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Accuracy checks and evaluation of errors in the Silver Cup 003846  
planetable survey

The surveying involved in mapping this area was checked as it was being done and afterwards in the following ways:

1. All main course shots, i.e. those involved in traverse closures, as opposed to side shots from points in a closed traverse, were checked by reading rod intervals and vertical angles on backsights as well as on foresights. This gave a check on all the more important horizontal distances and changing elevation as the Survey proceeded. In other words all columns of the plane table notes were checked before the Survey was continued except the elevation column, and this could include only mistakes in addition of the changes of elevation. Such mistakes, if they occur, can easily be removed later without necessitating any repetition of surveying.
2. The plane table was oriented arbitrarily at the first set up and thereafter by backsighting a previous course. The compass needle was not used to orient the table. However compass north lines were plotted at several points. These may be used in either of two ways:
  - (a) Assuming that the compass north lines anywhere within the limited area (approx 1000' x 4600') should be parallel, any divergence of the compass north lines as plotted at these points would give a measure of the accumulated angular error that was introduced between them.
  - or (b) Assuming that the foresight - backsight procedure used effectively eliminated any source of angular error in orientation of the table (such as might be expected to arise from any local attraction if the table were instead oriented by means of the compass needle), and using the plotted compass north lines in conjunction with the known topographic survey coordinates of Alpha, Barbara and Caribbean, the difference between true north (astronomical) and compass north can be determined in this area.

## Accuracy checks and calculation of errors in the Silver Cup planitable Survey

3. The available topographic survey stations (Alpha, Barbara, Caribbean and Nettie L) were used to as much advantage as was possible. The survey was extended to include Alpha. This was meant to give a known elevation from which the elevation of all other points could be calculated and a tie in to the topographic survey coordinates, but the extension to Alpha includes one very long and steep shot which is not known to be reliable. However direction lines to Barbara, Caribbean and Nettie L were plotted at several points, and the vertical angles to these topographic survey stations were also recorded at some of these points. A complete plot of the survey including these lines and their intercepts, on any convenient scale, can be matched to a plot of Alpha, Barbara and Caribbean on topographic coordinates to the same scale, to give a composite from which the horizontal distance from any of these points to the appropriate topographic station can be measured. This horizontal distance, plus the corresponding vertical angle at any point, provides an independent means of determining the elevation of that point. Assuming this plot does not introduce further error in itself, the coincidence or lack of coincidence of these direction lines and the plotted positions of Barbara and Caribbean gives a measure of the accumulated angular error in the various parts of the survey. (The procedure suggested in 2(6), above, was carried out on such a composite plot.)

4. Closed traverses were incorporated in the Survey.

Even though the table is oriented correctly by back sighting there is a possibility that it may be shifted by some unobserved movement before the next main course is shot and an accidental error so introduced. Such an error would be discovered in a traverse closure. This survey was closed in the conventional way at three points (at G28, at Q3, and G96). This indicated that a satisfactory accuracy was being obtained so it was not considered necessary to break the survey down into any further sub-closures to localize errors. Two of the three closures indicated that the survey was directionally correct; the closure error at the points was of a strictly linear nature. The third, (actually the second in the

## Accuracy checks and evaluation<sup>3</sup> of errors in the Silver Cup planitable Survey

order of our surveying, i.e. the closure at O3), was found to have both an angular and a linear component. However the total closure error at this point was considered within allowable limits so no resurveying was called for.

This survey does not include any adjusted closures. It was not found necessary to adjust any courses to bring closures to the required accuracy, and such adjustment was objected to in principle, because it involves assumptions that are perhaps as often invalid as they are valid.

The lower portion of the Survey, from 700 portal to Tower Tunnel, was not closed in the conventional sense but the centre line of the tramline down this part of the hill was plotted wherever it crossed the switchback road and these points were found to lie on a straight line. As either an angular error or a linear error could have caused these centre-line points to plot differently this line can probably be considered a legitimate closure.

5. Some further independent checking was provided as an incidental part of a compass and tape pickup of geology by Hans Trebitz and Doug Irving.
6. A rough check of the elevations in this Survey ~~area~~ can be obtained from two barometer traverses from Silver Cup cabin to Alpha. These were done on August 8<sup>th</sup> and August 10<sup>th</sup>/56 using barometer #D-786. This barometer will duplicate readings to within 10 ft.

4

Difference between true (astronomical) north and compass north  
 at Silver Cup mine July 22-Aug 18, 1956.  
 (using the procedure discussed in 26 & 3 of "accuracy checks & evaluation  
 of errors")

Declinational from

$$\Delta 1 = 23^{\circ} 50' \quad \left. \right\} \text{plane table sheet } \#1$$

$$\Delta 1/2 = 22^{\circ} 15'$$

$$\Delta 31 = 21^{\circ} 20'$$

$$\Delta 31 = 22^{\circ}$$

$$\Delta 35 = 21^{\circ}$$

$$\Delta 47 = 21\frac{1}{2}^{\circ} \quad \left. \right\} \text{plane table sheet } \#3$$

$$\Delta 55 = 22^{\circ}$$

$$\Delta 56 = 22^{\circ} \quad \left. \right\} \text{plane table sheet } \#4$$

$$\Delta 12 = 21\frac{1}{2}^{\circ}$$

$$\Delta 65 = 21\frac{1}{2}^{\circ} \quad \left. \right\} \text{plane table sheet } \#5 - A \text{ part}$$

$$\Delta 14 = 21\frac{1}{2}^{\circ} \quad \left. \right\} \text{plane table sheet } \#5 - B \text{ part}$$

$$\Delta 60 = 21^{\circ} \quad \text{— plane table sheet } \#6$$

$$\text{total} = 12$$

average of all, less the most divergent determinations ( $21^{\circ}, 21^{\circ} + 23^{\circ} 50'$ )

$$= 195^{\circ} 35' \div 9 = \underline{21^{\circ} 44'}$$

average of all shots including the divergent ones

$$= 261^{\circ} 25' \div 12 = \underline{21^{\circ} 47'}$$

$$\begin{array}{r}
 21^{\circ} 44' \\
 9 \overline{) 195^{\circ} 35'} \\
 18 \\
 \hline
 15 \\
 9 \\
 \hline
 6 \\
 35 \\
 \hline
 9 \\
 36 \\
 \hline
 35 \\
 36
 \end{array}$$

$$\begin{array}{r}
 21^{\circ} 47' \\
 12 \overline{) 261^{\circ} 25'} \\
 24 \\
 \hline
 21 \\
 12 \\
 \hline
 9 \\
 56 \\
 \hline
 48 \\
 48 \\
 \hline
 85 \\
 84
 \end{array}$$

Accumulated angular error as indicated by lack of coincidence of direction line to topographic survey stations and the plotted positions of the topographic stations Alpha, Barbara and Caribbean.

These figures were obtained from a composite ( $1''/1000'$  scale) plot produced by transferring direction lines from the plane table sheets to the smaller scale drawing and fitting to this a separate plot of Alpha, Barbara & Caribbean.

direction line fails to coincide by approximate angle represented

$\Delta 3$ - Barbara	fits exactly	nil	
✓ - Caribbean	40ft (North) in 6900'	$1/3^\circ$ ( $20'$ )	
$\Delta 9$ - Caribbean	30ft (South) in 6900'	$1/4^\circ$ ( $15' +$ )	
$\Delta 10$ - Barbara	fits exactly (4900' to Barbara)	nil	
✓ - Caribbean	25ft (South) in 7160'	( $12' +$ )	
$\Delta 12$ - Caribbean	approximate - ran $20' N$ (Caribbean 7530' away)	( $10' -$ )	
$\Delta 58$ - ✓	15-20' in 7760	( $10' -$ )	
$\Delta 15$ - ✓	5' N (essentially exact) Caribbean 7670' away	( $2.4'$ )	
$\Delta 15$ - Barbara	exact (4930')	—?	
$\Delta 15$ - Nellie L	— no check	—?	
$\Delta 23$ - Caribbean	exact (6900')	nil	

accumulated  
angular  
error  
plane table  
sheet #1

These points are all on plane table sheet #1. They were plotted on reduced scale by putting  $\times$  ~~crosses~~ on the  $1''=1000'$  tracing coincident with  $\times$  on the  $1''=100'$  plane table sheet. Then lines from  $\times$  to all stations on plane table sheet #1 were a common <sup>direction</sup> to both the  $1''=100'$  & the  $1''=1000'$  plot. Distances in these directions were plotted at the smaller scale on the tracing.  $\odot 2$  was one point replaced in this way. This point on the 1000 scale sheet was then put coincident with  $\odot 2$  of plane table sheets #2 & #3. All other direction lines. This one point coincidence gave a hub from which rays could be drawn to pick up other points but in addition one course had to be coincident on the 1000 scale plot and the plane table sheet to which it was transferred. On the reduced scale this was a less reliable base line for further plotting. Also due to the reduction of scale the error introduced by plotting error was ten times greater, relatively, when it was equal in absolute measure. These two factors probably account for most of the increase in accumulated angular error suggested by the following figures.

direction line fails to coincide by approx. angle represented  
 $\Delta 32$ -Caribou (Sheet 2) 200' (south) in 6660 approx  $2^\circ$  ( $1050'$ )

If this represents an angular error on the plane table that it would be necessary to rotate  $\Delta 32$ -Caribou clockwise to correct it. If Sheet 2 is then reoriented on this base compass N at  $\Delta 31$  would be increased by this amount ( $21^\circ 20' + 1050' = 23^\circ 10'$  from true north). It seems probable that most of this angular error is in the ~~1000'~~ composite rather than in the  $1''=1000'$  plane table original.

$\Delta 38$ -Caribou (Sheet 3)	60' (south) in 6200' +	$610^\circ$ (36')
$\Delta 47$ -Barbara (✓)	100' (south) in 6050'	$1^\circ$
$\Delta 47$ -Barbara (✓)	70' (east) in 4875'	(51')
$\Delta 51$ -Caribou ("")	110' (south) in 6250'	$10^\circ$
$\Delta 53$ -Caribou ("")	175' (south) in 6150'	$13\frac{1}{4}^\circ$

Three more direction lines were plotted on Sheet 1 from X, a setup off from the ~~one~~ cairn on Alpha. These did not check nearly as well as the other shots on Sheet 1.

X - Barbara	70' west in 6000'	(42')
✓ - Caribou	75' N in 8600'	(45'+)
- - Nettle L	no check	-?

If the composite  $1''=1000'$  plot used to arrive at these figures can be considered completely accurate it may be assumed that any warping of a line, or any dislocation of a contact or similar feature, that represents an angular displacement in excess of  $2^\circ$  ( $1050'$ ) must be attributed to some other cause than accumulated survey error. As the composite is more likely to have errors in it than the original work it is probable that the accumulated angular error anywhere in the survey does not even approach this high a value; (for confirmation see other checks on the accuracy of the survey).

Closure at A18-G28

I

length of traverse involved:

$\Delta 10-11$	100' =	177 $\frac{1}{2}$ '	cumulative
11-12	=	277 $\frac{1}{2}$ '	455
12-13	=	334	789
13-14	=	268	1057
14-15	=	414	1471
15-16	=	365	1836
16-17	=	250	2086
17-18	=	130	2216
G28- $\Delta 10$	=	200'	2416

TPST to mons 303 301

(error is all linear)

Closure at O3

length of traverse involved

$\Delta 3-02$	=	385
2-10	=	234
10-11	=	177 $\frac{1}{2}$
11-12	=	277 $\frac{1}{2}$
12-13	=	334
13-14	=	267
14-15	=	414
15-16	=	365
16-17	=	221
17-20	=	60
20-21	=	221
21-26	=	149
26-27	=	107
27-28	=	174
28-29	=	92.
29-30	=	171
30-03	=	122 $\frac{1}{2}$
03-02	=	150
$\Delta 3-4$	=	182
4-5	=	162 $\frac{1}{2}$
5-6	=	248
6-7	=	275
7-8	=	212
8-9	=	273

closure error = 9' in 2416' HD

$$= \frac{9}{2416} \times 100\% = \text{approx } 0.4\%$$

2416 | 966.4  
966.4

elevation closure error = 4.11'

on that  $\Delta 17-18 \rightarrow 628$

+ 3.8' on that  $\Delta 10-G28 \rightarrow 218$

horizontal distance total = 4983'

closure error = 12 ft HD + 2.6' vertical

$$\text{relative error} = \frac{12}{4983} \times 100\% = 0.24\%$$

4983 | 1200.0  
996.6  
2034.0  
1993.2  
408.0

001-0

S △ W

777-0

(error has both linear and angular components here)

probable

099-0 : SA

Closure at G96

(error is all linear)

(7-10) HD 5.6 vertical

82KNW027

### ELEVATIONS BY BAROMETER D-786

Wed Aug 8/56 Silvers Cup cabin 935 AM = 5360' - 153 = 5207'

700 portal 1006 AM = 6370' - 153 = 6117'

$\Delta 3$  at 400 portal 1018 AM = 6700' - 153 = 6547'

$\Delta 2$  at 300 portal 1027 AM = 6775' - 153 = 6622'

GAT at the upper staff 1033 AM = 6953' - 153 = 6800'

Alpha 1114 AM = 7800' (7799) - 153' correction = 7647' the elev.

given cup cabin 850 AM = 5360' given by topographic survey.

7 Fri Aug 10/56 — Silvers cup cabin 853 AM = 5320' - 123 = 5197'

300 portal 928 AM = 6740' - 123 = 6617'

Alpha 1006 AM = 7770' - 123' correction = 7647'

elevation of silver cup cabin by average = 5202' (datum for further barometer traverses out of Silver Cup camp)

Difference in Elevation from 6/55 and A59 : 201  
 " " " from A15-A14 between 100 and 55.3'  
 Average 78'

Difference in Elevation from barometer readings.

Assumed el.  
 $\Delta_2$  = No ~~13~~<sup>3</sup> - Adit

6742'

True Elevation & 7697

Difference      7697  
6742  
905

Assumed El.

$\Delta_3$  = No ~~13~~<sup>4</sup> Adit

6648'

7697  
6648  
999

Reading at A ~~13~~<sup>2</sup>

6700

at Ready

7800

Difference Corr. to

~~1100~~

~~101~~

at A 2

6775

7800

~~1100~~  
 1025

~~101~~  
 120'

Reading

$\Delta_2$  : 6790

~~7760~~  
 7710

~~7770~~

1030

1251