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GEOLOGY  
AND  
ECONOMIC POTENTIAL  
OF THE  
BEAR PROJECT

ALBERNI MINING DIVISION  
BRITISH COLUMBIA

FOR

INTERNATIONAL COAST MINERALS CORPORATION

1500 - 1176 West Georgia Street  
Vancouver, British Columbia

PROPERTY FILE

R.Tim Henneberry, FGAC  
July 9, 1987

## SUMMARY

International Coast Minerals Corporation has clear title to 4 reverted crown grants and 1 staked fraction in the Alberni Mining Division, known as the Bear Property, lying in the historic Kennedy River Gold District. The Bear Property hosts the Bear Fault, a 4 kilometre shear zone hosting auriferous quartz veins. Previous exploration and development has been concentrated on a 200 metre strike length of this fault. Consistent gold values (27 metres at 0.311 ounces per ton gold over 1 metre width) have been defined in the "Footwall Vein" within a short 60 metre section of the Bear Fault. The ore shoot is defined both on surface and in the Subway Adit driven in 1913.

An exploration program consisting of detailed mapping and sampling in the showing area, combined with a property wide geophysical and geochemical survey was completed in June, 1987. The strike extension of the Bear Shear Zone was successfully traced by both surveys. The "Black Vein" appears to lie on the hanging wall of the Bear Shear Zone.

Additional exploration targets have also been identified, including the "stockwork showing" located 150 metres east of the adit portal along the strike projection of the Bear Fault and the Mine Fault, a 45 kilometre regional fault from which the Bear Fault originates.

An exploration program consisting of surface trenching, diamond drilling and level development is recommended for the Bear Property. Estimated cost is 1.43 million dollars.

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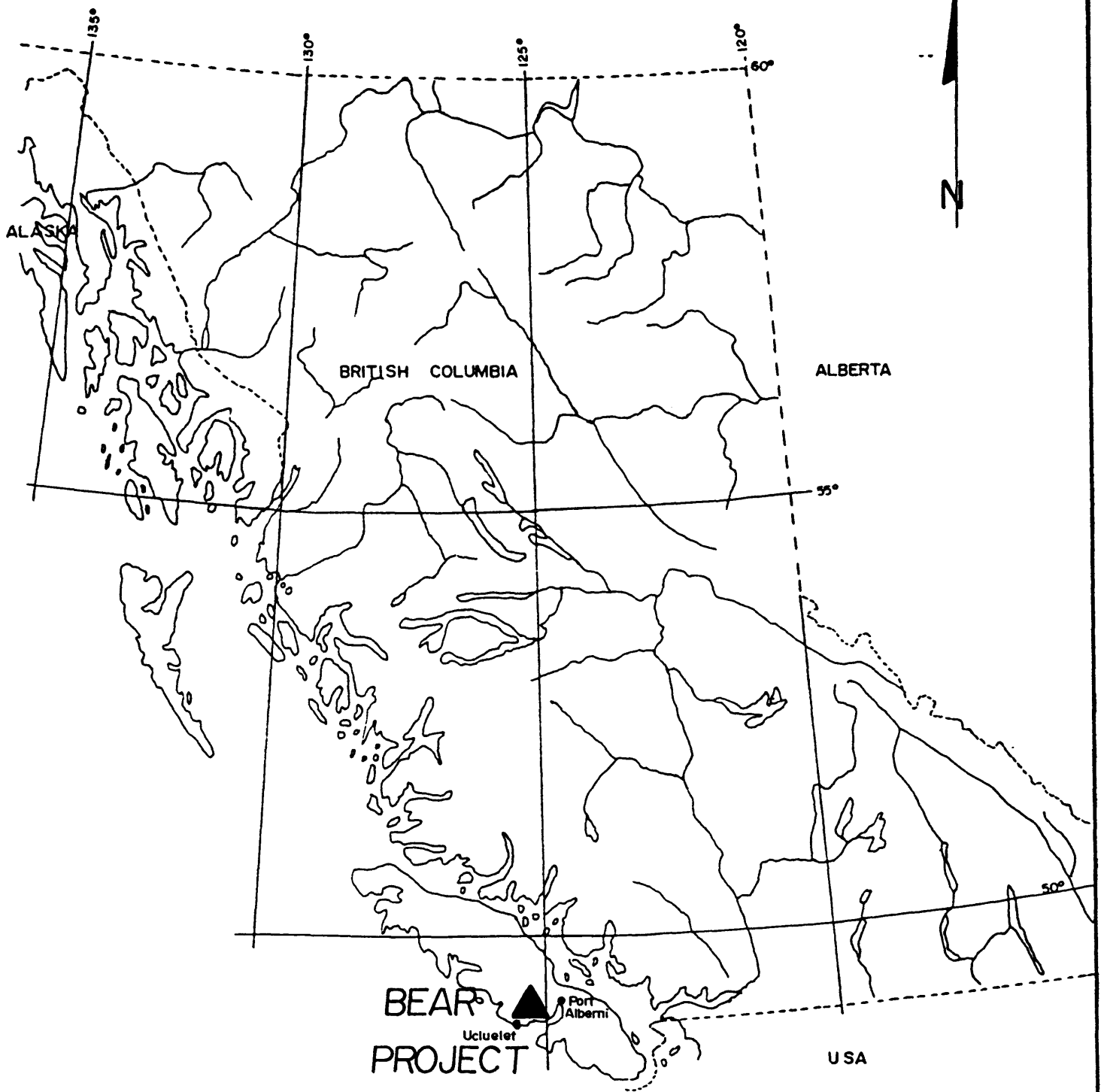
## INTRODUCTION

The Bear Property, consisting of 4 reverted crown grants and one staked fraction, lies within the Kennedy River District of Vancouver Island. The Kennedy River District has been intermittently active since the initial discovery of gold at the turn of the century. Exploration activity hit a peak in the early 1980's and rapidly declined.

Kerr Addison Mines is presently conducting a large scale exploration program in the district. One of their major projects is the Tommy Property, directly across Kennedy River from the Bear Property, optioned from International Coast Minerals Corporation. Kerr Addison can earn a 60 percent interest by spending 1.75 million dollars on the property, including drilling 2000 metres before October, 1987. The diamond drilling commenced July 6, 1987. Kerr Addison has additional property under option in the district. Multinational Resources in a joint venture with Teck has been exploring the Au claims 3 kilometres southeast of the Bear. Lesser groups and individuals hold much of the remaining property.

The purpose of this report is to compile the existing data on the Bear Property in an effort to direct an exploration program to outline sufficient tonnage to bring the Bear Property to production. The initial goal is to locate 100 to 150 thousand tons at 0.3 to 0.7 ounces per ton gold. At a production rate of 100 to 150 tons per day at least three years of life would be sustained.





ICM CORP

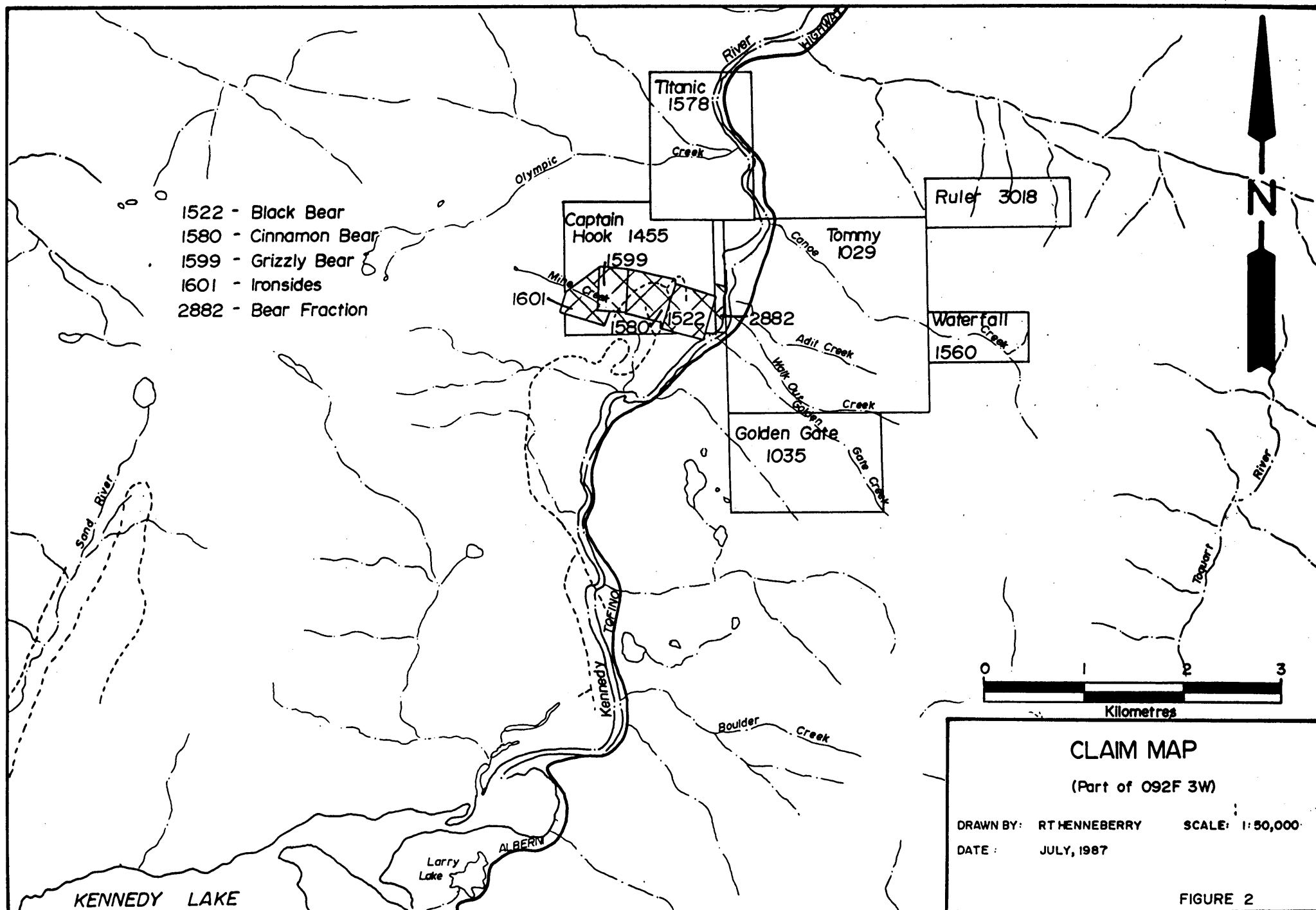
## PROPERTY LOCATION

|            |               |            |  |
|------------|---------------|------------|--|
| DR. BY:    | RT HENNEBERRY | SCALE:     |  |
| DATE:      | JULY, 1987    | APPRD. BY: |  |
| CHK'D. BY: |               | REV.:      |  |
| DWG. NO.   |               | FIGURE 1   |  |

## LOCATION, ACCESS

The Bear Property lies within the Alberni Mining Division of Vancouver Island. The property is located 55 road kilometres west of Port Alberni and 30 road kilometres northeast of Ucluelet (Figure 1). A new logging road extends from the Alberni-Tofino Highway to the southern part of the property. Topography ranges from 40 to 440 metres above sea level. Precipitous cliffs are found on the western half of the claims. The Kennedy River Valley receives very little snow at lower elevations, allowing work to continue year round.

The lower (southern) section of the claim group was logged during the last year. A large part of the northern section is in an active timber lease, due to be logged later this year. New logging roads will provide access to the remainder of the claim group. Water for diamond drilling is available from Kennedy River, bordering the eastern end of the property. A hydro-electric power line runs along the Alberni-Tofino Highway.



## OWNERSHIP

The Bear Project consists of 4 reverted crown grants and one staked fraction totaling approximately 71 hectares (Figure 2). All claims are owned outright by International Coast Minerals Corporation of Vancouver.

| Claim Name    | Lot No. | Record No. | Expiry Date    |
|---------------|---------|------------|----------------|
| Black Bear    | 293     | 1522       | January, 1989  |
| Cinnamon Bear | 294     | 1580       | December, 1995 |
| Grizzly Bear  | 300     | 1599       | January, 1996  |
| Ironsides     | 487     | 1601       | January, 1990  |
| Bear Fraction |         | 2882       | April, 1988    |

## PREVIOUS EXPLORATION

Gold was initially discovered in the Kennedy River District at the turn of the century. Quartz veins associated with the Bear Shear Zone were discovered in Bear Creek in 1902. During the period from 1902 to 1913 all of the development work was completed. The shear zone hosting the quartz veins was traced approximately 130 metres on surface, predominantly in Bear Creek. A tunnel (the Subway Adit) was driven 62 metres along a strong 90 to 120 centimetre wide quartz vein ("Footwall Vein") on the footwall contact of the Bear Shear Zone. (Ministry of Mines Annual Report, 1916).

The property changed hands several times before being obtained by W.W. Ejtel of Vancouver, in the early 1980's. Mr. Ejtel relocated the Subway Adit and had several major companies examine the showings. A brief summary of each examination follows. Sampling information may be found in Appendix A. This sampling information has been incorporated into the plans and sections.

Teck Explorations Limited examined the Bear showings in the immediate vicinity of the Subway Adit in August, 1984 (Groves, 1985). Significant gold values were obtained from 4 of the 5 samples taken, with values as high as 0.677 ounces per ton gold over 2.13 metres. Of particular interest was the presence of considerable gold (0.220 ounces per over 0.61 metres) in the hosting sheared volcanics between the main footwall vein and a hanging wall splay.

Dr. Bill Groves examined the showings in May, 1985 on behalf of the owner (Groves, 1985). He verified the Teck results and did additional sampling along strike to the east of the showings. Trenching by the owner located a granitic intrusive hosting concentrated sheeted veinlet zones ("Stockwork showing") within and in both the footwall and hanging wall of the Bear Shear Zone. Significant gold values were obtained from 5 selected veinlet grab samples. The best value obtained was 0.802 ounces per ton and the 5 samples averaged 0.416 ounces per ton.

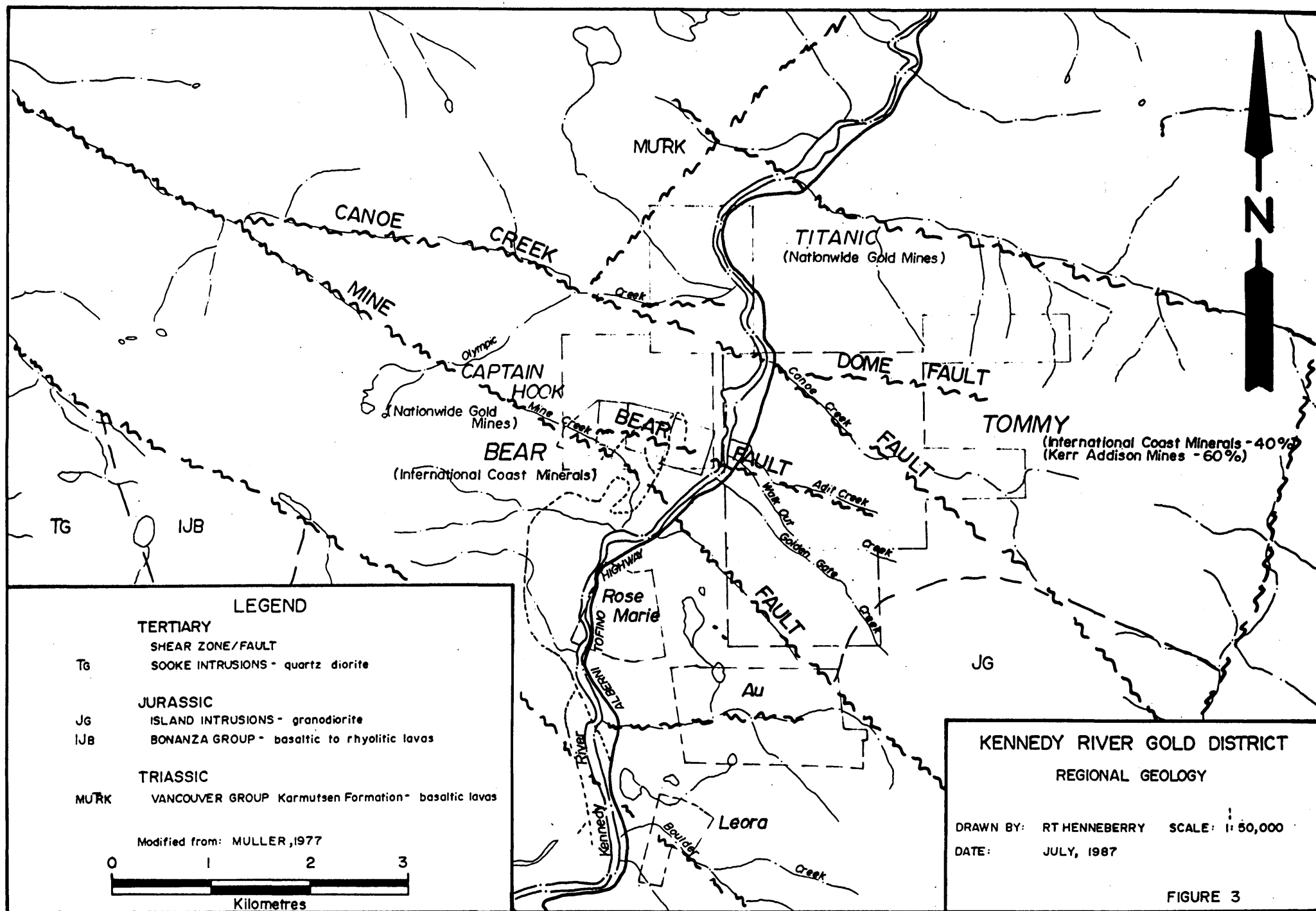
J.N. Helsen of Noranda Exploration Company Limited examined the claims in September, 1985 (Helsen, 1985). This examination, considerably more detailed than the property had previously received, included surface sampling from all exposures, and a soil geochemical line immediately west of the "Black Vein" outcrop exposure. Sampling again verified the original Teck data in the showing area. The newly discovered "Black Vein" approximately 150 metres west of the showing, but within the Bear Shear Zone was sampled. Results were 0.940 ounces per ton gold across 2.9 metres. The soil line located one anomalous value of 50 parts per billion gold likely highlighting the "Black Vein".

A VLF-EM survey was carried out by the owner in late 1985 (Ejtel, 1986). The geophysical grid was laid out from the "Stockwork showing" to the west of the "Black Vein". The Bear Shear Zone exhibited consistently anomalous values through the section tested.

Paul Wilton, the provincial government district geologist, examined the "Black Vein" in late 1985 (Wilton, 1987). His channel sampling yielded 1.23 ounces per ton gold over 2.74 metres. A 0.49 metre width assayed 7.42 ounces per ton.

R. Brown of Lac Minerals inspected the showings in January, 1986 (Brown, 1986). Brown's sampling results confirmed the results obtained by the earlier parties.

L. Goldsmith sampled the "Black Vein" and the main showing vein on surface in June, 1986 (Goldsmith, 1986). Again results duplicated previous sampling. A bulk sample of 4.82 tons was taken from the "Black Vein" and shipped to the Cominco Smelter in Trail. Although samples taken from the outcrop exposure averaged in excess of 1 ounce per ton gold, Cominco's sample returned only 0.280 ounces per ton gold ?



## REGIONAL GEOLOGY

The Kennedy River District lies within a structurally active section of Vancouver Island (Figure 3). Rocks of the Vancouver and Bonanza Groups are intruded by Island and Sooke intrusions. Gold mineralization is predominantly localized by west-northwest trending fault/shear zones, active during Tertiary time. (Muller and Carson, 1968).

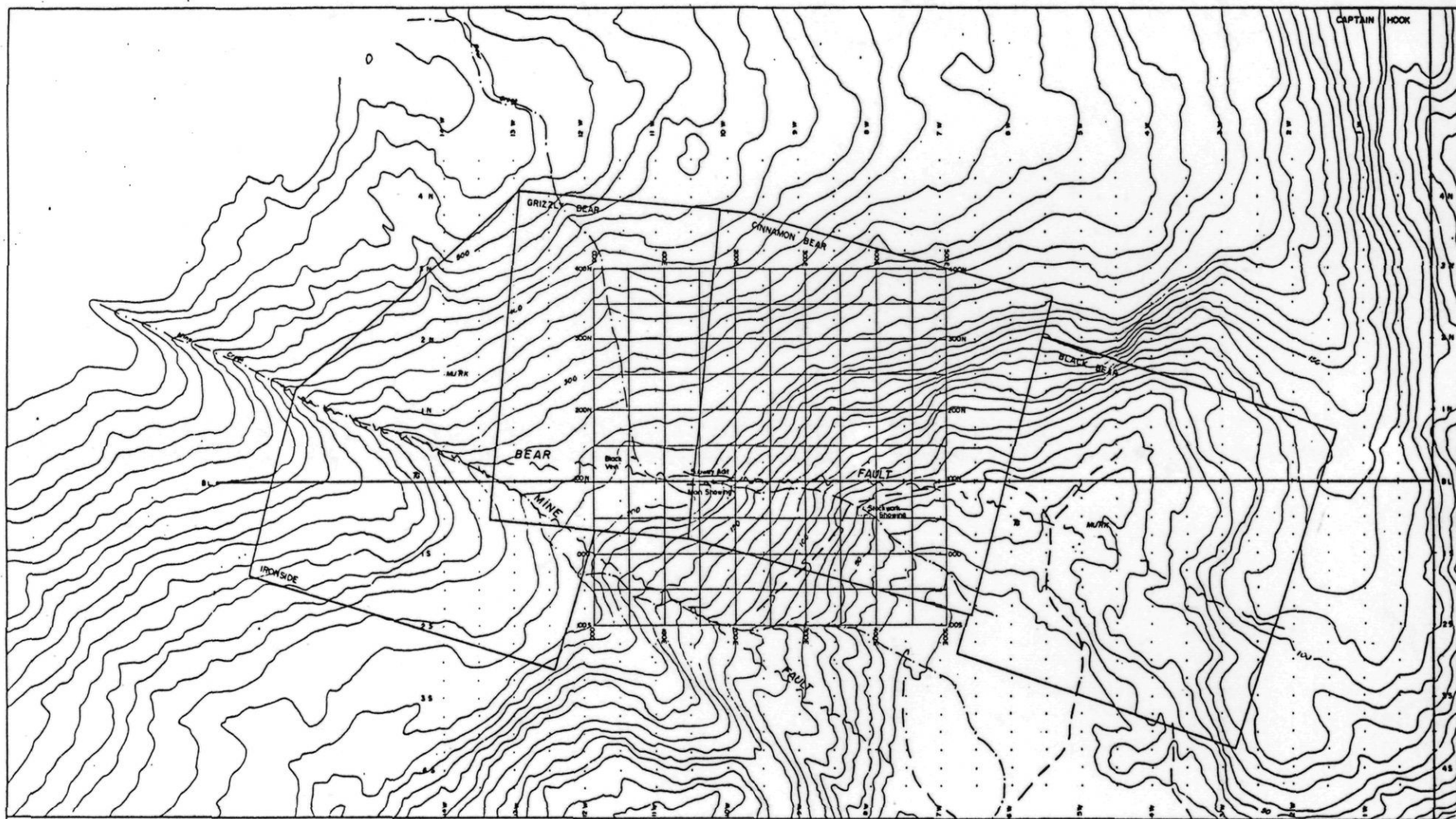
The Karmutsen and Quatsino Formations comprise the Triassic Vancouver Group outcroppings in the district. Andesitic to basaltic flows, tuffs and volcaniclastics of the Karmutsen Formation are overlain by massive limestone of the Quatsino Formation. Alteration is generally greenschist facies, though the limestone can be marbled near intrusive contacts. Jurassic Bonanza Group andesitic to latitic flows, tuffs and breccias overlie the Vancouver Group rocks.

Two periods of intrusive activity have been documented in the district. The Jurassic Island Intrusions are mainly of granodioritic to quartz dioritic composition. Contacts with Karmutsen rocks are generally sharp and well-defined. Tertiary Sooke Intrusions of predominantly quartz diorite composition consist of small stocks (less than 2 kilometres), dykes and sills outcropping throughout the district. Contacts with older rocks can be either sharp or sheared. Muller and Carson (1968) speculate that several smaller Tertiary stocks are present within the Kennedy River District.

West-northwesterly to westerly trending faults of Tertiary age cut the rock units in the district, indicating a period of intense structural activity. Gold mineralization is predominantly localized within these structures, suggesting a Tertiary age for the mineralization. Muller's (1977) map of Vancouver Island indicates several divergent and cross faults within the Kennedy River District. This structural setting is similar to the setting of the important epithermal gold districts of the southwestern United States (Buchanan, 1981).

Several showings have definite shear zone associations in the Kennedy River District including: Tommy K, Leora, Rose Marie, Au and the Bear. The Tommy K is of particular interest because International Coast Minerals Corporation has a 40 percent interest, with the operator, Kerr Addison Mines, earning their 60 percent interest by spending 1.75 million dollars. Exploration is ongoing on most of these projects and the reader is referred to Annual Government Reports and Assessment Reports for further information.





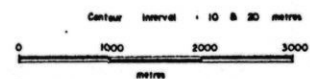
# LEGEND

## TERTIARY

- SHEAR ZONE / FAULT
- BOCKE INTRUSIONS
- QUARTZ DIORITE

## TRIASSIC

- VANCOUVER GROUP
- KARMUTSEN FORMATION ANDESITIC LAVAS



INTERNATIONAL COAST MINERALS CORPORATION

## BEAR PROJECT SURFACE GEOLOGY

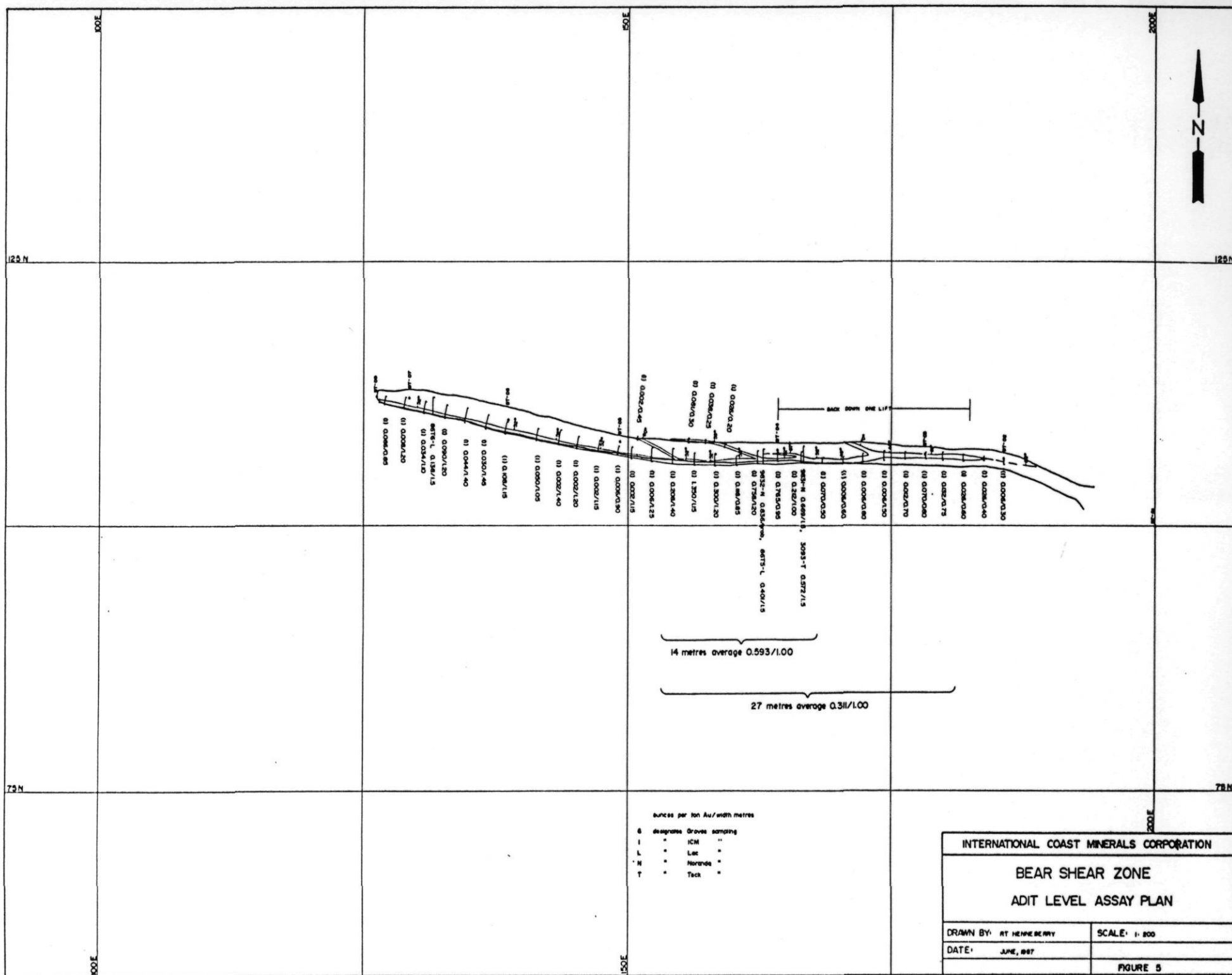
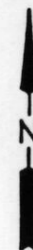
|                         |              |
|-------------------------|--------------|
| DRN BY: R. T. HENDERSON | SCALE 1:2500 |
| DATE: July 1967         |              |
|                         | FIGURE 4     |

## PROPERTY GEOLOGY

The dominant geological feature on the Bear Property is the Mine Fault traceable for approximately 45 kilometres from Alberni Inlet through to Tofino Inlet (Figure 4). The Bear Shear Zone is a splay fault traceable from its junction point approximately 4 kilometres to the southeast. The long axis of the Bear Property covers a strike length of approximately 2 kilometres along the Bear Shear Zone from the junction point southeast. A small section of the Mine Fault strikes across the claim group.

The Bear Shear Zone forms the contact between Karmutsen andesites and a quartz diorite of suspected Tertiary age. Both rock units are well brecciated proximal to the Shear Zone. Quartz veinlet swarms infill the brecciated wall rock within a 100 metre halo of the Shear Zone. Karmutsen alteration consists predominantly of fracture and groundmass chlorite. Within the Shear Zone itself the volcanics are intensely brecciated and locally silicified. Clay alteration of feldspar and fracture chlorite form the quartz diorite alteration assemblage within the Shear Zone halo. Groundmass chlorite and silicification mark the intrusive within the Shear Zone itself.

The primary exploration target is auriferous quartz veins within the Bear Shear Zone. Significant gold values have also been obtained from the stockworks associated with the footwall and hanging wall of the Shear Zone, predominantly to the east of the quartz veins. To date the exploration program has been confined to a 200 metre section of the Bear Fault, containing the adit and surface trenches. The Mine Fault has yet to be explored.



## 1987 PROGRAM

A detailed exploration program was undertaken during May and June. The Bear Shear Zone was surveyed, mapped and sampled, both on surface and underground. A grid was established over the entire property to allow completion of a geochemical and geophysical survey. These surveys were directed at testing for strike extensions and testing for parallel and splay footwall and hanging wall structures. A base line of 1400 metres was cut at 270 degrees. Flagged cross lines were established at 50 metre intervals along the base line. Sample stations were established at 25 metre intervals along the cross lines.

### Bear Shear Zone

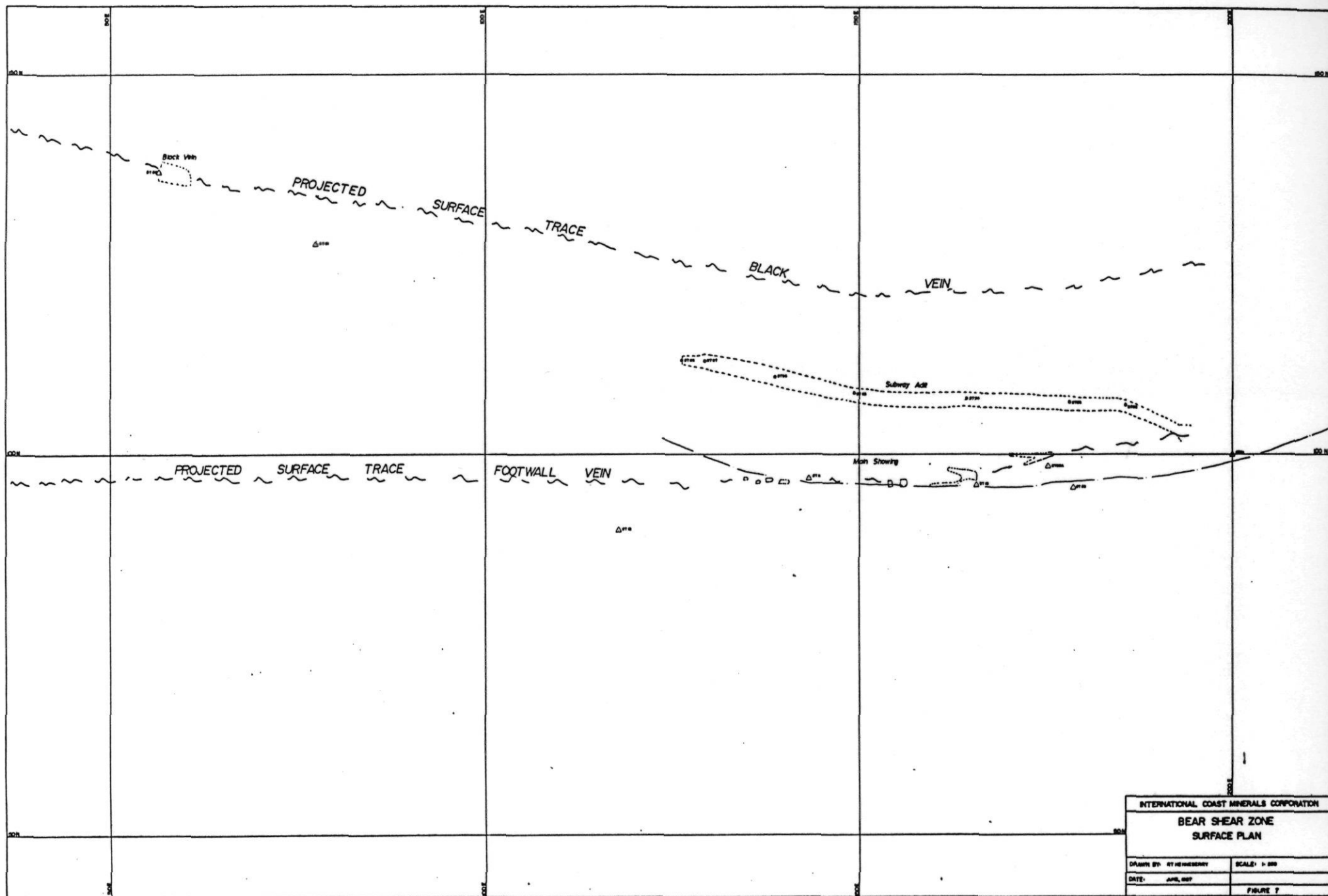
Previous examinations of the showing area had for the most part concentrated of sampling identical locations on the veins to verify earlier results. The high grade gold values obtained were for the most part duplicatable, but most of the exposed strike lengths of the veins remained unsampled. A detailed sampling program was required to ascertain mineralized shoot geometry. A survey was required to tie the surface and underground workings together to allow the compilation of proper plans and sections.

A total of 15 survey points were established, 7 underground and 8 on surface. An arbitrary origin was chosen with the mine grid laid out parallel and perpendicular to the Bear Shear Zone, which in this case is due north and due east. Mine elevation 200 metres is actually 180 metres above sea level. The survey was conducted by Bob Potter, P.Eng. of Kerr Addison Mines. A surface and an underground plan map were drawn for mapping and sampling the showing area.

The adit level (200 Level) was mapped at a scale of 1:200, and sampled at 2 metre intervals throughout its entire length (Figure 5). The Subway Adit is collared as a cross cut, picking up the footwall of the shear zone ("Footwall Vein") 7 metres from the portal. A definite vein channel is followed to the face, pinching and swelling between 10 and 150 centimetres. A quartz vein pinches and swells irregularly within the vein channel. Sheared and altered volcanics fill the remaining space in the channel. Four hanging wall splays were mapped within a strike length of 27 metres. Although gold values were obtained throughout the drift, the best zone is associated with splay veins. A mineralized shoot of 27 metres strike length averages 0.311 ounces per ton gold over 1.00 metres width. A higher grade zone of 12 metres averages 0.593 ounces per ton gold over a 1.00 metre width.

Surface was mapped at 1:200 and sampled at 2 metre spacings, where possible (Figure 6). Bear Creek actually flows over the exposure of the footwall of the zone on surface. The "Footwall Vein" outcrops intermittently over a strike length of 45 metres, from the point where it appears from the north wall 25 metres west of the portal to a point where it disappears under considerable overburden cover to the west. The footwall contact is sharply defined and traceable through the entire length of the





exposure. Two hanging wall splays were mapped, correlating with two of the splays mapped in the adit. Significant gold mineralization was located in the sheared volcanic rock between the footwall vein and the western hanging wall splay. Noranda tested this zone and found the grade decreases noticeably with distance from the junction point. Appreciable gold occurs within 5 metres of the junction point. A mineralized shoot has not been defined on surface, because the sample density is not strong enough, due to the discontinuous surface outcropping. The completed sampling indicates that a mineralized shoot will be outlined once sample spacing can be closed. Recent hand-trenching to the west has continued to uncover quartz along the footwall of the zone. Overburden depths are now in the order of 3 to 4 metres, necessitating mechanical removal methods.

Mineralization consists of sulfides, predominantly pyrite and pyrrhotite. Gold is intimately associated with the sulfides. Gold is not always present whenever sulfides are noted, though vein sulfides assay gold 90 percent of the time. Gold does not assay if sulfides are not present.

The "Black Vein" lies 75 metres northwest from the western end of the surface exposure (Figure 7). Considerable gold assays have been obtained from this exposure. Massive pyrrhotite with 5 to 10 percent sphalerite are present in the vein. The projected strike extension of the "Footwall Vein" lies approximately 25 to 35 metres in the footwall of the "Black Vein" suggesting this vein may be a parallel structure. Recently completed geochemical and geophysical surveys successfully traced the "Black Vein" to a point 30 to 40 metres west of the main showing workings.

A zone of quartz veinlets and stringers ("Stockwork showing") outcrops approximately 250 metres east of the portal. Economic gold values were obtained from several of the stringers, within the Bear Fault (see Groves sampling data - Appendix A). The recently completely logging has completely covered this showing. Mechanical equipment will be required to re-open this zone for mapping and detailed sampling purposes.

#### Soil Geochemistry

A geochemical survey was conducted over the established grid. 390 of a possible 1073 samples were taken. The precipitous terrain, combined with a surprisingly thick humus layer accounted for the small number of samples recovered. Samples were analyzed for Au, Ag, As, Cu, Zn and Fe. Details of lab procedures are appended with the actual lab reports in Appendix B.

Responses from the Au geochemistry are extremely encouraging (Figure 8a). The "Footwall Vein" yielded anomalous gold values discontinuously through its entire property length (Anomaly A). The "Black Vein" appears to be traceable from lines 1350W to 750W (Anomaly B). A linear anomaly (Anomaly D) runs from line 1200W to line 1300W between 150N and 175N. A large cluster of anomalous values lies between lines 450W and 950W between 150S and 325S (Anomaly C). This anomaly may be a stockwork zone in the footwall of the Bear Shear Zone, the continuation of the "Stockwork showing", centred on line 850W - 100S. Additional spot anomalies are found throughout the grid area. These anomalies should also be investigated.

Silver responses did not exceed background (Figure 8b). On the Bear Property silver is a poor indicator element for gold.

Isolated stations recorded anomalous arsenic values (Figure 8c). These anomalous values appear to be of local extent only and do not correlate with anomalous gold values. On the Bear Property arsenic appears to be a poor indicator element for gold.

As with arsenic, isolated stations recorded anomalous copper values (Figure 8d). Line 200W exhibits weakly anomalous copper values between 175S and 275S. The anomalous copper values do not correlate with anomalous gold values. Copper appears to be a poor indicator element for gold.

Zinc appears to have a positive correlation with gold with respect to Anomaly C, the suspected stockwork zone (Figure 8e). None of the other gold anomalies show a corresponding zinc anomaly. The remaining anomalous zinc values appear to be local in extent. Zinc, in one instance, displays a positive correlation with gold.

Iron appears to be in anomalous concentrations on the eastern half of the grid (Figure 8f). This zone does not correlate with any of the gold anomalies or with the known geological structure. Iron appears to be a poor indicator element on this property.

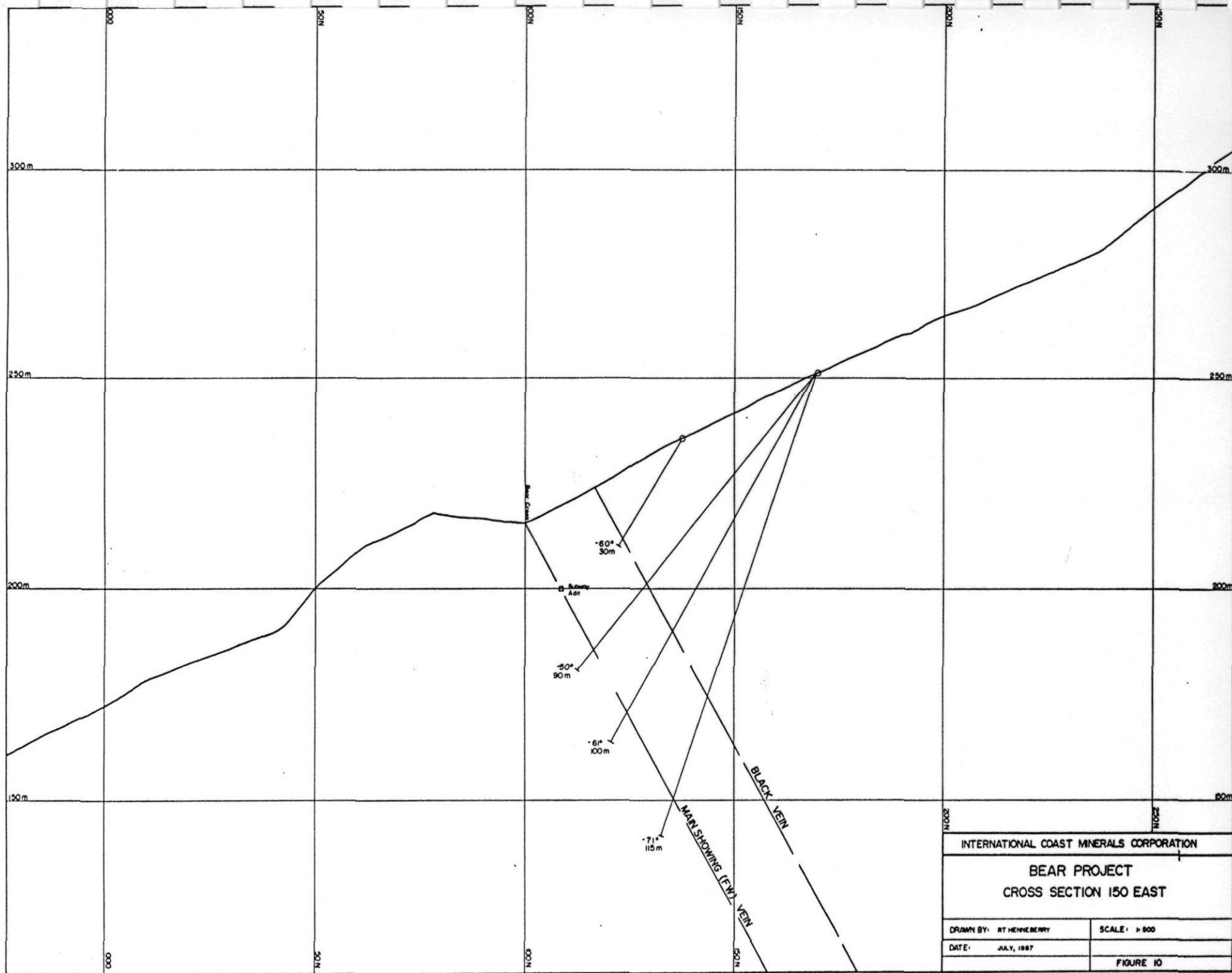
Although the chosen elements for the most part did not display positive correlations with gold, the geochemical survey was a success in tracing the Bear Shear Zone along strike. Several additional structures were located as a result of this survey. In the future gold, and possibly zinc, should be the only elements considered for a geochemical survey.

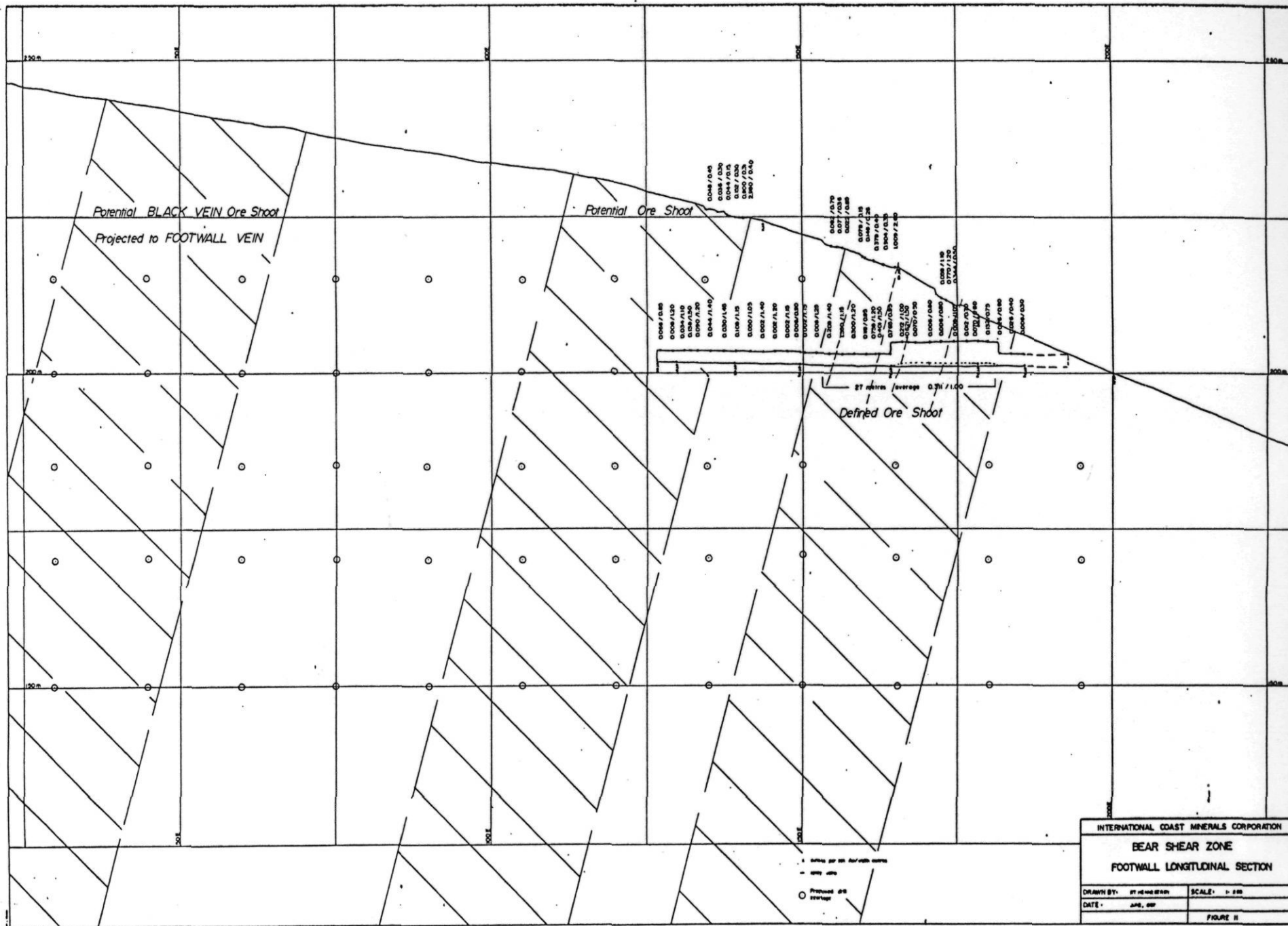
#### Geophysical Survey

Delta Geoscience Limited was contracted to carry out VLF and proton magnetometer surveys over the Bear Grid. The geophysical report, "Geophysical Report on the Bear Claim Group" by Grant Hendrickson is contained as APPENDIX C. An additional plan of then filtered VLF data was plotted (Figure 9). Jimmy Creek, Washington was the transmitter station. Readings were taken at 12.5 metre spacings along the cross lines.

This survey was successful in tracing both the Bear Fault and the Mine Fault along strike. The "Stockwork showing" yields a weak electromagnetic response. Responses obtained from sections of the Mine Fault exhibit similar characteristics to the known zones within the Bear Fault. A distinct linear anomaly lies north of the Mine Fault (125N to 150N) between lines 1300W and 1400W. A large, weak anomaly located between lines 400W and 550W, just south of the base line also requires investigation. Several spot anomalies were also identified throughout the grid. All anomalies require follow up by prospecting.







## DISCUSSION

Sampling and mapping within the presently exposed footwall section of the Bear Shear Zone has uncovered significant gold mineralization. The soil and geophysical surveys have indicated both the footwall and hanging wall of the Bear Shear Zone have gold-bearing potential. The Mine Fault exhibits similar geophysical responses, suggesting this fault also has gold-bearing potential. Gold geochemistry has located a large anomaly on the southeastern section of the claim group, indicating a possible stockwork zone may be present.

The important gold mineralization appears to be localized within the Bear Fault, proximal to the junction point with the Mine Fault. This one kilometre strike length hosts two distinct auriferous vein structures. The next phase of the Bear exploration program will be directed at proving up significant tonnage to sustain a 100 to 150 ton per day operation. Exploration will consist of surface trenching and diamond drilling. Prospecting will be confined to the gold anomalies and the Mine Fault, the gold bearing potential of which has yet to be tested.

Phase A of the recommended exploration program consists of mechanical trenching of all three known vein structures. Trenches should be spaced at 10 metre intervals along strike from the adit portal to the "Black Vein" (between sections 015E and 195E). While the excavator is on site an attempt should be made to clean out the "stockwork showing" on section 350E. The purpose of the trenching is to establish mineralized shoot geometry. One hundred hours of excavator time has been budgeted.

As part of Phase A, prospecting and sampling should be undertaken along the Mine Fault within the property boundaries. Silt samples at 100 metre spacings along Mine Fault Creek should pinpoint potential anomalous areas worthy of detailed prospecting.

The remainder of Phase A consists of surface diamond drilling. Initial drilling will be on 15 metre section spacings between sections 015E and 195E (Figures 10, 11). Drill holes should intersect the footwall zone at elevations 215 m, 185 m, 170 m and 150 m. A total of 3000 metres is required to carry on this Phase.

Phase B will consist of deeper drilling to elevation 000m. A 150 Level adit is also recommended as part of Phase B. Initially drifting should be downsized to 1.2 by 1.8 metres to ensure maximum gold recovery with minimal dilution. The drift can later be slashed open to size. A further 8000 metres of drilling and 200 metres of level development is recommended.

## CONCLUSIONS AND RECOMMENDATIONS

A detailed exploration program is warranted for the International Coast Minerals Corporation's Kennedy River Bear Property. A two phase exploration program consisting of surface trenching, diamond drilling and level development is recommended.

### Phase A

Surface trenching of the Bear Shear Zone "Footwall Vein" and "Black Vein" forms the initial part of Phase A exploration program. Trenches are recommended at 10 metre section spacings between sections 015E and 195E.

Initial exploration of the Mine Fault, consisting of silt sampling and prospecting, investigation of the gold soil anomalies and investigation of the geophysical anomalies should also be undertaken at this time.

Diamond drilling on a modified 15 metre by 15 metre grid concludes Phase A. Close to 60 surface holes will be drilled between sections 015E and 200E, between elevation 220 metres and 150 metres. 3000 metres of diamond drilling is required.

Total cost of Phase A is estimated at \$344,000.00

### Phase B

Deeper diamond drilling to elevation 000 and establishment of a 150 Level form the Phase B exploration program. This Phase is contingent on the results of Phase A. 8000 metres of diamond drilling will test projected down dip extensions of the mineralized shoots in all three veins. 200 metres of development will examine the Bear Shear Zone Vein at the 150 Level. Drill testing of the footwall and Black Veins will be possible from the established Level.

Estimated Phase B cost is \$1,084,500.00

This offering will provide funds for Phase A.

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Wilton, W.P. (1987). Report on the Southwestern District. In: British Columbia Mineral Exploration Review, 1986. pp. 69-70.

## STATEMENT OF QUALIFICATIONS

I, R. Tim Henneberry, am a consulting geologist residing at 4054 Dundas Street, Burnaby, British Columbia.

I earned a Bachelor of Science Degree majoring in geology from Dalhousie University, graduating in May, 1980.

I have practiced my profession continuously since graduation.

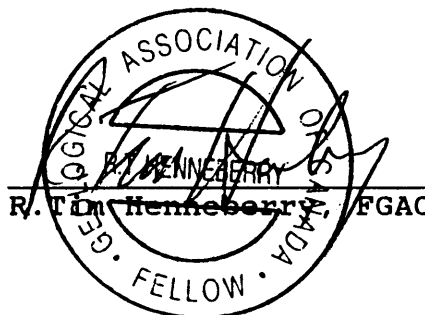
I am a Fellow of the Geological Association of Canada.

I have not received directly or indirectly, nor do I expect to receive any interest, direct or indirect, in the Bear Group Claims, nor do I beneficially own, directly or indirectly any securities in International Coast Minerals Limited, nor do I expect to receive any such interest.

This report is based on a sampling program carried out by the author from June 16 to June 18, 1987, a geochemical sampling program supervised by the author, a geophysical survey conducted by Delta Geoscience Limited and compilation of previous data.

I consent to the use of this report in a prospectus, in a statement of material facts, or for any other purpose normal to the business of International Coast Minerals Limited.

Dated this 14<sup>th</sup> day of July in the City of Vancouver, British Columbia.



COST ESTIMATES  
Phase A

|   |  |            |
|---|--|------------|
| Excavator                               |  |            |
| Mobilization / demobilization           |  | 500.00     |
| 100 hours at \$100 per hour (inclusive) |  | 10000.00   |
| Diamond Drill                           |  |            |
| Mobilization / demobilization           |  | 1000.00    |
| Drilling charges 3000 metres at \$60    |  | 180000.00  |
| Core Boxes                              |  | 2500.00    |
| Personnel                               |  |            |
| Geologist 60 days at \$350              |  | 21000.00   |
| Assistant 60 days at \$250              |  | 15000.00   |
| Assistant 60 days at \$180              |  | 10800.00   |
| Assistant 60 days at \$140              |  | 8400.00    |
| Accommodation                           |  |            |
| 480 days at \$60                        |  | 28800.00   |
| Transportation                          |  |            |
| 3 vehicles 60 days at \$30              |  | 5400.00    |
| Analysis                                |  |            |
| 1000 samples at \$15.50                 |  | 15500.00   |
| Supplies                                |  |            |
| Bags, racks, splitter                   |  | 10000.00   |
| Documentation                           |  |            |
| Geologist 20 days at \$350              |  | 7000.00    |
| Blueprint, photocopy, mylar             |  | 4000.00    |
|   |  | -----      |
| SUBTOTAL                                |  | 319,910.00 |
| Contingency                             |  | 24,090.00  |
|   |  | -----      |
| PHASE A TOTAL                           |  | 344,000.00 |

Initiation of Phase B is contingent on positive results from the Phase A exploration program. A completed Engineer's report should be prepared documenting the results of Phase A, before the exploration program continues.

COST ESTIMATE  
Phase B

|   |              |
|---|--------------|
| Diamond Drill                               |              |
| Mobilization / demobilization               | 1000.00      |
| Drilling charges 8000 metres at \$60        | 480000.00    |
| Core Boxes                                  | 6000.00      |
|   |              |
| Excavator                                   |              |
| 100 hours at \$100 (inclusive)              | 10000.00     |
|   |              |
| Personnel                                   |              |
| Geologist 130 days at \$350                 | 45500.00     |
| Assistant 130 days at \$250                 | 32500.00     |
| Assistant 130 days at \$180                 | 23400.00     |
| Assistant 130 days at \$140                 | 18200.00     |
|   |              |
| Accommodation                               |              |
| 1040 man days at \$60                       | 62400.00     |
|   |              |
| Transportation                              |              |
| 3 vehicles 130 days at \$30                 | 11700.00     |
|   |              |
| Analysis                                    |              |
| 1000 samples at \$15.50                     | 15500.00     |
|   |              |
| Supplies                                    |              |
| Bags, racks, splitter                       | 9000.00      |
|   |              |
| Documentation                               |              |
| Geologist 30 days at \$350                  | 10500.00     |
| Blueprint, photocopy, mylar                 | 4000.00      |
| SUBTOTAL                                    | 729,700.00   |
| All inclusive costs for 200 metres of drift |              |
| is estimated at \$1000 per metre            | 200,000.00   |
| Contingency                                 | 154,800.00   |
|   |              |
| PHASE B TOTAL                               | 1,084,500.00 |

|              |              |
|--------------|--------------|
| Phase A      | 344,000.00   |
| Phase B      | 1,084,500.00 |
|              | -----        |
| TOTAL BUDGET | 1,428,500.00 |



**APPENDIX A**  
**Geological Sampling Results**

**Teck (August, 1984)**

| Location             | Number | Type        | Au<br>oz/ton | Au<br>ppb | Width<br>metres |
|----------------------|--------|-------------|--------------|-----------|-----------------|
| <u>Main Showing</u>  |        |             |              |           |                 |
| BT09A + 1W           | 3125   | quartz      | 0.770        |           | 1.22            |
| BT10 + 0.4W          | 3091   | quartz      | 0.677        |           | 2.13            |
| BT10 + 2.6W          | 3092   | HW volcanic | 0.220        |           | 0.61            |
| BT03 + 11.6W         | 3093   | quartz      | 0.572        |           | 1.53            |
| <u>Lower Showing</u> |        |             |              |           |                 |
|                      | 3094   | granite     | 0.017        |           | grab            |

**Groves (May, 1985)**

| Location                          | Number | Type        | Au<br>oz/ton | Au<br>ppb | Width<br>metres |
|-----------------------------------|--------|-------------|--------------|-----------|-----------------|
| <u>Main Showing</u>               |        |             |              |           |                 |
| BT09A + 1W                        | 6960   | quartz      | 0.211        |           | 2.13            |
| BT10 + 3W                         | 6962   | quartz      | 0.130        |           | 0.31            |
| BT10 + 0.4W                       | 6963   | quartz      | 0.802        |           | 2.13            |
| BT10 + 2.6W                       | 6964   | HW volcanic | 0.750        |           | 1.22            |
| <u>Lower Showing</u>              |        |             |              |           |                 |
|                                   | 6954   | qtz/granite | 0.718        |           | grab            |
|                                   | 6965   | quartz      | 0.090        |           | grab            |
| <u>Black Vein (upper showing)</u> |        |             |              |           |                 |
| (Taken by Wilton of BCDM)         |        | quartz      | 1.230        |           | 2.74            |

**Noranda (September, 1985)**

| Location            | Number | Type        | Au<br>oz/ton | Au<br>ppb | Width<br>metres |
|---------------------|--------|-------------|--------------|-----------|-----------------|
| <u>Main Showing</u> |        |             |              |           |                 |
| BT10 + 5.3W         | 57451  | quartz      | 0.077*       | 2400      | 0.36            |
| BT10 + 5.3W         | 57452  | HW volcanic |              | 10        | 0.45            |
| BT10 + 2.6W         | 57453  | FW volcanic |              | 10        | 0.60            |
| BT10 + 4W           | 57454  | quartz      | 0.148*       | 4600      | 0.26            |
| BT10 + 4W           | 57455  | HW volcanic | 0.010*       | 300       | 1.90            |
| BT10 + 0.4W         | 57456  | quartz      | 1.158*       | 36000     | 1.30            |
| BT10 + 0.4W         | 57457  | HW volcanic |              | 60        | 0.70            |
| BT09A + 1W          | 57458  | quartz      | 0.064*       | 2000      | 0.75            |
| BT10 + 0            | 9833   | HW volcanic | 0.263        |           | grab            |
| BT03 + 11.6W        | 9831   | quartz      | 0.669        |           | 1.50            |
| BT04 + 1.4W         | 9832   | quartz      | 0.836        |           | grab            |

# Noranda (September, 1985)

| Location                          | Number | Type             | Au<br>oz/ton | Au<br>ppb | Width<br>metres |
|-----------------------------------|--------|------------------|--------------|-----------|-----------------|
| <u>Lower Showing</u>              |        |                  |              |           |                 |
|                                   | 9837   | qtz/granite      | 0.116        |           | grab            |
| <u>Black Vein (upper showing)</u> |        |                  |              |           |                 |
|                                   | 9834   | quartz           | 1.236        |           | 1.00            |
|                                   | 9835   | quartz           | 0.857        |           | 1.00            |
|                                   | 9836   | quartz           | 0.702        |           | 0.90            |
|                                   |        | Weighted Average | 0.940        |           | 2.90            |
|                                   | 57459  | quartz           | 0.035*       | 1100      | 0.30            |
|                                   | 57460  | quartz           | 0.116*       | 3600      | 0.35            |
|                                   | 57461  | quartz           | 0.080*       | 2500      | 0.60            |

## Lac (January, 1986)

| Location                          | Number | Type        | Au<br>oz/ton | Au<br>ppb | Width<br>metres |
|-----------------------------------|--------|-------------|--------------|-----------|-----------------|
| <u>Main Showing</u>               |        |             |              |           |                 |
| BT10 + 0.4W                       | 86T3   | quartz      | 1.626        | 5000      | 1.00            |
| ?                                 | 86T3a  | quartz      | 0.270*       | 8400      | 0.20            |
| BT10 + 10.0W                      | 86T3b  | quartz      | 0.061*       | 1900      | 0.10            |
| BT10 + 2.6W                       | 86T3c  | HW volcanic | 0.100*       | 3100      | 0.50            |
| BT09A + 1W                        | 86T4   | quartz      | 0.232*       | 7200      | 0.80            |
| BT04 + 1.4W                       | 86T5   | quartz      | 0.401        | +10000    | 1.50            |
| BT06 + 7.2W                       | 86T6   | quartz      | 0.138*       | 4300      | 1.50            |
| <u>Lower Showing</u>              |        |             |              |           |                 |
|                                   | 86T7   | qtz/granite |              | 160       | 5.00            |
|                                   | 86T8   | qtz/granite | 0.047*       | 1450      | 2.00            |
| <u>Black Vein (upper showing)</u> |        |             |              |           |                 |
|                                   | 86T1   | quartz      | 1.173        | +10000    | 2.50            |
|                                   | 86T1a  | quartz      | 0.507        | +10000    | 0.47            |
|                                   | 86T1b  | quartz      | 0.745        | +10000    | 1.20            |
|                                   | 86T2a  | quartz      | 0.161*       | 5000      | 0.80            |

\* designates calculation from ppb to oz/ton. High sulfide content of vein suggests ppb analysis could be out considerably and all anomalous gold values (+1000 ppb) should be Fire Assayed. An example is 86T3 which yielded 5000 ppb (converted 0.161 ounces per ton), but when fire assayed yielded 1.626 ounces per ton.

**Goldsmith (June, 1986)**

| Location                          | Number | Type          | Au<br>oz/ton | Au<br>ppb | Width<br>metres |
|-----------------------------------|--------|---------------|--------------|-----------|-----------------|
| <u>Main Showing</u>               |        |               |              |           |                 |
| BT10 + 0.4W                       | 2V     | qtz/HW volc's | 1.228        |           | 2.10            |
| <u>Black Vein (upper showing)</u> |        |               |              |           |                 |
|                                   |        | quartz        | 0.146        |           | 2.00            |

**Henneberry (May, 1987)**

| Location            | Number | Type   | Au<br>oz/ton | Au<br>ppb | Width<br>metres |
|---------------------|--------|--------|--------------|-----------|-----------------|
| <u>Main Showing</u> |        |        |              |           |                 |
| BT11 + 3.0W         | 1128   | quartz | 0.800        |           | 0.31            |
| BT11 + 5.7W         | 1129   | quartz | 0.044        |           | 0.15            |

**Henneberry (June, 1987)**

| Location            | Number | Type   | Au<br>oz/ton | Width<br>metres |
|---------------------|--------|--------|--------------|-----------------|
| <u>Main Showing</u> |        |        |              |                 |
| BT09A - 1.0 W       | 1130   | quartz | 0.344        | 0.50            |
| BT09A + 1.0 W       | 1131   | quartz | 0.058        | 1.10            |
| BT10 + 2.5 W        | 1134   | quartz | 0.904        | 0.35            |
| BT10 + 4.1 W        | 1135   | quartz | 0.378        | 0.40            |
| BT10 + 5.8 W        | 1136   | quartz | 0.078        | 0.15            |
| BT10 + 9.5 W        | 1137   | quartz | 0.022        | 0.65            |
| BT10 + 11.3 W       | 1138   | quartz | 0.082        | 0.70            |
| BT11 + 2.6 W        | 1139   | quartz | 2.980        | 0.40            |
| BT11 + 4.4 W        | 1140   | quartz | 0.152        | 0.30            |
| BT11 + 6.9 W        | 1141   | quartz | 0.036        | 0.30            |
| BT11 + 8.5 W        | 1143   | quartz | 0.048        | 0.45            |
|                     |        |        |              |                 |
| BT02 + 0.0 W        | 4151   | quartz | 0.006        | 0.30            |
| BT02 + 2.0 W        | 4152   | quartz | 0.026        | 0.40            |
| BT02 + 4.0 W        | 4153   | quartz | 0.026        | 0.60            |
| BT02 + 6.0 W        | 4154   | quartz | 0.132        | 0.75            |
| BT03 + 0.0 W        | 4155   | quartz | 0.070        | 0.60            |
| BT03 + 2.0 W        | 4156   | quartz | 0.012        | 0.70            |
| BT03 + 4.0 W        | 4157   | quartz | 0.006        | 1.05            |
| BT03 + 6.0 W        | 4158   | quartz | 0.006        | 0.80            |
| BT03 + 8.0 W        | 4159   | quartz | 0.006        | 0.60            |
| BT03 + 10.0 W       | 4160   | quartz | 0.070        | 0.50            |
| BT03 + 12.0 W       | 4161   | quartz | 0.212        | 1.00            |
| BT04 + 0.0 W        | 4162   | quartz | 0.765        | 0.95            |
| BT04 + 2.0 W        | 4163   | quartz | 0.758        | 1.20            |
| BT04 + 4.0 W        | 4164   | quartz | 0.118        | 0.85            |

# Henneberry (June, 1987)

| Location      | Number | Type   | Au<br>oz/ton | Width<br>metres |
|---------------|--------|--------|--------------|-----------------|
| BT04 + 6.0 W  | 4165   | quartz | 0.300        | 1.20            |
| BT04 + 8.0 W  | 4166   | quartz | 1.350        | 1.15            |
| BT04 + 10.0 W | 4167   | quartz | 0.208        | 1.40            |
| BT04 + 12.0 W | 4168   | quartz | 0.006        | 1.25            |
| BT04 + 14.0 W | 4169   | quartz | 0.002        | 1.15            |
| BT05 + 0.0 W  | 4170   | quartz | 0.006        | 0.90            |
| BT05 + 2.0 W  | 4171   | quartz | 0.002        | 1.15            |
| BT05 + 4.0 W  | 4172   | quartz | 0.002        | 1.20            |
| BT05 + 6.0 W  | 4173   | quartz | 0.002        | 1.40            |
| BT05 + 8.0 W  | 4174   | quartz | 0.050        | 1.05            |
| BT06 + 0.0 W  | 4175   | quartz | 0.108        | 1.15            |
| BT06 + 2.0 W  | 4176   | quartz | 0.030        | 1.45            |
| BT06 + 4.0 W  | 4177   | quartz | 0.044        | 1.40            |
| BT06 + 6.0 W  | 4178   | quartz | 0.090        | 1.20            |
| BT06 + 8.0 W  | 4179   | quartz | 0.034        | 1.10            |
| BT06 + 10.0 W | 4180   | quartz | 0.008        | 1.20            |
| BT06 + 12.0 W | 4181   | quartz | 0.066        | 0.85            |

## Main Showing HW Splay # 1

|               |      |        |       |      |
|---------------|------|--------|-------|------|
| BT09A - 1.0 W | 1130 | quartz | 0.344 | 0.50 |
| BT09A + 1.0 W | 1131 | quartz | 0.058 | 1.10 |
| BT09A + 3.0 W | 1132 | quartz | 0.156 | 0.35 |
| BT09A + 5.0 W | 1133 | quartz | 0.006 | 0.25 |
| BT04 + 5.0 W  | 4182 | quartz | 0.026 | 0.20 |
| BT04 + 7.0 W  | 4183 | quartz | 0.038 | 0.25 |
| BT04 + 9.0 W  | 4184 | quartz | 0.081 | 0.30 |

## Main Showing HW Splay # 3

|               |      |        |       |      |
|---------------|------|--------|-------|------|
| BT10 + 7.0 W  | 1142 | quartz | 0.300 | 0.30 |
| BT04 + 14.5 W | 4185 | quartz | 0.002 | 0.45 |

The surface sampling on the Main Showing zone was concentrated on filling in the holes, in an effort to keep sampling spacing within 2 to 3 metres if possible. A lot of duplicate samples were taken from locations where surface blasting indicated a significant improvement beneath the weathered cap on the vein. Sampling also concentrated on establishing the strike extension of the zone to the west and on establishing the gold content of the hanging wall splays on surface. Hand - trenching to the north has indicated an increase of vein width.

Underground sampling was spaced at 2 metre intervals along the zone in an effort to establish an accurate gold concentration of the main vein at this elevation.



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Analytical Chemists • Geochemists • Registered Assayers

212 BROOKSBANK AVE., NORTH VANCOUVER,  
BRITISH COLUMBIA, CANADA V7J-2C1

PHONE (604) 984-0221

## CERTIFICATE OF ANALYSIS A8715264

To: NATIONWIDE GOLD MINES CORP.

1500 - 1176 W. GEORGIA ST.  
VANCOUVER, BC  
V6E 4A2

\*Page No. : 1  
Tot. Pages: 1  
Date : 03-JUN-87  
Invoice # : I-8715264  
P.O. # : NONE

Project :

Comments: ATTN: TIM HENNEBERRY

| SAMPLE DESCRIPTION | PREP CODE | Au FA oz/T |   |       |  |  |  |  |  |  |  |
|--------------------|-----------|------------|---|-------|--|--|--|--|--|--|--|
| 1126               | 207       | ---        | < | 0.044 |  |  |  |  |  |  |  |
| 1127               | 207       | ---        |   | 0.002 |  |  |  |  |  |  |  |
| 1128               | 207       | ---        |   | 0.800 |  |  |  |  |  |  |  |
| 1129               | 207       | ---        |   | 0.044 |  |  |  |  |  |  |  |

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CERTIFICATION :

*W. Sen*



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BRITISH COLUMBIA, CANADA V7J-2C1

PHONE (604) 984-0221

To: INP EXPLAND DEVELOPMENT

1500 - 1176 W. GEORGIA ST.  
VANCOUVER, BC  
V6E 4A2

Project: BEAR

Comments: ATTN: AUGUST OLSEN ✓ CC: TIM HENNEBERRY

Page No. : 1  
Tot. Pages: 2  
Date : 23-JUN-87  
Invoice # : I-8716504  
P.O. # : NONE

## CERTIFICATE OF ANALYSIS A8716504

| SAMPLE DESCRIPTION | PREP CODE |     | Au FA oz/T |  |  |  |  |  |  |  |  |  |
|--------------------|-----------|-----|------------|--|--|--|--|--|--|--|--|--|
| 1130               | 207       | --- | 0.344      |  |  |  |  |  |  |  |  |  |
| 1131               | 207       | --- | 0.058      |  |  |  |  |  |  |  |  |  |
| 1132               | 207       | --- | 0.156      |  |  |  |  |  |  |  |  |  |
| 1133               | 207       | --- | 0.006      |  |  |  |  |  |  |  |  |  |
| 1134               | 207       | --- | 0.904      |  |  |  |  |  |  |  |  |  |
| 1135               | 207       | --- | 0.378      |  |  |  |  |  |  |  |  |  |
| 1136               | 207       | --- | 0.078      |  |  |  |  |  |  |  |  |  |
| 1137               | 207       | --- | 0.022      |  |  |  |  |  |  |  |  |  |
| 1138               | 207       | --- | 0.082      |  |  |  |  |  |  |  |  |  |
| 1139               | 207       | --- | 2.980      |  |  |  |  |  |  |  |  |  |
| 1140               | 207       | --- | 0.152      |  |  |  |  |  |  |  |  |  |
| 1141               | 207       | --- | 0.036      |  |  |  |  |  |  |  |  |  |
| 1142               | 207       | --- | 0.300      |  |  |  |  |  |  |  |  |  |
| 1143               | 207       | --- | 0.048      |  |  |  |  |  |  |  |  |  |
| 4151               | 207       | --- | 0.006      |  |  |  |  |  |  |  |  |  |
| 4152               | 207       | --- | 0.026      |  |  |  |  |  |  |  |  |  |
| 4153               | 207       | --- | 0.026      |  |  |  |  |  |  |  |  |  |
| 4154               | 207       | --- | 0.132      |  |  |  |  |  |  |  |  |  |
| 4155               | 207       | --- | 0.070      |  |  |  |  |  |  |  |  |  |
| 4156               | 207       | --- | 0.012      |  |  |  |  |  |  |  |  |  |
| 4157               | 207       | --- | 0.006      |  |  |  |  |  |  |  |  |  |
| 4158               | 207       | --- | 0.006      |  |  |  |  |  |  |  |  |  |
| 4159               | 207       | --- | 0.006      |  |  |  |  |  |  |  |  |  |
| 4160               | 207       | --- | 0.070      |  |  |  |  |  |  |  |  |  |
| 4161               | 207       | --- | 0.212      |  |  |  |  |  |  |  |  |  |
| 4162               | 207       | --- | 0.765      |  |  |  |  |  |  |  |  |  |
| 4163               | 207       | --- | 0.758      |  |  |  |  |  |  |  |  |  |
| 4164               | 207       | --- | 0.118      |  |  |  |  |  |  |  |  |  |
| 4165               | 207       | --- | 0.300      |  |  |  |  |  |  |  |  |  |
| 4166               | 207       | --- | 1.350      |  |  |  |  |  |  |  |  |  |
| 4167               | 207       | --- | 0.208      |  |  |  |  |  |  |  |  |  |
| 4168               | 207       | --- | 0.006      |  |  |  |  |  |  |  |  |  |
| 4169               | 207       | --- | 0.002      |  |  |  |  |  |  |  |  |  |
| 4170               | 207       | --- | 0.006      |  |  |  |  |  |  |  |  |  |
| 4171               | 207       | --- | < 0.002    |  |  |  |  |  |  |  |  |  |
| 4172               | 207       | --- | 0.002      |  |  |  |  |  |  |  |  |  |
| 4173               | 207       | --- | < 0.002    |  |  |  |  |  |  |  |  |  |
| 4174               | 207       | --- | 0.050      |  |  |  |  |  |  |  |  |  |
| 4175               | 207       | --- | 0.108      |  |  |  |  |  |  |  |  |  |
| 4176               | 207       | --- | 0.030      |  |  |  |  |  |  |  |  |  |

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*[Signature]*



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To: INP EXPLAND DEVELOPMENT

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V6E 4A2

Project: BEAR

Comments: ATTN: AUGUST OLSEN CC: TIM HENNEBERRY

Page No.: 2

Tot. Pages: 2

Date: 23-JUN-87

Invoice #: I-8716504

P.O. #: NONE

## CERTIFICATE OF ANALYSIS A8716504

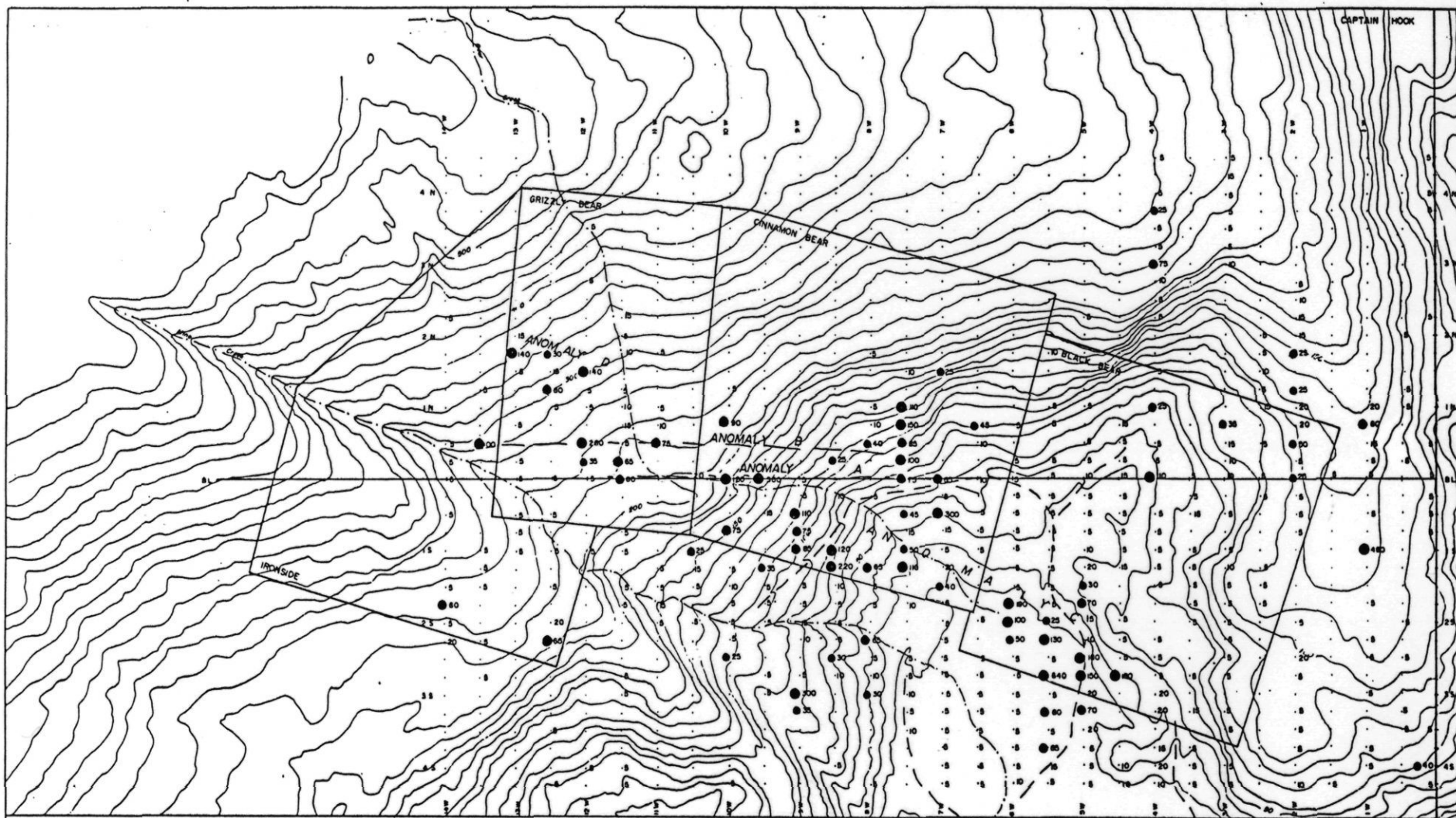
| SAMPLE DESCRIPTION | PREP CODE | Au FA oz/T |          |  |  |  |  |  |  |  |  |
|--------------------|-----------|------------|----------|--|--|--|--|--|--|--|--|
| 4177               | 207       | ---        | 0.044    |  |  |  |  |  |  |  |  |
| 4178               | 207       | ---        | 0.090    |  |  |  |  |  |  |  |  |
| 4179               | 207       | ---        | 0.034    |  |  |  |  |  |  |  |  |
| 4180               | 207       | ---        | 0.008    |  |  |  |  |  |  |  |  |
| 4181               | 207       | ---        | 0.066    |  |  |  |  |  |  |  |  |
| 4182               | 207       | ---        | 0.026    |  |  |  |  |  |  |  |  |
| 4183               | 207       | ---        | 0.038    |  |  |  |  |  |  |  |  |
| 4184               | 207       | ---        | 0.081    |  |  |  |  |  |  |  |  |
| 4185               | 207       | ---        | 0.002    |  |  |  |  |  |  |  |  |
| 10596              | 207       | ---        | 0.004    |  |  |  |  |  |  |  |  |
| 10597              | 207       | ---        | << 0.002 |  |  |  |  |  |  |  |  |
| 10598              | 207       | ---        | << 0.002 |  |  |  |  |  |  |  |  |
| 10599              | 207       | ---        | << 0.002 |  |  |  |  |  |  |  |  |

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CERTIFICATION :

*P. L. Swaiter*





# LEGEND

- > 100 ppb
- 60 - 99 ppb
- 20 - 59 ppb

Contour interval : 10 & 20 meters



INTERNATIONAL COAST MINERALS CORPORATION

BEAR PROJECT

SOIL GEOCHEMISTRY Au (ppb)

DRN BY: S. T. Hennessey

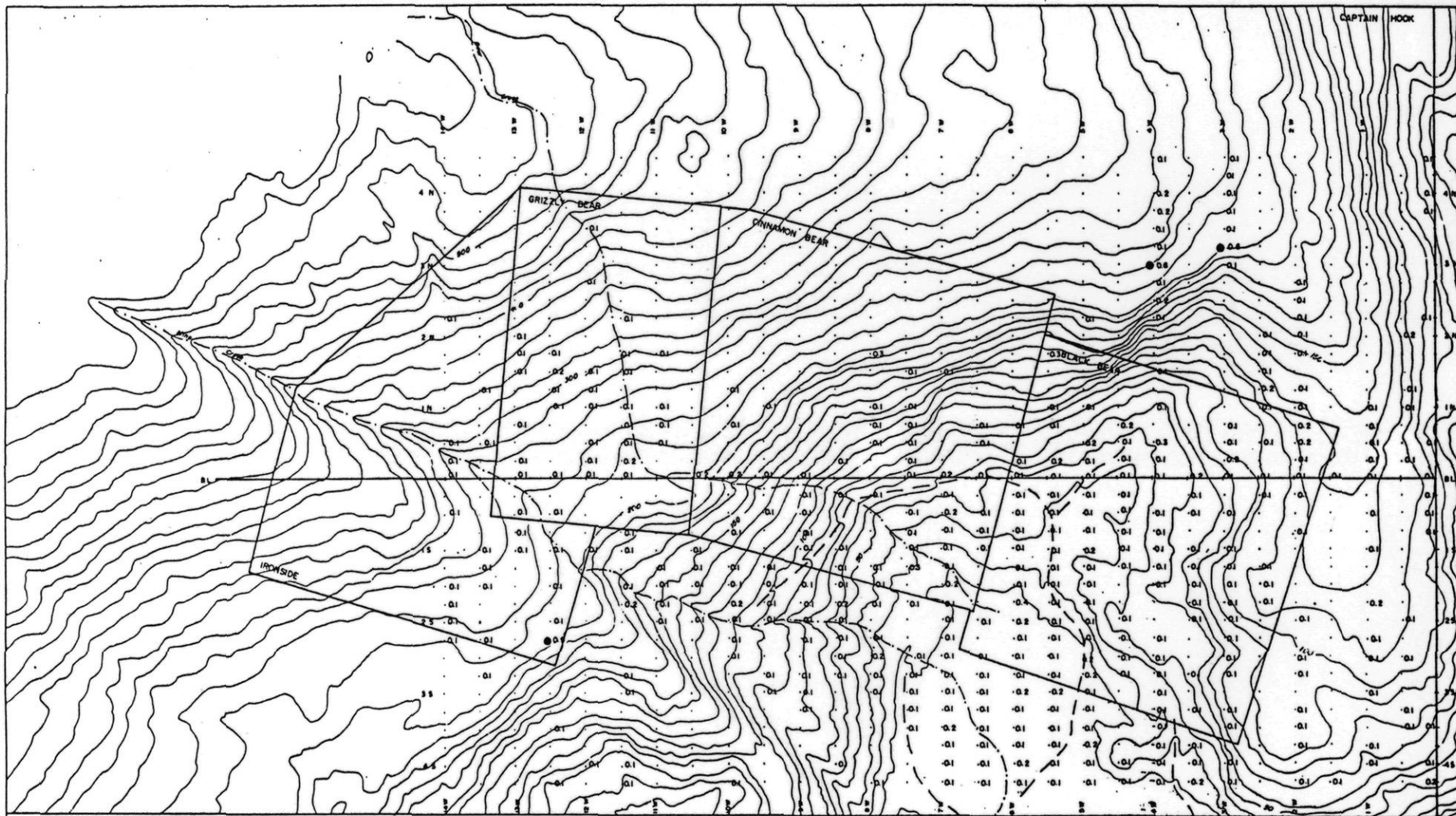
SCALE 1:2500

DATE: July 1987

FIGURE 8.6

**APPENDIX B**

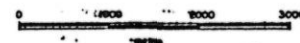
**Geochemistry Lab Reports  
Full Size and Reduced Geochemistry Maps**



LEGEND

● > 0.5 ppm

Contour Interval: 10 & 20 metres



INTERNATIONAL COAST MINERALS CORPORATION

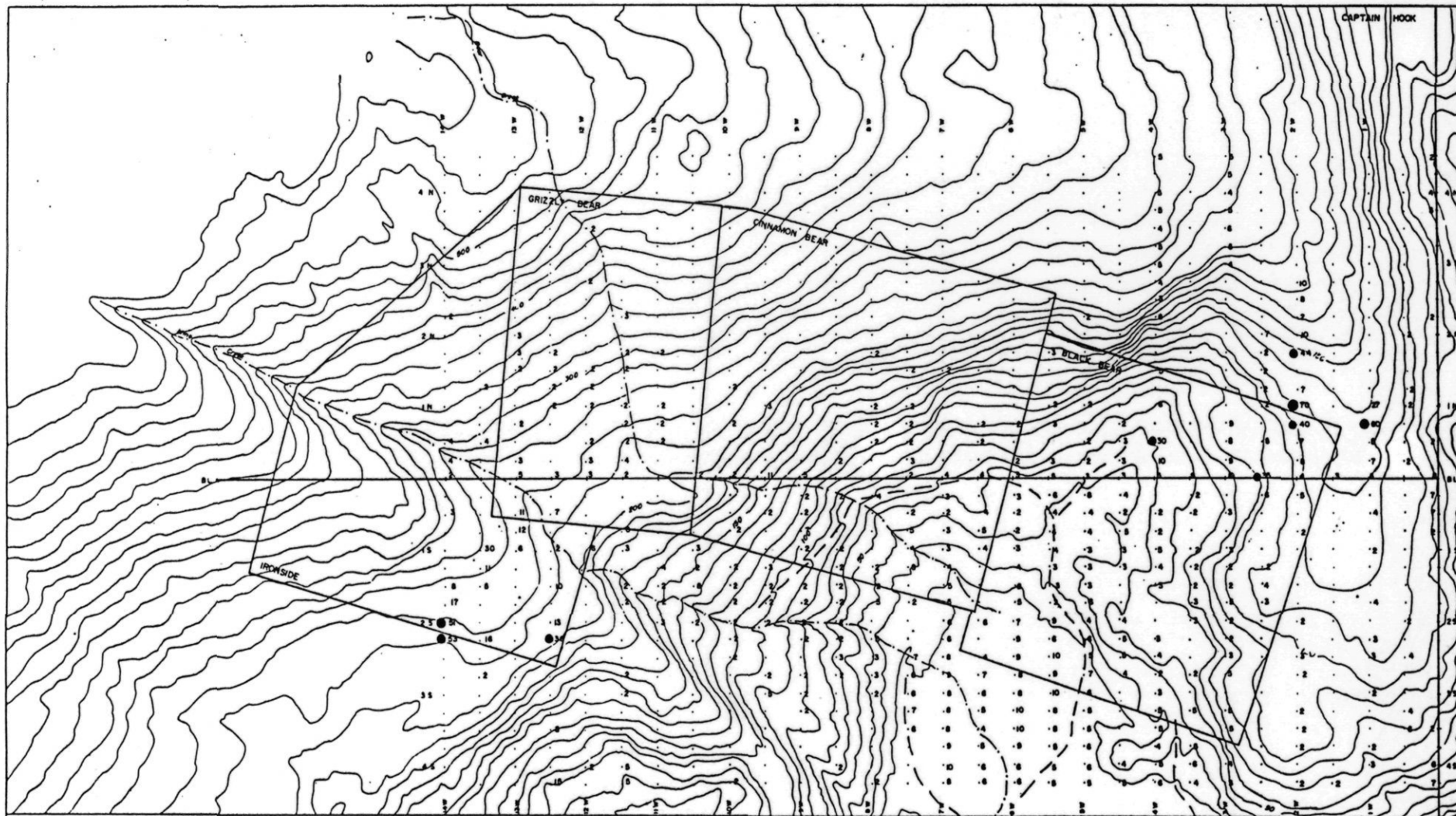
BEAR PROJECT  
SOIL GEOCHEMISTRY Ag (ppm)

DRN BY: S. T. McNeasey

SCALE: 1" = 2500'

DATE: July 1967

FIGURE 1.1



# LEGEND

- 70 ppm
- 50 - 69 ppm
- 30 - 49 ppm

Contour Interval - 10 & 20 meters



INTERNATIONAL COAST MINERALS CORPORATION

## BEAR PROJECT SOIL GEOCHEMISTRY As (ppm)

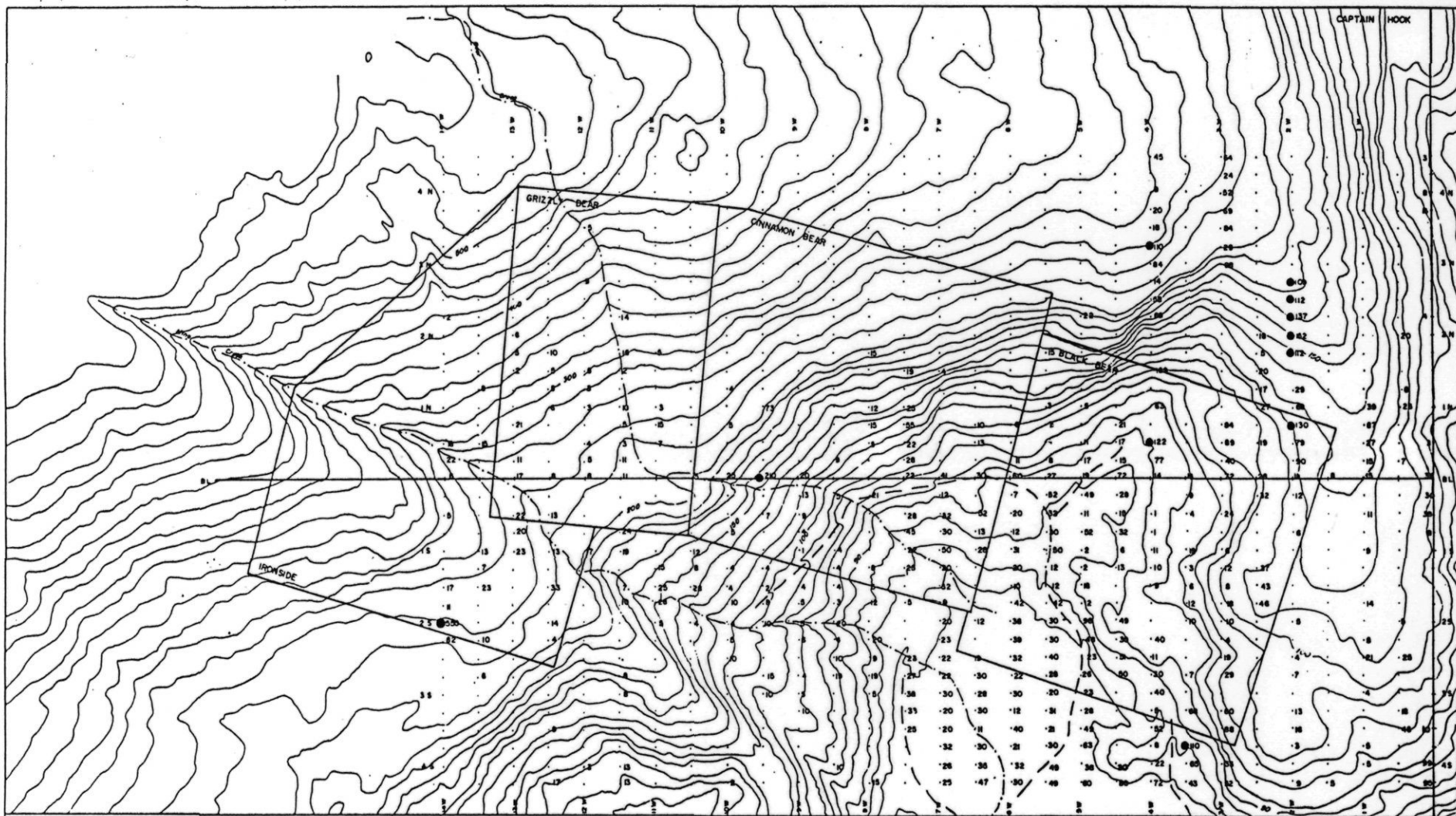
DRN BY: R. T. Hennesberry

SCALE: 1" = 2500'

DATE: July 1967

FIGURE 8c





# LEGEND

- > 500 ppm
- 100 - 500 ppm

Contour Interval: 10 & 20 metres

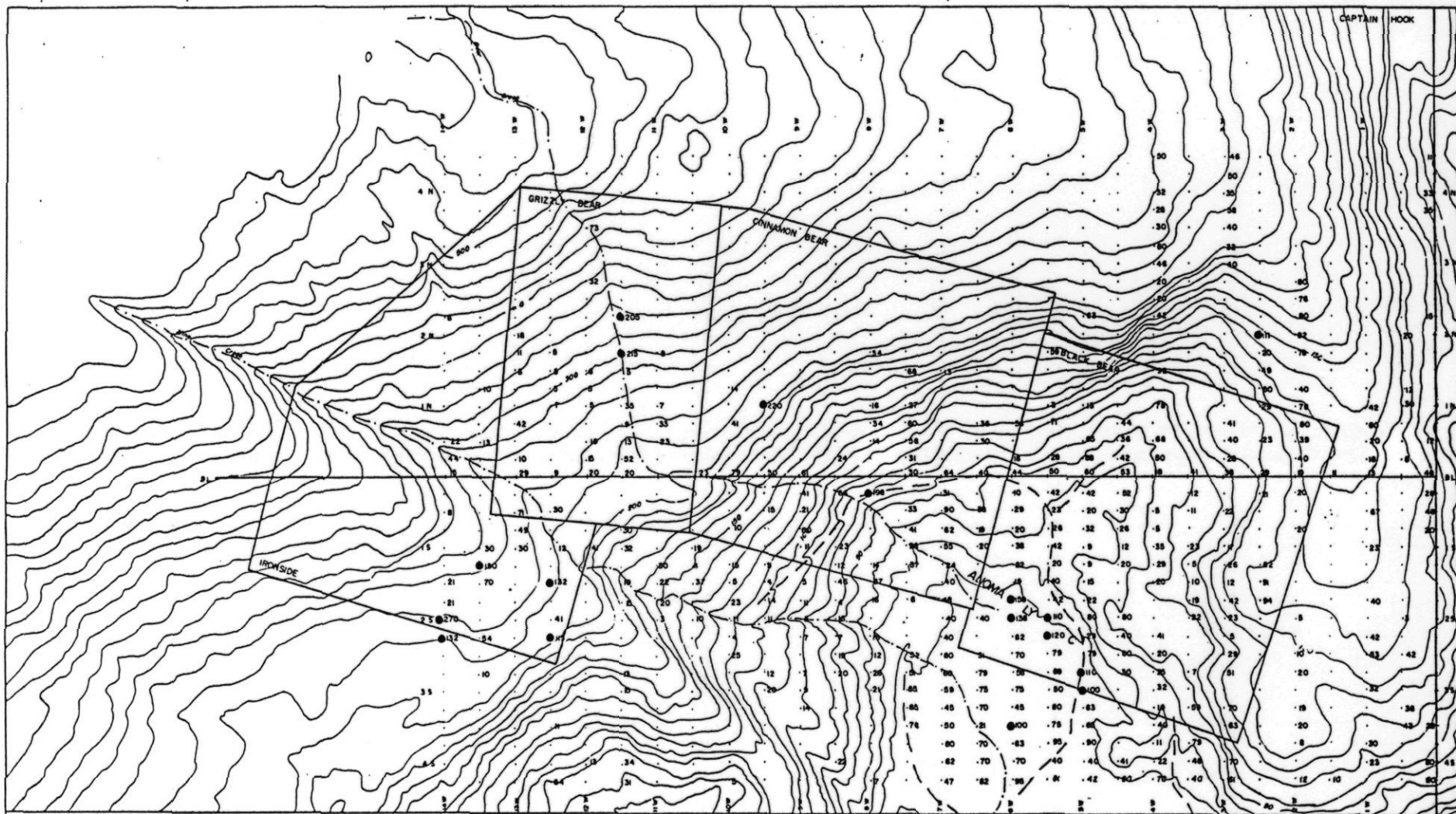


INTERNATIONAL COAST MINERALS CORPORATION

## BEAR PROJECT SOIL GEOCHEMISTRY Cu (ppm)

DRN 871 R T Honeyberry  
DATE July 1987

SCALE 1:2500  
FIGURE 84



# LEGEND

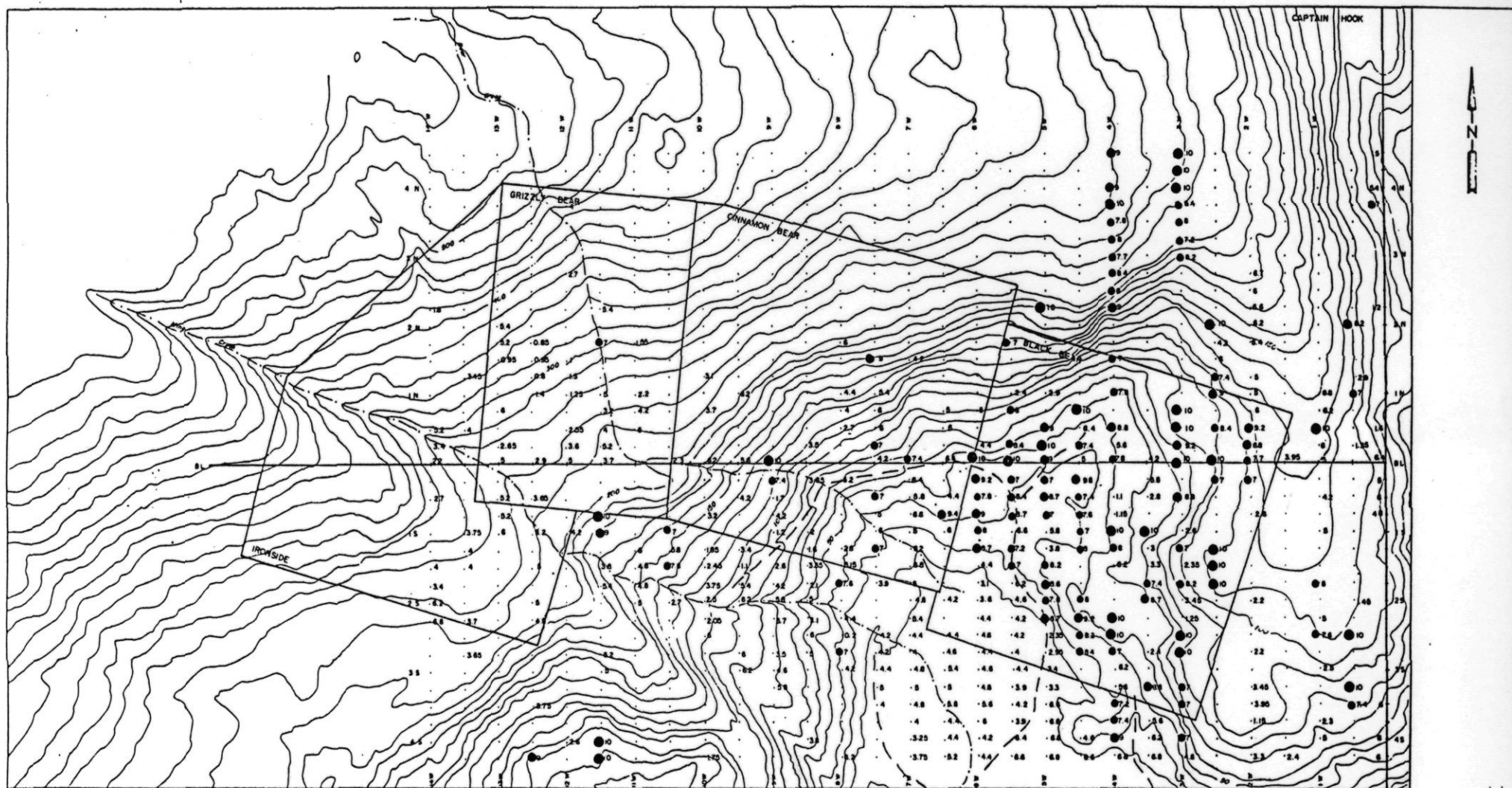
● > 100 ppm

Contour Interval: 10 & 20 metres

0 1000 2000 3000

metres

|  |                |
|--|----------------|
| INTERNATIONAL COAST MINERALS CORPORATION |                |
| BEAR PROJECT                             |                |
| SOIL GEOCHEMISTRY Zn (ppm)               |                |
| DRAWN BY: R. J. Hennessey                | SCALE: 1"=2000 |
| DATE: July 1987                          | FIGURE 6a      |



# LEGEND

- > 10 %
- 8.5 - 10 %
- 7.0 - 8.4 %

Contour Interval : 10 & 20 metres

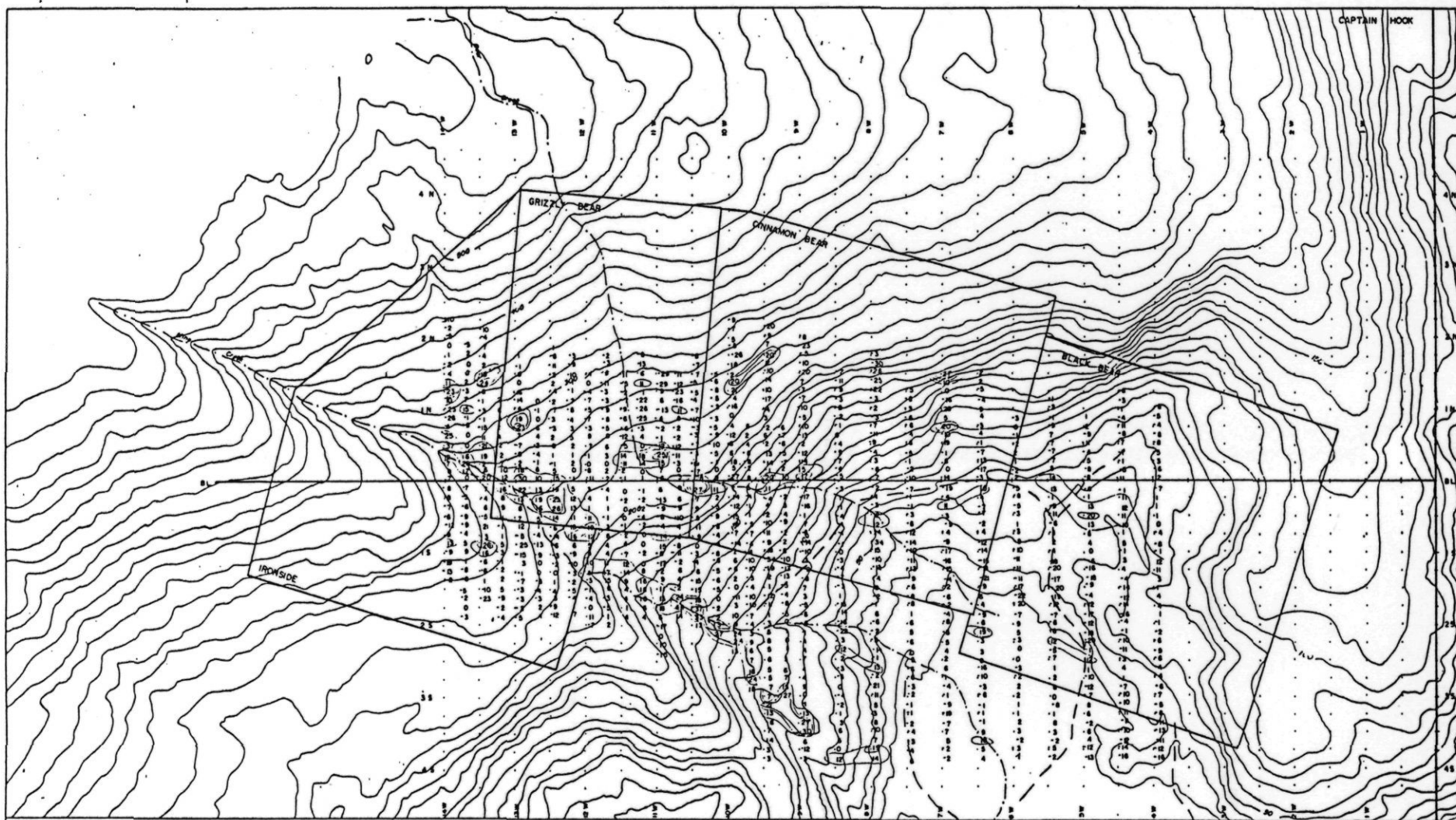


INTERNATIONAL COAST MINERALS CORPORATION

## BEAR PROJECT SOIL GEOCHEMISTRY Fe (%)

|                          |                   |
|--------------------------|-------------------|
| DRAWN BY: S. T. Monaghan | SCALE: 1" = 2000' |
| DATE: July 1987          | FIGURE: 87        |





# LEGEND

Contours  
 10-20  
 20-30  
 30-40

Contour Interval: 10 & 20 metres



INTERNATIONAL COAST MINERALS CORPORATION

## BEAR PROJECT VLF FRASER FILTERED DIPS

|                         |               |
|-------------------------|---------------|
| DRN BY: R. T. Hennessey | SCALE: 1:2500 |
| DATE: July 1987         | FIGURE 5      |





REPORT: 127-3509 ( COMPLETE )

REFERENCE INFO:

CLIENT: INP EXPLORATION AND DEVELOPMENT  
PROJECT: BEAR

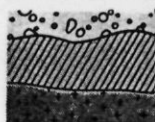
SUBMITTED BY: R.T. HENNEBERRY  
DATE PRINTED: 10-JUN-87

| ORDER | ELEMENT |                      | NUMBER OF ANALYSES | LOWER DETECTION LIMIT | EXTRACTION          | METHOD            |
|-------|---------|----------------------|--------------------|-----------------------|---------------------|-------------------|
| 1     | Cu      | Copper               | 116                | 1 PPM                 | HNO3-HCL HOT EXTR   | Atomic Absorption |
| 2     | Zn      | Zinc                 | 116                | 1 PPM                 | HNO3-HCL HOT EXTR   | Atomic Absorption |
| 3     | Ag      | Silver               | 116                | 0.1 PPM               | HNO3-HCL HOT EXTR   | Atomic Absorption |
| 4     | Fe      | Iron                 | 116                | 0.05 PCT              | HNO3-HCL HOT EXTR   | Atomic Absorption |
| 5     | As      | Arsenic              | 116                | 2 PPM                 | NITRIC PERCHLOR DIG | Colourimetric     |
| 6     | Au      | Gold - Fire Assay    | 116                | 5 PPB                 | FIRE-ASSAY          | Fire Assay AA     |
| 7     | Au/wt   | Sample weight/grams  | 110                | 0.1 G                 |                     |                   |
| 8     | Au/wt   | -20 Au Sample Weight | 22                 | 0.1 G                 |                     |                   |

| SAMPLE TYPES            | NUMBER | SIZE FRACTIONS | NUMBER | SAMPLE PREPARATIONS | NUMBER |
|-------------------------|--------|----------------|--------|---------------------|--------|
| 5 SOILS                 | 111    | 1 -80          | 116    | DRY, SEIVE -80      | 116    |
| 1 STREAM SEDIMENT, SILT | 5      |                |        |                     |        |

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INVOICE TO: MR. R. T. HENNEBERRY



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PROJECT: BEAR

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| SAMPLE<br>NUMBER | ELEMENT<br>UNITS | Cu<br>PPM | Zn<br>PPM | Ag<br>PPM | Fe<br>PCT | As<br>PPM | Au<br>PPB | Au/wt<br>G | Au/wt<br>G |
|------------------|------------------|-----------|-----------|-----------|-----------|-----------|-----------|------------|------------|
| S1 L4+00W 0+00S  |                  | 16        | 30        | 0.1       | 7.80      | 3         | <5        |            | 10.0       |
| S1 L4+00W 0+50S  |                  | 1         | 5         | 0.1       | 1.10      | 2         | <5        | 10.0       |            |
| S1 L4+00W 0+75S  |                  | 1         | 5         | <0.1      | 1.15      | 2         | <5        | 10.0       |            |
| S1 L4+00W 1+00S  |                  | 11        | 35        | <0.1      | >10.00    | 5         | <5        | 10.0       |            |
| S1 L4+00W 1+25S  |                  | 10        | 29        | <0.1      | 8.00      | 4         | <5        | 10.0       |            |
| S1 L4+00W 1+50S  |                  | 9         | 20        | 0.1       | 6.20      | 3         | <5        | 10.0       |            |
| S1 L4+00W 2+25S  |                  | 40        | 41        | <0.1      | >10.00    | 3         | <5        | 10.0       |            |
| S1 L4+00W 2+50S  |                  | 11        | 20        | <0.1      | >10.00    | 4         | <5        | 10.0       |            |
| S1 L4+00W 2+75S  |                  | 30        | 35        | <0.1      | 7.00      | 2         | <5        | 10.0       |            |
| S1 L4+00W 3+00S  |                  | 40        | 32        | 0.1       | 6.20      | 3         | 20        | 10.0       |            |
| S1 L4+00W 3+25S  |                  | 5         | 10        | <0.1      | 5.60      | 5         | 20        | 10.0       |            |
| S1 L4+00W 3+50S  |                  | 52        | 40        | 0.1       | 7.20      | 5         | 5         | 10.0       |            |
| S1 L4+00W 3+75S  |                  | 8         | 11        | 0.1       | 7.40      | 4         | 15        | 10.0       |            |
| S1 L4+00W 4+00S  |                  | 22        | 22        | <0.1      | 9.00      | 5         | 20        | 10.0       |            |
| S1 L4+00W 4+25S  |                  | 72        | 70        | <0.1      | 6.80      | 6         | 10        | 10.0       |            |
| S1 L4+50W 0+25S  |                  | 28        | 52        | <0.1      | 9.80      | 4         | <5        | 5.0        |            |
| S1 L4+50W 0+50S  |                  | 15        | 30        | <0.1      | 7.40      | 2         | <5        | 7.0        |            |
| S1 L4+50W 0+75S  |                  | 32        | 26        | <0.1      | 7.60      | 5         | 5         | 10.0       |            |
| S1 L4+50W 1+00S  |                  | 6         | 12        | <0.1      | 7.00      | 3         | 5         | 10.0       |            |
| S1 L4+50W 1+25S  |                  | 13        | 20        | <0.1      | 8.00      | 3         | 15        | 10.0       |            |
| S1 L4+50W 2+00S  |                  | 49        | 80        | <0.1      | 8.00      | 4         | <5        | 10.0       |            |
| S1 L4+50W 2+25S  |                  | 30        | 40        | 0.1       | 9.20      | 5         | <5        | 10.0       |            |
| S1 L4+50W 2+50S  |                  | 51        | 60        | 0.1       | 8.20      | 5         | <5        | 10.0       |            |
| S1 L4+50W 2+75S  |                  | 50        | 30        | 0.1       | 8.40      | 4         | 180       | 10.0       |            |
| S1 L4+50W 4+00S  |                  | 30        | 41        | 0.1       | 4.60      | 4         | 10        | 2.0        | 3.0        |
| S1 L4+50W 4+25S  |                  | 80        | 50        | <0.1      | 6.60      | 5         | 10        | 2.0        | 8.0        |
| S1 L5+00W 0+00S  |                  | 11        | 60        | <0.1      | 5.40      | 3         | <5        |            | 2.0        |
| S1 L5+00W 0+25S  |                  | 49        | 42        | <0.1      | 7.00      | 8         | <5        |            | 10.0       |
| S1 L5+00W 0+50S  |                  | 11        | 20        | 0.1       | 8.20      | 4         | 5         | 4.0        | 6.0        |
| S1 L5+00W 0+75S  |                  | 52        | 32        | <0.1      | 7.00      | 4         | <5        | 10.0       |            |
| S1 L5+00W 1+00S  |                  | 2         | 9         | 0.2       | 5.80      | 3         | 10        | 10.0       |            |
| S1 L5+00W 1+25S  |                  | 2         | 9         | <0.1      | 3.80      | 3         | 20        | 6.0        |            |
| S1 L5+00W 1+50S  |                  | 18        | 15        | <0.1      | 8.20      | 3         | 30        | 10.0       |            |
| S1 L5+00W 1+75S  |                  | 12        | 22        | 0.1       | 8.60      | 3         | 70        | 5.0        |            |
| S1 L5+00W 2+00S  |                  | 98        | 80        | <0.1      | 7.80      | 4         | 15        | 10.0       |            |
| S1 L5+00W 2+25S  |                  | 48        | 29        | <0.1      | 8.20      | 6         | 10        | 10.0       |            |
| S1 L5+00W 2+50S  |                  | 23        | 79        | 0.2       | 2.35      | 5         | 180       | 2.0        | 8.0        |
| S1 L5+00W 2+75S  |                  | 26        | 110       | 0.2       | 2.95      | 7         | 150       |            | 10.0       |
| S1 L5+00W 3+00S  |                  | 23        | 100       | 0.1       | 3.40      | 6         | 20        |            | 10.0       |
| S1 L5+00W 3+25S  |                  | 28        | 63        | <0.1      | 3.30      | 5         | 70        | 3.0        | 7.0        |



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| SAMPLE<br>NUMBER | ELEMENT<br>UNITS | Cu<br>PPM | Zn<br>PPM | Ag<br>PPM | Fe<br>PCT | As<br>PPM | Au<br>PPB | Au/wt<br>G | Au/wt<br>G |
|------------------|------------------|-----------|-----------|-----------|-----------|-----------|-----------|------------|------------|
| S1 L5+00W 3+50S  |                  | 49        | 65        | <0.1      | 6.60      | 5         | 20        | 10.0       |            |
| S1 L5+00W 3+75S  |                  | 63        | 90        | 0.2       | 6.60      | 6         | <5        | 10.0       |            |
| S1 L5+00W 4+00S  |                  | 38        | 40        | <0.1      | 6.80      | 6         | <5        | 8.0        |            |
| S1 L5+00W 4+25S  |                  | 60        | 42        | <0.1      | 6.80      | 5         | <5        |            | 10.0       |
| S1 L5+50W 0+00S  |                  | 20        | 50        | 0.1       | >10.00    | 5         | <5        | 10.0       |            |
| S1 L5+50W 0+25S  |                  | 52        | 42        | <0.1      | 7.00      | 6         | <5        | 10.0       |            |
| S1 L5+50W 0+50S  |                  | 32        | 23        | <0.1      | 8.40      | 4         | <5        | 10.0       |            |
| S1 L5+50W 0+75S  |                  | 30        | 26        | 0.1       | 8.20      | 4         | <5        | 10.0       |            |
| S1 L5+50W 1+00S  |                  | 50        | 42        | 0.1       | 6.60      | 4         | <5        | 10.0       |            |
| S1 L5+50W 1+25S  |                  | 12        | 20        | <0.1      | 7.20      | 3         | <5        | 10.0       |            |
| S1 L5+50W 1+50S  |                  | 42        | 40        | <0.1      | 7.00      | 3         | <5        | 10.0       |            |
| S1 L5+50W 1+75S  |                  | 42        | 42        | 0.1       | 6.20      | 2         | <5        | 10.0       |            |
| S1 L5+50W 2+00S  |                  | 30        | 110       | <0.1      | 4.60      | 9         | 25        | 10.0       |            |
| S1 L5+50W 2+25S  |                  | 30        | 120       | <0.1      | 4.20      | 6         | 130       | 10.0       |            |
| S1 L5+50W 2+50S  |                  | 40        | 79        | 0.1       | 4.20      | 10        | <5        | 10.0       |            |
| S1 L5+50W 2+75S  |                  | 28        | 69        | 0.1       | 4.00      | 9         | 640       | 5.0        |            |
| S1 L5+50W 3+00S  |                  | 20        | 50        | 0.2       | 4.60      | 10        | <5        | 10.0       |            |
| S1 L5+50W 3+25S  |                  | 31        | 80        | <0.1      | 3.90      | 8         | 60        | 7.0        |            |
| S1 L5+50W 3+50S  |                  | 21        | 75        | <0.1      | 4.20      | 8         | <5        | 10.0       |            |
| S1 L5+50W 3+75S  |                  | 30        | 95        | <0.1      | 3.40      | 5         | 65        | 10.0       |            |
| S1 L5+50W 4+00S  |                  | 49        | 40        | <0.1      | 6.40      | 5         | 15        | 10.0       |            |
| S1 L5+50W 4+25S  |                  | 49        | 51        | <0.1      | 6.60      | 5         | <5        | 10.0       |            |
| S1 L6+00W 0+00S  |                  | 60        | 33        | <0.1      | 5.00      | 3         | <5        | 2.0        | 8.0        |
| S1 L6+00W 0+25S  |                  | 7         | 10        | 0.1       | 9.20      | 3         | <5        | 6.0        |            |
| S1 L6+00W 0+50S  |                  | 20        | 29        | 0.1       | 7.80      | 2         | <5        | 10.0       |            |
| S1 L6+00W 0+75S  |                  | 12        | 20        | 0.1       | 9.00      | 2         | <5        | 8.0        |            |
| S1 L6+00W 1+00S  |                  | 31        | 38        | <0.1      | 8.00      | 3         | <5        | 10.0       |            |
| S1 L6+00W 1+25S  |                  | 20        | 22        | <0.1      | 8.20      | 4         | 5         | 10.0       |            |
| S1 L6+00W 1+50S  |                  | 10        | 19        | 0.1       | 4.40      | 2         | <5        | 10.0       |            |
| S1 L6+00W 1+75S  |                  | 42        | 158       | 0.4       | 3.10      | 5         | 190       | 3.0        | 7.0        |
| S1 L6+00W 2+00S  |                  | 38        | 138       | 0.2       | 3.60      | 7         | 100       | 6.0        |            |
| S1 L6+00W 2+25S  |                  | 39        | 62        | <0.1      | 4.40      | 9         | 50        | 10.0       |            |
| S1 L6+00W 2+50S  |                  | 32        | 70        | <0.1      | 4.60      | 9         | <5        | 8.0        |            |
| S1 L6+00W 2+75S  |                  | 22        | 58        | <0.1      | 4.40      | 8         | <5        | 8.0        |            |
| S1 L6+00W 3+00S  |                  | 30        | 75        | 0.2       | 4.60      | 8         | <5        | 10.0       |            |
| S1 L6+00W 3+25S  |                  | 12        | 45        | 0.1       | 4.80      | 10        | <5        | 6.0        |            |
| S1 L6+00W 3+50S  |                  | 40        | 100       | <0.1      | 5.60      | 10        | <5        | 10.0       |            |
| S1 L6+00W 3+75S  |                  | 21        | 63        | <0.1      | 6.00      | 9         | <5        | 10.0       |            |
| S1 L6+00W 4+00S  |                  | 32        | 70        | 0.2       | 4.20      | 6         | <5        | 10.0       |            |
| S1 L6+00W 4+25S  |                  | 30        | 98        | 0.1       | 4.40      | 6         | 10        | 10.0       |            |





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| SAMPLE<br>NUMBER | ELEMENT<br>UNITS | Cu<br>PPM | Zn<br>PPM | Ag<br>PPM | Fe<br>PCT | As<br>PPM | Au<br>PPB | Au/wt<br>G | Au/wt<br>G |
|------------------|------------------|-----------|-----------|-----------|-----------|-----------|-----------|------------|------------|
| S1 L6+50W 0+00S  |                  | 30        | 40        | 0.1       | 6.40      | 4         | 10        | 4.0        | 6.0        |
| S1 L6+50W 0+50S  |                  | 52        | 38        | <0.1      | 4.40      | 4         | <5        | 10.0       |            |
| S1 L6+50W 0+75S  |                  | 13        | 19        | 0.1       | 9.40      | 5         | <5        | 5.0        |            |
| S1 L6+50W 1+00S  |                  | 28        | 20        | 0.1       | 6.00      | 4         | <5        | 8.0        |            |
| S1 L6+50W 2+00S  |                  | 12        | 40        | <0.1      | 4.20      | 6         | <5        | 2.0        | 8.0        |
| S1 L6+50W 2+50S  |                  | 19        | 31        | <0.1      | 4.40      | 4         | <5        | 5.0        |            |
| S1 L6+50W 2+75S  |                  | 30        | 79        | 0.1       | 4.60      | 7         | <5        | 4.0        | 6.0        |
| S1 L6+50W 3+00S  |                  | 28        | 75        | <0.1      | 5.40      | 6         | <5        | 10.0       |            |
| S1 L6+50W 3+25S  |                  | 30        | 70        | <0.1      | 5.00      | 5         | <5        | 10.0       |            |
| S1 L6+50W 3+50S  |                  | 11        | 21        | <0.1      | 5.80      | 4         | <5        | 10.0       |            |
| S1 L6+50W 3+75S  |                  | 30        | 70        | 0.1       | 4.40      | 5         | <5        | 10.0       |            |
| S1 L6+50W 4+00S  |                  | 35        | 70        | 0.1       | 4.40      | 6         | <5        | 5.0        |            |
| S1 L6+50W 4+25S  |                  | 47        | 82        | 0.1       | 5.20      | 6         | <5        | 10.0       |            |
| S1 L7+00W 0+00S  |                  | 41        | 61        | 0.2       | 6.80      | 4         | 10        | 10.0       |            |
| S1 L7+00W 0+25S  |                  | 12        | 31        | 0.1       | 6.40      | 3         | 5         | 4.0        | 6.0        |
| S1 L7+00W 0+50S  |                  | 32        | 90        | 0.2       | 5.80      | 2         | 300       | 10.0       |            |
| S1 L7+00W 0+75S  |                  | 30        | 62        | 0.1       | 6.60      | 3         | 15        | 3.0        | 7.0        |
| S1 L7+00W 1+00S  |                  | 50        | 55        | <0.1      | 5.00      | 3         | <5        | 7.0        |            |
| S1 L7+00W 1+25S  |                  | 20        | 24        | 0.1       | 6.20      | 4         | 20        | 10.0       |            |
| S1 L7+00W 1+50S  |                  | 32        | 40        | 0.2       | 6.80      | 5         | 40        | 7.0        |            |
| S1 L7+00W 1+75S  |                  | 19        | 18        | 0.1       | 5.00      | 5         | <5        | 7.0        |            |
| S1 L7+00W 2+00S  |                  | 20        | 40        | 0.1       | 4.80      | 6         | <5        | 7.0        |            |
| S1 L7+00W 2+25S  |                  | 23        | 40        | <0.1      | 5.40      | 6         | <5        | 10.0       |            |
| S1 L7+00W 2+50S  |                  | 22        | 60        | 0.1       | 4.40      | 8         | <5        | 2.0        | 8.0        |
| S1 L7+00W 2+75S  |                  | 22        | 60        | 0.1       | 4.00      | 9         | <5        | 6.0        |            |
| S1 L7+00W 3+00S  |                  | 30        | 59        | 0.1       | 4.80      | 8         | <5        | 10.0       |            |
| S1 L7+00W 3+25S  |                  | 20        | 45        | <0.1      | 5.00      | 8         | <5        | 10.0       |            |
| S1 L7+00W 3+50S  |                  | 20        | 50        | 0.2       | 4.80      | 8         | <5        | 10.0       |            |
| S1 L7+00W 3+75S  |                  | 32        | 80        | <0.1      | 4.00      | 9         | <5        | 2.0        | 8.0        |
| S1 L7+00W 4+00S  |                  | 26        | 62        | <0.1      | 3.25      | 10        | <5        | 5.0        |            |
| S1 L7+00W 4+25S  |                  | 25        | 47        | <0.1      | 3.75      | 8         | <5        | 10.0       |            |
| T1 L1+77N 5+05W  |                  | 10        | 22        | <0.1      | 8.60      | 2         | 10        | 5.0        |            |
| T1 L2+00N 5+25W  |                  | 13        | 50        | 0.1       | 6.00      | 2         | <5        | 1.0        | 9.0        |
| T1 L7+15W 1+50N  |                  | 30        | 50        | <0.1      | 3.80      | <2        | <5        | 8.0        |            |
| T1 L7+55W 1+30N  |                  | 65        | 59        | 0.4       | 3.00      | <2        | <5        | 8.0        |            |
| T1 L8+50W 1+50N  |                  | 13        | 10        | 0.3       | 1.00      | <2        | <5        | 4.0        | 6.0        |

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PROJECT: BEAR

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| SAMPLE<br>NUMBER | ELEMENT<br>UNITS | Cu<br>PPM | Zn<br>PPM | Ag<br>PPM | Fe<br>PCT | As<br>PPM | Au<br>PPB | Au/wt<br>G | Au/wt<br>G |
|------------------|------------------|-----------|-----------|-----------|-----------|-----------|-----------|------------|------------|
| S1 0+00W 0+50N   |                  | 3         | 12        | <0.1      | 1.60      | 2         | <5        |            |            |
| S1 0+00W 2+25N   |                  | 4         | 5         | <0.1      | 1.20      | 2         | <5        |            | 5.0        |
| S1 0+00W 3+75N   |                  | 15        | 35        | <0.1      | 7.00      | 3         | <5        | 10.0       |            |
| S1 0+00W 4+00N   |                  | 8         | 33        | <0.1      | 5.40      | 4         | <5        | 10.0       |            |
| S1 0+00W 4+50N   |                  | 3         | 11        | <0.1      | 1.50      | 2         | <5        | 8.0        | 2.0        |
| S1 0+00W 5+25N   |                  | 19        | 31        | <0.1      | 5.20      | 7         | 30        |            |            |
| S1 0+00W 5+75N   |                  | 2         | 9         | <0.1      | 1.00      | <2        | <5        | 9.0        |            |
| S1 0+00W 6+00N   |                  | 22        | 83        | <0.1      | >10.00    | 3         | <5        | 10.0       |            |
| S1 0+00W 6+25N   |                  | 8         | 18        | <0.1      | 4.20      | 2         | <5        | 10.0       |            |
| S1 0+00W 0+00S   |                  | 36        | 48        | <0.1      | 6.40      | 8         | <5        | 10.0       |            |
| S1 0+00W 0+25S   |                  | 30        | 28        | <0.1      | 5.00      | 7         | <5        | 8.0        |            |
| S1 0+00W 0+50S   |                  | 38        | 48        | <0.1      | 6.00      | 7         | <5        |            | 5.0        |
| S1 0+00W 0+75S   |                  | 8         | 20        | <0.1      | 4.80      | 2         | <5        | 8.0        |            |
| S1 0+00W 3+50S   |                  | 10        | 28        | <0.1      | 6.00      | 2         | 5         | 10.0       |            |
| S1 0+00W 4+00S   |                  | 99        | 80        | <0.1      | 6.00      | 6         | 40        |            |            |
| S1 0+00W 4+25S   |                  | 95        | 80        | 0.2       | 6.00      | 7         | 5         |            |            |
| S1 0+00W 5+00S   |                  | 104       | 82        | <0.1      | 6.60      | 8         | <5        |            | 7.0        |
| S1 0+50W 0+25N   |                  | 7         | 8         | <0.1      | 1.35      | 2         | <5        | 5.0        |            |
| S1 0+50W 1+00N   |                  | 23        | 30        | <0.1      | 7.00      | 2         | <5        | 10.0       |            |
| S1 0+50W 1+25N   |                  | 8         | 12        | <0.1      | 2.90      | 2         | <5        | 7.0        |            |
| S1 0+50W 2+00N   |                  | 20        | 20        | 0.2       | 9.20      | 2         | <5        | 8.0        | 2.0        |
| S1 0+50W 2+00S   |                  | 5         | 3         | <0.1      | 1.45      | <2        | <5        |            | 5.0        |
| S1 0+50W 2+50S   |                  | 25        | 42        | <0.1      | 10.00     | 4         | <5        | 10.0       |            |
| S1 0+50W 3+25S   |                  | 18        | 38        | <0.1      | >10.00    | 4         | <5        | 10.0       |            |
| S1 0+50W 3+50S   |                  | 45        | 43        | <0.1      | 7.40      | 6         | <5        | 3.0        |            |
| S1 1+00W 0+00N   |                  | 15        | 13        | <0.1      | 5.00      | 5         | <5        | 4.0        |            |
| S1 1+00W 0+25N   |                  | 15        | 18        | <0.1      | 6.00      | 7         | <5        | 4.0        |            |
| S1 1+00W 0+50N   |                  | 27        | 20        | <0.1      | >10.00    | 5         | <5        | 9.0        | 1.0        |
| S1 1+00W 0+75N   |                  | 87        | 60        | <0.1      | 6.20      | 60        | 60        |            | 6.0        |
| S1 1+00W 1+00N   |                  | 39        | 42        | <0.1      | 6.80      | 27        | 20        | 8.0        | 2.0        |
| S1 1+00W 5+00N   |                  | 37        | 23        | <0.1      | 8.20      | 4         | 5         | 10.0       |            |
| S1 1+00W 5+25N   |                  | 38        | 22        | <0.1      | 8.00      | 5         | <5        | 7.0        |            |
| S1 1+00W 5+50N   |                  | 24        | 30        | <0.1      | 9.80      | 4         | <5        | 8.0        | 2.0        |
| S1 1+00W 5+75N   |                  | 79        | 69        | <0.1      | 7.00      | 5         | 30        |            | 8.0        |
| S1 1+00W 6+00N   |                  | 39        | 28        | <0.1      | 7.80      | 5         | <5        | 8.0        | 2.0        |
| S1 1+00W 6+25N   |                  | 40        | 29        | <0.1      | 6.00      | 3         | 10        | 6.0        | 4.0        |
| S1 1+00W 6+50N   |                  | 28        | 20        | <0.1      | 5.80      | 4         | 25        |            |            |
| S1 1+00W 6+75N   |                  | 31        | 33        | <0.1      | 7.00      | 3         | 10        |            | 6.0        |
| S1 1+00W 7+00N   |                  | 29        | 30        | <0.1      | 6.00      | 4         | <5        | 6.0        | 4.0        |
| S1 1+00W 7+25N   |                  | 8         | 10        | <0.1      | 2.70      | 2         | <5        | 6.0        | 4.0        |



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| SAMPLE<br>NUMBER | ELEMENT<br>UNITS | Cu<br>PPM | Zn<br>PPM | Ag<br>PPM | Fe<br>PCT | As<br>PPM | Au<br>PPB | Au/wt<br>G | Au/wt<br>G |
|------------------|------------------|-----------|-----------|-----------|-----------|-----------|-----------|------------|------------|
| S1 1+00W 0+50S   |                  | 11        | 67        | <0.1      | 4.20      | 4         | <5        | 4.0        |            |
| S1 1+00W 1+00S   |                  | 9         | 23        | <0.1      | 5.00      | 2         | 480       |            | 7.0        |
| S1 1+00W 1+75S   |                  | 14        | 40        | 0.2       | 8.00      | 4         | <5        | 10.0       |            |
| S1 1+00W 2+25S   |                  | 8         | 42        | <0.1      | 5.00      | 3         | <5        | 2.0        |            |
| S1 1+00W 2+50S   |                  | 21        | 53        | <0.1      | 7.60      | 3         | <5        | 4.0        |            |
| S1 1+00W 3+00S   |                  | 4         | 32        | <0.1      | 2.50      | 2         | <5        | 4.0        |            |
| S1 1+00W 3+75S   |                  | 5         | 30        | <0.1      | 2.30      | <2        | <5        | 5.0        |            |
| S1 1+00W 4+00S   |                  | 5         | 23        | <0.1      | 5.00      | 3         | <5        | 6.0        |            |
| S1 1+50W 0+00N   |                  | 8         | 11        | <0.1      | 3.95      | 3         | 5         | 10.0       |            |
| S1 1+50W 4+25S   |                  | 5         | 10        | <0.1      | 2.40      | <2        | <5        | 6.0        | 2.0        |
| S1 2+00W 0+00N   |                  | 11        | 10        | <0.1      | 5.40      | 4         | 25        |            | 5.0        |
| S1 2+00W 0+25N   |                  | 90        | 40        | <0.1      | 8.80      | 8         | 5         |            |            |
| S1 2+00W 0+50N   |                  | 79        | 39        | 0.2       | 9.20      | 7         | 50        | 7.0        | 3.0        |
| S1 2+00W 0+75N   |                  | 130       | 80        | 0.2       | 6.00      | 40        | 20        |            | 5.0        |
| S1 2+00W 1+00N   |                  | 68        | 78        | <0.1      | 5.00      | 70        | 20        |            | 10.0       |
| S1 2+00W 1+25N   |                  | 29        | 40        | <0.1      | 5.00      | 7         | 25        | 10.0       |            |
| S1 2+00W 1+75N   |                  | 112       | 78        | <0.1      | 6.40      | 44        | 25        |            | 8.0        |
| S1 2+00W 2+00N   |                  | 152       | 82        | <0.1      | 6.20      | 10        | 15        | 10.0       |            |
| S1 2+00W 2+25N   |                  | 137       | 80        | <0.1      | 6.60      | 7         | 15        |            |            |
| S1 2+00W 2+50N   |                  | 112       | 76        | <0.1      | 6.00      | 8         | 10        |            | 7.0        |
| S1 2+00W 2+75N   |                  | 109       | 80        | <0.1      | 6.20      | 10        | 5         | 10.0       |            |
| S1 2+00W 5+00N   |                  | 88        | 50        | <0.1      | 6.40      | 7         | 10        |            |            |
| S1 2+00W 5+25N   |                  | 44        | 29        | <0.1      | 5.20      | 3         | <5        |            | 6.0        |
| S1 2+00W 5+50N   |                  | 38        | 30        | 0.2       | 6.40      | 5         | 5         | 8.0        | 2.0        |
| S1 2+00W 5+75N   |                  | 35        | 30        | <0.1      | 7.20      | 5         | <5        | 7.0        | 3.0        |
| S1 2+00W 6+00N   |                  | 68        | 30        | 0.2       | 7.00      | 5         | 20        | 10.0       |            |
| S1 2+00W 6+25N   |                  | 39        | 28        | <0.1      | 5.40      | 5         | <5        |            | 9.0        |
| S1 2+00W 6+50N   |                  | 42        | 35        | <0.1      | 5.80      | 4         | 10        | 8.0        | 2.0        |
| S1 2+00W 6+75N   |                  | 36        | 26        | <0.1      | 8.00      | 4         | <5        |            | 6.0        |
| S1 2+00W 7+00N   |                  | 103       | 42        | <0.1      | 6.00      | 7         | 15        | 6.0        | 4.0        |
| S1 2+00W 7+25N   |                  | 87        | 48        | <0.1      | 4.60      | 4         | 5         |            | 7.0        |
| S1 2+00W 7+50N   |                  | 62        | 42        | <0.1      | 6.00      | 8         | 10        |            | 6.0        |
| S1 2+00W 0+00S   |                  | 19        | 19        | <0.1      | 7.20      | 5         | 5         | 8.0        | 2.0        |
| S1 2+00W 0+25S   |                  | 12        | 20        | <0.1      | 7.00      | 5         | <5        | 8.0        | 2.0        |
| S1 2+00W 0+75S   |                  | 6         | 20        | <0.1      | 2.60      | 2         | 5         | 6.0        | 4.0        |
| S1 2+00W 2+00S   |                  | 5         | 5         | <0.1      | 2.20      | 2         | <5        | 6.0        | 4.0        |
| S1 2+00W 2+50S   |                  | 4         | 10        | <0.1      | 1.60      | 3         | 20        |            | 5.0        |
| S1 2+00W 2+75S   |                  | 7         | 20        | <0.1      | 2.20      | 2         | <5        | 9.0        |            |
| S1 2+00W 3+25S   |                  | 13        | 19        | <0.1      | 3.45      | 2         | 5         | 7.0        | 3.0        |
| S1 2+00W 3+50S   |                  | 16        | 20        | <0.1      | 3.95      | <2        | 5         | 6.0        |            |



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| SAMPLE<br>NUMBER | ELEMENT<br>UNITS | Cu<br>PPM | Zn<br>PPM | Ag<br>PPM | Fe<br>PCT | As<br>PPM | Au<br>PPB | Au/wt<br>G | Au/wt<br>G |
|------------------|------------------|-----------|-----------|-----------|-----------|-----------|-----------|------------|------------|
| S1 2+00W 3+75N   |                  | 3         | 8         | <0.1      | 1.15      | 2         | 5         |            |            |
| S1 2+00W 4+25S   |                  | 9         | 12        | <0.1      | 3.30      | 2         | 10        |            | 7.0        |
| S1 2+50W 0+00S   |                  | 28        | 22        | <0.1      | 7.00      | 3         | <5        |            | 6.0        |
| S1 2+50W 0+25S   |                  | 32        | 21        | <0.1      | 7.00      | 6         | 15        |            | 8.0        |
| S1 2+50W 1+25S   |                  | 37        | 82        | <0.1      | >10.00    | <2        | <5        | 9.0        | 1.0        |
| S1 2+50W 1+50S   |                  | 43        | 91        | <0.1      | >10.00    | 4         | <5        | 6.0        |            |
| S1 2+50W 1+75S   |                  | 46        | 94        | <0.1      | >10.00    | 3         | <5        | 8.0        | 2.0        |
| S1 3+00W 0+00N   |                  | 72        | 38        | <0.1      | >10.00    | 10        | 10        |            |            |
| S1 3+00W 0+25N   |                  | 40        | 28        | 0.2       | 9.20      | 9         | 10        | 10.0       |            |
| S1 3+00W 0+50N   |                  | 89        | 40        | <0.1      | >10.00    | 8         | 15        | 7.0        | 3.0        |
| S1 3+00W 0+75N   |                  | 84        | 41        | <0.1      | >10.00    | 9         | 35        |            | 5.0        |
| S1 3+00W 3+00N   |                  | 98        | 40        | <0.1      | 8.20      | 4         | 10        | 10.0       |            |
| S1 3+00W 3+25N   |                  | 29        | 32        | 0.6       | 9.20      | 5         | <5        | 7.0        | 3.0        |
| S1 3+00W 3+50N   |                  | 84        | 40        | <0.1      | 8.00      | 6         | <5        | 7.0        | 3.0        |
| S1 3+00W 3+75N   |                  | 69        | 38        | <0.1      | 8.40      | 5         | <5        |            | 6.0        |
| S1 3+00W 4+00N   |                  | 52        | 35        | <0.1      | >10.00    | 4         | <5        |            | 5.0        |
| S1 3+00W 4+25N   |                  | 24        | 50        | <0.1      | >10.00    | 5         | 15        |            | 6.0        |
| S1 3+00W 4+50N   |                  | 64        | 46        | <0.1      | >10.00    | 5         | <5        |            | 5.0        |
| S1 3+00W 4+75N   |                  | 69        | 43        | <0.1      | >10.00    | 4         | <5        |            | 5.0        |
| S1 3+00W 0+50S   |                  | 24        | 22        | <0.1      | 8.80      | 3         | <5        | 8.0        | 2.0        |
| S1 3+00W 1+00S   |                  | 6         | 17        | <0.1      | 2.60      | 3         | <5        |            | 7.0        |
| S1 3+00W 1+25S   |                  | 12        | 26        | <0.1      | 7.00      | 2         | 10        | 8.0        | 2.0        |
| S1 3+00W 1+50S   |                  | 8         | 12        | <0.1      | 2.35      | 2         | <5        |            |            |
| S1 3+00W 1+75S   |                  | 18        | 42        | <0.1      | 8.20      | 5         | <5        | 10.0       |            |
| S1 3+00W 2+00S   |                  | 10        | 23        | <0.1      | 3.45      | 2         | <5        |            | 5.0        |
| S1 3+00W 2+25S   |                  | 4         | 5         | <0.1      | 1.25      | 2         | <5        | 8.0        | 2.0        |
| S1 3+00W 2+50S   |                  | 19        | 29        | <0.1      | >10.00    | 3         | <5        |            | 8.0        |
| S1 3+00W 2+75S   |                  | 29        | 51        | <0.1      | >10.00    | 5         | <5        |            |            |
| S1 3+00W 3+25S   |                  | 60        | 70        | <0.1      | 7.00      | 5         | <5        |            | 5.0        |
| S1 3+00W 3+50S   |                  | 88        | 63        | <0.1      | 7.00      | 5         | <5        |            |            |
| S1 3+00W 4+00S   |                  | 33        | 40        | <0.1      | 7.00      | 4         | <5        | 3.0        |            |
| S1 3+00W 4+25S   |                  | 52        | 61        | <0.1      | 4.80      | 3         | <5        |            |            |
| S1 3+50W 0+00S   |                  | 14        | 41        | 0.2       | 4.20      | IS        | <5        |            |            |
| S1 3+50W 0+25S   |                  | 9         | 12        | <0.1      | 5.80      | 2         | <5        | 7.0        | 3.0        |
| S1 3+50W 0+50S   |                  | 4         | 11        | <0.1      | 2.80      | <2        | 15        |            | 5.0        |
| S1 3+50W 1+00S   |                  | 19        | 23        | <0.1      | >10.00    | 2         | <5        | 6.0        |            |
| S1 3+50W 1+25S   |                  | 3         | 5         | <0.1      | 3.00      | <2        | <5        | 5.0        |            |
| S1 3+50W 1+50S   |                  | 6         | 10        | <0.1      | 3.30      | 2         | <5        |            | 7.0        |
| S1 3+50W 1+75S   |                  | 12        | 19        | <0.1      | 7.40      | 3         | <5        | 10.0       |            |
| S1 3+50W 2+00S   |                  | 10        | 22        | <0.1      | 8.20      | 3         | <5        |            |            |



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| SAMPLE<br>NUMBER | ELEMENT<br>UNITS | Cu<br>PPM | Zn<br>PPM | Ag<br>PPM | Fe<br>PCT | As<br>PPM | Au<br>PPB | Au/wt<br>G | Au/wt<br>G |
|------------------|------------------|-----------|-----------|-----------|-----------|-----------|-----------|------------|------------|
| S1 3+50W 2+75S   |                  | 7         | 7         | <0.1      | 2.40      | <2        | <5        |            | 8.0        |
| S1 3+50W 3+25S   |                  | 68        | 59        | <0.1      | 8.80      | 5         | 15        |            |            |
| S1 3+50W 3+75S   |                  | 110       | 79        | <0.1      | 5.60      | 5         | <5        |            |            |
| S1 3+50W 4+00S   |                  | 65        | 48        | <0.1      | 6.20      | 6         | <5        |            |            |
| S1 3+50W 4+25S   |                  | 43        | 40        | 0.2       | 6.80      | 4         | <5        | 6.0        | 4.0        |
| S1 4+00W 0+00N   |                  | 14        | 18        | <0.1      | 6.40      | 5         | 110       | 6.0        | 4.0        |
| S1 4+00W 0+25N   |                  | 77        | 50        | <0.1      | 5.60      | 10        | <5        | 8.0        | 2.0        |
| S1 4+00W 0+50N   |                  | 122       | 68        | 0.3       | 8.80      | 30        | <5        |            | 6.0        |
| S1 4+00W 1+00N   |                  | 63        | 78        | <0.1      | 7.80      | 6         | 25        |            | 9.0        |
| S1 4+00W 1+50N   |                  | 159       | 92        | <0.1      | 7.00      | 5         | <5        |            |            |
| S1 4+00W 2+25N   |                  | 69        | 42        | <0.1      | 9.00      | 6         |           |            |            |
| S1 4+00W 2+50N   |                  | 35        | 20        | 0.2       | 8.00      | 3         | <5        | 7.0        | 3.0        |
| S1 4+00W 2+75N   |                  | 17        | 20        | <0.1      | 8.40      | 4         | 10        |            | 8.0        |
| S1 4+00W 3+00N   |                  | 84        | 46        | 0.6       | 7.20      | 5         | 75        |            | 8.0        |
| S1 4+00W 3+25N   |                  | 110       | 60        | 0.1       | 8.00      | 5         | <5        |            |            |
| S1 4+00W 3+50N   |                  | 18        | 30        | 0.1       | 7.80      | 4         | <5        |            | 5.0        |
| S1 4+00W 3+75N   |                  | 20        | 28        | 0.2       | 10.00     | 5         | 25        |            |            |
| S1 4+00W 4+00N   |                  | 49        | 32        | 0.2       | 9.00      | 5         | <5        |            | 5.0        |
| S1 4+00W 4+50N   |                  | 45        | 50        | 0.1       | 9.00      | 5         | <5        |            | 5.0        |
| S1 4+00W 4+75N   |                  | 37        | 30        | <0.1      | >10.00    | 5         | 5         |            |            |
| S1 4+00W 5+00N   |                  | 105       | 36        | <0.1      | 9.00      | 3         | <5        |            |            |
| S1 4+00W 5+25N   |                  | 58        | 40        | <0.1      | >10.00    | 5         | 5         | 7.0        | 3.0        |
| S1 4+00W 7+00N   |                  | 26        | 30        | 0.2       | 8.20      | 4         | <5        |            | 7.0        |
| S1 12+50W 0+00N  |                  | 8         | 9         | <0.1      | 2.90      | 3         | <5        |            |            |
| S1 12+50W 1+00N  |                  | 6         | 7         | <0.1      | 1.40      | 2         | <5        |            |            |
| S1 12+50W 1+25N  |                  | 5         | 5         | <0.1      | 0.80      | 2         | 80        | 7.0        | 3.0        |
| S1 12+50W 1+50N  |                  | 5         | 5         | 0.2       | 0.95      | <2        | 15        |            |            |
| S1 12+50W 1+75N  |                  | 10        | 5         | <0.1      | 0.85      | 2         | 30        |            |            |
| S1 12+50W 0+50S  |                  | 13        | 30        | <0.1      | 3.65      | 7         | 5         |            | 7.0        |
| S1 12+50W 1+00S  |                  | 13        | 12        | <0.1      | 3.20      | 2         | <5        |            |            |
| S1 12+50W 1+50S  |                  | 33        | 132       | <0.1      | 5.00      | 10        | <5        |            | 6.0        |
| S1 12+50W 2+00S  |                  | 14        | 41        | <0.1      | 5.00      | 13        | 20        |            |            |
| S1 12+50W 2+25S  |                  | 41        | 115       | 0.9       | 4.80      | 38        | 65        |            | 7.0        |
| S1 12+50W 3+50S  |                  | 9         | 11        | <0.1      | 3.75      | 3         | <5        |            |            |
| S1 12+50W 4+25S  |                  | 17        | 64        | <0.1      | 9.00      | 15        | <5        |            |            |
| S1 13+00W 0+00N  |                  | 17        | 29        | <0.1      | 5.00      | 5         | 5         |            | 6.0        |
| S1 13+00W 0+25N  |                  | 11        | 10        | <0.1      | 2.65      | 3         | <5        |            |            |
| S1 13+00W 0+75N  |                  | 21        | 42        | <0.1      | 6.00      | 2         | <5        | 7.0        | 3.0        |
| S1 13+00W 1+50N  |                  | 2         | 3         | <0.1      | 0.95      | 2         | 5         |            | 5.0        |
| S1 13+00W 1+75N  |                  | 5         | 11        | <0.1      | 5.20      | 3         | 140       |            |            |





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| SAMPLE<br>NUMBER | ELEMENT<br>UNITS | Cu<br>PPM | Zn<br>PPM | Ag<br>PPM | Fe<br>PCT | As<br>PPM | Au<br>PPB | Au/wt<br>G | Au/wt<br>G |
|------------------|------------------|-----------|-----------|-----------|-----------|-----------|-----------|------------|------------|
| S1 13+00W 2+00N  |                  | 6         | 18        | <0.1      | 5.40      | 3         | 15        |            |            |
| S1 13+00W 0+50S  |                  | 22        | 71        | <0.1      | 5.20      | 11        | <5        |            | 9.0        |
| S1 13+00W 0+75S  |                  | 20        | 49        | <0.1      | 5.20      | 12        | <5        |            | 6.0        |
| S1 13+00W 1+00S  |                  | 23        | 30        | <0.1      | 6.00      | 6         | <5        |            | 8.0        |
| S1 13+50W 0+50N  |                  | 15        | 13        | <0.1      | 4.00      | 4         | 100       |            |            |
| S1 13+50W 1+25N  |                  | 8         | 10        | <0.1      | 3.45      | <2        | <5        |            | 9.0        |
| S1 13+50W 1+00S  |                  | 13        | 30        | <0.1      | 3.75      | 30        | <5        |            |            |
| S1 13+50W 1+25S  |                  | 7         | 150       | <0.1      | 4.00      | 11        | <5        |            |            |
| S1 13+50W 1+50S  |                  | 23        | 70        | <0.1      | 4.00      | 5         | <5        |            |            |
| S1 13+50W 2+25S  |                  | 10        | 54        | <0.1      | 3.70      | 16        | <5        |            |            |
| S1 13+50W 2+75S  |                  | 6         | 10        | <0.1      | 3.65      | 2         | <5        |            |            |
| S1 14+00W 0+00S  |                  | 6         | 15        | <0.1      | 2.20      | 2         | <5        |            |            |
| S1 14+00W 0+50S  |                  | 5         | 8         | <0.1      | 2.70      | 3         | <5        |            |            |
| S1 14+00W 1+50S  |                  | 17        | 21        | <0.1      | 4.00      | 8         | <5        |            |            |
| S1 14+00W 1+75S  |                  | 11        | 21        | <0.1      | 3.40      | 17        | 60        |            |            |
| S1 14+00W 2+00S  |                  | 550       | 270       | <0.1      | 6.20      | 51        | <5        |            |            |
| S1 14+00W 2+25S  |                  | 82        | 132       | <0.1      | 6.80      | 53        | 20        |            |            |

APPENDIX C

Geophysical Report on the Bear Claim Group  
By : Grant Hendrickson

**GEOPHYSICAL REPORT**

**ON THE**

**BEAR CLAIM GROUP,**

**KENNEDY RIVER GOLD DISTRICT,**

**WESTERN VANCOUVER ISLAND, B.C.**

**BY**

**DELTA GEOSCIENCE LTD.**

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## Introduction

At the request of International Coast Minerals Corporation, Delta Geoscience Ltd. conducted V.L.F., Magnetic and Gradiometer surveys on the Bear claim group. This claim group is located in the Kennedy River gold district of western Vancouver Island. The nearest settlement is the town of Uclulet.

The purpose of these surveys was to further define the spatial position of fault structures that are known to contain quartz veins. The known association of gold and quartz sulphide veins within these fault structures is the exploration target.

The geology of the claim group is discussed in reports by R.T. Henneberry, the geological consultant hired by International Coast Minerals.

Waldo W. Ejtél, the President of I.C.M. and Grant Hendrickson, the senior geophysicist for Delta Geoscience Ltd., were present in the field to assist in the initial planning and orientation of the geophysical work.

### Personnel

All the field work was conducted by Eric Hards, a junior geophysicist employed by Delta Geoscience Ltd. International Coast Minerals provided a helper to assist the geophysicist.

### Equipment

- 1 - Scintrex I.G.S. system configured as a VLF/MAG/GRADIOMETER.
- 1 - Scintrex MP-3 base station magnetometer.
- 1 - H.P. field computer system.

### Data Presentation

Data is presented in stacked plan of profile form at a scale of 1:2500. This format is ideal for showing the spatial position and strength of anomalous responses and facilitates interpretation. The spatial position of the V.L.F. conductor axis is shown by dashed lines.

A base station standard of 55900 nanotesla was assumed for this survey.

## Survey Procedures

I.C.M. had previously established a grid on the Bear claim group. Lines were orientated N-S to cross the structures at close to right angles. Line separation varied from 25m in the vicinity of the mineralized veins to 50m on the apparent strike projections of the vein. Station separation was 12.5 metres.

The Seattle V.L.F. station transmitting at 24.8 khz. was chosen for this survey, since it was on strike with the apparent location of structures and the proximity of the station ensured excellent field strength.

The magnetic data was corrected for the diurnal variation of the earth's magnetic field thru the base station magnetic monitor.

The gradiometer was used to highlight local anomalies, and eliminate the regional responses. Pyrrhotite mineralization present within the quartz vein system encouraged the use of the magnetometer and gradiometer.

The V.L.F. data was subsequently filtered using both the Fraser filter and the Hjelt filter. Both filters help to reduce topography affects. The Fraser filter gives a good indication of the spatial position of conductors. The Hjelt filter also does this, however provides an additional indication of the attitude and depth to the best part of the V.L.F. conductor.

Due to the nature of the terrain and vegetation present on the grid, accuracy in chaining and line location was difficult, thus errors in position  $\pm 7.5$  metres have to be expected and should be kept in mind when trenching or drilling anomalies.

## Discussion of the Data

A perusal of the filtered V.L.F. profile plan indicates two main structural trends, NW and EW. The EW trend appears to be a splay off the dominant NW trend. All of the presently known mineralization is contained in the EW trending structure between lines 1125W and 900W. The EW and NW trending structures appear to be faulted and offset by NE trending structures that would have been invisible to the V.L.F. due to their orientation with respect to the V.L.F. transmitter.

Moderate to weak V.L.F. responses were characteristic of the veins or structures present on the Bear grid. The NW trending structures on the south side of the grid generally have a stronger V.L.F. response than the EW trending structure. The stronger anomalies generally display a steep north dip. Weaker V.L.F. responses do not give a reliable dip indication however frequently closely spaced parallel structures/veins are indicated. The Hjelt filtered V.L.F. data gives a good indication of the depths to best test the V.L.F. conductors.

The magnetic data is complex. At times a direct correlation of anomalous magnetic response with a V.L.F. conductor was noted, suggesting pyrrhotite mineralization as the cause. In general, the magnetic responses were to the immediate north of the known quartz sulphide veins. Magnetic anomalies not associated with V.L.F. conductors may be caused by magnetic dikes possibly diabase.

The magnetics also suggest that a NE trending structure may, in part, be controlling the distribution of the stronger magnetic responses.

The strong magnetic response on L.1175W should be checked out by trenching. Three closely spaced zones are indicated. This strong magnetic anomaly has a flanking V.L.F. response.



## Conclusions & Recommendation

The VLF/MAG/GRADIOMETER surveys have accurately and cost effectively shown the spatial position of fault structures on the Bear claim group. Numerous trenching targets have been revealed. The geophysical response over the known mineralizations provide strong encouragement to test similar responses parallel to and on strike with the known mineralization.

The presence of pyrrhotite mineralization suggests that magnetic anomalies closely associated with V.L.F. conductors be checked by trenching. V.L.F. conductors without a magnetic response also should be checked with trenching, since the other sulphide minerals (pyrite, chalcopyrite and sphalerite) are not magnetic and pyrrhotite itself is quite variable in its magnetic susceptibility.

As it is quite easy to trench the anomalies found by this survey, I do not recommend any other geophysical technique at this time. If trenching becomes difficult and expensive, the sulphide content of the V.L.F. conductors could be evaluated thru induced polarization surveys prior to further trenching or drilling.



Grant A. Hendrickson.

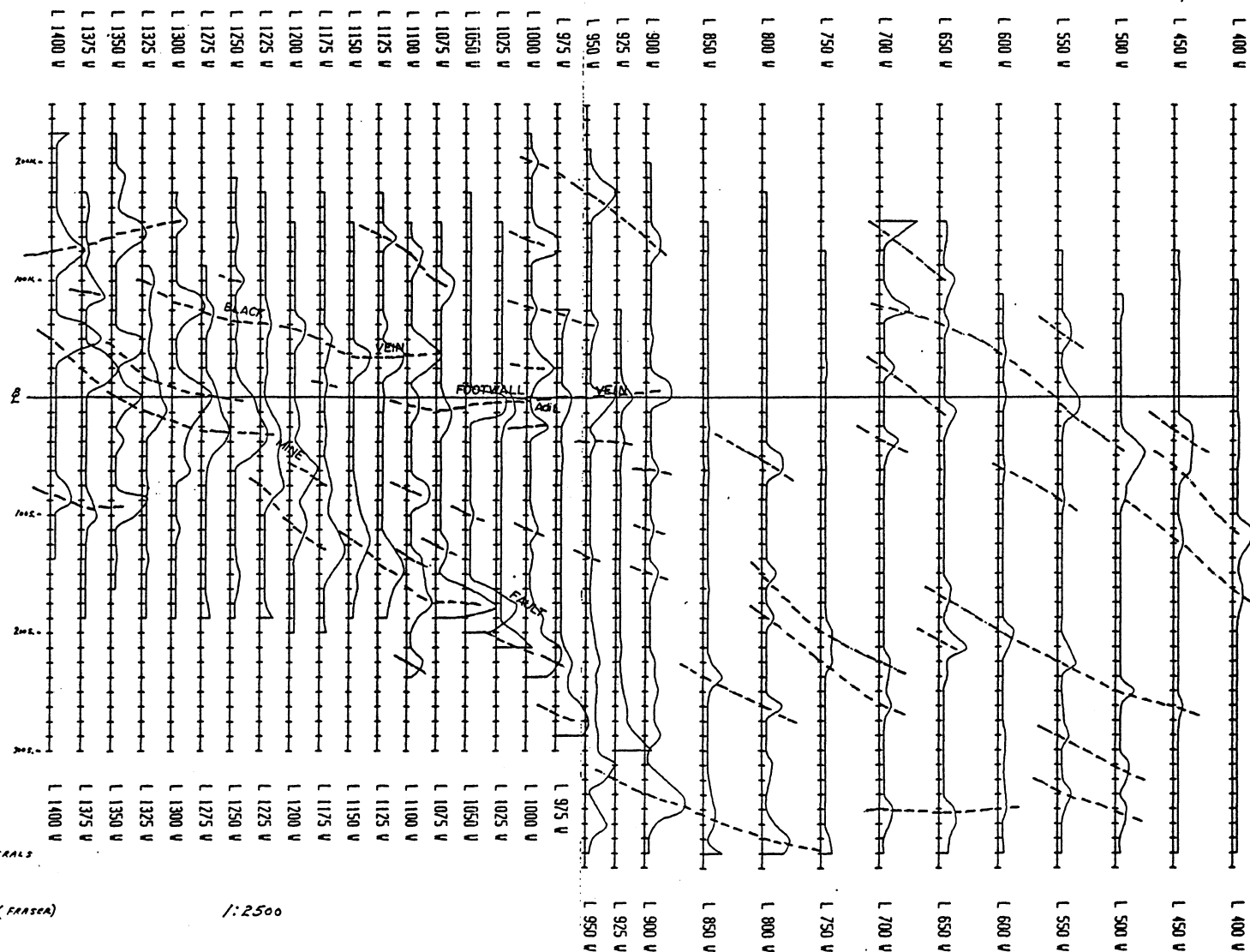
Statement of Qualification

Grant A. Hendrickson

- B.Science, U.B.C. 1971, Geophysics option.
- For the past 16 years, I have been actively involved in mineral exploration projects throughout Canada and the United States.
- I am a registered Professional Geophysicist with the Association of Professional Engineers, Geologists and Geophysicists of Alberta.
- I am an active member of the S.E.G., E.A.E.G., and C.I.M.



Grant A. Hendrickson.



INTERNATIONAL COAST MINERALS

BEAR PROTECT

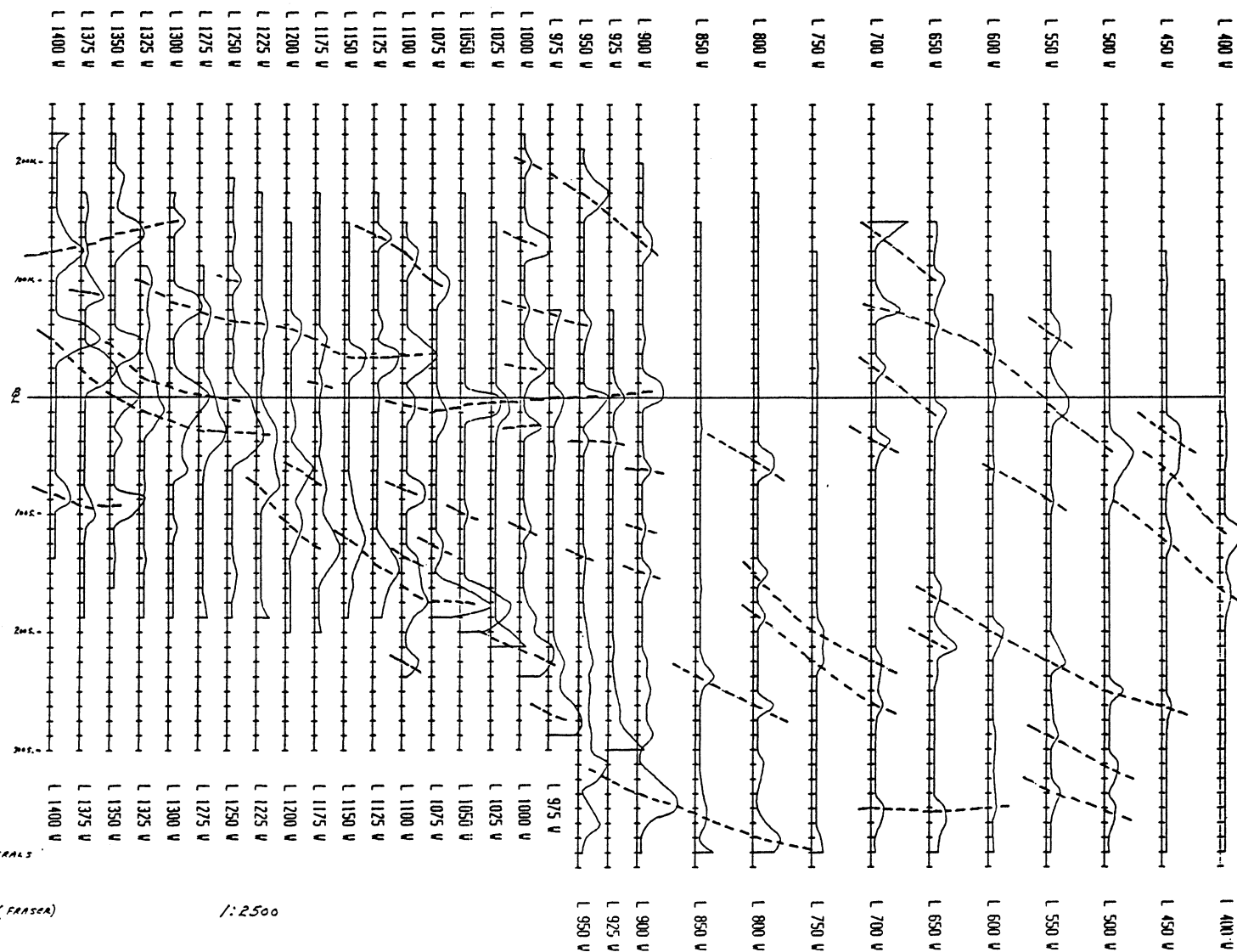
FILTERED VLF PROFILES (FRASER)

1cm = 25%, 1ms = 4%

SEATTLE VLF STATION 248386

1:2500

CONDUCTOR AXIS LOCATION



INTERNATIONAL COAST MINERALS

BEAR PROTECT

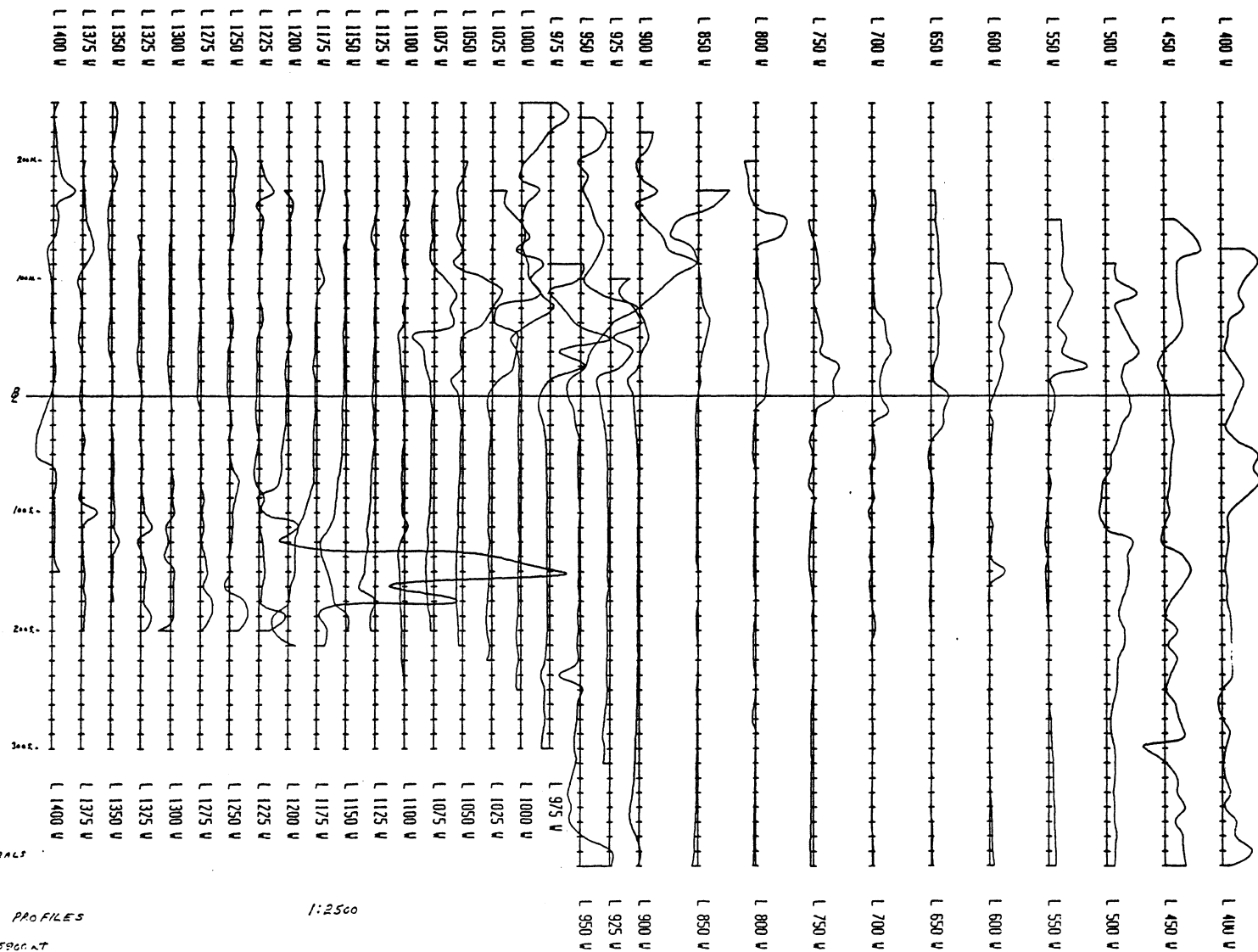
FILTERED VLF PROFILES (FRASER)

1:2500, 1000 - 400

SAMPLE VLF STATION 20000

1:2500

----- CONDUCTOR AXIS LOCATION



Z

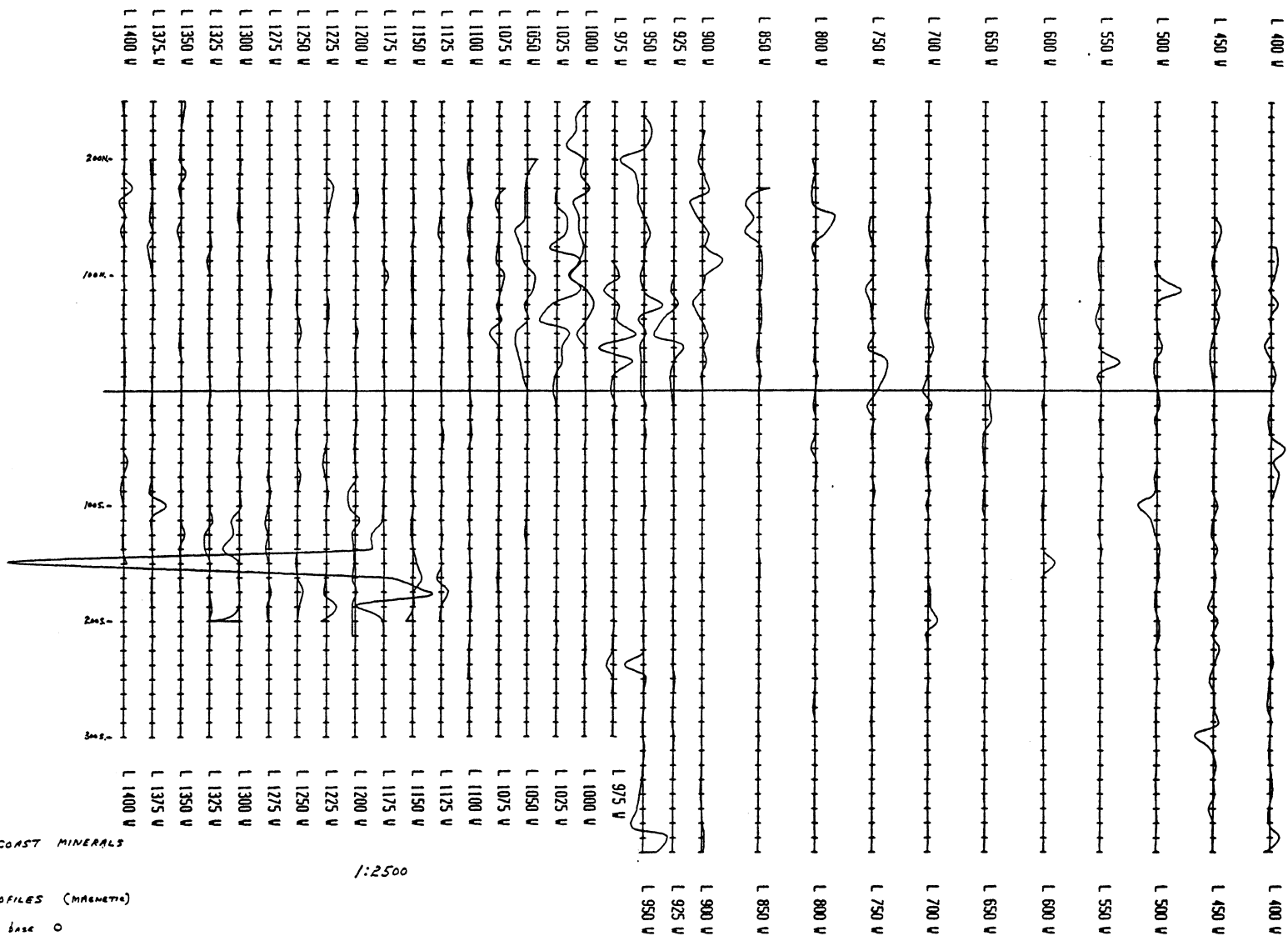
INTERNATIONAL COAST MINERALS

BEAR PROJECT

TOTAL FIELD MAGNETIC PROFILES

1 cm = 500 FT., base 5590 FT

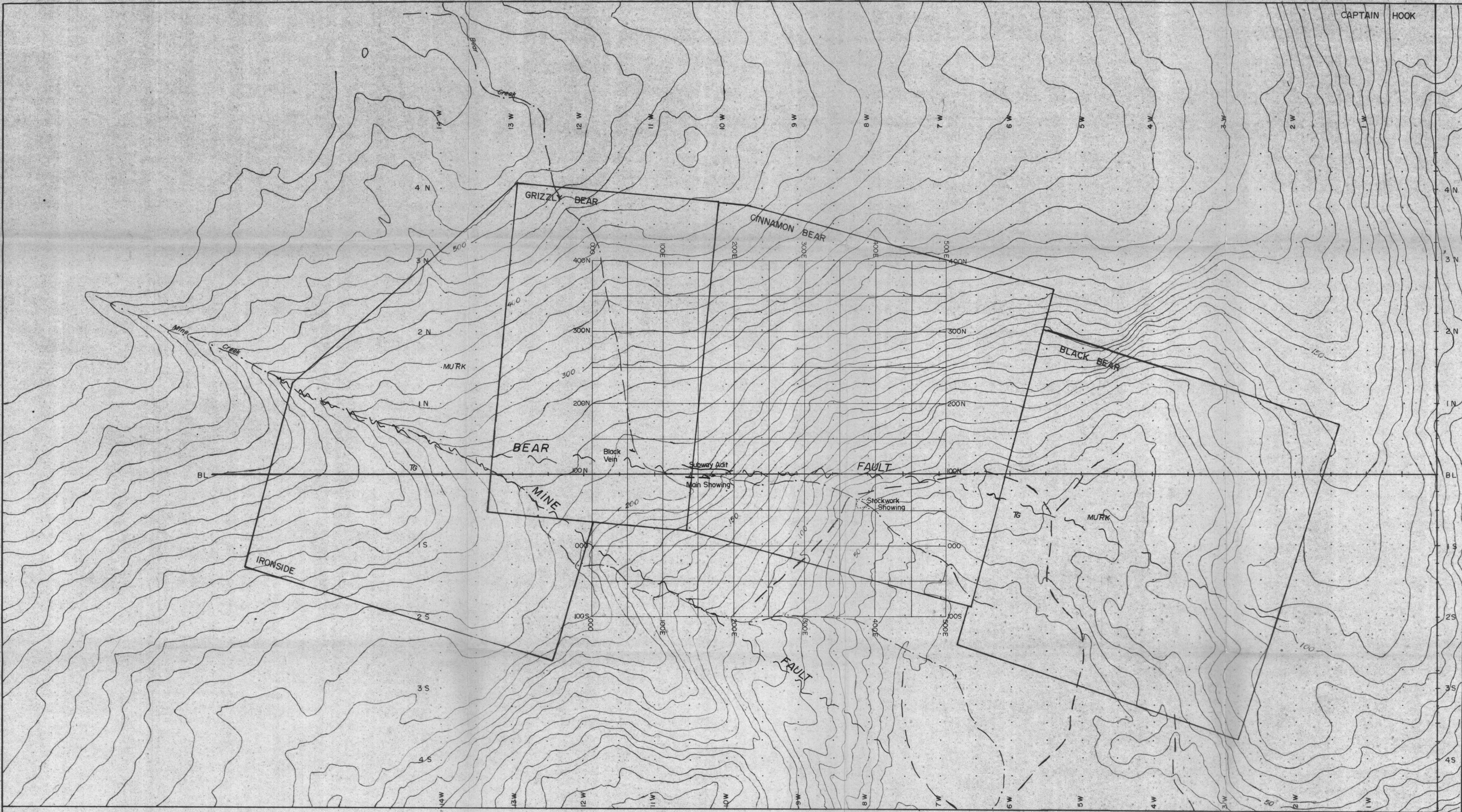
1:2500



INTERNATIONAL COAST MINERALS  
 BEAR PROJECT  
 GRADIOMETER PROFILES (MAGNETIC)  
 1cm = 200  $\frac{m}{\mu}$ , base 0

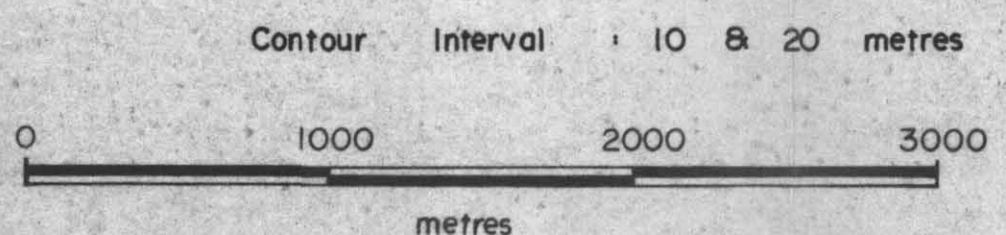
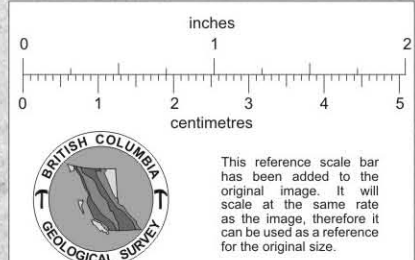
1:2500





LEGEND

- TERTIARY
- ~~~~ SHEAR ZONE / FAULT
  - ~~~~~ SOOKE INTRUSIONS
  - Tg QUARTZ DIORITE
- TRIASSIC
- VANCOUVER GROUP
  - MURK KARMUTSEN FORMATION ANDESITIC LAVAS



|  |              |
|--|--------------|
| INTERNATIONAL COAST MINERALS CORPORATION |              |
| BEAR PROJECT                             |              |
| SURFACE GEOLOGY                          |              |
| DRN BY: R. T. Henneberry                 | SCALE 1:2500 |
| DATE: July 1987                          | FIGURE 4     |

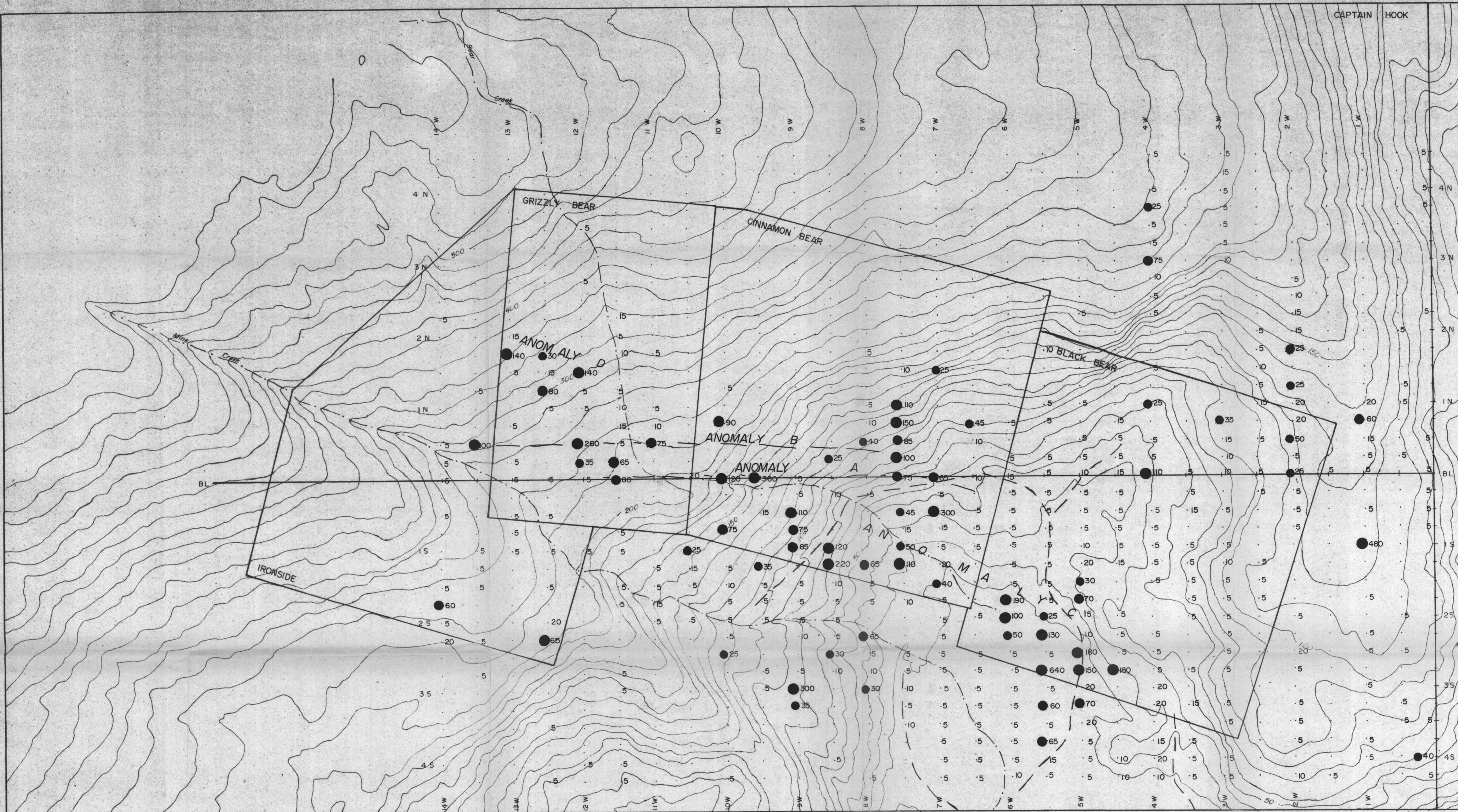






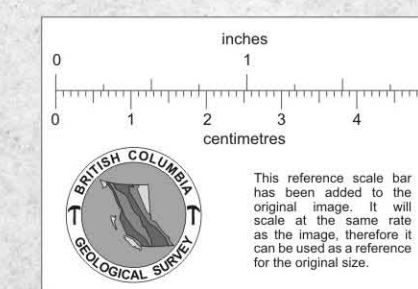






# LEGEND

- > 100 ppb
- 60 - 99 ppb
- 25 - 59 ppb



Contour Interval : 10 & 20 metres



INTERNATIONAL COAST MINERALS CORPORATION

## BEAR PROJECT

SOIL GEOCHEMISTRY Au (ppb)

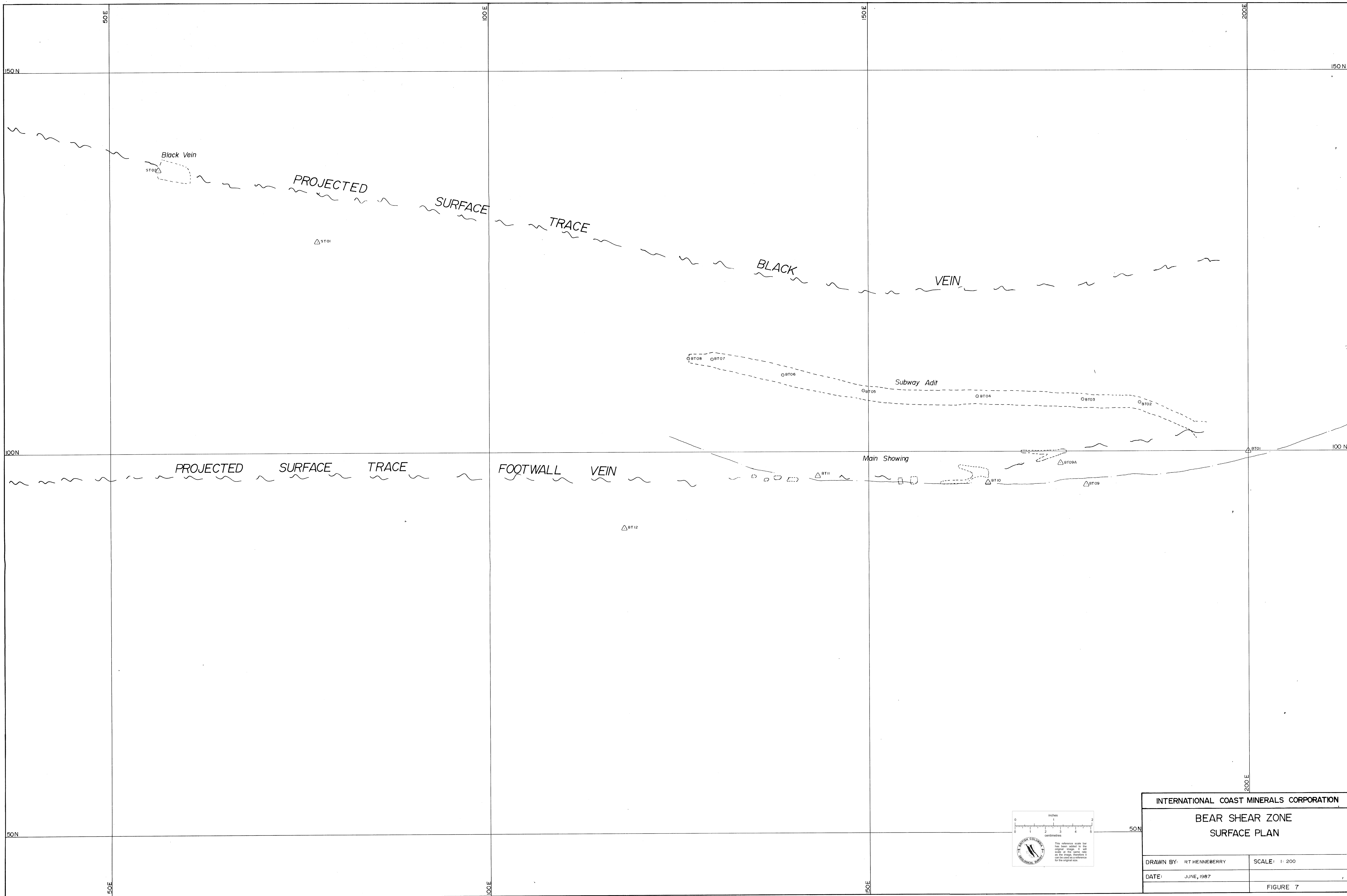
DRN BY: R. T. Henneberry

SCALE 1:2500

DATE: July 1987

FIGURE 8a









200E

125N

10 BT

200E

75 N

INTERNATIONAL COAST MINERALS CORPORATION

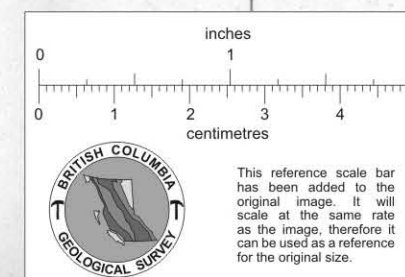
BEAR SHEAR ZONE  
SURFACE ASSAY PLAN

DRAWN BY: RT HENNEBERRY

SCALE: 1 200

DATE: JUNE, 1987

FIGURE 6



ounces per ton Au / width metres

|   |            |                 |
|---|------------|-----------------|
| G | designates | Groves sampling |
| I | "          | ICM             |
| L | "          | Lac             |
| N | "          | Noranda         |
| T | "          | Teck            |

3091-T 0677/2.13 2V-1 1228/2.10

3092-T 0220/0.61

6963-G 0802/2.13 8613-L 1626/1.0 57456-N 1158/1.3

6964-G 0750/1.2 8613-L 0100/0.5

6962-G 0130/0.31 1134-L 0904/0.35

57454-N 0148/0.26 1135-L 0378/0.40

57451-N 0077/0.36 1136-L 0078/0.15

57455-N 0010/1.9

57452-N 0003/0.31

1142-L 0300/0.30

1137-L 0022/0.65

86130-L 006/0.1

1138-L 0082/0.70

11-LB

1139-L 2980/0.40

1128-L 0800/0.51

1140-L 0152/0.30

1129-L 0044/0.15

1141-L 0036/0.30

1143-L 0048/0.45

21-LB

150E

150E

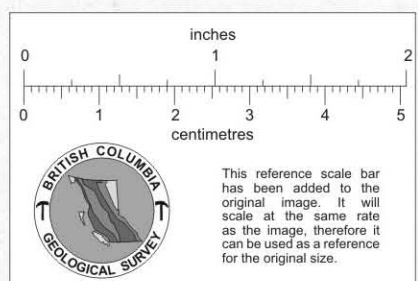
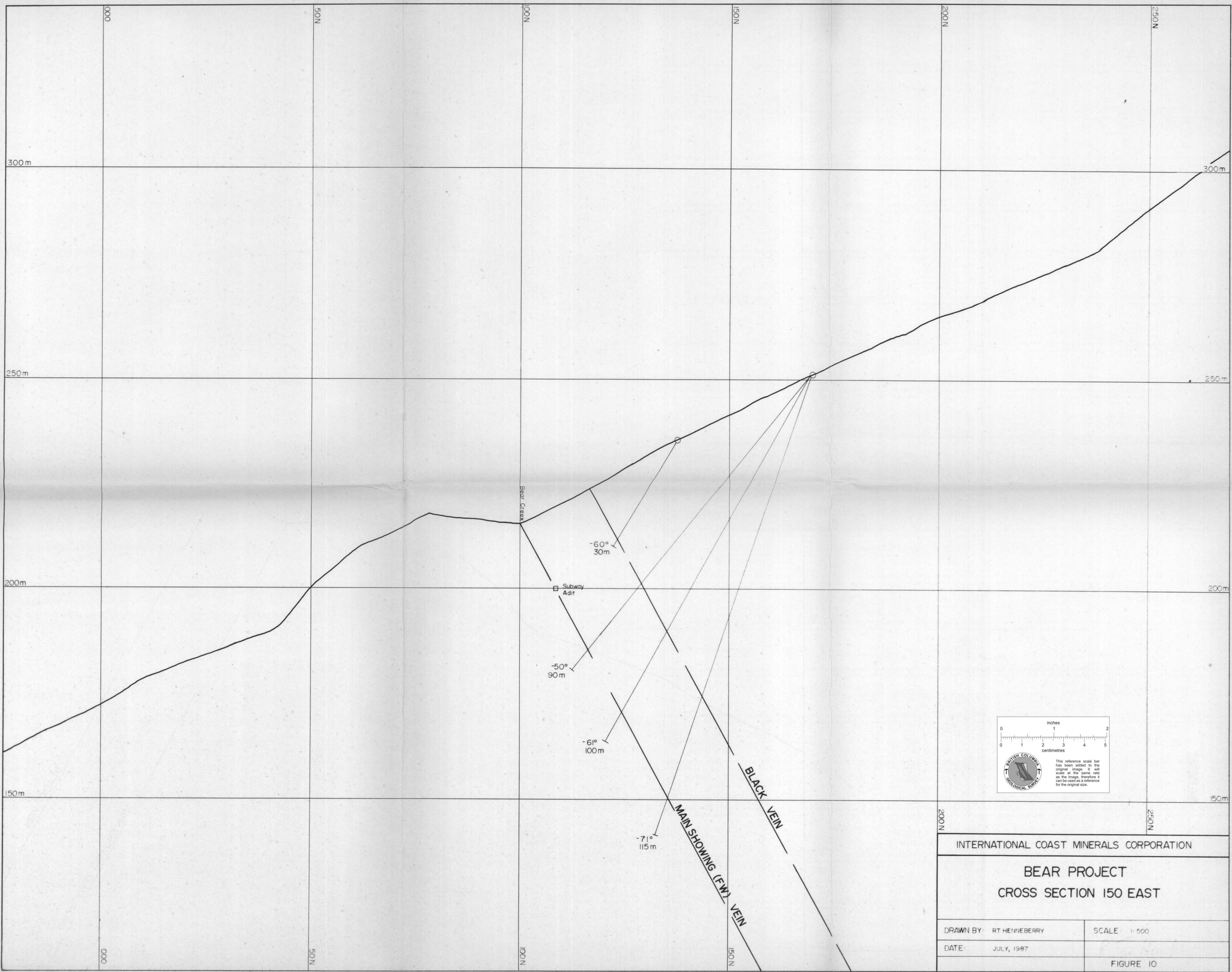
100E

100E

125N

75 N





INTERNATIONAL COAST MINERALS CORPORATION

BEAR PROJECT  
CROSS SECTION 150 EAST

DRAWN BY: RT HENNEBERRY

SCALE: 1" = 500'

DATE: JULY, 1987

FIGURE 10



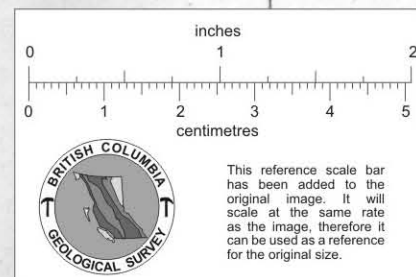
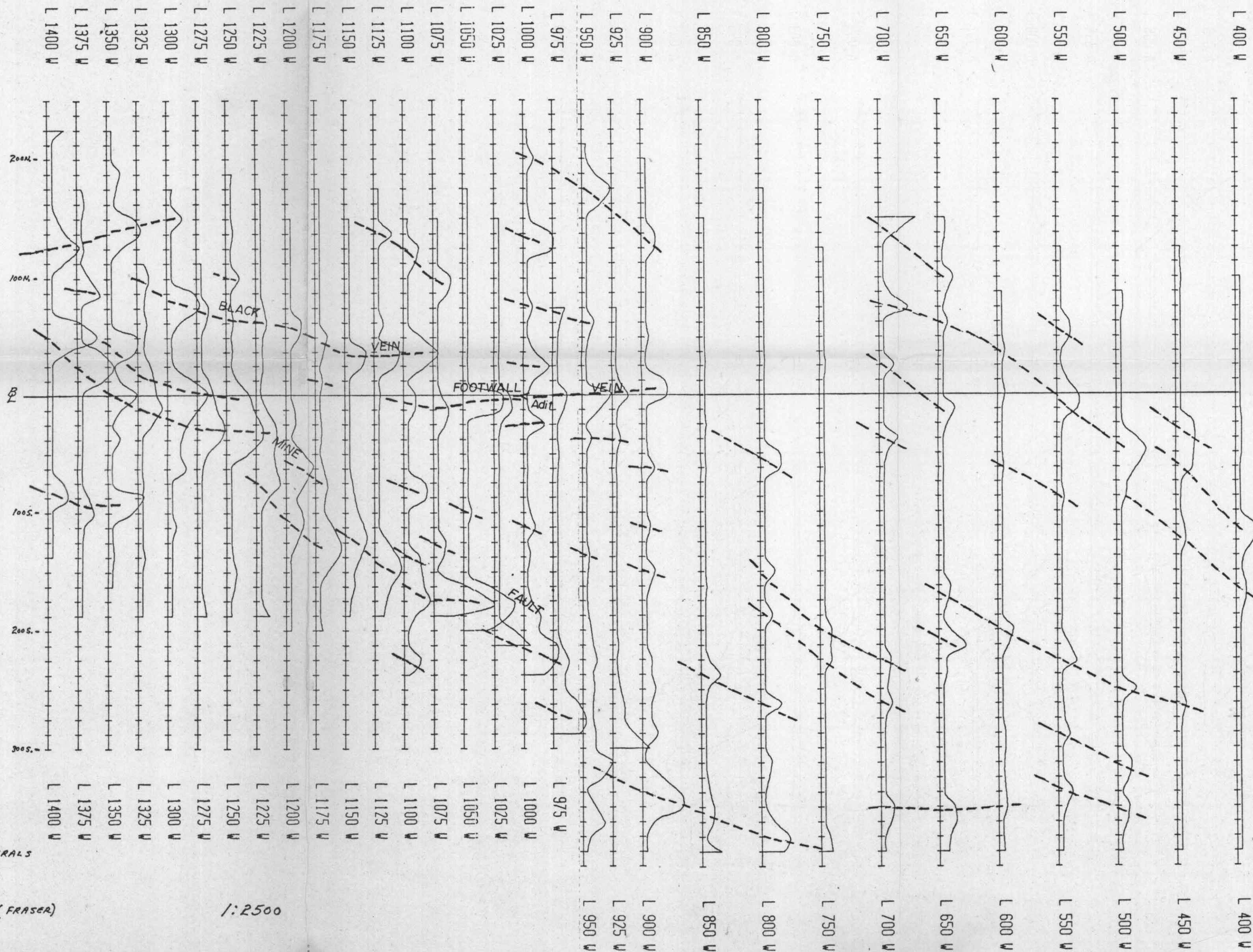


FIGURE 5





INTERNATIONAL COAST MINERALS

BEAR PROJECT

FILTERED VLF PROFILES (FRASER)

1cm = 25', base - 4%

SEATTLE VLF STATION 24.8KHz

1:2500

--- CONDUCTOR AXIS LOCATION