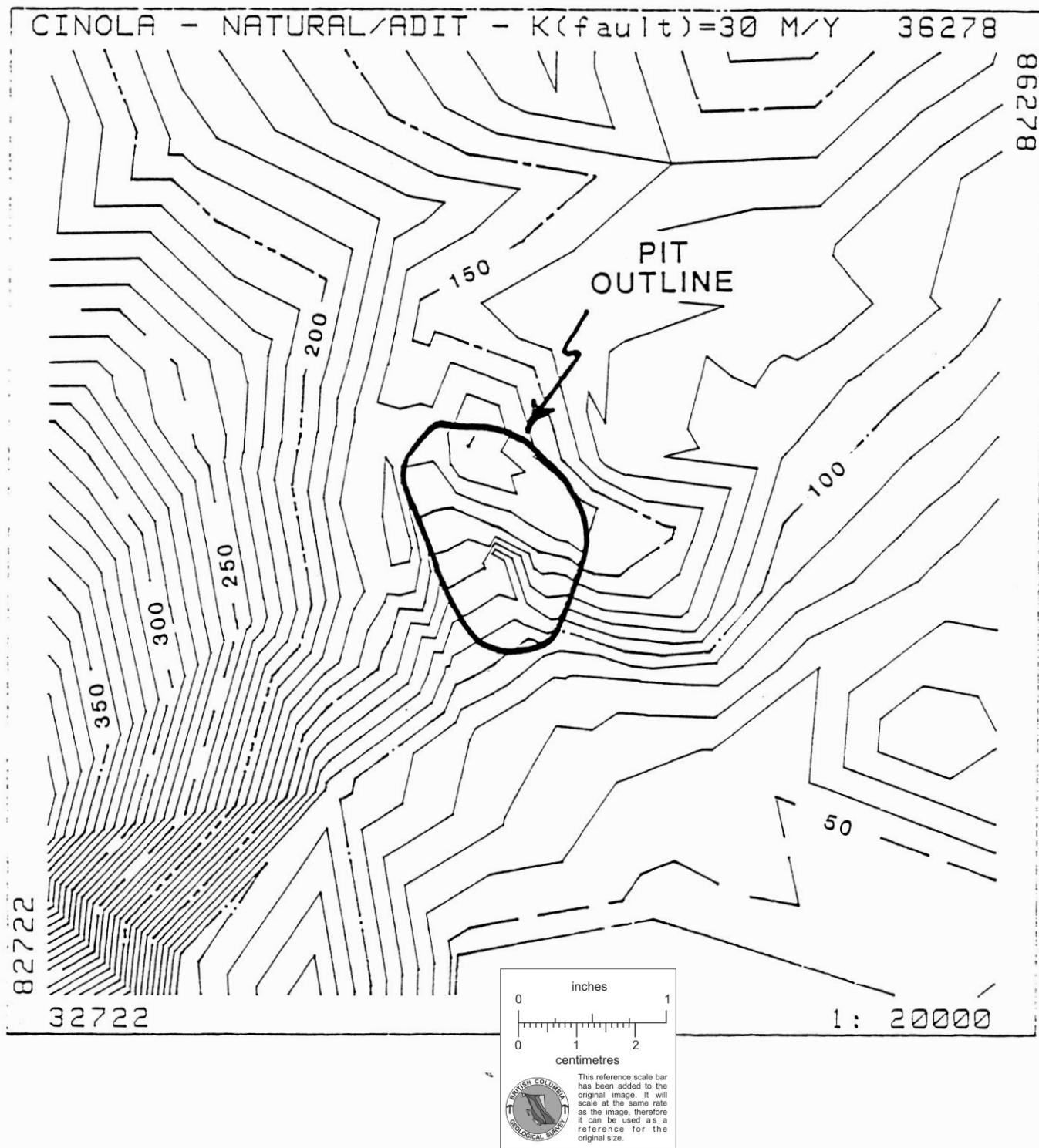


Figure 5 - Water Table - High Conductivity Fault with Adit

Drainage

3.0 EFFECT OF A POSTULATED HIGH CONDUCTIVITY FEATURE3.1 STATEMENT OF THE QUESTION

The representatives of the Governments wished an analysis of the conditions that would exist during mining, and after mine reclamation, if the Specogna Fault proved to have an effective hydraulic conductivity of 30 meters per year, a factor of five higher than the measured value, and of the best value for calibration of the existing heads. The principal concerns appeared to be:

1. the impact on the inflow to the mine, which might, if too high, overwhelm the water treatment plant capacity;
2. the impact on the flow in (particularly) upper Barbie Creek of diversion through such a structure both during operation and after backfilling; and
3. the impact on the flow from the pit backfill to the lower Barbie Creek area after reclamation.

### 3.2 ANALYSES PERFORMED

Two analyses were performed, and the results compared to the standard analyses presented in Appendix C of the ABC Geohydrology Report. These analyses were conducted with the Specogna Fault and associated hydrothermal breccia assumed to have a hydraulic conductivity of 30 meters per year, for the following cases:

1. prior to mining (this analysis has already been presented in Appendix C of the ABC Geohydrology Report);
2. with the mine at full depth; and
3. after reclamation of the pit.

The results of the new analyses are presented in Exhibit B, and are summarized below.

#### 3.2.1 Flow to the pit

The assumption of a high hydraulic conductivity fault/breccia feature increases the flow to the pit when fully mined from 1,300 cubic meters per day for the standard case (ABC Geohydrology Report) to 1,900 cubic meters per day for the high hydraulic conductivity case.

### 3.2.2 Impact on Barbie Creek

The increased hydraulic conductivity results in a diversion of some flow from upper Barbie Creek. The flow in Barbie Creek at the three times analysed (before, during, and after mining) is illustrated on Figure 6. The impact of mining on the flows in Upper Barbie Creek amounts to about a 13% reduction in the baseflow, and after reclamation this impact reduces to about 10%. This level of difference is not detectable in real stream systems, which are subject to far greater daily and seasonal variation.

### 3.3 CONCLUSIONS FROM THE ANALYSIS

The overall conclusion from this evaluation is that, if there is a high hydraulic conductivity through-going feature along the Specogna Fault alignment, then there will be a small computed reduction of the flow in Barbie Creek during and after mining. This reduction is small when compared with the normal variability of the stream flow, and so would not be detectable in the field.

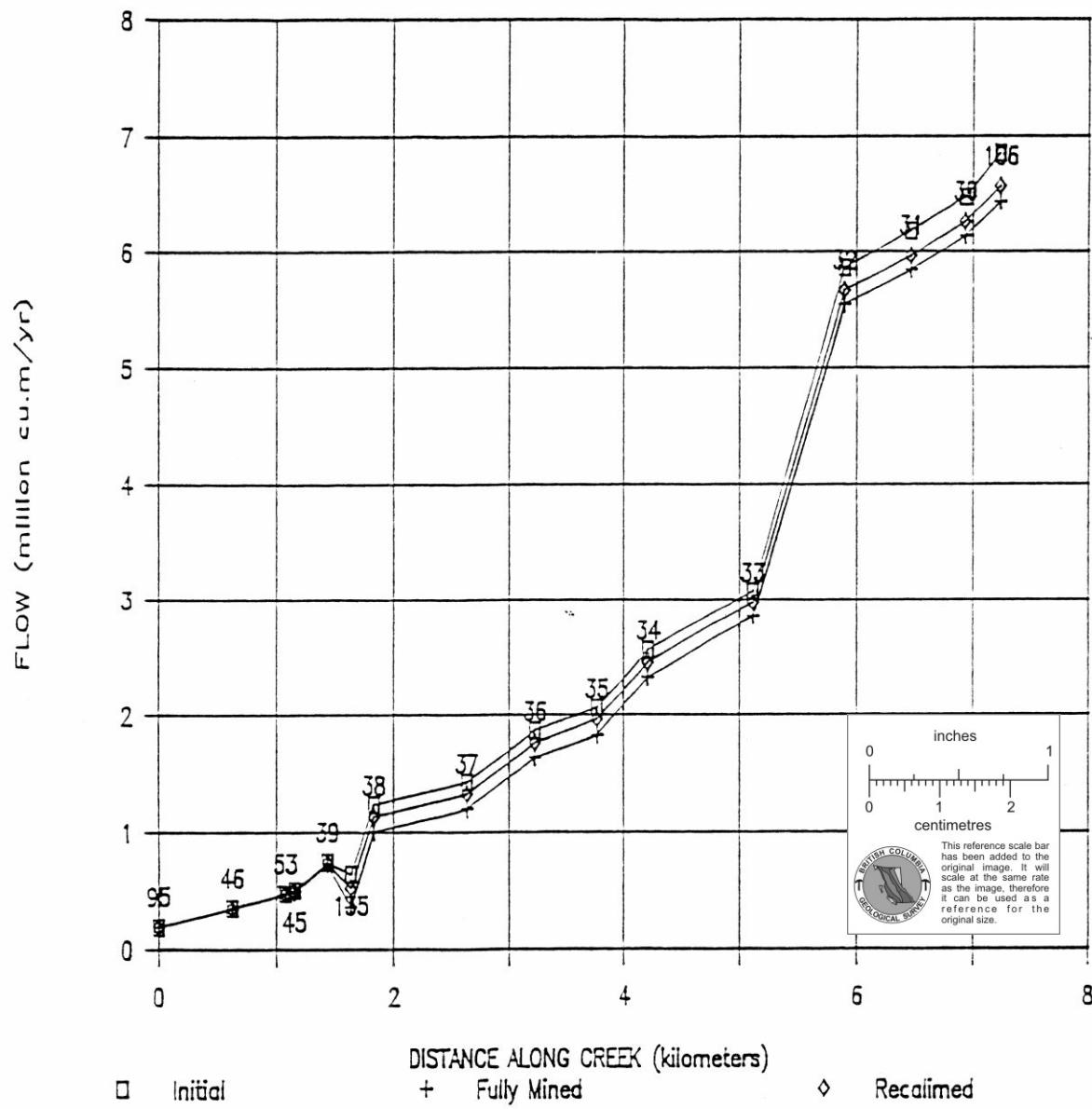


Figure 6 - Barbie Creek Baseflow -  $K(\text{fault}) = 30 \text{ meters/year}$

#### 4.0 PROOF OF ANALYSES AND RESPONSE TO VARIANCES

It is possible that the evaluations made in the Phase II report about inflow to the pit and flow after pit reclamation could be incorrect. This section evaluates the mechanisms that ensure that if this were to be the case, it would be identified in a timely manner, and that there are "fall-back" engineering remedies available for the possible consequences of those unexpected flows. In presenting this section, it is pointed out that this does not reflect a lack of confidence in the predicted ranges of outcomes of the proposed project, but illustrates that the project plan as set out contains within it defense against not only anticipated potential impacts, but also unanticipated impacts.

##### 4.1 METHODS OF CHECKING EVALUATION

There are several methods by which the evaluations presented in the Stage II report, the ABC Geohydrology Report, and this report will be checked during the actual operation of the facility.

These are summarized below:

1. Water Level Monitoring. There are currently a number of completed drill holes in the vicinity of the pit which will be used for monitoring groundwater levels after the pit is constructed. In addition, it is likely that further monitoring holes will be installed during the development of

the pit to evaluate the impact of the pit, and the effectiveness of any slope stabilization or dewatering activities. Accordingly the head predictions of the evaluation will be checked against the expected values throughout the project; remediation could be triggered if operationally significant differences between predicted and actual heads were identified.

2. Mine Inflow Monitoring. Mine inflow will be measured as a routine part of the operation of the project. This is necessary to ensure that pump capacity will be available to remove it from the pit, and that treatment capacity is available for that portion of the inflow that requires quality adjustment prior to use or discharge. These monitored flows will be checked against predictions, and any variance may be the basis for remedial action.
3. Stream Flow Monitoring. The measurement of flow in the streams in the vicinity of the pit will be part of the overall project monitoring program. Any significant reduction of flow will be identified by this program, and the significance of any such observed changes can be evaluated.

Accordingly, it is considered that any geohydrological changes that occur will be identified, and can be compared with the changes contemplated in the pre-mining evaluation studies.

#### 4.2 AVAILABLE REMEDIES

Significant unanticipated changes in pit hydrology flow would need to be evaluated with respect to a number of matters relating to impact. The remedies that are available are discussed below.

##### 4.2.1 Excessive pit inflow

The pit water management system is designed on the basis of a reasonable variation around the predicted flows. If these flows were significantly different, then pit pumping and water treatment plant capacity might need to be modified. The pit pumping system is predicated mainly on the removal from the pit of direct storm precipitation. Groundwater inflow is a small percentage of such flows, and it is not considered credible for this to drive mine dewatering system design or requirements.

##### 4.2.2 Excessive flow to the water treatment plant

The inflow to the pit might, in the worst case, be both of greater quantity and of sufficiently low quality to require treatment prior to discharge. This is considered to be unlikely, as the source of any significantly increased flow would have to be surface water, which is generally of excellent quality, and the flow rate through the rock would have to be high, making it unlikely that quality changes could occur. However if this unlikely circumstance occurred, two remedies appear to be available. First,

the flow quantity requiring treatment could be reduced, by a number of methods including grouting of the (presumably) high hydraulic conductivity flow conduit, channelizing of the portion of the surface streams that would be providing the flow, or dewatering of the flow conduit far enough from the orebody that the water produced would not require treatment. Second, the capacity of the treatment plant, or of the water storage associated with it, could be increased to accommodate the increased flow.

#### 4.2.3 Excessive reduction in stream flow

The principal stream flow of concern with respect to the pit is the flow in upper Barbie Creek, adjacent to the pit. In this location it is understood that the flow is critical for fish habitat and spawning. In the event that the flow to the pit is significantly greater than predicted, the flow in the upper portion of Barbie Creek may be reduced, perhaps significantly in the extreme case. In the event that this were to occur, there are several engineered remedies that would be available, including channelization or sealing of the portion of the stream that overlies the conduit that is providing excessive inflow to pit, grouting of the conduit to the pit, interception of inflow water prior to its entry to the pit and replacement of this water into the stream (from a stream point of view this replacement would only be necessary during critical low flow periods, particularly those that happen to coincide with spawning).

#### 4.2.4 Excessive impact on stream quality

The quality of water in streams might be more negatively impacted than expected if the seepage through the pit backfill after reclamation was either of significantly greater quantity or worse quality than currently expected. The reasons that this might occur, and the remedies that are available, are discussed below

1. Pit backfill material proves to be of much higher hydraulic conductivity than currently expected. If the backfill were highly permeable throughout its mass, it is possible that seepage flows from the pit backfill in excess of the amounts calculated might occur. The permeability of the backfill material will be much better known once the waste rock pile has been built. The hydraulic conductivity of this feature can be ascertained, and the hydraulic conductivity of the backfill estimated. In the event that the hydraulic conductivity is considered to be too high, then the backfill material can be admixed with further excess mudstone. The amount of mudstone in the waste pile is about 5%; if this were raised to 10% the waste rock in the pit would be essentially impermeable.
2. Material to the south of the pit is of much higher hydraulic conductivity than current conditions and field measurements indicate. If the material to the south of the pit were of much higher hydraulic conductivity than the current evaluation suggests, it is possible that the seepage outflow

from the backfilled pit might be significantly greater than expected, which might also create an unexpected negative impact. Monitoring of the flow to the pit and of the impact of mine development on groundwater levels would provide prior indication of this possibility. If this were to occur, then there are several engineering solutions, including lining of the pit face on the south end with mudstone prior to backfilling (to combat the possible presence of high hydraulic conductivity features), and grouting the material to the south of the pit (to reduce inflow during mining, and seepage after reclamation).

3. Water quality in the backfill is more lower than anticipated.

If the quality of the water in the backfill were poor, and the quality of the seepage was not significantly modified by flow through the bedrock, it is possible that the quality of the surface water downgradient from the pit might be unexpectedly impacted. Measurement of quality of flow from the waste pile would provide prior indication of any such a potential problem. If such indications occur, then admixture of more neutralizing material with the pit backfill, to further reduce the potential for future acid drainage, might be indicated.

In summary, if the current predictions of the impact of the pit on the hydrologic system flow and quality prove to be significantly different from the actual conditions, this will be identifiable

May 18, 1989

prior to the completion of the project, at which time available and feasible remedies exist for the rectification of any groundwater-related problems that might occur as a result of the changed conditions.

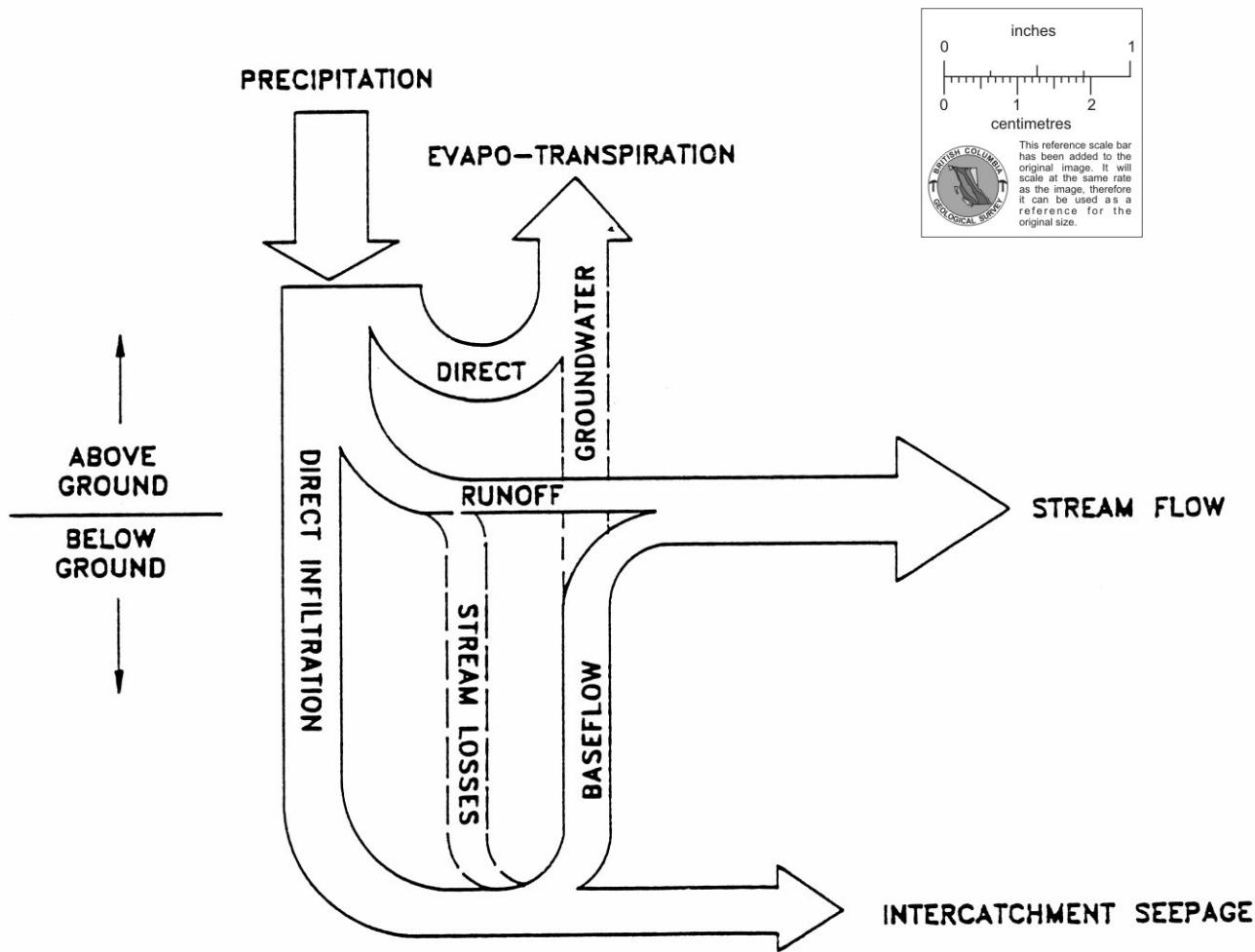
## 5.0 PARTITIONING OF PRECIPITATION

### 5.1 CONCEPT

The evaluations upon which the Stage II report, the ABC Geohydrology Report, and the current report are based in part on the availability of infiltration water to the groundwater system. This section describes the partitioning of incident precipitation that has been used in this study to develop groundwater flows.

Approximately 2.1 meters of (mainly) rain is estimated to fall on the project site each year. The fate of this precipitation is of concern for the entire project, both in terms of project water management, and in terms of the impact of the project on the surface and groundwater resources of the area. The process is illustrated in Figure 7 and comprises the following elements:

1. Precipitation. About 2.1 meters of precipitation falls on the project area, mainly as rain. The precipitation occurs in all months of the year. In the wetter months of October, November, and December, the precipitation rate reaches 300 mm/month (Stage II report). This precipitation is the source of all of the water in the project area.

Figure 7 - Groundwater/Surface Water Concept

2. Runoff. During and after high precipitation events, some of the incident precipitation runs off directly to streams, without entering the groundwater system. In the Queen Charlottes, the dense ground cover and lush growth make direct runoff relatively limited, as the retention capacity of the ground surface is high. Normally, runoff is defined as water that moves to surface water courses without moving below the ground surface. In this project, because of the ground cover, runoff is defined as any water that reaches the streams without entering the groundwater system that is below the root zone of the plants (about 2 meters below ground surface). Because of this definition, runoff is considered in this study to be a residual flow.
3. Direct Evaporation. When the precipitation reaches the ground surface, a portion of it directly evaporates from the leaves of plants, or from the ground surface (swamps, pools, streams, lakes, and other bodies of open water). The amount of evaporation is dependent among other things on the amount of open water, the temperature, humidity, wind velocity, and other factors.
4. Evapotranspiration. Some of the incident precipitation enters the groundwater system. Of that portion, some is captured by the roots of plants and trees, and is evapotranspired as part of the growth cycle. The quantity of water that is evapotranspired by plants is a complex function

of many variables, including temperature, humidity, wind velocity, plant type, soil type, and water availability.

5. Infiltration. The portion of incident precipitation that percolates below the root system of the plant community is described in this study as "infiltration". This water flows in the alluvial and bedrock groundwater system.
6. Baseflow Seepage. The groundwater that flows in the system must ultimately emerge to the surface water system. This seepage emerges at the surface, generally in topographic lows. Upon emerging, this water must once again pass through the root zone, where uptake and evapotranspiration is possible. If direct infiltration is adequate to satisfy this demand, then the seepage emerges at the surface, and either evaporates or flows by runoff to surface streams.
7. Stream Losses. If a stream flows across an area where the groundwater table is below the ground surface, then there will be a tendency for flow in the stream to recharge the groundwater system. The rate at which the stream is depleted in these circumstances depends among other things on the permeability of the streambed and underlying materials, the flow depth and width of the stream, and the depth to the water table.
8. Inter-catchment groundwater flow. Some of the groundwater in the system may flow from one catchment to the next, by

underflowing beneath catchment boundaries. This "deep seepage" would escape the local stream/evapotranspiration system, and represents the extent of unaccounted for flow (if neighboring catchments are unmonitored).

9. Stream Flow. The stream flow is the residual of the precipitation less evaporation/evapotranspiration and less inter-catchment seepage.

The above concept of flow is expressed in steady-state terms. The system has some storage, and in the short term (days to months) the amount of water stored will vary, creating a transient flow source or sink. However in the context of evaluation of a mining project these transients are of short duration, and in the context of the precipitation in the Queen Charlottes, the volumes of water are relatively small.

## 5.2 QUANTITATIVE ESTIMATE OF FLOWS

The system in the project area has been calibrated to establish the most reasonable flow rates for the above partitioning.

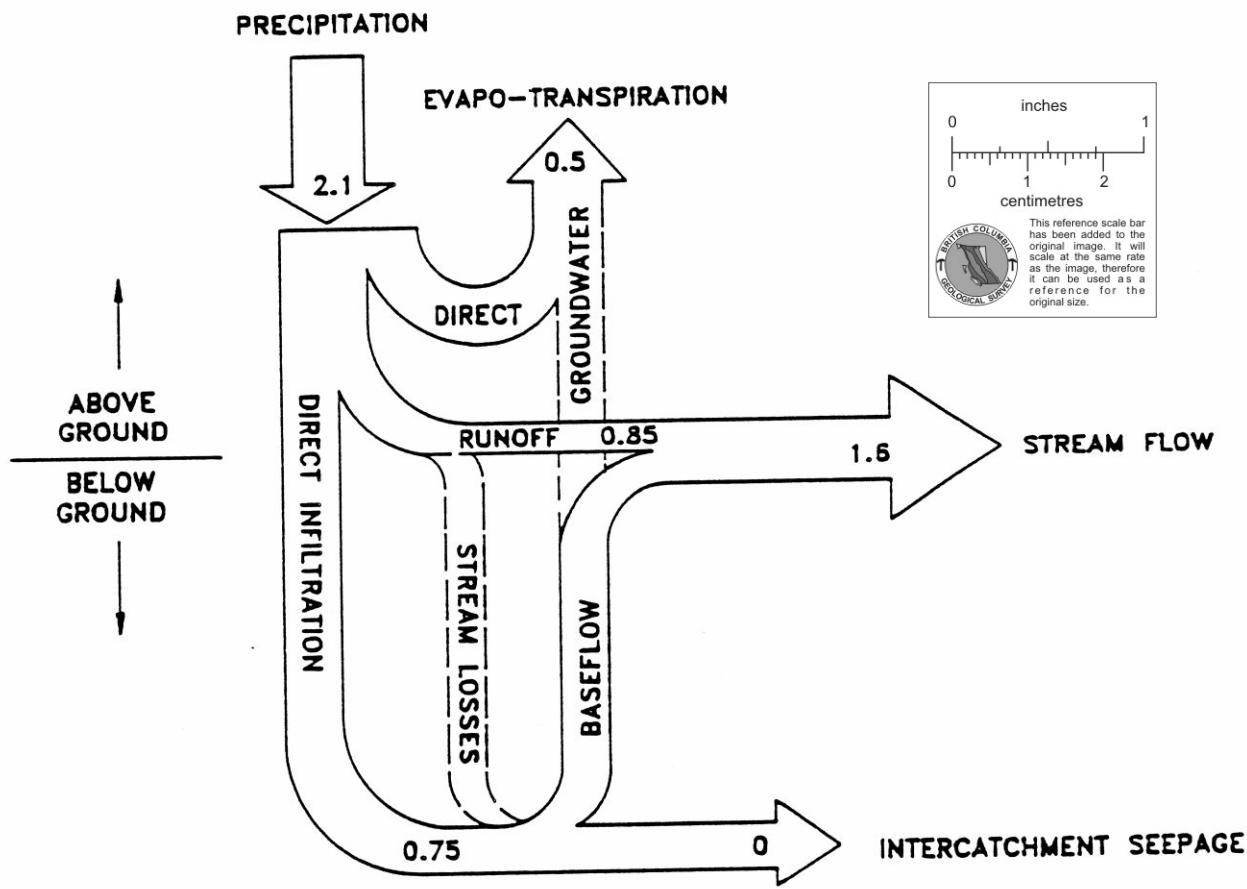
Quantitative values are needed in order to be able to establish the likely impact of the project on groundwater and surface water resources. The above discussion illustrates the complexity of the detailed flow system; the approach taken in the study was to somewhat arbitrarily consider the dividing line between the surface and the groundwater system to be the bottom of the root

zone of the surface plant community. The system was then calibrated by finding the infiltration rate that best matched the observed stream flows and groundwater table.

Calibration of the infiltration was performed by setting up a numerical model of the groundwater system, applying the known topography, geology, hydrogeology, and other information to the model, and computing what average infiltration to the groundwater system is required to create the observed groundwater table over the site area. This activity is reported in detail in the ABC Geohydrology Report (Appendix B). This analysis indicated that the infiltration rate to the groundwater system below the root zone averages about 0.75 meters per year.

In addition to this value, field observations of stream flow indicate that about 65% to 70% of the precipitation that falls ultimately reports to local streams (that is within the catchment area of the streams).

When all these factors are assembled into the conceptual model described above, the typical annual average flows are as indicated in Figure 8. Flows are expressed in volume/unit area of catchment/unit time, and the unit used is meters/year, allowing direct comparison with precipitation.



NOTE - All Flow Rates In Meters/Year

Figure 8 - Groundwater/Surface Water Concept - Quantitative

### 5.3 BASEFLOW

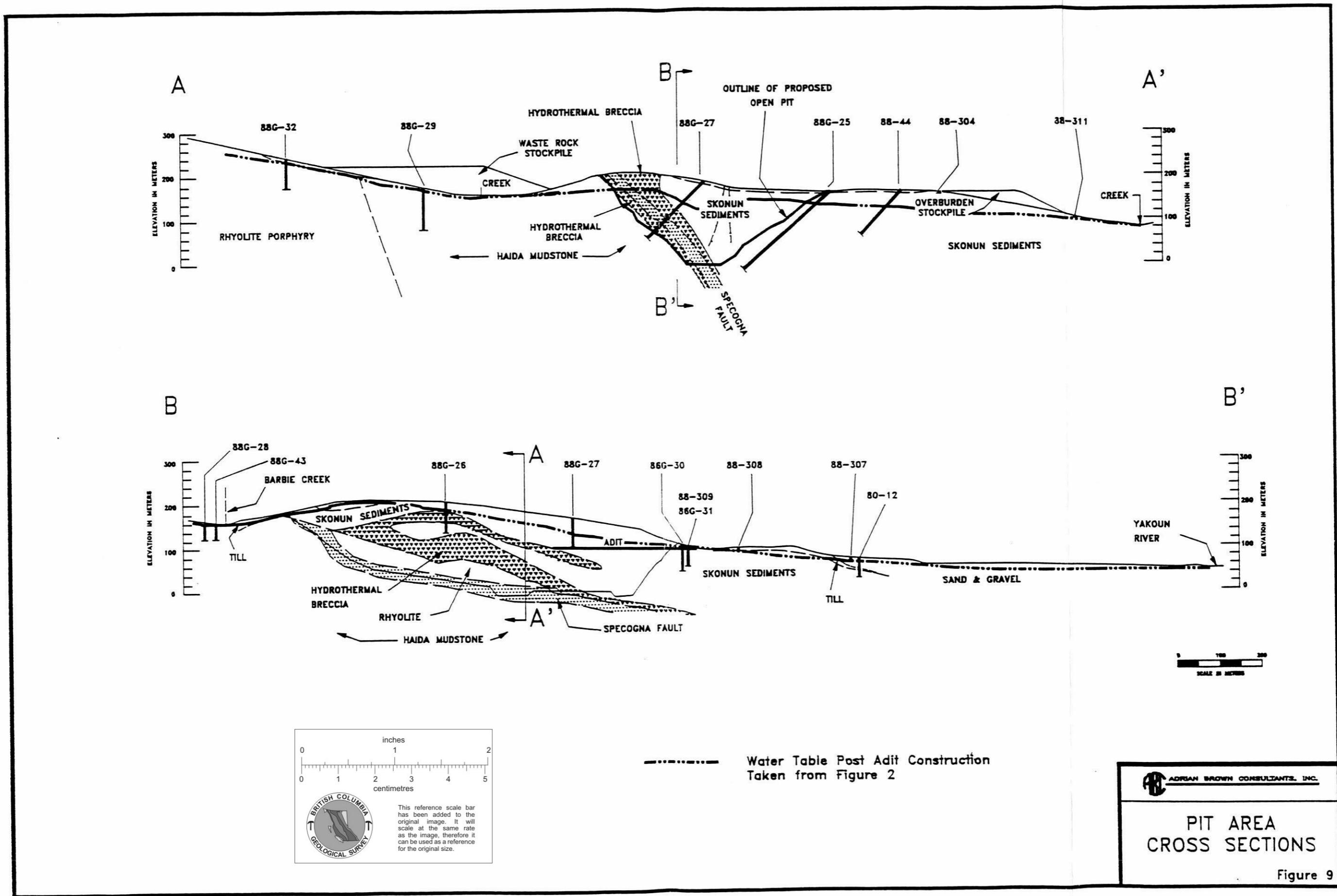
The term "baseflow" has been used in the reports describing the groundwater evaluations in this project. This term is sufficiently difficult as to require some description here. As shown in the above figures, the baseflow is defined in this project as the flow that moves from the groundwater system below the root zone to the surface water system. In surface water hydrology, baseflow is usually reserved for the flow that remains in the streams when all surface runoff has ceased, and is frequently measured as the asymptote of the recession flow curve after a precipitation event. However in the Queen Charlotte Islands context this definition poses a problem. Here, the precipitation rate is sufficiently high that the groundwater table is near the surface over much of the islands, and thus plants on the surface have direct access to the saturated groundwater system. During dry, hot periods, the forest's demand for water exceeds the incident precipitation, and so the plants draw on the groundwater. This has the effect of intercepting the "baseflow", and directly evapotranspiring it. Accordingly, in dry periods it would be expected that the stream flow would be less than the "baseflow".

To overcome these difficulties, baseflow is defined in this study as the streamflow when total evaporation plus evapotranspiration is exactly equal to precipitation.

6.0 CROSS SECTIONS IN THE VICINITY OF THE PIT

Two cross sections through the pit have been developed for this report, and are presented on Figure 9. The locations of the sections are indicated on Figure 1. In each case the post-adit construction, pre-mining groundwater table has been shown on the section. These levels have been taken from the contour plan presented in Figure 2.

The geology information has been developed from detailed information collected during exploration of the orebody, geotechnical drilling for the pit slopes, waste piles, and other structures, and from condemnation drilling outside the orebody limits. The locations of the principal drill holes used for this construction are indicated on the sections, and on Figure 1. For more detail on the geology the reader is directed to the Stage II report.



**EXHIBIT A**

-----KEY ANALYSIS PARAMETERS-----

Number of nodes.....136  
Number of elements.....248  
Number of materials.....5  
Number of soils.....7

-----MATERIAL AND SOIL DATA-----

MATERIAL OR SOIL	HYDRAULIC CONDUCTIVITY [L/T]	SPECIFIC STORAGE [V/L]	SPECIFIC YIELD [-]	DISTRIBUTED INFLOW [L/T]
1	3.00E+00	1.00E-06	.0200	7.50E-01
2	3.00E-01	1.00E-06	.0200	7.50E-02
3	2.00E-00	1.00E-06	.0500	7.50E-01
4	1.50E-00	1.00E-06	.0500	7.50E-01
5	6.00E+00	1.00E-06	.0200	7.50E-01
6				7.50E-01
7				7.50E-01

## -----NODE AND FLOW DATA-----

-NODE DATA-	X-COORD	Y-COORD	BASE-EL	MAX-EL	INIT-W/T	NEW-W/T	BOUN	FIXED-INF	INFILT_INF	STORE_INF	STREAM_INF	OUTFLOW	NODE
---	[L]	[L]	[L]	[L]	[L]	[L]	DARY	[L]/[T]	[L]/[T]	[L]/[T]	[L]/[T]	[L]/[T]	---
1	-1 134	88750.0	39150.0	-290.0	20.0	20.0	20.0 SWMP	0.000E+00	3.481E+05	0.000E+00	2.713E+07	2.771E+07	1
2	1 131	89000.0	37400.0	-290.0	20.0	20.0	20.0 SWMP	0.000E+00	1.015E+06	0.000E+00	2.191E+07	2.317E+07	2
3	2 132	90000.0	36000.0	-275.0	25.0	25.0	25.0 SWMP	0.000E+00	1.220E+06	0.000E+00	1.952E+07	2.093E+07	3
4	3 133	89850.0	34000.0	-275.0	25.0	25.0	25.0 SWMP	0.000E+00	6.966E+05	0.000E+00	1.586E+07	1.678E+07	4
5	4 130	89000.0	31550.0	-270.0	30.0	30.0	30.0 SWMP	0.000E+00	6.703E+05	0.000E+00	1.512E+07	1.604E+07	5
6	5 129	87600.0	32500.0	-265.0	35.0	35.0	35.0 SWMP	0.000E+00	6.165E+05	0.000E+00	1.454E+07	1.536E+07	6
7	6 128	86850.0	32350.0	-265.0	35.0	35.0	35.0 SWMP	0.000E+00	5.719E+05	0.000E+00	1.347E+07	1.405E+07	7
8	7 127	86000.0	32300.0	-260.0	40.0	40.0	40.0 SWMP	0.000E+00	1.420E+05	0.000E+00	1.299E+07	1.352E+07	8
9	8 124	84950.0	33125.0	-255.0	45.0	45.0	45.0 SWMP	0.000E+00	8.513E+04	0.000E+00	6.061E-06	6.223E+06	9
10	9 121	84275.0	33000.0	-255.0	45.0	45.0	45.0 SWMP	0.000E+00	1.257E+05	0.000E+00	4.648E+06	5.059E+06	10
11	10 120	84200.0	31900.0	-250.0	50.0	50.0	50.0 SWMP	0.000E+00	1.226E+05	0.000E+00	4.518E+06	4.801E+06	11
12	11 94	83600.0	32200.0	-250.0	50.0	50.0	50.0 SWMP	0.000E+00	5.222E+05	0.000E+00	4.077E+06	4.672E+06	12
13	12 93	82300.0	31450.0	-245.0	55.0	55.0	55.0 SWMP	0.000E+00	5.044E+05	0.000E+00	2.163E+06	3.051E+06	13
14	13 122	80500.0	30800.0	-240.0	60.0	60.0	60.0 SWMP	0.000E+00	7.658E+05	0.000E+00	0.000E+00	1.061E+06	14
15	22 119	79500.0	32750.0	-370.0	670.0	670.0	670.0 SWMP	0.000E+00	5.819E+05	0.000E+00	0.000E+00	2.733E+05	15
16	27 118	81000.0	34500.0	-95.0	395.0	395.0	395.0 SWMP	0.000E+00	6.400E+05	0.000E+00	0.000E+00	5.342E+05	16
17	16 117	82300.0	36000.0	-25.0	275.0	275.0	275.0 SWMP	0.000E+00	4.347E+05	0.000E+00	0.000E+00	5.131E+05	17
18	24 114	83200.0	37100.0	-150.0	150.0	150.0	150.0 SWMP	0.000E+00	7.562E+05	0.000E+00	5.162E+05	1.082E+06	18
19	23 115	84550.0	38850.0	-180.0	120.0	120.0	120.0 SWMP	0.000E+00	6.294E+05	0.000E+00	0.000E+00	5.940E+05	19
20	-1 116	86200.0	40400.0	-240.0	60.0	60.0	60.0 SWMP	0.000E+00	4.025E+05	0.000E+00	1.212E+07	1.238E+07	20
21	20 113	87000.0	39700.0	-235.0	65.0	65.0	65.0 SWMP	0.000E+00	5.237E+05	0.000E+00	1.176E+07	1.195E+07	21
22	1 112	87900.0	39000.0	-180.0	120.0	120.0	120.0 SWMP	0.000E+00	8.831E+05	0.000E+00	0.000E+00	7.385E+05	22
23	21 111	86000.0	39000.0	-210.0	90.0	90.0	90.0 SWMP	0.000E+00	1.378E+06	0.000E+00	1.036E+07	1.159E+07	23
24	23 110	84400.0	37450.0	-195.0	105.0	105.0	105.0 SWMP	0.000E+00	1.173E+06	0.000E+00	7.150E+06	8.234E+06	24
25	24 109	84600.0	36000.0	-180.0	120.0	120.0	120.0 SWMP	0.000E+00	7.487E+05	0.000E+00	5.215E+06	5.390E+06	25
26	25 108	83325.0	35825.0	-115.0	185.0	185.0	185.0 SWMP	0.000E+00	7.426E+05	0.000E+00	4.333E+06	5.040E+06	26
27	26 107	82200.0	35000.0	-25.0	275.0	275.0	275.0 SWMP	0.000E+00	6.241E+05	0.000E+00	5.286E+06	5.926E+06	27
28	27 104	81700.0	34000.0	65.0	365.0	365.0	365.0 SWMP	0.000E+00	6.200E+05	0.000E+00	5.700E+06	5.305E+06	28
29	28 100	80600.0	32900.0	160.0	460.0	460.0	460.0 SWMP	0.000E+00	5.069E+05	0.000E+00	1.013E+06	1.429E+06	29
30	106 99	85375.0	33550.0	-250.0	50.0	50.0	50.0 SWMP	0.000E+00	2.316E+05	0.000E+00	6.159E+06	6.516E+06	30
31	30 98	85525.0	34000.0	-240.0	60.0	60.0	60.0 SWMP	0.000E+00	1.119E+05	0.000E+00	5.997E+06	6.223E+06	31
32	31 97	86000.0	34300.0	-236.0	64.0	64.0	64.0 SWMP	0.000E+00	3.376E+05	0.000E+00	5.463E+06	5.904E+06	32
33	32 96	86350.0	35000.0	-223.0	77.0	77.0	77.0 SWMP	0.000E+00	3.262E+05	0.000E+00	2.705E+06	3.080E+06	33
34	33 95	86400.0	35900.0	-195.0	105.0	105.0	105.0 SWMP	0.000E+00	4.734E+05	0.000E+00	2.045E+06	2.558E+06	34
35	34 46	86000.0	35700.0	-190.0	110.0	110.0	110.0 SWMP	0.000E+00	1.731E+05	0.000E+00	1.851E+06	2.066E+06	35
36	35 53	85525.0	35450.0	-179.0	121.0	121.0	121.0 SWMP	0.000E+00	2.190E+05	0.000E+00	1.616E+06	1.871E+06	36
37	36 45	84925.0	35400.0	-175.0	125.0	140.0	125.0 SWMP	0.000E+00	1.518E+05	0.000E+00	1.212E+06	1.431E+06	37
38	37 92	84150.0	35225.0	-153.0	145.0	165.0	145.0 SWMP	0.000E+00	9.677E+04	0.000E+00	7.064E+05	1.239E+06	38
39	103 71	83950.0	34675.0	-138.0	162.0	160.0	162.0 SWMP	0.000E+00	5.684E+04	0.000E+00	6.444E+05	7.523E+05	39
40	9 90	84825.0	33600.0	-240.0	60.0	60.0	60.0 SWMP	0.000E+00	4.751E+04	0.000E+00	1.052E+06	1.057E+06	40
41	40 86	84550.0	33850.0	-227.0	73.0	73.0	73.0 SWMP	0.000E+00	1.405E+04	0.000E+00	8.045E+05	9.500E+05	41
42	41 103	84300.0	33775.0	-217.0	91.0	90.0	81.0 SWMP	0.000E+00	6.625E+03	0.000E+00	7.682E+05	6.223E+05	42
43	42 95	84250.0	33775.0	-195.0	105.0	127.0	105.0 SWMP	0.000E+00	1.253E+04	0.000E+00	3.822E+05	4.257E+05	43
44	43 84	84000.0	34275.0	-136.0	164.0	170.0	164.0 SWMP	0.000E+00	2.867E+04	0.000E+00	2.567E+05	3.073E+05	44
45	39 102	83925.0	34600.0	-138.0	162.0	175.0	162.0 SWMP	0.000E+00	2.250E+04	0.000E+00	4.682E+05	5.036E+05	45
46	53 77	83425.0	34725.0	-55.0	245.0	230.0	245.0 SWMP	0.000E+00	1.680E+05	0.000E+00	1.341E+05	1.439E+05	46
47	54 71	83525.0	34150.0	-55.0	245.0	220.0	245.0 SWMP	0.000E+00	2.555E+05	0.000E+00	0.000E+00	1.847E+05	47
48	49 61	83800.0	34025.0	-122.0	178.0	170.0	178.0 SWMP	0.000E+00	3.298E+04	0.000E+00	0.000E+00	7.114E+04	48
49	43 75	84050.0	33975.0	-160.0	140.0	135.0	140.0 SWMP	0.000E+00	2.355E+04	0.000E+00	7.114E+04	9.151E+04	49
50	43 70	84125.0	34225.0	-141.0	159.0	175.0	159.0 SWMP	0.000E+00	7.070E+03	0.000E+00	0.000E+00	7.153E+03	50

-----NODE AND FLOW DATA-----

-NODE DATA-		X-COORD	Y-COORD	BASE-EL	MAX-EL	INIT-W/T	NEW-W/T	BOUN	FIXED-INF	INFILT_INF	STORE_INF	STREAM_INF	OUTFLOW	NODE	
#	LNK	INT	[L]	[L]	[L]	[L]	[L]	DARY	[L/T]	[L/T]	[L/T]	[L/T]	[L/T]	#	
51	44	60	34075.0	34450.0	-115.0	185.0	195.0	185.0	SWMP	0.000E+00	1.251E+04	0.000E+00	4.610E+00	1.152E+04	51
52	39	82	34025.0	34700.0	-115.0	185.0	185.0	185.0	SWMP	0.000E+00	7.375E+03	0.000E+00	1.865E+00	3.064E+03	52
53	45	123	33850.0	34575.0	-130.0	170.0	165.0	170.0	SWMP	0.000E+00	6.664E+04	0.000E+00	3.395E+05	4.725E+05	53
54	44	123	33875.0	34250.0	-124.0	176.0	165.0	176.0	SWMP	0.000E+00	4.422E+04	0.000E+00	1.799E+05	2.615E+05	54
55	39	75	34375.0	34050.0	-171.0	129.0	125.0	125.8	SWMP	0.000E+00	9.891E+03	0.000E+00	0.000E+00	1.551E-01	55
56	45	31	34250.0	34225.0	-120.0	180.0	185.0	172.0	SWMP	0.000E+00	6.867E+03	0.000E+00	0.000E+00	3.556E-01	56
57	51	79	34150.0	34475.0	-96.0	204.0	180.0	198.8	SWMP	0.000E-00	5.109E+03	0.000E+00	3.676E+00	1.064E+00	57
58	52	74	34075.0	34700.0	-94.0	206.0	190.0	199.2	SWMP	0.000E+00	9.772E-03	0.000E+00	0.000E+00	3.094E-01	58
59	135	50	34175.0	34850.0	-98.0	202.0	175.0	187.8	SWMP	0.000E+00	2.358E+04	0.000E+00	0.000E+00	1.384E-01	59
60	82	79	34350.0	34850.0	-117.0	183.0	140.0	163.0	SWMP	0.000E+00	4.378E+04	0.000E+00	1.605E-01	2.749E+04	60
61	83	73	34600.0	34725.0	-146.0	154.0	135.0	154.0	SWMP	0.000E+00	3.353E+04	0.000E+00	5.582E+02	5.710E-04	61
62	83	66	34700.0	34575.0	-135.0	165.0	127.0	164.7	SWMP	0.000E+00	2.306E-04	0.000E+00	0.000E+00	9.000E-00	62
63	64	93	34725.0	34375.0	-130.0	170.0	122.0	162.0	SWMP	0.000E+00	3.164E+04	0.000E+00	0.000E+00	9.900E-00	63
64	65	72	34650.0	34250.0	-170.0	130.0	135.0	130.0	SWMP	0.000E+00	1.188E+04	0.000E+00	3.513E+03	5.212E+04	64
65	37	67	34625.0	34125.0	-200.0	100.0	120.0	100.0	SWMP	0.000E+00	1.469E+04	0.000E+00	2.603E+04	1.097E+05	65
66	88	136	34550.0	34050.0	-195.0	105.0	105.0	105.0	SWMP	0.000E+00	9.766E+03	0.000E+00	9.409E-01	4.762E-03	66
67	43	93	34300.0	34250.0	-110.0	190.0	150.0	171.8	SWMP	0.000E+00	1.172E+04	0.000E+00	0.000E+00	1.400E-00	67
68	57	57	34225.0	34475.0	-83.0	217.0	145.0	198.2	SWMP	0.000E+00	1.453E+04	0.000E+00	0.000E+00	2.212E+00	68
69	136	51	34175.0	34725.0	-95.0	215.0	185.0	200.0	SWMP	0.000E+00	1.102E+04	0.000E+00	0.000E+00	4.416E-01	69
70	60	67	34300.0	34750.0	-96.0	204.0	160.0	198.8	SWMP	0.000E+00	1.367E+04	0.000E+00	2.007E-01	1.063E-01	70
71	61	63	34575.0	34650.0	-130.0	170.0	135.0	170.0	SWMP	0.000E+00	1.411E+04	0.000E+00	3.731E-02	1.397E-04	71
72	54	64	34650.0	34475.0	-125.0	175.0	123.0	173.4	SWMP	0.000E+00	1.391E+04	0.000E+00	0.000E+00	0.000E+00	72
73	66	65	34475.0	34150.0	-145.0	155.0	115.0	136.6	SWMP	0.000E+00	1.313E+04	0.000E+00	0.000E+00	2.541E-01	73
74	80	87	34350.0	34350.0	-90.0	210.0	130.0	182.5	SWMP	0.000E+00	1.445E+04	0.000E+00	0.000E+00	7.048E-01	74
75	81	105	34250.0	34550.0	-85.0	215.0	145.0	200.8	SWMP	0.000E+00	1.063E+04	0.000E+00	0.000E+00	1.294E-00	75
76	70	62	34275.0	34700.0	-88.0	212.0	180.0	205.7	SWMP	0.000E+00	1.588E+04	0.000E+00	0.000E+00	1.772E-01	76
77	71	83	34490.0	34600.0	-115.0	185.0	140.0	185.0	SWMP	0.000E+00	1.547E+04	0.000E+00	0.000E+00	6.383E-03	77
78	64	126	34550.0	34400.0	-135.0	165.0	130.0	165.0	SWMP	0.000E+00	1.719E+04	0.000E+00	2.108E-01	2.449E-04	78
79	65	101	34600.0	34175.0	-175.0	125.0	122.0	123.2	SWMP	0.000E+00	8.516E-03	0.000E+00	1.227E-01	4.884E-02	79
80	79	59	34500.0	34225.0	-140.0	160.0	110.0	150.0	SWMP	0.000E+00	1.127E+04	0.000E+00	2.871E+00	1.393E-01	80
81	72	58	34400.0	34475.0	-105.0	195.0	140.0	195.0	SWMP	0.000E+00	2.041E+04	0.000E+00	5.405E+00	2.795E+02	81
82	123	52	34600.0	35120.0	-162.0	133.0	140.0	133.0	SWMP	0.000E+00	8.574E+04	0.000E+00	9.849E-02	1.119E-05	82
83	126	37	34800.0	34730.0	-176.0	124.0	125.0	124.0	SWMP	0.000E+00	4.304E+04	0.000E+00	4.310E-04	1.008E-05	83
84	102	135	35000.0	34475.0	-148.0	152.0	110.0	152.0	SWMP	0.000E+00	8.331E+04	0.000E+00	0.000E+00	3.266E+04	84
85	87	38	34775.0	34200.0	-170.0	130.0	132.0	130.0	SWMP	0.000E+00	2.523E+04	0.000E+00	0.000E+00	1.232E+04	85
86	103	37	35075.0	34150.0	-130.0	170.0	112.0	127.7	SWMP	0.000E+00	5.531E+04	0.000E+00	0.000E+00	0.000E+00	86
87	105	36	34900.0	33950.0	-220.0	80.0	105.0	80.0	SWMP	0.000E+00	5.484E+04	0.000E+00	7.722E-04	1.799E-05	87
88	41	35	34625.0	34000.0	-205.0	95.0	105.0	92.7	SWMP	0.000E+00	3.078E+04	0.000E+00	3.607E-01	1.312E-01	88
89	41	34	34425.0	33950.0	-207.0	93.0	110.0	93.0	SWMP	0.000E+00	8.242E+03	0.000E+00	5.770E-01	4.659E+04	89
90	42	33	33825.0	33875.0	-196.0	104.0	126.0	104.0	SWMP	0.000E+00	2.707E+05	0.000E+00	0.000E+00	3.854E+05	90
91	9	32	34450.0	33450.0	-231.0	69.0	69.0	69.0	SWMP	0.000E+00	1.492E+04	0.000E+00	0.000E+00	1.317E+04	91
92	10	31	33750.0	32820.0	-150.0	150.0	150.0	139.1	SWMP	0.000E+00	2.614E+05	0.000E+00	0.000E+00	0.000E+00	92
93	122	30	33325.0	33000.0	-205.0	95.0	95.0	95.0	SWMP	0.000E+00	1.513E+05	0.000E+00	4.760E+05	7.062E+05	93
94	93	106	32700.0	33375.0	134.0	434.0	434.0	434.0	SWMP	0.000E+00	6.724E+05	0.000E+00	2.597E+05	1.902E+05	94
95	46	56	33000.0	34275.0	40.0	340.0	340.0	340.0	SWMP	0.000E+00	2.677E+05	0.000E+00	0.000E+00	1.857E-05	95
96	26	55	33000.0	35000.0	-23.0	277.0	277.0	277.0	SWMP	0.000E+00	3.402E+05	0.000E+00	0.000E+00	2.566E+05	96
97	39	89	33575.0	35100.0	-76.0	224.0	210.0	224.0	SWMP	0.000E+00	1.973E+05	0.000E+00	0.000E+00	1.470E+05	97
98	38	50	34000.0	33575.0	-122.0	178.0	174.0	178.0	SWMP	0.000E+00	2.658E+05	0.000E+00	0.000E+00	1.856E+05	98
99	36	48	35000.0	33750.0	-160.0	140.0	140.0	140.0	SWMP	0.000E+00	2.313E-05	0.000E+00	0.000E+00	1.886E+05	99
100	33	49	36000.0	35250.0	-193.0	107.0	107.0	107.0	SWMP	0.000E+00	1.382E+05	0.000E+00	0.000E+00	1.674E-05	100

-----NODE AND FLOW DATA-----

-NODE DATA-		X-COORD	Y-COORD	BASE-EL	MAX-EL	INIT-W/T	NEW-W/T	BOUN	FIXED-INF	INFILT_INF	STORE_INF	STREAM_INF	OUTFLOW	NODE
#	LNK	INT	[L]	[L]	[L]	[L]	[L]	DARY	[L3/T]	[L3/T]	[L3/T]	[L3/T]	[L3/T]	#
101	32	47	85390.0	34760.0	-189.0	111.0	105.0	111.0 SWMP	0.000E+00	1.314E+05	0.000E+00	5.062E+05	5.341E+05	101
102	31	54	85400.0	34300.0	-209.0	91.0	85.0	91.0 SWMP	0.000E+00	1.155E+05	0.000E+00	3.117E+04	1.572E+05	102
103	105	44	85175.0	34000.0	-214.0	86.0	90.0	86.0 SWMP	0.000E+00	5.563E+04	0.000E+00	-5.633E+05	5.380E+04	103
104	40	43	84875.0	33800.0	-233.0	67.0	77.0	67.0 SWMP	0.000E+00	3.594E+04	0.000E+00	0.000E+00	5.377E+04	104
105	106	42	85150.0	33700.0	-241.0	59.0	59.0	59.0 SWMP	0.000E+00	1.021E+05	0.000E+00	1.970E+05	5.360E+05	105
106	8	41	85350.0	33250.0	-248.0	52.0	52.0	52.0 SWMP	0.000E+00	9.297E+04	0.000E+00	6.781E+06	5.344E+06	106
107	7	40	853825.0	33750.0	-212.0	88.0	88.0	88.0 SWMP	0.000E+00	4.253E+05	0.000E+00	0.000E+00	1.225E+05	107
108	6	22	87000.0	33700.0	-240.0	60.0	60.0	60.0 SWMP	0.000E+00	6.378E+05	0.000E+00	0.000E+00	5.695E+05	108
109	3	19	88500.0	33700.0	-225.0	75.0	75.0	75.0 SWMP	0.000E+00	1.904E+06	0.000E+00	0.000E+00	1.613E+06	109
110	3	17	88250.0	35000.0	-245.0	55.0	55.0	55.0 SWMP	0.000E+00	9.369E+05	0.000E+00	0.000E+00	1.097E+06	110
111	32	18	87000.0	34450.0	-250.0	50.0	50.0	50.0 SWMP	0.000E+00	6.906E+05	0.000E+00	5.886E+05	1.624E+06	111
112	111	16	87000.0	35600.0	-195.0	105.0	105.0	105.0 SWMP	0.000E+00	6.772E+05	0.000E+00	0.000E+00	5.388E+05	112
113	2	15	87950.0	35550.0	-150.0	150.0	150.0	150.0 SWMP	0.000E+00	1.422E+06	0.000E+00	0.000E+00	1.155E+06	113
114	115	29	87000.0	37000.0	-210.0	90.0	90.0	90.0 SWMP	0.000E+00	1.097E+06	0.000E+00	7.398E+05	1.395E+06	114
115	1	23	87200.0	38000.0	-240.0	60.0	60.0	60.0 SWMP	0.000E+00	1.437E+06	0.000E+00	1.395E+06	5.392E+06	115
116	23	27	85700.0	37500.0	-170.0	130.0	130.0	130.0 SWMP	0.000E+00	1.390E+06	0.000E+00	0.000E+00	5.352E+06	116
117	114	23	85450.0	36350.0	-115.0	185.0	185.0	185.0 SWMP	0.000E+00	9.173E+05	0.000E+00	0.000E+00	7.398E+05	117
118	29	25	80900.0	32600.0	265.0	585.0	585.0	585.0 SWMP	0.000E+00	9.844E+05	0.000E+00	0.000E+00	4.400E+04	118
119	13	24	82000.0	32100.0	-150.0	150.0	150.0	150.0 SWMP	0.000E+00	1.092E+06	0.000E+00	0.000E+00	1.489E+06	119
120	94	23	81900.0	33200.0	225.0	525.0	525.0	525.0 SWMP	0.000E+00	5.323E+05	0.000E+00	0.000E+00	1.139E+02	120
121	27	21	82350.0	34200.0	105.0	405.0	405.0	405.0 SWMP	0.000E+00	4.381E+05	0.000E+00	0.000E+00	3.379E+05	121
122	12	20	83300.0	32700.0	-210.0	90.0	90.0	90.0 SWMP	0.000E+00	3.322E+05	0.000E+00	9.624E+05	1.179E+06	122
123	125	14	84680.0	35080.0	-167.0	133.0	135.0	133.0 SWMP	0.000E+00	2.361E+04	0.000E+00	5.372E+04	1.488E+05	123
124	125	13	85090.0	33160.0	-178.0	122.0	122.0	122.0 SWMP	0.000E+00	4.701E+04	0.000E+00	0.000E+00	7.355E+04	124
125	101	12	85230.0	34870.0	-186.0	114.0	114.0	114.0 SWMP	0.000E+00	3.610E+04	0.000E+00	1.945E+05	5.734E+05	125
126	101	11	84810.0	34780.0	-171.0	129.0	124.0	129.0 SWMP	0.000E+00	4.559E+04	0.000E+00	1.886E+05	2.068E+05	126
127	36	10	85180.0	35250.0	-170.0	130.0	130.0	130.0 SWMP	0.000E+00	6.231E+04	0.000E+00	0.000E+00	1.667E+04	127
128	101	7	85350.0	34840.0	-165.0	115.0	110.0	115.0 SWMP	0.000E+00	2.763E+04	0.000E+00	4.841E+04	6.841E+04	128
129	128	8	85420.0	35020.0	-182.0	118.0	115.0	118.0 SWMP	0.000E+00	2.025E+04	0.000E+00	0.000E+00	1.973E+04	129
130	123	7	85350.0	35200.0	-177.0	123.0	110.0	123.0 SWMP	0.000E+00	1.620E+04	0.000E+00	0.000E+00	2.368E+04	130
131	132	6	85500.0	35230.0	-174.0	126.0	118.0	126.0 SWMP	0.000E+00	1.270E+04	0.000E+00	1.895E+04	2.318E+04	131
132	133	5	85580.0	35060.0	-185.0	115.0	110.0	115.0 SWMP	0.000E+00	1.140E+04	0.000E+00	2.318E+04	3.222E+04	132
133	32	4	85740.0	34990.0	-195.0	105.0	100.0	105.0 SWMP	0.000E+00	1.028E+05	0.000E+00	3.222E+04	1.379E+05	133
134	131	3	85540.0	35280.0	-173.0	127.0	110.0	127.0 SWMP	0.000E+00	4.088E+04	0.000E+00	0.000E+00	1.395E+04	134
135	38	2	84050.0	35050.0	-145.0	155.0	150.0	155.0 SWMP	0.000E+00	5.766E+04	0.000E+00	7.411E+05	5.590E+05	135
136	39	1	84060.0	34865.0	-115.0	195.0	185.0	183.5 SWMP	0.000E+00	5.463E+03	0.000E+00	1.400E+00	1.547E+01	136

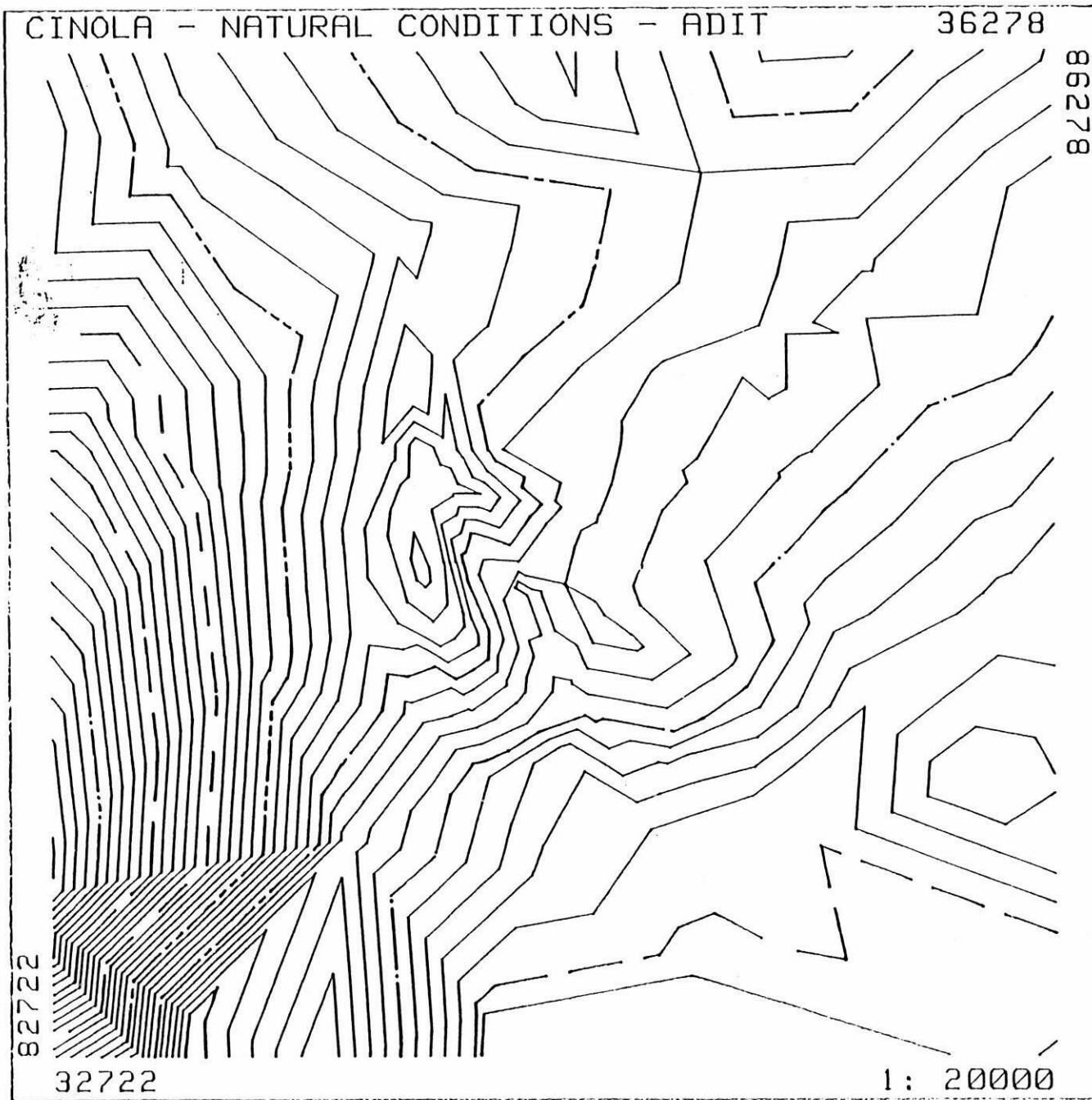
-----SINK FLOW DATA-----

SINK CONN	TOT_FLOW	SINK CONN	TOT_FLOW	SINK CONN	TOT_FLOW	SINK CONN	TOT_FLOW	SINK CONN	TOT_FLOW					
#	#	#	#	#	#	#	#	#	#					
	[L3/T]		[L3/T]		[L3/T]		[L3/T]		[L3/T]					
0	0	0.0000E+00												
1	2	4.0066E+07	2	0	0.0000E+00	3	0	0.0000E+00	4	0	0.0000E+00	5	0	0.0000E+00
6	0	0.0000E+00	7	0	0.0000E+00	8	0	0.0000E+00	9	0	0.0000E+00	10	0	0.0000E+00
11	0	0.0000E+00	12	0	0.0000E+00	13	0	0.0000E+00	14	0	0.0000E+00	15	0	0.0000E+00
16	0	0.0000E+00	17	0	0.0000E+00	18	0	0.0000E+00	19	0	0.0000E+00	20	0	0.0000E+00

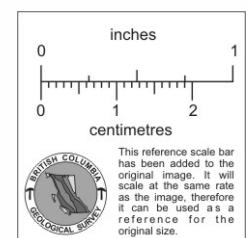
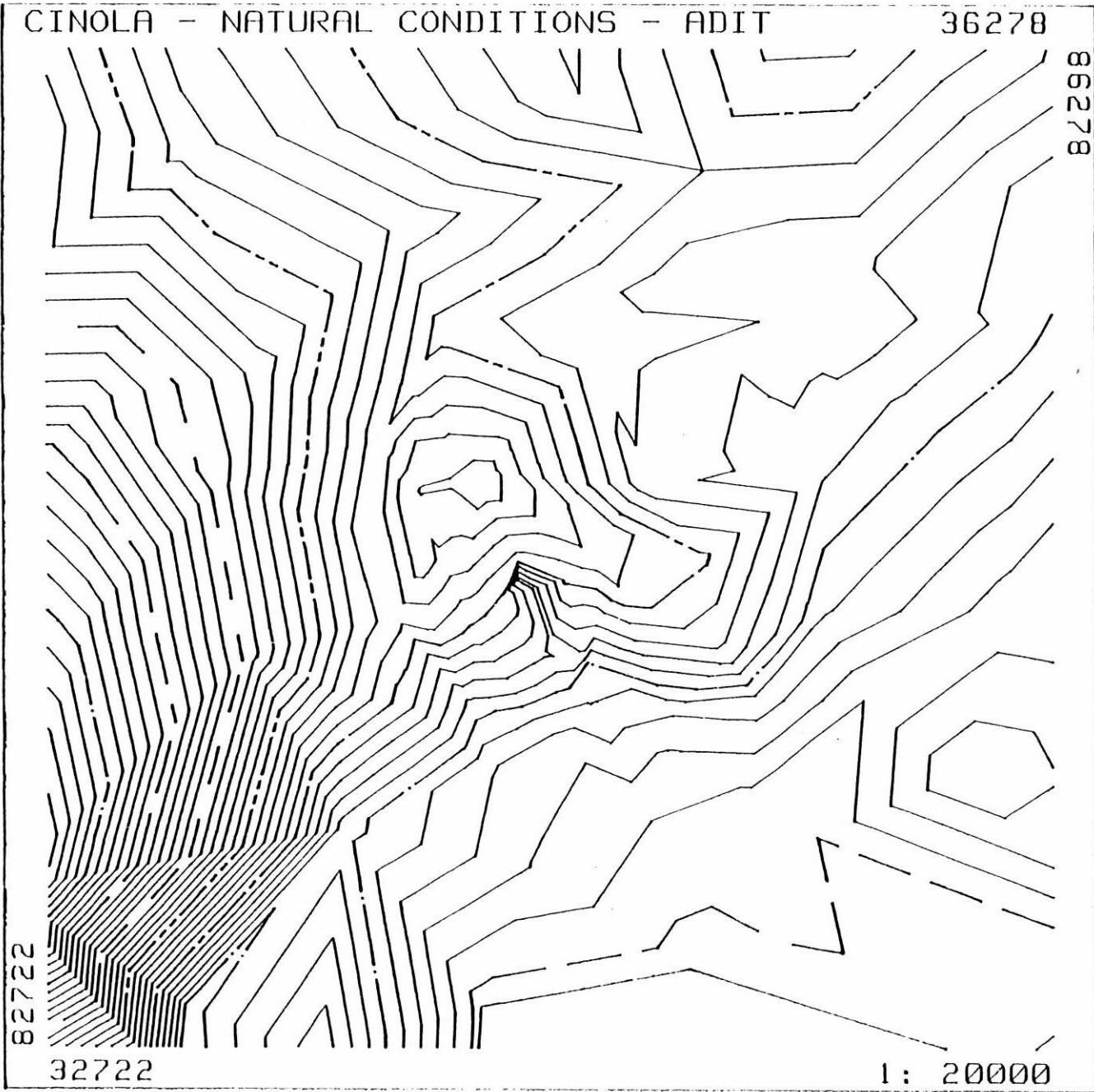
UNITS - Length [L]: meters Time [T]: year

-----ELEMENT DATA-----

-----ELEMENT DATA-----



HEADS  
INITIAL



HEADS  
CURRENT

-----KEY ANALYSIS PARAMETERS-----

Number of nodes.....136  
Number of elements.....252  
Number of materials.....3  
Number of soils.....7

-----MATERIAL AND SOIL DATA-----

MATERIAL OR SOIL	HYDRAULIC CONDUCTIVITY [L/T]	SPECIFIC STORAGE [1/L]	SPECIFIC YIELD [-]	DISTRIBUTED INFLOW [L/T]
1	3.00E+00	1.00E-06	.0200	7.50E-01
2	3.00E-01	1.00E-06	.0200	7.50E-02
3	1.00E+00	1.00E-06	.0500	7.50E-01
4	1.50E+00	1.00E-06	.0500	7.50E-01
5	3.00E-01	1.00E-06	.0200	7.50E-01
6				7.50E-01
7				7.50E-01

## -----NODE AND FLOW DATA-----

-NODE DATA-	X-COORD	Y-COORD	BASE-EL	MAX-EL	INIT-W/T	NEW-H/T	BOUN	FIXED-INF	INFILT_INF	STORE_INF	STREAM_INF	OUTFLOW	NODE
---	[L]	[L]	[L]	[L]	[L]	[L]	DARY	[L3/T]	[L3/T]	[L3/T]	[L3/T]	---	
1	-1 134	98750.0	39150.0	-280.0	20.0	20.0	SWMP	0.000E+00	3.481E+05	0.000E+00	2.708E+07	2.748E+07	1
2	1 131	89000.0	37400.0	-280.0	20.0	20.0	SWMP	0.000E+00	1.015E+06	0.000E+00	2.166E+07	2.295E+07	2
3	2 132	90000.0	36000.0	-275.0	25.0	25.0	SWMP	0.000E+00	1.220E+06	0.000E+00	1.947E+07	2.071E+07	3
4	3 133	89850.0	34000.0	-275.0	25.0	25.0	SWMP	0.000E+00	6.966E+05	0.000E+00	1.581E+07	1.656E+07	4
5	4 130	89000.0	31650.0	-270.0	30.0	30.0	SWMP	0.000E+00	6.703E+05	0.000E+00	1.513E+07	1.581E+07	5
6	5 129	67600.0	32500.0	-265.0	35.0	35.0	SWMP	0.000E+00	6.169E+05	0.000E+00	1.449E+07	1.513E+07	6
7	6 128	86850.0	32950.0	-265.0	35.0	35.0	SWMP	0.000E+00	3.719E+05	0.000E+00	1.342E+07	1.382E+07	7
8	7 127	86000.0	32800.0	-260.0	40.0	40.0	SWMP	0.000E+00	1.420E+05	0.000E+00	1.295E+07	1.310E+07	8
9	8 124	84950.0	33125.0	-255.0	45.0	45.0	SWMP	0.000E+00	8.513E+04	0.000E+00	6.032E+05	6.132E+06	9
10	9 121	84275.0	33000.0	-255.0	45.0	45.0	SWMP	0.000E+00	1.257E+05	0.000E+00	4.648E+05	4.906E+06	10
11	10 120	84200.0	31900.0	-250.0	50.0	50.0	SWMP	0.000E+00	1.228E+05	0.000E+00	4.513E+05	4.648E+06	11
12	11 94	83600.0	32200.0	-250.0	50.0	50.0	SWMP	0.000E+00	3.222E+05	0.000E+00	4.077E+05	4.513E+06	12
13	12 93	82300.0	31450.0	-245.0	55.0	55.0	SWMP	0.000E+00	3.044E+05	0.000E+00	2.163E+05	2.664E+06	13
14	13 122	80500.0	30600.0	-240.0	60.0	60.0	SWMP	0.000E+00	7.656E+05	0.000E+00	0.000E+00	9.150E+05	14
15	29 119	79500.0	32750.0	-70.0	670.0	670.0	SWMP	0.000E+00	5.617E+05	0.000E+00	0.000E+00	4.799E+05	15
16	27 118	81000.0	34500.0	75.0	375.0	375.0	SWMP	0.000E+00	6.400E+05	0.000E+00	0.000E+00	5.600E+05	16
17	18 117	82300.0	36000.0	-25.0	275.0	275.0	SWMP	0.000E+00	4.347E+05	0.000E+00	0.000E+00	3.162E+05	17
18	24 114	83200.0	37100.0	-150.0	150.0	150.0	SWMP	0.000E+00	7.662E+05	0.000E+00	3.162E+05	1.085E+06	18
19	23 115	84550.0	38650.0	-180.0	120.0	120.0	SWMP	0.000E+00	6.294E+05	0.000E+00	0.000E+00	5.940E+05	19
20	-1 116	86200.0	40400.0	-240.0	60.0	60.0	SWMP	0.000E+00	4.025E+05	0.000E+00	1.212E+07	1.254E+07	20
21	20 113	87000.0	39700.0	-235.0	65.0	65.0	SWMP	0.000E+00	3.237E+05	0.000E+00	1.176E+07	1.212E+07	21
22	1 112	87900.0	39000.0	-180.0	120.0	120.0	SWMP	0.000E+00	8.331E+05	0.000E+00	0.000E+00	7.385E+05	22
23	21 111	86000.0	39000.0	-210.0	90.0	90.0	SWMP	0.000E+00	1.378E+06	0.000E+00	1.036E+07	1.176E+07	23
24	23 110	84400.0	37450.0	-195.0	105.0	105.0	SWMP	0.000E+00	1.173E+06	0.000E+00	7.150E+05	8.412E+06	24
25	24 109	84600.0	36000.0	-180.0	120.0	120.0	SWMP	0.000E+00	7.487E+05	0.000E+00	5.215E+05	6.065E+06	25
26	25 108	83325.0	35825.0	-115.0	135.0	135.0	SWMP	0.000E+00	7.425E+05	0.000E+00	4.358E+05	5.215E+06	26
27	26 107	82200.0	35000.0	-25.0	275.0	275.0	SWMP	0.000E+00	6.241E+05	0.000E+00	3.286E+06	4.105E+06	27
28	27 104	81700.0	34000.0	65.0	365.0	365.0	SWMP	0.000E+00	6.200E+05	0.000E+00	1.700E+06	2.452E+06	28
29	28 100	80600.0	32900.0	160.0	460.0	460.0	SWMP	0.000E+00	5.069E+05	0.000E+00	1.013E+06	1.700E+06	29
30	106 99	85375.0	33550.0	-250.0	50.0	50.0	SWMP	0.000E+00	2.315E+05	0.000E+00	6.134E+05	6.426E+06	30
31	30 98	85525.0	34000.0	-240.0	60.0	60.0	SWMP	0.000E+00	1.119E+05	0.000E+00	5.972E+05	6.134E+06	31
32	31 97	86000.0	34300.0	-236.0	64.0	64.0	SWMP	0.000E+00	3.396E+05	0.000E+00	5.439E+05	5.817E+06	32
33	32 96	86350.0	35000.0	-223.0	77.0	77.0	SWMP	0.000E+00	3.262E+05	0.000E+00	2.690E+05	3.045E+06	33
34	33 95	86400.0	35900.0	-195.0	105.0	105.0	SWMP	0.000E+00	4.734E+05	0.000E+00	2.030E+05	2.522E+06	34
35	34 46	86000.0	35700.0	-190.0	110.0	110.0	SWMP	0.000E+00	1.731E+05	0.000E+00	1.836E+05	2.030E+06	35
36	35 53	85525.0	35450.0	-179.0	121.0	121.0	SWMP	0.000E+00	2.190E+05	0.000E+00	1.601E+05	1.836E+06	36
37	36 45	84925.0	35400.0	-175.0	125.0	125.0	SWMP	0.000E+00	1.518E+05	0.000E+00	1.203E+05	1.395E+06	37
38	37 92	84150.0	35225.0	-165.0	145.0	145.0	SWMP	0.000E+00	9.677E+04	0.000E+00	5.874E+05	1.203E+06	38
39	38 91	83950.0	34875.0	-138.0	162.0	162.0	SWMP	0.000E+00	5.624E+04	0.000E+00	5.437E+05	7.400E+05	39
40	39 90	84825.0	35600.0	-240.0	60.0	60.0	SWMP	0.000E+00	4.751E+04	0.000E+00	1.023E+05	1.113E+06	40
41	40 66	84550.0	33850.0	-227.0	73.0	73.0	SWMP	0.000E+00	1.405E+04	0.000E+00	7.315E+05	9.705E+05	41
42	41 103	84300.0	33775.0	-219.0	81.0	81.0	SWMP	0.000E+00	6.625E+03	0.000E+00	7.665E+05	7.777E+05	42
43	42 65	84250.0	33975.0	-195.0	105.0	105.0	SWMP	0.000E+00	1.253E+04	0.000E+00	3.312E+05	3.975E+05	43
44	43 64	84000.0	34275.0	-136.0	164.0	164.0	SWMP	0.000E+00	2.887E+04	0.000E+00	2.557E+05	2.397E+05	44
45	39 102	83925.0	34600.0	-138.0	162.0	162.0	SWMP	0.000E+00	2.250E+04	0.000E+00	4.682E+05	4.976E+05	45
46	53 78	83425.0	34725.0	-85.0	245.0	245.0	SWMP	0.000E+00	1.680E+05	0.000E+00	1.841E+05	3.395E+05	46
47	54 77	83525.0	34150.0	-83.0	245.0	245.0	SWMP	0.000E+00	2.555E+05	0.000E+00	0.000E+00	1.799E+05	47
48	49 71	83800.0	34025.0	-102.0	176.0	176.0	SWMP	0.000E+00	3.299E+04	0.000E+00	0.000E+00	7.114E+04	48
49	43 61	84050.0	33975.0	-160.0	140.0	140.0	SWMP	0.000E+00	2.355E+04	0.000E+00	7.114E+04	3.151E+04	49
50	43 76	84125.0	34225.0	-141.0	159.0	159.0	SWMP	0.000E+00	7.070E+03	0.000E+00	0.000E+00	2.113E+02	50

-----NODE AND FLOW DATA-----

-NODE DATA-		X-COORD	Y-COORD	BASE-EL	MAX-EL	INIT-W/T	NEW-W/T	BOUN	FIXED-INF	INFILT_INF	STORE_INF	STREAM_INF	OUTFLOW	NODE
##	LNK	INT	[L]	[L]	[L]	[L]	[L]	DARY	[L3/T]	[L3/T]	[L3/T]	[L3/T]	[L3/T]	##
51	44	70	34075.0	34450.0	-115.0	185.0	185.0	173.6 SWMP	0.000E+00	1.251E+04	0.000E+00	4.276E+00	8.306E-02	51
52	39	60	34025.0	34700.0	-115.0	185.0	185.0	171.9 SWMP	0.000E+00	7.375E+03	0.000E+00	1.777E+00	5.500E-02	52
53	45	82	33850.0	34575.0	-130.0	170.0	170.0	170.0 SWMP	0.000E+00	6.664E+04	0.000E+00	3.395E+05	4.682E+05	53
54	44	123	33875.0	34250.0	-124.0	176.0	176.0	176.0 SWMP	0.000E+00	4.422E+04	0.000E+00	1.799E+05	2.587E+05	54
55	39	125	34375.0	34050.0	-171.0	129.0	129.0	105.2 SWAO	0.000E+00	2.391E+03	0.000E+00	0.000E+00	5.539E-01	55
56	43	75	34250.0	34225.0	-120.0	180.0	180.0	126.1 SWAO	0.000E+00	6.367E+03	0.000E+00	0.000E+00	3.224E+00	56
57	51	61	34150.0	34475.0	-96.0	204.0	204.0	147.2 SWAO	0.000E+00	5.109E+03	0.000E+00	8.745E+00	4.276E+00	57
58	52	133	34075.0	34700.0	-94.0	206.0	206.0	160.0 SWAO	0.000E+00	9.772E+03	0.000E+00	0.000E+00	1.777E+00	58
59	173	107	34175.0	34850.0	-99.0	202.0	202.0	162.7 SWAO	0.000E+00	2.358E+04	0.000E+00	0.000E+00	1.029E+00	59
60	82	74	34350.0	34850.0	-117.0	183.0	183.0	179.7 SWAO	0.000E+00	4.378E+04	0.000E+00	1.560E-01	3.574E-02	60
61	83	60	34600.0	34725.0	-146.0	154.0	154.0	154.0 SWMP	0.000E+00	3.353E+04	0.000E+00	4.373E-02	3.650E+04	61
62	83	79	34700.0	34575.0	-135.0	165.0	165.0	161.7 SWAO	0.000E+00	2.306E+04	0.000E+00	0.000E+00	1.194E-02	62
63	54	73	34725.0	34375.0	-130.0	170.0	170.0	159.2 SWAO	0.000E+00	5.164E+04	0.000E+00	0.000E+00	7.503E-03	63
64	65	68	34650.0	34250.0	-170.0	130.0	130.0	130.0 SWMP	0.000E+00	1.220E+04	0.000E+00	4.494E-02	1.869E+04	64
65	87	68	34625.0	34125.0	-200.0	100.0	100.0	100.0 SWMP	0.000E+00	1.425E+04	0.000E+00	1.369E+04	7.192E+04	65
66	88	72	34550.0	34050.0	-195.0	105.0	105.0	93.0 SWAP	0.000E+00	9.109E+03	0.000E+00	7.463E-01	2.848E-01	66
67	43	69	34300.0	34250.0	-110.0	190.0	190.0	125.7 SWAP	0.000E+00	1.172E+04	0.000E+00	0.000E+00	5.272E-00	67
68	57	133	34225.0	34475.0	-83.0	217.0	217.0	145.3 SWAO	0.000E+00	1.453E+04	0.000E+00	0.000E+00	8.745E-00	68
69	173	68	34175.0	34725.0	-95.0	215.0	215.0	160.2 SWAO	0.000E+00	1.102E+04	0.000E+00	0.000E+00	2.292E+00	69
70	80	57	34300.0	34775.0	-96.0	204.0	204.0	160.2 SWAO	0.000E+00	1.367E+04	0.000E+00	1.922E-01	1.560E-01	70
71	51	51	34575.0	34650.0	-130.0	170.0	170.0	166.3 SWAO	0.000E+00	1.411E+04	0.000E+00	7.016E-02	4.373E-02	71
72	64	67	34650.0	34475.0	-125.0	175.0	175.0	168.0 SWAO	0.000E+00	1.391E+04	0.000E+00	0.000E+00	1.783E-02	72
73	66	63	34475.0	34150.0	-145.0	155.0	155.0	108.4 SWAO	0.000E+00	1.239E+04	0.000E+00	0.000E+00	7.463E-01	73
74	30	64	34350.0	34350.0	-90.0	210.0	210.0	131.0 SWAP	0.000E+00	1.443E+04	0.000E+00	0.000E+00	2.459E+00	74
75	31	65	34250.0	34550.0	-85.0	215.0	215.0	149.5 SWAO	0.000E+00	1.063E+04	0.000E+00	0.000E+00	5.049E+00	75
76	70	87	34275.0	34700.0	-88.0	212.0	212.0	175.4 SWAO	0.000E+00	1.538E+04	0.000E+00	0.000E+00	1.922E-01	76
77	71	105	34490.0	34600.0	-115.0	185.0	185.0	169.5 SWAO	0.000E+00	1.547E+04	0.000E+00	0.000E+00	9.016E-02	77
78	64	62	34550.0	34400.0	-135.0	165.0	165.0	150.4 SWAP	0.000E+00	1.778E+04	0.000E+00	0.000E+00	1.981E-02	78
79	-2	63	34600.0	34140.0	-175.0	117.0	117.0	117.0 SWMP	0.000E+00	7.969E+03	0.000E+00	7.731E+04	4.927E+04	79
80	79	126	34510.0	34200.0	-140.0	117.0	117.0	117.0 SWMP	0.000E+00	9.556E+03	0.000E+00	6.966E-04	7.731E+04	80
81	138	101	34400.0	34475.0	-105.0	195.0	195.0	147.5 SWAP	0.000E+00	1.597E+04	0.000E+00	5.049E+00	1.417E-01	81
82	123	59	34600.0	35120.0	-162.0	138.0	138.0	138.0 SWMP	0.000E+00	9.674E+04	0.000E+00	9.374E-02	8.302E+04	82
83	126	58	34800.0	34730.0	-176.0	124.0	124.0	124.0 SWMP	0.000E+00	4.304E+04	0.000E+00	5.550E+04	1.782E+05	83
84	102	52	35000.0	34475.0	-148.0	152.0	152.0	152.0 SWMP	0.000E+00	8.331E+04	0.000E+00	0.000E+00	2.976E+04	84
85	37	39	34775.0	34200.0	-170.0	130.0	130.0	130.0 SWMP	0.000E+00	2.523E+04	0.000E+00	0.000E+00	1.054E+04	85
86	103	133	35075.0	34150.0	-130.0	170.0	170.0	125.7 SWAO	0.000E+00	5.531E+04	0.000E+00	0.000E+00	-3.126E-04	86
87	105	56	34900.0	33950.0	-220.0	80.0	80.0	80.0 SWMP	0.000E+00	3.484E+04	0.000E+00	5.246E-04	1.375E+05	87
88	41	77	34625.0	34000.0	-205.0	95.0	95.0	82.3 SWAO	0.000E+00	3.078E+04	0.000E+00	2.348E-01	1.263E-01	88
89	41	53	34425.0	33950.0	-207.0	93.0	93.0	93.0 SWMP	0.000E+00	3.242E+03	0.000E+00	5.539E-01	3.316E+03	89
90	42	55	33825.0	33575.0	-196.0	104.0	104.0	104.0 SWMP	0.000E+00	2.707E+05	0.000E+00	0.000E+00	3.590E+05	90
91	9	54	34450.0	33450.0	-231.0	69.0	69.0	69.0 SWMP	0.000E+00	1.492E+04	0.000E+00	0.000E+00	1.317E+04	91
92	10	53	33750.0	32820.0	-150.0	150.0	150.0	138.2 SWAP	0.000E+00	2.614E+05	0.000E+00	0.000E+00	0.000E+00	92
93	102	52	33325.0	33000.0	-205.0	95.0	95.0	95.0 SWMP	0.000E+00	1.513E+05	0.000E+00	4.950E+05	9.624E+05	93
94	93	51	32700.0	33375.0	134.0	434.0	434.0	434.0 SWMP	0.000E+00	6.724E+05	0.000E+00	2.597E+05	4.760E+05	94
95	46	50	33000.0	34275.0	40.0	340.0	340.0	340.0 SWMP	0.000E+00	2.677E+05	0.000E+00	0.000E+00	1.341E+05	95
96	26	106	33000.0	35000.0	-23.0	277.0	277.0	277.0 SWMP	0.000E+00	3.402E+05	0.000E+00	0.000E+00	2.523E+05	96
97	39	55	33575.0	35100.0	-76.0	224.0	224.0	224.0 SWMP	0.000E+00	1.973E+05	0.000E+00	0.000E+00	1.470E+05	97
98	38	55	34000.0	35575.0	-122.0	178.0	178.0	178.0 SWMP	0.000E+00	2.653E+05	0.000E+00	0.000E+00	7.960E+04	98
99	36	57	35000.0	35750.0	-160.0	140.0	140.0	140.0 SWMP	0.000E+00	2.313E+05	0.000E+00	0.000E+00	1.286E+05	99
100	33	50	36000.0	35250.0	-193.0	107.0	107.0	107.0 SWMP	0.000E+00	1.882E+05	0.000E+00	0.000E+00	1.674E+05	100

**--NODE AND FLOW DATA--**

-NODE	DATA-	X-COORD	Y-COORD	BASE-EL	MAX-EL	INIT-W/T	NEW-W/T	BOUN	FIXED-INF	INFILT_INF	STORE_INF	STREAM_INF	OUTFLW	NODE
##	LNK, INT	[L]	[L]	[L]	[L]	[L]	[L]	DARY	[L3/T]	[L3/T]	[L3/T]	[L3/T]	[L3/T]	##
101	32	48	85370.0	34760.0	-189.0	111.0	111.0	SWMP	0.000E+00	1.314E+05	0.000E+00	4.271E+05	6.326E+05	101
102	31	49	85400.0	34300.0	-209.0	91.0	91.0	SWMP	0.000E+00	1.155E+05	0.000E+00	2.976E+04	1.547E+05	102
103	105	47	85175.0	34000.0	-214.0	86.0	86.0	SWMP	0.000E+00	5.563E+04	0.000E+00	-3.128E+04	6.471E+04	103
104	40	54	84875.0	33800.0	-233.0	67.0	67.0	SWMP	0.000E+00	3.594E+04	0.000E+00	0.000E+00	5.774E+04	104
105	106	44	85150.0	33700.0	-241.0	59.0	59.0	SWMP	0.000E+00	1.021E+05	0.000E+00	2.022E+05	3.145E+05	105
106	3	43	85350.0	33250.0	-248.0	52.0	52.0	SWMP	0.000E+00	9.297E+04	0.000E+00	6.740E+05	6.313E+05	106
107	7	42	85325.0	33750.0	-212.0	88.0	88.0	SWMP	0.000E+00	4.253E+05	0.000E+00	0.000E+00	3.225E+05	107
108	6	41	87000.0	33700.0	-240.0	60.0	60.0	SWMP	0.000E+00	5.873E+03	0.000E+00	0.000E+00	5.873E+03	108
109	5	40	88500.0	33700.0	-225.0	75.0	75.0	SWMP	0.000E+00	1.904E+06	0.000E+00	0.000E+00	1.813E+06	109
110	3	22	88250.0	35000.0	-245.0	55.0	55.0	SWMP	0.000E+00	9.369E+05	0.000E+00	0.000E+00	1.097E+06	110
111	32	19	87000.0	34450.0	-250.0	50.0	50.0	SWMP	0.000E+00	8.706E+05	0.000E+00	6.888E+05	1.624E+06	111
112	111	17	87000.0	35600.0	-195.0	105.0	105.0	SWMP	0.000E+00	6.772E+05	0.000E+00	0.000E+00	6.886E+05	112
113	2	12	87950.0	35550.0	-150.0	150.0	150.0	SWMP	0.000E+00	1.422E+06	0.000E+00	0.000E+00	1.155E+06	113
114	115	15	87000.0	37000.0	-210.0	90.0	90.0	SWMP	0.000E+00	1.097E+06	0.000E+00	7.698E+05	1.895E+06	114
115	1	15	87800.0	36000.0	-240.0	60.0	60.0	SWMP	0.000E+00	1.437E+06	0.000E+00	1.295E+06	3.378E+06	115
116	27	29	85700.0	37500.0	-170.0	130.0	130.0	SWMP	0.000E+00	1.370E+05	0.000E+00	0.000E+00	1.352E+06	116
117	114	23	85450.0	36550.0	-115.0	185.0	185.0	SWMP	0.000E+00	9.173E+05	0.000E+00	0.000E+00	7.698E+05	117
118	29	27	80900.0	32600.0	265.0	565.0	565.0	SWMP	0.000E+00	9.844E+05	0.000E+00	0.000E+00	5.333E+05	118
119	13	26	82000.0	32100.0	-150.0	150.0	150.0	SWMP	0.000E+00	1.092E+06	0.000E+00	0.000E+00	1.248E+06	119
120	94	25	81900.0	33200.0	225.0	525.0	525.0	SWMP	0.000E+00	5.323E+05	0.000E+00	0.000E+00	2.577E+05	120
121	27	24	82350.0	34200.0	105.0	405.0	405.0	SWMP	0.000E+00	4.381E+05	0.000E+00	0.000E+00	2.737E+05	121
122	12	23	83300.0	32700.0	-210.0	90.0	90.0	SWMP	0.000E+00	3.322E+05	0.000E+00	9.524E+05	1.412E+06	122
123	125	21	84680.0	35080.0	-167.0	133.0	133.0	SWMP	0.000E+00	2.361E+04	0.000E+00	3.302E+04	1.199E+05	123
124	125	20	85090.0	35160.0	-178.0	122.0	122.0	SWMP	0.000E+00	4.701E+04	0.000E+00	0.000E+00	7.335E+04	124
125	101	14	85230.0	34870.0	-186.0	114.0	114.0	SWMP	0.000E+00	3.610E+04	0.000E+00	1.938E+05	2.445E+05	125
126	101	13	84810.0	34780.0	-171.0	129.0	129.0	SWMP	0.000E+00	4.559E+04	0.000E+00	1.782E+05	1.842E+05	126
127	36	12	85180.0	35260.0	-170.0	130.0	130.0	SWMP	0.000E+00	6.231E+04	0.000E+00	0.000E+00	1.567E+04	127
128	101	11	85350.0	34840.0	-185.0	115.0	115.0	SWMP	0.000E+00	2.763E+04	0.000E+00	4.841E+04	6.841E+04	128
129	128	10	85420.0	35020.0	-182.0	118.0	118.0	SWMP	0.000E+00	2.025E+04	0.000E+00	0.000E+00	1.973E+04	129
130	128	9	85350.0	35200.0	-177.0	123.0	123.0	SWMP	0.000E+00	1.620E+04	0.000E+00	0.000E+00	2.868E+04	130
131	132	3	85500.0	35230.0	-174.0	126.0	126.0	SWMP	0.000E+00	1.270E+04	0.000E+00	1.395E+04	2.318E+04	131
132	133	7	85580.0	35060.0	-185.0	115.0	115.0	SWMP	0.000E+00	1.140E+04	0.000E+00	2.318E+04	3.122E+04	132
133	32	6	85740.0	34990.0	-195.0	105.0	105.0	SWMP	0.000E+00	1.028E+05	0.000E+00	3.222E+04	1.379E+05	133
134	131	5	85540.0	35280.0	-173.0	127.0	127.0	SWMP	0.000E+00	4.088E+04	0.000E+00	0.000E+00	1.395E+04	134
135	38	4	84050.0	35050.0	-145.0	155.0	155.0	SWMP	0.000E+00	5.766E+04	0.000E+00	7.400E+05	6.078E+05	135
136	39	3	84060.0	34865.0	-115.0	185.0	185.0	SWMP	0.000E+00	5.463E+03	0.000E+00	2.292E+00	9.550E-01	136
137	80	2	84450.0	34370.0	-110.0	117.0	117.0	SWMP	0.000E+00	7.094E+03	0.000E+00	3.477E+04	6.766E-04	137
138	137	1	84400.0	34400.0	-105.0	117.0	117.0	SWMP	0.000E+00	1.433E+03	0.000E+00	1.417E-01	3.477E+04	138

-----SINK FLOW DATA-----

SINK	CONN	TOT_FLOW												
#	#	[L3/T1]												
0	0	0.0000E+00												
1	2	4.0016E+07	2	1	4.3236E-04	3	0	0.0000E+00	4	0	0.0000E+00	5	0	0.0000E+00
6	0	0.0000E+00	7	0	0.0000E+00	8	0	0.0000E+00	9	0	0.0000E+00	10	0	0.0000E+00
11	0	0.0000E+00	12	0	0.0000E+00	13	0	0.0000E+00	14	0	0.0000E+00	15	0	0.0000E+00
16	0	0.0000E+00	17	0	0.0000E+00	18	0	0.0000E+00	19	0	0.0000E+00	20	0	0.0000E+00

-----ELEMENT DATA-----

ELEM	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	ELEM	
Node1	96	27	27	96	28	120	94	120	120	118	118	15	118	118	15	29	16	16	27	17	26	25	98	26	18	18	24	19	20	23	Node1	
Node2	26	121	28	121	120	94	95	119	118	14	15	118	28	120	29	28	28	27	26	26	25	98	26	96	25	24	23	23	22	Node2		
Node3	27	96	121	95	121	121	94	119	119	14	29	29	28	16	16	27	17	17	18	18	25	97	97	24	19	19	20	21	21	Node3		
Mat1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	3	3	1	1	3	3	3	3	Mat1	
Soil	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	3	3	1	1	3	3	3	3	Soil	
ELEM	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60 ELEM		
Node1	23	23	24	116	115	117	116	115	34	114	113	114	112	113	33	112	110	112	111	109	109	109	109	109	109	108	108	108	7	7	3 Node1	
Node2	116	24	117	115	1	114	114	2	114	113	2	34	113	3	112	110	3	113	110	3	110	4	5	6	108	108	7	108	107	7 Node2		
Node3	22	116	116	22	22	116	115	1	117	115	115	112	114	2	34	113	113	111	112	110	111	3	4	5	6	111	9	107	30	30 Node3		
Mat1	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3 Mat1		
Soil	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3 Soil		
ELEM	91	92	93	94	95	96	97	98	99	100	101	102	103	104	105	106	107	108	109	110	111	112	113	114	115	116	117	118	119	120 ELEM		
Node1	3	3	106	106	30	30	107	31	31	103	103	103	103	103	102	102	101	103	32	33	32	107	33	100	133	100	36	99	33	117 Node1		
Node2	30	106	105	30	31	107	32	32	102	105	104	37	86	102	34	101	102	101	33	32	107	106	100	33	100	35	35	76	34	25 Node2		
Node3	106	9	9	105	105	31	31	102	103	31	105	104	37	86	86	84	32	32	100	111	111	111	74	34	134	36	117	117	117	99 Node3		
Mat1	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3 Mat1		
Soil	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3 Soil		
ELEM	91	92	93	94	95	96	97	98	99	100	101	102	103	104	105	106	107	108	109	110	111	112	113	114	115	116	117	118	119	120 ELEM		
Node1	25	22	28	38	62	127	37	127	63	93	93	63	61	60	70	76	76	77	71	71	72	62	63	85	85	85	85	65	64	64	64 Node1	
Node2	98	98	38	82	127	36	58	134	84	62	61	82	82	70	71	71	77	72	62	72	63	63	86	87	65	85	85	63	72	78 Node2		
Node3	99	37	37	37	37	37	37	37	36	101	84	62	61	60	61	61	70	71	71	61	62	62	84	84	63	86	87	64	63	72	78 Node3	
Mat1	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4 Mat1		
Soil	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	4	4	4	4	4	4	4	4	4	4	4	4	4	4 Soil		
ELEM	121	122	123	124	125	126	127	128	129	130	131	132	133	134	135	136	137	138	139	140	141	142	143	144	145	146	147	148	149	150 ELEM		
Node1	78	78	73	78	79	79	79	66	65	88	88	40	40	40	21	91	41	89	89	89	89	89	66	66	73	73	55	55	55	55	55 Node1	
Node2	72	77	81	80	64	65	65	88	88	104	40	105	9	91	40	41	39	43	55	66	88	41	73	79	79	80	74	73	87	56 Node2		
Node3	77	81	137	79	73	54	65	65	87	87	104	104	105	9	41	42	42	42	43	55	66	88	55	73	80	74	67	56	43 Node3			
Mat1	4	4	4	4	4	4	3	3	3	5	3	3	2	2	2	2	2	2	2	2	2	2	5	5	5	5	4	4	4	4 Mat1		
Soil	4	4	4	4	4	4	4	3	3	3	3	3	2	2	2	2	2	2	2	2	2	2	3	3	3	3	2	2	2	2 Soil		
ELEM	151	152	153	154	155	156	157	158	159	160	161	162	163	164	165	166	167	168	169	170	171	172	173	174	175	176	177	178	180 ELEM			
Node1	43	43	44	50	56	56	56	56	56	74	74	74	61	61	73	56	68	68	58	59	70	60	60	135	39	58	58	52	57	51	45 Node1	
Node2	56	50	50	56	57	58	67	67	75	81	80	77	76	76	73	58	69	69	70	60	82	38	39	135	136	39	57	52	52	52 Node2		
Node3	50	44	51	51	51	57	63	74	68	75	137	76	73	69	69	57	58	59	59	59	38	59	136	97	39	52	58	51	45	39 Node3		
Mat1	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	1	2	2	2	2	2	2	2 Mat1		
Soil	2	3	3	2	2	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	3	3	2	1	2	2	2	2 Soil		
ELEM	181	182	183	184	185	186	187	188	189	190	191	192	193	194	195	196	197	198	199	200	201	202	203	204	205	206	207	208	209	210 ELEM		
Node1	135	39	46	45	54	54	44	49	49	41	42	42	91	91	92	93	94	94	94	94	94	94	94	48	48	47	47	47	47	46	97	74 Node1
Node2	98	97	53	39	45	44	51	44	43	40	43	49	42	90	10	11	92	93	90	90	90	49	49	54	54	53	46	95	96	96	122 Node2	
Node3	97	46	39	53	53	45	45	54	44	88	49	90	90	10	9	10	90	90	47	48	48	54	47	53	46	95	94	95	46	93 Node3		
Mat1	1	1	1	2	2	2	2	2	2	2	2	2	2	2	1	1	1	1	1	1	2	2	2	1	1	1	1	1	1	1 Mat1		
Soil	1	1	5	5	5	5	5	5	5	5	5	5	2	2	2	2	2	2	1	1	1	2	2	5	5	5	1	1	1	1 Soil		

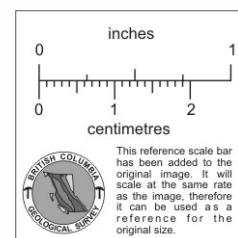
-----ELEMENT DATA-----

CINOLA - ADIT - INITIAL

35166

α  
υ  
η  
δ

$+_{125}$   
 $+_{38} \quad +_{126} \quad +_{59} \quad +_{60}$   
 $+_{78} \quad +_{128}$   
 $+_{52} +_{58} \quad +_{88} \quad +_{78} \quad +_{81} \quad +_{83}$   
 $+_{71}$   
 $+_{45} \quad +_{77} \quad +_{82}$   
 $+_{75}$   
 $+_{51} \quad +_{57} \quad +_{88} \quad +_{81} \quad +_{72} \quad +_{84}$   
 $+_{74} \quad +_{128} \quad +_{127} \quad +_{78} \quad +_{83}$   
 $+_{44} \quad +_{84}$   
 $+_{50} \quad +_{67} \quad +_{80} \quad +_{85}$   
 $+_{73} \quad +_{+}_{65}$   
 $+_{55} \quad +_{88} \quad +_{88}$   
 $+_{48} \quad +_{43} \quad +_{88} \quad +_{87}$



33833

1 : 7500

## NODES NUMBERS

CINOLA - PIT AREA - SPECOGNA

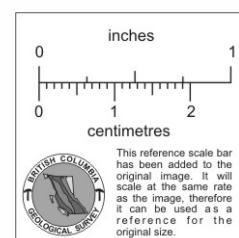
35166

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A complex network graph illustrating connections between various nodes, each labeled with a unique number. The nodes are interconnected by a dense web of lines representing edges. The labels are as follows:

- Top row: 248, 171, 230, 231.
- Second row: 173, 245, 172, 103, 221, 102, 222.
- Third row: 175, 246, 170, 104, 105, 101.
- Fourth row: 180, 176, 168, 106, 107, 109.
- Fifth row: 184, 178, 187, 183, 182, 108, 110.
- Sixth row: 178, 179, 188, 150, 180, 122, 121.
- Seventh row: 187, 186, 185, 158, 182, 109, 111.
- Eighth row: 188, 153, 155, 158, 157, 120, 112.
- Ninth row: 188, 152, 151, 147, 148, 124, 113.
- Tenth row: 202, 189, 150, 148, 149, 125, 114.
- Bottom row: 188, 151, 148, 148, 149, 126, 117.
- Bottom right corner: 115, 114, 113, 73.
- Bottom left corner: 33, 30, 30, 00.

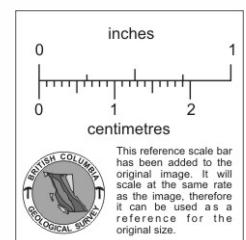
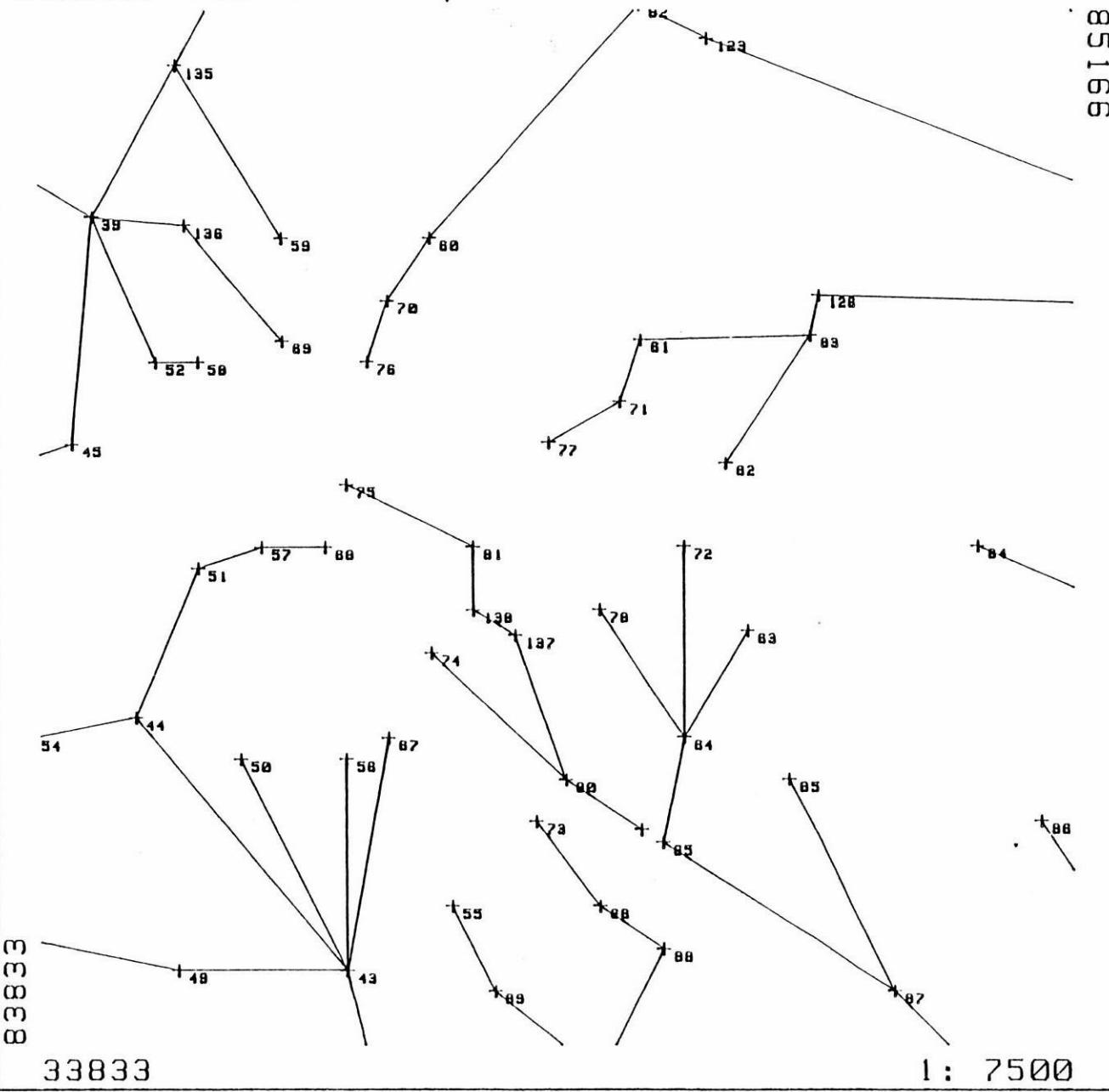
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# ELEMENTS NUMBERS

CINOLA - ADIT - K(Spec)=30 M/Y

35166

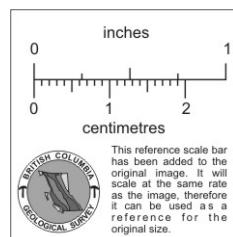
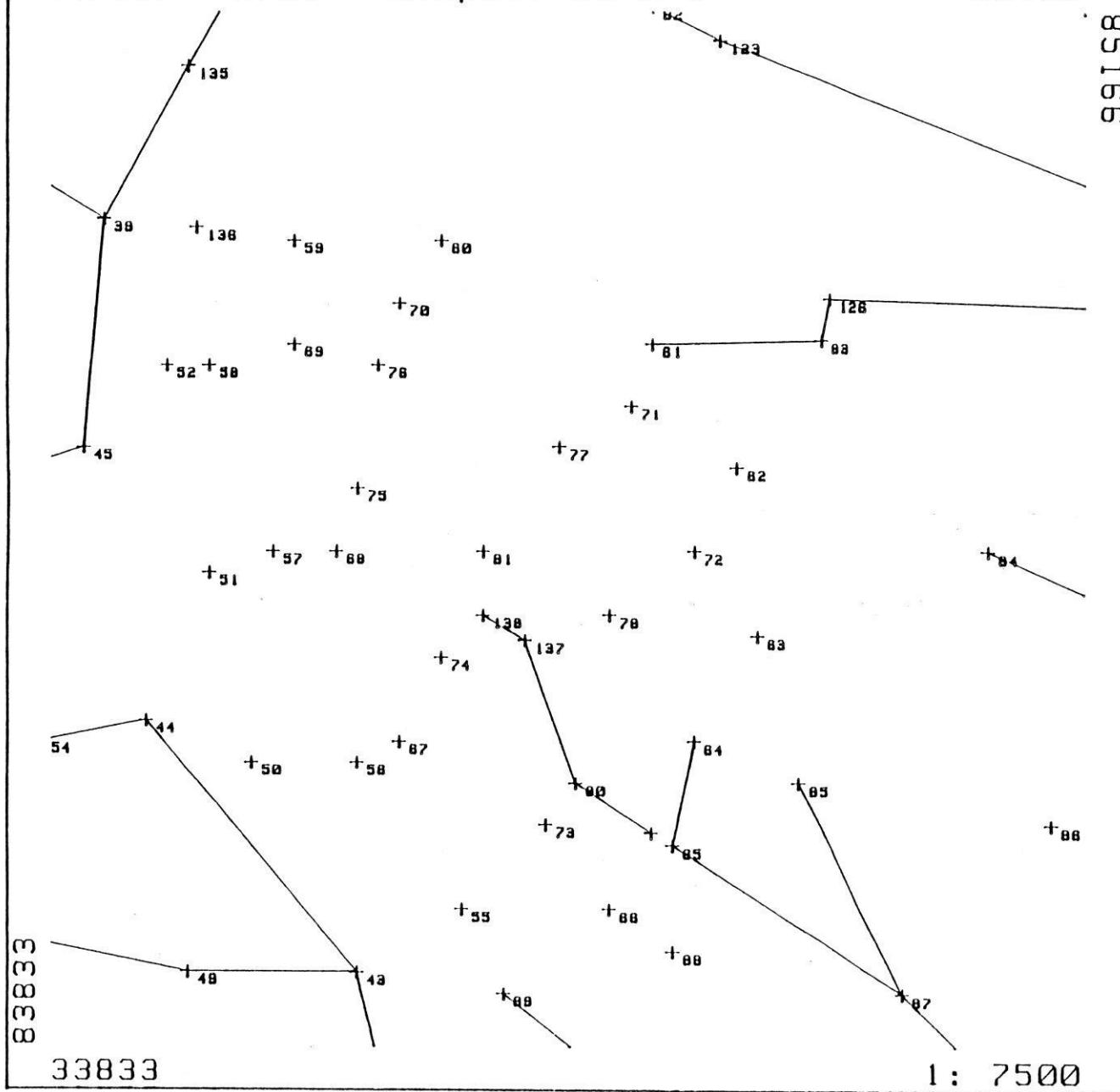


BOREHOLE  
NUMBERS

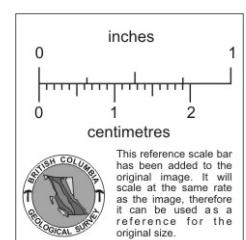
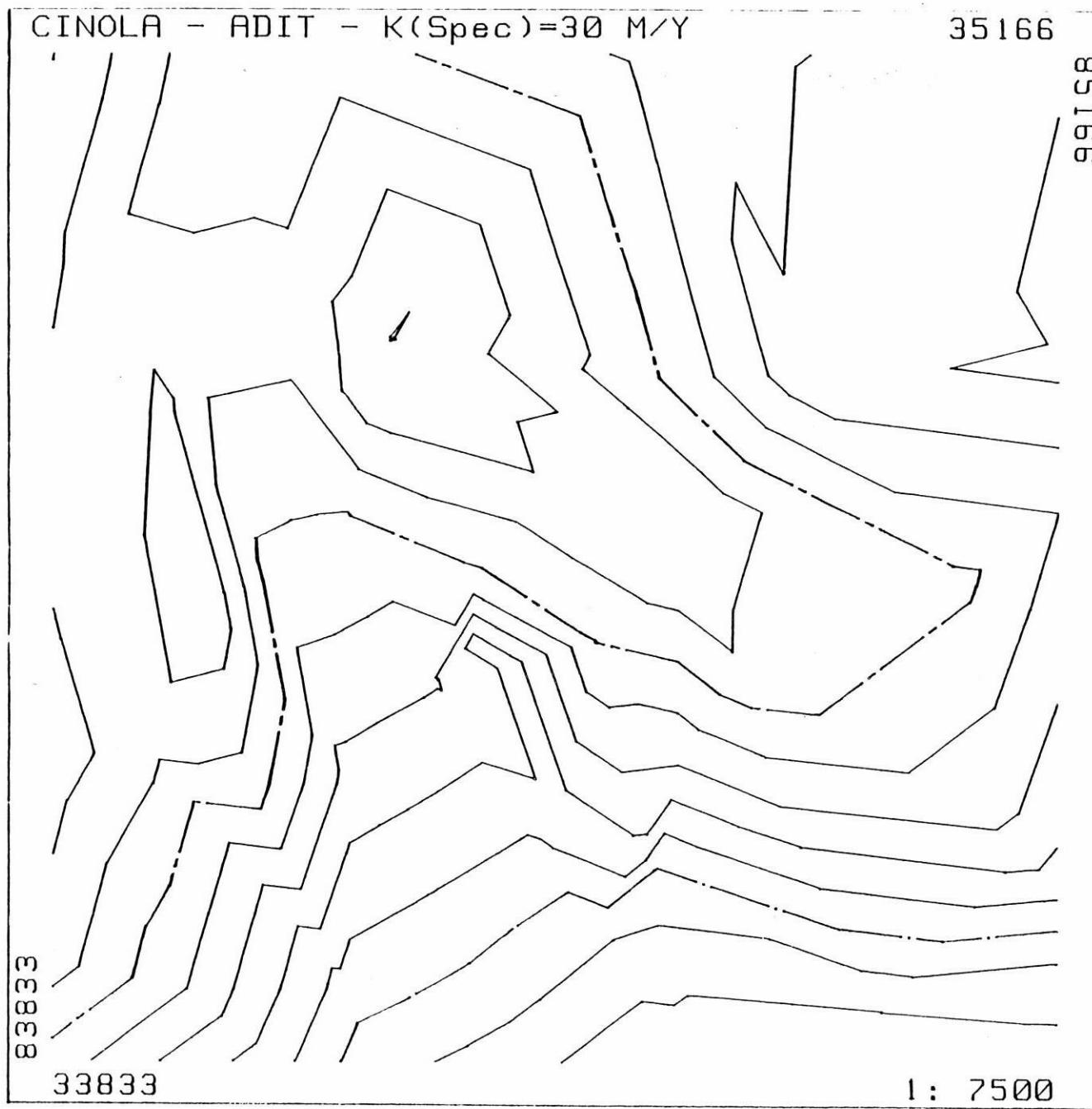
CINOLA - ADIT - K(Spec)=30 M/Y

35166

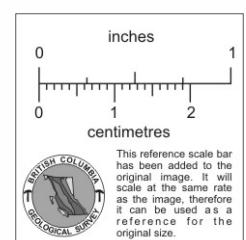
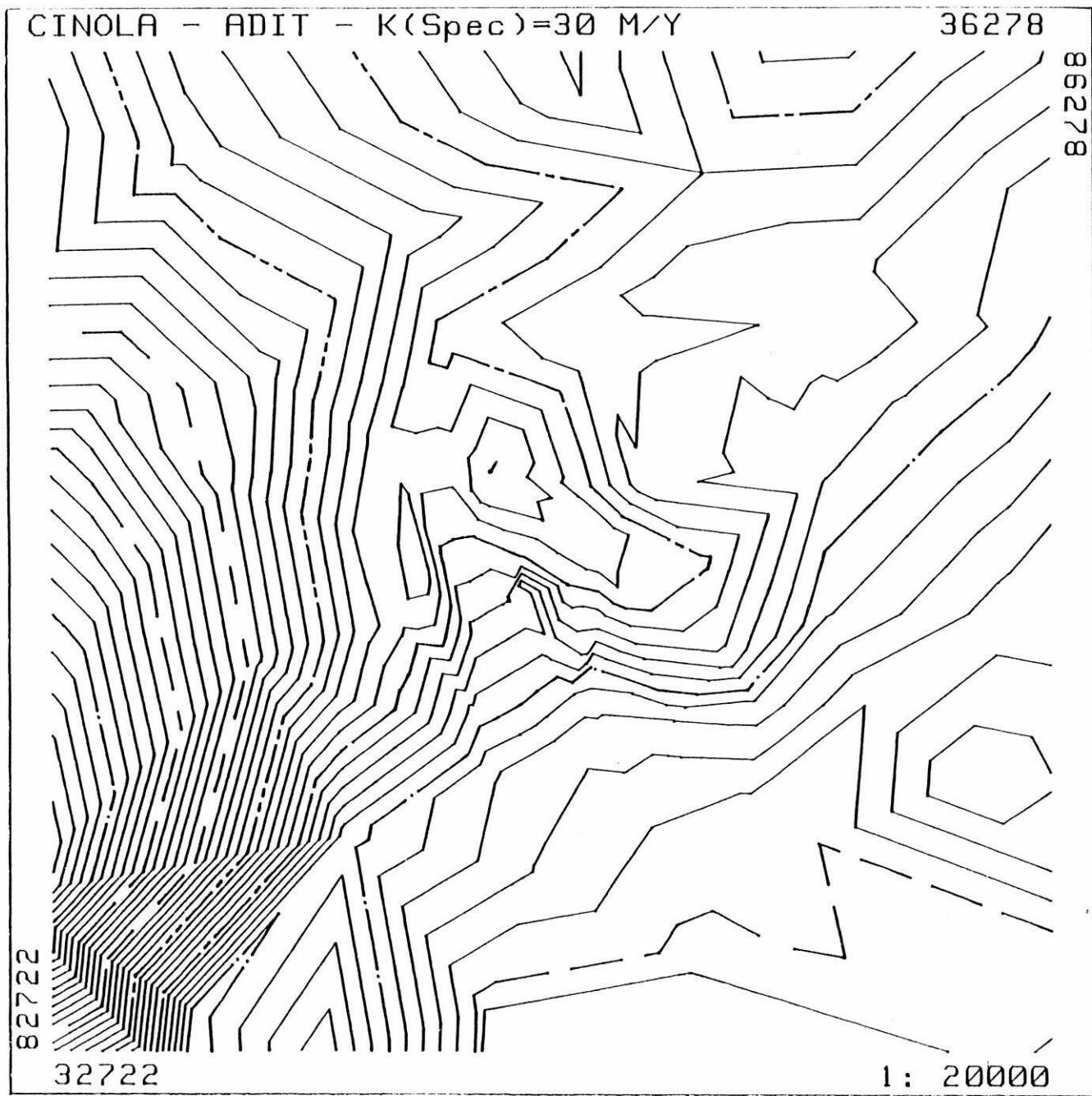
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# DREAMS NUMBERS



HEADS  
CURRENT



HEADS  
CURRENT

**EXHIBIT B**

## -----KEY ANALYSIS PARAMETERS-----

Number of nodes.....136  
Number of elements.....248  
Number of materials.....5  
Number of soils.....7

## -----MATERIAL AND SOIL DATA-----

MATERIAL OR SOIL	HYDRAULIC CONDUCTIVITY CL/TI	SPECIFIC STORAGE CL/LI	SPECIFIC YIELD CL	DISTRIBUTED INFLOW CL/TI
1	3.00E+00	1.00E-06	.0200	7.50E-01
2	3.00E-01	1.00E-06	.0200	7.50E-02
3	1.00E+00	1.00E-06	.0500	7.50E-01
4	1.50E+00	1.00E-06	.0500	7.50E-01
5	3.00E+01	1.00E-06	.0200	7.50E-01
6				7.50E-01
7				7.50E-01

CINOLA - PIT - INITIAL

TIME: 0 year

UNITS - Length [L]: meters Time [T]: year

## -----NODE AND FLOW DATA-----

-NODE DATA-	X-COORD	Y-COORD	BASE-EL	MAX-EL	INIT-W/T	NEW-W/T	BOUN	FIXED-INF	INFILT_INF	STORE_INF	STREAM_INF	OUTFLOW	NODE	
###	LNK	INT	[L]	[L]	[L]	[L]	[L]	DARY.	[L]/[T]	[L]/[T]	[L]/[T]	[L]/[T]	###	
1	-1	133	88750.0	38150.0	-130.0	20.0	20.0	20.0	SWMP	0.000E+00	3.481E-05	0.000E+00	2.702E+07	2.753E+07
2	1	137	89000.0	37400.0	-230.0	20.0	20.0	20.0	SWMP	0.000E+00	1.015E+06	0.000E+00	2.190E+07	2.299E+07
3	2	134	90000.0	36000.0	-275.0	25.0	25.0	25.0	SWMP	0.000E+00	1.120E+06	0.000E+00	1.940E+07	2.075E+07
4	3	131	89250.0	34000.0	-275.0	25.0	25.0	25.0	SWMP	0.000E+00	6.966E+05	0.000E+00	1.573E+07	1.661E+07
5	4	132	89000.0	31650.0	-270.0	30.0	30.0	30.0	SWMP	0.000E+00	6.703E+05	0.000E+00	1.506E+07	1.566E+07
6	5	133	87500.0	32500.0	-235.0	35.0	35.0	35.0	SWMP	0.000E+00	6.189E+05	0.000E+00	1.443E+07	1.518E+07
7	6	130	86250.0	31850.0	-235.0	35.0	35.0	35.0	SWMP	0.000E+00	3.719E+05	0.000E+00	1.333E+07	1.387E+07
8	7	129	86000.0	32300.0	-230.0	40.0	40.0	40.0	SWMP	0.000E+00	1.420E+05	0.000E+00	1.238E+07	1.314E+07
9	8	128	84950.0	33125.0	-235.0	45.0	45.0	45.0	SWMP	0.000E+00	3.513E+04	0.000E+00	5.294E+06	6.161E+06
10	9	127	84275.0	33000.0	-235.0	45.0	45.0	45.0	SWMP	0.000E+00	1.027E+05	0.000E+00	4.848E+06	4.706E+06
11	10	124	84200.0	31500.0	-250.0	50.0	50.0	50.0	SWMP	0.000E+00	1.223E+05	0.000E+00	4.513E+06	4.448E+06
12	11	121	83500.0	31200.0	-250.0	50.0	50.0	50.0	SWMP	0.000E+00	3.022E+05	0.000E+00	4.077E+06	4.518E+06
13	12	120	83200.0	31450.0	-245.0	55.0	55.0	55.0	SWMP	0.000E+00	3.044E+05	0.000E+00	2.153E+06	2.364E+06
14	13	74	80500.0	30800.0	-240.0	60.0	60.0	60.0	SWMP	0.000E+00	7.653E+05	0.000E+00	0.000E+00	3.150E+05
15	29	73	79500.0	32750.0	-370.0	570.0	570.0	570.0	SWMP	0.000E+00	5.819E+05	0.000E+00	0.000E+00	4.779E+05
16	27	122	81000.0	34500.0	-35.0	375.0	375.0	375.0	SWMP	0.000E+00	3.400E+05	0.000E+00	0.000E+00	3.600E+05
17	18	119	82300.0	36000.0	-25.0	375.0	375.0	375.0	SWMP	0.000E+00	4.347E+05	0.000E+00	0.000E+00	3.162E+05
18	24	113	83200.0	37100.0	-150.0	150.0	150.0	150.0	SWMP	0.000E+00	7.562E+05	0.000E+00	3.162E+05	1.083E+05
19	23	117	84550.0	38650.0	-130.0	120.0	120.0	120.0	SWMP	0.300E+00	6.284E+05	0.000E+00	0.000E+00	5.940E+05
20	-1	114	86200.0	40400.0	-240.0	60.0	60.0	60.0	SWMP	0.000E+00	4.025E+05	0.000E+00	1.212E+07	1.254E+07
21	20	115	87000.0	39700.0	-235.0	65.0	65.0	65.0	SWMP	0.000E+00	3.237E+05	0.000E+00	1.176E+07	1.212E+07
22	1	116	87900.0	39000.0	-130.0	120.0	120.0	120.0	SWMP	0.000E+00	8.831E+05	0.000E+00	0.000E+00	7.386E+05
23	21	117	86000.0	39000.0	-210.0	90.0	90.0	90.0	SWMP	0.000E+00	1.373E+06	0.000E+00	1.036E+07	1.176E+07
24	23	112	84400.0	37450.0	-195.0	105.0	105.0	105.0	SWMP	0.000E+00	1.173E+06	0.000E+00	7.150E+06	8.412E+06
25	24	111	84600.0	36000.0	-180.0	120.0	120.0	120.0	SWMP	0.000E+00	7.487E+05	0.000E+00	5.215E+06	6.065E+06
26	25	110	83325.0	35325.0	-115.0	185.0	185.0	185.0	SWMP	0.000E+00	7.423E+05	0.000E+00	4.358E+06	5.215E+06
27	26	109	82200.0	35000.0	-25.0	275.0	275.0	275.0	SWMP	0.000E+00	6.241E+05	0.000E+00	3.286E+06	4.105E+06
28	27	108	81700.0	34000.0	65.0	365.0	365.0	365.0	SWMP	0.000E+00	6.200E+05	0.000E+00	1.700E+06	2.452E+06
29	28	107	80600.0	32900.0	160.0	460.0	460.0	460.0	SWMP	0.000E+00	5.067E+05	0.000E+00	1.013E+06	1.700E+06
30	106	104	85375.0	33350.0	-250.0	50.0	50.0	50.0	SWMP	0.000E+00	2.316E+05	0.000E+00	5.123E+06	6.451E+06
31	30	100	85325.0	34000.0	-240.0	60.0	60.0	60.0	SWMP	0.000E+00	1.119E+05	0.000E+00	5.931E+06	6.159E+06
32	31	99	86000.0	34300.0	-235.0	64.0	64.0	64.0	SWMP	0.000E+00	3.396E+05	0.000E+00	5.434E+06	5.841E+06
33	32	98	86350.0	35000.0	-225.0	77.0	77.0	77.0	SWMP	0.000E+00	7.252E+05	0.000E+00	2.492E+06	3.060E+06
34	33	97	86400.0	35500.0	-195.0	105.0	105.0	105.0	SWMP	0.000E+00	4.774E+05	0.000E+00	1.032E+06	2.537E+06
35	34	96	86000.0	35700.0	-190.0	110.0	110.0	110.0	SWMP	0.000E+00	1.771E+05	0.000E+00	1.338E+06	2.045E+06
36	35	95	85325.0	35450.0	-175.0	121.0	121.0	121.0	SWMP	0.000E+00	2.190E+05	0.000E+00	1.503E+06	1.851E+06
37	36	48	84525.0	35400.0	-175.0	125.0	125.0	125.0	SWMP	0.000E+00	1.518E+05	0.000E+00	1.205E+06	1.410E+06
38	37	53	84150.0	35225.0	-155.0	145.0	145.0	145.0	SWMP	0.000E+00	3.677E+04	0.000E+00	1.044E+06	1.218E+06
39	38	45	83950.0	34875.0	-135.0	162.0	162.0	162.0	SWMP	0.000E+00	5.684E+04	0.000E+00	6.466E+05	7.411E+05
40	39	42	84825.0	33600.0	-240.0	60.0	60.0	60.0	SWMP	0.000E+00	4.751E+04	0.000E+00	9.297E+05	1.142E+06
41	40	51	84550.0	33350.0	-227.0	75.0	75.0	75.0	SWMP	0.000E+00	1.405E+04	0.000E+00	3.238E+05	9.988E+05
42	41	50	84300.0	33775.0	-219.0	81.0	81.0	81.0	SWMP	0.000E+00	6.625E+03	0.000E+00	7.727E+05	7.794E+05
43	42	56	84250.0	33875.0	-195.0	105.0	105.0	105.0	SWMP	0.000E+00	1.253E+04	0.000E+00	3.858E+05	3.991E+05
44	43	103	84000.0	34275.0	-135.0	164.0	164.0	164.0	SWMP	0.000E+00	2.367E+04	0.000E+00	2.592E+05	2.907E+05
45	39	35	83725.0	34600.0	-133.0	162.0	162.0	162.0	SWMP	0.000E+00	2.250E+04	0.000E+00	4.682E+05	4.974E+05
46	53	34	83425.0	34725.0	-55.0	245.0	245.0	245.0	SWMP	0.000E+00	1.680E+05	0.000E+00	1.841E+05	3.375E+05
47	54	102	83525.0	34150.0	-55.0	245.0	245.0	245.0	SWMP	0.000E+00	2.555E+05	0.000E+00	0.000E+00	1.729E+05
48	49	77	83800.0	34025.0	-122.0	178.0	178.0	178.0	SWMP	0.000E+00	3.268E+04	0.000E+00	0.000E+00	7.114E+04
49	45	71	84050.0	33975.0	-160.0	140.0	140.0	140.0	SWMP	0.000E+00	3.355E+04	0.000E+00	7.114E+04	9.151E+04
50	43	51	84125.0	34025.0	-141.0	157.0	157.0	157.0	SWMP	0.000E+00	7.076E+03	0.000E+00	1.451E+02	50

## -----NODE AND FLOW DATA-----

-NODE DATA-			X-COORD #	Y-COORD #	BASE-EL [L]	MAX-EL [L]	INIT-W/T [L]	NEW-W/T [L]	BOUN DARY	FIXED-INF [L3/T]	INFILT_INF [L3/T]	STORE_INF [L3/T]	STREAM_INF [L3/T]	OUTFLOW NODE #	
LNK	INT	[L]	[L]	[L]	[L]	[L]	[L]	[L]		[L3/T]	[L3/T]	[L3/T]	[L3/T]		
51	44	76	34075.0	34450.0	-115.0	185.0	185.0	182.3	SWAP	0.000E+00	1.251E+04	0.000E+00	3.930E-01	3.559E-02	51
52	39	70	34025.0	34700.0	-115.0	185.0	185.0	174.4	SWAP	0.000E+00	7.373E+03	0.000E+00	2.333E-01	5.674E-02	52
53	45	60	33850.0	34575.0	-130.0	170.0	170.0	170.0	SWMP	0.000E+00	5.664E+04	0.000E+00	3.395E+05	4.682E+05	53
54	44	32	33875.0	34250.0	-124.0	176.0	176.0	176.0	SWMP	0.000E+00	4.422E+04	0.000E+00	1.779E+05	2.567E+05	54
55	89	123	34375.0	34650.0	-171.0	129.0	126.8	107.7	SWAP	0.000E+00	9.391E+03	0.000E+00	0.300E+00	7.177E+01	55
56	43	125	34250.0	34225.0	-120.0	180.0	172.0	132.3	SWAP	0.000E+00	5.387E+03	0.000E+00	0.300E+00	1.335E+00	56
57	51	75	34150.0	34475.0	-98.0	204.0	199.2	153.3	SWAP	0.000E+00	5.103E+03	0.000E+00	7.115E+01	4.714E+00	57
58	52	81	34075.0	34700.0	-94.0	206.0	195.1	163.8	SWAP	0.000E+00	9.772E+03	0.000E+00	0.300E+00	1.919E+00	58
59	135	78	34175.0	34850.0	-98.0	202.0	187.8	164.6	SWAP	0.000E+00	2.333E+04	0.000E+00	0.300E+00	1.099E+00	59
60	92	74	34350.0	34850.0	-117.0	123.0	183.0	161.4	SWAP	0.000E+00	4.373E+04	0.000E+00	1.638E+00	1.014E+01	60
61	63	30	34600.0	34725.0	-146.0	154.0	154.0	154.0	SWMP	0.000E+00	3.353E+04	0.000E+00	2.399E+01	4.710E+04	61
62	33	77	34700.0	34575.0	-135.0	165.0	164.8	164.8	SWAP	0.000E+00	2.703E+04	0.000E+00	0.300E+00	2.032E+03	62
63	64	73	34725.0	34735.0	-130.0	173.0	162.0	161.3	SWAP	0.000E+00	3.164E+04	0.000E+00	0.300E+00	2.068E+03	63
64	65	69	34650.0	34250.0	-170.0	150.0	150.0	150.0	SWMP	0.000E+00	1.220E+04	0.000E+00	1.254E+01	1.803E+04	64
65	87	88	34625.0	34125.0	-200.0	100.0	100.0	100.0	SWMP	0.000E+00	1.425E+04	0.000E+00	6.331E+03	6.315E+04	65
66	68	72	34550.0	34050.0	-195.0	105.0	105.0	93.9	SWAP	0.000E+00	9.109E+03	0.000E+00	1.134E+02	3.712E+01	66
67	43	69	34300.0	34250.0	-110.0	190.0	171.8	132.5	SWAP	0.000E+00	1.172E+04	0.000E+00	0.300E+00	6.307E+00	67
68	57	136	34225.0	34475.0	-83.0	217.0	198.2	152.1	SWAP	0.000E+00	1.453E+04	0.000E+00	0.300E+00	3.978E+00	68
69	176	68	34175.0	34725.0	-85.0	215.0	200.0	164.0	SWAP	0.000E+00	1.102E+04	0.000E+00	0.300E+00	2.470E+00	69
70	60	57	34300.0	34775.0	-76.0	204.0	198.8	183.3	SWAP	0.000E+00	1.767E+04	0.000E+00	1.545E+00	1.652E+01	70
71	61	51	34575.0	34650.0	-130.0	170.0	170.0	170.0	SWMP	0.000E+00	1.411E+04	0.000E+00	5.539E+01	5.583E+02	71
72	64	67	34450.0	34475.0	-125.0	175.0	177.4	172.6	SWAP	0.000E+00	1.391E+04	0.000E+00	0.300E+00	5.307E+03	72
73	68	63	34475.0	34150.0	-145.0	155.0	156.8	112.1	SWAP	0.000E+00	1.237E+04	0.000E+00	0.300E+00	3.883E+01	73
74	30	64	34750.0	34350.0	-70.0	210.0	182.5	177.4	SWAP	0.000E+00	1.443E+04	0.000E+00	0.300E+00	2.754E+00	74
75	81	65	34250.0	34550.0	-85.0	215.0	200.8	153.9	SWAP	0.000E+00	1.063E+04	0.000E+00	0.300E+00	5.582E+00	75
76	70	37	34275.0	34700.0	-88.0	212.0	205.7	179.9	SWAP	0.000E+00	1.588E+04	0.000E+00	0.300E+00	2.065E+01	76
77	71	105	34490.0	34600.0	-115.0	195.0	185.0	177.9	SWAP	0.000E+00	1.537E+04	0.000E+00	0.300E+00	9.190E+02	77
78	64	62	34550.0	34400.0	-135.0	165.0	165.0	165.0	SWMP	0.000E+00	1.778E+04	0.000E+00	3.357E+01	3.513E+03	78
79	63	33	34600.0	34175.0	-175.0	125.0	123.2	117.5	SWAP	0.000E+00	7.769E+03	0.000E+00	2.220E+05	4.080E+02	79
80	79	126	34500.0	34225.0	-140.0	160.0	150.0	131.2	SWAP	0.000E+00	9.656E+03	0.000E+00	1.369E+05	1.262E+01	80
81	78	101	34400.0	34475.0	-105.0	195.0	185.0	168.7	SWAP	0.000E+00	1.597E+04	0.000E+00	3.331E+01	2.169E+01	81
82	123	59	34600.0	35120.0	-162.0	136.0	138.0	138.0	SWMP	0.000E+00	5.674E+04	0.000E+00	7.923E+01	6.372E+04	82
83	123	58	34800.0	34730.0	-176.0	124.0	124.0	124.0	SWMP	0.000E+00	4.304E+04	0.000E+00	5.521E+04	1.366E+05	83
84	102	52	35000.0	34475.0	-148.0	152.0	152.0	152.0	SWMP	0.000E+00	8.331E+04	0.000E+00	0.300E+00	3.117E+04	84
85	87	39	34775.0	34200.0	-170.0	130.0	130.0	130.0	SWMP	0.000E+00	1.522E+04	0.000E+00	0.300E+00	1.207E+04	85
86	107	123	35075.0	34150.0	-130.0	170.0	127.7	126.6	SWAP	0.000E+00	5.531E+04	0.000E+00	0.300E+00	-2.384E+05	86
87	105	58	34900.0	33950.0	-220.0	90.0	80.0	80.0	SWMP	0.000E+00	3.484E+04	0.000E+00	1.511E+05	1.327E+05	87
88	41	37	34625.0	34000.0	-205.0	75.0	92.7	82.7	SWAP	0.000E+00	7.079E+04	0.000E+00	1.137E+04	1.642E+01	88
89	41	56	34425.0	33950.0	-207.0	93.0	80.0	93.0	SWMP	0.000E+00	3.242E+03	0.000E+00	6.434E+03	2.517E+04	89
90	42	55	33825.0	33575.0	-196.0	104.0	104.0	104.0	SWMP	0.000E+00	1.707E+05	0.000E+00	0.300E+00	5.690E+05	90
91	7	34	34450.0	33450.0	-231.0	69.0	69.0	67.0	SWMP	0.000E+00	1.492E+04	0.000E+00	0.300E+00	1.317E+04	91
92	10	33	33750.0	32820.0	-150.0	150.0	139.1	138.2	SWAP	0.000E+00	2.614E+05	0.000E+00	0.300E+00	0.000E+00	92
93	122	52	33325.0	33000.0	-205.0	95.0	95.0	95.0	SWMP	0.000E+00	1.513E+05	0.000E+00	4.760E+05	9.624E+05	93
94	93	31	32700.0	33375.0	-134.0	434.0	434.0	434.0	SWMP	0.000E+00	6.724E+05	0.000E+00	2.377E+05	4.760E+05	94
95	46	30	33000.0	34275.0	-40.0	340.0	340.0	340.0	SWMP	0.000E+00	2.677E+05	0.000E+00	0.300E+00	1.341E+05	95
96	24	106	33000.0	35000.0	-23.0	277.0	277.0	277.0	SWMP	0.000E+00	3.402E+05	0.000E+00	0.300E+00	2.523E+05	96
97	39	56	33375.0	35100.0	-76.0	224.0	224.0	224.0	SWMP	0.000E+00	1.973E+05	0.000E+00	0.300E+00	1.470E+05	97
98	38	55	34000.0	33575.0	-122.0	173.0	173.0	178.0	SWMP	0.000E+00	2.658E+05	0.000E+00	0.300E+00	7.766E+04	98
99	36	59	35000.0	35750.0	-160.0	140.0	140.0	140.0	SWMP	0.000E+00	2.313E+05	0.000E+00	0.300E+00	1.386E+05	99
100	33	50	36000.0	35150.0	-173.0	107.0	107.0	107.0	SWMP	0.000E+00	1.382E+05	0.000E+00	0.300E+00	1.674E+05	100

CINOLA - PIT - INITIAL

TIME: 0 year

UNITS - Length [L]: meters Time [T]: year

## -----NODE AND FLOW DATA-----

NODE DATA-			X-COORD	Y-COORD	BASE-EL	MAX-EL	INIT-W/T	NEW-W/T	BOUN	FIXED-INF	INFILT_INF	STORE_INF	STREAM_INF	OUTFLOW NODE
##	LNK	INT	[L]	[L]	[L]	[L]	[L]	[L]	DARY	[L]/[T]	[L]/[T]	[L]/[T]	[L]/[T]	##
101	32	48	85390.0	34760.0	-189.0	111.0	111.0	111.0	SWMP	0.000E+00	1.314E+05	0.000E+00	4.904E+05	5.417E+05 101
102	31	49	85400.0	34300.0	-209.0	91.0	91.0	91.0	SWMP	0.000E+00	1.155E+05	0.000E+00	2.335E+04	1.561E+05 102
103	105	47	85175.0	34000.0	-214.0	86.0	86.0	86.0	SWMP	0.000E+00	5.563E+04	0.000E+00	-1.155E-03	5.462E+04 103
104	40	54	84875.0	33800.0	-203.0	67.0	67.0	67.0	SWMP	0.000E+00	3.374E+04	0.000E+00	0.000E+00	5.759E+04 104
105	106	44	85150.0	33700.0	-141.0	59.0	59.0	59.0	SWMP	0.000E+00	1.021E+05	0.000E+00	1.860E-05	5.082E+05 105
106	3	43	85350.0	33250.0	-248.0	51.0	51.0	51.0	SWMP	0.000E+00	2.277E+04	0.000E+00	5.212E+04	5.833E+04 106
107	7	42	85815.0	33750.0	-212.0	83.0	83.0	83.0	SWMP	0.000E+00	4.237E+05	0.000E+00	1.000E-00	5.225E+05 107
108	3	41	87000.0	33700.0	-140.0	60.0	60.0	60.0	SWMP	0.000E+00	6.876E+05	0.000E+00	0.000E+00	5.395E+04 108
109	5	40	86500.0	33700.0	-125.0	75.0	75.0	75.0	SWMP	0.000E+00	1.504E+06	0.000E+00	0.000E+00	5.313E+04 109
110	3	21	88250.0	35000.0	-245.0	55.0	55.0	55.0	SWMP	0.000E+00	5.369E+05	0.000E+00	0.000E+00	1.097E+04 110
111	32	19	87000.0	34450.0	-150.0	50.0	50.0	50.0	SWMP	0.000E+00	3.906E+05	0.000E+00	5.833E-05	5.624E+04 111
112	111	17	87000.0	35600.0	-195.0	105.0	105.0	105.0	SWMP	0.000E+00	5.772E+05	0.000E+00	0.000E+00	5.388E-05 112
113	1	18	87750.0	33550.0	-150.0	150.0	150.0	150.0	SWMP	0.000E+00	1.422E+06	0.000E+00	0.000E+00	5.135E+04 113
114	115	16	87000.0	37000.0	-210.0	90.0	90.0	90.0	SWMP	0.000E+00	1.097E+06	0.000E+00	7.398E-05	5.695E+04 114
115	1	15	87000.0	36000.0	-240.0	60.0	60.0	60.0	SWMP	0.000E+00	1.437E+06	0.000E+00	5.739E-05	5.7395E+04 115
116	23	29	85700.0	37500.0	-170.0	130.0	130.0	130.0	SWMP	0.000E+00	1.370E+06	0.000E+00	0.000E+00	1.352E+04 116
117	114	28	85450.0	36550.0	-115.0	125.0	125.0	125.0	SWMP	0.000E+00	5.173E+05	0.000E+00	0.000E+00	5.199E+04 117
118	23	27	80900.0	32600.0	165.0	565.0	565.0	565.0	SWMP	0.000E+00	9.844E+05	0.000E+00	0.000E+00	5.333E+04 118
119	13	26	82000.0	32100.0	-150.0	150.0	150.0	150.0	SWMP	0.000E+00	1.092E+06	0.000E+00	0.000E+00	5.248E+04 119
120	94	23	81900.0	33200.0	225.0	525.0	525.0	525.0	SWMP	0.000E+00	5.323E+05	0.000E+00	0.000E+00	5.597E+04 120
121	27	24	82350.0	34200.0	105.0	405.0	405.0	405.0	SWMP	0.000E+00	4.738E+05	0.000E+00	0.000E+00	5.739E+04 121
122	12	23	83300.0	32700.0	-210.0	50.0	50.0	50.0	SWMP	0.000E+00	3.222E+05	0.000E+00	5.124E+04	5.412E+04 122
123	125	21	84680.0	35030.0	-167.0	133.0	133.0	133.0	SWMP	0.000E+00	2.281E+04	0.000E+00	3.350E-04	5.206E+05 123
124	125	20	85090.0	35130.0	-173.0	122.0	122.0	122.0	SWMP	0.000E+00	4.701E+04	0.000E+00	0.000E+00	5.385E+04 124
125	101	14	85230.0	34870.0	-136.0	114.0	114.0	114.0	SWMP	0.000E+00	3.610E+04	0.000E+00	1.743E+04	5.452E+04 125
126	101	13	84810.0	34730.0	-171.0	129.0	129.0	129.0	SWMP	0.000E+00	4.589E+04	0.000E+00	1.710E+05	5.726E+04 126
127	36	12	85160.0	35230.0	-170.0	130.0	130.0	130.0	SWMP	0.000E+00	5.221E+04	0.000E+00	0.000E+00	5.667E+04 127
128	101	11	85350.0	34640.0	-125.0	115.0	115.0	115.0	SWMP	0.000E+00	2.363E+04	0.000E+00	4.341E+04	5.341E+04 128
129	123	10	85420.0	35020.0	-182.0	118.0	116.0	116.0	SWMP	0.000E+00	2.025E+04	0.000E+00	0.000E+00	5.773E+04 129
130	128	9	85350.0	35200.0	-177.0	123.0	123.0	123.0	SWMP	0.000E+00	1.520E+04	0.000E+00	0.000E+00	5.368E+04 130
131	132	8	85500.0	35130.0	-174.0	126.0	126.0	126.0	SWMP	0.000E+00	1.270E+04	0.000E+00	1.395E+04	5.318E+04 131
132	133	7	85580.0	35060.0	-185.0	115.0	115.0	115.0	SWMP	0.000E+00	1.140E+04	0.000E+00	2.313E+04	5.222E+04 132
133	32	6	85740.0	34730.0	-195.0	105.0	105.0	105.0	SWMP	0.000E+00	1.028E+05	0.000E+00	3.222E-04	5.379E+04 133
134	131	5	85340.0	35230.0	-173.0	127.0	127.0	127.0	SWMP	0.000E+00	4.089E+04	0.000E+00	0.000E+00	5.395E+04 134
135	38	4	84050.0	35050.0	-145.0	155.0	155.0	155.0	SWMP	0.000E+00	5.736E+04	0.000E+00	7.480E+04	5.268E+04 135
136	37	3	84060.0	34865.0	-115.0	135.0	135.0	135.0	SWMP	0.000E+00	5.463E+03	0.000E+00	6.272E-01	5.073E+04 136

## -----SINK FLOW DATA-----

SINK CONN	TOT_FLOW	SINK CONN	TOT_FLOW	SINK CONN	TOT_FLOW	SINK CONN	TOT_FLOW	SINK CONN	TOT_FLOW		
#	#	L/[T]	#	#	L/[T]	#	#	L/[T]	#		
0	0	0.0000E+00									
1	2	4.0086E+07	2	0	0.0000E+00	3	0	0.0000E+00	4	0	0.0000E+00
5	0	0.0000E+00	7	0	0.0000E+00	8	0	0.0000E+00	9	0	0.0000E+00
11	0	0.0000E+00	12	0	0.0000E+00	13	0	0.0000E+00	14	0	0.0000E+00
15	0	0.0000E+00	17	0	0.0000E+00	18	0	0.0000E+00	19	0	0.0000E+00

-----ELEMENT DATA-----

-----ELEMENT DATA-----

-----KEY ANALYSIS PARAMETERS-----

Number of nodes.....136  
Number of elements.....248  
Number of materials.....5  
Number of soils.....7

-----MATERIAL AND SOIL DATA-----

MATERIAL OR SOIL	HYDRAULIC CONDUCTIVITY [L/T]	SPECIFIC STORAGE [1/L]	SPECIFIC YIELD [-]	DISTRIBUTED INFLOW [L/T]
1	3.00E+00	1.00E-06	.0200	7.50E-01
2	3.00E-01	1.00E-06	.0200	7.50E-02
3	3.00E+00	1.00E-06	.0500	7.50E-01
4	1.50E+00	1.00E-06	.0500	7.50E-01
5	3.00E+01	1.00E-06	.0200	7.50E-01
6				7.50E-01
7				7.50E-01

-----NODE AND FLOW DATA-----

-NODE DATA-	X-COORD	Y-COORD	BASE-EL	MAX-EL	INIT-W/T	NEW-W/T	BOUN	FIXED-INF	INFILT_INF	STORE_INF	STREAM_INF	OUTFLOW	NODE
---	[L]	[L]	[L]	[L]	[L]	[L]	DARY	[L3/T]	[L3/T]	[L3/T]	[L3/T]	[L3/T]	---
1	-1 136	38750.0	39150.0	-280.0	20.0	20.0	20.0 SWMP	0.000E+00	3.481E+05	0.000E+00	2.544E+07	2.663E+07	1
2	1 134	39000.0	37400.0	-280.0	20.0	20.0	20.0 SWMP	0.000E+00	1.015E-06	0.000E+00	2.121E+07	2.230E+07	2
3	2 131	39000.0	36000.0	-275.0	25.0	25.0	25.0 SWMP	0.000E+00	1.220E-06	0.000E+00	1.882E+07	2.006E+07	3
4	3 132	39950.0	34000.0	-275.0	25.0	25.0	25.0 SWMP	0.000E+00	6.766E+05	0.000E+00	1.516E+07	1.591E+07	4
5	4 133	39000.0	31650.0	-270.0	30.0	30.0	30.0 SWMP	0.000E+00	6.703E+05	0.000E+00	1.448E+07	1.516E+07	5
6	5 130	37500.0	32500.0	-265.0	35.0	35.0	35.0 SWMP	0.000E+00	6.169E-05	0.000E+00	1.385E+07	1.448E+07	6
7	6 129	35250.0	32250.0	-215.0	35.0	35.0	35.0 SWMP	0.000E+00	1.719E-05	0.000E+00	1.277E+07	1.318E+07	7
8	7 123	36000.0	32800.0	-250.0	40.0	40.0	40.0 SWMP	0.000E+00	1.420E-05	0.000E+00	1.230E+07	1.245E+07	8
9	8 127	64750.0	33125.0	-255.0	45.0	45.0	45.0 SWMP	0.000E+00	6.513E+04	0.000E+00	5.774E+06	5.874E+06	9
10	9 124	34275.0	33000.0	-255.0	45.0	45.0	45.0 SWMP	0.000E+00	1.257E-05	0.000E+00	4.548E+06	4.908E+06	10
11	10 121	34200.0	31900.0	-250.0	50.0	50.0	50.0 SWMP	0.000E+00	1.226E-05	0.000E+00	4.518E+06	4.546E+06	11
12	11 120	37500.0	32200.0	-250.0	50.0	50.0	50.0 SWMP	0.000E+00	5.222E-05	0.000E+00	4.077E+06	4.518E+06	12
13	12 94	32300.0	31450.0	-245.0	55.0	55.0	55.0 SWMP	0.000E+00	3.044E-05	0.000E+00	2.183E+06	2.564E+06	13
14	13 93	30500.0	30800.0	-240.0	60.0	60.0	60.0 SWMP	0.000E+00	7.656E-05	0.000E+00	0.000E+00	9.150E+05	14
15	23 122	79500.0	32750.0	-370.0	670.0	670.0	670.0 SWMP	0.000E+00	5.819E-05	0.000E+00	0.000E+00	4.799E+05	15
16	27 119	31000.0	34500.0	-73.0	395.0	395.0	395.0 SWMP	0.000E+00	6.400E+05	0.000E+00	0.000E+00	5.600E+05	16
17	19 118	32300.0	36000.0	-25.0	275.0	275.0	275.0 SWMP	0.000E+00	4.347E-05	0.000E+00	0.000E+00	3.162E+05	17
18	24 117	33200.0	37100.0	-150.0	150.0	150.0	150.0 SWMP	0.000E+00	7.862E-05	0.000E+00	3.162E+05	1.085E+06	18
19	22 114	84550.0	38650.0	-180.0	120.0	120.0	120.0 SWMP	0.000E+00	6.294E-05	0.000E+00	0.000E+00	5.940E+05	19
20	-1 115	86200.0	-40400.0	-240.0	60.0	60.0	60.0 SWMP	0.000E+00	4.025E-05	0.000E+00	1.212E+07	1.254E+07	20
21	20 116	37000.0	39700.0	-255.0	65.0	65.0	65.0 SWMP	0.000E+00	3.237E-05	0.000E+00	1.176E+07	1.212E+07	21
22	1 117	37900.0	39000.0	-180.0	120.0	120.0	120.0 SWMP	0.000E+00	3.831E-05	0.000E+00	0.000E+00	7.385E+05	22
23	21 112	36000.0	39000.0	-210.0	90.0	90.0	90.0 SWMP	0.000E+00	1.373E+06	0.000E+00	1.036E+07	1.176E+07	23
24	23 111	34400.0	37450.0	-195.0	105.0	105.0	105.0 SWMP	0.000E+00	1.173E+06	0.000E+00	7.150E+05	8.412E+05	24
25	24 110	34600.0	36000.0	-180.0	120.0	120.0	120.0 SWMP	0.000E+00	7.487E+05	0.000E+00	5.215E+06	6.065E+06	25
26	23 109	33325.0	35825.0	-115.0	185.0	185.0	185.0 SWMP	0.000E+00	7.424E+05	0.000E+00	4.358E+06	5.215E+06	26
27	25 108	32200.0	35000.0	-25.0	275.0	275.0	275.0 SWMP	0.000E+00	6.241E-05	0.000E+00	3.288E+06	4.105E+06	27
28	27 107	31700.0	34000.0	65.0	365.0	365.0	365.0 SWMP	0.000E+00	6.200E-05	0.000E+00	1.700E+06	2.452E+06	28
29	28 104	80600.0	32900.0	160.0	460.0	460.0	460.0 SWMP	0.000E+00	5.069E-05	0.000E+00	1.013E+06	1.700E+06	29
30	106 100	35375.0	33550.0	-250.0	50.0	50.0	50.0 SWMP	0.000E+00	2.316E+05	0.000E+00	5.938E+06	6.130E+06	30
31	30 77	35525.0	34000.0	-240.0	60.0	60.0	60.0 SWMP	0.000E+00	1.119E+05	0.000E+00	5.876E+06	5.838E+06	31
32	31 78	36000.0	34300.0	-236.0	64.0	64.0	64.0 SWMP	0.000E+00	3.396E+05	0.000E+00	5.160E+06	5.538E+06	32
33	32 77	36350.0	35000.0	-223.0	77.0	77.0	77.0 SWMP	0.000E+00	3.262E+05	0.000E+00	2.469E+06	2.844E+06	33
34	33 76	36400.0	35900.0	-195.0	105.0	105.0	105.0 SWMP	0.000E+00	4.734E+05	0.000E+00	1.830E+06	2.322E+06	34
35	34 75	36000.0	35700.0	-190.0	110.0	110.0	110.0 SWMP	0.000E+00	1.731E+05	0.000E+00	1.635E+06	1.830E+06	35
36	33 73	35525.0	35450.0	-175.0	121.0	121.0	121.0 SWMP	0.000E+00	2.130E+05	0.000E+00	1.400E+06	1.635E+06	36
37	36 72	34925.0	35400.0	-175.0	125.0	125.0	125.0 SWMP	0.000E+00	1.512E-05	0.000E+00	1.003E+06	1.193E+06	37
38	37 45	34150.0	35225.0	-155.0	145.0	145.0	145.0 SWMP	0.000E+00	3.577E+04	0.000E+00	4.336E+05	1.003E+06	38
39	133 92	33325.0	34675.0	-138.0	162.0	162.0	162.0 SWMP	0.000E+00	5.684E-04	0.000E+00	6.349E+05	7.264E+05	39
40	3 91	34825.0	33600.0	-240.0	60.0	60.0	60.0 SWMP	0.000E+00	4.751E-04	0.000E+00	7.422E+05	8.550E+05	40
41	40 90	84550.0	33650.0	-227.0	73.0	73.0	73.0 SWMP	0.000E+00	1.405E-04	0.000E+00	7.575E+05	7.285E+05	41
42	41 89	84300.0	33775.0	-219.0	81.0	81.0	81.0 SWMP	0.000E+00	5.625E-03	0.000E+00	7.474E+05	7.575E+05	42
43	42 88	84250.0	33975.0	-195.0	105.0	105.0	105.0 SWMP	0.000E+00	1.253E+04	0.000E+00	3.705E+05	3.784E+05	43
44	43 86	84000.0	34275.0	-156.0	164.0	164.0	164.0 SWMP	0.000E+00	2.867E+04	0.000E+00	2.567E+05	2.770E+05	44
45	39 103	33925.0	34600.0	-133.0	162.0	162.0	162.0 SWMP	0.000E+00	2.250E+04	0.000E+00	4.662E+05	4.379E+05	45
46	53 85	33425.0	34725.0	-65.0	245.0	245.0	245.0 SWMP	0.000E+00	1.680E+05	0.000E+00	1.841E+05	3.395E+05	46
47	54 87	33325.0	34150.0	-53.0	245.0	245.0	245.0 SWMP	0.000E+00	2.555E+05	0.000E+00	0.000E+00	1.799E+05	47
48	49 105	33800.0	34025.0	-122.0	173.0	173.0	173.0 SWMP	0.000E+00	3.286E-04	0.000E+00	0.000E+00	7.114E+04	48
49	43 84	84050.0	33975.0	-160.0	140.0	140.0	140.0 SWMP	0.000E+00	2.355E+04	0.000E+00	7.114E+04	9.151E+04	49
50	42 102	84125.0	34225.0	-141.0	153.0	153.0	153.0 SWMP	0.000E+00	7.070E+03	0.000E+00	0.000E+00	1.027E+04	50

## -----NODE AND FLOW DATA-----

-NODE DATA-			X-COORD	Y-COORD	BASE-EL	MAX-EL	INIT-W/T	NEW-W/T	BOUN	FIXED-INF	INFILT_INF	STORE_INF	STREAM_INF	OUTFLOW	NODE
##	LNK	INT	[L]	[L]	[L]	[L]	[L]	[L]	DARY	[L3/T]	[L3/T]	[L3/T]	[L3/T]	[L3/T]	##
51	44	63	84075.0	34450.0	-115.0	185.0	185.0	185.0	SWMP	0.000E+00	1.251E+04	0.000E+00	0.000E+00	2.198E-03	51
52	39	126	84025.0	34700.0	-115.0	185.0	185.0	185.0	SWMP	0.000E+00	7.375E+03	0.000E+00	0.000E+00	4.118E-02	52
53	45	82	83850.0	34575.0	-130.0	170.0	170.0	170.0	SWMP	0.000E+00	6.664E+04	0.000E+00	3.395E+05	4.682E+05	53
54	44	127	83875.0	34250.0	-124.0	176.0	176.0	176.0	SWMP	0.000E+00	4.422E+04	0.000E+00	1.799E+05	2.567E+05	54
55	-2	125	84375.0	34050.0	-171.0	129.0	126.8	65.3	SWMP	0.000E+00	9.891E+03	0.000E+00	0.000E+00	1.120E-04	55
56	-2	101	84250.0	34225.0	-120.0	180.0	172.0	62.3	SWMP	0.000E+00	6.887E+03	0.000E+00	0.000E+00	-4.325E-03	56
57	-2	81	84150.0	34475.0	-86.0	204.0	198.8	65.8	SWMP	0.000E+00	5.109E+03	0.000E+00	0.000E+00	1.352E-01	57
58	-2	80	84075.0	34700.0	-84.0	206.0	199.2	110.6	SWMP	0.000E+00	9.772E+03	0.000E+00	0.000E+00	2.108E+00	58
59	-2	79	84175.0	34850.0	-88.0	202.0	187.8	137.0	SWMP	0.000E+00	1.758E+04	0.000E+00	0.000E+00	1.920E+00	59
60	-2	78	84550.0	34850.0	-117.0	183.0	183.0	147.9	SWMP	0.000E+00	4.378E+04	0.000E+00	0.000E+00	1.509E-01	60
61	-2	77	84600.0	34725.0	-146.0	154.0	154.0	140.3	SWMP	0.000E+00	3.353E+04	0.000E+00	0.000E+00	5.792E-02	61
62	-2	76	84700.0	34575.0	-135.0	165.0	164.3	137.1	SWMP	0.000E+00	1.308E+04	0.000E+00	0.000E+00	1.148E-02	62
63	-2	75	84725.0	34375.0	-130.0	170.0	162.0	133.3	SWMP	0.000E+00	3.164E+04	0.000E+00	0.000E+00	1.956E-03	63
64	-2	74	84650.0	34250.0	-170.0	130.0	130.0	95.8	SWMP	0.000E+00	1.138E+04	0.000E+00	0.000E+00	1.304E-03	64
65	-2	73	84625.0	34125.0	-200.0	100.0	100.0	83.1	SWMP	0.000E+00	1.456E+04	0.000E+00	0.000E+00	5.585E-04	65
66	-2	72	84550.0	34050.0	-185.0	105.0	105.0	70.2	SWMP	0.000E+00	9.766E+03	0.000E+00	0.000E+00	7.777E-04	66
67	-2	71	84300.0	34250.0	-110.0	120.0	171.3	62.3	SWMP	0.000E+00	1.172E+04	0.000E+00	0.000E+00	2.562E-03	67
68	-2	70	84225.0	34475.0	-83.0	120.0	198.2	60.5	SWMP	0.000E+00	1.453E+04	0.000E+00	0.000E+00	-6.716E-02	68
69	-2	67	84175.0	34725.0	-85.0	120.0	200.0	109.0	SWMP	0.000E+00	1.102E+04	0.000E+00	0.000E+00	1.156E-00	69
70	-2	68	84300.0	34775.0	-96.0	120.0	198.8	118.7	SWMP	0.000E+00	1.387E+04	0.000E+00	0.000E+00	1.374E-01	70
71	-2	67	84575.0	34650.0	-130.0	120.0	170.0	119.6	SWMP	0.000E+00	1.411E+04	0.000E+00	0.000E+00	4.694E-02	71
72	-2	66	84650.0	34475.0	-125.0	120.0	173.4	120.0	SWMP	0.000E+00	1.591E+04	0.000E+00	0.000E+00	2.370E-03	72
73	-2	65	84475.0	34150.0	-145.0	60.0	136.3	60.0	SWMP	0.000E+00	1.313E+04	0.000E+00	0.000E+00	6.390E-04	73
74	-2	64	84350.0	34350.0	-80.0	60.0	182.5	60.0	SWMP	0.000E+00	1.445E+04	0.000E+00	0.000E+00	1.149E+04	74
75	-2	63	84250.0	34550.0	-85.0	60.0	200.3	60.0	SWMP	0.000E+00	1.063E+04	0.000E+00	0.000E+00	2.444E-05	75
76	-2	62	84275.0	34700.0	-88.0	60.0	205.7	60.0	SWMP	0.000E+00	1.588E+04	0.000E+00	0.000E+00	7.239E+04	76
77	-2	61	84490.0	34600.0	-115.0	60.0	185.0	60.0	SWMP	0.000E+00	1.547E+04	0.000E+00	0.000E+00	5.356E-04	77
78	-2	60	84550.0	34400.0	-133.0	60.0	165.0	60.0	SWMP	0.000E+00	1.719E+04	0.000E+00	0.000E+00	2.972E-04	78
79	-2	59	84600.0	34175.0	-175.0	60.0	123.2	60.0	SWMP	0.000E+00	6.516E-03	0.000E+00	0.000E+00	3.741E-04	79
80	-2	58	84500.0	34225.0	-140.0	0.0	150.0	0.0	SWMP	0.000E+00	1.227E+04	0.000E+00	0.000E+00	9.351E+04	80
81	-2	57	84400.0	34475.0	-105.0	0.0	195.0	0.0	SWMP	0.000E+00	2.041E+04	0.000E+00	0.000E+00	9.113E+04	81
82	123	56	84600.0	35120.0	-162.0	138.0	138.0	138.0	SWMP	0.000E+00	8.674E+04	0.000E+00	0.000E+00	6.672E+04	82
83	125	55	84800.0	34730.0	-176.0	124.0	124.0	124.0	SWMP	0.000E+00	4.304E+04	0.000E+00	0.000E+00	1.160E-05	83
84	102	52	85000.0	34475.0	-148.0	152.0	152.0	152.0	SWMP	0.000E+00	3.331E+04	0.000E+00	0.000E+00	1.331E+04	84
85	37	39	84775.0	34200.0	-170.0	130.0	130.0	116.4	SWMP	0.000E+00	1.523E+04	0.000E+00	0.000E+00	2.061E-03	85
86	103	105	85075.0	34150.0	-130.0	170.0	127.7	125.2	SWMP	0.000E+00	5.531E+04	0.000E+00	0.000E+00	3.712E-04	86
87	105	38	84900.0	33950.0	-220.0	80.0	80.0	80.0	SWMP	0.000E+00	3.484E+04	0.000E+00	0.000E+00	2.061E-03	87
88	41	37	84625.0	34000.0	-205.0	95.0	92.7	73.9	SWMP	0.000E+00	3.073E+04	0.000E+00	0.000E+00	1.079E-03	88
89	41	36	84425.0	33950.0	-207.0	93.0	93.0	69.3	SWMP	0.000E+00	3.242E+03	0.000E+00	0.000E+00	3.394E-04	89
90	42	35	83825.0	33575.0	-193.0	104.0	104.0	104.0	SWMP	0.000E+00	2.707E+05	0.000E+00	0.000E+00	3.690E-05	90
91	9	34	84450.0	34450.0	-231.0	67.0	69.0	69.0	SWMP	0.000E+00	1.492E+04	0.000E+00	0.000E+00	1.317E+04	91
92	10	33	83750.0	32820.0	-150.0	150.0	139.1	138.2	SWMP	0.000E+00	2.614E+05	0.000E+00	0.000E+00	0.000E+00	92
93	122	32	83325.0	33000.0	-205.0	95.0	95.0	95.0	SWMP	0.000E+00	1.513E+05	0.000E+00	4.760E+05	3.624E+05	93
94	93	31	82700.0	33375.0	134.0	434.0	434.0	434.0	SWMP	0.000E+00	6.724E+05	0.000E+00	2.377E+05	4.960E+05	94
95	46	30	83000.0	34275.0	40.0	340.0	340.0	340.0	SWMP	0.000E+00	2.677E+05	0.000E+00	0.000E+00	1.341E+05	95
96	26	106	83000.0	35000.0	-23.0	277.0	277.0	277.0	SWMP	0.000E+00	3.402E+05	0.000E+00	0.000E+00	2.523E-05	96
97	39	51	83575.0	35100.0	-76.0	224.0	224.0	224.0	SWMP	0.000E+00	1.273E+05	0.000E+00	0.000E+00	1.470E+05	97
98	38	50	84000.0	35575.0	-122.0	178.0	178.0	178.0	SWMP	0.000E+00	2.658E+05	0.000E+00	0.000E+00	7.960E-04	98
99	36	48	85000.0	35750.0	-160.0	140.0	140.0	140.0	SWMP	0.000E+00	2.313E+05	0.000E+00	0.000E+00	1.386E-05	99
100	33	49	86000.0	35250.0	-193.0	107.0	107.0	107.0	SWMP	0.000E+00	1.382E+05	0.000E+00	0.000E+00	1.374E-05	100

## -----NODE AND FLOW DATA-----

-NODE DATA-		X-COORD	Y-COORD	BASE-EL	MAX-EL	INIT-W/T	NEW-W/T	BOUN	FIXED-INF	INFILT_INF	STORE_INF	STREAM_INF	OUTFLOW	NODE
#	LNK	INT	[L]	[L]	[L]	[L]	[L]	DARY	[L3/T]	[L3/T]	[L3/T]	[L3/T]	[L3/T]	#
101	32	47	85390.0	34760.0	-189.0	111.0	111.0	111.0	SWMP	0.000E+00	1.314E+05	0.000E+00	4.186E+05	5.541E+05 101
102	31	54	85400.0	34300.0	-209.0	91.0	91.0	91.0	SWMP	0.000E+00	1.155E+05	0.000E+00	1.331E+04	1.378E+05 102
103	105	44	85175.0	34000.0	-214.0	86.0	86.0	86.0	SWMP	0.000E+00	5.563E+04	0.000E+00	3.712E-04	6.333E+04 103
104	40	43	84875.0	33300.0	-233.0	67.0	67.0	67.0	SWMP	0.000E+00	3.574E+04	0.000E+00	0.000E+00	1.366E+04 104
105	106	42	85150.0	33700.0	-241.0	59.0	59.0	59.0	SWMP	0.000E+00	1.021E+05	0.000E+00	1.108E+05	2.230E+05 105
106	9	41	85350.0	33250.0	-248.0	52.0	52.0	52.0	SWMP	0.000E+00	9.297E+04	0.000E+00	8.353E-06	6.426E+05 106
107	7	40	85825.0	33750.0	-212.0	38.0	38.0	38.0	SWMP	0.000E+00	4.253E-05	0.000E+00	0.000E+00	3.225E+05 107
108	8	22	87000.0	33700.0	-240.0	60.0	60.0	60.0	SWMP	0.000E+00	6.373E+03	0.000E+00	0.000E+00	6.675E+05 108
109	3	19	86500.0	33700.0	-225.0	75.0	75.0	75.0	SWMP	0.000E+00	1.304E-06	0.000E+00	0.000E+00	1.813E-06 109
110	7	17	88250.0	35000.0	-245.0	55.0	55.0	55.0	SWMP	0.000E+00	9.338E+05	0.000E+00	0.000E+00	1.097E+05 110
111	72	13	87000.0	34450.0	-250.0	50.0	50.0	50.0	SWMP	0.000E+00	3.706E+05	0.000E+00	6.322E-05	1.524E+06 111
112	111	16	87000.0	33600.0	-175.0	105.0	105.0	105.0	SWMP	0.000E+00	6.772E+05	0.000E+00	0.000E+00	6.688E-05 112
113	2	15	87950.0	35550.0	-150.0	150.0	150.0	150.0	SWMP	0.000E+00	1.422E+06	0.000E+00	0.000E+00	1.155E+06 113
114	115	29	87000.0	37000.0	-210.0	90.0	90.0	90.0	SWMP	0.000E+00	1.097E+06	0.000E+00	7.698E+05	1.395E+06 114
115	1	23	87800.0	33000.0	-240.0	60.0	60.0	60.0	SWMP	0.000E+00	1.437E+06	0.000E+00	1.393E-06	7.398E+05 115
116	27	27	85700.0	37500.0	-170.0	100.0	100.0	100.0	SWMP	0.000E+00	1.330E+06	0.000E+00	0.000E+00	1.332E+05 116
117	114	26	85450.0	36550.0	-115.0	185.0	185.0	185.0	SWMP	0.000E+00	9.173E+05	0.000E+00	0.000E+00	7.698E+05 117
118	29	25	80900.0	32600.0	-255.0	555.0	555.0	555.0	SWMP	0.000E+00	9.344E+05	0.000E+00	0.000E+00	5.333E+05 118
119	13	24	82000.0	32100.0	-150.0	150.0	150.0	150.0	SWMP	0.000E+00	1.092E+06	0.000E+00	0.000E+00	1.248E+06 119
120	74	23	81900.0	33200.0	-225.0	525.0	525.0	525.0	SWMP	0.000E+00	5.322E+05	0.000E+00	0.000E+00	2.337E+05 120
121	27	21	82350.0	34200.0	-105.0	405.0	405.0	405.0	SWMP	0.000E+00	4.331E+05	0.000E+00	0.000E+00	2.732E+05 121
122	12	20	83300.0	32700.0	-210.0	90.0	90.0	90.0	SWMP	0.000E+00	3.322E+05	0.000E+00	9.324E+05	1.412E+06 122
123	125	14	84680.0	35080.0	-157.0	133.0	133.0	133.0	SWMP	0.000E+00	2.361E+04	0.000E+00	6.672E+04	1.036E+05 123
124	125	13	85090.0	35160.0	-178.0	122.0	122.0	122.0	SWMP	0.000E+00	4.701E+04	0.000E+00	0.000E+00	7.335E+04 124
125	101	12	85230.0	34870.0	-186.0	114.0	114.0	114.0	SWMP	0.000E+00	3.610E+04	0.000E+00	1.775E+05	2.282E+05 125
126	101	11	84810.0	34780.0	-171.0	129.0	129.0	129.0	SWMP	0.000E+00	4.589E+04	0.000E+00	1.160E+05	1.220E+05 126
127	36	10	85180.0	35260.0	-170.0	130.0	130.0	130.0	SWMP	0.000E+00	6.231E+04	0.000E+00	0.000E+00	1.667E+04 127
128	101	7	85350.0	34840.0	-185.0	115.0	115.0	115.0	SWMP	0.000E+00	2.763E+04	0.000E+00	4.541E+04	6.841E+04 128
129	128	8	85420.0	35020.0	-182.0	118.0	118.0	118.0	SWMP	0.000E+00	2.025E+04	0.000E+00	0.000E+00	1.973E+04 129
130	128	7	85350.0	35200.0	-177.0	123.0	123.0	123.0	SWMP	0.000E+00	1.620E+04	0.000E+00	0.000E+00	2.368E+04 130
131	132	6	85500.0	35230.0	-174.0	126.0	126.0	126.0	SWMP	0.000E+00	1.270E+04	0.000E+00	1.395E+04	2.318E+04 131
132	133	5	85560.0	35060.0	-185.0	115.0	115.0	115.0	SWMP	0.000E+00	1.140E+04	0.000E+00	2.318E+04	3.222E+04 132
133	52	4	85740.0	34990.0	-195.0	105.0	105.0	105.0	SWMP	0.000E+00	1.023E+05	0.000E+00	3.222E+04	1.379E+05 133
134	131	3	85540.0	35280.0	-173.0	127.0	127.0	127.0	SWMP	0.000E+00	4.088E+04	0.000E+00	0.000E+00	1.395E+04 134
135	53	2	84050.0	35050.0	-145.0	155.0	155.0	155.0	SWMP	0.000E+00	5.766E+04	0.000E+00	7.254E+05	3.540E+05 135
136	57	1	84060.0	34865.0	-115.0	135.0	137.3	137.3	SWMP	0.000E+00	5.463E+03	0.000E+00	0.000E+00	1.151E+00 136

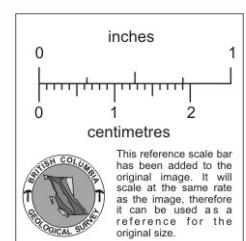
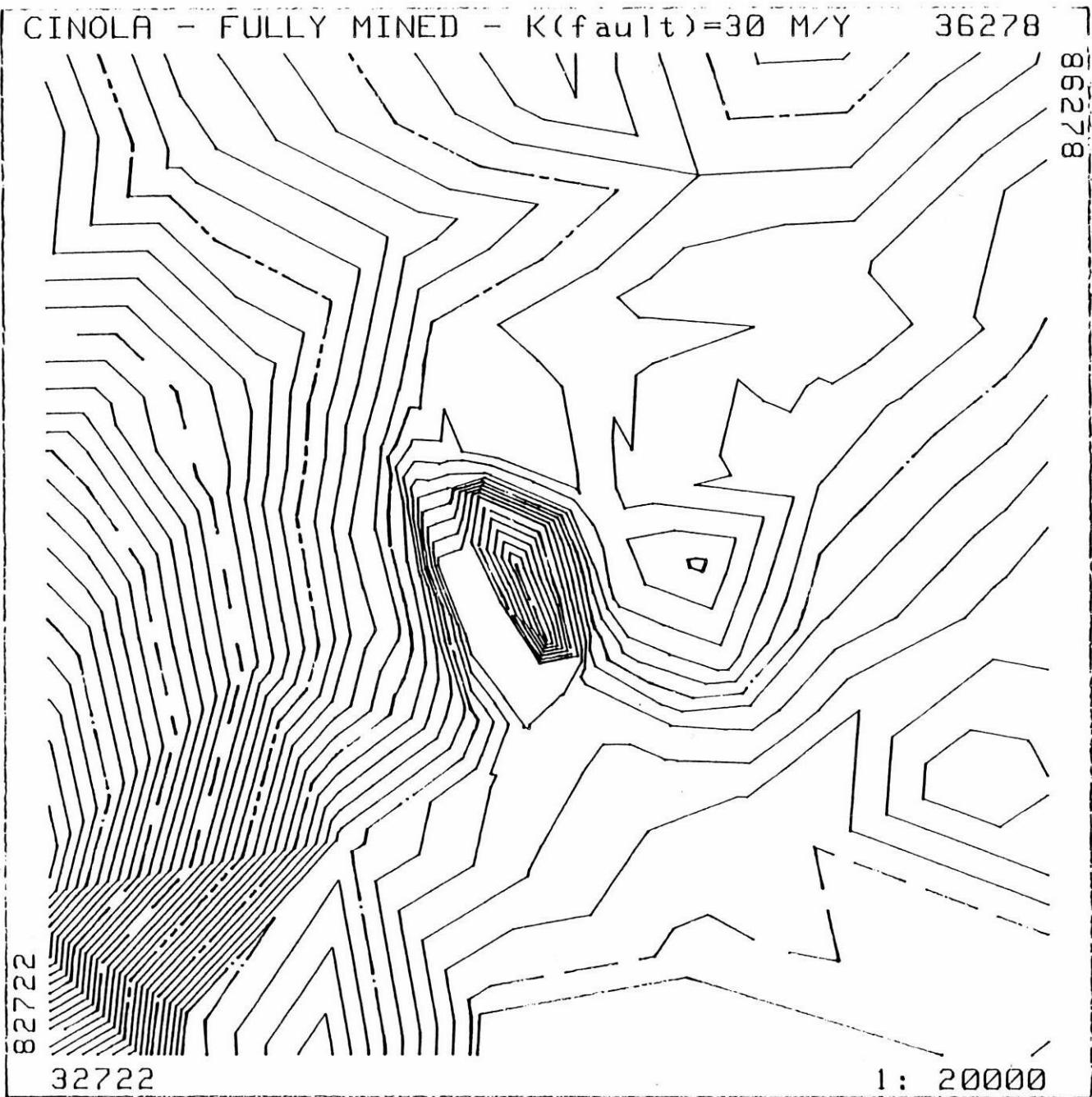
## -----SINK FLOW DATA-----

SINK	CONN	TOT_FLOW												
#	#	[L3/T]												
0	0	0.0000E+00												
1	2	5.9371E+07	2	27	5.7455E-05	3	0	0.0000E+00	4	0	0.0000E+00	5	0	0.0000E+00
5	0	0.0000E+00	7	0	0.0000E+00	8	0	0.0000E+00	9	0	0.0000E+00	10	0	0.0000E+00
11	0	0.0000E+00	12	0	0.0000E+00	13	0	0.0000E+00	14	0	0.0000E+00	15	0	0.0000E+00
15	0	0.0000E+00	17	0	0.0000E+00	18	0	0.0000E+00	19	0	0.0000E+00	20	0	0.0000E+00

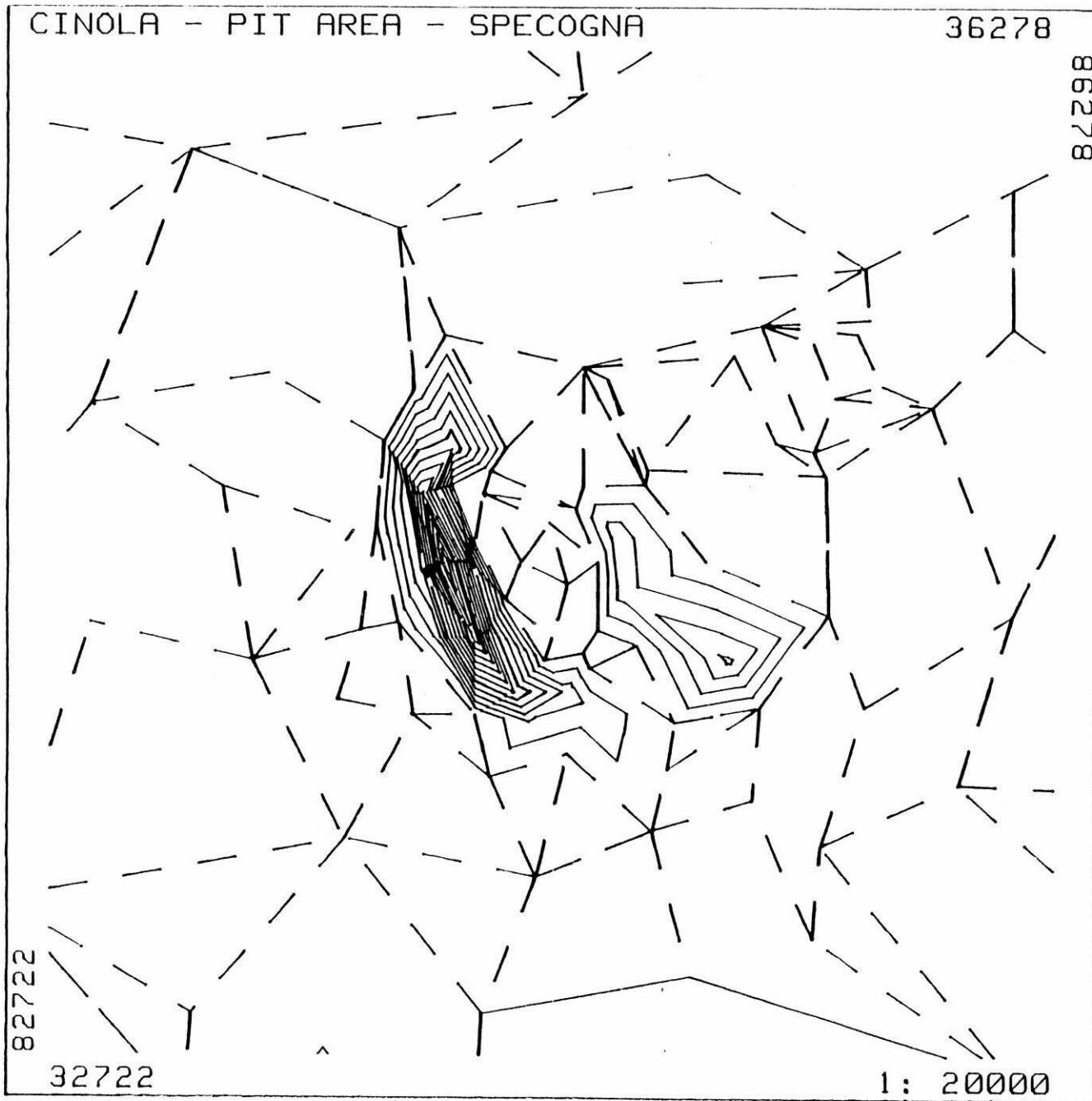
-----ELEMENT DATA-----

ELEM	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	ELEM	
Node1	96	27	27	76	28	120	94	120	120	118	118	15	118	118	15	29	16	16	27	17	26	26	98	26	18	18	24	19	20	23	Node1	
Node2	26	121	28	121	120	94	95	119	118	14	15	118	28	120	29	28	28	27	26	26	23	98	26	96	25	24	23	23	22	Node2		
Node3	27	96	121	95	121	121	121	94	119	119	14	29	29	28	16	16	27	17	17	19	18	25	97	27	24	19	19	20	21	21	Node3	
Mati	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	3	3	1	1	1	3	3	3	3	Mati
Soil	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	3	3	1	1	1	3	3	3	3	Soil
ELEM	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	ELEM	
Node1	23	23	24	116	115	117	116	115	34	114	113	114	112	113	33	112	110	112	111	109	109	109	109	109	109	108	108	108	7	7	8	Node1
Node2	116	24	117	115	1	114	114	2	114	113	2	34	113	3	112	110	3	33	110	3	110	4	5	6	108	109	7	108	107	7	Node2	
Node3	22	116	115	22	22	116	115	1	117	115	115	112	114	2	34	117	113	111	112	110	111	3	4	5	6	111	6	107	30	30	Node3	
Mati	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	Mati	
Soil	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	Soil	
ELEM	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	ELEM	
Node1	8	9	106	106	50	39	107	31	31	103	103	103	103	103	102	102	101	101	103	32	33	32	107	35	100	133	100	36	99	35	117	Node1
Node2	30	106	105	50	31	107	32	32	102	105	104	67	86	102	84	101	102	101	33	32	107	108	100	33	100	35	36	34	25	Node2		
Node3	106	9	3	105	105	31	31	102	103	31	105	104	37	86	86	84	32	32	100	111	111	111	34	34	134	36	117	117	117	99	Node3	
Mati	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	Mati	
Soil	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	Soil	
ELEM	91	92	93	94	95	96	97	98	99	100	101	102	103	104	105	106	107	108	109	110	111	112	113	114	115	116	117	118	119	120	ELEM	
Node1	25	99	98	36	62	127	37	127	83	63	83	83	61	60	70	76	73	77	71	71	72	82	63	85	85	65	64	84	64	84	Node1	
Node2	98	98	38	62	127	36	36	134	84	62	61	82	82	70	71	71	77	72	62	72	63	63	86	87	65	85	63	72	72	72	Node2	
Node3	99	37	37	37	37	37	99	36	101	64	62	61	60	61	61	70	71	71	61	62	62	84	84	83	86	87	64	63	72	76	Node3	
Mati	3	3	3	3	3	3	3	3	3	3	3	3	3	3	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	Mati	
Soil	3	3	3	3	3	3	3	3	3	3	3	3	3	3	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	Soil	
ELEM	121	122	123	124	125	126	127	128	129	130	131	132	133	134	135	136	137	138	139	140	141	142	143	144	145	146	147	148	149	150	ELEM	
Node1	78	78	78	78	79	79	79	66	65	88	88	40	40	40	91	91	41	89	89	89	89	66	66	73	73	73	55	55	55	55	55	Node1
Node2	72	77	81	30	64	53	66	88	88	104	40	105	9	91	40	41	89	43	55	66	88	41	73	79	79	80	74	73	67	56	Node2	
Node3	77	81	60	79	78	64	65	65	87	87	104	104	105	9	41	42	42	42	43	55	66	88	55	73	80	74	67	56	43	43	Node3	
Mati	4	4	4	4	4	4	4	3	3	3	3	3	3	2	2	2	2	2	2	5	5	5	5	4	4	4	4	5	5	2	Mati	
Soil	4	4	4	4	4	4	4	3	3	3	3	3	3	2	2	2	2	2	2	3	3	3	4	4	4	4	4	4	4	2	Soil	
ELEM	151	152	153	154	155	156	157	158	159	160	161	162	163	164	165	166	167	168	169	170	171	172	173	174	175	176	177	178	179	180	ELEM	
Node1	43	43	44	50	56	56	56	68	74	74	74	81	81	75	68	68	68	59	69	70	60	60	60	135	37	58	58	57	51	45	Node1	
Node2	56	50	50	53	57	68	67	67	75	81	80	77	76	76	75	58	69	69	70	60	82	38	37	135	136	39	57	52	52	52	Node2	
Node3	50	44	51	51	51	57	68	74	68	75	81	76	75	69	57	58	59	59	59	38	59	136	97	37	52	58	51	45	39	Node3		
Mati	2	2	2	2	2	3	3	3	3	3	3	3	3	2	2	2	2	2	2	3	3	3	2	1	2	2	2	2	2	2	Mati	
Soil	2	3	3	2	2	4	4	4	4	4	4	4	4	4	4	4	4	4	4	3	3	2	1	2	2	2	2	2	2	3	Soil	
ELEM	181	182	183	184	185	186	187	188	189	190	191	192	193	194	195	196	197	198	199	200	201	202	203	204	205	206	207	208	209	210	ELEM	
Node1	135	37	46	45	54	54	44	49	49	41	42	42	91	91	92	93	94	94	47	90	48	48	47	47	47	47	47	46	97	94	Node1	
Node2	98	97	53	39	45	44	51	44	43	40	43	49	42	30	10	11	92	93	90	90	49	49	54	54	53	46	95	96	96	122	Node2	
Node3	97	46	37	53	53	45	45	54	44	38	49	30	30	10	9	10	90	90	47	48	48	54	47	53	46	95	96	96	93	Nodes3		
Mati	1	1	1	2	2	2	2	2	2	3	3	2	2	2	2	2	1	1	1	1	2	2	1	1	1	1	1	1	1	1	Mati	
Soil	1	1	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	1	1	1	1	1	1	3	3	3	3	1	1	1	1	Soil

-----ELEMENT DATA-----



HEADS  
CURRENT

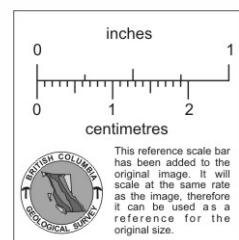


Legend:

- 0
- 50
- 100

(meters)

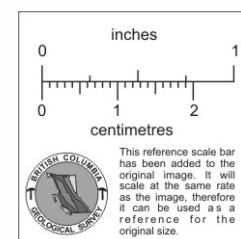
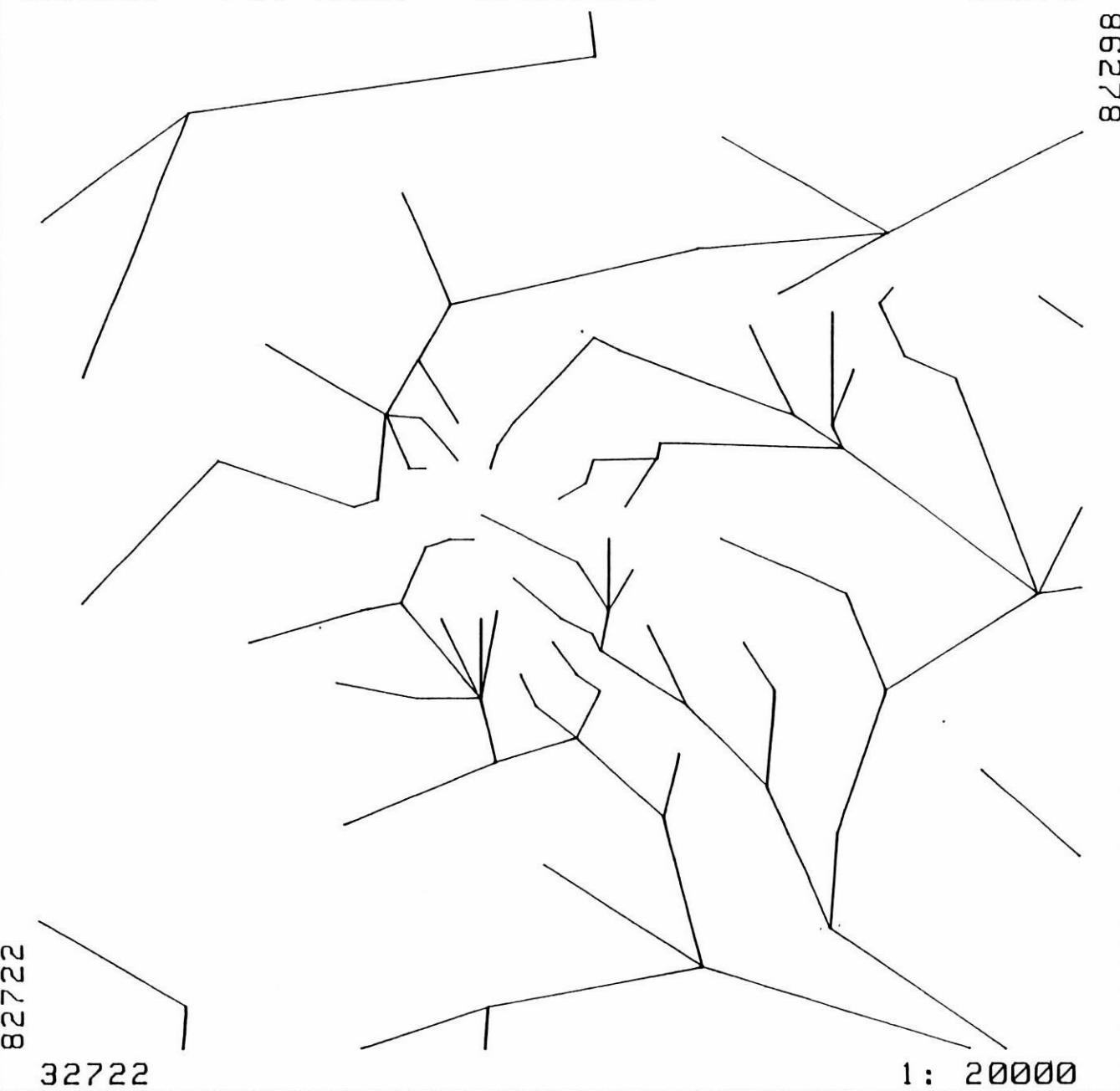
Interval:  
10 meters



HEADS  
DEPTH > CURR

CINOLA - PIT AREA - SPECOGNA

36278



STREAMS  
LOCATIONS

6

-----KEY ANALYSIS PARAMETERS-----

Number of nodes.....133  
Number of elements.....248  
Number of materials.....6  
Number of soils.....7

-----MATERIAL AND SOIL DATA-----

MATERIAL OR SOIL	HYDRAULIC CONDUCTIVITY [L/T]	SPECIFIC STORAGE [L/L]	SPECIFIC YIELD [-]	DISTRIBUTED INFLOW [L/T]
1	1.00E-00	1.00E-06	.0200	7.50E-01
2	1.00E-01	1.00E-06	.0200	7.50E-02
3	1.00E+00	1.00E-06	.0300	7.50E-01
4	1.00E-00	1.00E-06	.0300	7.50E-01
5	1.00E-00	1.00E-06	.0200	7.50E-01
6	1.00E-00	1.00E-06	.0300	7.50E-01
7				7.50E-01

## -----NODE AND FLOW DATA-----

-NODE DATA-		X-COORD	Y-COORD	BASE-EL	MAX-EL	INIT-W/T	NEW-W/T	BOUN	FIXED-INF	INFILT_INF	STORE_INF	STREAM_INF	OUTFLOW	NODE
#	LNK INT	[L]	[L]	[L]	[L]	[L]	[L]	DARY	[L/T]	[L/T]	[L/T]	[L/T]	[L/T]	#
1	-1 136	38750.0	39150.0	-280.0	20.0	20.0	20.0	SWMP	0.000E+00	3.481E+05	0.000E+00	2.713E+07	1.753E+07	1
2	1 134	39000.0	37400.0	-280.0	20.0	20.0	20.0	SWMP	0.000E+00	1.015E+06	0.000E+00	2.191E+07	2.299E+07	2
3	2 131	30000.0	36000.0	-275.0	25.0	25.0	25.0	SWMP	0.000E+00	1.220E+06	0.000E+00	1.952E+07	2.073E+07	3
4	3 132	34950.0	34000.0	-275.0	25.0	25.0	25.0	SWMP	0.000E+00	6.966E+05	0.000E+00	1.586E+07	1.561E+07	4
5	4 133	39000.0	31650.0	-270.0	30.0	30.0	30.0	SWMP	0.000E+00	6.703E+05	0.000E+00	1.518E+07	1.536E+07	5
6	5 130	37600.0	32500.0	-265.0	35.0	35.0	35.0	SWMP	0.000E+00	6.169E+05	0.000E+00	1.454E+07	1.513E+07	6
7	6 127	36350.0	32950.0	-265.0	35.0	35.0	35.0	SWMP	0.000E+00	7.719E+05	0.000E+00	1.347E+07	1.367E+07	7
8	7 128	36000.0	32600.0	-260.0	40.0	40.0	40.0	SWMP	0.000E+00	1.420E+05	0.000E+00	1.299E+07	1.314E+07	8
9	8 127	34950.0	33125.0	-255.0	45.0	45.0	45.0	SWMP	0.000E+00	8.513E+04	0.000E+00	6.313E+06	6.417E+06	9
10	9 124	34275.0	35000.0	-255.0	45.0	45.0	45.0	SWMP	0.000E+00	1.257E+05	0.000E+00	6.542E+06	4.705E+06	10
11	10 121	34200.0	31900.0	-250.0	50.0	50.0	50.0	SWMP	0.000E+00	1.226E+05	0.000E+00	4.518E+06	4.548E+06	11
12	11 120	33500.0	31200.0	-250.0	50.0	50.0	50.0	SWMP	0.000E+00	5.222E+05	0.000E+00	4.072E+06	4.518E+06	12
13	12 74	32300.0	31450.0	-245.0	55.0	55.0	55.0	SWMP	0.000E+00	3.044E+05	0.000E+00	2.162E+06	2.548E+06	13
14	13 73	30500.0	30600.0	-240.0	60.0	60.0	60.0	SWMP	0.000E+00	7.656E+05	0.000E+00	0.000E+00	5.150E+05	14
15	17 122	77500.0	32750.0	370.0	670.0	670.0	670.0	SWMP	0.000E+00	5.319E+05	0.000E+00	0.000E+00	4.799E+05	15
16	17 119	31000.0	34500.0	35.0	375.0	375.0	375.0	SWMP	0.000E+00	5.400E+05	0.000E+00	0.000E+00	5.500E+05	16
17	16 118	32300.0	36000.0	-25.0	275.0	275.0	275.0	SWMP	0.000E+00	4.347E+05	0.000E+00	0.000E+00	3.161E+05	17
18	24 117	33200.0	37100.0	-150.0	150.0	150.0	150.0	SWMP	0.000E+00	7.332E+05	0.000E+00	0.000E+00	1.162E+05	18
19	23 114	34550.0	38650.0	-130.0	120.0	120.0	120.0	SWMP	0.000E+00	6.274E+05	0.000E+00	0.000E+00	5.740E+05	19
20	-1 115	36200.0	40400.0	-240.0	60.0	60.0	60.0	SWMP	0.000E+00	4.025E+05	0.000E+00	1.212E+07	1.254E+07	20
21	20 116	37000.0	39700.0	-235.0	65.0	65.0	65.0	SWMP	0.000E+00	5.237E+05	0.000E+00	1.176E+07	1.212E+07	21
22	1 113	37200.0	39000.0	-180.0	120.0	120.0	120.0	SWMP	0.000E+00	6.331E+05	0.000E+00	0.000E+00	7.335E+05	22
23	21 112	36000.0	39000.0	-210.0	90.0	90.0	90.0	SWMP	0.000E+00	1.373E+05	0.000E+00	1.036E+07	1.176E+07	23
24	23 111	34400.0	37450.0	-195.0	105.0	105.0	105.0	SWMP	0.000E+00	1.173E+05	0.000E+00	7.150E+06	6.412E+06	24
25	24 110	34600.0	38000.0	-180.0	120.0	120.0	120.0	SWMP	0.000E+00	7.487E+05	0.000E+00	5.215E+06	6.065E+06	25
26	25 109	33325.0	35825.0	-115.0	165.0	165.0	165.0	SWMP	0.000E+00	7.426E+05	0.000E+00	4.338E+06	5.215E+06	26
27	26 108	32200.0	35000.0	-25.0	275.0	275.0	275.0	SWMP	0.000E+00	6.241E+05	0.000E+00	5.236E+06	4.105E+06	27
28	27 107	31700.0	34000.0	65.0	365.0	365.0	365.0	SWMP	0.000E+00	6.200E+05	0.000E+00	1.700E+06	2.452E+06	28
29	23 104	30600.0	32900.0	160.0	460.0	460.0	460.0	SWMP	0.000E+00	5.069E+05	0.000E+00	1.012E+06	1.700E+06	29
30	106 100	35375.0	33550.0	-250.0	50.0	50.0	50.0	SWMP	0.000E+00	2.316E+05	0.000E+00	5.760E+06	6.272E+06	30
31	30 79	35525.0	34000.0	-240.0	60.0	60.0	60.0	SWMP	0.000E+00	1.119E+05	0.000E+00	5.313E+06	5.300E+06	31
32	31 78	36000.0	34300.0	-235.0	64.0	64.0	64.0	SWMP	0.000E+00	5.396E+05	0.000E+00	5.299E+06	5.678E+06	32
33	32 77	36350.0	35000.0	-223.0	77.0	77.0	77.0	SWMP	0.000E+00	5.262E+05	0.000E+00	2.633E+06	2.997E+06	33
34	33 76	36400.0	35800.0	-195.0	105.0	105.0	105.0	SWMP	0.000E+00	4.774E+05	0.000E+00	1.273E+05	2.471E+06	34
35	34 75	36000.0	35700.0	-190.0	110.0	110.0	110.0	SWMP	0.000E+00	1.731E+05	0.000E+00	1.724E+06	1.979E+06	35
36	35 74	35525.0	35450.0	-179.0	121.0	121.0	121.0	SWMP	0.000E+00	2.190E+05	0.000E+00	1.549E+06	1.784E+06	36
37	36 73	34925.0	35400.0	-175.0	125.0	125.0	125.0	SWMP	0.000E+00	1.513E+05	0.000E+00	1.152E+06	1.344E+06	37
38	37 72	35525.0	35225.0	-155.0	145.0	145.0	145.0	SWMP	0.000E+00	9.677E+04	0.000E+00	5.510E+05	1.152E+06	38
39	38 72	35750.0	34675.0	-133.0	162.0	162.0	162.0	SWMP	0.000E+00	5.684E+04	0.000E+00	5.406E+05	7.347E+05	39
40	39 71	34825.0	33300.0	-240.0	60.0	60.0	60.0	SWMP	0.000E+00	4.751E+04	0.000E+00	1.248E+06	1.394E+06	40
41	40 70	34550.0	33650.0	-227.0	73.0	73.0	73.0	SWMP	0.000E+00	1.405E+04	0.000E+00	1.199E+06	1.237E+06	41
42	41 69	34300.0	33775.0	-219.0	61.0	61.0	61.0	SWMP	0.000E+00	6.625E+03	0.000E+00	7.655E+05	7.769E+05	42
43	42 68	34250.0	33775.0	-195.0	105.0	105.0	105.0	SWMP	0.000E+00	1.253E+04	0.000E+00	5.773E+05	5.766E+05	43
44	43 63	34000.0	34275.0	-136.0	164.0	164.0	164.0	SWMP	0.000E+00	2.857E+04	0.000E+00	2.567E+05	2.383E+05	44
45	45 63	33725.0	34600.0	-138.0	162.0	162.0	162.0	SWMP	0.000E+00	2.250E+04	0.000E+00	4.682E+05	4.736E+05	45
46	46 67	33425.0	34725.0	-55.0	245.0	245.0	245.0	SWMP	0.000E+00	1.680E+05	0.000E+00	1.341E+05	3.395E+05	46
47	54 105	33525.0	34150.0	-35.0	245.0	245.0	245.0	SWMP	0.000E+00	2.555E+05	0.000E+00	0.000E+00	1.799E+05	47
48	48 84	33800.0	34025.0	-122.0	178.0	178.0	178.0	SWMP	0.000E+00	3.238E+04	0.000E+00	0.000E+00	7.114E+04	48
49	49 102	34050.0	33975.0	-160.0	140.0	140.0	140.0	SWMP	0.000E+00	2.355E+04	0.000E+00	7.114E+04	6.151E+04	49
50	47 83	34125.0	34225.0	-141.0	159.0	159.0	159.0	SWMP	0.000E+00	7.070E+03	0.000E+00	0.000E+00	7.407E+02	50

## -----NODE AND FLOW DATA-----

-NODE DATA-	X-COORD	Y-COORD	BASE-EL	MAX-EL	INIT-W/T	NEW-W/T	BOUN	FIXED-INF	INFILT_INF	STORE_INF	STREAM_INF	OUTFLOW	NODE
#	LNK	INT	[L]	[L]	[L]	[L]	[L]	DARY	[L3/T]	[L3/T]	[L3/T]	[L3/T]	#
51	44	126	84075.0	34450.0	-115.0	185.0	185.0	167.8 SWAO	0.000E+00	1.251E+04	0.000E+00	0.000E+00	-1.945E-02
52	39	62	84025.0	34700.0	-115.0	185.0	185.0	157.9 SWAO	0.000E+00	7.375E+03	0.000E+00	0.000E+00	1.338E-02
53	45	123	83850.0	34575.0	-130.0	170.0	170.0	170.0 SWMP	0.000E+00	6.664E+04	0.000E+00	3.395E+05	4.682E+05
54	44	125	83875.0	34250.0	-124.0	176.0	176.0	176.0 SWMP	0.000E+00	4.422E+04	0.000E+00	1.779E+05	2.587E+05
55	66	101	84375.0	34050.0	-171.0	129.0	126.8	111.7 SWAO	0.000E+00	5.391E+03	0.000E+00	0.000E+00	-2.636E-01
56	67	75	84250.0	34225.0	-120.0	180.0	172.0	125.1 SWAO	0.000E+00	5.867E+03	0.000E+00	0.000E+00	1.020E-01
57	68	65	84150.0	34175.0	-96.0	204.0	198.3	122.7 SWAO	0.000E+00	5.109E+03	0.000E+00	0.000E+00	1.411E-01
58	69	65	84075.0	34700.0	-84.0	208.0	199.2	138.3 SWAO	0.000E+00	5.772E+03	0.000E+00	0.300E+00	2.211E-01
59	76	64	84175.0	34650.0	-98.0	202.0	187.8	149.2 SWAO	0.000E+00	2.533E+04	0.000E+00	0.000E+00	1.088E-01
60	70	79	84350.0	34850.0	-117.0	163.0	163.0	142.9 SWAO	0.000E+00	4.378E+04	0.000E+00	0.000E+00	2.261E-02
61	71	62	84600.0	34725.0	-146.0	154.0	154.0	135.0 SWAO	0.000E+00	5.333E+04	0.000E+00	0.000E+00	-2.829E-03
62	72	72	84700.0	34575.0	-135.0	165.0	164.3	137.0 SWAO	0.000E+00	2.506E+04	0.000E+00	0.000E+00	7.398E-02
63	64	73	84725.0	34375.0	-130.0	170.0	162.0	136.0 SWAO	0.000E+00	5.154E+04	0.000E+00	0.000E+00	3.708E-01
64	77	61	84650.0	34250.0	-170.0	130.0	130.0	125.8 SWAO	0.000E+00	1.188E+04	0.000E+00	3.708E-01	-4.560E-01
65	66	71	84625.0	34125.0	-200.0	100.0	100.0	100.0 SWMP	0.000E+00	1.447E+04	0.000E+00	0.000E+00	7.470E-04
66	83	77	84550.0	34050.0	-195.0	122.0	105.0	122.0 SWMP	0.000E+00	5.766E+03	0.000E+00	4.570E+08	5.506E-05
67	73	60	84300.0	34250.0	-110.0	122.0	171.3	122.0 SWMP	0.000E+00	1.172E+04	0.000E+00	1.020E-01	1.796E-04
68	74	70	84225.0	34475.0	-83.0	122.0	198.1	122.0 SWMP	0.000E+00	1.453E+04	0.000E+00	1.411E-01	3.229E-04
69	76	59	84175.0	34725.0	-85.0	122.0	200.0	122.0 SWMP	0.000E+00	1.102E+04	0.000E+00	2.211E-01	5.463E-04
70	75	53	84300.0	34775.0	-96.0	122.0	199.3	122.0 SWMP	0.000E+00	1.337E+04	0.000E+00	2.261E-02	6.699E+04
71	77	67	84575.0	34650.0	-130.0	122.0	170.0	122.0 SWMP	0.000E+00	1.411E+04	0.000E+00	-2.829E-03	5.181E+04
72	78	76	84650.0	34475.0	-125.0	122.0	177.4	122.0 SWMP	0.000E+00	1.391E+04	0.000E+00	7.398E-02	4.366E-04
73	68	81	84475.0	34150.0	-145.0	122.0	136.3	122.0 SWMP	0.000E+00	1.313E+04	0.000E+00	1.796E-04	2.286E-04
74	80	57	84350.0	34350.0	-80.0	122.0	182.5	122.0 SWMP	0.000E+00	1.445E+04	0.000E+00	3.229E+04	4.674E+04
75	81	68	84250.0	34550.0	-85.0	122.0	200.3	122.0 SWMP	0.000E+00	1.063E+04	0.000E+00	0.000E+00	1.063E+04
76	81	74	84275.0	34700.0	-88.0	122.0	205.7	122.0 SWMP	0.000E+00	1.588E+04	0.000E+00	1.216E-05	1.375E+05
77	81	60	84490.0	34600.0	-115.0	122.0	185.0	122.0 SWMP	0.000E+00	1.547E+04	0.000E+00	5.181E+04	6.723E+04
78	80	56	84550.0	34400.0	-135.0	122.0	165.0	122.0 SWMP	0.000E+00	1.719E+04	0.000E+00	4.366E+04	7.082E+04
79	66	57	84600.0	34175.0	-175.0	122.0	123.2	115.3 SWAO	0.000E+00	8.515E+03	0.000E+00	-4.550E-01	4.451E-02
80	66	73	84500.0	34225.0	-140.0	122.0	150.0	122.0 SWMP	0.000E+00	1.227E+04	0.000E+00	3.534E+05	3.595E+05
81	80	55	84400.0	34475.0	-105.0	122.0	195.0	122.0 SWMP	0.000E+00	2.041E+04	0.000E+00	2.151E+05	2.358E+05
82	123	66	84600.0	35120.0	-162.0	138.0	138.0	138.0 SWMP	0.000E+00	5.374E+04	0.000E+00	0.000E+00	6.346E+04
83	123	38	84800.0	34730.0	-176.0	124.0	124.0	124.0 SWMP	0.000E+00	4.304E+04	0.000E+00	0.000E+00	1.096E+05
84	102	52	85000.0	34475.0	-146.0	152.0	152.0	152.0 SWMP	0.000E+00	8.331E+04	0.000E+00	0.000E+00	1.547E+04
85	87	39	84775.0	34200.0	-170.0	130.0	130.0	127.4 SWAO	0.000E+00	2.523E+04	0.000E+00	0.000E+00	-1.149E-01
86	103	135	85075.0	34150.0	-130.0	170.0	127.7	127.1 SWAO	0.000E+00	5.531E+04	0.000E+00	0.000E+00	7.123E-02
87	105	38	84900.0	33950.0	-220.0	80.0	80.0	80.0 SWMP	0.000E+00	5.484E+04	0.000E+00	-1.149E-01	5.879E+04
88	41	37	84625.0	34000.0	-205.0	95.0	92.7	95.0 SWMP	0.000E+00	3.078E+04	0.000E+00	7.506E-05	3.703E+05
89	41	36	84425.0	33950.0	-207.0	93.0	92.0	93.0 SWMP	0.000E+00	5.242E+03	0.000E+00	0.000E+00	5.157E+04
90	42	35	83825.0	33575.0	-196.0	104.0	104.0	104.0 SWMP	0.000E+00	2.707E+05	0.000E+00	0.000E+00	3.690E+05
91	7	34	84450.0	33450.0	-231.0	69.0	69.0	69.0 SWMP	0.000E+00	1.492E+04	0.000E+00	0.000E+00	1.317E+04
92	10	33	83750.0	32320.0	-150.0	150.0	139.1	138.2 SWAO	0.000E+00	2.514E+05	0.000E+00	0.000E+00	0.000E+00
93	122	52	83325.0	33000.0	-205.0	95.0	95.0	95.0 SWMP	0.000E+00	1.513E+05	0.000E+00	4.760E+05	9.624E+05
94	93	31	82700.0	33375.0	-134.0	434.0	434.0	434.0 SWMP	0.000E+00	6.724E+05	0.000E+00	2.597E+05	4.760E+05
95	46	30	83000.0	34275.0	-40.0	340.0	340.0	340.0 SWMP	0.000E+00	2.677E+05	0.000E+00	0.000E+00	1.841E+05
96	23	106	83000.0	35000.0	-23.0	277.0	277.0	277.0 SWMP	0.000E+00	3.402E+05	0.000E+00	0.000E+00	2.522E+05
97	39	51	83575.0	35100.0	-76.0	224.0	224.0	224.0 SWMP	0.000E+00	1.973E+05	0.000E+00	0.000E+00	1.470E+05
98	33	50	84000.0	35575.0	-122.0	178.0	178.0	178.0 SWMP	0.000E+00	2.653E+05	0.000E+00	0.000E+00	1.256E+05
99	76	48	85000.0	35750.0	-150.0	140.0	140.0	140.0 SWMP	0.000E+00	2.312E+05	0.000E+00	0.000E+00	1.886E+05
100	53	49	86000.0	35250.0	-193.0	107.0	107.0	107.0 SWMP	0.000E+00	1.382E+05	0.000E+00	0.000E+00	1.574E+05

-----NODE AND FLOW DATA-----

-NODE DATA-		X-COORD	Y-COORD	BASE-EL	MAX-EL	INIT-W/T	NEW-W/T	BOUN	FIXED-INF	INFILT_INF	STORE_INF	STREAM_INF	OUTFLOW	NOSE	
#	LNK	INT	[L]	[L]	[L]	[L]	[L]	DARY	[L]/[T]	[L]/[T]	[L]/[T]	[L]/[T]	[L]/[T]	#	
101	32	47	85390.0	34760.0	-189.0	111.0	111.0	111.0	SWMP	0.000E+00	1.314E+05	0.000E+00	4.089E-05	5.445E+05	101
102	31	54	85400.0	34300.0	-209.0	91.0	91.0	91.0	SWMP	0.000E+00	1.155E+05	0.000E+00	1.547E-04	1.405E+05	102
103	105	44	85175.0	34000.0	-214.0	86.0	86.0	86.0	SWMP	0.000E+00	5.583E+04	0.000E+00	7.123E-02	6.511E+04	103
104	40	43	84875.0	33800.0	-233.0	67.0	67.0	67.0	SWMP	0.000E+00	3.594E+04	0.000E+00	0.000E+00	6.113E+04	104
105	106	42	85150.0	33700.0	-241.0	59.0	59.0	59.0	SWMP	0.000E+00	1.021E+05	0.000E+00	1.237E+05	1.382E+05	105
106	3	41	85350.0	33250.0	-243.0	52.0	52.0	52.0	SWMP	0.000E+00	7.297E+04	0.000E+00	6.508E+05	6.581E+04	106
107	7	40	85325.0	33750.0	-212.0	88.0	88.0	88.0	SWMP	0.000E+00	4.255E+05	0.000E+00	0.000E+00	7.225E+05	107
108	3	22	87000.0	33700.0	-140.0	60.0	60.0	60.0	SWMP	0.000E+00	6.373E+05	0.000E+00	0.000E+00	6.395E+05	108
109	3	19	88500.0	33700.0	-225.0	75.0	75.0	75.0	SWMP	0.000E+00	1.404E+06	0.000E+00	0.000E+00	1.813E+06	109
110	7	17	68250.0	35000.0	-245.0	55.0	55.0	55.0	SWMP	0.000E+00	9.347E+05	0.000E+00	0.000E+00	1.097E+06	110
111	32	18	87000.0	34450.0	-250.0	50.0	50.0	50.0	SWMP	0.000E+00	8.206E+05	0.000E+00	6.886E+05	1.624E+06	111
112	111	16	87000.0	35300.0	-175.0	105.0	105.0	105.0	SWMP	0.000E+00	6.772E+05	0.000E+00	1.000E+00	6.382E+05	112
113	1	15	87950.0	35550.0	-150.0	150.0	150.0	150.0	SWMP	0.000E+00	1.422E+06	0.000E+00	0.000E+00	1.155E+06	113
114	115	27	87000.0	37000.0	-210.0	70.0	70.0	70.0	SWMP	0.000E+00	1.087E+06	0.000E+00	7.398E+05	1.275E+06	114
115	1	23	87300.0	36000.0	-240.0	60.0	60.0	60.0	SWMP	0.000E+00	1.437E+06	0.000E+00	1.375E+06	3.398E+06	115
116	23	27	85700.0	37500.0	-170.0	130.0	130.0	130.0	SWMP	0.000E+00	1.399E+06	0.000E+00	0.000E+00	1.352E+06	116
117	114	26	85450.0	36550.0	-115.0	185.0	185.0	185.0	SWMP	0.000E+00	7.177E+05	0.000E+00	0.000E+00	7.895E+05	117
118	29	25	80900.0	32600.0	215.0	585.0	585.0	585.0	SWMP	0.000E+00	7.844E+05	0.000E+00	0.000E+00	5.373E+05	118
119	13	24	82000.0	32100.0	-150.0	150.0	150.0	150.0	SWMP	0.000E+00	1.092E+06	0.000E+00	0.000E+00	1.246E+06	119
120	94	23	81900.0	33200.0	222.0	525.0	525.0	525.0	SWMP	0.000E+00	5.523E+05	0.000E+00	0.000E+00	1.377E+05	120
121	27	21	82250.0	34200.0	105.0	405.0	405.0	405.0	SWMP	0.000E+00	4.381E+05	0.000E+00	0.000E+00	2.739E+05	121
122	12	20	83300.0	32700.0	-210.0	90.0	90.0	90.0	SWMP	0.000E+00	1.522E+05	0.000E+00	7.324E+05	1.412E+06	122
123	125	14	84620.0	35080.0	-167.0	133.0	133.0	133.0	SWMP	0.000E+00	1.361E+04	0.000E+00	6.346E+04	1.004E+05	123
124	125	13	85090.0	35150.0	-173.0	122.0	122.0	122.0	SWMP	0.000E+00	4.701E+04	0.000E+00	0.000E+00	7.385E+04	124
125	101	12	85230.0	34870.0	-188.0	114.0	114.0	114.0	SWMP	0.000E+00	3.610E+04	0.000E+00	1.742E+05	2.249E+05	125
126	101	11	84610.0	34780.0	-171.0	129.0	129.0	129.0	SWMP	0.000E+00	4.589E+04	0.000E+00	1.095E+05	1.156E+05	126
127	36	10	85130.0	35260.0	-170.0	130.0	130.0	130.0	SWMP	0.000E+00	6.231E+04	0.000E+00	0.000E+00	1.667E+04	127
128	101	9	85350.0	34640.0	-195.0	115.0	115.0	115.0	SWMP	0.000E+00	1.963E+04	0.000E+00	4.341E+04	6.241E+04	128
129	123	8	85420.0	35020.0	-182.0	118.0	118.0	118.0	SWMP	0.000E+00	2.025E+04	0.000E+00	0.000E+00	1.973E+04	129
130	128	7	85350.0	35100.0	-177.0	123.0	123.0	123.0	SWMP	0.000E+00	1.620E+04	0.000E+00	0.000E+00	2.863E+04	130
131	132	6	85500.0	35230.0	-174.0	126.0	126.0	126.0	SWMP	0.000E+00	1.270E+04	0.000E+00	1.875E+04	2.318E+04	131
132	133	5	85580.0	35060.0	-185.0	115.0	115.0	115.0	SWMP	0.000E+00	1.140E+04	0.000E+00	2.318E+04	2.222E+04	132
133	32	4	85740.0	34790.0	-195.0	105.0	105.0	105.0	SWMP	0.000E+00	1.023E+05	0.000E+00	7.222E+04	1.379E+05	133
134	131	3	85540.0	35280.0	-173.0	127.0	127.0	127.0	SWMP	0.000E+00	4.088E+04	0.000E+00	0.000E+00	1.395E+04	134
135	33	2	84050.0	35050.0	-145.0	155.0	155.0	155.0	SWMP	0.000E+00	5.766E+04	0.000E+00	7.347E+05	7.654E+05	135
136	37	1	84060.0	34865.0	-115.0	185.0	183.5	180.8	SWMP	0.000E+00	5.463E+03	0.000E+00	0.000E+00	5.601E-01	136

-----SINK FLOW DATA-----

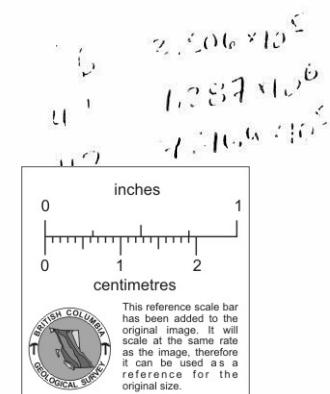
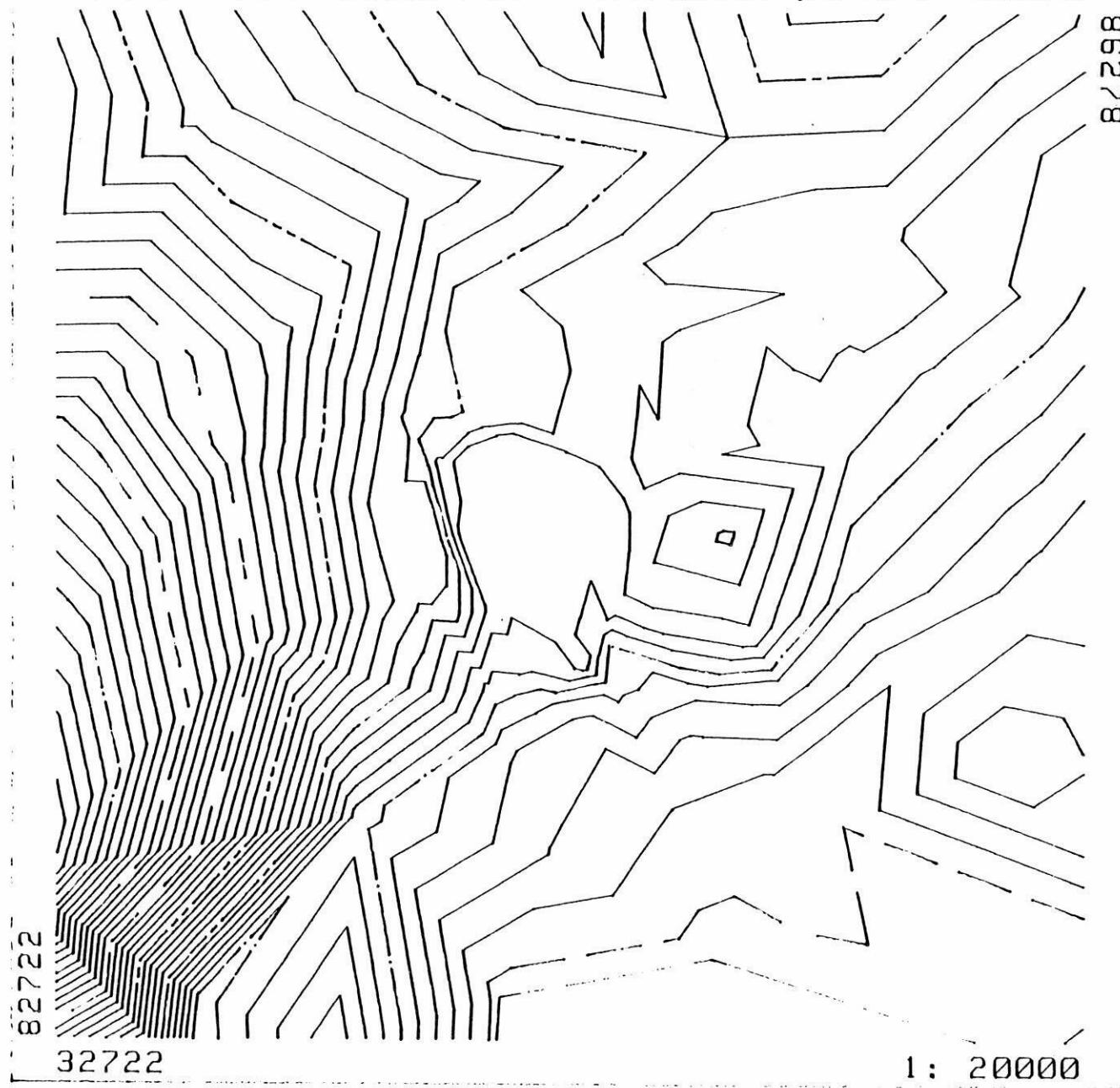
SINK	CONN	TOT_FLOW												
#	#	[L]/[T]												
0	0	0.0000E+00	1	2	4.0063E+07	2	0	0.0000E+00	3	0	0.0000E+00	4	0	0.0000E+00
5	0	0.0000E+00	7	0	0.0000E+00	8	0	0.0000E+00	9	0	0.0000E+00	10	0	0.0000E+00
11	0	0.0000E+00	12	0	0.0000E+00	13	0	0.0000E+00	14	0	0.0000E+00	15	0	0.0000E+00
16	0	0.0000E+00	17	0	0.0000E+00	18	0	0.0000E+00	19	0	0.0000E+00	20	0	0.0000E+00

-----ELEMENT DATA-----

ELEM	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	ELEM		
Node1	96	27	27	96	28	120	94	120	120	118	15	118	118	15	29	16	16	27	17	26	26	98	26	18	18	24	19	20	23	Node1			
Node2	26	121	23	121	121	120	94	95	119	118	14	15	118	23	120	29	28	28	27	26	26	25	98	26	96	25	24	23	23	22	Node2		
Node3	17	96	121	95	121	121	121	94	119	119	14	29	29	28	16	16	27	17	17	18	18	25	97	97	24	19	19	20	21	21	Node3		
Mat1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	3	3	1	1	3	3	3	3	3	Mat1		
Soil	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	Soil		
ELEM	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	ELEM		
Node1	33	23	24	116	116	115	117	116	115	34	114	113	114	112	113	33	112	110	112	111	109	109	109	109	109	109	108	108	108	7	7	6	Node1
Node2	116	24	117	115	1	114	114	2	114	113	2	34	113	3	112	110	3	33	110	3	110	4	5	6	108	108	107	7	108	107	7	Node2	
Node3	12	116	116	22	22	116	115	1	117	115	115	112	114	2	34	113	113	111	112	110	111	7	4	5	6	111	111	6	107	30	30	Node3	
Mat1	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	Mat1		
Soil	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	Soil		
ELEM	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	ELEM		
Node1	8	3	106	106	30	30	107	31	31	103	103	103	103	102	102	101	101	103	31	33	32	107	35	100	100	34	35	35	117	Node1			
Node2	30	106	105	30	31	107	32	32	102	105	104	37	85	102	34	101	102	101	33	32	107	108	100	33	100	35	35	36	34	25	Node2		
Node3	109	3	9	105	105	31	31	102	103	31	105	104	37	85	85	84	32	32	100	111	111	111	34	34	134	33	117	117	117	99	Node3		
Mat1	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	Mat1		
Soil	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	Soil		
ELEM	91	92	93	94	95	96	97	98	99	100	101	102	103	104	105	106	107	108	109	110	111	112	113	114	115	116	117	118	120	ELEM			
Node1	25	99	98	98	62	127	37	127	83	83	83	83	81	60	70	76	76	77	71	71	72	62	63	38	85	85	85	84	84	84	Node1		
Node2	98	98	98	62	127	36	36	134	84	84	62	61	32	32	70	71	71	77	72	62	72	63	63	66	66	67	65	85	63	72	Node2		
Node3	99	77	37	37	37	37	37	37	38	38	101	84	62	61	60	61	61	70	71	71	61	62	82	84	84	83	86	97	63	72	78	Node3	
Mat1	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	4	4	4	4	4	4	4	4	4	4	4	4	4	4	Mat1		
Soil	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	3	4	4	4	4	4	4	4	4	4	4	4	4	4	Soil		
ELEM	121	122	123	124	125	126	127	128	129	130	131	132	133	134	135	136	137	138	139	140	141	142	143	144	145	146	147	148	149	150	ELEM		
Node1	78	78	78	78	79	79	79	79	79	66	65	68	88	40	40	40	40	91	91	41	89	89	89	89	89	66	73	73	55	55	55	Node1	
Node2	72	77	81	80	64	65	66	88	88	104	40	105	9	91	40	41	89	43	53	66	88	41	73	79	80	74	73	67	56	Node2			
Node3	77	81	80	79	78	64	65	63	87	67	104	104	105	9	41	42	42	42	43	55	66	88	73	80	74	67	67	56	43	Node3			
Mat1	4	4	4	4	4	4	4	3	3	3	5	3	3	2	2	2	2	2	2	2	5	5	5	6	4	4	4	4	4	2	Mat1		
Soil	4	4	4	4	4	4	4	3	3	3	3	3	3	2	2	2	2	2	2	3	3	3	3	3	4	4	4	4	4	2	Soil		
ELEM	151	152	153	154	155	156	157	158	159	160	161	162	163	164	165	166	167	168	169	170	171	172	173	174	175	176	177	178	180	ELEM			
Node1	43	43	44	50	56	56	56	68	74	74	74	81	61	75	68	68	68	68	68	70	60	60	135	39	58	58	52	57	51	45	Node1		
Node2	56	50	50	58	57	68	67	67	75	81	80	77	76	75	58	67	67	67	67	70	60	62	38	39	135	136	39	57	52	52	52	Node2	
Node3	50	44	51	51	51	57	68	74	68	75	81	76	75	67	67	57	53	59	59	59	38	59	134	97	39	52	58	51	45	39	Node3		
Mat1	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	Mat1		
Soil	2	3	3	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	1	2	2	2	2	2	2	2	2	3	Soil		
ELEM	181	182	183	184	185	186	187	188	189	190	191	192	193	194	195	196	197	198	199	200	201	202	203	204	205	206	207	206	209	210	ELEM		
Node1	135	39	46	45	54	44	42	49	41	42	42	91	71	32	73	74	94	47	90	48	48	47	47	47	47	46	97	94	Node1				
Node2	98	97	93	39	45	44	51	44	43	40	43	49	42	90	10	11	92	93	90	90	49	49	54	54	53	46	95	96	96	122	Node2		
Node3	97	46	39	53	53	45	45	54	44	38	49	90	90	10	9	10	90	90	47	48	48	54	47	53	46	95	94	93	93	Node3			
Mat1	1	1	1	2	2	2	2	2	2	2	2	2	2	2	2	2	1	1	1	1	1	2	2	1	1	1	1	1	1	1	Mat1		
Soil	1	1	1	3	3	5	5	5	5	5	3	2	2	2	2	2	1	1	1	1	2	5	5	5	5	5	1	1	1	1	Soil		

-----ELEMENT DATA-----

CINOLA - RECLAIMED PIT - K(fault) = 30 M/Y 36278



HEADS  
CURRENT

Malagasy 1-1

-----KEY ANALYSIS PARAMETERS-----

Number of nodes.....136  
Number of elements.....248  
Number of materials.....3  
Number of soils.....7

-----MATERIAL AND SOIL DATA-----

MATERIAL OF SOIL	HYDRAULIC CONDUCTIVITY CL/TJ	SPECIFIC STORAGE CL/CL	SPECIFIC YIELD CL-3	DISTRIBUTED INFLOW CL/TJ
1	3.00E-00	1.00E-06	.0200	7.50E-01
2	3.00E-01	1.00E-06	.0200	7.50E-02
3	3.00E+00	1.00E-06	.0500	7.50E-01
4	3.00E+00	1.00E-06	.3000	7.50E-01
5	3.00E+01	1.00E-06	.0200	7.50E-01
6	3.00E+00	1.00E-06	.3000	7.50E-01
7				7.50E-01

## -----NODE AND FLOW DATA-----

-NODE DATA-		X-COORD	Y-COORD	BASE-EL	MAX-EL	INIT-W/T	NEW-W/T	BOUN	FIXED-INF	INFILT_INF	STORE_INF	STREAM_INF	OUTFLOW	NODE
#	LINK INT	[L]	[L]	[L]	[L]	[L]	[L]	DARY	[L3/T]	[L3/T]	[L3/T]	[L3/T]	[L3/T]	#
1	-1 136	38750.0	39150.0	-280.0	20.0	20.0	20.0	SWMP	0.000E+00	3.481E-05	0.000E+00	2.713E-07	2.753E+07	1
2	1 134	39000.0	37400.0	-280.0	20.0	20.0	20.0	SWMP	0.000E+00	1.015E+06	0.000E+00	2.191E+07	2.299E+07	2
3	2 131	30000.0	36000.0	-275.0	25.0	25.0	25.0	SWMP	0.000E+00	1.220E+06	0.000E+00	1.952E-07	2.075E+07	3
4	3 132	39850.0	34000.0	-275.0	25.0	25.0	25.0	SWMP	0.000E+00	6.766E+05	0.000E+00	1.338E+07	1.661E+07	4
5	4 133	38900.0	31850.0	-270.0	30.0	30.0	30.0	SWMP	0.000E+00	6.703E+05	0.000E+00	1.518E+07	1.538E+07	5
6	5 130	37600.0	32500.0	-265.0	35.0	35.0	35.0	SWMP	0.000E+00	6.159E+05	0.000E+00	1.454E+07	1.519E+07	6
7	6 129	36850.0	32350.0	-265.0	35.0	35.0	35.0	SWMP	0.000E+00	3.713E+05	0.000E+00	1.347E+07	1.337E+07	7
8	7 128	36000.0	32800.0	-260.0	40.0	40.0	40.0	SWMP	0.000E+00	1.420E+05	0.000E+00	1.289E+07	1.314E+07	8
9	8 127	64950.0	33125.0	-255.0	45.0	45.0	45.0	SWMP	0.000E+00	8.513E+04	0.000E+00	6.375E+06	6.475E+06	9
10	9 124	34275.0	33000.0	-255.0	45.0	45.0	45.0	SWMP	0.000E+00	1.257E+05	0.000E+00	4.648E+06	4.706E+06	10
11	10 121	34200.0	31800.0	-250.0	50.0	50.0	50.0	SWMP	0.000E+00	1.223E+05	0.000E+00	4.516E+06	4.648E+06	11
12	11 120	33500.0	32200.0	-150.0	50.0	50.0	50.0	SWMP	0.000E+00	3.222E+05	0.000E+00	4.077E+06	4.518E+06	12
13	12 124	32700.0	31450.0	-245.0	55.0	55.0	55.0	SWMP	0.000E+00	3.044E+05	0.000E+00	2.163E+06	2.664E+06	13
14	13 123	30500.0	30800.0	-240.0	60.0	60.0	60.0	SWMP	0.000E+00	7.155E+05	0.000E+00	0.000E+00	9.150E+05	14
15	29 122	77500.0	31750.0	-370.0	670.0	670.0	670.0	SWMP	0.000E+00	5.619E+05	0.000E+00	0.000E+00	4.779E+05	15
16	27 119	81000.0	34500.0	-193.0	375.0	375.0	375.0	SWMP	0.000E+00	6.400E+05	0.000E+00	0.000E+00	5.600E+05	16
17	16 119	32300.0	36000.0	-193.0	275.0	275.0	275.0	SWMP	0.000E+00	4.347E+05	0.000E+00	0.000E+00	3.162E+05	17
18	24 117	33200.0	37100.0	-150.0	150.0	150.0	150.0	SWMP	0.000E+00	7.552E+05	0.000E+00	3.162E+05	1.085E+06	18
19	23 114	84550.0	38650.0	-180.0	120.0	120.0	120.0	SWMP	0.000E+00	6.224E-05	0.000E+00	0.000E+00	5.240E+05	19
20	-1 115	36200.0	40400.0	-240.0	60.0	60.0	60.0	SWMP	0.000E+00	4.025E+05	0.000E+00	1.212E+07	1.254E+07	20
21	20 116	37000.0	39700.0	-235.0	65.0	65.0	65.0	SWMP	0.000E+00	3.237E+05	0.000E+00	1.176E+07	1.212E+07	21
22	1 113	37900.0	39000.0	-130.0	120.0	120.0	120.0	SWMP	0.000E+00	6.831E-05	0.000E+00	0.000E+00	7.338E+05	22
23	21 112	36000.0	39000.0	-210.0	90.0	90.0	90.0	SWMP	0.000E+00	1.376E+05	0.000E+00	1.036E+07	1.176E+07	23
24	23 111	34400.0	37450.0	-195.0	105.0	105.0	105.0	SWMP	0.000E+00	1.173E+06	0.000E+00	7.150E+06	8.412E+06	24
25	24 110	34600.0	38000.0	-180.0	120.0	120.0	120.0	SWMP	0.000E+00	7.487E+05	0.000E+00	5.215E+06	6.065E+06	25
26	25 109	33325.0	35325.0	-115.0	185.0	185.0	185.0	SWMP	0.000E+00	7.425E+05	0.000E+00	4.358E+06	5.215E+06	26
27	26 108	32200.0	35000.0	-25.0	275.0	275.0	275.0	SWMP	0.000E+00	6.241E+05	0.000E+00	5.233E+06	4.105E+06	27
28	27 107	31700.0	34000.0	65.0	365.0	365.0	365.0	SWMP	0.000E+00	6.200E+05	0.000E+00	1.700E+06	2.452E+06	28
29	28 104	30600.0	32900.0	160.0	460.0	460.0	460.0	SWMP	0.000E+00	5.069E+05	0.000E+00	1.013E+06	1.700E+06	29
30	106 109	85375.0	35550.0	-250.0	50.0	50.0	50.0	SWMP	0.000E+00	2.316E+05	0.000E+00	5.960E+06	6.252E+06	30
31	30 99	85525.0	34000.0	-240.0	60.0	60.0	60.0	SWMP	0.000E+00	1.119E+05	0.000E+00	5.798E+06	5.760E+06	31
32	31 98	36000.0	34300.0	-236.0	54.0	54.0	64.0	SWMP	0.000E+00	1.173E+06	0.000E+00	5.279E+06	5.358E+06	32
33	32 97	36350.0	35000.0	-223.0	77.0	77.0	77.0	SWMP	0.000E+00	3.282E+05	0.000E+00	2.618E+06	2.273E+06	33
34	33 95	36400.0	35900.0	-195.0	105.0	105.0	105.0	SWMP	0.000E+00	4.774E+05	0.000E+00	1.938E+06	2.450E+06	34
35	34 95	36000.0	35700.0	-190.0	110.0	110.0	110.0	SWMP	0.000E+00	1.731E+05	0.000E+00	1.764E+06	1.938E+06	35
36	35 46	35525.0	35450.0	-179.0	121.0	121.0	121.0	SWMP	0.000E+00	2.190E+05	0.000E+00	1.529E+06	1.764E+06	36
37	36 53	34925.0	35400.0	-175.0	125.0	125.0	125.0	SWMP	0.000E+00	1.518E-05	0.000E+00	1.181E+06	1.323E+06	37
38	37 45	34150.0	35225.0	-155.0	145.0	145.0	145.0	SWMP	0.000E+00	9.677E-04	0.000E+00	6.003E-05	1.131E+06	38
39	105 92	30350.0	34875.0	-138.0	162.0	162.0	162.0	SWMP	0.000E+00	5.634E+04	0.000E+00	6.415E+05	7.362E+05	39
40	9 91	34825.0	33600.0	-240.0	60.0	60.0	60.0	SWMP	0.000E+00	4.751E+04	0.000E+00	1.362E+06	1.415E+06	40
41	40 90	34550.0	33850.0	-227.0	73.0	73.0	73.0	SWMP	0.000E+00	1.405E+04	0.000E+00	9.219E+05	1.055E+06	41
42	41 89	34300.0	33775.0	-219.0	91.0	91.0	91.0	SWMP	0.000E+00	5.625E+03	0.000E+00	7.647E+05	7.789E+05	42
43	42 86	34250.0	33975.0	-195.0	105.0	105.0	105.0	SWMP	0.000E+00	1.253E+04	0.000E+00	3.798E+05	3.957E+05	43
44	43 103	34000.0	34275.0	-136.0	164.0	164.0	164.0	SWMP	0.000E+00	2.857E+04	0.000E+00	2.567E+05	2.803E+05	44
45	39 25	33925.0	34600.0	-138.0	162.0	162.0	162.0	SWMP	0.000E+00	2.250E+04	0.000E+00	4.682E+05	4.745E+05	45
46	53 37	33425.0	34725.0	-55.0	245.0	245.0	245.0	SWMP	0.000E+00	1.630E+05	0.000E+00	1.841E+05	3.375E+05	46
47	54 105	33525.0	34150.0	-55.0	245.0	245.0	245.0	SWMP	0.000E+00	2.555E+05	0.000E+00	0.000E+00	1.799E+05	47
48	49 34	33600.0	34025.0	-122.0	173.0	173.0	173.0	SWMP	0.000E+00	3.238E+04	0.000E+00	0.000E+00	7.114E+04	48
49	43 102	34050.0	33975.0	-160.0	140.0	140.0	140.0	SWMP	0.000E+00	2.355E+04	0.000E+00	7.114E+04	7.151E+04	49
50	43 83	34125.0	34225.0	-141.0	159.0	159.0	159.0	SWMP	0.000E+00	7.070E-03	0.000E+00	0.000E+00	-4.237E-04	50

-----NODE AND FLOW DATA-----

-NODE DATA-		X-COORD	Y-COORD	BASE-EL	MAX-EL	INIT-W/T	NEW-W/T	DOWN	FIXED-INF	INFILT_INF	STORE_INF	STREAM_INF	OUTFLOW	NODE
---	---	[L]	[L]	[L]	[L]	[L]	[L]	DARY	[L3/T]	[L3/T]	[L3/T]	[L3/T]	[L3/T]	---
51	44	126	84075.0	34450.0	-115.0	185.0	185.0	168.3 SWRD	0.000E+00	1.251E-04	0.000E+00	0.000E+00	-5.062E-04	51
52	39	82	84025.0	34700.0	-115.0	185.0	185.0	163.3 SWRD	0.000E+00	7.375E-03	0.000E+00	0.000E+00	-8.770E-03	52
53	45	123	83850.0	34575.0	-130.0	170.0	170.0	170.0 SWMP	0.000E+00	5.664E-04	0.000E+00	5.333E+05	4.682E+05	53
54	44	125	83875.0	34250.0	-124.0	176.0	176.0	176.0 SWMP	0.000E+00	4.422E-04	0.000E+00	1.799E+05	2.567E+05	54
55	58	101	84375.0	34050.0	-171.0	127.0	125.3	101.3 SWRD	0.000E+00	9.371E-03	0.000E+00	0.000E+00	-2.314E-01	55
56	57	73	84250.0	34225.0	-120.0	160.0	172.0	124.3 SWRD	0.000E+00	8.867E-03	0.000E+00	0.000E+00	-6.632E-03	56
57	53	65	84150.0	34475.0	-96.0	104.0	198.3	129.5 SWRD	0.000E+00	5.109E-03	0.000E+00	0.000E+00	-6.379E-03	57
58	59	60	84075.0	34700.0	-74.0	205.0	199.1	146.3 SWRD	0.000E+00	9.772E-03	0.000E+00	0.000E+00	-1.378E-01	58
59	76	64	84175.0	34850.0	-58.0	202.0	187.3	150.3 SWRD	0.000E+00	2.353E-04	0.000E+00	0.000E+00	-6.649E-01	59
60	70	79	84350.0	34850.0	-117.0	183.0	183.0	143.7 SWRD	0.000E+00	4.378E-04	0.000E+00	0.000E+00	-5.227E-02	60
61	71	62	84600.0	34725.0	-146.0	154.0	154.0	135.1 SWRD	0.000E+00	5.353E-04	0.000E+00	0.000E+00	-1.643E-02	61
62	72	72	84700.0	34575.0	-125.0	165.0	164.7	133.0 SWRD	0.000E+00	2.706E-04	0.000E+00	0.000E+00	7.638E-03	62
63	64	78	84725.0	34375.0	-130.0	170.0	162.0	178.0 SWRD	0.000E+00	5.154E-04	0.000E+00	0.000E+00	3.465E-02	63
64	79	61	84650.0	34250.0	-170.0	130.0	130.0	126.7 SWRD	0.000E+00	1.188E-04	0.000E+00	3.465E-02	-1.606E-01	64
65	66	71	84625.0	34125.0	-200.0	100.0	100.0	100.0 SWMP	0.000E+00	1.467E-04	0.000E+00	0.000E+00	7.007E+04	65
66	66	77	84650.0	34050.0	-195.0	122.0	105.0	118.7 SWRD	0.000E+00	9.766E-03	0.000E+00	4.371E+05	-2.214E+00	66
67	73	60	84300.0	34250.0	-110.0	122.0	171.3	122.0 SWMP	0.000E+00	1.172E-04	0.000E+00	-5.322E-03	1.748E+04	67
68	74	70	84225.0	34475.0	-83.0	122.0	198.2	122.0 SWMP	0.000E+00	1.453E-04	0.000E+00	-5.379E-03	3.342E+04	68
69	73	59	84175.0	34725.0	-85.0	122.0	200.0	122.0 SWMP	0.000E+00	1.102E-04	0.000E+00	-1.378E-01	6.799E+04	69
70	75	58	84300.0	34775.0	-96.0	122.0	198.3	122.0 SWMP	0.000E+00	1.357E-04	0.000E+00	-5.227E-02	7.038E+04	70
71	77	67	84375.0	34650.0	-130.0	122.0	170.0	122.0 SWMP	0.000E+00	1.411E-04	0.000E+00	-1.643E-02	5.205E+04	71
72	73	73	84650.0	34475.0	-125.0	122.0	173.4	122.0 SWMP	0.000E+00	1.371E-04	0.000E+00	3.656E-03	4.366E+04	72
73	66	81	84475.0	34150.0	-145.0	122.0	136.3	122.0 SWMP	0.000E+00	1.312E-04	0.000E+00	1.748E+04	9.539E-03	73
74	30	57	84350.0	34350.0	-90.0	122.0	182.5	122.0 SWMP	0.000E+00	1.445E-04	0.000E+00	1.342E+04	4.738E+04	74
75	81	63	84250.0	34550.0	-85.0	122.0	200.3	122.0 SWMP	0.000E+00	1.063E+04	0.000E+00	0.000E+00	1.063E+04	75
76	51	74	84275.0	34700.0	-38.0	122.0	205.7	122.0 SWMP	0.000E+00	1.538E+04	0.000E+00	1.403E+05	1.562E+05	76
77	31	30	84490.0	34600.0	-115.0	122.0	185.0	122.0 SWMP	0.000E+00	1.547E+04	0.000E+00	5.205E-04	6.752E+04	77
78	30	56	84550.0	34400.0	-135.0	122.0	165.0	122.0 SWMP	0.000E+00	1.719E+04	0.000E+00	4.366E+04	7.081E+04	78
79	66	67	84600.0	34175.0	-175.0	122.0	123.2	115.7 SWRD	0.000E+00	8.515E-03	0.000E+00	-1.606E-01	-2.190E-02	79
80	66	73	84500.0	34225.0	-140.0	122.0	150.0	122.0 SWMP	0.000E+00	1.227E+04	0.000E+00	3.735E+05	3.795E+05	80
81	80	55	84400.0	34475.0	-105.0	122.0	195.0	122.0 SWMP	0.000E+00	2.041E+04	0.000E+00	1.344E+05	2.548E+05	81
82	123	56	84600.0	35120.0	-162.0	133.0	133.0	138.0 SWMP	0.000E+00	8.674E+04	0.000E+00	0.000E+00	6.380E+04	82
83	123	38	84800.0	34730.0	-176.0	124.0	124.0	124.0 SWMP	0.000E+00	4.304E+04	0.000E+00	0.000E+00	1.097E+05	83
84	102	52	85000.0	34475.0	-148.0	152.0	152.0	152.0 SWMP	0.000E+00	8.331E+04	0.000E+00	0.000E+00	1.547E+04	84
85	37	39	84775.0	34200.0	-170.0	130.0	130.0	127.4 SWRD	0.000E+00	2.512E+04	0.000E+00	0.000E+00	-4.576E-02	85
86	103	133	85075.0	34150.0	-130.0	170.0	127.7	127.1 SWRD	0.000E+00	5.531E+04	0.000E+00	0.000E+00	2.342E-02	86
87	105	33	84900.0	33750.0	-220.0	80.0	80.0	80.0 SWRD	0.0005-00	3.484E-04	0.000E+00	-4.374E-02	5.767E-04	87
88	41	37	84625.0	34000.0	-205.0	95.0	92.7	91.9 SWRD	0.0005-00	1.078E-04	0.000E+00	-2.214E-00	-1.377E+00	88
89	41	36	84425.0	33950.0	-207.0	97.0	97.0	97.0 SWMP	0.0005-00	8.242E-03	0.000E+00	0.000E+00	1.460E-05	89
90	42	73	83825.0	33575.0	-196.0	104.0	104.0	104.0 SWMP	0.0005-00	2.707E-05	0.000E+00	0.000E+00	3.590E-05	90
91	3	34	84450.0	33450.0	-231.0	69.0	69.0	67.0 SWMP	0.0005-00	1.497E-04	0.000E+00	0.000E+00	1.317E-04	91
92	10	33	83750.0	33820.0	-150.0	150.0	137.1	133.2 SWRD	0.000E+00	2.614E-05	0.000E+00	0.000E+00	0.000E+00	92
93	122	52	83325.0	33000.0	-205.0	95.0	95.0	95.0 SWMP	0.000E+00	1.513E+05	0.000E+00	4.960E+05	9.324E-05	93
94	93	31	82700.0	33375.0	134.0	434.0	434.0	434.0 SWMP	0.000E+00	6.724E+05	0.000E+00	2.577E+05	4.760E+05	94
95	46	30	83000.0	34275.0	40.0	340.0	340.0	340.0 SWMP	0.000E+00	2.677E-05	0.000E+00	0.000E+00	1.311E-05	95
96	26	104	83000.0	33000.0	-23.0	277.0	277.0	277.0 SWMP	0.000E+00	3.402E-05	0.000E+00	0.000E+00	2.523E-05	96
97	79	51	83375.0	33100.0	-76.0	224.0	224.0	224.0 SWMP	0.000E+00	1.977E-05	0.000E+00	0.000E+00	1.470E-05	97
98	58	50	84000.0	33575.0	-122.0	172.0	172.0	172.0 SWMP	0.000E+00	2.833E-05	0.000E+00	0.000E+00	7.960E-04	98
99	56	48	85000.0	33750.0	-160.0	140.0	140.0	140.0 SWMP	0.000E+00	2.513E-05	0.000E+00	0.000E+00	1.366E-05	99
100	33	42	86000.0	33250.0	-193.0	107.0	107.0	107.0 SWMP	0.000E+00	1.382E-05	0.000E+00	0.000E+00	1.374E-05	100

-----NODE AND FLOW DATA-----

-NODE DATA-		X-COORD	Y-COORD	BASE-EL	MAX-EL	INIT-W/T	NEW-W/T	BOUN	FIXED-INF	INFILT_INF	STORE_INF	STREAM_INF	OUTFLOW	NODE	
#	LNK	INT	[L]	[L]	[L]	[L]	[L]	DARY	[L]/[T]	[L]/[T]	[L]/[T]	[L]/[T]	[L]/[T]	#	
101	32	47	85390.0	34760.0	-189.0	111.0	111.0	111.0	SWMP	0.000E+00	1.314E+05	0.000E+00	4.094E+05	5.449E+05	101
102	31	54	85400.0	34300.0	-209.0	91.0	91.0	91.0	SWMP	0.000E+00	1.155E+05	0.000E+00	1.547E+04	1.405E+05	102
103	105	44	85175.0	34000.0	-214.0	86.0	86.0	86.0	SWMP	0.000E+00	5.563E-04	0.000E+00	2.842E-02	6.511E+04	103
104	40	43	84875.0	33800.0	-233.0	67.0	67.0	67.0	SWMP	0.000E+00	3.594E+04	0.000E+00	0.000E+00	1.078E+05	104
105	106	42	85150.0	33700.0	-241.0	59.0	59.0	59.0	SWMP	0.000E+00	1.021E+05	0.000E+00	1.222E+05	2.350E+05	105
106	8	41	85330.0	33250.0	-248.0	52.0	52.0	52.0	SWMP	0.000E+00	5.297E+04	0.000E+00	5.487E-06	5.560E+05	106
107	7	40	85325.0	33750.0	-212.0	68.0	68.0	68.0	SWMP	0.000E+00	4.253E+05	0.000E+00	0.000E+00	1.225E+05	107
108	8	22	87000.0	33700.0	-240.0	60.0	60.0	60.0	SWMP	0.000E+00	6.873E-05	0.000E+00	0.000E+00	5.675E+05	108
109	3	19	88200.0	33700.0	-225.0	75.0	75.0	75.0	SWMP	0.000E+00	1.704E+04	0.000E+00	0.000E+00	1.813E+06	109
110	3	17	88250.0	33000.0	-245.0	55.0	55.0	55.0	SWMP	0.000E+00	9.369E+05	0.000E+00	0.000E+00	1.097E+05	110
111	32	18	87000.0	34450.0	-250.0	50.0	50.0	50.0	SWMP	0.000E+00	8.706E+05	0.000E+00	6.888E+05	1.624E+05	111
112	111	19	87000.0	33600.0	-195.0	105.0	105.0	105.0	SWMP	0.000E+00	5.777E+05	0.000E+00	0.000E+00	5.388E+05	112
113	2	15	67950.0	33550.0	-150.0	150.0	150.0	150.0	SWMP	0.000E+00	1.422E+06	0.000E+00	0.000E+00	1.155E+06	113
114	115	27	37000.0	37000.0	-210.0	90.0	90.0	90.0	SWMP	0.000E+00	1.097E+06	0.000E+00	7.695E+05	1.295E+06	114
115	1	28	87800.0	38000.0	-240.0	50.0	50.0	50.0	SWMP	0.000E+00	1.437E+06	0.000E+00	1.395E-05	3.398E+05	115
116	27	27	65700.0	37500.0	-170.0	130.0	130.0	130.0	SWMP	1.000E-00	1.359E+06	0.000E+00	0.000E+00	1.362E+06	116
117	114	26	85450.0	36550.0	-115.0	125.0	125.0	125.0	SWMP	0.000E+00	9.173E+05	0.000E+00	0.000E+00	7.698E+05	117
118	27	25	30900.0	32600.0	255.0	565.0	565.0	565.0	SWMP	0.000E+00	9.844E+05	0.000E+00	0.000E+00	5.333E+05	118
119	13	24	82000.0	32100.0	-150.0	150.0	150.0	150.0	SWMP	0.000E+00	1.692E+06	0.000E+00	0.000E+00	1.124E+06	119
120	74	23	61900.0	33200.0	225.0	525.0	525.0	525.0	SWMP	0.000E+00	5.523E+05	0.000E+00	0.000E+00	2.597E+05	120
121	27	21	82350.0	34200.0	105.0	405.0	405.0	405.0	SWMP	0.000E+00	4.381E+05	0.000E+00	0.000E+00	2.739E+05	121
122	12	20	83300.0	32700.0	-210.0	90.0	90.0	90.0	SWMP	0.000E+00	5.322E+05	0.000E+00	9.824E+05	1.412E+06	122
123	125	14	84680.0	35080.0	-167.0	133.0	133.0	133.0	SWMP	0.000E+00	2.731E+04	0.000E+00	6.380E+04	1.007E+05	123
124	125	13	85090.0	35160.0	-178.0	122.0	122.0	122.0	SWMP	0.000E+00	4.701E+04	0.000E+00	0.000E+00	7.385E+04	124
125	101	12	85230.0	34870.0	-186.0	114.0	114.0	114.0	SWMP	0.000E+00	3.610E+04	0.000E+00	1.746E+05	2.253E+05	125
126	101	11	84810.0	34780.0	-171.0	129.0	129.0	129.0	SWMP	0.000E+00	4.539E+04	0.000E+00	1.077E+05	1.157E+05	126
127	33	10	85190.0	35260.0	-170.0	130.0	130.0	130.0	SWMP	0.000E+00	5.231E+04	0.000E+00	0.000E+00	1.667E+04	127
128	101	9	85350.0	34840.0	-165.0	115.0	115.0	115.0	SWMP	0.000E+00	2.763E+04	0.000E+00	4.341E+04	6.341E+04	128
129	123	3	85420.0	35020.0	-162.0	118.0	118.0	118.0	SWMP	0.000E+00	2.025E+04	0.000E+00	0.000E+00	1.973E+04	129
130	128	7	85350.0	35200.0	-177.0	123.0	123.0	123.0	SWMP	0.000E+00	1.620E+04	0.000E+00	0.000E+00	2.368E+04	130
131	132	6	85500.0	35230.0	-174.0	126.0	126.0	126.0	SWMP	0.000E+00	1.170E+04	0.000E+00	1.395E+04	2.316E+04	131
132	133	5	85530.0	35060.0	-185.0	115.0	115.0	115.0	SWMP	0.000E+00	1.140E+04	0.000E+00	2.318E+04	3.222E+04	132
133	72	4	35740.0	34990.0	-195.0	105.0	105.0	105.0	SWMP	0.000E+00	1.023E+05	0.000E+00	5.222E+04	1.379E+05	133
134	131	3	85540.0	35280.0	-173.0	127.0	127.0	127.0	SWMP	0.000E+00	4.088E+04	0.000E+00	0.000E+00	1.365E+04	134
135	33	2	84050.0	35050.0	-145.0	155.0	155.0	155.0	SWMP	0.000E+00	5.766E+04	0.000E+00	7.362E+05	5.207E+05	135
136	39	1	84060.0	34865.0	-115.0	185.0	185.0	185.0	SWMP	0.000E+00	5.467E+03	0.000E+00	0.000E+00	-1.220E+00	136

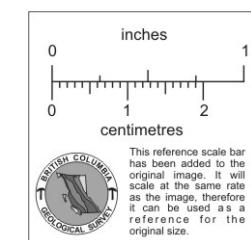
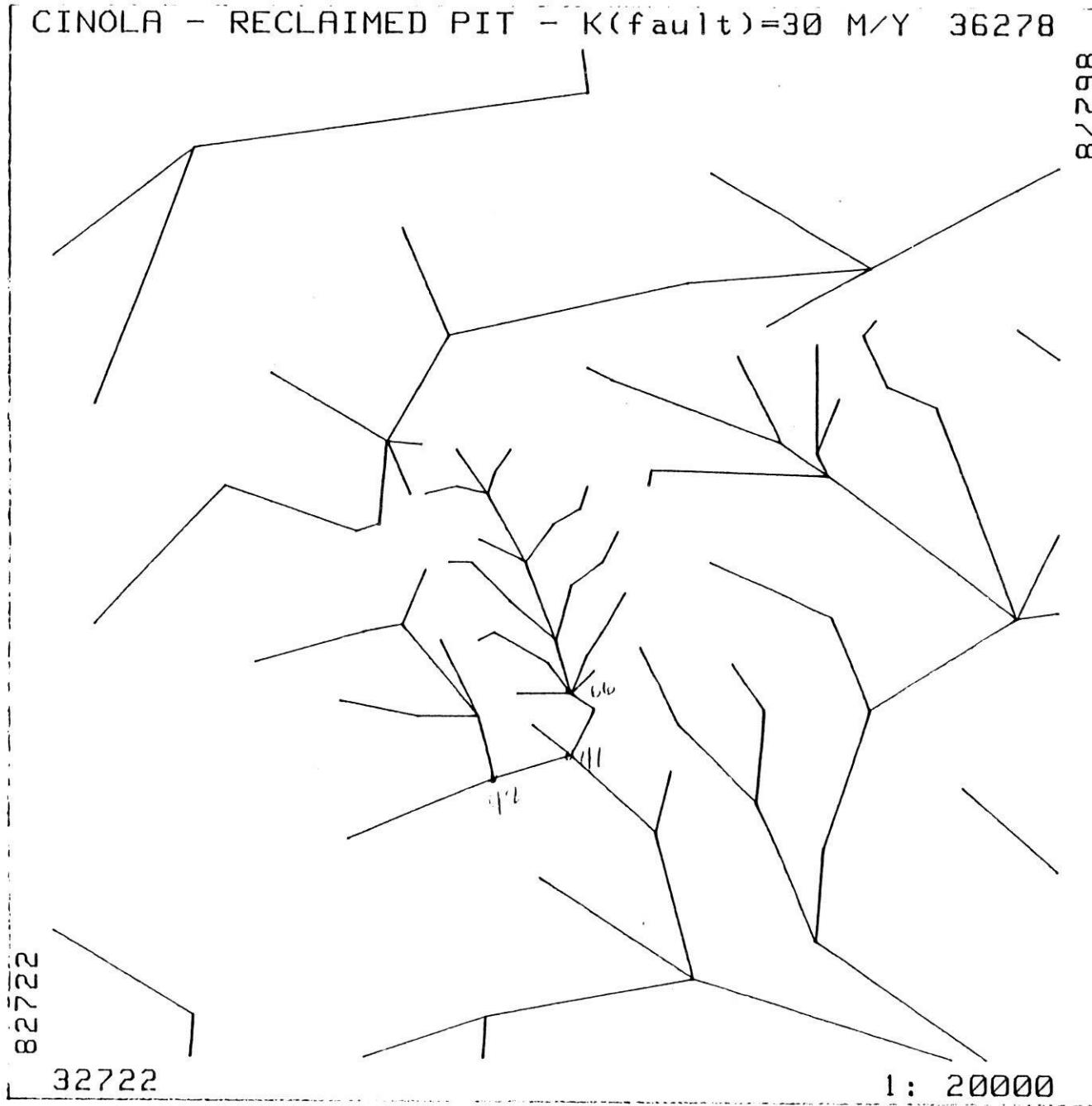
-----SINK FLOW DATA-----

SINK	CONN	TOT_FLOW												
#	#	[L]/[T]												
0	0	0.0000E+00												
1	2	4.0065E-07	2	0	0.0000E+00	3	0	0.0000E+00	4	0	0.0000E+00	5	0	0.0000E+00
6	0	0.0000E+00	7	0	0.0000E+00	8	0	0.0000E+00	9	0	0.0000E+00	10	0	0.0000E+00
11	0	0.0000E+00	12	0	0.0000E+00	13	0	0.0000E+00	14	0	0.0000E+00	15	0	0.0000E+00
16	0	0.0000E+00	17	0	0.0000E+00	18	0	0.0000E+00	19	0	0.0000E+00	20	0	0.0000E+00

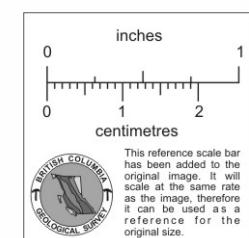
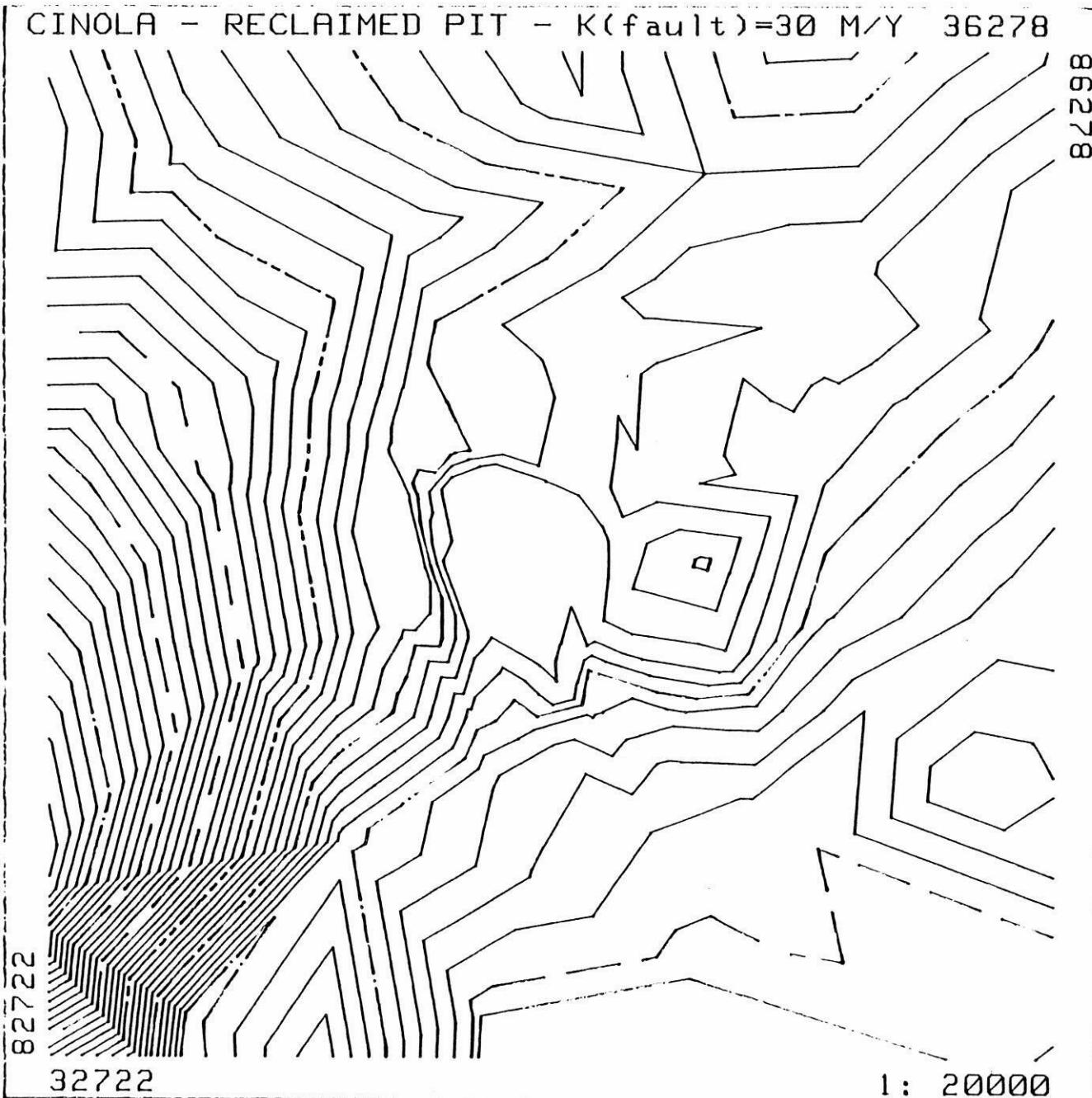
-----ELEMENT DATA-----

-----ELEMENT DATA-----

CINOLA - RECLAIMED PIT - K(fault)=30 M/Y 36278



STREAMS  
LOCATIONS



HEADS  
CURRENT

Materials 1-6

**APPENDIX 3.2.8-1**

**SUMMARY OF KINETIC TEST DATA USED IN THE  
EVALUATION OF CRITICAL NNP VALUE FOR ACID GENERATION,  
CINOLA GOLD PROJECT**

**(Pages 1 to 6)**

## APPENDIX 3.2.8-1

TABLE 1

Reprinted From Stage II Report, Volume V

TABLE 3.3.3-1

## Results of Acid-base Accounting From Norecol Humidity Cell Experiments (Series I and II), Cinola Gold Project

HUMIDITY CELL	SAMPLE	SERIES	PASTE pH	t CaCO <sub>3</sub> /1000 t					NET NEUTRALIZATION POTENTIAL	KINETIC TESTS <sup>a</sup> pH<5
				TOTAL SULPHUR (%S)	SULPHIDE (%S)	LEACHABLE SULPHATE (%S)	MAXIMUM ACIDITY	NEUTRALIZATION POTENTIAL		
1	Weathered Skonun Sediments (Conglomerate)	I <sup>b</sup>	4.6	-	0.38	-	11.9	-3.3	-15.2	Yes
		II <sup>b</sup>	4.3	0.58	0.22	0.26	18.2	-0.33	-18.5	Yes
2	Skonun Sediments (Conglomerate)	I	4.8	-	1.43	-	44.7	+1.3	-43.4	Yes
		II	3.7	1.45	1.13	0.21	45.3	-3.97	-48.8	Yes
3	Argillically Altered Skonun Sediments	II <sup>c</sup>	2.6	2.59	1.52	0.84	80.9	-20.8	-101.7	Yes
4	Skonun Sediments (Single-phase breccia)	I	5.4	-	1.85	-	57.8	-0.1	-57.9	Yes
		II	3.7	1.66	1.43	0.12	51.9	-1.06	-53.0	Yes

<sup>a</sup> Based on humidity cell data reported in Volume V Appendix 3.3.3 - 1A and Appendix 3.3.3-2A of the Stage II Report.<sup>b</sup> Analysis for Series I and II were performed by different laboratories for comparison.<sup>c</sup> Argillically altered Skonun sediments were only tested in Series II. Maximum potential acidity was calculated from sulphide for Series I and from total sulphur for Series II.

## APPENDIX 3.2.8-1

TABLE 2

Reprinted from Stage II Report, Volume V

TABLE 3.4.3-2

Summary of Norecol Acid-base Accounting Study Results for Waste Rock Pads,  
Cinola Gold Project

PARAMETER	UNITS	BOTTOM SAND <sup>a</sup>	PAD 1	PAD 2	PAD 3	PAD 4
Quantity of waste rock	t	-	20	30	30	30
Total S	%	0.003	1.95	2.96	3.06	1.75
Total S	kg	-	390	888	918	525
Total SO <sub>4</sub> <sup>b</sup>	kg	-	1170	2660	2750	1580
Neutralization potential	t CaCO <sub>3</sub> /1000 t	3.59	2.16	3.05	-6.37	0.69
Paste pH	-	7.8	5.3	7.2	3.5	7.1
Net neutralization potential	t CaCO <sub>3</sub> /1000 t	+3.50	-58.7	-89.5	-102	-54.0
Kinetic Tests: pH<5 <sup>c</sup>			Yes 4 months	Yes 2 months	Yes immediate	Yes 1 month
Time period of onset						

<sup>a</sup> Sand used at the bottom of each waste rock pad.<sup>b</sup> Total sulphate is calculated by assuming the total sulphur content could be completely oxidized to sulphate.<sup>c</sup> Based on humidity cell data reported in Appendix 3.4.3-1 of Volume V of the Stage II Report.

## APPENDIX 3.2.8-1

TABLE 3

Reprinted from Table Stage II Report, Volume V

TABLE 3.5.2-1

Description of Waste Rock Samples Used In Norecol Column Experiments,  
Cinola Gold Project

WASTE ROCK GROUP	SECTION No. <sup>a</sup>	HOLE No. <sup>b</sup>	SAMPLE No.	LITHOLOGIC UNIT <sup>c</sup>	ABA SAMPLING NET NP <sup>d</sup>	KINETIC TESTS pH <5
Skonun	11+82	86-R-30	43515	2d	-41	Yes <sup>e</sup>
Sediments (Composite)	14+89 15+25	86-R-43 87-R-12	43286 45580	2c 2c	-102 -44	Yes <sup>e</sup> Yes <sup>e</sup>
Single and Multiphase Breccia (Composite)	13+20 15+55 12+12	86-R-38 86-R-25 86-R-27	44438 42642 42478	4c 4c 4b	-52 -59 -28	Yes <sup>f</sup> Yes <sup>f</sup> Yes <sup>f</sup>

<sup>a</sup> Section locations on Figure 3.2.3-1.<sup>b</sup> Drill hole locations are shown on Table 3.2.4-1, Volume V.<sup>c</sup> Lithological units are described in Section 3.2.3, Volume V.<sup>d</sup> Based on ABA data reported in Volume V Appendix 3.2.3-1 of the Stage II Report.<sup>e</sup> pH remained constant at low levels (2.2-3.8) or dropped to ~3.5 in upper part of column for unflushed, constant trickle and wet/dry cycle conditions.

pH generally remained &gt;6 in lower part of columns and other conditions (flushed, unsaturated with water table)

<sup>f</sup> pH constant in range 2.5 to 3.5 for all column experimental conditions.

Refer to Table 3.5.3-1 of Volume V for details

## APPENDIX 3.2.8-1

TABLE 4

Reprinted from Table Stage II Report, Volume V

TABLE 3.6.3-1

## Results of Norecol Acid-base Accounting Study of Argillically Altered Rock from the Cinola Gold Project (Series IV)

SAMPLE	TOTAL SULPHUR (%S)	SULPHIDE <sup>a</sup> (%S)	LEACHABLE SULPHATE (as %S)	PASTE pH	MAXIMUM ACID POTENTIAL <sup>b,c</sup>	NEUTRALIZATION POTENTIAL <sup>c,d</sup>	NET NEUTRALIZATION POTENTIAL <sup>d</sup>	KINETIC TESTS pH<5
<b>Before Wash Tests</b>								
R-1	4.30	4.08	0.22	2.93	127.5	-3.1	-130.6	Yes
R-1	4.42	4.30	0.12	3.58	134.4	0.8	-133.6	Yes
R-3	5.64	5.51	0.13	3.95	172.2	3.3	-168.9	Yes
R-4	4.71	4.59	0.12	3.96	143.4	3.6	-139.8	Yes
<b>After Wash Tests</b>								
R-1	3.03	2.97	0.06	2.99	92.8	-0.1	-92.9	Yes
R-2	3.91	3.87	0.05	3.54	120.6	1.6	-119.0	Yes
R-3	5.64	5.58	0.06	3.77	174.4	3.3	-171.1	Yes
R-4	5.51	5.44	0.77	3.76	170.0	2.6	-167.4	Yes

<sup>a</sup> Sulphide is calculated by subtracting leachable sulphate from total sulphur.<sup>b</sup> Maximum acid potential is calculated from sulphide.<sup>c</sup> Potentials expressed in tonnes of calcium carbonate equivalent per 1000 t of sample<sup>d</sup> A negative net neutralization potential indicates that the sample has a potential to produce acid mine drainage.<sup>e</sup> Based on humidity cell data reported in Volume V, Appendix 3.3.4-2 of the Stage II Report.

## APPENDIX 3.2.8-1

TABLE 5

REPRINTED FROM STAGE II REPORT, VOLUME V APPENDICES

## APPENDIX 3.3.4-3

TABLE 1

ACID-BASE ACCOUNTING RESULTS FROM WASTE ROCK USED IN NORECOL HUMIDITY CELL EXPERIMENTS (SERIES III), CINOLA GOLD PROJECT

WASTE ROCK GROUP	HUMIDITY CELL No.	PASTE PH	TOTAL SULPHUR (%)	MAXIMUM POTENTIAL ACIDITY	NEUTRALIZATION POTENTIAL	NET NEUTRALIZATION POTENTIAL	HUMIDITY CELL pH<5 <sup>a</sup>
<b>HAIDA MUDSTONES</b>							
	6	8.2	1.30	40.6	29.7	-10.9	No
	17	8.2	1.38	43.1	151	+108	No
	19	8.4	0.87	27.3	49.4	+22.1	No
	20	7.7	1.15	35.9	7.12	-28.8	Yes
	22	8.1	1.21	37.8	86.4	+48.6	No
	31	7.6	1.71	53.4	35.1	-18.3	No
<b>SKONUN SEDIMENTS</b>							
Sandstone	4	5.4	3.01	94.1	1.32	-92.8	Yes
	7	4.9	1.98	61.9	2.47	-59.4	Yes
	16	4.6	3.12	97.2	0.30	-97.2	Yes
	21	4.1	2.46	73.8	-0.45	-74.3	Yes
	23	5.1	3.84	120	-1.89	-122	Yes
	32	4.1	3.08	96.3	3.04	-93.3	Yes
Matrix Conglomerate	1	6.3	0.96	29.9	1.00	-28.9	Yes
	5	4.7	0.84	26.2	0.50	-25.7	Yes
	8	4.7	2.34	73.1	1.25	-71.9	Yes
	10	4.8	2.16	67.5	0.95	-66.6	Yes
	12	4.9	1.90	59.4	0.37	-58.8	Yes
	27	5.7	2.35	73.4	1.30	-72.1	Yes

continued . . .

## APPENDIX 3.2.8-1

TABLE 5 (continued)

REPRINTED FROM STAGE II REPORT, VOLUME V APPENDICES

## APPENDIX 3.3.4-3

TABLE 1 (concluded)

## ACID-BASE ACCOUNTING RESULTS FROM WASTE ROCK USED IN NORECOL HUMIDITY CELL EXPERIMENTS (SERIES III), CINOLA GOLD PROJECT

WASTE ROCK GROUP	HUMIDITY CELL No.	PASTE pH	TOTAL SULPHUR (%)	MAXIMUM POTENTIAL ACIDITY	NEUTRALIZATION POTENTIAL	NET NEUTRALIZATION POTENTIAL	(t CaCO <sub>3</sub> /1000 t)	
							HUMIDITY CELL pH < 5 <sup>a</sup>	
Clast conglomerate and Single Phase Breccia	11	7.7	2.53	79.1	6.23	-72.9	Yes	
	14	7.7	2.61	81.6	13.4	-68.2	No	
	15	6.4	2.20	68.8	1.74	-67.1	Yes	
	18	5.0	1.47	45.9	0.95	-45.0	Yes	
	28	6.5	2.55	79.7	2.54	-77.2	Yes	
	29	7.6	2.23	69.7	9.33	-60.4	No	
	30	5.0	1.63	50.9	0.25	-50.7	Yes	
RHYOLITE	33	5.0	3.22	101	2.39	-98.6	Yes	
MULTIPHASE BRECCIA								
	9	4.4	1.51	47.2	0.22	-47.0	Yes	
	26	4.3	2.14	66.9	0.01	-66.9	Yes	
	34	6.9	3.00	31.3	1.51	-29.8	Yes	
ARGILLICALLY ALTERED SKONUN SEDIMENTS								
	2	4.9	4.10	128	1.32	-127	Yes	
	3	3.8	6.08	190	0.01	-190	Yes	
	13	6.5	4.00	125	3.99	-121	Yes	
	24	6.6	4.05	127	6.58	-120	Yes	
	25	7.2	4.83	151	7.15	-144	Yes	

<sup>a</sup> Based on humidity cell data reported in Volume V Appendix 3.3.4-1B of the Stage II Report. All cells ran for 20 weeks, except cells 11, 20, 22 which have been running for 2 years.

**APPENDIX 4.2.2-1**  
**HIGH WEST MONTHLY WATER BALANCE FOR**  
**AVERAGE ANNUAL PRECIPITATION**  
**(Pages 1 to 50)**

CINOLA GOLD PROJECT

HIGH WEST AREA

MONTHLY WATER BALANCE FOR AVERAGE ANNUAL PRECIPITATION: PREPRODUCTION

PREPRODUCTION (page 1 of 1)

FILE: WBREP

DATE: 29-Jun-89

W S RESERVOIR CATCHMENT = 162 ha  
 CATCHMENT FOR DITCH IE7 = 75 ha  
 RUNOFF FACTOR = 0.6

## WATER SUPPLY RESERVOIR

MONTH	PRECIP	POTENT	EVAPOT	POND	DIRECT	RUNOFF	POND	SEEPAGE	SEEP TO	FLOW TO	EXC/	WATER	WATER	RUNOFF IN	REDUCTION
				AREA	PRECIP	EVAP	IN	IMP #1	FLOR CK	DEF	IN RES	ELEV	DITCH IE7	IN FLOW	
	mm	mm		ha			1000 m <sup>3</sup> /d			M m <sup>3</sup>		m	1000 m <sup>3</sup> /d		
1	2	3		4	5	6	7	8	9	10	11	12	13	14	15
JUL	80	104		0.03	0.00	3.34	0.00	0.000	0.000	2.64	0.70	0.022	285	1.55	4.1
AUG	78	99		0.59	0.01	3.25	0.02	0.000	0.000	2.58	0.67	0.042	290	1.51	4.1
SEP	166	71		1.43	0.08	7.11	0.03	0.000	0.001	5.67	1.49	0.087	291	3.32	4.1
OCT	297	44		2.06	0.20	12.23	0.03	0.000	0.001	4.91	7.52	0.320	297	5.75	12.1
NOV	260	21		5.33	0.51	10.31	0.04	0.000	0.002	4.44	5.85	0.516	300	5.22	12.1
DEC	280	12		7.83	0.66	10.34	0.03	0.000	0.000	4.29	6.57	0.720	302	5.08	12.1
MEAN	190	58		2.95	0.24	7.84	0.03	0.000	0.001	4.08	0.98	0.088	294	3.72	8.1
TOTAL	1141	350										7.50E+05	M <sup>3</sup>	6.85E+05	M <sup>3</sup>

## NOTES RE COLUMNS:

- 1 From Stage II Report, Vol III
- 3 From Stage II Report, Vol III
- 4 From curve of area vs. elevation
- 5 From columns 2 and 4
- 6 From columns 2, 4, catchment, and runoff factor
- 7 From columns 3 and 4
- 9 Set equal to zero
- 9 From seepage calculations
- 10 Controlled flow
- 11 Net result of columns 5 to 10.
- 12 Water volume in storage
- 13 From curve of capacity vs. elevation
- 14 From column 2, catchment, and runoff factor
- 15 Reduction in Florence Creek flow due to filling of water storage reservoir

## CINOLA GOLD PROJECT

HIGH WEST AREA

MONTHLY WATER BALANCE FOR AVERAGE ANNUAL PRECIPITATION: YEAR 1

YEAR 1 (page 1 of 3)

FILE: WB1

DATE: 29-Jun-99

W S RESERVOIR CATCHMENT = 162 ha  
 CATCHMENT FOR DITCH IE1 = 75 ha  
 RUNOFF FACTOR = 0.7

## WATER SUPPLY RESERVOIR

MONTH	PRECIP	POTENT	POND	DIRECT	RUNOFF	POND	SEEPAGE	SEEP TO	WATER	DECANT	FLOW TO	EXC/	WATER	WATER	RUNOFF IN	
	mm	mm	ha					1000 m <sup>3</sup> /d						m	1000 m <sup>3</sup> /d	
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	
JAN	216	18	9.35	0.65	7.45	0.04	0.000	0.003	0.20	0.00	3.12	4.73	0.879	303	3.66	
FEB	216	16	10.11	0.79	8.20	0.06	0.000	0.004	0.20	0.00	3.46	5.26	1.027	305	4.05	
MAR	144	26	11.63	0.54	4.89	0.10	0.000	0.004	0.20	0.00	4.16	0.97	1.057	305	2.44	
APR	171	40	11.63	0.66	6.00	0.16	0.000	0.004	0.20	0.00	5.11	1.20	1.093	305	2.39	
MAY	112	55	11.63	0.42	3.80	0.25	0.000	0.004	0.20	0.76	3.24	-0.22	1.066	305	1.90	
JUN	54	37	11.63	0.33	2.95	0.34	0.000	0.004	0.20	1.45	2.51	-1.22	1.049	305	1.47	
JUL	80	104	11.63	0.30	2.72	0.39	0.000	0.004	0.20	1.63	2.31	-1.52	1.002	305	1.35	
AUG	78	98	11.63	0.29	2.65	0.37	0.000	0.004	0.20	1.65	2.25	-1.54	0.954	304	1.62	
SEP	166	71	10.87	0.60	5.85	0.26	0.000	0.004	0.20	0.35	4.96	0.69	0.975	304	2.91	
OCT	297	44	10.87	1.04	10.14	0.15	0.000	0.004	0.20	0.00	4.29	6.53	1.177	306	5.03	
NOV	260	21	10.40	1.07	9.08	0.09	0.000	0.004	0.20	0.00	3.88	5.99	1.357	307	4.55	
DEC	260	12	10.17	1.10	8.74	0.05	0.000	0.004	0.20	0.00	3.76	5.83	1.537	309	4.40	
MEAN	173	50	11.33	0.65	6.02	0.19	0.000	0.004	0.20	0.49	3.58	2.20	1.100	305	3.00	
TOTAL	2084	598											1.31E+06 m <sup>3</sup>			1.09E+06 m <sup>3</sup>

## NOTES RE COLUMNS:

2 From Stage II Report, Vol III

3 From Stage II Report, Vol III

4 From curve of area vs. elevation

5 From columns 2 and 4

6 From columns 2, 4, catchment, and runoff factor

7 From columns 3 and 4

8 Set equal to zero

9 From seepage calculations

10 Mill make-up plus mill and mine domestic supply

11 Decant to Imp. #1 to maintain min. water vol, see column 28

12 Flow to Florence Creek equal to excess (column 13) when reservoir full, controlled at other times

13 Net result of columns 5 to 12

14 Water volume in storage

15 From curve of capacity vs. elevation

16 From column 2, catchment, and runoff factor

PULP DENSITY =	38 t	DRY DENSITY OF PLACED TAILINGS =	1.20 t/m <sup>3</sup>
TAILINGS MOISTURE CONTENT =	45 %	BULK DENSITY OF WASTE ROCK =	2.20 t/m <sup>3</sup>

IMPOUNDMENT #1 CATCHMENT =	44 ha	AREA OF LOW GRADE ORE STOCKPILE =	3.0 ha
TAILINGS DEPOSITION RATE =	6000 t/day	VOL OF TAILS PRODUCED IN YEAR =	1.83 M m <sup>3</sup>
WASTE ROCK DEPOSITION RATE =	0 t/day	VOL OF WASTE ROCK IN YEAR =	0.00 M m <sup>3</sup>
MILL EFFLUENT RECYCLE RATIO =	84 %	TOTAL VOL OF SOLIDS IN YEAR =	1.83 M m <sup>3</sup>

**IMPOUNDMENT NUMBER 1  
(ACTIVE)**

MONTH	POND AREA ha	DIRECT PRECIP mm	LOCAL RUNOFF mm	MILL RUNOFF mm	POND EVAP mm	SEEPAGE IN 1000 m <sup>3</sup> /d	SEEP TO IMP #3 mm	FROM MILL mm	RETURN TO MILL mm	RET IN PORES mm	EXC/DEF WS RES			TOT TAILS+ WASTE ROCK M m <sup>3</sup>	SOLIDS ELEV m	WATER ELEV m	
											17	18	19	20	21	22	23
JAN	3.0	0.21	2.00	0.34	0.01	0.073	0.003	9.71	9.28	2.70	0.33	0.00	0.110	0.000	0.155	270	271
FEB	5.9	0.46	2.06	0.38	0.03	0.074	0.005	9.71	9.28	2.70	0.65	0.00	0.128	0.295	271	273	
MAR	7.7	0.35	1.18	0.23	0.06	0.074	0.007	9.71	9.28	2.70	-0.51	0.00	0.113	0.450	273	274	
APR	8.5	0.49	1.41	0.29	0.11	0.074	0.008	9.71	9.28	2.70	-0.14	0.00	0.108	0.600	275	276	
MAY	10.4	0.33	0.95	0.19	0.22	0.074	0.009	9.71	9.28	2.70	-1.03	0.76	0.100	0.755	276	277	
JUN	11.3	0.32	0.64	0.14	0.33	0.074	0.010	9.71	9.28	2.70	-1.45	1.45	0.100	0.905	278	279	
JUL	13.1	0.34	0.56	0.13	0.44	0.074	0.012	9.71	9.28	2.70	-1.63	1.63	0.100	1.050	180	280	
AUG	14.0	0.35	0.53	0.12	0.44	0.074	0.013	9.71	9.28	2.70	-1.65	1.65	0.100	1.215	280	281	
SEP	15.1	0.34	1.12	0.27	0.36	0.074	0.014	9.71	9.28	2.70	-0.35	0.35	0.100	1.365	281	282	
OCT	16.2	1.55	1.86	0.47	0.23	0.074	0.014	9.71	9.28	2.70	1.44	0.00	0.145	1.520	282	283	
NOV	17.3	1.50	1.62	0.42	0.12	0.074	0.015	9.71	9.28	2.70	1.21	0.00	0.181	1.670	283	284	
DEC	18.4	1.54	1.50	0.41	0.07	0.074	0.016	9.71	9.28	2.70	1.17	0.00	0.217	1.825	284	285	
MEAN	11.8	0.69	1.27	0.28	0.20	0.074	0.011	9.71	9.28	2.70	-0.17	0.49	0.125	0.389	278	279	
TOTAL														-6.20E+04 m <sup>3</sup>			

17 From curve of area vs. elevation

18 From columns 2 and 17

19 From columns 2, 17, catchment, and runoff factor

20 Mill site and low grade ore stockpile runoff, plus other wastes

21 From columns 3 and 17

22-23 From seepage calculations

24 Mill effluent

25 Mill effluent recycle (as a % of total mill inflow)

26 From moisture content and deposition rates

27 Net result of columns 18 to 26

28 From columns 27 and 29

29 From columns 27 and 28; 100 000 m<sup>3</sup> minimum

30 From deposition rates and densities

31 From curve of capacity vs. elevation

32 From curve of capacity vs. elevation

IMPOUNDMENT #3 CATCHMENT = 425 ha

## SETTLING POND (IMPOUNDMENT NUMBER 3)

MONTH	POND AREA ha	DIRECT PRECIP	RUNOFF EVAP	POND IMP #1	SEEP FR OUT	SEEPAGE	EXC/ DEF	FLOW TO FLO CK	WATER IN POND	WATER ELEV	REDUCTION IN FLOW
-----<----1000 m <sup>3</sup> /d---->-----											
JAN	1.4	0.10	27.44	0.01	0.003	0.004	27.53	27.53	0.100	220	17.8
FEB	1.4	0.11	30.38	0.01	0.005	0.004	30.48	30.48	0.100	220	17.8
MAR	1.4	0.07	20.37	0.01	0.007	0.004	20.43	20.43	0.100	220	10.0
APR	1.4	0.09	25.00	0.02	0.008	0.004	25.07	25.07	0.100	220	10.0
MAY	1.4	0.05	15.85	0.03	0.009	0.004	15.87	15.87	0.100	220	10.1
JUN	1.4	0.04	12.18	0.04	0.010	0.004	12.29	12.29	0.100	220	10.2
JUL	1.4	0.04	11.32	0.05	0.012	0.004	11.32	11.32	0.100	220	10.2
AUG	1.4	0.04	11.04	0.04	0.013	0.004	11.04	11.04	0.100	220	10.2
SEP	1.4	0.08	24.27	0.03	0.014	0.004	24.32	24.32	0.100	220	10.0
OCT	1.4	0.13	37.73	0.02	0.014	0.004	37.85	37.85	0.100	220	17.8
NOV	1.4	0.12	34.13	0.01	0.015	0.004	34.25	34.25	0.100	220	17.8
DEC	1.4	0.12	33.93	0.01	0.016	0.004	33.15	33.15	0.100	220	17.8
MEAN	1.4	0.08	23.51	0.02	0.011	0.004	23.57	23.57	0.100	220	13.3
TOTAL									8.60E+06	m <sup>3</sup>	

33-34 As for Impoundment #1

35 Runoff from undisturbed catchment, plus columns 12 and 16

36-42 As for Impoundment #1

43 Reduction in Upper Florence Creek flow, before flow augmentation

## CINOLA GOLD PROJECT

HIGH WEST AREA

MONTHLY WATER BALANCE FOR AVERAGE ANNUAL PRECIPITATION: YEAR 2

YEAR 2 (page 1 of 3)

FILE: WEI

DATE: 29-Jun-89

W S RESERVOIR CATCHMENT = 162 ha  
 CATCHMENT FOR DITCH IE1 = 75 ha  
 RUNOFF FACTOR = 0.7

## WATER SUPPLY RESERVOIR

MONTH	PRECIP	POTENT	POND	DIRECT	RUNOFF	POND	SEEPAGE	SEEP TO	WATER	DECANT	FLOW TO	EXC/	WATER	WATER	RUNOFF IN	
													M m3			1000 m3/d
JAN	216	13	14.71	1.02	7.18	0.06	0.000	0.005	0.20	0.00	3.98	3.95	1.660	310	3.66	
FEB	215	16	15.48	1.19	7.91	0.09	0.000	0.005	0.20	0.00	3.81	0.00	1.660	310	4.05	
MAR	144	26	15.48	0.72	4.76	0.13	0.000	0.005	0.20	0.00	5.15	0.00	1.660	310	2.44	
APR	171	40	15.48	0.88	5.35	0.21	0.000	0.005	0.20	0.00	5.32	0.00	1.660	310	2.99	
MAY	112	56	15.48	0.55	3.71	0.33	0.000	0.005	0.20	0.00	3.73	0.00	1.660	310	1.90	
JUN	84	87	15.48	0.43	2.87	0.45	0.000	0.005	0.20	0.00	2.65	0.00	1.660	310	1.47	
JUL	80	104	15.48	0.40	2.65	0.52	0.000	0.005	0.20	0.00	2.32	0.00	1.660	310	1.35	
AUG	78	98	15.48	0.39	2.53	0.49	0.000	0.005	0.20	0.83	1.45	0.00	1.660	310	1.32	
SEP	166	71	15.48	0.86	5.68	0.37	0.000	0.005	0.20	0.24	5.72	0.00	1.660	310	2.91	
OCT	297	44	15.48	1.48	9.83	0.22	0.000	0.005	0.20	0.00	10.88	0.00	1.660	310	5.03	
NOV	260	21	15.48	1.34	8.89	0.11	0.000	0.005	0.20	0.00	9.92	0.00	1.660	310	4.55	
DEC	260	12	15.48	1.30	8.60	0.06	0.000	0.005	0.20	0.00	9.64	0.00	1.660	310	4.40	
MEAN	173	50	15.41	0.88	5.86	0.25	0.000	0.005	0.20	0.09	5.85	0.34	1.660	310	3.00	
TOTAL	2084	598										2.14E-06 m3				1.09E+06 m3

## NOTES RE COLUMNS:

2 From Stage II Report, Vol III

3 From Stage II Report, Vol III

4 From curve of area vs. elevation

5 From columns 2 and 4

6 From columns 2, 4, catchment, and runoff factor

7 From columns 3 and 4

8 Set equal to zero

9 From seepage calculations

10 Mill make-up plus mill and mine domestic supply

11 Decant to Imp. #1 to maintain min. water vol. see column 28

12 Flow to Florence Creek; equal to excess (column 13) when reservoir full, controlled at other times

13 Net result of columns 5 to 12

14 Water volume in storage

15 From curve of capacity vs. elevation

16 From column 2, catchment, and runoff factor

PULP DENSITY =	13 t	DRY DENSITY OF PLACED TAILINGS =	1.20 t/m <sup>3</sup>
TAILINGS MOISTURE CONTENT =	45 %	BULK DENSITY OF WASTE ROCK =	2.20 t/m <sup>3</sup>

IMPOUNDMENT #1 CATCHMENT =	44 ha	AREA OF LOW GRADE ORE STOCKPILE =	8.0 ha
TAILINGS DEPOSITION RATE =	6000 t/day	VOL OF TAILS PRODUCED IN YEAR =	1.83 M m <sup>3</sup>
WASTE ROCK DEPOSITION RATE =	0 t/day	VOL OF WASTE ROCK IN YEAR =	0.00 M m <sup>3</sup>
MILL EFFLUENT RECYCLE RATIO=	64 %	TOTAL VOL OF SOLIDS IN YEAR =	1.83 M m <sup>3</sup>

**IMPOUNDMENT NUMBER 1  
(ACTIVE)**

MONTH	POND AREA ha	1000 m <sup>3</sup> /d										EXC/DEF WS RES	FROM POND	TOT TAILS+ WASTE ROCK M m <sup>3</sup>	GELSOLIDS M m <sup>3</sup>	WATER ELEV. m
		DIRECT PRECIP	LOCAL RUNOFF	MILL RUNOFF	POND EVAP	SEEPAGE IN	SEEP TO IMP #3	FROM MILL	RETURN TO MILL	RET IN PORES	WATER ELEV.					
	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32
JAN	19.5	1.36	1.19	0.59	0.08	0.075	0.017	9.71	9.28	2.70	0.84	0.00	0.243	1.825	284	285
FEB	20.6	1.59	1.26	0.65	0.12	0.075	0.018	9.71	9.28	2.70	1.16	0.00	0.275	1.980	285	286
MAR	21.7	1.01	0.73	0.39	0.18	0.075	0.019	9.71	9.28	2.70	-0.28	0.00	0.267	2.275	286	288
APR	22.8	1.30	0.85	0.48	0.30	0.075	0.020	9.71	9.28	2.70	0.10	0.00	0.270	2.425	287	289
MAY	23.9	0.86	0.51	0.30	0.51	0.075	0.020	9.71	9.28	2.70	-1.05	0.00	0.287	2.580	289	289
JUN	23.9	0.57	0.33	0.24	0.69	0.075	0.020	9.71	9.28	2.70	-1.62	0.00	0.183	2.730	289	290
JUL	25.0	0.65	0.34	0.22	0.84	0.075	0.021	9.71	9.28	2.70	-1.86	0.00	0.131	2.885	290	290
AUG	25.0	0.63	0.33	0.21	0.79	0.075	0.021	9.71	9.28	2.70	-1.84	0.83	0.100	3.040	290	291
SEP	26.0	1.44	0.70	0.46	0.62	0.075	0.022	9.71	9.28	2.70	-0.24	0.24	0.100	3.190	291	291
OCT	25.0	2.49	1.21	0.80	0.37	0.075	0.022	9.71	9.28	2.70	1.91	0.00	0.159	3.245	291	292
NOV	27.0	2.34	1.03	0.73	0.19	0.075	0.023	9.71	9.28	2.70	1.89	0.00	0.210	3.495	292	292
DEC	27.0	2.25	1.00	0.70	0.10	0.075	0.023	9.71	9.28	2.70	1.64	0.00	0.251	3.650	292	293
MEAN	24.1	1.38	0.79	0.48	0.40	0.075	0.021	9.71	9.28	2.70	0.03	0.09	0.203	2.814	289	290
TOTAL													1.08E+04 m <sup>3</sup>			

17 From curve of area vs. elevation

18 From columns 2 and 17

19 From columns 2, 17, catchment, and runoff factor

20 Mill site and low grade ore stockpile runoff, plus other wastes

21 From columns 3 and 17

22-23 From seepage calculations

24 Mill effluent

25 Mill effluent recycle (as a % of total mill inflow)

26 From moisture content and deposition rates

27 Net result of columns 18 to 26

28 From columns 27 and 29

29 From column 27 and 28; 100 000 m<sup>3</sup> minimum

30 From deposition rates and densities

31 From curve of capacity vs. elevation

32 From curve of capacity vs. elevation

IMPOUNDMENT #3 CATCHMENT = 420 ha

## SETTLING POND (IMPOUNDMENT NUMBER 3)

MONTH	POND AREA ha	DIRECT PRECIP	RUNOFF EVAP	POND IMP #1 1000 m3/d	SEEP FR IMP #1	SEEPAGE OUT	EXC/ DEF	FLOW TO FLO CK	WATER IN POND		REDUCTION IN FLOW	
									M m3	m		
		33	34	35	36	37	38	39	40	41	42	43
JAN	1.4	0.10	23.05	0.01	0.017	0.004	28.16	28.16	0.100	220		
FEB	1.4	0.11	35.47	0.01	0.018	0.004	35.58	35.58	0.100	220	6.2	
MAR	1.4	0.07	21.20	0.01	0.013	0.004	21.27	21.27	0.100	220	6.8	
APR	1.4	0.08	25.01	0.02	0.020	0.004	26.09	26.09	0.100	220	6.9	
MAY	1.4	0.05	15.21	0.03	0.020	0.004	15.25	15.25	0.100	220	9.2	
JUN	1.4	0.04	12.83	0.04	0.020	0.004	12.84	12.84	0.100	220	9.3	
JUL	1.4	0.04	11.24	0.05	0.021	0.004	11.25	11.25	0.100	220	10.7	
AUG	1.4	0.04	10.14	0.04	0.021	0.004	10.15	10.15	0.100	220	16.4	
SEP	1.4	0.08	24.34	0.03	0.022	0.004	24.90	24.90	0.100	220	6.2	
OCT	1.4	0.13	43.39	0.02	0.022	0.004	44.12	44.12	0.100	220	6.4	
NOV	1.4	0.12	39.86	0.01	0.023	0.004	39.99	39.99	0.100	220	6.2	
DEC	1.4	0.12	39.81	0.01	0.023	0.004	39.75	39.75	0.100	220	6.1	
MEAN	1.4	0.08	25.58	0.02	0.021	0.004	25.65	25.66	0.100	220	9.1	
TOTAL								9.36E+06	m3			

33-34 As for Impoundment #1

35 Runoff from undisturbed catchment, plus columns 12 and 16

36-42 As for Impoundment #1

43 Reduction in Upper Florence Creek flow, before flow augmentation

## CINOLA GOLD PROJECT

HIGH WEST AREA

MONTHLY WATER BALANCE FOR AVERAGE ANNUAL PRECIPITATION: YEAR 3

YEAR 3 (page 1 of 3)

FILE: WBS

DATE: 29-Jun-89

W S RESERVOIR CATCHMENT = 162 ha  
 CATCHMENT FOR DITCH IE1 = 75 ha  
 RUNOFF FACTOR = 0.7

## WATER SUPPLY RESERVOIR

MONTH	PRECIP	POTENT	POND	DIRECT	RUNOFF	POND	SEEPAGE	SEEP TO	WATER	DECANT	FLOW TO	EXC/	WATER	WATER	RUNOFF IN	
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	
JAN	216	13	15.48	1.03	7.15	0.05	0.000	0.005	0.20	0.00	7.96	0.00	1.660	310	3.66	
FEB	216	16	15.48	1.19	7.91	0.09	0.000	0.005	0.20	0.00	8.81	0.00	1.660	310	4.05	
MAR	144	26	15.48	0.72	4.76	0.13	0.000	0.005	0.20	0.00	5.15	0.00	1.660	310	2.44	
APR	171	40	15.48	0.88	5.85	0.21	0.000	0.005	0.20	0.00	6.32	0.00	1.660	310	2.88	
MAY	112	55	15.48	0.58	3.71	0.03	0.000	0.005	0.20	0.00	3.73	0.00	1.660	310	1.80	
JUN	84	37	15.48	0.43	2.37	0.45	0.000	0.005	0.20	0.00	2.65	0.00	1.660	310	1.47	
JUL	80	104	15.48	0.40	2.65	0.52	0.000	0.005	0.20	0.00	2.32	0.00	1.660	310	1.35	
AUG	78	98	15.48	0.39	2.59	0.49	0.000	0.005	0.20	0.00	2.28	0.00	1.660	310	1.32	
SEP	166	71	15.48	0.86	5.33	0.37	0.000	0.005	0.20	0.00	5.96	0.00	1.660	310	2.91	
OCT	297	44	15.48	1.48	9.83	0.22	0.000	0.005	0.20	0.00	10.88	0.00	1.660	310	5.08	
NOV	260	21	15.48	1.04	8.89	0.11	0.000	0.005	0.20	0.00	9.92	0.00	1.660	310	4.55	
DEC	260	12	15.48	1.00	8.60	0.06	0.000	0.005	0.20	0.00	9.54	0.00	1.660	310	4.40	
MEAN	173	50	15.48	0.98	5.86	0.25	0.000	0.005	0.20	0.00	6.28	0.00	1.660	310	3.00	
TOTAL	2084	598										2.29E+06 m3				1.09E+06 m3

## NOTES RE COLUMNS:

2 From Stage II Report, Vol III

3 From Stage II Report, Vol III

4 From curve of area vs. elevation

5 From columns 2 and 4

6 From columns 2, 4, catchment, and runoff factor

7 From columns 3 and 4

8 Set equal to zero

9 From seepage calculations

10 Mill make-up plus mill and mine domestic supply

11 Decant to Imp. #1 to maintain min. water vol, see column 28

12 Flow to Florence Creek; equal to excess (column 13) when reservoir full, controlled at other times

13 Net result of columns 5 to 12

14 Water volume in storage

15 From curve of capacity vs. elevation

16 From column 2, catchment, and runoff factor

PULP DENSITY = 38 % DRY DENSITY OF PLACED TAILINGS = 1.20 t/m<sup>3</sup>  
 TAILINGS MOISTURE CONTENT = 45 % BULK DENSITY OF WASTE ROCK = 2.20 t/m<sup>3</sup>

IMPOUNDMENT #1 CATCHMENT = 44 ha AREA OF LOW GRADE ORE STOCKPILE = 10.0 ha  
 TAILINGS DEPOSITION RATE = 6000 t/day VOL OF TAILS PRODUCED IN YEAR = 1.83 M m<sup>3</sup>  
 WASTE ROCK DEPOSITION RATE = 2500 t/day VOL OF WASTE ROCK IN YEAR = 0.43 M m<sup>3</sup>  
 MILL EFFLUENT RECYCLE RATIO= 94 % TOTAL VOL OF SOLIDS IN YEAR = 2.26 M m<sup>3</sup>

IMPOUNDMENT NUMBER 1  
 (ACTIVE)

MONTH	POND AREA ha	DIRECT PRECIP		LOCAL RUNOFF		MILL RUNOFF		SEEPAGE IN 1000 m <sup>3</sup> /d	SEEP TO IMP #3	FROM MILL	RETURN TO MIL	RET IN PORES	EXC/DEF WS RES	FROM POND	WATER IN POND	TOT TAILS+ WASTE ROCK	SOLIDS ELEV	WATER ELEV
		17	18	19	20	21	22											
JAN	28.0	1.95	0.78	0.68	0.12	0.075	0.024	9.71	9.28	2.70	1.07	0.00	0.261	0.950	292	290		
FEB	29.0	2.24	0.91	0.76	0.17	0.075	0.025	9.71	9.28	2.70	1.41	0.00	0.294	0.842	293	291		
MAR	30.0	1.39	0.46	0.46	0.25	0.075	0.026	9.71	9.28	2.70	-0.17	0.00	0.323	4.206	294	292		
APR	30.0	1.71	0.55	0.55	0.40	0.075	0.026	9.71	9.28	2.70	0.20	0.00	0.334	4.392	295	293		
MAY	31.0	1.12	0.38	0.35	0.65	0.075	0.026	9.71	9.28	2.70	-1.08	0.00	0.300	4.583	295	293		
JUN	31.0	2.87	0.25	0.27	0.90	0.075	0.026	9.71	9.28	2.70	-1.73	0.00	0.249	4.769	295	297		
JUL	32.0	0.83	0.22	0.25	1.07	0.075	0.027	9.71	9.28	2.70	-2.01	0.00	0.136	4.961	297	297		
AUG	32.0	0.91	0.21	0.25	1.01	0.075	0.027	9.71	9.28	2.70	-1.38	0.00	0.125	5.152	297	297		
SEP	33.0	1.83	0.43	0.54	0.79	0.075	0.028	9.71	9.28	2.70	-0.22	0.00	0.119	5.338	298	298		
OCT	33.0	3.16	0.74	0.94	0.47	0.075	0.028	9.71	9.28	2.70	2.14	0.00	0.185	5.529	298	298		
NOV	34.0	2.95	0.61	0.65	0.24	0.075	0.028	9.71	9.28	2.70	1.63	0.00	0.243	5.715	299	300		
DEC	35.0	2.94	0.53	0.82	0.14	0.075	0.030	9.71	9.28	2.70	1.92	0.00	0.303	5.906	300	301		
MEAN	31.5	1.81	0.49	0.56	0.52	0.075	0.027	9.71	9.28	2.70	0.11	0.00	0.249	4.872	296	297		
TOTAL													4.19E+04 m <sup>3</sup>					

17 From curve of area vs. elevation

18 From columns 2 and 17

19 From columns 2, 17, catchment, and runoff factor

20 Mill site and low grade ore stockpile runoff, plus other wastes

21 From columns 3 and 17

22-23 From seepage calculations

24 Mill effluent

25 Mill effluent recycle (as a % of total mill inflow)

26 From moisture content and deposition rates

27 Net result of columns 18 to 26

28 From columns 27 and 29

29 From column 27 and 28; 100 000 m<sup>3</sup> minimum

30 From deposition rates and densities

31 From curve of capacity vs. elevation

32 From curve of capacity vs. elevation

## YEAR 3 (page 3 of 3)

IMPOUNDMENT #3 CATCHMENT = 418 ha

## SETTLING POND (IMPOUNDMENT NUMBER 3)

MONTH	POND AREA ha	DIRECT PRECIP	RUNOFF 34	POND EVAP 35	SEEP FR IMP #1 36	SEEPAGE 37	EXC/DEF 38	FLOW TO FLO CK 39	WATER IN POND 40	WATER ELEV 41	REDUCTION IN FLOW 42	I
				1000 m3/d					1 m3			
JAN	1.4	0.10	31.93	0.01	0.024	0.004	32.04	32.04	0.100	220		
FEB	1.4	0.11	35.35	0.01	0.025	0.004	35.48	35.48	0.100	220		6.5
MAR	1.4	0.07	21.13	0.01	0.026	0.004	21.21	21.21	0.100	220		7.1
APR	1.4	0.08	25.93	0.02	0.025	0.004	26.01	26.01	0.100	220		7.1
MAY	1.4	0.05	16.15	0.02	0.026	0.004	16.21	16.21	0.100	220		9.5
JUN	1.4	0.04	12.23	0.04	0.025	0.004	12.31	12.31	0.100	220		10.0
JUL	1.4	0.04	11.20	0.05	0.027	0.004	11.21	11.21	0.100	220		10.9
AUG	1.4	0.04	10.93	0.04	0.027	0.004	10.95	10.95	0.100	220		10.8
SEP	1.4	0.08	25.00	0.03	0.028	0.004	25.07	25.07	0.100	220		7.7
OCT	1.4	0.13	43.85	0.02	0.028	0.004	43.99	43.99	0.100	220		6.5
NOV	1.4	0.12	39.74	0.01	0.029	0.004	39.88	39.88	0.100	220		6.4
DEC	1.4	0.12	38.50	0.01	0.030	0.004	38.63	38.63	0.100	220		6.3
MEAN	1.4	0.08	25.93	0.02	0.027	0.004	26.01	26.01	0.100	220		7.9
TOTAL								9.49E-06 m3				

33-34 As for Impoundment #1

35 Runoff from undisturbed catchment, plus columns 12 and 16

36-42 As for Impoundment #1

43 Reduction in Upper Florence Creek flow, before flow augmentation

## CINOLA GOLD PROJECT

HIGH WEST AREA

MONTHLY WATER BALANCE FOR AVERAGE ANNUAL PRECIPITATION: YEAR 4

YEAR 4 (page 1 of 3)

FILE: WB4

DATE: 29-Jun-93

W S RESERVOIR CATCHMENT = 162 ha  
 CATCHMENT FOR DITCH IEI = 75 ha  
 RUNOFF FACTOR = 0.7

## WATER SUPPLY RESERVOIR

MONTH	PRECIP	POTENT	POND	DIRECT	RUNOFF	POND	SEEPAGE	SEEP TO	WATER	DECANT	FLOW TO	EXC/	WATER	WATER	RUNOFF IN	
			ha	ha				1000 m3/d						M m3	m	1000 m3/d
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	
JAN	216	18	15.48	1.08	7.15	0.06	0.000	0.005	0.20	0.00	7.95	0.00	1.660	310	3.66	
FEB	216	16	15.48	1.19	7.31	0.09	0.000	0.005	0.20	0.00	8.81	0.00	1.660	310	4.05	
MAR	144	26	15.48	0.72	4.76	0.13	0.000	0.005	0.20	0.00	5.15	0.00	1.660	310	2.44	
APR	171	40	15.48	0.89	5.85	0.21	0.000	0.005	0.20	0.00	5.82	0.00	1.660	310	2.99	
MAY	112	66	15.48	0.56	3.71	0.33	0.000	0.005	0.20	0.00	3.73	0.00	1.660	310	1.90	
JUN	84	87	15.48	0.43	2.87	0.45	0.000	0.005	0.20	0.00	2.65	0.00	1.660	310	1.47	
JUL	90	104	15.48	0.40	2.65	0.52	0.000	0.005	0.20	0.00	2.51	0.00	1.660	310	1.35	
AUG	78	98	15.48	0.39	2.58	0.49	0.000	0.005	0.20	0.00	2.28	0.00	1.660	310	1.32	
SEP	166	71	15.48	0.86	5.68	0.37	0.000	0.005	0.20	0.00	5.96	0.00	1.660	310	2.91	
OCT	297	44	15.48	1.48	9.83	0.22	0.000	0.005	0.20	0.00	10.88	0.00	1.660	310	5.03	
NOV	260	21	15.48	1.34	8.89	0.11	0.000	0.005	0.20	0.00	9.92	0.00	1.660	310	4.55	
DEC	260	12	15.48	1.30	8.50	0.06	0.000	0.005	0.20	0.00	9.54	0.00	1.660	310	4.40	
MEAN	173	50	15.48	0.88	5.86	0.25	0.000	0.005	0.20	0.00	6.23	0.00	1.660	310	3.00	
TOTAL	2084	598										2.295E+06	m3			1.09E+06

## NOTES RE COLUMNS:

2 From Stage II Report, Vol III

3 From Stage II Report, Vol III

4 From curve of area vs. elevation

5 From columns 2 and 4

6 From columns 2, 4, catchment, and runoff factor

7 From columns 3 and 4

8 Set equal to zero

9 From seepage calculations

10 Mill make-up plus mill and mine domestic supply

11 Decant to Imp. #1 to maintain min. water vol, see column 28

12 Flow to Florence Creek; equal to excess (column 13) when reservoir full, controlled at other times

13 Net result of columns 5 to 12

14 Water volume in storage

15 From curve of capacity vs. elevation

16 From column 2, catchment, and runoff factor

PULP DENSITY =	38 t	DRY DENSITY OF PLACED TAILINGS =	1.20 t/m <sup>3</sup>
TAILINGS MOISTURE CONTENT =	45 %	BULK DENSITY OF WASTE ROCK =	2.20 t/m <sup>3</sup>
IMPOUNDMENT #1 CATCHMENT =	44 ha	AREA OF LOW GRADE ORE STOCKPILE =	8.0 ha
TAILINGS DEPOSITION RATE =	6000 t/day	VOL OF TAILS PRODUCED IN YEAR =	1.83 M m <sup>3</sup>
WASTE ROCK DEPOSITION RATE =	2500 t/day	VOL OF WASTE ROCK IN YEAR =	0.41 M m <sup>3</sup>
MILL EFFLUENT RECYCLE RATIO=	84 %	TOTAL VOL OF SOLIDS IN YEAR =	2.24 M m <sup>3</sup>

**IMPOUNDMENT NUMBER 1  
(ACTIVE)**

MONTH	POND AREA ha	DIRECT PRECIP ha	LOCAL RUNOFF	MILL RUNOFF	POND EVAP	SEEPAGE IN 1000 m <sup>3</sup> /d	SEEP TO IMP #3	FROM MILL	RETURN TO MILL	RET IN PORES	EXC/DEF WS REG	FROM WATER IN POND	TOT TAILS+ WASTE ROCK m <sup>3</sup>	SOLIDS ELEV m	WATER ELEV m																
																17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32
JAN	35.0	2.44	0.44	0.59	0.15	0.075	0.030	9.71	9.28	2.70	1.09	0.00	0.336	5.906	300	300															
FEB	36.0	2.78	0.43	0.65	0.21	0.075	0.031	9.71	9.28	2.70	1.42	0.00	0.376	5.268	301	301															
MAR	37.0	1.72	0.23	0.39	0.31	0.075	0.031	9.71	9.28	2.70	-0.21	0.00	0.370	6.459	301	301															
APR	37.0	2.11	0.29	0.48	0.49	0.075	0.031	9.71	9.28	2.70	0.14	0.00	0.374	6.643	301	302															
MAY	38.0	1.37	0.15	0.30	0.31	0.075	0.032	9.71	9.28	2.70	-1.21	0.00	0.336	5.333	302	302															
JUN	38.0	1.06	0.12	0.24	1.10	0.075	0.032	9.71	9.28	2.70	-1.92	0.00	0.279	7.017	303	303															
JUL	38.0	0.98	0.11	0.22	1.27	0.075	0.032	9.71	9.28	2.70	-2.20	0.00	0.210	7.207	303	304															
AUG	39.0	0.98	0.09	0.21	1.23	0.075	0.033	9.71	9.28	2.70	-2.19	0.00	0.143	7.393	304	304															
SEP	39.0	2.16	0.19	0.46	0.92	0.075	0.033	9.71	9.28	2.70	-0.34	0.00	0.132	7.582	304	305															
OCT	40.0	3.33	0.27	0.30	0.57	0.075	0.034	9.71	9.28	2.70	2.10	0.00	0.197	7.772	305	305															
NOV	40.0	3.47	0.24	0.73	0.26	0.075	0.034	9.71	9.28	2.70	1.92	0.00	0.255	7.956	305	306															
DEC	41.0	3.44	0.16	0.70	0.15	0.075	0.035	9.71	9.28	2.70	1.92	0.00	0.315	8.146	306	306															
MEAN	38.2	2.19	0.23	0.48	0.63	0.075	0.032	9.71	9.28	2.70	0.03	0.00	0.276	7.120	303	304															
TOTAL												1.23E+04	m <sup>3</sup>																		

17 From curve of area vs. elevation

18 From columns 2 and 17

19 From columns 2, 17, catchment, and runoff factor

20 Mill site and low grade ore stockpile runoff, plus other wastes

21 From columns 3 and 17

22-23 From seepage calculations

24 Mill effluent

25 Mill effluent recycle (as a % of total mill inflow)

26 From moisture content and deposition rates

27 Net result of columns 18 to 26

28 From columns 27 and 29

29 From column 27 and 28; 100 000 m<sup>3</sup> minimum

30 From deposition rates and densities

31 From curve of capacity vs. elevation

32 From curve of capacity vs. elevation

IMPOUNDMENT #3 CATCHMENT = 420 ha

## SETTLING POND (IMPOUNDMENT NUMBER 3)

MONTH	POND	DIRECT	RUNOFF	POND	SEEP	FR	SEEPAGE	EXC/	FLOW TO	WATER	WATER	REDUCTION
	AREA	PRECIP		EVAP	IMP #1	OUT		DEF	FLOW CK	IN POND	ELEV	
	ha									M m3	m	%
	33	34	35	36	37	38	39	39	40	41	42	43
JAN	1.4	0.10	22.03	0.01	0.030	0.004	32.15	32.15	0.100	220		6.2
FEB	1.4	0.11	35.47	0.01	0.031	0.004	35.53	35.53	0.100	220		6.2
MAR	1.4	0.07	21.20	0.01	0.031	0.004	21.29	21.28	0.100	220		6.3
APR	1.4	0.08	25.01	0.02	0.031	0.004	25.10	25.10	0.100	220		6.3
MAY	1.4	0.05	16.21	0.02	0.032	0.004	16.26	16.26	0.100	220		6.2
JUN	1.4	0.04	12.83	0.04	0.032	0.004	12.35	12.35	0.100	220		9.7
JUL	1.4	0.04	11.24	0.05	0.032	0.004	11.26	11.25	0.100	220		10.6
AUG	1.4	0.04	10.97	0.04	0.033	0.004	10.99	10.99	0.100	220		10.5
SEP	1.4	0.08	25.08	0.03	0.033	0.004	25.17	25.15	0.100	220		7.4
OCT	1.4	0.13	43.99	0.02	0.034	0.004	44.13	44.13	0.100	220		6.4
NOV	1.4	0.12	39.86	0.01	0.034	0.004	40.00	40.00	0.100	220		6.2
DEC	1.4	0.12	38.61	0.01	0.035	0.004	38.76	38.76	0.100	220		6.1
MEAN	1.4	0.08	25.01	0.02	0.032	0.004	26.09	26.09	0.100	220		7.6
TOTAL									9.52E+06 m3			

33-34 As for Impoundment #1

35 Runoff from undisturbed catchment, plus columns 12 and 16

36-42 As for Impoundment #1

43 Reduction in Upper Florence Creek flow, before flow augmentation

## CONOLA GOLD PROJECT

HIGH WEST AREA

MONTHLY WATER BALANCE FOR AVERAGE ANNUAL PRECIPITATION: YEAR 5

YEAR 5 (page 1 of 4)

FILE: WBS

DATE: 29-Jun-89

W S RESERVOIR CATCHMENT = 162 ha  
 CATCHMENT FOR DITCH IE1 = 75 ha  
 RUNOFF FACTOR = 0.7

## WATER SUPPLY RESERVOIR

MONTH	PRECIP	POTENT EVAPOT	POND AREA	DIRECT PRECIP	RUNOFF	POND EVAP	SEEPAGE IN	SEEP TO IMP #1	WATER SUPPLY	DECANT	FLOW TO SET POND	EXC/ DEF IN RES		WATER ELEV	RUNOFF IN DITCH IE1
												mm	mm	ha	mm
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16
JAN	216	13	15.48	1.08	7.15	0.06	0.000	0.005	0.20	0.00	7.96	0.00	1.660	310	0.66
FEB	216	16	15.48	1.19	7.31	0.09	0.000	0.005	0.20	0.00	8.31	0.00	1.660	310	4.05
MAR	144	26	15.48	0.72	4.76	0.13	0.000	0.005	0.20	0.00	5.15	0.00	1.660	310	2.44
APR	171	40	15.48	0.88	5.85	0.21	0.000	0.005	0.20	0.00	5.32	0.00	1.660	310	2.99
MAY	112	65	15.48	0.55	3.71	0.33	0.000	0.005	0.20	0.00	3.73	0.00	1.660	310	1.93
JUN	84	37	15.48	0.43	2.37	0.45	0.000	0.005	0.20	0.00	2.65	0.00	1.660	310	1.47
JUL	80	104	15.48	0.40	2.65	0.52	0.000	0.005	0.20	0.00	2.32	0.00	1.660	310	1.35
AUG	78	98	15.48	0.39	2.58	0.49	0.000	0.005	0.20	0.00	2.28	0.00	1.660	310	1.32
SEP	166	71	15.48	0.86	5.68	0.37	0.000	0.005	0.20	0.00	5.36	0.00	1.660	310	2.91
OCT	297	44	15.48	1.48	9.33	0.22	0.000	0.005	0.20	0.00	10.88	0.00	1.660	310	5.03
NOV	260	21	15.48	1.34	8.89	0.11	0.000	0.005	0.20	0.00	9.92	0.00	1.660	310	4.55
DEC	260	12	15.48	1.30	8.50	0.06	0.000	0.005	0.20	0.00	9.64	0.00	1.660	310	4.40
MEAN	173	50	15.48	0.88	5.86	0.25	0.000	0.005	0.20	0.00	6.28	0.00	1.660	310	3.00
TOTAL	2084	598										2.29E-06 m3			1.09E+06

## NOTES RE COLUMNS:

- 2 From Stage II Report, Vol III
- 3 From Stage II Report, Vol III
- 4 From curve of area vs. elevation
- 5 From columns 2 and 4
- 6 From columns 2, 4, catchment, and runoff factor
- 7 From columns 3 and 4
- 8 Set equal to zero
- 9 From seepage calculations
- 10 Mill make-up plus mill and mine domestic supply
- 11 Decant to Imp. #1 to maintain min. water vol, if necessary

- 12 Flow to Florence Creek; equal to excess (column 13) when reservoir full, controlled at other times
- 13 Net result of columns 5 to 12
- 14 Water volume in storage
- 15 From curve of capacity vs. elevation
- 16 From column 2, catchment, and runoff factor

IMPOUNDMENT #1 CATCHMENT = 44 ha

## IMPOUNDMENT NUMBER 1

MONTH	POND AREA ha	DIRECT PRECIP	LOCAL RUNOFF	POND EVAP	SEEPAGE IN	SEEP TO DECANT IMP #2	DECANT TO SET POND	EXC/DEF	FROM WSR	WATER IN POND	TOT TAILS+ WASTE ROCK	SOLIDS ELEV	WATER ELEV		
-----> 1000 m <sup>3</sup> /d ----->															
		17	18	19	20	21	22	23	24	25	26	27	28	29	30
JAN	41.0	2.86	0.15	0.17	0.075	0.032	13.03	0.00	-10.16	0.00	0.000	8.146	306	306	
FEB	41.0	2.86	0.16	0.23	0.075	0.029	0.00	0.00	2.83	0.00	0.079	8.146	306	306	
MAR	41.0	1.90	0.10	0.34	0.075	0.028	0.00	0.00	1.71	0.00	0.132	8.146	306	306	
APR	41.0	2.25	0.12	0.55	0.075	0.029	0.00	0.00	1.88	0.00	0.189	8.146	306	306	
MAY	41.0	1.48	0.08	0.87	0.075	0.027	0.00	0.00	0.73	0.00	0.211	8.146	306	306	
JUN	41.0	1.11	0.06	1.19	0.075	0.027	0.00	0.00	0.03	0.00	0.212	8.146	306	306	
JUL	41.0	1.06	0.05	1.38	0.075	0.026	0.00	0.00	-0.21	0.00	0.205	8.146	305	306	
AUG	41.0	1.03	0.05	1.30	0.075	0.026	0.00	0.00	-0.16	0.00	0.200	8.146	306	306	
SEP	41.0	2.20	0.12	0.87	0.075	0.026	0.00	0.00	1.39	0.00	0.242	8.146	306	306	
OCT	41.0	3.93	0.20	0.58	0.075	0.025	0.00	0.00	3.60	0.00	0.354	8.146	306	307	
NOV	42.0	3.52	0.12	0.29	0.075	0.025	0.00	0.00	3.40	0.00	0.456	8.146	306	307	
DEC	42.0	3.52	0.00	0.16	0.075	0.024	0.00	0.00	3.41	0.00	0.561	8.146	306	307	
MEAN	41.2	2.31	0.10	0.57	0.075	0.027	1.11	0.00	0.58	0.00	0.233	8.146	306	306	
TOTAL											2.47E+05 m <sup>3</sup>				

17 From curve of area vs. elevation

30 From curve of capacity vs. elevation

18 From columns 2 and 17

19 From columns 2, 17, catchment, and runoff factor

20 From columns 3 and 17

21-22 From seepage calculations

23 Decant of pond water to Imp #2

24 Set to zero for Year 5

25 Net result of columns 18 to 24

26 Decant from water supply res., if necessary

27 From columns 25 and 26; 100 000 m<sup>3</sup> minimum

28-29 From Year 4

PULP DENSITY = 38 t DRY DENSITY OF PLACED TAILINGS = 1.20 t/m<sup>3</sup>  
 TAILINGS MOISTURE CONTENT = 45 % BULK DENSITY OF WASTE ROCK = 2.20 t/m<sup>3</sup>

IMPOUNDMENT #2 CATCHMENT = 50 ha AREA OF LOW GRADE ORE STOCKPILE = 5.0 ha  
 TAILINGS DEPOSITION RATE = 6000 t/day VOL OF TAILS PRODUCED IN YEAR = 1.83 M m<sup>3</sup>  
 WASTE ROCK DEPOSITION RATE = 2500 t/day VOL OF WASTE ROCK IN YEAR = 0.41 M m<sup>3</sup>  
 MILL EFFLUENT RECYCLE RATIO= 84 % TOTAL VOL OF SOLIDS IN YEAR = 2.24 M m<sup>3</sup>

IMPOUNDMENT NUMBER 2  
 (ACTIVE)

MONTH	POND AREA ha	DIRECT PRECIP	LOCAL RUNOFF	MILL RUNOFF	POND EVAP	SEEPAGE IN 1000 m <sup>3</sup> /d	SEEPAGE OUT	FROM CUT	RETURN TO MILL	RET IN MILL PORES	EXC/DEF IMP #1		WATER IN POND	TOT TAILS IN POND	WASTE ROCK	COLLDS ELEV	WATER ELEV
											31	32	33	34	35	36	37
JAN	0.0	0.00	2.44	0.44	0.00	0.085	0.000	9.71	9.29	2.70	0.89	13.03	0.425	0.190	242	248	
FEB	10.1	0.73	2.16	0.49	0.05	0.082	0.006	9.71	9.29	2.70	1.16	0.00	0.458	0.362	245	250	
MAR	13.0	0.60	1.20	0.29	0.11	0.081	0.007	9.71	9.29	2.70	-0.21	0.00	0.451	0.552	247	251	
APR	13.8	0.79	1.44	0.35	0.18	0.081	0.008	9.71	9.29	2.70	0.20	0.00	0.457	0.736	249	252	
MAY	14.6	0.53	0.90	0.23	0.81	0.080	0.009	9.71	9.29	2.70	-0.36	0.00	0.430	0.817	251	253	
JUN	15.4	0.43	0.58	0.13	0.45	0.080	0.009	9.71	9.29	2.70	-1.37	0.00	0.289	1.111	252	254	
JUL	16.2	0.42	0.51	0.15	0.54	0.079	0.010	9.71	9.29	2.70	-1.55	0.00	0.341	1.301	253	255	
AUG	17.0	0.43	0.58	0.16	0.54	0.079	0.011	9.71	9.29	2.70	-1.59	0.00	0.292	1.491	254	256	
SEP	17.8	0.98	1.25	0.35	0.42	0.079	0.011	9.71	9.29	2.70	-0.05	0.00	0.291	1.675	255	257	
OCT	18.6	1.78	2.11	0.60	0.26	0.078	0.012	9.71	9.29	2.70	2.02	0.00	0.353	1.865	256	258	
NOV	19.4	1.68	1.35	0.55	0.14	0.079	0.013	9.71	9.29	2.70	1.74	0.00	0.405	2.050	257	260	
DEC	21.0	1.76	1.70	0.53	0.08	0.077	0.014	9.71	9.29	2.70	1.70	0.00	0.458	2.240	259	261	
MEAN	14.8	0.85	1.41	0.36	0.26	0.080	0.009	9.71	9.29	2.70	0.15	1.11	0.396	1.213	252	255	
TOTAL													5.41E+04 m <sup>3</sup>				

31 From curve of area vs. elevation

42 From columns 20, 41 and 43

32 From columns 2 and 31

43 From columns 41 and 42; 100 000 m<sup>3</sup> minimum

33 From columns 2, 31, catchment, and runoff factor

44 From deposition rates and densities

34 Mill site and low grade ore stockpile runoff, plus other wastes

45 From curve of capacity vs. elevation

35 From columns 3 and 31

46 From curve of capacity vs. elevation

36-37 From seepage calculations

38 Mill effluent

39 Mill effluent recycle (as a % of total mill inflow)

40 From moisture content and deposition rates

41 Net result of columns 32 to 40

IMPOUNDMENT #3 CATCHMENT = 373 ha

## SETTLING POND (IMPOUNDMENT NUMBER 3)

MONTH	POND AREA ha	DIRECT PRECIP	RUNOFF EVAP	POND IMP #2	SEEP FR OUT	SEEPAGE IMP #1	DECANT FR	EXC/DEF	FLOW TO FLO CK	WATER IN POND	WATER ELEV	REDUCTION IN FLOW	
					1000 m3/d								
					47	48	49	50	51	52	53	54	55
JAN	1.4	0.10	29.74	0.01	0.000	0.004	0.00	29.83	29.83	0.100	220		
FEB	1.4	0.11	32.93	0.01	0.004	0.004	0.00	33.03	33.03	0.100	220		12.0
MAR	1.4	0.07	19.67	0.01	0.005	0.004	0.00	19.72	19.72	0.100	220		12.6
APR	1.4	0.08	24.14	0.02	0.006	0.004	0.00	24.20	24.20	0.100	220		12.7
MAY	1.4	0.03	15.02	0.03	0.005	0.004	0.00	15.05	15.05	0.100	220		14.1
JUN	1.4	0.04	11.40	0.04	0.007	0.004	0.00	11.41	11.41	0.100	220		15.7
JUL	1.4	0.04	10.39	0.05	0.007	0.004	0.00	10.39	10.39	0.100	220		15.5
AUG	1.4	0.04	10.14	0.04	0.008	0.004	0.00	10.14	10.14	0.100	220		15.4
SEP	1.4	0.08	23.76	0.03	0.008	0.004	0.00	23.81	23.81	0.100	220		13.2
OCT	1.4	0.13	40.84	0.02	0.009	0.004	0.00	40.95	40.95	0.100	220		12.1
NOV	1.4	0.12	37.01	0.01	0.009	0.004	0.00	37.13	37.13	0.100	220		12.0
DEC	1.4	0.12	35.36	0.01	0.010	0.004	0.00	35.37	35.37	0.100	220		11.9
MEAN	1.4	0.08	24.13	0.02	0.007	0.004	0.00	24.19	24.19	0.100	220		13.5
TOTAL										8.83E+06 m3			

47-48 As for Impoundment #1

49 Runoff from undisturbed catchment, plus columns 12 and 16

50-57 As for Impoundment #1

58 Reduction in Upper Florence Creek flow, before flow augmentation

## CINOLA GOLD PROJECT

HIGH WEST AREA

MONTHLY WATER BALANCE FOR AVERAGE ANNUAL PRECIPITATION: YEAR 6

YEAR 6 (page 1 of 4)

FILE: WB6

DATE: 29-Jun-89

# S RESERVOIR CATCHMENT = 162 ha  
 CATCHMENT FOR DITCH IEI = 75 ha  
 RUNOFF FACTOR = 0.7

## WATER SUPPLY RESERVOIR

MONTH	PRECIP	POTENT	POND	DIRECT	RUNOFF	POND	SEEPAGE	SEEP TO	WATER	DECANT	FLOW TO	EXC/	WATER	WATER	RUNOFF IN	
	mm	mm	ha	mm	mm	ha	mm	mm	mm	mm	mm	m3/d	M m3	m	1000 m3/d	
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	
JAN	216	13	15.48	1.08	7.15	0.06	0.000	0.005	0.20	0.00	7.95	0.00	1.660	310	3.66	
FEB	216	16	15.48	1.19	7.91	0.09	0.000	0.005	0.20	0.00	8.81	0.00	1.660	310	4.05	
MAR	144	26	15.48	0.72	4.76	0.13	0.000	0.005	0.20	0.00	5.15	0.00	1.660	310	2.44	
APR	171	40	15.48	0.88	5.85	0.21	0.000	0.005	0.20	0.00	8.22	0.00	1.660	310	2.99	
MAY	112	65	15.48	0.56	3.71	0.33	0.000	0.005	0.20	0.00	3.73	0.00	1.660	310	1.90	
JUN	34	87	15.48	0.43	2.87	0.45	0.000	0.005	0.20	0.00	2.65	1.00	1.660	310	1.47	
JUL	80	104	15.48	0.40	2.65	0.52	0.000	0.005	0.20	0.00	2.32	0.00	1.660	310	1.35	
AUG	78	98	15.48	0.39	2.58	0.49	0.000	0.005	0.20	0.00	2.28	0.00	1.660	310	1.32	
SEP	166	71	15.48	0.86	5.68	0.37	0.000	0.005	0.20	0.00	5.96	0.00	1.660	310	2.91	
OCT	297	44	15.48	1.48	9.83	0.22	0.000	0.005	0.20	0.00	10.88	0.00	1.660	310	5.03	
NOV	250	21	15.48	1.34	8.89	0.11	0.000	0.005	0.20	0.00	9.92	0.00	1.660	310	4.55	
DEC	250	12	15.48	1.30	9.60	0.05	0.000	0.005	0.20	0.00	9.54	0.00	1.660	310	4.40	
MEAN	173	50	15.48	0.88	5.86	0.25	0.000	0.005	0.20	0.00	6.13	0.00	1.660	310	3.00	
TOTAL	2084	593										2.29E+06 m3				1.09E+06

## NOTES RE COLUMNS:

2 From Stage II Report, Vol III

3 From Stage II Report, Vol III

4 From curve of area vs. elevation

5 From columns 2 and 4

6 From columns 2, 4, catchment, and runoff factor

7 From columns 3 and 4

8 Set equal to zero

9 From seepage calculations

10 Mill make-up plus mill and mine domestic supply

11 Decant to Imp. #1 to maintain min. water vol, if necessary

12 Flow to Florence Creek; equal to excess (column 13) when reservoir full, controlled at other times

13 Net result of columns 5 to 12

14 Water volume in storage

15 From curve of capacity vs. elevation

16 From column 2, catchment, and runoff factor

IMPOUNDMENT #1 CATCHMENT = 44 ha

## IMPOUNDMENT NUMBER 1

MONTH	POND AREA ha	DIRECT PRECIP	LOCAL RUNOFF	POND EVAP	SEEPAGE IN 1000 m3/d	SEEP TO DECANT IMP #2	DECANT TO IMP #2 SET POND	EXC/DEF	FROM WSR	WATER IN POND	TOT TAILS+ WASTE ROCK	SOLIDS ELEV	WATER ELEV	
17	18	19	20	21	22	23	24	25	26	27	28	29	30	
JAN	42.0	2.93	0.10	0.18	0.075	0.024	0.00	3.33	-0.43	0.00	0.551	8.146	306	307
FEB	42.0	2.93	0.11	0.24	0.075	0.024	0.00	3.33	-0.48	0.00	0.535	8.146	306	307
MAR	42.0	1.95	0.07	0.35	0.075	0.024	0.00	2.15	-0.43	0.00	0.521	8.146	306	307
APR	42.0	2.32	0.08	0.56	0.075	0.023	0.00	2.34	-0.45	0.00	0.508	8.146	306	307
MAY	42.0	1.52	0.05	0.89	0.075	0.023	0.00	1.16	-0.43	0.00	0.494	8.146	306	307
JUN	42.0	1.14	0.04	1.22	0.075	0.023	0.00	0.46	-0.45	0.00	0.481	8.146	306	307
JUL	42.0	1.08	0.04	1.41	0.075	0.022	0.00	0.20	-0.43	0.00	0.467	8.146	306	307
AUG	42.0	1.06	0.04	1.33	0.075	0.022	0.00	0.25	-0.43	0.00	0.454	8.146	306	307
SEP	42.0	2.25	0.08	0.99	0.075	0.022	0.00	1.83	-0.45	0.00	0.440	8.146	306	307
OCT	42.0	4.02	0.13	0.60	0.075	0.022	0.00	4.05	-0.43	0.00	0.427	8.146	306	307
NOV	42.0	3.52	0.12	0.29	0.075	0.021	0.00	3.85	-0.43	0.00	0.413	8.146	306	307
DEC	42.0	3.52	0.00	0.16	0.075	0.021	0.00	3.85	-0.43	0.00	0.400	8.146	306	307
MEAN	42.0	2.35	0.07	0.69	0.075	0.023	0.00	2.23	-0.44	0.00	0.474	8.146	306	307
TOTAL									$-1.61E+05 \text{ m}^3$					

17 From curve of area vs. elevation

30 From curve of capacity vs. elevation

18 From columns 2 and 17

19 From columns 2, 17, catchment, and runoff factor

20 From columns 3 and 17

21-22 From seepage calculations

23 Decant of pond water to Imp #2

24 Decant to reduce water volume to nominal 400 000 m<sup>3</sup>

25 Net result of columns 18 to 24

26 Decant from water supply res., if necessary

27 From columns 25 and 26; 100 000 m<sup>3</sup> minimum

28-29 From Year 4

PULP DENSITY =	38 t	DRY DENSITY OF PLACED TAILINGS =	1.20 t/m <sup>3</sup>
TAILINGS MOISTURE CONTENT =	45 %	BULK DENSITY OF WASTE ROCK =	2.20 t/m <sup>3</sup>

IMPOUNDMENT #2 CATCHMENT =	50 ha	AREA OF LOW GRADE ORE STOCKPILE =	2.0 ha
TAILINGS DEPOSITION RATE =	6000 t/day	VOL OF TAILS PRODUCED IN YEAR =	1.83 M m <sup>3</sup>
WASTE ROCK DEPOSITION RATE =	2500 t/day	VOL OF WASTE ROCK IN YEAR =	0.41 M m <sup>3</sup>
MILL EFFLUENT RECYCLE RATIO=	84 %	TOTAL VOL OF SOLIDS IN YEAR =	2.24 M m <sup>3</sup>

**IMPOUNDMENT NUMBER 2  
(ACTIVE)**

MONTH	POND AREA ha	DIRECT PRECIP ha	LOCAL RUNOFF	MILL RUNOFF	POND EVAP	SEEPAGE IN 1000 m <sup>3</sup> /d	SEEPAGE OUT	FROM MILL	RETURN TO MILL	RET IN PORES	EXC/ DEF	FROM IMP #1	WATER IN POND	TOT TAILS+ WASTE ROCK	SOLIDS	WATER ELEV	
											31	32	33	34	35	36	37
JAN	21.8	1.52	1.38	0.29	0.09	0.077	0.015	9.71	9.28	2.70	0.89	0.00	0.458	2.240	258	261	
FEB	21.8	1.68	1.53	0.32	0.12	0.077	0.015	9.71	9.28	2.70	1.19	0.00	0.485	2.430	259	261	
MAR	22.5	1.05	0.89	0.20	0.19	0.077	0.016	9.71	9.28	2.70	-0.27	0.00	0.510	2.792	261	263	
APR	23.3	1.33	1.07	0.24	0.31	0.076	0.016	9.71	9.28	2.70	0.11	0.00	0.518	2.976	262	264	
MAY	24.0	0.87	0.66	0.15	0.51	0.076	0.017	9.71	9.28	2.70	-1.05	0.00	0.481	3.166	262	264	
JUN	24.0	0.67	0.51	0.12	0.70	0.076	0.017	9.71	9.28	2.70	-1.61	0.00	0.432	3.350	263	265	
JUL	24.8	0.64	0.46	0.11	0.83	0.075	0.019	9.71	9.28	2.70	-1.85	0.00	0.375	3.541	264	265	
AUG	24.8	0.62	0.44	0.11	0.78	0.075	0.018	9.71	9.28	2.70	-1.83	0.00	0.319	3.731	265	266	
SEP	25.5	1.41	0.95	0.23	0.60	0.075	0.018	9.71	9.28	2.70	-0.23	0.00	0.312	3.915	265	267	
OCT	25.3	2.51	1.59	0.40	0.37	0.075	0.019	9.71	9.28	2.70	1.92	0.00	0.371	4.105	266	268	
NOV	27.0	2.34	1.40	0.36	0.19	0.074	0.020	9.71	9.28	2.70	1.69	0.00	0.422	4.289	267	269	
DEC	27.3	2.03	1.31	0.35	0.11	0.074	0.020	9.71	9.28	2.70	1.66	0.00	0.473	4.480	269	270	
MEAN	24.5	1.41	1.01	0.24	0.40	0.076	0.017	9.71	9.28	2.70	0.04	0.00	0.434	3.453	264	265	
TOTAL													1.5E+04 m <sup>3</sup>				

31 From curve of area vs. elevation

32 From columns 2 and 31

33 From columns 2, 31, catchment, and runoff factor

34 Mill site and low grade ore stockpile runoff, plus other wastes

35 From columns 3 and 31

36-37 From seepage calculations

38 Mill effluent

39 Mill effluent recycle (as a % of total mill inflow)

40 From moisture content and deposition rates

41 Net result of columns 32 to 40

42 From columns 41 and 43

43 From column 41 and 42; 100 000 m<sup>3</sup> minimum

44 From deposition rates and densities

45 From curve of capacity vs. elevation

46 From curve of capacity vs. elevation

IMPOUNDMENT #3 CATCHMENT = 376 ha

## SETTLING POND (IMPOUNDMENT NUMBER 3)

MONTH	POND AREA ha	DIRECT PRECIP?	RUNOFF 48	POND EVAP	SEEP FR IMP #2	SEEPAGE OUT	DECANT FR IMP #1	EXC/ DEF	FLOW TO FLO CK	WATER IN POND m m3	WATER ELEV m	REDUCTION IN FLOW %
-----> 1000 m3/d ----->												
47	48	49	50	51	52	53	54	55	56	57	58	
JAN	1.4	0.10	29.66	0.01	0.011	0.004	3.33	33.31	33.31	0.100	220	3.3
FEB	1.4	0.11	33.09	0.01	0.011	0.004	3.33	36.52	36.52	0.100	220	4.1
MAR	1.4	0.07	19.77	0.01	0.011	0.004	2.15	21.98	21.98	0.100	220	4.2
APR	1.4	0.08	24.25	0.02	0.011	0.004	2.34	26.56	26.56	0.100	220	5.1
MAY	1.4	0.05	15.10	0.03	0.012	0.004	1.16	16.29	16.29	0.100	220	3.1
JUN	1.4	0.04	11.46	0.04	0.012	0.004	0.46	11.93	11.93	0.100	220	12.4
JUL	1.4	0.04	10.44	0.05	0.012	0.004	0.20	10.64	10.64	0.100	220	14.8
AUG	1.4	0.04	10.19	0.04	0.012	0.004	0.25	10.44	10.44	0.100	220	14.3
SEP	1.4	0.08	23.37	0.03	0.013	0.004	1.83	25.26	25.26	0.100	220	7.1
OCT	1.4	0.13	41.04	0.02	0.013	0.004	4.05	45.21	45.21	0.100	220	4.4
NOV	1.4	0.12	37.19	0.01	0.014	0.004	3.85	41.17	41.17	0.100	220	3.8
DEC	1.4	0.12	36.03	0.01	0.014	0.004	3.85	40.00	40.00	0.100	220	3.5
MEAN	1.4	0.08	24.25	0.02	0.012	0.004	2.23	26.54	26.54	0.100	220	7.1
TOTAL									9.69E+06	m3		

46-47 As for Impoundment #1

48 Runoff from undisturbed catchment, plus columns 12 and 16

49-56 As for Impoundment #1

57 Reduction in Upper Florence Creek flow, before flow augmentation

## CINOLA GOLD PROJECT

HIGH WEST AREA

MONTHLY WATER BALANCE FOR AVERAGE ANNUAL PRECIPITATION: YEAR 7

YEAR 7 (page 1 of 4)

FILE: WB7

DATE: 29-Jun-89

W S RESERVOIR CATCHMENT = 162 ha  
 CATCHMENT FOR DITCH I&I = 75 ha  
 RUNOFF FACTOR = 0.7

## WATER SUPPLY RESERVOIR

MONTH	PRECIP	POTENT	POND	DIRECT	RUNOFF	POND	SEEPAGE	SEEP TO	WATER	DECANT	FLOW TO	EXC/	WATER	WATER	RUNOFF IN	
	mm	mm	ha	mm	mm	ha	mm	mm	mm	mm	mm	m	m	m	m	1000 m3/d
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	
																-1000 m3/d-
JAN	216	13	15.48	1.08	7.15	0.06	0.000	0.005	0.20	0.00	7.96	0.00	1.660	310	3.66	
FEB	216	16	15.48	1.19	7.31	0.09	0.000	0.005	0.20	0.00	8.81	0.00	1.660	310	4.05	
MAR	144	26	15.48	0.72	4.76	0.13	0.000	0.005	0.20	0.00	5.15	0.00	1.660	310	2.44	
APR	171	40	15.48	0.66	5.85	0.21	0.000	0.005	0.20	0.00	6.32	0.00	1.660	310	2.99	
MAY	112	66	15.48	1.33	3.71	0.33	0.000	0.005	0.20	0.00	3.73	0.00	1.660	310	1.90	
JUN	64	87	15.48	0.43	2.87	0.45	0.000	0.005	0.20	0.00	2.35	0.00	1.660	310	1.47	
JUL	80	104	15.48	0.40	2.65	0.52	0.000	0.005	0.20	0.23	2.09	0.00	1.660	310	1.35	
AUG	78	98	15.48	0.39	2.58	0.49	0.000	0.005	0.20	0.16	2.10	0.00	1.660	310	1.32	
SEP	166	71	15.48	0.86	5.68	0.37	0.000	0.005	0.20	0.00	5.96	0.00	1.660	310	2.91	
OCT	297	44	15.48	1.48	9.33	0.22	0.000	0.005	0.20	0.00	10.38	0.00	1.660	310	5.08	
NOV	260	21	15.48	1.34	8.89	0.11	0.000	0.005	0.20	0.00	9.92	0.00	1.660	310	4.55	
DEC	250	12	15.48	1.30	8.60	0.06	0.000	0.005	0.20	0.00	9.54	0.00	1.660	310	4.40	
MEAN	173	50	15.48	0.88	5.86	0.25	0.000	0.005	0.20	0.04	6.25	0.00	1.660	310	3.00	
TOTAL	2084	598											2.28E+06 m3			1.09E+06

## NOTES RE COLUMNS:

- 2 From Stage II Report, Vol III
- 3 From Stage II Report, Vol III
- 4 From curve of area vs. elevation
- 5 From columns 2 and 4
- 6 From columns 2, 4, catchment, and runoff factor
- 7 From columns 3 and 4
- 8 Set equal to zero
- 9 From seepage calculations
- 10 Mill make-up plus mill and mine domestic supply
- 11 Decant to Imp. #1 to maintain min. water vol. if necessary

- 12 Flow to Florence Creek; equal to excess (column 13) when reservoir full, controlled at other times
- 13 Net result of columns 5 to 12
- 14 Water volume in storage
- 15 From curve of capacity vs. elevation
- 16 From column 2, catchment, and runoff factor

IMPOUNDMENT #1 CATCHMENT = 44 ha

## IMPOUNDMENT NUMBER 1

MONTH	POND AREA ha	DIRECT		LOCAL		POND	SEEPAGE	SEEP IN	TO DECANT	TO SPILL	EXC/DEF	FROM WSR	WATER IN POND	TOT TAILS+ WASTE ROCK	SOLIDS ELEV	WATER ELEV
		PRECIP	RUNOFF	EVAP	IMP #2	IMP #2	SET POND	1000 m3/d					M m3	M m3	m	m
	17	18	19	20	21	22	23	24	25	26	27	28	29	30		
JAN	42.0	2.83	0.10	0.13	0.075	0.021	0.00	2.80	0.00	0.00	0.400	0.00	8.146	306	307	
FEB	42.0	2.83	0.11	0.24	0.075	0.021	0.00	2.35	0.00	0.00	0.400	0.00	8.146	306	307	
MAR	42.0	1.95	0.07	0.35	0.075	0.020	0.00	1.72	0.00	0.00	0.400	0.00	8.146	306	307	
APR	42.0	2.32	0.08	0.56	0.075	0.020	0.00	1.89	0.00	0.00	0.400	0.00	8.146	306	307	
MAY	42.0	1.52	0.05	0.99	0.075	0.020	0.00	0.73	0.00	0.00	0.400	0.00	8.146	306	307	
JUN	42.0	1.14	0.04	1.22	0.075	0.019	0.00	0.01	0.00	0.00	0.400	0.00	8.146	306	307	
JUL	42.0	1.08	0.04	1.41	0.075	0.019	0.00	0.00	-0.23	0.23	0.400	0.00	8.146	306	307	
AUG	42.0	1.06	0.04	1.33	0.075	0.019	0.00	0.00	-0.18	0.18	0.400	0.00	8.146	306	307	
SEP	42.0	2.25	0.08	0.99	0.075	0.019	0.00	1.39	0.00	0.00	0.400	0.00	8.146	306	307	
OCT	42.0	4.02	0.13	0.50	0.075	0.019	0.00	3.62	0.00	0.00	0.400	0.00	8.146	306	307	
NOV	42.0	3.52	0.12	0.29	0.075	0.019	0.00	2.41	0.00	0.00	0.400	0.00	8.146	306	307	
DEC	42.0	3.52	0.00	0.16	0.075	0.018	0.00	3.42	0.00	0.00	0.400	0.00	8.146	306	307	
MEAN	42.0	2.85	0.07	0.63	0.075	0.020	0.00	1.82	-0.04	0.04	0.400	0.00	8.146	306	307	
TOTAL									-1.28E+04 m3							

17 From curve of area vs. elevation

30 From curve of capacity vs. elevation

18 From columns 2 and 17

19 From columns 2, 17, catchment, and runoff factor

20 From columns 3 and 17

21-22 From seepage calculations

23 Decant of pond water to Imp #2

24 Spillway flow

25 Net result of columns 18 to 24

26 Decant from water supply res., if necessary

27 From column 26; 400 000 m3 maximum

28-29 From Year 4

PULP DENSITY = 38 t/m<sup>3</sup> DRY DENSITY OF PLACED TAILINGS = 1.20 t/m<sup>3</sup>  
 TAILINGS MOISTURE CONTENT = 45 % BULK DENSITY OF WASTE ROCK = 2.20 t/m<sup>3</sup>

IMPOUNDMENT #2 CATCHMENT = 50 ha AREA OF LOW GRADE ORE STOCKPILE = 0.0 ha  
 TAILINGS DEPOSITION RATE = 6000 t/day VOL OF TAILS PRODUCED IN YEAR = 1.83 M m<sup>3</sup>  
 WASTE ROCK DEPOSITION RATE = 3300 t/day VOL OF WASTE ROCK IN YEAR = 0.55 M m<sup>3</sup>  
 MILL EFFLUENT RECYCLE RATIO= 84 % TOTAL VOL OF SOLIDS IN YEAR = 2.37 M m<sup>3</sup>

IMPOUNDMENT NUMBER 2  
 (ACTIVE)

MONTH	POND AREA ha	DIRECT PRECIP <--	LOCAL RUNOFF	MILL RUNOFF	POND EVAP	SEEPAGE IN 1000 m <sup>3</sup> /d	SEEPAGE OUT	FROM MILL TO MILL	RETURN TO MILL	RET IN PORES	EXC/ DEF	FROM IMP #1	WATER IN POND M m <sup>3</sup>	TOT TAILS+ WASTE ROCK M m <sup>3</sup>	SOLIDS ELEV	WATER ELEV	
											31	32	33	34	35	36	37
JAN	28.5	1.99	1.05	0.20	0.12	0.074	0.021	9.71	9.28	2.70	0.89	0.00	0.501	4.681	269	271	
FEB	28.5	2.20	1.15	0.22	0.16	0.074	0.021	9.71	9.28	2.70	1.19	0.00	0.534	4.863	269	271	
MAR	29.3	1.36	0.67	0.13	0.25	0.073	0.022	9.71	9.28	2.70	-0.31	0.00	0.524	5.065	270	271	
APR	29.3	1.57	0.33	0.16	0.39	0.073	0.022	9.71	9.28	2.70	0.04	0.00	0.525	5.260	270	272	
MAY	30.0	1.08	0.51	0.10	0.64	0.073	0.022	9.71	9.28	2.70	-1.17	0.00	0.489	5.461	271	273	
JUN	30.8	0.86	0.23	0.08	0.39	0.072	0.023	9.71	9.28	2.70	-1.80	0.00	0.435	5.656	272	273	
JUL	30.8	0.73	0.35	0.07	1.01	0.072	0.023	9.71	9.28	2.70	-2.04	0.00	0.372	5.858	272	273	
AUG	30.8	0.77	0.34	0.07	0.97	0.072	0.023	9.71	9.28	2.70	-2.02	0.00	0.309	6.059	273	274	
SEP	31.5	1.74	0.72	0.15	0.75	0.072	0.024	9.71	9.28	2.70	-0.36	0.00	0.299	6.254	273	274	
OCT	31.5	3.02	1.24	0.27	0.45	0.072	0.024	9.71	9.28	2.70	1.35	0.00	0.356	6.455	274	275	
NOV	32.3	2.80	1.08	0.24	0.23	0.072	0.024	9.71	9.28	2.70	1.66	0.00	0.406	6.651	275	276	
DEC	33.0	2.77	1.00	0.23	0.13	0.071	0.025	9.71	9.28	2.70	1.54	0.00	0.457	6.852	275	276	
MEAN	30.5	1.75	0.77	0.16	0.50	0.073	0.023	9.71	9.28	2.70	-0.04	0.00	0.433	5.755	272	273	
TOTAL													-1.62E+04 m <sup>3</sup>				

31 From curve of area vs. elevation

42 From columns 41 and 43

32 From columns 2 and 31

43 From column 41 and 42; 100 000 m<sup>3</sup> minimum

33 From columns 2, 31, catchment, and runoff factor

44 From deposition rates and densities

34 Mill site and low grade ore stockpile runoff, plus other wastes

45 From curve of capacity vs. elevation

35 From columns 3 and 31

46 From curve of capacity vs. elevation

36-37 From seepage calculations

38 Mill effluent

39 Mill effluent recycle (as a % of total mill inflow)

40 From moisture content and deposition rates

41 Net result of columns 32 to 40

IMPOUNDMENT #3 CATCHMENT = 378 ha

## SETTLING POND (IMPOUNDMENT NUMBER 3)

MONTH	POND AREA ha	DIRECT PRECIP	RUNOFF 1000 m3/d	POND EVAP	SEEPAGE IMP #2	SPILL FR IMP #1	EXC/DEF	FLOW TO FLOC	WATER IN POND m	WATER ELEV m	REDUCTION IN FLOW %	
JAN	1.4	0.10	29.98	0.01	0.015	0.004	2.90	32.99	32.99	0.100	220	4.1
FEB	1.4	0.11	33.20	0.01	0.015	0.004	2.85	36.16	36.16	0.100	220	4.9
MAR	1.4	0.07	19.82	0.01	0.015	0.004	1.72	21.62	21.62	0.100	220	5.5
APR	1.4	0.08	24.34	0.02	0.015	0.004	1.89	25.30	25.30	0.100	220	6.2
MAY	1.4	0.05	15.15	0.03	0.016	0.004	0.73	15.81	15.81	0.100	220	9.3
JUN	1.4	0.04	11.50	0.04	0.016	0.004	0.01	11.53	11.53	0.100	220	14.9
JUL	1.4	0.04	10.25	0.05	0.016	0.004	0.00	10.25	10.25	0.100	220	17.4
AUG	1.4	0.04	10.05	0.04	0.016	0.004	0.00	10.05	10.05	0.100	220	17.0
SEP	1.4	0.08	23.45	0.03	0.017	0.004	1.39	24.90	24.90	0.100	220	8.2
OCT	1.4	0.13	41.17	0.02	0.017	0.004	3.62	44.92	44.92	0.100	220	4.9
NOV	1.4	0.12	37.31	0.01	0.017	0.004	3.41	40.85	40.85	0.100	220	4.5
DEC	1.4	0.12	36.15	0.01	0.018	0.004	3.42	39.69	39.69	0.100	220	4.1
MEAN	1.4	0.08	24.30	0.02	0.016	0.004	1.32	26.19	26.19	0.100	220	9.5
TOTAL										9,562+06.43		

46-47 As for Impoundment #1

48 Runoff from undisturbed catchment, plus columns 12 and 16

49-55 As for Impoundment #1

57 Reduction in Upper Florence Creek flow, before flow augmentation

## CINOLA GOLD PROJECT

HIGH WEST AREA

MONTHLY WATER BALANCE FOR AVERAGE ANNUAL PRECIPITATION: YEAR 8

YEAR 8 (page 1 of 4)

FILE: W88

DATE: 29-Jun-89

W S RESERVOIR CATCHMENT = 162 ha  
 CATCHMENT FOR DITCH IE1 = 75 ha  
 RUNOFF FACTOR = 0.7

## WATER SUPPLY RESERVOIR

MONTH	PRECIP	POTENT	POND	DIRECT	RUNOFF	POND	SEEPAGE	WATER	DECANT	FLOW TO	EXC/	WATER	WATER	RUNOFF IN		
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	
JAN	216	13	15.48	1.08	7.15	0.06	0.000	0.005	0.20	0.00	7.95	0.00	1.660	310	3.86	
FEB	216	16	15.48	1.19	7.31	0.09	0.000	0.005	0.20	0.00	8.31	0.00	1.660	310	4.05	
MAR	144	26	15.48	0.72	4.76	0.13	0.000	0.005	0.20	0.00	5.15	0.00	1.660	310	2.44	
APR	171	40	15.48	0.88	5.85	0.21	0.000	0.005	0.20	0.00	5.82	0.00	1.660	310	2.99	
MAY	112	65	15.48	0.56	3.71	0.33	0.000	0.005	0.20	0.00	3.73	0.00	1.660	310	1.90	
JUN	84	37	15.48	0.43	2.87	0.45	0.000	0.005	0.20	0.00	2.85	0.00	1.660	310	1.47	
JUL	80	104	15.48	0.40	2.65	0.52	0.000	0.005	0.20	0.23	2.09	0.00	1.660	310	1.85	
AUG	78	98	15.48	0.39	2.58	0.49	0.000	0.005	0.20	0.18	2.10	0.00	1.660	310	1.82	
SEP	156	71	15.48	0.86	5.68	0.37	0.000	0.005	0.20	0.00	5.96	0.00	1.660	310	2.91	
OCT	297	44	15.48	1.48	3.83	0.22	0.000	0.005	0.20	0.00	10.88	0.00	1.660	310	5.03	
NOV	260	21	15.48	1.34	8.89	0.11	0.000	0.005	0.20	0.00	9.92	0.00	1.660	310	4.55	
DEC	260	12	15.48	1.30	8.60	0.06	0.000	0.005	0.20	0.00	9.54	0.00	1.660	310	4.40	
MEAN	173	50	15.48	0.88	5.86	0.25	0.000	0.005	0.20	0.03	6.25	0.00	1.660	310	3.00	
TOTAL	2084	593										2.28E+06 m3				1.09E+06

## NOTES RE COLUMNS:

2 From Stage II Report, Vol III

3 From Stage II Report, Vol III

4 From curve of area vs. elevation

5 From columns 2 and 4

6 From columns 2, 4, catchment, and runoff factor

7 From columns 3 and 4

8 Set equal to zero

9 From seepage calculations

10 Mill intake plus mill and mine domestic supply

11 Decant to Imp. #1 to maintain min. water vol, if necessary

12 Flow to Florence Creek; equal to excess (column 13) when reservoir full, controlled at other times

13 Net result of columns 5 to 12

14 Water volume in storage

15 From curve of capacity vs. elevation

16 From column 2, catchment, and runoff factor

IMPOUNDMENT #1 CATCHMENT = 44 ha

## IMPOUNDMENT NUMBER 1

MONTH AREA ha	POND	DIRECT	LOCAL	POND	SEEPAGE	SEEP IN	DECANT TO IMP #2	SPILL TO SET POND	EXC/DEF	FROM WSR	WATER IN POND	TOT TAILS+ WASTE ROCK	SOLIDS ELEV	WATER ELEV
	PRECIP	RUNOFF	EVAP		1000 m3/d				-->	M m3	M m3	m	m	m
	17	18	19	20	21	22	23	24	25	26	27	28	29	30
JAN	42.0	2.93	0.10	0.18	0.075	0.018	0.00	2.90	0.00	0.00	0.400	8.146	306	307
FEB	42.0	2.93	0.11	0.24	0.075	0.018	0.00	2.85	0.00	0.00	0.400	8.146	306	307
MAR	42.0	1.95	0.07	0.35	0.075	0.018	0.00	1.72	0.00	0.00	0.400	8.146	306	307
APR	42.0	2.92	0.08	0.58	0.075	0.018	0.00	1.89	0.00	0.00	0.400	8.146	306	307
MAY	42.0	1.51	0.05	0.89	0.075	0.017	0.00	0.73	0.00	0.00	0.400	8.146	306	307
JUN	42.0	1.14	0.04	1.22	0.075	0.017	0.00	0.02	0.00	0.00	0.400	8.146	306	307
JUL	42.0	1.08	0.04	1.41	0.075	0.017	0.00	0.00	-0.23	0.23	0.400	8.146	306	307
AUG	42.0	1.06	0.04	1.33	0.075	0.017	0.00	0.00	-0.18	0.18	0.400	8.146	306	307
SEP	42.0	2.25	0.08	0.99	0.075	0.017	0.00	1.39	0.00	0.00	0.400	8.146	306	307
OCT	42.0	4.02	0.13	0.50	0.075	0.016	0.00	3.62	0.00	0.00	0.400	8.146	305	307
NOV	42.0	3.52	0.12	0.29	0.075	0.016	0.00	3.41	0.00	0.00	0.400	8.146	306	307
DEC	42.0	3.52	0.00	0.16	0.075	0.016	0.00	3.42	0.00	0.00	0.400	8.146	306	307
MEAN	42.0	2.35	0.07	0.69	0.075	0.017	0.00	1.82	-0.03	0.03	0.400	8.146	306	307
TOTAL									-1.27E+04 m3					

17 From curve of area vs. elevation

30 From curve of capacity vs. elevation

18 From columns 2 and 17

19 From columns 2, 17, catchment, and runoff factor

20 From columns 3 and 17

21-22 From seepage calculations

23 Decant of pond water to imp #2

24 Spillway flow

25 Net result of columns 18 to 24

26 Decant from water supply res., if necessary

27 From column 26; 400 000 m3 maximum

28-29 From Year 4

PULP DENSITY = 38.1 DRY DENSITY OF PLACED TAILINGS = 1.20 t/m<sup>3</sup>  
TAILINGS MOISTURE CONTENT = 45.1 BULK DENSITY OF WASTE ROCK = 2.30 t/m<sup>3</sup>

IMPOUNDMENT #2 CATCHMENT =	50 ha	AREA OF LOW GRADE ORE STOCKPILE =	0.0 ha
TAILINGS DEPOSITION RATE =	6000 t/day	VOL OF TAILS PRODUCED IN YEAR =	1.83 M m3
WASTE ROCK DEPOSITION RATE =	2500 t/day	VOL OF WASTE ROCK IN YEAR =	0.41 M m3
MILL EFFLUENT RECYCLE RATIO=	94 %	TOTAL VOL OF SOLIDS IN YEAR =	2.24 M m3

IMPOUNDMENT NUMBER 2  
(ACTIVE)

MONTH	POND	DIRECT	LOCAL	MILL	POND	SEEPAGE	SEEPAGE	FROM	RETURN	RET IN	EXC/	FROM	WATER	TOT TAILS+	SOLIDS	WATER
	AREA	PRECIP	RUNOFF	RUNOFF	EVAP.	IN	OUT	MILL	TO MILL	PORES	DEF	IMP #1	IN POND	WASTE	ROCK	ELEV
	ha	mm	mm	mm	mm	mm	mm	mm	mm	mm	%	MM	m3	m3	m3	m3
1000 m3/d																
	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46
JAN	33.0	2.30	0.83	0.20	0.14	0.071	0.025	3.71	9.28	2.70	0.96	0.00	0.486	6.852	275	276
FEB	33.8	2.60	0.88	0.22	0.19	0.071	0.026	3.71	9.28	2.70	1.27	0.00	0.522	7.214	275	276
MAR	34.5	1.60	0.50	0.13	0.29	0.071	0.026	3.71	9.28	2.70	-0.28	0.00	0.513	7.404	277	278
APR	34.5	1.97	0.62	0.15	0.46	0.071	0.026	3.71	9.28	2.70	0.05	0.00	0.515	7.588	277	278
MAY	35.3	1.27	0.37	0.10	0.75	0.070	0.027	3.71	9.28	2.70	-1.24	0.00	0.477	7.779	278	279
JUN	35.3	0.93	0.22	0.09	1.02	0.070	0.027	3.71	9.28	2.70	-1.90	0.00	0.420	7.968	278	280
JUL	36.0	0.93	0.25	0.07	1.21	0.070	0.028	3.71	9.28	2.70	-2.19	0.00	0.352	8.153	279	290
AUG	36.0	0.31	0.15	0.07	1.14	0.070	0.028	3.71	9.28	2.70	-2.15	0.00	0.295	8.343	280	290
SEP	36.0	1.99	0.54	0.15	0.85	0.070	0.028	3.71	9.28	2.70	-0.40	0.00	0.273	8.527	280	281
OCT	36.8	0.53	0.89	0.27	0.52	0.069	0.028	3.71	9.28	2.70	1.92	0.00	0.383	8.713	281	281
NOV	36.8	0.19	0.80	0.24	0.26	0.069	0.028	3.71	9.28	2.70	1.74	0.00	0.385	8.892	281	282
DEC	37.3	0.15	0.73	0.23	0.15	0.069	0.028	3.71	9.28	2.70	1.74	0.00	0.439	9.082	281	283
MEAN	35.5	2.06	0.58	0.16	0.58	0.070	0.027	3.71	9.28	2.70	-0.05	0.00	0.416	9.065	279	280
TOTAL														-1.8E+04 m3		

### 31 From curve of area vs. elevation

32 From columns 2 and 3

33 From columns 2, 31, catchment, and runoff factor

34 Mill site and low grade ore stockpile runoff, plus other wastes

35 From columns 3 and 31

### 36-37 From seepage calculations

### 39 Mill effluent

39 Mill effluent recycle (as a % of total mill inflow)

#### 4.3. From moisture content and desorption rates

41 Net result of columns 32 to 40

42 From columns 41 and 43

43 From columns 41 and 42; 100 000 ml<sup>-3</sup> minimum

#### 44 From densoitation rates and densities

#### 45. From curve of capacity vs. elevation

#### 46. Area curves of capacity vs. elevation.

IMPOUNDMENT #3 CATCHMENT = 373 ha

## SETTLING POND (IMPOUNDMENT NUMBER 3)

MONTH	POND	DIRECT	RUNOFF	POND	SEEP FR	SEEPAGE	DECANT FR	EXC/	FLOW TO	WATER	WATER REDUCTION	
	AREA	PRECIP		EVAP	IMP #2	OUT	IMP #1	DEF	FLG CK	IN POND	ELEV	IN FLOW
	ha	<-----	1000 m3/d	----->						m m3	a	%
	47	48	49	50	51	52	53	54	55	56	57	58
JAN	1.4	0.10	29.99	0.01	0.019	0.004	2.90	22.99	22.99	0.100	220	4.1
FEB	1.4	0.11	33.20	0.01	0.018	0.004	2.85	33.16	33.16	0.100	220	4.9
MAR	1.4	0.07	19.83	0.01	0.019	0.004	1.72	21.62	21.62	0.100	220	5.5
APR	1.4	0.08	24.84	0.02	0.019	0.004	1.39	25.31	25.31	0.100	220	6.1
MAY	1.4	0.05	15.15	0.03	0.019	0.004	0.73	15.92	15.92	0.100	220	6.3
JUN	1.4	0.04	11.50	0.04	0.019	0.004	0.02	11.53	11.53	0.100	220	14.9
JUL	1.4	0.04	10.23	0.05	0.020	0.004	0.00	10.25	10.25	0.100	220	17.4
AUG	1.4	0.04	10.05	0.04	0.020	0.004	0.00	10.06	10.06	0.100	220	17.0
SEP	1.4	0.08	23.45	0.03	0.020	0.004	1.89	24.90	24.90	0.100	220	8.2
OCT	1.4	0.13	41.17	0.02	0.020	0.004	8.62	44.92	44.92	0.100	220	4.3
NOV	1.4	0.12	37.31	0.01	0.020	0.004	8.41	40.85	40.85	0.100	220	4.5
DEC	1.4	0.12	35.15	0.01	0.021	0.004	8.42	39.70	39.70	0.100	220	4.1
MEAN	1.4	0.08	24.30	0.02	0.019	0.004	1.82	29.19	26.19	0.100	220	9.5
TOTAL									9.565+06 m3			

46-47 As for Impoundment #1

48 Runoff from undisturbed catchment, plus columns 12 and 16

49-56 As for Impoundment #1

57 Reduction in Upper Florence Creek flow, before flow augmentation

## CINOLA GOLD PROJECT

HIGH WEST AREA

MONTHLY WATER BALANCE FOR AVERAGE ANNUAL PRECIPITATION: YEAR 9

YEAR 9 (page 1 of 5)

FILE: WB9

DATE: 29-Jun-89

W S RESERVOIR CATCHMENT = 162 ha  
 CATCHMENT FOR DITCH IEI = 75 ha  
 RUNOFF FACTOR = 0.7

## WATER SUPPLY RESERVOIR

MONTH	PRECIP	POTENT	POND	DIRECT	RUNOFF	POND	SEEPAGE	SEEP TO	WATER	DECANT	FLOW TO	EXC/	WATER	WATER	RUNOFF IN	
	mm	mm	ha	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	m	m	1000 m <sup>3</sup> /d
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	
JAN	216	13	15.48	1.03	7.15	0.06	0.000	0.005	0.20	0.00	7.95	0.00	1.660	310	3.66	
FEB	216	16	15.48	1.19	7.91	0.09	0.000	0.005	0.20	0.00	8.81	0.00	1.660	310	4.05	
MAR	144	26	15.48	0.72	4.76	0.13	0.000	0.005	0.20	0.00	5.15	0.00	1.660	310	2.44	
APR	171	40	15.48	0.88	5.85	0.21	0.000	0.005	0.20	0.00	6.32	0.00	1.660	310	2.99	
MAY	112	65	15.48	0.55	3.71	0.03	0.000	0.005	0.20	0.00	3.73	0.00	1.660	310	1.50	
JUN	94	87	15.48	0.43	2.87	0.45	0.000	0.005	0.20	0.00	2.65	0.00	1.660	310	1.47	
JUL	80	104	15.48	0.40	2.65	0.52	0.000	0.005	0.20	0.23	2.09	0.00	1.660	310	1.35	
AUG	78	98	15.48	0.39	2.58	0.49	0.000	0.005	0.20	0.18	2.10	0.00	1.660	310	1.32	
SEP	166	71	15.48	0.85	5.68	0.37	0.000	0.005	0.20	0.00	5.95	0.00	1.660	310	2.91	
OCT	297	44	15.48	1.43	9.83	0.22	0.000	0.005	0.20	0.00	10.88	0.00	1.660	310	5.03	
NOV	260	21	15.48	1.34	8.89	0.11	0.000	0.005	0.20	0.00	9.92	0.00	1.660	310	4.55	
DEC	260	12	15.48	1.30	8.60	0.06	0.000	0.005	0.20	0.00	9.64	0.00	1.660	310	4.40	
MEAN	173	50	15.48	0.88	5.96	0.25	0.000	0.005	0.20	0.03	6.25	0.00	1.660	310	3.00	
TOTAL	2084	598										2.285E-06 m <sup>3</sup>				1.09E-06 m <sup>3</sup>

## NOTES RE COLUMNS:

2 From Stage II Report, Vol III

3 From Stage II Report, Vol III

4 From curve of area vs. elevation

5 From columns 2 and 4

6 From columns 2, 4, catchment, and runoff factor

7 From columns 3 and 4

8 Set equal to zero

9 From seepage calculations

10 Mill make-up plus mill and mine domestic supply

11 Decant to Imp. #1 to maintain min. water vol, if necessary

12 Flow to Florence Creek; equal to excess (column 13) when reservoir full, controlled at other times

13 Net result of columns 5 to 12

14 Water volume in storage

15 From curve of capacity vs. elevation

16 From column 2, catchment, and runoff factor

IMPOUNDMENT #1 CATCHMENT = 44 ha

## IMPOUNDMENT NUMBER 1

MONTH	POND AREA ha	DIRECT PRECIP		LOCAL RUNOFF		SEEPAGE EVAP		SEEP TO IMP #1		DECANT TO IMP #2		SPILL TO SET POND		EXC/DEF FROM WSR	WATER IN POND M m3	TOT TAILS+ WASTE ROCK M m3	SOLIDS ELEV m
		17	18	19	20	21	22	23	24	25	26	27	28				
JAN	42.0	2.93	0.10	0.18	0.075	0.016	0.00	2.91	0.00	0.00	0.00	0.400	0.400	8.146	306		
FEB	42.0	2.93	0.11	0.24	0.075	0.016	0.00	2.85	0.00	0.00	0.400	0.400	8.146	306			
MAR	42.0	1.95	0.07	0.35	0.075	0.016	0.00	1.72	0.00	0.00	0.400	0.400	8.146	306			
APR	42.0	2.82	0.08	0.55	0.075	0.016	0.00	1.90	0.00	0.00	0.400	0.400	8.146	306			
MAY	42.0	1.52	0.05	0.89	0.075	0.016	0.00	0.72	0.00	0.00	0.400	0.400	8.146	306			
JUN	42.0	1.14	0.04	1.22	0.075	0.016	0.00	0.02	0.00	0.00	0.400	0.400	8.146	306			
JUL	42.0	1.08	0.04	1.41	0.075	0.016	0.00	0.00	-0.23	0.23	0.400	0.400	8.146	306			
AUG	42.0	1.06	0.04	1.33	0.075	0.016	0.00	0.00	-0.18	0.18	0.400	0.400	8.146	306			
SEP	42.0	2.25	0.08	0.99	0.075	0.016	0.00	1.39	0.00	0.00	0.400	0.400	8.146	306			
OCT	42.0	4.02	0.13	0.60	0.075	0.016	0.00	3.62	0.00	0.00	0.400	0.400	8.146	306			
NOV	42.0	3.52	0.12	0.29	0.075	0.016	0.00	3.41	0.00	0.00	0.400	0.400	8.146	306			
DEC	42.0	3.52	0.00	0.16	0.075	0.016	0.00	3.42	0.00	0.00	0.400	0.400	8.146	306			
MEAN	42.0	2.85	0.07	0.69	0.075	0.016	0.00	1.82	-0.03	0.03	0.400	0.400	8.146	306			
TOTAL										-1.26E+04							

17 From curve of area vs. elevation

30 From curve of capacity vs. elevation.

18 From columns 2 and 17

19 From columns 2, 17, catchment, and runoff factor

20 From columns 3 and 17

21-22 From seepage calculations

23 Decant of pond water to Imp #2

24 Spillway flow

25 Net result of columns 18 to 24

26 Decant from water supply res., if necessary

27 From column 26; 400 000 m3 maximum

28-29 From Year 4

IMPOUNDMENT #2 CATCHMENT = 50 ha

## IMPOUNDMENT NUMBER 2

MONTH	POND	DIRECT	LOCAL	POND	SEEPAGE	SEEPAGE	DECANT TO	DECANT TO	EXC/	FROM	WATER	TOT TAILLS+	SOLIDS
	AREA ha <-----	PRECIP	RUNOFF	EVAP	IN	CUT	IMP #3	SET POND	DEF	IMPR#1	IN POND	WASTE ROCK	ELEV
	31	32	33	34	35	36	37	38	39	40	41	42	43
JAN	38.4	2.68	0.57	0.16	0.069	0.023	17.28	0.00	-14.16	0.00	0.000	9.092	281
FEB	36.3	2.84	0.71	0.00	0.069	0.025	0.00	0.00	3.60	0.00	0.101	9.092	281
MAR	37.6	1.73	0.40	0.82	0.069	0.025	0.00	0.00	1.88	0.00	0.159	9.092	281
APR	37.6	2.14	0.49	0.50	0.069	0.024	0.00	0.00	2.13	0.00	0.224	9.092	281
MAY	37.8	1.03	0.31	0.30	0.069	0.024	0.00	0.00	0.32	0.00	0.253	9.092	281
JUN	37.6	1.05	0.14	1.09	0.069	0.024	0.00	0.00	0.25	0.00	0.250	9.092	281
JUL	37.6	0.37	0.22	1.26	0.069	0.023	0.00	0.00	-0.02	0.00	0.260	9.092	281
AUG	37.6	0.95	0.22	1.19	0.069	0.023	0.00	0.00	0.02	0.00	0.260	9.092	281
SEP	37.6	2.08	0.48	0.89	0.069	0.023	0.00	0.00	1.72	0.00	0.312	9.092	281
OCT	37.6	3.60	0.83	0.58	0.069	0.023	0.00	0.00	3.95	0.00	0.104	9.092	281
NOV	39.4	3.23	0.70	0.27	0.069	0.022	0.00	0.00	3.81	0.00	0.548	9.092	281
DEC	39.4	3.22	0.68	0.15	0.069	0.022	0.00	0.00	3.80	0.00	0.566	9.092	281
MEAN	37.7	2.15	0.49	0.60	0.069	0.024	1.47	0.00	0.62	0.00	0.291	9.092	281
TOTAL									2.27E+05	m3			

31 From curve of area vs. elevation

44 From curve of capacity vs. elevation

32 From columns 2 and 31

33 From columns 2, 31, catchment, and runoff factor

34 From columns 3 and 31

35-36 From seepage calculations

37 Decant of pond water to Imp #3

38 Set to zero for Year 9

39 Net result of columns 32 to 38

40 Decant from Imp#1, if necessary

41 From column 40

42-43 From Year 8

PULP DENSITY =	38 t	DRY DENSITY OF PLACED TAILINGS =	1.20 t/m <sup>3</sup>
TAILINGS MOISTURE CONTENT =	45 %	BULK DENSITY OF WASTE ROCK =	2.20 t/m <sup>3</sup>

IMPOUNDMENT #3 CATCHMENT =	45 ha	AREA OF LOW GRADE ORE STOCKPILE =	0.0 ha
TAILINGS DEPOSITION RATE =	5000 t/day	VOL OF TAILS PRODUCED IN YEAR =	1.93 M m <sup>3</sup>
WASTE ROCK DEPOSITION RATE =	2500 t/day	VOL OF WASTE ROCK IN YEAR =	0.41 M m <sup>3</sup>
MILL EFFLUENT RECYCLE RATIO =	84 %	TOTAL VOL OF SOLIDS IN YEAR =	2.24 M m <sup>3</sup>

**IMPOUNDMENT NUMBER 3  
(ACTIVE)**

MONTH	POND AREA ha	DIRECT PRECIP		LOCAL RUNOFF		MILL RUNOFF		SEEPAGE IN		SEEPAGE OUT		FROM MILL TO MILL		RETURN PORES		EXC/DEF IMP #2		FROM WATER IN POND		TOT TAILS+ WASTE ROCK		GELSOLIDS ELEV		WATER ELEV	
		45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	55	56	57	58	59	60	55	60
JAN	1.4	0.10	2.13	0.20	0.01	0.028	0.006	9.71	9.28	2.70	17.44	17.28	0.641	0.190	208	220									
FEB	6.5	0.51	2.07	0.22	0.04	0.025	0.014	9.71	9.28	2.70	0.50	0.00	0.654	0.362	230	240									
MAR	7.3	0.34	1.23	0.13	0.06	0.024	0.015	9.71	9.28	2.70	-0.63	0.00	0.635	0.552	233	242									
APR	8.5	0.49	1.45	0.16	0.11	0.024	0.016	9.71	9.28	2.70	-0.28	0.00	0.623	0.726	235	244									
MAY	9.3	0.35	0.89	0.10	0.21	0.023	0.017	9.71	9.28	2.70	-1.13	0.00	0.581	0.327	240	245									
JUN	10.4	0.29	0.69	0.08	0.30	0.023	0.017	9.71	9.28	2.70	-1.52	0.00	0.546	1.111	241	247									
JUL	11.5	0.30	0.60	0.07	0.39	0.023	0.018	9.71	9.28	2.70	-1.69	0.00	0.493	1.301	243	248									
AUG	12.3	0.31	0.58	0.07	0.39	0.023	0.019	9.71	9.28	2.70	-1.70	0.00	0.441	1.491	245	249									
SEP	12.9	0.71	1.24	0.15	0.30	0.022	0.019	9.71	9.28	2.70	-0.47	0.00	0.427	1.675	247	250									
OCT	13.5	1.29	2.11	0.27	0.19	0.022	0.019	9.71	9.28	2.70	1.21	0.00	0.464	1.865	249	251									
NOV	15.2	1.02	1.81	0.24	0.11	0.022	0.020	9.71	9.28	2.70	0.39	0.00	0.494	2.050	250	253									
DEC	16.1	1.05	1.70	0.23	0.06	0.022	0.021	9.71	9.28	2.70	0.94	0.00	0.523	2.240	251	254									
MEAN	10.5	0.61	1.37	0.16	0.18	0.023	0.017	9.71	9.28	2.70	1.16	1.47	0.544	1.213	241	247									
TOTAL											4.2E+05 m <sup>3</sup>														

45 From curve of area vs. elevation

46 From columns 2 and 45

47 From columns 2, 45, catchment, and runoff factor

48 Mill site and low grade ore stockpile runoff, plus other wastes

49 From columns 3 and 45

50-51 From seepage calculations

52 Mill effluent

53 Mill effluent recycle (as a % of total mill inflow)

54 From moisture content and deposition rates

55 Net result of columns 46 to 54

56 From columns 37, 55 and 57

57 From column 55 and 56; 100 000 m<sup>3</sup> minimum

58 From deposition rates and densities

59 From curve of capacity vs. elevation

60 From curve of capacity vs. elevation

SETTLING POND CATCHMENT = 333 ha

## SETTLING POND

MONTH	POND AREA ha	DIRECT PRECIP	RUNOFF	POND	SEEP FR	SEEPAGE	DECANT FR	DECANT FR	EXC/	FLOW TO	REDUCTION			
				EVAP	IMP #3	OUT	IMP #1	IMP #2	DEF	FLOW CK	IN FLOW			
				1000 m3/d										
				61	62	63	64	65	66	67	68	69	70	71
JAN	1.4	0.10	27.79	0.01	0.006	0.004	2.91	0.00	30.79	30.79	9.6			
FEB	1.4	0.11	30.77	0.01	0.014	0.004	2.85	0.00	33.73	33.73	10.4			
MAR	1.4	0.07	18.37	0.01	0.015	0.004	1.72	0.00	20.16	20.16	11.0			
APR	1.4	0.08	22.54	0.02	0.016	0.004	1.30	0.00	24.51	24.51	11.7			
MAY	1.4	0.05	14.01	0.03	0.017	0.004	0.73	0.00	14.78	14.78	15.4			
JUN	1.4	0.04	10.52	0.04	0.017	0.004	0.02	0.00	10.65	10.65	20.4			
JUL	1.4	0.04	9.44	0.05	0.018	0.004	0.00	0.00	9.44	9.44	22.9			
AUG	1.4	0.04	9.26	0.04	0.019	0.004	0.00	0.00	9.27	9.27	22.5			
SEP	1.4	0.08	21.71	0.03	0.019	0.004	1.39	0.00	23.16	23.16	13.7			
OCT	1.4	0.12	38.15	0.02	0.019	0.004	3.62	0.00	41.90	41.90	10.4			
NOV	1.4	0.12	34.58	0.01	0.020	0.004	3.41	0.00	38.12	38.12	10.0			
DEC	1.4	0.12	33.51	0.01	0.021	0.004	3.42	0.00	37.05	37.05	9.6			
MEAN	1.4	0.08	22.50	0.02	0.017	0.004	1.82	0.00	24.39	24.39	14.0			
TOTAL									8.90E+06 m3					

61-62 As for Impoundment #1

63 Runoff from undisturbed catchment, plus columns 12 and 15

64-70 As for Impoundment #1

71 Reduction in Upper Florence Creek flow, before flow augmentation

## CINOLA GOLD PROJECT

HIGH WEST AREA

MONTHLY WATER BALANCE FOR AVERAGE ANNUAL PRECIPITATION: YEAR 10

YEAR 10 (page 1 of 5)

FILE: WB10

DATE: 29-Jun-89

W S RESERVOIR CATCHMENT = 162 ha  
 CATCHMENT FOR DITCH IEI = 75 ha  
 RUNOFF FACTOR = 0.7

## WATER SUPPLY RESERVOIR

MONTH	PRECIP	POTENT EVAPOT	POND	DIRECT	RUNOFF	POND	SEEPAGE	SEEP TO	WATER	DECANT	FLOW TO	EXC/	WATER	WATER	RUNOFF IN
			AREA	PRECIP	EVAP	IN	IMP #1	SUPPLY	TO IMP#1	SET POND	DEF	IN RES	ELEV	DITCH IEI	
	mm	mm	ha	mm	mm	mm	mm	mm	mm	mm	m3/d	M m3	m	1000 m3/d	
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16
JAN	216	13	15.48	1.08	7.15	0.06	0.000	0.005	0.20	0.00	7.95	0.00	1.660	310	3.66
FEB	216	15	15.48	1.19	7.91	0.09	0.000	0.005	0.20	0.00	8.81	0.00	1.660	310	4.05
MAR	144	26	15.48	0.72	4.76	0.13	0.000	0.005	0.20	0.00	5.15	0.00	1.660	310	2.44
APR	171	40	15.48	0.29	5.35	0.21	0.000	0.005	0.20	0.00	6.22	0.00	1.660	310	2.99
MAY	112	55	15.48	0.56	3.71	0.33	0.000	0.005	0.20	0.00	3.73	0.00	1.660	310	1.90
JUN	94	87	15.48	0.43	2.87	0.45	0.000	0.005	0.20	0.00	2.65	0.00	1.660	310	1.47
JUL	30	104	15.48	0.40	2.65	0.52	0.000	0.005	0.20	0.23	2.09	0.00	1.660	310	1.85
AUG	78	98	15.48	0.39	2.58	0.49	0.000	0.005	0.20	0.18	2.10	0.00	1.660	310	1.82
SEP	166	71	15.48	0.36	5.68	0.37	0.000	0.005	0.20	0.00	5.96	0.00	1.660	310	2.91
OCT	297	44	15.48	1.48	9.88	0.22	0.000	0.005	0.20	0.00	10.88	0.00	1.660	310	5.03
NOV	260	21	15.48	1.34	8.89	0.11	0.000	0.005	0.20	0.00	8.92	0.00	1.660	310	4.55
DEC	260	12	15.48	1.30	8.60	0.06	0.000	0.005	0.20	0.00	9.64	0.00	1.660	310	4.40
MEAN	173	50	15.48	0.88	5.86	0.25	0.000	0.005	0.20	0.03	6.25	0.00	1.660	310	3.00
TOTAL	2094	599										2.28E+06 m3			1.095E+06

## NOTES RE COLUMNS:

2 From Stage II Report, Vol III

3 From Stage II Report, Vol III

4 From curve of area vs. elevation

5 From columns 2 and 4

6 From columns 2, 4, catchment, and runoff factor

7 From columns 3 and 4

8 Set equal to zero

9 From seepage calculations

10 Mill make-up plus mill and mine domestic supply

11 Decant to Imp. #1 to maintain min. water vol, if necessary

12 Flow to Florence Creek; equal to excess (column 13) when reservoir full, controlled at other times

13 Net result of columns 5 to 12

14 Water volume in storage

15 From curve of capacity vs. elevation

16 From column 2, catchment, and runoff factor

IMPOUNDMENT #1 CATCHMENT = 44 ha

## IMPOUNDMENT NUMBER 1

MONTH	POND AREA ha	DIRECT PRECIP	LOCAL RUNOFF	POND EVAP	SEEPAGE		DECANT TO IMP #2	DECANT TO SET POND	SPILL TO	EXC/DEF	FROM WSR	WATER IN POND	TOT TAILS+ WASTE ROCK	SOLIDS	ELEV			
					IN	IMP #2												
					1000 m <sup>3</sup> /d	17	18	19	20	21	22	23	24	25	26	27	28	29
JAN	42.0	2.32	0.10	0.19	0.075	0.016	0.00	2.31	0.00	0.00	0.00	0.400	0.400	0.400	0.400	0.400	0.146	306
FEB	42.0	2.33	0.11	0.24	0.075	0.016	0.00	2.85	0.00	0.00	0.00	0.400	0.400	0.400	0.400	0.400	0.146	306
MAR	42.0	1.95	0.07	0.35	0.075	0.016	0.00	1.72	0.00	0.00	0.00	0.400	0.400	0.400	0.400	0.400	0.146	306
APR	42.0	2.32	0.08	0.35	0.075	0.016	0.00	1.80	0.00	0.00	0.00	0.400	0.400	0.400	0.400	0.400	0.146	306
MAY	42.0	1.51	0.08	0.59	0.075	0.016	0.00	0.73	0.00	0.00	0.00	0.400	0.400	0.400	0.400	0.400	0.146	306
JUN	42.0	1.14	0.04	1.02	0.075	0.016	0.00	0.02	0.00	0.00	0.00	0.400	0.400	0.400	0.400	0.400	0.146	306
JUL	42.0	1.08	0.04	1.41	0.075	0.016	0.00	0.00	0.00	-0.23	0.23	0.400	0.400	0.400	0.400	0.400	0.146	306
AUG	42.0	1.06	0.04	1.33	0.075	0.016	0.00	0.00	0.00	-0.18	0.18	0.400	0.400	0.400	0.400	0.400	0.146	306
SEP	42.0	2.25	0.08	0.99	0.075	0.016	0.00	1.39	0.00	0.00	0.00	0.400	0.400	0.400	0.400	0.400	0.146	306
OCT	42.0	4.02	0.13	0.50	0.075	0.016	0.00	3.62	0.00	0.00	0.00	0.400	0.400	0.400	0.400	0.400	0.146	306
NOV	42.0	3.52	0.12	0.29	0.075	0.016	0.00	3.41	0.00	0.00	0.00	0.400	0.400	0.400	0.400	0.400	0.146	306
DEC	42.0	3.52	0.00	0.16	0.075	0.016	0.00	3.42	0.00	0.00	0.00	0.400	0.400	0.400	0.400	0.400	0.146	306
MEAN	42.0	2.35	0.07	0.69	0.075	0.016	0.00	1.82	-0.03	0.03	0.00	0.400	0.400	0.400	0.400	0.400	0.146	306
TOTAL												-1.26E+04 m <sup>3</sup>						

17 From curve of area vs. elevation

30 From curve of capacity vs. elevation

18 From columns 2 and 17

19 From columns 2, 17, catchment, and runoff factor

20 From columns 3 and 17

21-22 From seepage calculations

23 Decant of pond water to Imp #2

24 Spillway flow

25 Net result of columns 18 to 24

26 Decant from water storage reservoir, if necessary

27 From column 25; 400 000 m<sup>3</sup> maximum

28-29 From Year 4

IMPOUNDMENT #2 CATCHMENT = 50 ha

## IMPOUNDMENT NUMBER 2

MONTH	POND AREA ha	DIRECT PRECIP	LOCAL RUNOFF	POND EVAP	SEEPAGE			DECANT TO IMP #3	DECANT TO SET POND	EXC/DEF FROM IMP#1	WATER IN POND	TOT TAILS+ WASTE ROCK	SOLIDS ELEV
					IN	IMP #3 1000 m3/d	SET POND						
31	32	33	34	35	36	37	38	39	40	41	42	43	
JAN	38.4	2.69	0.57	0.16	0.069	0.022	0.00	3.23	-0.10	0.00	0.439	9.092	281
FEB	38.4	2.95	0.63	0.22	0.069	0.022	0.00	3.53	-0.12	0.00	0.432	9.092	281
MAR	38.4	1.78	0.38	0.32	0.069	0.022	0.00	1.99	-0.10	0.00	0.426	9.092	281
APR	38.4	2.19	0.46	0.51	0.069	0.021	0.00	2.29	-0.11	0.00	0.425	9.092	281
MAY	38.4	1.89	0.29	0.82	0.069	0.021	0.00	1.02	-0.10	0.00	0.420	9.092	281
JUN	38.4	1.08	0.23	1.11	0.069	0.021	0.00	0.34	-0.11	0.00	0.419	9.092	281
JUL	38.4	0.99	0.21	1.29	0.069	0.021	0.00	0.06	-0.10	0.00	0.415	9.092	281
AUG	38.4	0.97	0.20	1.21	0.069	0.021	0.43	0.00	-0.43	0.00	0.403	9.092	281
SEP	38.4	2.12	0.45	0.91	0.069	0.021	-0.53	1.21	-0.02	0.00	0.402	9.092	281
OCT	38.4	3.69	0.78	0.55	0.069	0.020	0.00	3.98	-0.02	0.00	0.401	9.092	281
NOV	38.4	2.88	0.70	0.27	0.069	0.020	0.00	3.64	-0.02	0.00	0.401	9.092	281
DEC	38.4	3.22	0.58	0.15	0.069	0.020	0.00	3.83	-0.02	0.00	0.400	9.092	281
MEAN	38.4	2.19	0.46	0.63	0.069	0.021	0.08	2.10	-0.11	0.00	0.415	9.092	281
TOTAL									$-3.88E+04 \text{ m}^3$				

31 From curve of area vs. elevation

44 From curve of capacity vs. elevation

32 From columns 2 and 31

33 From columns 2, 31, catchment, and runoff factor

34 From columns 3 and 31

35-36 From seepage calculations

37 Decant of pond water to Imp #3

38 Decant to reduce water volume to nominal 400 000 m<sup>3</sup>

39 Net result of columns 32 to 38

40 Decant from Imp#1, if necessary

41 From column 40

42-43 From Year 3

PULP DENSITY =	38 t	DRY DENSITY OF PLACED TAILINGS =	1.20 t/m <sup>3</sup>
TAILINGS MOISTURE CONTENT =	45 %	BULK DENSITY OF WASTE ROCK =	2.20 t/m <sup>3</sup>

IMPOUNDMENT #3 CATCHMENT =	45 ha	AREA OF LOW GRADE ORE STOCKPILE =	0.0 ha
TAILINGS DEPOSITION RATE =	6000 t/day	VOL OF TAILS PRODUCED IN YEAR =	1.83 M m <sup>3</sup>
WASTE ROCK DEPOSITION RATE =	2500 t/day	VOL OF WASTE ROCK IN YEAR =	0.41 M m <sup>3</sup>
MILL EFFLUENT RECYCLE RATIO=	84 %	TOTAL VOL OF SOLIDS IN YEAR =	2.24 M m <sup>3</sup>

**IMPOUNDMENT NUMBER 3  
(ACTIVE)**

MONTH	POND AREA ha	DIRECT PRECIP		LOCAL RUNOFF		MILL RUNOFF		POND EVAP		SEEPAGE IN		SEEPAGE OUT		FROM MILL	RETURN TO MILL	RET IN STORES	EXC/DCF	FROM IMP #2	WATER IN POND M m <sup>3</sup>	FOT TAILS+ WASTE ROCK M m <sup>3</sup>	SOLIDS ELEV.	WATER ELEV.
		45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60					
JAN	15.2	1.05	1.45	0.20	0.05	0.022	0.020	9.71	9.28	2.70	0.37	0.00	0.303	0.292	2.126	250	250					
FEB	16.1	1.24	1.55	0.22	0.09	0.022	0.021	9.71	9.28	2.70	0.35	0.00	0.321	2.488	252	251						
MAR	16.9	0.79	0.91	0.13	0.14	0.021	0.021	9.71	9.28	2.70	-0.59	0.00	0.303	2.678	254	255						
APR	17.5	1.01	1.09	0.15	0.24	0.021	0.022	9.71	9.28	2.70	-0.25	0.10	0.295	2.562	255	255						
MAY	18.3	0.57	0.67	0.10	0.40	0.021	0.022	9.71	9.28	2.70	-1.23	0.00	0.257	3.052	255	255						
JUN	19.5	0.34	0.50	0.08	0.55	0.021	0.023	9.71	9.28	2.70	-1.72	0.10	0.206	3.233	257	258						
JUL	20.3	0.52	0.45	0.07	0.63	0.021	0.023	9.71	9.28	2.70	-1.92	0.00	0.146	3.427	258	258						
AUG	21.2	0.53	0.42	0.07	0.67	0.020	0.024	9.71	9.28	2.70	-1.93	0.43	0.100	3.617	259	259						
SEP	21.2	1.17	0.92	0.15	0.50	0.020	0.024	9.71	9.28	2.70	-0.53	0.53	0.100	3.801	260	260						
OCT	22.0	2.11	1.54	0.27	0.31	0.020	0.024	9.71	9.28	2.70	1.33	0.10	0.141	3.991	260	261						
NOV	22.2	2.01	1.33	0.24	0.16	0.020	0.025	9.71	9.28	2.70	1.13	0.00	0.175	4.175	261	261						
DEC	24.3	2.04	1.22	0.23	0.09	0.020	0.025	9.71	9.28	2.70	1.11	0.00	0.210	4.365	262	262						
MEAN	19.7	1.14	1.00	0.16	0.83	0.021	0.023	9.71	9.28	2.70	-0.31	0.08	0.213	3.339	257	259						
TOTAL													-1.1E-05	m <sup>3</sup>								

45 From curve of area vs. elevation

46 From columns 2 and 45

47 From columns 2, 45, catchment, and runoff factor

48 Mill site and low grade ore stockpile runoff, plus other wastes

49 From columns 3 and 45

50-51 From seepage calculations

52 Mill effluent

53 Mill effluent recycle (as a % of total mill inflow)

54 From moisture content and deposition rates

55 Net result of columns 46 to 54

56 From columns 53 and 57

57 From column 53 and 56; 100 000 m<sup>3</sup> minimum

58 From deposition rates and densities

59 From curve of capacity vs. elevation

60 From curve of capacity vs. elevation

SETTLING POND CATCHMENT = 388 ha

## SETTLING POND

MONTH	POND AREA ha	DIRECT PRECIP	RUNOFF	POND	GEEP FR	GEEPAGE	DECANT FR	DECANT FR	EXC/	FLOW TO	REDUCTION	
				EVAP	IMP #3	OUT	IMP #1	IMP #2	DEF	FLO CK	IN FLOW	
		(--)				1000 m3/d					:	
		61	62	63	64	65	66	67	68	69	70	71
JAN	1.4	0.10	27.79	0.01	0.020	0.004	2.91	3.23	34.03	34.03	1.5	
FEB	1.4	0.11	30.77	0.01	0.021	0.004	2.85	3.53	37.27	37.27	2.4	
MAR	1.4	0.07	18.37	0.01	0.021	0.004	1.72	1.99	22.15	22.15	3.5	
APR	1.4	0.08	22.54	0.02	0.022	0.004	1.60	2.29	26.31	26.31	4.7	
MAY	1.4	0.05	14.01	0.03	0.022	0.004	0.73	1.02	15.30	15.30	10.4	
JUN	1.4	0.04	10.62	0.04	0.023	0.004	0.02	0.34	11.00	11.00	18.1	
JUL	1.4	0.04	9.44	0.05	0.023	0.004	0.00	0.06	9.31	9.31	22.4	
AUG	1.4	0.04	9.26	0.04	0.024	0.004	0.00	0.00	9.27	9.27	22.4	
SEP	1.4	0.08	21.71	0.03	0.024	0.004	1.39	1.21	24.37	24.37	9.9	
OCT	1.4	0.13	38.15	0.02	0.024	0.004	3.62	3.98	45.39	45.39	3.1	
NOV	1.4	0.12	34.55	0.01	0.025	0.004	3.41	3.64	41.96	41.96	1.1	
DEC	1.4	0.12	33.51	0.01	0.025	0.004	3.42	3.63	40.89	40.89	1.7	
MEAN	1.4	0.08	22.50	0.02	0.023	0.004	1.82	2.10	25.50	25.50	8.6	
TOTAL											5.67E-06 m3	

61-62 As for Impoundment #1

63 Runoff from undisturbed catchment, plus columns 12 and 13

64-70 As for Impoundment #1

71 Reduction in Upper Florence Creek flow, before flow augmentation

## CINOLA GOLD PROJECT

HIGH WEST AREA

YEAR 11 (page 1 of 5)

MONTHLY WATER BALANCE FOR AVERAGE ANNUAL PRECIPITATION: YEAR 11

FILE: WB11

DATE: 29-Jun-89

W S RESERVOIR CATCHMENT = 162 ha  
 CATCHMENT FOR DITCH IE1 = 75 ha  
 RUNOFF FACTOR = 0.7

## WATER SUPPLY RESERVOIR

MONTH	PRECIP	POTENT	POND	DIRECT	RUNOFF	POND	SEEPAGE	IN	IMP #1	WATER	DECANT	FLOW TO	EXC/	WATER	WATER	RUNOFF IN	
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16		
JAN	216	13	15.48	1.08	7.15	0.05	0.000	0.005	0.20	0.00	7.96	0.00	1.660	310	3.66		
FEB	216	16	15.48	1.19	7.91	0.09	0.000	0.005	0.20	0.00	8.81	0.00	1.660	310	4.05		
MAR	144	26	15.48	0.72	4.76	0.13	0.000	0.005	0.20	0.00	5.15	0.00	1.660	310	2.44		
APR	171	40	15.49	0.88	5.85	0.21	0.000	0.005	0.20	0.00	6.32	0.00	1.660	310	2.99		
MAY	112	56	15.48	0.56	3.71	0.03	0.000	0.005	0.20	0.00	3.73	0.00	1.660	310	1.90		
JUN	94	67	15.48	0.42	2.87	0.45	0.000	0.005	0.20	0.00	2.65	0.00	1.660	310	1.47		
JUL	80	104	15.48	0.40	2.65	0.52	0.000	0.005	0.20	0.07	2.05	0.00	1.660	310	1.05		
AUG	78	98	15.43	0.39	2.58	0.49	0.000	0.005	0.20	0.18	2.10	0.00	1.560	310	1.32		
SEP	166	71	15.48	0.86	5.68	0.37	0.000	0.005	0.20	0.00	5.96	0.00	1.660	310	2.91		
OCT	297	44	15.43	1.48	3.33	0.22	0.000	0.005	0.20	0.00	10.88	0.00	1.660	310	5.08		
NOV	260	21	15.48	1.34	8.89	0.11	0.000	0.005	0.20	0.00	9.92	0.00	1.660	310	4.55		
DEC	260	12	15.48	1.30	8.60	0.06	0.000	0.005	0.20	0.00	9.64	0.00	1.660	310	4.40		
MEAN	173	50	15.48	0.88	5.86	0.25	0.000	0.005	0.20	0.04	5.24	0.00	1.660	310	3.00		
TOTAL	2084	598											2.265E-06 m3			1.095E-06	

## NOTES RE COLUMNS:

2 From Stage II Report, Vol III

3 From Stage II Report, Vol III

4 From curve of area vs. elevation

5 From columns 2 and 4

6 From columns 2, 4, catchment, and runoff factor

7 From columns 2 and 4

8 Set equal to zero

9 From seepage calculations

10 Mill make-up plus mill and mine domestic supply

11 Decant to Imp. #1 to maintain min. water vol, if necessary

12 Flow to Florence Creek; equal to excess (column 13) when reservoir full, controlled at other times

13 Net result of columns 5 to 12

14 Water volume in storage

15 From curve of capacity vs. elevation

16 From column 2, catchment, and runoff factor

IMPOUNDMENT #1 CATCHMENT = 44 ha

## IMPOUNDMENT NUMBER 1

MONTH AREA ha	POND PRECIP mm	DIRECT RUNOFF mm	LOCAL POND EVAP mm	SEEPAGE IN 1000 m3/d	BEER TO IMP #2	DECANT TO IMP #2	SPILL TO SET POND	EXC/		WATER DEF m	FROM WSR in pond	WATER TOT TAILS+ WASTE ROCK m	SOLIDS ELEV m	WATER ELEV m
								17	18	19	20	21	22	23
JAN	42.0	2.93	0.10	0.18	0.075	0.016	0.00	2.91	0.00	0.00	0.400	8.146	306	307
FEB	42.0	2.93	0.11	0.24	0.075	0.016	0.00	2.25	0.00	0.00	0.400	8.146	306	307
MAR	42.0	1.95	0.07	0.35	0.075	0.016	0.00	1.72	0.00	0.00	0.400	8.146	306	307
APR	42.0	2.32	0.08	0.56	0.075	0.016	0.00	1.90	0.00	0.00	0.400	8.146	306	307
MAY	42.0	1.52	0.08	0.89	0.075	0.016	0.00	0.73	0.00	0.00	0.400	8.146	306	307
JUN	42.0	1.14	0.04	1.22	0.075	0.016	0.00	0.02	0.00	0.00	0.400	8.146	306	307
JUL	42.0	1.08	0.04	1.41	0.075	0.016	0.04	0.00	-0.27	0.27	0.400	8.146	306	307
AUG	42.0	1.06	0.04	1.33	0.075	0.016	0.00	0.00	-0.18	0.18	0.400	8.146	306	307
SEP	42.0	2.25	0.08	0.99	0.075	0.016	0.00	1.39	0.00	0.00	0.400	8.146	306	307
OCT	42.0	1.02	0.13	0.60	0.075	0.016	0.00	0.62	0.00	0.00	0.400	8.146	306	307
NOV	42.0	0.52	0.12	0.29	0.075	0.016	0.00	0.41	0.00	0.00	0.400	8.146	306	307
DEC	42.0	0.52	0.00	0.16	0.075	0.016	0.00	0.42	0.00	0.00	0.400	8.146	306	307
MEAN	42.0	2.35	0.07	0.59	0.075	0.016	0.00	1.32	-0.04	0.04	0.400	8.146	306	307
TOTAL											-1.4E+04			

17 From curve of area vs. elevation

30 From curve of capacity vs. elevation

18 From columns 2 and 17

19 From columns 2, 17, catchment, and runoff factor

20 From columns 3 and 17

21-22 From seepage calculations

23 Decant of pond water to Imp #2

24 Spillway flow

25 Net result of columns 18 to 24

26 Decant from water supply res., if necessary

27 From column 26; 400 000 m3 maximum

28-29 From Year 4

IMPOUNDMENT #2 CATCHMENT = 50 ha

## IMPOUNDMENT NUMBER 2

MONTH	POND AREA ha	DIRECT PRECIP. mm	LOCAL RUNOFF mm	POND EVAP. mm	SEEPAGE IN 1000 m <sup>3</sup> /d	SEEP TO IMP #3	DECANT TO IMP #3	SPILL TO SPILL POND	EXC/ DEF IMP#1		WATER IN POND m <sup>3</sup>	TOT TAILS+ WASTE ROCK m <sup>3</sup>	SOLIDS ELEV m	WATER ELEV m	
									31	32	33	34	35	36	
JAN	38.4	2.68	0.57	0.16	0.069	0.019	0.00	0.18	0.00	0.00	0.400	9.092	281	283	
FEB	38.4	2.96	0.63	0.22	0.069	0.019	0.00	0.42	0.00	0.00	0.400	9.092	281	283	
MAR	38.4	1.78	0.66	0.22	0.069	0.019	0.00	1.39	0.00	0.00	0.400	9.092	281	283	
APR	38.4	2.19	0.46	0.51	0.069	0.019	0.00	2.19	0.00	0.00	0.400	9.092	281	283	
MAY	38.4	1.89	0.29	0.22	0.069	0.019	0.00	0.91	0.00	0.00	0.400	9.092	281	283	
JUN	38.4	1.03	0.23	1.11	0.069	0.019	0.00	0.24	0.00	0.00	0.400	9.092	281	283	
JUL	38.4	0.99	0.21	1.29	0.069	0.019	0.00	0.00	-0.04	0.04	0.400	9.092	281	283	
AUG	38.4	0.97	0.20	1.21	0.069	0.019	0.00	0.01	0.00	0.00	0.400	9.092	281	283	
SEP	38.4	2.12	0.45	0.91	0.069	0.019	0.00	1.72	0.00	0.00	0.400	9.092	281	283	
OCT	38.4	3.69	0.78	0.55	0.069	0.018	0.00	3.35	0.00	0.00	0.400	9.092	281	283	
NOV	38.4	3.03	0.70	0.27	0.069	0.018	0.00	3.81	0.00	0.00	0.400	9.092	281	283	
DEC	38.4	3.22	0.68	0.15	0.069	0.018	0.00	3.90	0.00	0.00	0.400	9.092	281	283	
MEAN	38.4	2.19	0.46	0.63	0.069	0.019	0.00	2.08	-0.00	0.00	0.400	9.092	281	283	
TOTAL											-1.17E+03 m <sup>3</sup>				

31 From curve of area vs. elevation

44 From curve of capacity vs. elevation

32 From columns 2 and 31

33 From columns 2, 31, catchment, and runoff factor

34 From columns 3 and 31

35-36 From seepage calculations

37 Decant of pond water to Imp #3

38 Spillway flow

39 Net result of columns 32 to 38

40 Decant from Imp#1, if necessary

41 From column 40

42-43 From Year 8

PULP DENSITY = 36 t/m<sup>3</sup>  
 TAILINGS MOISTURE CONTENT = 45 %

DRY DENSITY OF PLACED TAILINGS = 1.20 t/m<sup>3</sup>  
 BULK DENSITY OF WASTE ROCK = 2.20 t/m<sup>3</sup>

IMPOUNDMENT #3 CATCHMENT = 45 ha  
 TAILINGS DEPOSITION RATE = 6000 t/day  
 WASTE ROCK DEPOSITION RATE = 2500 t/day  
 MILL EFFLUENT RECYCLE RATIO= 84 %

AREA OF LOW GRADE ORE STOCKPILE = 0.0 ha  
 VOL OF TAILS PRODUCED IN YEAR = 1.83 M m<sup>3</sup>  
 VOL OF WASTE ROCK IN YEAR = 0.41 M m<sup>3</sup>  
 TOTAL VOL OF SOLIDS IN YEAR = 2.24 M m<sup>3</sup>

IMPOUNDMENT NUMBER 3  
 (ACTIVE)

MONTH	POND AREA ha	1000 m <sup>3</sup> /d										EXC/DEF	FROM IMP #2	WATER IN POND	TOT TAILS+ WASTE ROCK	SOLIDS ELEV	WATER ELEV		
		DIRECT PRECIP	LOCAL RUNOFF	MILL RUNOFF	POND EVAP	SEEPAGE IN	SEEPAGE OUT	FROM MILL	RETURN TO MIL	RET IN PORES	50							58	59
JAN	26.6	1.85	0.90	0.20	0.11	0.019	0.026	9.71	9.28	2.70	0.55	0.00	0.428	4,480	262	26			
FEB	26.6	2.05	0.99	0.22	0.15	0.019	0.026	9.71	9.28	2.70	0.83	0.00	0.452	4,842	263	263			
MAR	27.8	1.29	0.56	0.13	0.23	0.019	0.026	9.71	9.28	2.70	-0.54	0.00	0.435	5,032	264	266			
APR	28.3	1.65	0.64	0.15	0.39	0.019	0.027	9.71	9.28	2.70	-0.22	0.00	0.428	5,216	265	266			
MAY	28.9	1.04	0.41	0.10	0.62	0.019	0.027	9.71	9.28	2.70	-1.35	0.00	0.387	5,406	266	267			
JUN	30.1	0.84	0.29	0.08	0.87	0.019	0.027	9.71	9.28	2.70	-1.94	0.00	0.328	5,590	266	267			
JUL	30.1	0.73	0.27	0.07	1.01	0.019	0.027	9.71	9.28	2.70	-2.17	0.00	0.261	5,781	267	267			
AUG	31.2	0.79	0.24	0.07	0.99	0.018	0.028	9.71	9.28	2.70	-2.17	0.00	0.194	5,971	268	268			
SEP	31.2	1.73	0.53	0.15	0.74	0.018	0.028	9.71	9.28	2.70	-0.61	0.00	0.175	6,155	268	269			
OCT	32.4	3.10	0.95	0.27	0.46	0.018	0.028	9.71	9.28	2.70	1.47	0.00	0.221	6,345	269	271			
NOV	33.5	2.90	0.70	0.24	0.23	0.018	0.029	9.71	9.28	2.70	1.32	0.00	0.261	6,539	270	271			
DEC	33.5	2.81	0.68	0.23	0.13	0.018	0.029	9.71	9.28	2.70	1.30	0.00	0.301	6,720	270	271			
MEAN	30.1	1.73	0.59	0.16	0.50	0.019	0.027	9.71	9.28	2.70	-0.30	0.00	0.322	5,693	267	266			
TOTAL														-1.1E+05 m <sup>3</sup>					

45 From curve of area vs. elevation

56 From columns 37, 55 and 57

46 From columns 2 and 45

57 From column 55 and 56; 100 000 m<sup>3</sup> minimum

47 From columns 2, 45, catchment, and runoff factor

58 From deposition rates and densities

48 Mill site and low grade ore stockpile runoff, plus other wastes

59 From curve of capacity vs. elevation

49 From columns 3 and 45

60 From curve of capacity vs. elevation

50-51 From seepage calculations

52 Mill effluent

53 Mill effluent recycle (as % of total mill inflow)

54 From moisture content and deposition rates

55 Net result of columns 46 to 54

PULP DENSITY = 39 t/m<sup>3</sup>  
 TAILINGS MOISTURE CONTENT = 45 %

DRY DENSITY OF PLACED TAILINGS = 1.20 t/m<sup>3</sup>  
 BULK DENSITY OF WASTE ROCK = 2.20 t/m<sup>3</sup>

IMPOUNDMENT #3 CATCHMENT = 45 ha  
 TAILINGS DEPOSITION RATE = 5000 t/day  
 WASTE ROCK DEPOSITION RATE = 2500 t/day  
 MILL EFFLUENT RECYCLE RATIO= 84 %

AREA OF LOW GRADE ORE STOCKPILE = 0.0 ha  
 VOL OF TAILS PRODUCED IN YEAR = 1.83 M m<sup>3</sup>  
 VOL OF WASTE ROCK IN YEAR = 0.41 M m<sup>3</sup>  
 TOTAL VOL OF SOLIDS IN YEAR = 2.24 M m<sup>3</sup>

IMPOUNDMENT NUMBER 3  
 (ACTIVE)

MONTH	POND AREA ha <-----	DIRECT PRECIP mm	LOCAL RUNOFF mm	MILL RUNOFF mm	POND EVAP mm	SEEPAGE IN 1000 m <sup>3</sup> /d	SEEPAGE OUT 1000 m <sup>3</sup> /d	FROM MILL TO MILL PORES	RETURN MILL PORES	RET IN MILL PORES	EXCV	FROM DEF	FROM IMP #2	WATER IN POND	TOT TAILS+ WASTE ROCK	SOLIDS ELEV
											55	56	57	58	59	59
JAN	25.6	1.35	0.90	0.20	0.11	0.019	0.026	9.71	9.28	2.70	0.55	0.00	0.411	4.480	262	
FEB	25.6	2.05	0.99	0.22	0.15	0.019	0.026	9.71	9.28	2.70	0.83	0.00	0.452	4.842	263	
MAR	27.9	1.23	0.56	0.13	0.23	0.019	0.026	9.71	9.28	2.70	-0.54	0.00	0.435	5.032	264	
APR	22.9	1.65	0.64	0.16	0.39	0.019	0.027	9.71	9.28	2.70	-0.22	0.00	0.429	5.216	265	
MAY	29.9	1.04	0.41	0.10	0.32	0.019	0.027	9.71	9.28	2.70	-1.35	0.00	0.387	5.406	266	
JUN	30.1	0.84	0.29	0.08	0.37	0.019	0.027	9.71	9.28	2.70	-1.34	0.00	0.323	5.590	266	
JUL	30.1	0.73	0.27	0.07	1.01	0.019	0.027	9.71	9.28	2.70	-2.17	0.00	0.261	5.781	267	
AUG	31.2	0.79	0.24	0.07	0.99	0.018	0.028	9.71	9.28	2.70	-2.17	0.00	0.194	5.971	268	
SEP	31.2	1.73	0.53	0.15	0.74	0.019	0.029	9.71	9.28	2.70	-0.61	0.00	0.175	6.155	268	
OCT	32.4	3.10	0.85	0.27	0.46	0.019	0.028	9.71	9.28	2.70	1.47	0.00	0.221	6.345	269	
NOV	33.5	2.30	0.70	0.24	0.23	0.019	0.029	9.71	9.28	2.70	1.82	0.00	0.281	6.529	270	
DEC	33.5	1.31	0.59	0.23	0.10	0.019	0.029	9.71	9.28	2.70	1.80	0.00	0.301	6.720	270	
MEAN	30.1	1.73	0.59	0.16	0.50	0.019	0.027	9.71	9.28	2.70	-0.00	0.00	0.322	5.693	267	
TOTAL													-1.1E+05 m <sup>3</sup>			

45 From curve of area vs. elevation

46 From columns 2 and 45

47 From columns 2, 45, catchment, and runoff factor

48 Mill site and low grade ore stockpile runoff, plus other wastes

49 From columns 3 and 45

50-51 From seepage calculations

52 Mill effluent

53 Mill effluent recycle (as % of total mill inflow)

54 From moisture content and deposition rates

55 Net result of columns 45 to 54

56 From columns 37, 55 and 57

57 Prod column 55 and 56; 100 000 m<sup>3</sup> minimum

58 From deposition rates and densities

59 From curve of capacity vs. elevation

60 From curve of capacity vs. elevation

SETTLING POND CATCHMENT = 333 ha

## SETTLING POND

MONTH	POND AREA ha	DIRECT PRECIP	RUNOFF	POND	BEEF FR	SEEPAGE	SPILL FR	SPILL FR	EXCV	FLOW TO	REDUCTION	
				EVAP	IMP #3	OUT	IMP #1	IMP #2	DEF	FLO CK	IN FLOW	
				1000 m3/d								
				61	62	63	64	65	66	67	68	69
JAN	1.4	0.10	27.79	0.01	0.026	0.004	2.91	0.13	33.94	33.94	1.7	
FEB	1.4	0.11	30.77	0.01	0.025	0.004	2.85	3.42	37.16	37.16	2.7	
MAR	1.4	0.07	19.37	0.01	0.026	0.004	1.72	1.29	22.06	22.06	3.9	
APR	1.4	0.08	22.54	0.02	0.027	0.004	1.90	2.13	26.71	26.71	5.0	
MAY	1.4	0.05	14.01	0.03	0.027	0.004	0.73	0.91	15.70	15.70	10.3	
JUN	1.4	0.04	10.62	0.04	0.027	0.004	0.02	0.24	10.60	10.60	12.3	
JUL	1.4	0.04	9.40	0.05	0.027	0.004	0.00	0.00	9.41	9.41	20.1	
AUG	1.4	0.04	9.26	0.04	0.028	0.004	0.00	0.01	9.28	9.28	22.4	
SEP	1.4	0.08	21.71	0.03	0.028	0.004	1.39	1.72	24.88	24.88	5.3	
OCT	1.4	0.13	38.15	0.02	0.028	0.004	3.62	3.65	45.87	45.87	3.2	
NOV	1.4	0.12	34.58	0.01	0.028	0.004	3.41	3.61	41.94	41.94	2.3	
DEC	1.4	0.12	33.51	0.01	0.028	0.004	3.42	3.20	40.87	40.87	1.7	
MEAN	1.4	0.08	22.49	0.02	0.027	0.004	1.82	2.08	26.48	26.48	3.7	
TOTAL									9.66E-05	m3		

61-62 As for Impoundment #1

63 Runoff from undisturbed catchment, plus columns 10 and 11

64-70 As for Impoundment #1

71 Reduction in Upper Florence Creek flow, before flow augmentation

## CINOLA GOLD PROJECT

HIGH WEST AREA

MONTHLY WATER BALANCE FOR AVERAGE ANNUAL PRECIPITATION: YEAR 12

YEAR 12 (page 1 of 5)

FILE: WB12

DATE: 29-Jun-89

W S RESERVOIR CATCHMENT = 162 ha  
 CATCHMENT FOR DITCH IE1 = 75 ha  
 RUNOFF FACTOR = 0.7

## WATER SUPPLY RESERVOIR

MONTH	PRECIP	POTENT	POND	DIRECT	RUNOFF	POND	SEEPAGE	SEEP TO	WATER	DECANT	FLOW TO	EXC/	WATER	WATER	RUNOFF IN	
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	
			ha	mm	mm	ha	mm	in	1000 m3/d				m	m3	1000 m3/d	
JAN	216	13	15.48	1.08	7.15	0.06	0.000	0.005	0.20	0.00	7.96	0.00	1.660	310	3.66	
FEB	216	19	15.48	1.19	7.91	0.09	0.000	0.005	0.20	0.00	8.51	0.00	1.660	310	4.05	
MAR	144	26	15.48	0.72	4.76	0.13	0.000	0.005	0.20	0.00	5.15	0.00	1.660	310	2.44	
APR	171	40	15.48	0.88	5.85	0.21	0.000	0.005	0.20	0.00	6.52	0.00	1.660	310	2.99	
MAY	112	66	15.48	0.56	3.71	0.03	0.000	0.005	0.20	0.00	3.73	0.00	1.660	310	1.30	
JUN	84	57	15.48	0.48	2.37	0.45	0.000	0.005	0.20	0.00	2.53	0.00	1.660	310	1.47	
JUL	80	104	15.48	0.40	2.65	0.52	0.000	0.005	0.20	0.27	2.05	0.00	1.660	310	1.35	
AUG	78	99	15.48	0.39	2.52	0.49	0.000	0.005	0.20	1.02	1.26	0.00	1.660	310	1.22	
SEP	166	71	15.48	0.86	5.68	0.37	0.000	0.005	0.20	0.00	5.96	0.00	1.660	310	2.91	
OCT	297	44	15.48	1.48	9.83	0.22	0.000	0.005	0.20	0.00	10.28	0.00	1.660	310	5.03	
NOV	260	21	15.48	1.34	9.89	0.11	0.000	0.005	0.20	0.00	9.92	0.00	1.660	310	4.55	
DEC	260	12	15.48	1.30	9.60	0.06	0.000	0.005	0.20	0.00	9.54	0.00	1.660	310	4.40	
MEAN	173	50	15.48	0.88	5.86	0.25	0.000	0.005	0.20	0.11	6.17	0.00	1.660	310	3.00	
TOTAL	2084	599									2.25E+06	m3				1.095E+06 m3

## NOTES RE COLUMNS:

2 From Stage II Report, Vol III

3 From Stage II Report, Vol III

4 From curve of area vs. elevation

5 From columns 2 and 4

6 From columns 2, 4, catchment, and runoff factor

7 From columns 3 and 4

8 Set equal to zero

9 From seepage calculations

10 Mill make-up plus mill and mine domestic supply

11 Decant to Imp. #1 to maintain min. water vol, if necessary

12 Flow to Florence Creek; equal to excess (column 13) when reservoir full, controlled at other times

13 Net result of columns 3 to 12

14 Water volume in storage

15 From curve of capacity vs. elevation

16 From column 2, catchment, and runoff factor

IMPOUNDMENT #1 CATCHMENT = 44 ha

## IMPOUNDMENT NUMBER 1

MONTH	POND AREA ha	1000 m <sup>3</sup> /d										EXC/ DEF	FROM WSR	WATER IN POND	TOT TAILS+ WASTE ROCK	SOLIDS ELEV	WATER ELEV
		DIRECT PRECIP	LOCAL RUNOFF	POND EVAP	SEEPAGE IN	SEEP TO IMP #2	DECANT TO IMP #2	SPILL TO SET POND									
		17	18	19	20	21	22	23	24	25	26	27	28	29	30		
JAN	42.0	2.83	0.10	0.13	0.075	0.016	0.00	2.91	0.00	0.00	0.00	0.400	8.146	306	307		
FEB	42.0	2.83	0.11	0.24	0.075	0.016	0.00	2.85	0.00	0.00	0.400	8.146	306	307			
MAR	42.0	1.65	0.07	0.35	0.075	0.016	0.00	1.72	0.00	0.00	0.400	8.146	306	307			
APR	42.0	2.32	0.08	0.56	0.075	0.016	0.00	1.90	0.00	0.00	0.400	8.146	306	307			
MAY	42.0	1.52	0.05	0.39	0.075	0.016	0.00	0.72	0.00	0.00	0.400	8.146	306	307			
JUN	42.0	1.14	0.04	1.22	0.075	0.016	0.00	0.02	0.00	0.00	0.400	8.146	306	307			
JUL	42.0	1.08	0.04	1.41	0.075	0.016	0.04	1.00	-0.27	0.27	0.400	8.146	306	307			
AUG	42.0	1.06	0.04	1.33	0.075	0.016	0.84	0.00	-1.02	1.02	0.400	8.146	306	307			
SEP	42.0	2.25	0.08	0.99	0.075	0.016	0.00	1.89	0.00	0.00	0.400	8.146	306	307			
OCT	42.0	4.02	0.18	0.60	0.075	0.016	0.00	3.62	0.00	0.00	0.400	8.146	306	307			
NOV	42.0	3.52	0.12	0.29	0.075	0.016	0.00	3.41	0.00	0.00	0.400	8.146	306	307			
DEC	42.0	3.52	0.00	0.16	0.075	0.016	0.00	3.42	0.00	0.00	0.400	8.146	306	307			
MEAN	42.0	2.35	0.07	0.63	0.075	0.016	0.074	1.82	-0.11	0.11	0.400	8.146	306	307			
TOTAL											-4.0E-04						

17 From curve of area vs. elevation

30 From curve of capacity vs. elevation

18 From columns 2 and 17

19 From columns 2, 17, catchment, and runoff factor

20 From columns 3 and 17

21-22 From seepage calculations

23 Decant of pond water to Imp #2

24 Spillway flow

25 Net result of columns 18 to 24

26 Decant from water supply res., if necessary

27 From column 26; 400 000 m<sup>3</sup> maximum

28-29 From Year 4

IMPOUNDMENT #2 CATCHMENT = 50 ha

## IMPOUNDMENT NUMBER 2

MONTH	POND AREA ha <----- ha	DIRECT PRECIP	LOCAL RUNOFF	POND EVAP	SEEPAGE			DECANT TO IMP #3	SPILL TO SET POND	EXC/ DEF IMP#1	FROM IMP#1	WATER IN POND	TOT TAILWAT- E ROCK	SOLIDS ELEV	WATER ELEV		
					IN 1000 m <sup>3</sup> /d	IMP #3	IMP #3										
31	32	33	34	35	36	37	38	39	40	41	42	43	44				
JAN	38.4	2.68	0.37	0.16	0.069	0.018	0.00	0.13	0.00	0.00	0.00	0.00	0.400	9.031	281	283	
FEB	38.4	2.95	0.38	0.22	0.069	0.018	0.00	0.42	0.00	0.00	0.00	0.00	0.400	9.032	281	283	
MAR	38.4	1.78	0.38	0.32	0.069	0.018	0.00	1.89	0.00	0.00	0.00	0.00	0.400	9.032	281	283	
APR	38.4	2.19	0.46	0.51	0.069	0.017	0.00	2.19	0.00	0.00	0.00	0.00	0.400	9.032	281	283	
MAY	38.4	1.23	0.23	0.32	0.069	0.017	0.00	0.81	0.00	0.00	0.00	0.00	0.400	9.032	281	283	
JUN	38.4	1.03	0.23	1.11	0.069	0.017	0.00	0.24	0.00	0.00	0.00	0.00	0.400	9.032	281	283	
JUL	38.4	0.99	0.21	1.03	0.069	0.017	0.00	0.00	0.00	-0.04	0.04	0.00	0.400	9.032	281	283	
AUG	38.4	0.97	0.20	1.21	0.069	0.017	0.85	0.00	0.00	-0.84	0.84	0.00	0.400	9.032	281	283	
SEP	38.4	2.12	0.45	0.31	0.069	0.017	0.57	1.05	0.00	0.00	0.00	0.00	0.400	9.032	281	283	
OCT	38.4	3.68	0.72	0.55	0.069	0.017	0.00	3.96	0.00	0.00	0.00	0.00	0.400	9.032	281	283	
NOV	38.4	3.03	0.70	0.57	0.069	0.017	0.00	3.81	0.00	0.00	0.00	0.00	0.400	9.032	281	283	
DEC	38.4	3.22	0.68	0.16	0.069	0.017	0.00	3.81	0.00	0.00	0.00	0.00	0.400	9.032	281	283	
MEAN	38.4	2.19	0.46	0.53	0.069	0.017	0.13	2.03	-0.07	0.07	0.07	0.400	9.032	281	283		
TOTAL									-0.722+04 m3								

31 From curve of area vs. elevation

44 From curve of capacity vs. elevation

32 From columns 3 and 31

33 From columns 2, 31, catchment, and runoff factor

34 From columns 3 and 31

35-36 From seepage calculations

37 Decant of pond water to Imp #3

38 Sailway flow

39 Net result of columns 32 to 33

40 Decant from Imp#1, if necessary

41 From column 40

42-43 From Year 3

PULP DENSITY = 36 t/m<sup>3</sup>  
 TAILINGS MOISTURE CONTENT = 45 %  
 DRY DENSITY OF PLACED TAILINGS = 1.20 t/m<sup>3</sup>  
 BULK DENSITY OF WASTE ROCK = 2.20 t/m<sup>3</sup>

IMPOUNDMENT #3 CATCHMENT = 45 ha  
 TAILINGS DEPOSITION RATE = 6000 t/day  
 WASTE ROCK DEPOSITION RATE = 2500 t/day  
 MILL EFFLUENT RECYCLE RATIO= 84 %  
 AREA OF LOW GRADE ORE STOCKPILE = 0.0 ha  
 VOL OF TAILS PRODUCED IN YEAR = 1.83 M m<sup>3</sup>  
 VOL OF WASTE ROCK IN YEAR = 0.41 M m<sup>3</sup>  
 TOTAL VOL OF SOLIDS IN YEAR = 2.24 M m<sup>3</sup>

**IMPOUNDMENT NUMBER 3  
(ACTIVE)**

MONTH	POND AREA ha	DIRECT PRECIP mm	LOCAL RUNOFF mm	MILL RUNOFF mm	POND EVAP mm	SEEPAGE IN mm	SEEPAGE OUT mm	FROM MILL mm	RETURN TO MILL mm	RET IN PORES mm	EXC/ DEF mm	FROM IMP #2 mm	WATER IN POND mm	TOT TAILS+ WASTE ROCK mm	SOLIDS mm	WATER ELEV m	ELEV m
						1000 m <sup>3</sup> /d											
JAN	34.7	2.42	0.50	0.20	0.15	0.016	0.029	9.71	9.29	2.70	0.68	0.00	0.322	6.310	271	271	
FEB	35.8	2.76	0.50	0.22	0.20	0.018	0.030	9.71	9.29	2.70	0.98	0.00	0.350	7.082	271	272	
MAR	36.9	1.66	0.30	0.13	0.30	0.019	0.030	9.71	9.29	2.70	-0.50	0.00	0.334	7.272	272	273	
APR	37.0	2.11	0.32	0.16	0.49	0.017	0.030	9.71	9.29	2.70	-0.19	0.00	0.325	7.456	272	273	
MAY	37.0	1.34	0.20	0.10	0.79	0.017	0.030	9.71	9.29	2.70	-1.44	0.00	0.284	7.646	273	274	
JUN	38.2	1.07	0.13	0.06	1.11	0.017	0.031	9.71	9.29	2.70	-2.11	0.00	0.220	7.830	273	274	
JUL	38.2	0.98	0.12	0.07	1.29	0.017	0.031	9.71	9.29	2.70	-2.39	0.00	0.146	8.020	274	274	
AUG	38.2	0.95	0.12	0.07	1.21	0.017	0.031	9.71	9.29	2.70	-2.34	0.85	0.100	8.211	275	275	
SEP	39.3	2.18	0.22	0.15	0.93	0.017	0.031	9.71	9.29	2.70	-0.67	0.67	0.100	8.395	275	275	
OCT	39.3	3.77	0.38	0.27	0.56	0.017	0.031	9.71	9.29	2.70	1.57	0.00	0.149	8.585	275	276	
NOV	40.5	3.51	0.27	0.24	0.29	0.017	0.031	9.71	9.29	2.70	1.45	0.00	0.192	8.769	276	277	
DEC	41.5	3.49	0.20	0.23	0.16	0.017	0.032	9.71	9.29	2.70	1.47	0.00	0.238	8.959	276	277	
MEAN	38.0	2.18	0.27	0.16	0.62	0.017	0.030	9.71	9.29	2.70	-0.30	0.13	0.230	7.938	274	274	
TOTAL													-1.18+05 m <sup>3</sup>				

45 From curve of area vs. elevation

46 From columns 2 and 45

47 From columns 2, 45, catchment, and runoff factor

48 Mill site and low grade ore stockpile runoff, plus other wastes

49 From columns 3 and 45

50-51 From seepage calculations

52 Mill effluent

53 Mill effluent recycle (as a % of total mill inflow)

54 From moisture content and deposition rates

55 Net result of columns 46 to 54

56 From columns 37, 55 and 57

57 From column 55 and 56; 100 000 m<sup>3</sup> minimum

58 From deposition rates and densities

59 From curve of capacity vs. elevation

60 From curve of capacity vs. elevation

SETTLING POND CATCHMENT = 333 ha

## SETTLING POND

MONTH	POND AREA ha	1000 m <sup>3</sup> /d										REDUCTION IN FLOW
		DIRECT PRECIP mm	RUNOFF EVAP	POND IMP #3	SEEPAGE OUT	SPILL FR IMP #1	SPILL FR IMP #2	EXC/DEF	FLOW TO FLO CK	70	71	
61	62	63	64	65	66	67	68	69	70	71		
JAN	1.4	0.10	27.79	0.01	0.029	0.004	2.31	3.13	33.94	33.94	1.7	
FEB	1.4	0.11	30.77	0.01	0.030	0.004	2.85	3.42	37.17	37.17	2.7	
MAR	1.4	0.07	18.37	0.01	0.030	0.004	1.72	1.89	22.06	22.06	3.9	
APR	1.4	0.08	22.54	0.02	0.030	0.004	1.30	2.19	26.71	26.71	4.9	
MAY	1.4	0.05	14.01	0.03	0.030	0.004	0.73	0.91	15.71	15.71	10.2	
JUN	1.4	0.04	10.62	0.04	0.031	0.004	0.02	0.24	10.90	10.90	15.3	
JUL	1.4	0.04	9.40	0.05	0.031	0.004	0.00	0.00	9.42	9.42	23.1	
AUG	1.4	0.04	8.42	0.04	0.031	0.004	0.00	0.00	8.44	8.44	28.2	
SEP	1.4	0.08	21.71	0.03	0.031	0.004	1.39	1.05	24.22	24.22	10.4	
OCT	1.4	0.13	33.15	0.02	0.031	0.004	3.52	3.95	45.38	45.38	3.2	
NOV	1.4	0.12	34.58	0.01	0.031	0.004	3.41	3.81	41.68	41.68	1.3	
DEC	1.4	0.12	33.51	0.01	0.032	0.004	3.42	3.81	40.87	40.87	1.7	
MEAN	1.4	0.08	22.42	0.02	0.030	0.004	1.82	2.03	26.36	26.36	3.4	
TOTAL									9.625E-06	m <sup>3</sup>		

61-62 As for Impoundment #1

63 Runoff from undisturbed catchment, plus columns 12 and 16

64-70 As for Impoundment #1

71 Reduction in Upper Florence Creek flow, before flow augmentation

**APPENDIX 4.2.3-1**

**BASEFLOWS FROM THE YAKOUN RIVER NEAR PORT CLEMENTS  
(080A003) GAUGE AND FROM BARBIE  
AND FLORENCE CREEKS**

**(Pages 1 to 2)**

## APPENDIX 4.2.3-1

BASEFLOWS FROM THE YAKOUN RIVER NEAR PORT CLEMENTS  
(080A003) GAUGE AND FROM BARBIE AND FLORENCE CREEKS

YEAR	DATE	BASE FLOWS IN STUDY AREA STREAMS ( $m^3/s$ )			
		BARBIE MIDDLE	CREEK LOWER	FLORENCE MIDDLE	CREEK LOWER
1986	Dec 16		0.159		11.6
1987	Mar 3		0.159		11.5
1987	Mar 19	0.1	0.226		17.9
1987	Apr 6	0.037	0.101		8.8
1987	Apr 25	0.086	0.159		20.6
1987	May 9	0.051	0.109	0.43	16.9
1987	May 20	0.089	0.146	0.52	22.1
1987	May 23	0.044	0.104	0.36	10.4
1987	June 9		0.093	0.39	10.4
1987	June 25	0.035		0.114	7.76
1987	June 30	0.027		0.071	5.41
1987	July 6	0.02	0.051	0.058	3.91
1987	July 15	0.013	0.023	0.04	3.22
1987	July 20	0.009	0.012	0.025	2.68
1987	Aug 10	0.013	0.041	0.029	2.24
1987	Aug 27	0.008	0.041	0.03	2.02
1987	Sept 5	0.023	0.093	0.076	8.57
1987	Sept 10	0.013	0.051	0.038	4.25
1987	Sept 26	0.037	0.4	0.13	23.1
1987	Oct 11	0.034	0.113	0.115	15.6
1987	Oct 23	0.025	0.083	0.027	8.5
1987	Nov 2	0.086	0.191	0.341	25.9
1987	Nov 16		0.353	0.286	35.5
1987	Dec 17	0.132	0.194	0.24	30
1988	Jan 7	0.041	0.062	0.103	10
1988	Jan 31	0.04	0.104	0.092	21.8
1988	Feb 24	0.068	0.133	0.146	16.7
1988	Feb 28	0.057	0.097	0.112	13.2
1988	Mar 16	0.066	0.114	0.121	17.1
1988	Mar 27				36.3
1988	Apr 15	0.072	0.133	0.2	21.4
1988	Apr 27	0.036	0.057	0.111	10.5
1988	May 9	0.013	0.022	0.133	7.67
1988	June 6	0.071	0.171	0.121	21.9
1988	June 13	0.048	0.105	0.109	9.58

continued . . .

**APPENDIX 4.2.3-1 (concluded)**

BASEFLOWS FROM THE YAKOUN RIVER NEAR PORT CLEMENTS  
(080A003) GAUGE AND FROM BARBIE AND FLORENCE CREEKS

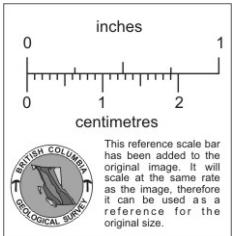
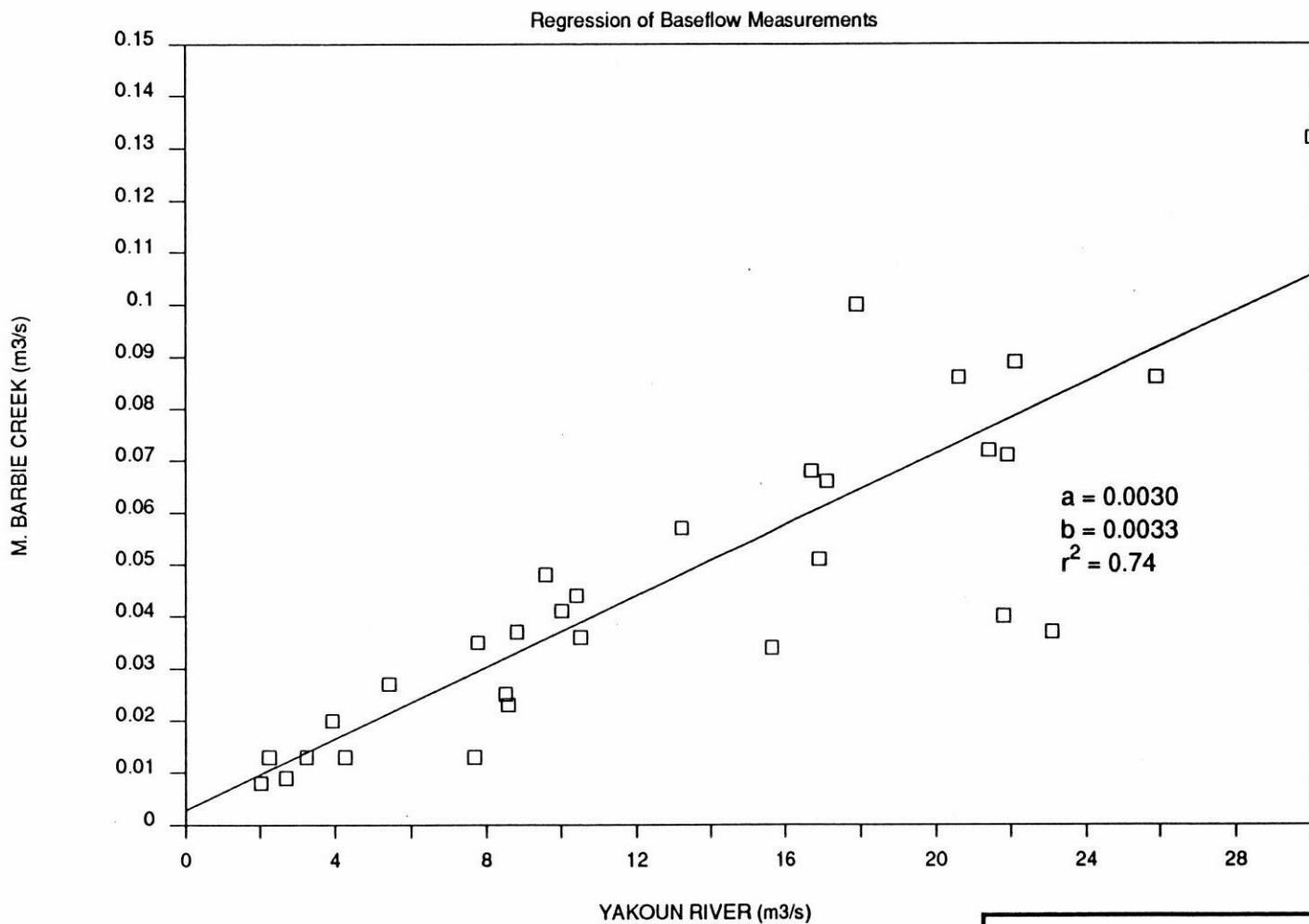
BASE FLOWS IN STUDY AREA STREAMS ( $m^3/s$ )						
YEAR	DATE	BARBIE CREEK MIDDLE	LOWER	FLORENCE CREEK MIDDLE	LOWER	YAKOUN WSC
1988	July 7	0.061	0.113	0.376	7.98	
1988	July 20	0.122	0.077	0.394	7.01	
1988	Aug 5	0.019	0.101	0.215	6.85	
1988	Aug 16	0.019	0.045	0.168	4.93	
1988	Aug 27	0.019	0.045	0.143	3.04	
1988	Sept 4	0.01	0.039	0.133	3.84	
1988	Sept 17	0.019	0.044	0.154	5.36	
1988	Oct 28	0.211	0.316	0.692	27.4	

**APPENDIX 4.2.3-2**

**LINEAR REGRESSION PLOTS FOR CONCURRENT BASE-FLOW  
DISCHARGES ON THE STUDY AREA CREEKS  
AND THE YAKOUN RIVER**

**(Pages 1 to 4)**

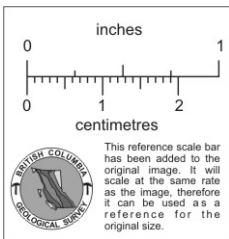
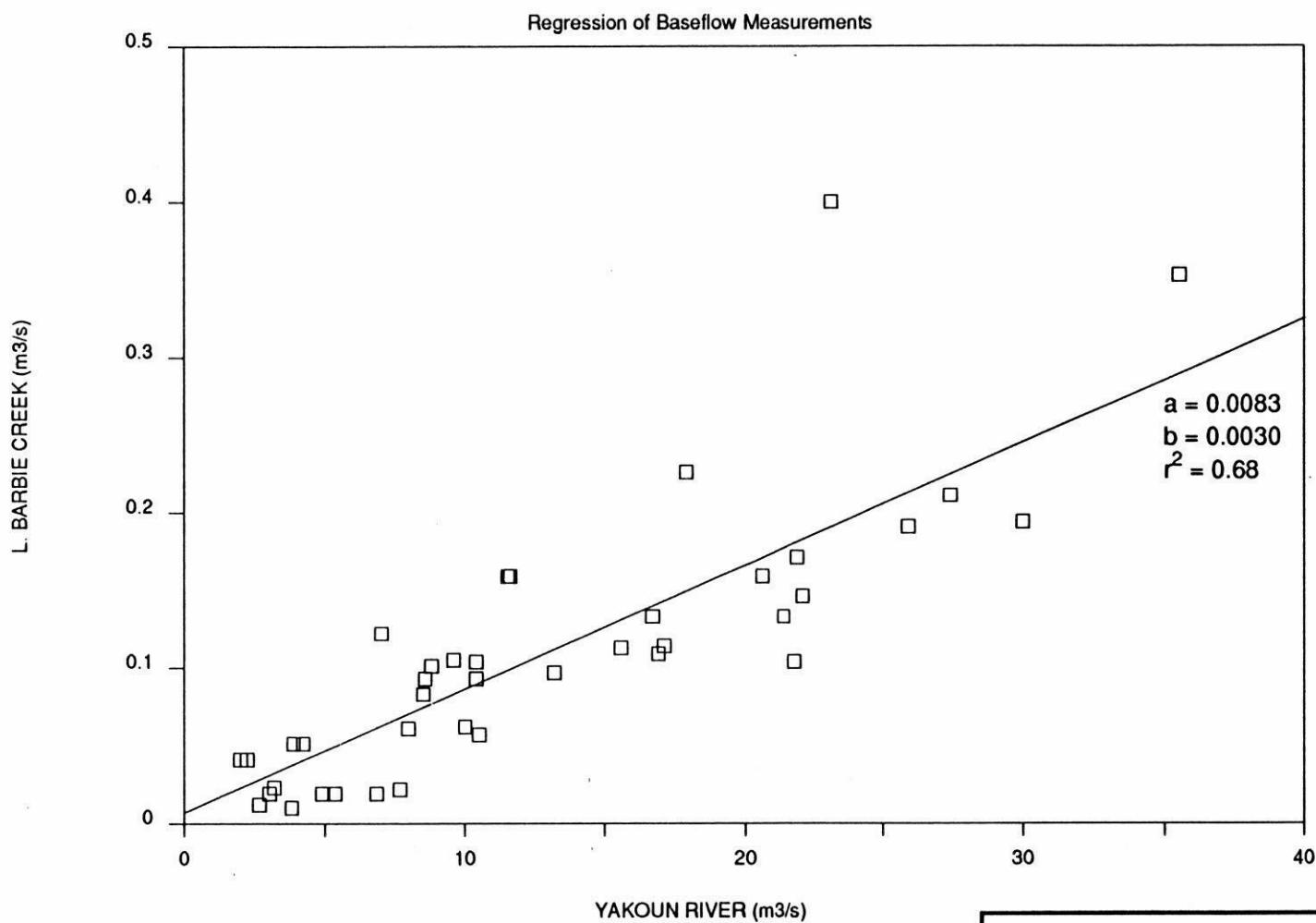
# Yakoun vs Middle Barbie



## YAKOUN VS MIDDLE BARBIE

Figure No. 1	CINOLA ADDENDUM REPORT
Date May 1989	Drawn by NORECOL

# Yakoun vs Lower Barbie



**YAKOUN VS LOWER BARBIE**

Figure No.  
**2**

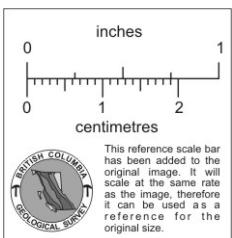
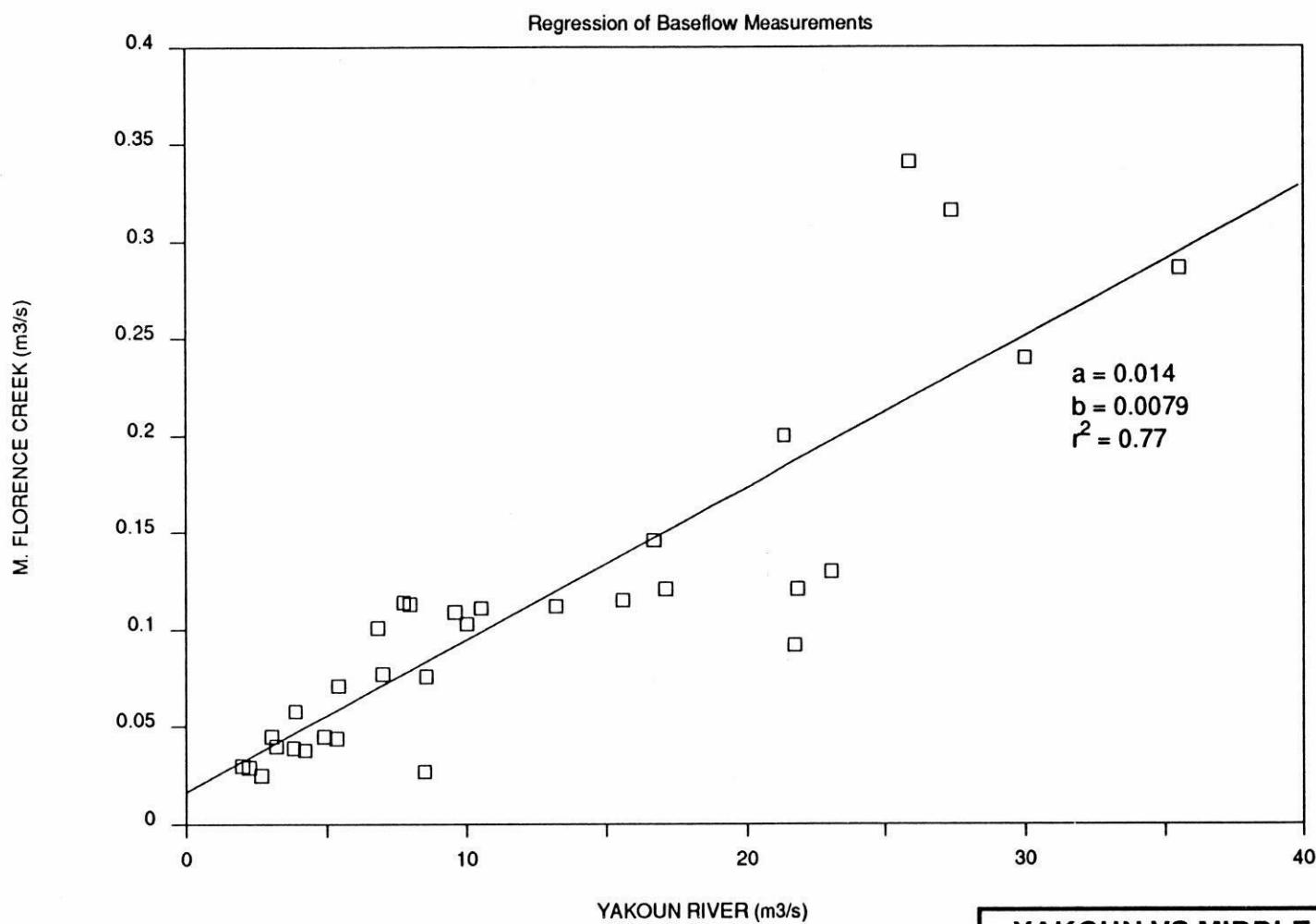
CINOLA ADDENDUM  
REPORT

Date  
**May 1989**

Drawn by

**NORECOL**

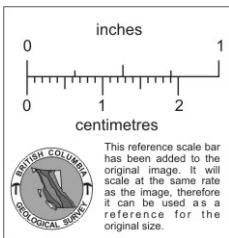
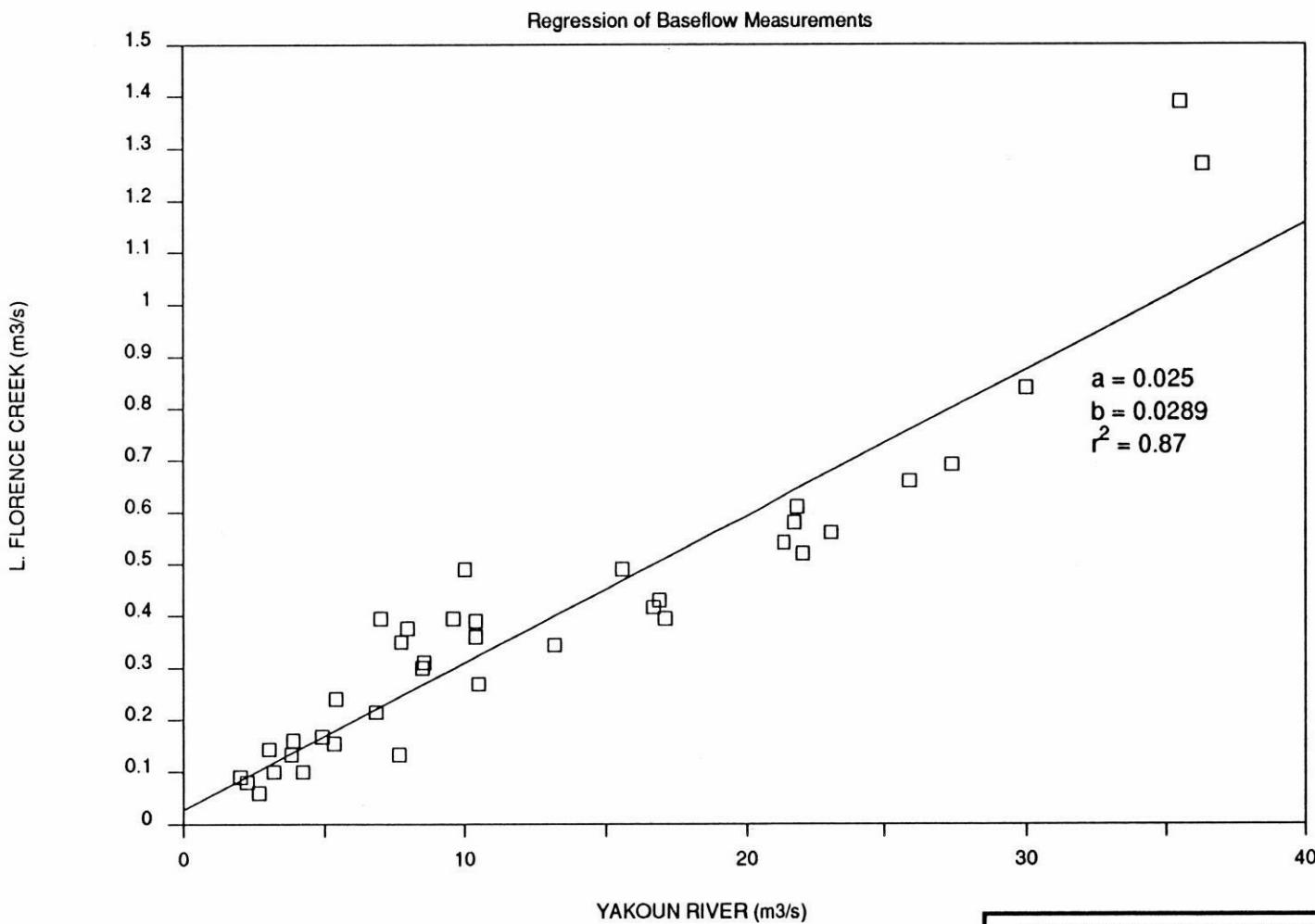
# Yakoun vs Middle Florence



## YAKOUN VS MIDDLE FLORENCE

Figure No. 3	CINOLA ADDENDUM REPORT
Date May 1989	Drawn by NORECOL

# Yakoun vs Lower Florence



**YAKOUN VS LOWER FLORENCE**

Figure No.  
**4**

CINOLA ADDENDUM  
REPORT

Date  
**May 1989**

Drawn by

**NORECOL**

**APPENDIX 4.2.6-1**

**MINE AREA: WATER MANAGEMENT PLAN  
FOR YEAR OF WETTEST PRECIPITATION**

**(Pages 1 to 9)**

CINOLA GOLD PROJECT - MINE AREA  
WATER MANAGEMENT PLAN FOR YEAR OF WETTEST PRECIPITATION: YEAR 3

50  
Sheet 1

FILE: MINWAT3

	Catchment Area (ha)	Runoff Factor		Catchment Area (ha)	Runoff Factor
Pit (Mudstone)	0.00	0.90	WRS: 3:1 slope to south	3.00	0.98
Pit (Acid Generating)	39.25	0.90	WRS: 3:1 slope to north	1.60	0.98
			WRS: Top surface	8.00	0.90
MSSP1: WRS Runoff	1.10	1.00	WRS: Active face	5.07	1.00
MSSP2: WRS Active face	0.60	1.00	Haul Road to WRS	1.44	1.00
MSSP3: Pit - Acid Gen.	1.35	1.00	WRS to Pit & Area south	9.08	0.60
MSSP4: Pit - Mudstone	0.00	1.00	Above WRS & below Div ditch	33.50	0.80
MSSP5: Temp. Haul Road	0.20	1.00			
MSSP6: M & O	2.45	1.00	Mudstone dump	20.00	0.90
MSSP7: WRS North	1.10	1.00	Overburden dump	12.23	0.70
MSSP8: Mine Plant	0.00	1.00	Area around M/S & O/B	37.45	0.60

MONTH	DAYS	PPTN POTENTIAL EVAPO- TRANSPERSION	DISCHARGE LOCAL from PIT		GROUNDWATER from PIT to MSSP3 to MSSP3	TOTAL MSSP3 LIME TREATPLANT	DISCHARGE LOCAL from WRS to MSSP2		TOTAL INFLOW to MSSP2 to MSSP2	DISCHARGE LOCAL to MSW1		TOTAL INFLOW to MSW1 to MSW1	
			ACID GEN	to MSSP3			1000 m <sup>3</sup> /d	1000 m <sup>3</sup> /d		1000 m <sup>3</sup> /d	1000 m <sup>3</sup> /d		
1	2	3	4	5	6	7	8	9	10	11	12	13	14
JAN	31	281	14	3.20	0.12	0.14	3.46	0.71	0.05	0.76	4.22	0.40	4.62
FEB	28	251	16	3.17	0.12	0.14	3.42	0.70	0.05	0.75	4.18	0.39	4.56
MAR	31	160	26	1.82	0.06	0.14	2.03	0.48	0.03	0.50	2.53	0.21	2.74
APR	30	180	41	2.12	0.07	0.14	2.33	0.53	0.03	0.56	2.88	0.23	3.11
MAY	31	104	66	1.19	0.03	0.14	1.35	0.37	0.01	0.38	1.73	0.09	1.82
JUN	30	96	88	1.13	0.02	0.14	1.29	0.36	0.01	0.37	1.65	0.06	1.71
JUL	31	110	105	1.25	0.02	0.14	1.41	0.38	0.01	0.39	1.80	0.06	1.86
AUG	31	89	98	1.01	0.01	0.14	1.16	0.34	0.00	0.34	1.51	0.03	1.54
SEP	30	185	71	2.18	0.06	0.14	2.38	0.54	0.03	0.56	2.94	0.21	3.15
OCT	31	317	44	3.61	0.13	0.14	3.88	0.78	0.06	0.83	4.71	0.42	5.13
NOV	30	337	19	3.97	0.15	0.14	4.25	0.84	0.06	0.90	5.16	0.49	5.65
DEC	31	268	11	3.05	0.11	0.14	3.31	0.68	0.05	0.73	4.04	0.38	4.42
MEAN		198	50	2.30	0.07	0.14	2.51	0.56	0.03	0.59	3.10	0.25	3.35
TOTAL		2378	599										

NOTES RE COLUMNS:

- 3 From Norecol (Yakoun R data # 18/17)
- 4 From Norecol report (Masset data)
- 5 From area and runoff factor
- 6 From area and runoff factor less 2/3 of potential evapotranspiration from pond
- 7 Groundwater to MSSP3
- 8 Total of 5 to 7
- 9 From area and runoff factor for active face, infiltration from 3:1 slopes and horizontal surface, and groundwater to WRS
- 10 From area and runoff factor
- 11 Total of 9 and 10
- 12 Total of 8 and 11
- 13 From area and runoff factor less 2/3 of potential evapotranspiration from pond
- 14 Total of 12 and 13

	Catchment Area (ha)	Runoff Factor	Quantity (m³/d)	
Between Pit & Haul Road	4.25	0.60	Groundwater to WRS	168
Mine Plant incl. MSSP8	1.45	0.80	Groundwater to MSSP4	140
			Groundwater to MSSP3	140
MSW1	4.52	1.00		
MSW2	3.13	1.00		

DISCHARGE	DISCHARGE	LOCAL	TOTAL	DISCHARGE	LOCAL	TOTAL	DISCHARGE	LOCAL	TOTAL
from WRS	from ABOVE	DISCHARGE	INFLOW	from PIT	INFLOW	INFLOW	from	INFLOW	INFLOW
to MSSP1	WRS to MSSP1	to MSSP1	to MSSP1	MUDSTONE	to MSSP4	to MSSP4	HAUL ROAD	to MSSP5	to MSSP5

1000 m³/d									
15	16	17	18	19	20	21	22	23	24
1.06	2.43	0.10	3.59	0.14	0.00	0.14	0.13	0.02	0.15
1.05	2.40	0.09	3.55	0.14	0.00	0.14	0.13	0.02	0.15
0.60	1.38	0.05	2.04	0.14	0.00	0.14	0.07	0.01	0.08
0.70	1.61	0.06	2.37	0.14	0.00	0.14	0.09	0.01	0.10
0.39	0.90	0.02	1.31	0.14	0.00	0.14	0.05	0.00	0.05
0.37	0.86	0.01	1.25	0.14	0.00	0.14	0.05	0.00	0.05
0.42	0.95	0.01	1.38	0.14	0.00	0.14	0.05	0.00	0.05
0.34	0.77	0.01	1.11	0.14	0.00	0.14	0.04	0.00	0.04
0.72	1.65	0.05	2.43	0.14	0.00	0.14	0.09	0.01	0.10
1.20	2.74	0.10	4.04	0.14	0.00	0.14	0.15	0.02	0.17
1.32	3.01	0.12	4.44	0.14	0.00	0.14	0.16	0.02	0.18
1.01	2.32	0.09	3.42	0.14	0.00	0.14	0.12	0.02	0.14
0.76	1.75	0.06	2.57	0.14	0.00	0.14	0.09	0.01	0.10

15 From areas and runoff factors

24 Total of 22 and 23

16 From area and runoff factor

17 From area and runoff factor less 2/3 of potential evapotranspiration from pond

18 Total of 15 to 17

19 From area, runoff factor, and groundwater to MSSP4

20 From area and runoff factor less 2/3 of potential evapotranspiration from pond

21 Total of 19 and 20

22 From area and runoff factor

23 From area and runoff factor less 2/3 of potential evapotranspiration from pond

DISCHARGE AREA		LOCAL	DISCH from TOTAL	LOCAL	TOTAL	DISCHARGE LOCAL	TOTAL	MINE PLANT			
from M/S DUMP	from O/B DUMP	from around DISCHARGE b/wn PIT & HAUL RD	INFLOW to MSSP6	DISCHARGE INFLOW to MSW2	INFLOW to MSW2	from WRS to NORTH	DISCHARGE INFLOW to MSSP7	including MSSP8			
<-----1000 m <sup>3</sup> /d----->											
25	26	27	28	29	30	31	32	33	34	35	36
1.63	0.78	2.04	0.21	0.23	5.04	0.27	5.31	0.14	0.10	0.24	0.11
1.61	0.77	2.01	0.21	0.23	4.98	0.27	5.25	0.14	0.09	0.23	0.10
0.93	0.44	1.16	0.11	0.13	2.86	0.14	3.00	0.08	0.05	0.13	0.06
1.08	0.51	1.35	0.12	0.15	3.32	0.16	3.48	0.09	0.06	0.15	0.07
0.60	0.29	0.75	0.05	0.09	1.83	0.06	1.89	0.05	0.02	0.07	0.04
0.58	0.27	0.72	0.03	0.08	1.73	0.04	1.77	0.05	0.01	0.06	0.04
0.64	0.30	0.80	0.03	0.09	1.92	0.04	1.96	0.06	0.01	0.07	0.04
0.52	0.25	0.65	0.02	0.07	1.54	0.02	1.57	0.05	0.01	0.05	0.03
1.11	0.53	1.39	0.11	0.16	3.33	0.14	3.53	0.10	0.05	0.15	0.07
1.84	0.88	2.30	0.23	0.26	5.67	0.29	5.96	0.16	0.10	0.26	0.12
2.02	0.96	2.52	0.26	0.29	6.24	0.34	6.58	0.18	0.12	0.30	0.13
1.56	0.74	1.94	0.21	0.22	4.66	0.26	4.93	0.14	0.09	0.23	0.10
1.17	0.56	1.46	0.13	0.17	3.59	0.17	3.76	0.10	0.06	0.16	0.08

- 25 From area and runoff factor
- 26 From area and runoff factor
- 27 From area and runoff factor
- 28 From area and runoff factor less 2/3 of potential evapotranspiration from pond
- 29 From area and runoff factor
- 30 Total of 25 to 29
- 31 From area and runoff factor less 2/3 of potential evapotranspiration from pond
- 32 Total of 30 and 31
- 33 From area and runoff factor

- 34 From area and runoff factor less 2/3 of potential evapotranspiration from pond
- 35 Total of 33 and 34
- 36 From area and runoff factor

CINOLA GOLD PROJECT - MINE AREA  
WATER MANAGEMENT PLAN FOR YEAR OF WETTEST PRECIPITATION: YEAR 7

53  
Sheet 1

FILE: MINWAT7

	Catchment Area (ha)	Runoff Factor		Catchment Area (ha)	Runoff Factor
Pit (Mudstone)	0.00	0.90	WRS: 3:1 slope to south	8.50	0.98
Pit (Acid Generating)	39.25	0.90	WRS: 3:1 slope to north	2.53	0.98
			WRS: Top surface	15.30	0.90
MSSP1: WRS Runoff	1.10	1.00	WRS: Active face	5.29	1.00
MSSP2: WRS Active face	0.60	1.00	Haul Road to WRS	2.16	1.00
MSSP3: Pit - Acid Gen.	1.35	1.00	WRS to Pit & Area south	9.66	0.60
MSSP4: Pit - Mudstone	0.00	1.00	Above WRS & below Div ditch	6.77	0.80
MSSP5: Temp. Haul Road	0.20	1.00			
MSSP6: M & O	2.45	1.00	Mudstone dump	20.00	0.90
MSSP7: WRS North	1.10	1.00	Overburden dump	12.23	0.70
MSSP8: Mine Plant	0.00	1.00	Area around M/S & O/B	37.45	0.60

MONTH	DAYS	PPTN	POTENTIAL EVapo- TRANSP	DISCHARGE LOCAL		GROUNDWATER from PIT	TOTAL from PIT to MSSP3	MSSP3 to LIME TREATPLANT	DISCHARGE LOCAL		TOTAL from WRS to MSSP2	DISCHARGE INFLOW to MSSP2	DISCHARGE LOCAL		TOTAL to MSW1 DISCHARGE INFLOW to MSW1
				ACID GEN	to MSSP3				from WRS	DISCHARGE INFLOW to MSSP2			to MSSP2	to MSSP2	
1	2	3	4	5	6	7	8	9	10	11	12	13	14		
JAN	31	281	14	3.20	0.12	0.34	3.66	0.81	0.05	0.86	4.52	0.40	4.92		
FEB	28	251	16	3.17	0.12	0.34	3.62	0.80	0.05	0.85	4.47	0.39	4.86		
MAR	31	160	26	1.82	0.06	0.34	2.23	0.53	0.03	0.56	2.78	0.21	2.99		
APR	30	180	41	2.12	0.07	0.34	2.53	0.59	0.03	0.62	3.15	0.23	3.38		
MAY	31	104	66	1.19	0.03	0.34	1.55	0.40	0.01	0.42	1.97	0.09	2.05		
JUN	30	96	88	1.13	0.02	0.34	1.49	0.39	0.01	0.40	1.89	0.06	1.94		
JUL	31	110	105	1.25	0.02	0.34	1.61	0.42	0.01	0.43	2.04	0.06	2.09		
AUG	31	89	98	1.01	0.01	0.34	1.36	0.37	0.00	0.37	1.74	0.03	1.77		
SEP	30	185	71	2.18	0.06	0.34	2.58	0.60	0.03	0.63	3.21	0.21	3.42		
OCT	31	317	44	3.61	0.13	0.34	4.08	0.89	0.06	0.94	5.02	0.42	5.44		
NOV	30	337	19	3.97	0.15	0.34	4.45	0.96	0.06	1.02	5.48	0.49	5.97		
DEC	31	268	11	3.05	0.11	0.34	3.51	0.78	0.05	0.83	4.33	0.38	4.71		
MEAN		198	50	2.30	0.07	0.34	2.71	0.63	0.03	0.66	3.37	0.25	3.62		
TOTAL		2378	599												

NOTES RE COLUMNS:

- 3 From Norecol (Yakoun R data \* 18/17)
- 4 From Norecol report (Masset data)
- 5 From area and runoff factor
- 6 From area and runoff factor less 2/3 of potential evapotranspiration from pond
- 7 Groundwater to MSSP3
- 8 Total of 5 to 7
- 9 From area and runoff factor for active face, infiltration from 3:1 slopes and horizontal surface, and groundwater to WRS
- 10 From area and runoff factor
- 11 Total of 9 and 10
- 12 Total of 8 and 11
- 13 From area and runoff factor less 2/3 of potential evapotranspiration from pond
- 14 Total of 12 and 13

	Catchment Area (ha)	Runoff Factor	Quantity (m³/d)	
Between Pit & Haul Road	4.25	0.60	Groundwater to WRS	168
Mine Plant incl. MSSP8	1.45	0.80	Groundwater to MSSP4	340
			Groundwater to MSSP3	340
MSW1	4.52	1.00		
MSW2	3.13	1.00		

DISCHARGE	DISCHARGE	LOCAL	TOTAL	DISCHARGE	LOCAL	TOTAL	DISCHARGE	LOCAL	TOTAL
from WRS	from ABOVE	DISCHARGE	INFLOW	from PIT	INFLOW	INFLOW	from	INFLOW	INFLOW
to MSSP1	WRS to MSSP1	to MSSP1	to MSSP1	MUDSTONE	to MSSP4	to MSSP4	HAUL ROAD	to MSSP5	to MSSP5

<-----1000 m³/d----->									
15	16	17	18	19	20	21	22	23	24
2.23	0.49	0.10	2.82	0.34	0.00	0.34	0.20	0.02	0.21
2.20	0.49	0.09	2.78	0.34	0.00	0.34	0.19	0.02	0.21
1.27	0.22	0.05	1.60	0.34	0.00	0.34	0.11	0.01	0.12
1.47	0.32	0.06	1.86	0.34	0.00	0.34	0.13	0.01	0.14
0.82	0.18	0.02	1.03	0.34	0.00	0.34	0.07	0.00	0.08
0.79	0.17	0.01	0.97	0.34	0.00	0.34	0.07	0.00	0.07
0.87	0.19	0.01	1.08	0.34	0.00	0.34	0.08	0.00	0.08
0.71	0.16	0.01	0.87	0.34	0.00	0.34	0.06	0.00	0.06
1.52	0.33	0.05	1.90	0.34	0.00	0.34	0.13	0.01	0.14
2.51	0.55	0.10	3.17	0.34	0.00	0.34	0.22	0.02	0.24
2.76	0.61	0.12	3.49	0.34	0.00	0.34	0.24	0.02	0.26
2.12	0.47	0.09	2.69	0.34	0.00	0.34	0.19	0.02	0.20
1.60	0.35	0.06	2.01	0.34	0.00	0.34	0.14	0.01	0.15

- 15 From areas and runoff factors
- 16 From area and runoff factor
- 17 From area and runoff factor less 2/3 of potential evapotranspiration from pond
- 18 Total of 15 to 17
- 19 From area, runoff factor, and groundwater to MSSP4
- 20 From area and runoff factor less 2/3 of potential evapotranspiration from pond
- 21 Total of 19 and 20
- 22 From area and runoff factor
- 23 From area and runoff factor less 2/3 of potential evapotranspiration from pond
- 24 Total of 22 and 23

DISCHARGE AREA		LOCAL	DISCH from TOTAL	LOCAL	TOTAL	DISCHARGE LOCAL	TOTAL	MINE PLANT
from	from around	DISCHARGE btwn PIT	INFLOW	DISCHARGE INFLOW	from WRS	DISCHARGE INFLOW	including	
M/S DUMP	O/B DUMP	M/S & O/B to MSSP6	& HAUL RD	to MSSP6	to MSW2	to MSW2	to NORTH	to MSSP7 to MSSP8
<-----1000 m <sup>3</sup> /d----->								
25	26	27	28	29	30 :	31	32 :	33
1.63	0.78	2.04	0.21	0.23	5.10 :	0.27	5.38 :	0.22
1.61	0.77	2.01	0.21	0.23	5.04 :	0.27	5.31 :	0.22
0.93	0.44	1.16	0.11	0.13	2.90 :	0.14	3.04 :	0.13
1.08	0.51	1.35	0.12	0.15	3.36 :	0.16	3.52 :	0.15
0.60	0.29	0.75	0.05	0.09	1.85 :	0.06	1.91 :	0.08
0.58	0.27	0.72	0.03	0.08	1.75 :	0.04	1.79 :	0.08
0.64	0.30	0.80	0.03	0.09	1.94 :	0.04	1.98 :	0.09
0.52	0.25	0.55	0.02	0.07	1.56 :	0.02	1.59 :	0.07
1.11	0.53	1.39	0.11	0.16	3.44 :	0.14	3.58 :	0.15
1.84	0.88	2.30	0.23	0.26	5.74 :	0.29	6.03 :	0.25
2.02	0.96	2.52	0.26	0.29	6.32 :	0.34	6.66 :	0.28
1.56	0.74	1.94	0.21	0.22	4.67 :	0.26	4.93 :	0.21
1.17	0.56	1.46	0.13	0.17	3.63 :	0.17	3.80 :	0.16
								0.06
								0.22 :
								0.08 :

- 25 From area and runoff factor
- 26 From area and runoff factor
- 27 From area and runoff factor
- 28 From area and runoff factor less 2/3 of potential evapotranspiration from pond
- 29 From area and runoff factor
- 30 Total of 25 to 29
- 31 From area and runoff factor less 2/3 of potential evapotranspiration from pond
- 32 Total of 30 and 31
- 33 From area and runoff factor

- 34 From area and runoff factor less 2/3 of potential evapotranspiration from pond
- 35 Total of 33 and 34
- 36 From area and runoff factor

CINOLA GOLD PROJECT - MINE AREA  
WATER MANAGEMENT PLAN FOR YEAR OF WETTEST PRECIPITATION: YEAR 12

56  
Sheet 1

FILE: MINWAT12

	Catchment Area (ha)	Runoff Factor		Catchment Area (ha)	Runoff Factor
Pit (Mudstone)	0.00	0.90	WRS: 3:1 slope to south	25.63	0.98
Pit (Acid Generating)	41.60	0.90	WRS: 3:1 slope to north	2.53	0.98
			WRS: Top surface	14.01	0.90
MSSP1: WRS Runoff	1.10	1.00	WRS: Active face	5.25	1.00
MSSP2: WRS Active face	0.60	1.00	Haul Road to WRS	2.61	1.00
MSSP3: Pit - Acid Gen.	1.35	1.00	WRS to Pit & Area south	9.71	0.60
MSSP4: Pit - Mudstone	0.00	1.00	Above WRS & below Div ditch	0.00	0.80
MSSP5: Temp. Haul Road	0.20	1.00			
MSSP6: M & O	2.45	1.00	Mudstone dump	20.00	0.90
MSSP7: WRS North	1.10	1.00	Overburden dump	12.23	0.70
MSSP8: Mine Plant	0.00	1.00	Area around M/S & O/B	37.45	0.60

MONTH	DAYS	PPTN	POTENTIAL EVapo- TRANSP	DISCHARGE LOCAL		GROUNDWATER from PIT to MSSP3	TOTAL MSSP3	DISCHARGE LOCAL from WRS TREATPLANT	TOTAL to MSW1	DISCHARGE LOCAL to MSW1	TOTAL to MSW1		
				ACID GEN	to MSSP3								
1	2	3	4	5	6	7	8	9	10	11	12	13	14
JAN	31	281	14	3.39	0.12	0.63	4.14	0.82	0.05	0.87	5.01	0.40	5.41
FEB	28	251	16	3.36	0.12	0.63	4.10	0.81	0.05	0.87	4.96	0.39	5.35
MAR	31	160	26	1.93	0.06	0.63	2.62	0.54	0.03	0.57	3.19	0.21	3.40
APR	30	180	41	2.25	0.07	0.63	2.94	0.60	0.03	0.63	3.57	0.23	3.80
MAY	31	104	66	1.26	0.03	0.63	1.91	0.41	0.01	0.42	2.33	0.09	2.42
JUN	30	96	82	1.20	0.02	0.63	1.84	0.40	0.01	0.41	2.25	0.06	2.30
JUL	31	110	105	1.33	0.02	0.63	1.97	0.42	0.01	0.43	2.40	0.06	2.46
AUG	31	89	98	1.07	0.01	0.63	1.71	0.38	0.00	0.38	2.09	0.03	2.12
SEP	30	185	71	2.31	0.06	0.63	3.00	0.61	0.03	0.64	3.64	0.21	3.84
OCT	31	317	44	3.83	0.13	0.63	4.58	0.91	0.06	0.96	5.54	0.42	5.96
NOV	30	337	19	4.21	0.15	0.63	4.98	0.98	0.06	1.04	6.02	0.49	6.51
DEC	31	268	11	3.24	0.11	0.63	3.98	0.79	0.05	0.84	4.82	0.38	5.20
MEAN		198	50	2.44	0.07	0.63	3.14	0.64	0.03	0.67	3.81	0.25	4.05
TOTAL		2378	599										

NOTES RE COLUMNS:

- 3 From Norecol (Yakoun R data # 18/17)
- 4 From Norecol report (Masset data)
- 5 From area and runoff factor
- 6 From area and runoff factor less 2/3 of potential evapotranspiration from pond
- 7 Groundwater to MSSP3
- 8 Total of 5 to 7
- 9 From area and runoff factor for active face, infiltration from 3:1 slopes and horizontal surface, and groundwater to WRS
- 10 From area and runoff factor
- 11 Total of 9 and 10

- 12 Total of 8 and 11
- 13 From area and runoff factor less 2/3 of potential evapotranspiration from pond
- 14 Total of 12 and 13

	Catchment Area (ha)	Runoff Factor	Quantity (m³/d)	
Between Pit & Haul Road	4.25	0.60	Groundwater to WRS	168
Mine Plant incl. MSSP8	1.45	0.80	Groundwater to MSSP4	625
			Groundwater to MSSP3	625
MSW1	4.52	1.00		
MSW2	3.13	1.00		

DISCHARGE from WRS	DISCHARGE from ABOVE	LOCAL DISCHARGE	TOTAL INFLOW	DISCHARGE from PIT	LOCAL INFLOW	TOTAL INFLOW	DISCHARGE from MUDSTONE	LOCAL INFLOW	TOTAL INFLOW
to MSSP1	WRS to MSSP1	to MSSP1	to MSSP1	to MSSP4	to MSSP4	to MSSP5	HAUL ROAD to MSSP5	to MSSP5	to MSSP5
<-----1000 m³/d----->									
15	16	17	18	19	20	21	22	23	24
3.64	0.00	0.10	3.74	0.63	0.00	0.63	0.24	0.02	0.25
3.60	0.00	0.09	3.70	0.63	0.00	0.63	0.23	0.02	0.25
2.08	0.00	0.05	2.13	0.63	0.00	0.63	0.13	0.01	0.14
2.41	0.00	0.06	2.47	0.63	0.00	0.63	0.16	0.01	0.17
1.35	0.00	0.02	1.37	0.63	0.00	0.63	0.09	0.00	0.09
1.29	0.00	0.01	1.30	0.63	0.00	0.63	0.08	0.00	0.09
1.43	0.00	0.01	1.44	0.63	0.00	0.63	0.09	0.00	0.10
1.15	0.00	0.01	1.16	0.63	0.00	0.63	0.07	0.00	0.08
2.48	0.00	0.05	2.53	0.63	0.00	0.63	0.16	0.01	0.17
4.11	0.00	0.10	4.21	0.63	0.00	0.63	0.27	0.02	0.29
4.52	0.00	0.12	4.64	0.63	0.00	0.63	0.29	0.02	0.31
3.48	0.00	0.09	3.57	0.63	0.00	0.63	0.23	0.02	0.24
2.62	0.00	0.06	2.68	0.63	0.00	0.63	0.17	0.01	0.18

- 15 From areas and runoff factors  
 16 From area and runoff factor  
 17 From area and runoff factor less 2/3 of potential evapotranspiration from pond  
 18 Total of 15 to 17  
 19 From area, runoff factor, and groundwater to MSSP4  
 20 From area and runoff factor less 2/3 of potential evapotranspiration from pond  
 21 Total of 19 and 20  
 22 From area and runoff factor  
 23 From area and runoff factor less 2/3 of potential evapotranspiration from pond
- 24 Total of 22 and 23

DISCHARGE AREA		LOCAL	DISCH from TOTAL	LOCAL	TOTAL	DISCHARGE LOCAL	TOTAL	MINE PLANT			
from M/S DUMP	from O/B DUMP	from around M/S & O/B	DISCHARGE b/wn PIT & HAUL RD	INFLOW to MSSP6	DISCHARGE INFLOW to MSW2	INFLOW from WRS to MSW2	DISCHARGE INFLOW to NORTH	including MSSP7 to MSSP8			
<-----1000 m <sup>3</sup> /d----->											
25	26	27	28	29	30 :	31	32 :	33	34	35 :	36 :
1.63	0.78	2.04	0.21	0.23	5.14 :	0.27	5.42 :	0.22	0.10	0.32 :	0.11 :
1.51	0.77	2.01	0.21	0.23	5.09 :	0.27	5.35 :	0.22	0.09	0.32 :	0.10 :
0.93	0.44	1.16	0.11	0.13	2.92 :	0.14	3.06 :	0.13	0.05	0.18 :	0.06 :
1.08	0.51	1.35	0.12	0.15	3.39 :	0.16	3.55 :	0.15	0.06	0.20 :	0.07 :
0.60	0.29	0.75	0.05	0.09	1.87 :	0.06	1.93 :	0.08	0.02	0.10 :	0.04 :
0.58	0.27	0.72	0.03	0.08	1.77 :	0.04	1.81 :	0.08	0.01	0.09 :	0.04 :
0.64	0.30	0.80	0.03	0.09	1.96 :	0.04	2.00 :	0.09	0.01	0.10 :	0.04 :
0.52	0.25	0.65	0.02	0.07	1.58 :	0.02	1.60 :	0.07	0.01	0.08 :	0.03 :
1.11	0.53	1.39	0.11	0.16	3.46 :	0.14	3.61 :	0.15	0.05	0.20 :	0.07 :
1.84	0.88	2.30	0.23	0.26	5.79 :	0.29	6.08 :	0.25	0.10	0.36 :	0.12 :
2.02	0.96	2.52	0.26	0.29	6.37 :	0.34	6.71 :	0.28	0.12	0.40 :	0.13 :
1.56	0.74	1.94	0.21	0.22	4.67 :	0.26	4.93 :	0.21	0.09	0.31 :	0.10 :
1.17	0.56	1.46	0.13	0.17	3.65 :	0.17	3.82 :	0.16	0.06	0.22 :	0.08 :

25 From area and runoff factor  
 26 From area and runoff factor  
 27 From area and runoff factor  
 28 From area and runoff factor less 2/3 of potential evapotranspiration from pond  
 29 From area and runoff factor  
 30 Total of 25 to 29  
 31 From area and runoff factor less 2/3 of potential evapotranspiration from pond  
 32 Total of 30 and 31  
 33 From area and runoff factor

34 From area and runoff factor less 2/3 of potential evapotranspiration from pond  
 35 Total of 33 and 34  
 36 From area and runoff factor

**APPENDIX 6.2.3-1**

**COMMENTARY FROM ENVIRONMENT CANADA  
ON MERCURY / NUTRIENTS**

**(Pages 1 to 2)**

NOTES  
CINOLA Hg/NUTRIENTS

- 1. The-concept/theory-of-Biodilution. Still have some problems with this concept. Jernelov et al offers no evidence of this in their paper. The theory that organisms in oligotrophic lakes tend to have higher Hg levels than organisms in eutrophic lakes could be due to biodilution, could also be due to some other phenomenon such as reduced availability of mercury under eutrophic conditions owing to production of sulphides and organic chelators.

Advice given to me is that Hecky et al in their limnoco<sup>r</sup>ral experiments in Southern Indian Lake, found that doubling the primary productivity had no effect on either the uptake of mercury by fish or on the growth of the fish. This does not necessarily constitute evidence of biodilution, for biodilution would of been accompanied by an increase in the growth rate of fish. Also I understand that the report does not claim that biodilution was involved!

Again, advice given to me re Rudd and Turner's experiment performed in limnoco<sup>r</sup>als with water-tight plastic bottoms installed in Clay Lake found that increasing the primary productivity 4X or 9X caused a substantial net increase in the mercury content of fish muscle. The authors concluded that enhancement of productivity increased both the rate of mercury methyl production (because of increased microbial activity) and the biodilution of mercury (because of increased fish growth), and that the effect of increased methyl mercury production far exceeded the opposing effect of biodilution. Thus, their conclusions are in direct opposition to the biodilution concept.

Jackson 1988 (Can. Jour. Fish. Aquat. Sci. 45: 1744-1757) found evidence that biodilution does does not play a significant role.

- 2. Availability-of-Mercury-(especially-inert-inorganic-cinnabar).

The concerns about increased inorganic mercury mobilisation are dismissed on the grounds that cinnabar, the source of mercury, is relatively insoluble and unreactive. This could still be open to some question. For instance in Rudd and Turner's experiments there were major increases in nutrient levels and primary production and only a trace of mercury was added (as radioactive Hg-203); yet the result was a net increase in the accumulation of mercury by fish. Moreover, cinnabar, though very insoluble and relatively stable to oxidation, does have a finite solubility and undergo oxidation (e.g. by trivalent iron in acid mine waters) to the more soluble mercuric sulphate. (As what could be happening now to cause the elevated Hg levels at the Cinola site). Consequently, some increase in the pool of potentially available inorganic mercury is likely in the event that mining causes an increase in the cinnabar particles into the environment. The amount may be small compared with the amounts in a heavily polluted body of water, but experience with the polluted reservoirs in Northern Manitoba has shown that it does not take much mercury to create a problem if the conditions are right for a rise in the rates of mercury methylation and bio-accumulation. Even without an increase in the abundance of

inorganic mercury, the enhanced primary production could cause an increase in methyl mercury production; the mercury from the cinnabar would simply enhance this increase.

3. A contingency plan:

In order to give approval of the mine, a contingency plan has to be developed as to what to do if mercury methylation does occur once mining begins.

**APPENDIX 7.2.2-1**

**FERGUSON BAY DOCK IMPACTS AND COMPENSATION  
HAY & COMPANY RESPONSE**

**(Pages 1 to 3)**

RECEIVED MAY 26 1989

**HAY & COMPANY**

**CONSULTANTS INC.**

May 24, 1989

File : NORE.02

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Norecol Environmental Consultants Ltd.  
Suite 700, 1090 West Pender Street  
Vancouver, B.C.  
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Attention : Ms. E. M. Neil

Dear Ms. Neil

Re: Ferguson Bay Dock Site

In reference to our recent meeting on the physical impacts and compensation potential for the above project, this letter presents our opinion and comments as requested.

The following comments are made on the basis of a review of existing data as no site visit was undertaken by Hay & Company. The data reviewed, included an air photo (BC86114 # 010), a plan showing marine vegetation zones (Norecol 1989), underwater photos inside and outside the bay (Norecol), panorama photos taken from the existing breakwater looking north and east across the eelgrass bed and along the adjacent shoreline (Norecol), plan showing bathymetric contours and the existing breakwater (Taylor Peach), and a substrate and biological survey of Ferguson Bay (MacMillan Bloedel, 1978).

Investigations by Taylor Peach (designers of the new facility) through discussions with locals and MacMillan Bloedel indicate that winds and waves approach the site from a variety of directions with some predominance from the north. Major winds around the Queen Charlotte Islands are southeast along Hecate Strait and westerly through Dixon Entrance. Overland winds are affected by local topography such as the mountains to the west and the north-south axis of Masset Sound. These topographic features will have an effect on wave directions at the site. In addition arctic outflow winds, which occur primarily during the winter, will cross Hecate Strait from the Skeena valley and generate waves across Masset Inlet approaching the site from the east.

There are no definite indications of predominance in coastal processes as indicated by the geomorphic features shown in the air photo. The influence of the tidal flows through Juskatla

Narrows to the west of Ferguson Bay is evident in the alignment of bars and spits, and the development of the Yakoun River delta is evident to the east. There is little evidence of recent shoreline development between Ferguson Bay and Yakoun Bay.

A narrow tidal shelf runs between the Yakoun River delta and the east side of the existing breakwater at the site. The air photo indicates the shelf to be approximately uniform in width except against the breakwater where it widens. No distinctive shelf is evident in the air photo to the west of the breakwater. The change in the width of the shelf is also borne out in the surveyed contours, Figure 1.

The reasons for the wider shelf on the east side of the breakwater are not evident in the data reviewed. The portion of the shelf exposed in the panorama photos appears quite stable with a heavy armouring of cobble and boulder although some minor erosion of the low backshore escarpment is evident in the fallen trees. The breakwater has been in place for at least 10 years and any significant littoral drift would be seen in either accretion or erosion of the upper foreshore at the root of the structure.

A layer of fine sediments appears on the surface in the sub-tidal zone as seen in the underwater photos and documented in the substrate and biological survey of 1978. Such sediments settling out from the water column can be expected in a large inlet where tidal velocities are low and should not present any physical constraints on compensation development.

With little source of sediments for shoreline development between Ferguson and Yakoun bays, it appears the wider shelf at the breakwater may have existed prior to construction or have developed through backshore erosion in response to the presence of the structure. In any event the present equilibrium of the foreshore east of the breakwater would indicate an opportunity for extending the existing eelgrass bed by excavating into the inter-tidal shelf at the appropriate elevation.

A more detailed study than this overview is recommended to confirm the potential for extending the existing eelgrass bed, or creating additional beds along the foreshore east of the breakwater. The elevation of the beds are not precisely known, the scope for such development may not exist where the shelf is narrow, and any change to the shelf may impact the adjacent backshore until a new state of equilibrium exists.

We would be pleased to visit the site to more closely examine the physical conditions and discuss compensation potential with Fisheries and Oceans. We have undertaken similar compensation projects and are known to the Fisheries and Oceans staff at Prince Rupert.

We trust this brief overview of site conditions meets your present needs and if there are any further queries, please call.

Yours very truly,

HAY & COMPANY CONSULTANTS INC.

A handwritten signature in black ink, appearing to read "D.D. McConnell".

D.D. McConnell, P.Eng.

DMc/  
encl.

FERGUSON  
BAY

EXISTING BREAKWATER

TOE OF RIPRAP

EELGRASS

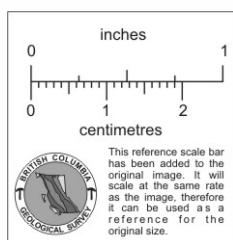
LAMINARIA

MASSET INLET

AREA FOR  
POTENTIAL  
COMPENSATION

IIWL

EDGE of TIDAL SHELF  
(air photo)



HAY & COMPANY CONSULTANTS INC.  
HORECOL

FIG.  
1

FERGUSON BAY BREAKWATER  
SITE PLAN