Tom Schwetz
Site visit:
Sat. June 18/05

885292

FortyTwo Metals Inc.

(A wholly owned subsidiary of ROCA Mines Inc.)

MAX Molybdenum Project

Development Proposal
For Campaign Production
Under a British Columbia
Small Mines Permit

June, 2005

Executive Summary

Rapid permitting and development of the MAX Molybdenum Project, located in south-eastern British Columbia would result in the production of molybdenite concentrates, suitable for sale to a number of possible consumers, traders or roasting facilitates.

Development of an underground mine to access the deposit is dramatically accelerated by comparison to other mines because existing underground access to the deposit can readily be used and further developed. In addition, existing rail in the access adit will facilitate .

The project site is road accessible year round. The site has favorable topography and foundation conditions for a new 500 tonne per day (tpd) concentrator, tailings storage and other facilities.

In early May 2005, ROCA began an underground diamond drilling program for infill sampling and definition drilling of the proposed mining area. In preparation for that work ROCA also completed rehabilitation of the access adit including the installation of a new ventilation system and underground electrical system. Permitting and procurement of equipment for the project is also underway.

A mine development and production schedule has been prepared for the proposed plan and is presented in this report. The schedule has been optimized to deliver the highest grade, as quickly as possible and at a low development cost. In addition, the production schedule has been capped at a total of 72,000 tonnes per year, to comply with the requirements of a British Columbia Small Mines Permit, an expedited permitting process that fits well with the size and grade of the MAX deposit, development and construction time for a small mine and the uncertainty of the commodity price.

The production schedule estimates a total campaigned production of approximately 1,700,000 kg (3,758,000 lbs) of molybdenum contained in a molybdenite concentrate over an approximately 2.5 year period, as summarized below:

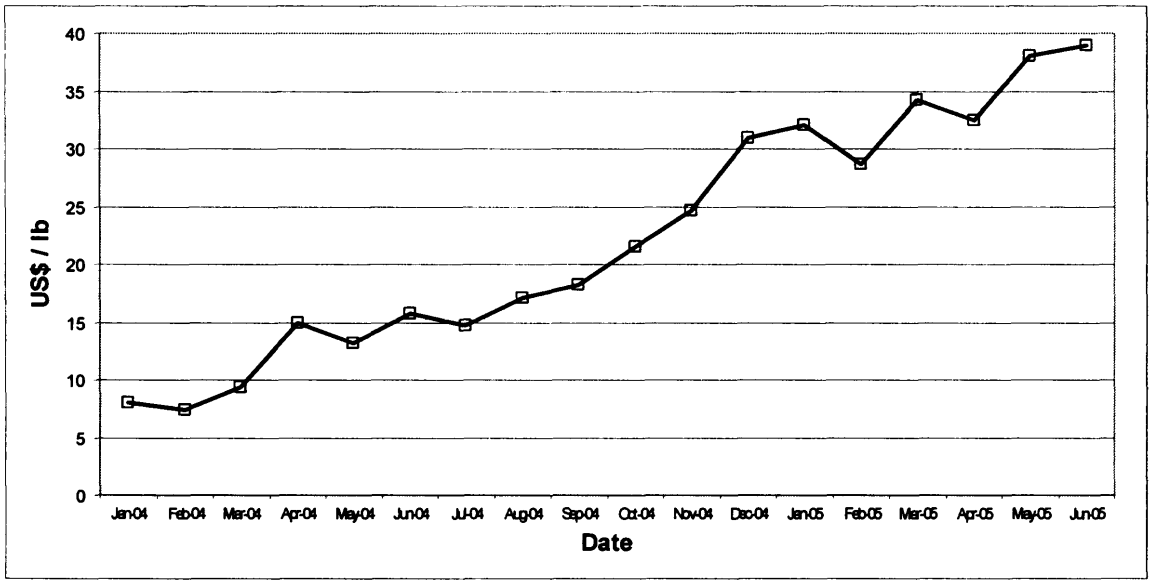
Operating year	Mo in Concentrate	
	kg	lbs
Year 1	704,696	1,553,572
Year 2	673,632	1,485,089
Year 3	326,587	719,994
Total	**1,704,915**	**3,758,655**

Initial production can begin as early as the 4th month after development begins and will be cash flowing approximately a month after that. Expansion of the mine beyond the proposed program may be warranted if commodity prices are sustained. Preliminary engineering for a continuous and expanded operation has also been studied.

Estimated total life-of-mine mining, milling, and general & administrative costs are approximately US$100/tonne. Estimated capital costs are US$4 million for mining, US$4

million for concentrator, US$800,000 for tailing management systems, and US$1.2 million for startup and contingency costs. A total capital cost of US$10 million is estimated for the startup of the project. Molybdenite concentrate will begin initial delivery in 5 to 6 months from securing production financing and subject to permitting applications.

Prices for molybdenum products have improved to current levels (+US$ 30/lb for molybdenum oxide) over the past 12 months. Historic prices are much lower; however, indications for robust prices for a long period of time are evident. The following chart shows the price change for molybdenum oxide over the past year. Similar increases in prices for other molybdenum products has also occurred.



Introduction

Fortytwo Metals Inc. (FortyTwo) is a wholly owned subsidiary of Roca Mines Inc. (ROCA), a TSX Venture Exchange listed company. Both companies are based in Vancouver, British Columbia, Canada. FortyTwo holds an option to earn 100% of the MAX Molybdenum Project, located approximately 65km south of Revelstoke, in south-eastern BC.

Previous exploration work by Newmont Exploration of Canada Ltd. and Esso Minerals Ltd. at the MAX is summarized in a "Technical Report on the MAX Molybdenum Property" by Mr. Terry Macauley, P.Eng. dated September 20, 2004. The report reviews the historic exploration work on the property and the following major tasks;

- 17,873 m of surface diamond drilling (including drilling by Roca in 2004);
- 1,276 m of primary (3.7 m x 4.6 m) underground adit access, portal, refuge and remuck stations;
- Approximately 724 m of secondary underground development in four crosscuts (3.1 m x3.7 m) and 10 drill stations;
- 22,151 m of underground diamond drilling; and,
- bulk sampling through the 960m Level of the deposit

Mr. Macauley's 2004 Technical Report also provides a National Instrument ("NI") 43-101 compliant resource estimate outlining a global 'measured' and 'indicated' resource of approximately 42.94 million tonnes of 0.20% MoS2 at a 0.10% MoS2 cutoff. In addition, a further 8.9 million tonnes averaging 0.16% MoS2 is categorized as 'inferred' at the 0.10% MoS2 cutoff grade.

Mr. Macauley also developed resource estimates for higher cutoff grades yielding smaller yet, well defined and continuous tonnages within the known deposit. The resulting higher-grade resource estimates are summarized in the following table.

MAX Resource Estimate at >0.10% MoS2 Cutoff Grades

Measured			**Indicated**		**Measured & Indicated**	
Cutoff % MoS_2	Tonnes	Grade % MoS_2	Tonnes	Grade % MoS_2	Tonnes	Grade % MoS_2
0.20	9,340,000	0.35	2,010,000	0.41	11,350,000	0.36
0.50	1,010,000	1.01	370,000	0.77	1,380,000	0.94
1.00	260,000	1.95	20,000	1.87	280,000	1.95

In late 2004, Roca engaged Hatch Associates Ltd. ("Hatch") to prepare an independent 'preliminary assessment' (scoping-level engineering) for the project to assess project economics. Because of continued uncertainty for the future price of molybdenum products Roca directed Hatch to study mining scenarios at a 0.50% MoS2 cutoff and at a 0.20% MoS2. The resulting difference in total resource estimates required the assessment of both small and large throughput rates.

Two throughput rates have been evaluated that both consider the development of 'continuously' (meaning no campaign mining and development) operated mine and concentrator; Case A, a 500 tonne per day operation that would develop part of an

estimated 1.38 million tonnes at a undiluted grade of 1.01% MoS_2 and Case B, a 2,500 tpd operation that would mine an estimated 11.35 million tonnes at an undilited grade of 0.36% MoS_2.

The results of the studies by Hatch generally indicate that the project is very sensitive to commodity prices and that the economics of both cases requires sustained prices above historic levels to develop and advance a full-scale mine.

A review of Case A at 500 tpd indicates that the development of a small-scale 'campaigned' development and mining operation can deliver a robust project by minimizing initial development and capital and, importantly, lead-time to production. By focusing on only providing the required underground development to ensure an initial campaign of approximately 184,000 tonnes, the operation can produce and deliver highgrade concentrates quickly. Subsequent development campaigns would provide access to stoping areas that would be the source for the next year's small-scale production. It is important to note that the proposed small-scale mining operation does not impair or significantly reduce the opportunity to expand the mine and provide production from other parts of the deposit in the future, should commodity prices allow.

Description of Existing Surface and Underground Development

From 1979 to 1981, approximately 2,000 metres (m) of adit, crosscuts and drift development was made on the 960 m Level, approximately 500 m below the surface outcrop. Underground diamond drilling of 22,151 m in 87 holes detailed the mineralization and explored the adjacent areas. Bulk samples from 189 drift and crosscut blast rounds over a total length of 687 m were processed through a crushing plant and sampling tower on site.

An adit at the 960 m Level elevation was driven in a southwest direction for 1,276 m to the edge of the area of interest. Its size is 3.7 x 4.6 m (12 x 15 feet) to allow for future use as a production haulage way and as such is larger than typical exploration adits. Beyond that point the adit profile was reduced to 3.0 x 3.7 m (10 x 12 feet), and it continued as a crosscut through the known deposit. Four drifts were driven to provide diamond drill stations; two of them through the deposit were also bulk sampled. Total length of adit and drifts is approximately 2000 m (6,560 feet).

Reported mining conditions during development contrasted strongly between the approach to the deposit and the drifting within it. Prior to reaching the Z Fault on the east side of the deposit, progress was impeded by numerous water bearing fracture zones. Ground support was required at a total of 13 locations, but outside those zones rock was competent and stood up well. West of the Z Fault in the mineralization and adjacent areas, water inflow was minimal and backs needed no support.

ROCA has recently re-opened and re-habilitated the 960 m L adit for an infill diamond drilling program which commenced in May 2005. Ventilation of the workings is currently carried out by a 150 hp portal fan and a pressurized 42" flexible vent ducting suspended from a messenger cable in the centre of the back of the adit. Power transmission to the working area is from the portal at 4130 volts to a transformer in the drill area where it is stepped down to 600 volts.

Currently no concentrator or tailings storage infrastructure exists at the site, a description of those planned facilities is provided in this document.

Details of Planned Surface and Underground Development

The following development plan for a small mine is estimated to be capable of campaigned production at a rate of approximately 72,000 tonnes per year of molybdenite ore. A concentrator to be developed at the site would be operated at a similar rate on an annualized basis. The estimated throughput is based on the small mine schedule discussed and balanced with an estimated concentrator throughput rate of 500 tpd operating for 180 days at an estimated 80% availability.

The small mine plan is tightly focused on the delivery of ore from stopes that require minimal lead time to develop and can be accessed by the existing 960m level adit. Initial operations require all access and ventilation delivered through the large-sized adit, a planned ventilation raise will be developed when production from lower levels requires the use of additional mining equipment, perhaps after Year 3 of operations.

Mining in the working areas will be achieved by diesel powered trackless equipment including load-haul-dump (LHD) and truck equipment operating in development headings and by remote LHD mucking operation in open stopes. The trackless equipment will deliver muck from the working stopes to a transfer station located at the 965m L where it will be transferred to 36" rail cars on the existing 0.9 m (36 inch) rail. A battery powered locomotive will be used to tram loaded cars to surface and return empty cars to the transfer station.

The working area is approximately 1,400 m from the portal and ventilation will be provided by a hanging rigid vent ducting from the back of the adit. The system would be capable of being reversed such that it can provide direct ventilation or exhaust from the workings.

Refuge stations located approximately every 300m will be established along the adit. During all production times from the working areas, materials and equipment that could present a fire hazard will not be allowed in the main adit access during normal production periods. Diesel powered equipment will operate capitvely in the working area, except for their initial placement in the mine and ultimate removal, and will be serviced and fueled in the truck shop.

The attached production schedule has been developed based on industry standard estimates for advance rates in various size openings for declines and level workings using trackless equipment. Similar estimates for conventional ladder equipped raises will provide flow through ventilation to working areas during production. These manways also provide secondary egress ways from the working area. Fan sizing requirements will change over time and in general will increase over time as production requires longer haulage and more diesel equipment is present in the mine.

Development of the proposed mine includes the excavation of a 4.5 x 4.5m decline from the main level (now referred to as the 965 m L due to the incline of the main adit). The

decline will provide access at a maximum grade of 15% and allow for the development of Levels at 950 m, 925 m, 900 m, 885 m, 860 m, 835 m. Open stopes will be developed with most of the level development being in ore grade material and stockpiled according to the development schedule. A sill pillar is planned between 885 m and 900 m since upper stopes (A-925, A-926, A-900, A-901) are not planned for backfilling at this time. Similarly, a pillar is planned between stopes occurring on the same level. Future backfilling, either with uncemented waste rock or cemented sand and gravel or pastefill could be achieved to facilitate pillar extraction should the price of molybdenum products allow.

A number of refuge stations, remuck stations, sumps and other development are planned and identified in the development schedule.

An expanded development plan that includes a truck dump and chutes is shown on Figures 3.4-2 to 4. The truck dump workings are not included in the schedule at present and it could be developed should mine planning expand on the workings described in this application. Its development would also be predicated on molybdenum prices since it also facilitates possible production of lower grade material from above that area.

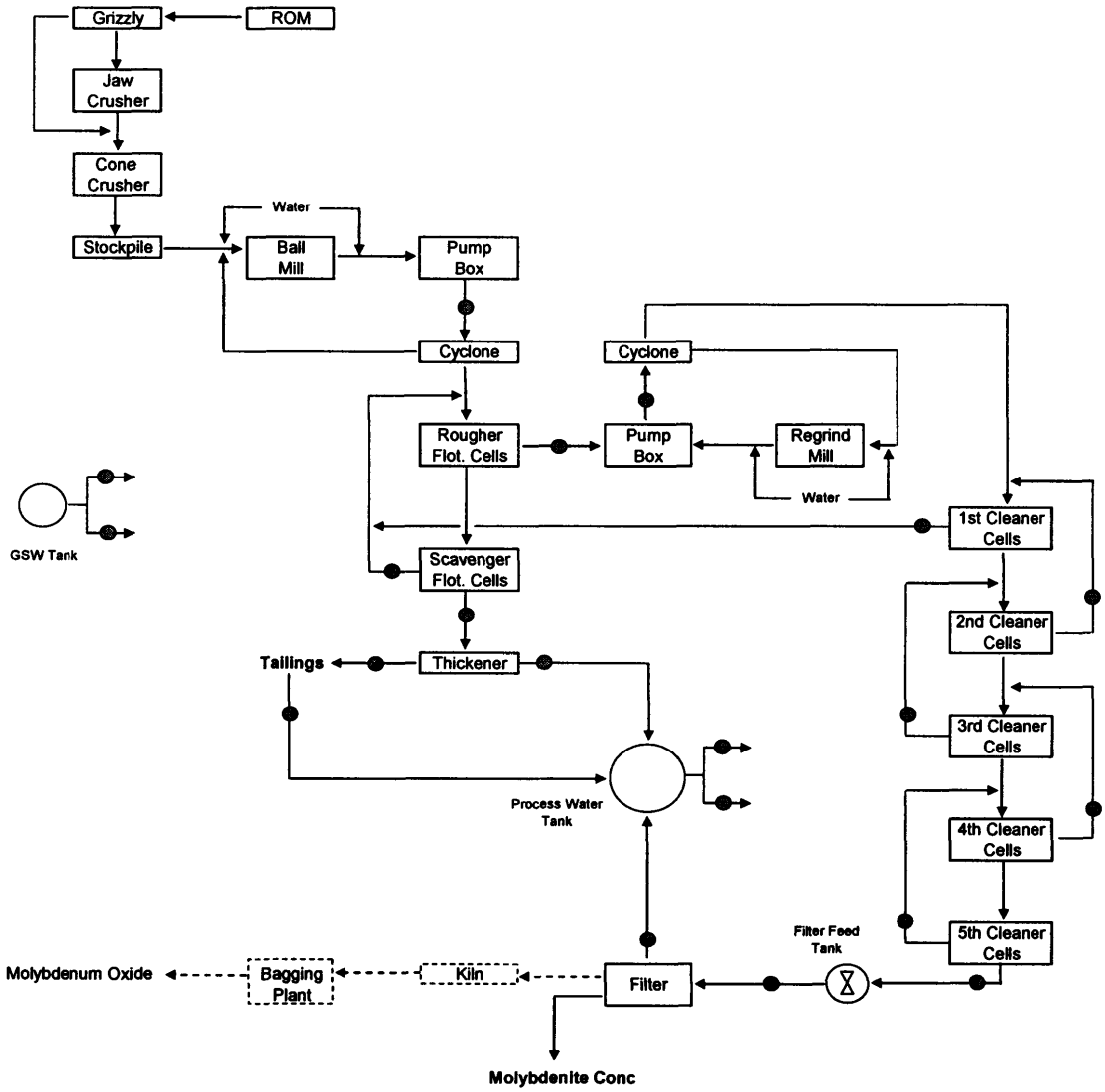
Mineral Process Plant

Development of process for a 500 tpd concentrator is based on information available from historical reports and literature pertaining to similar molybdenite concentrators such as Endako and Henderson mines.

Plant design criteria have been reported in two design memoranda, one dated December 9, 1982 from A. Gorken and one dated December 17, 1982 from S.W. Nabbs to various recipients as well as a report titled "Final Report Trout Lake Molybdenum Project" issued by Newmont Exploration of Canada Limited, dated January 31, 1983. These documents detail proposed design criteria for a 1,000 tons per day processing plant consisting of primary grinding and flotation sections, flotation concentrate regrinding and tailings thickener sections.

This data has been used to detail the design criteria for this study and a solids and solution balance was prepared for the proposed 500 tpd. For the purposes of this study it is assumed that crushing operations will produce a minus 12.7mm sizing, being supplied to a storage facility ahead of the primary mill. The process plant consists of a conventional grinding and flotation circuit. A ball mill, grinding minus 12.7mm crushed product to approximately 80 percent passing 106µm, operating in closed circuit with a hydrocyclone unit and the cyclone overflow product gravitates to the rougher and scavenger flotation cells operating in series. The rougher flotation concentrate undergoes further grinding in a secondary regrind ball mill followed by a series of five cleaning and re-cleaning flotation stages to produce a final molybdenite concentrate. The regrind mill will produce a product size of 80percent passing 45µm (325 mesh size) The flotation tailings will be pumped to a thickener prior to disposal to a tailings pond, the overflow water being recycled for use within the process plant. Water will also be recycled from the tailings dam to a process water tank. The final flotation concentrate will be filtered for direct transport.

Proposed Metallurgical Flowsheet



Primary Mill – 500 tpd

The minus 12.7mm crushed product is transferred by conveyor to a mill feed storage bin. A single storage bin of 400 tonnes (200m3) capacity will provide for approximately 20 hours surge capacity. The material will be discharged from the bin by an electro-magnetic vibrating feeder on to the mill feed conveyor (600 mm wide) and into the primary ball mill.

The estimated ball mill size to grind 500 tonnes per day of minus 12.7mm crushed ore to 80 percent passing 106 micron, is calculated to be 2.44m diameter by 3.5m (8' diam x 11'6") with a power draw of approximately 200 kW (270hp) (Work Index = 9.26 kWh/ton). Process water is added to the mill inlet for dilution to maintain a mill density of approximately 70% solids and to the mill discharge pumpbox. A weightometer will be installed on the conveyor to monitor and control the feed rate to the mill. The milled

product is pumped to a hydrocyclone at a density of approximately 45 - 50% solids. The cyclone underflow will gravitate to the mill inlet hopper and the cyclone overflow to the rougher flotation circuit. A circulating load of 200% has been assumed for the mill circuit in the solids and solution balance calculations.

Primary Flotation Circuit

Feed to the rougher flotation cells is the classified cyclone overflow product from the primary ball mill circuit at a slurry density of approximately 30% solids. Scavenger concentrate is directed to the inlet of the first rougher flotation cell. The proposed throughput of 500 tonnes per day at a slurry density of 32% solids equates to a volumetric flowrate of $56m^3$/hr. The rougher and scavenger flotation section will consist of 4 OK-5TC tank cells ($5m^3$ each). Total air requirement for these tank cells is approximately $20m^3$/min (700cfm) at 19 kPa. Flotation reagents, a combination of pine oil and a selected frother, will be delivered from their respective bulk storage tanks by a series of metering reagent pumps to the individual addition points.

Regrind Mill and Cleaner Flotation

The regrind mill has been sized to treat up to 25 tonnes per day of rougher flotation concentrate (5% weight recovery). Based on a work index of 3.0kWhr/tonne the required mill size is calculated to be 0.9m diameter x 1.83m long with a power requirement of approximately 8kW (11HP). Rougher concentrate will gravitate to the regrind mill pumpbox and the mill will operate in closed circuit with a hydrocyclone. The cyclone overflow product will gravitate to the first cleaner cell and cyclone underflow returned to the mill inlet. A series of five stages of flotation are included to upgrade the rougher concentrate. The 1st Cleaner Tails product will be pumped to the first rougher cell. Subsequent cleaner tails will be recycled to the head of the previous cleaner stage. For costing purposes, a series of four OK1.5-TC cells have been proposed for the four cleaning stages with a final stage consisting of a flotation column of approximately 2m3 capacity.

The final concentrate tonnage is estimated at a maximum of 10 tonnes per day, based on a final grade of 90% MoS_2 and 95% recovery from a feed stock of grade 2% MoS_2.

Tailings Disposal

The flotation tailings will be pumped to a thickener, the clean water overflow being recycled via the process water storage tank and the thickened tailings to the tailings pond. A flocculent addition system will be installed to assist solids settlement.
Settling test results give the basis to calculate the tailings thickener requirements and based on a feed slurry density of 30% solids and a flocculent addition of 0.02 lbs/ton the results indicate 0.85 sq feet/ton/24hours ($0.087m^2$/tonne/24hours). At the proposed treatment tonnage of 500 tonnes per day, and including a 50% safety factor, the calculated area requirement is 65 m^2 (thickener diameter = 9.1 metres).

Water Balance

It is assumed that approximately 85% of the water discharged with the tailings will be recycled to the plant. The solids and solution balance prepared indicates the plant make-up water requirement is approximately $2m^3$/hour, being attributed to the volume

retained at the tailings dam and evaporation losses. Details of all gland service water requirements have not been determined.

Water Storage
Two water storage tanks are proposed. One of 10 m diameter will provide approximately 5 hours storage capacity for the primary mill operation being the combined tailings thickener overflow and tailings dam water recycle process streams. A second tank of approximately 4.2 metres diameter is required for gland service water supply and general clean water service. Plant make-up water will be added to both the mill water tank and the gland service water tank as required.

Filtration
The same filtration equipment as proposed for the 3,000 tpd scenario has been included for this section of the treatment plant. As the project proceeds, this equipment specifications and sizing will require further investigation to ensure its compatibility with both tonnage process options.

Development and Production Schedule

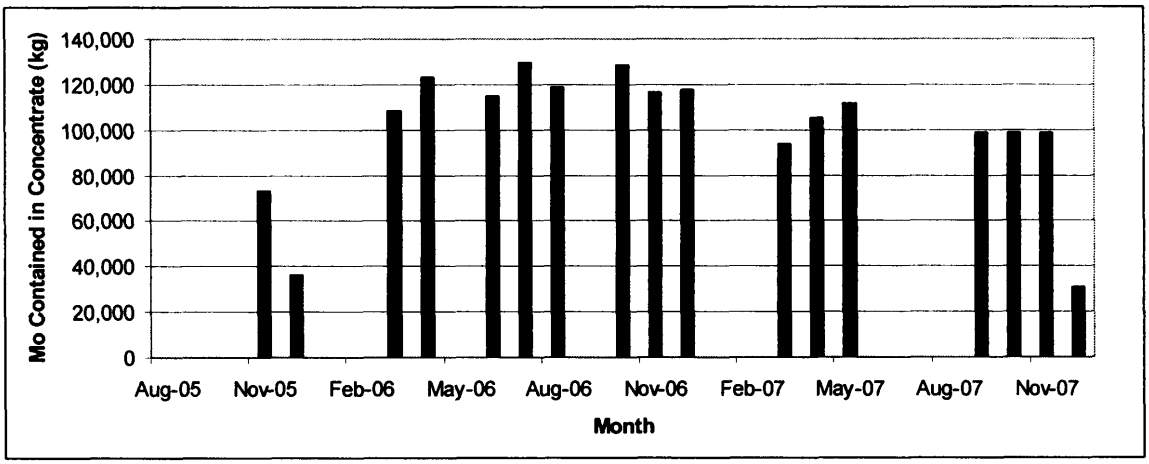
A schedule of development and planned production is based on the required underground development to access the proposed stopes shown in the figures. Standard industry advance rates have been used to evaluate the time to excavate the planned workings. Mine stopes have been scheduled to produce up to 500 tpd when in full production. It is assumed that concentrator components will be constructed during the mine development and a trial operating period will produce initial concentrates as shown on the attached schedule.

The production schedule estimates a total campaigned production of approximately 1,700,000 kg (3,758,000 lbs) of molybdenum contained in a molybdenite concentrate over an approximately 2.5 year period, as summarized below:

Operating year	Mo in Concentrate	
	kg	lbs
Year 1	704,696	1,553,572
Year 2	673,632	1,485,089
Year 3	326,587	719,994
Total	**1,704,915**	**3,758,655**

Initial production can begin as early as the 4th month after development begins and will be cash flowing approximately a month after that. Expansion of the mine beyond the proposed program may be warranted if commodity prices are sustained. Preliminary engineering for a continuous and expanded operation has also been studied.

Chart: Estimated Monthly Production of Mo contained in Concentrate (kg)



Access and Transportation

The MAX Project access road is located at the westerly extension of the Trout Lake City road, and is substantially paved from Trout Lake itself. Access to the mine portal and plant site from this road is made along the existing forestry and exploration road. That road was upgraded by the proponent in 2004.

Highway trucks and trailer will be required to haul concentrate from the mine to market, probably via the Galena Bay ferry and Revelstoke. At peak production periods an estimated 200 tonnes of concentrates per month will require shipment, requiring a total of approximately 2 to 3 truck loads per week from the site.

Travel time from the mine to Revelstoke (the TransCanada Highway and rail) is approximately 1.5 hours. An alternative centre for labour and supplies is Nakusp, approximately 1.0 hours

Attachments:

1. Production Schedule (3 pages) Excel Spreadsheet
2. Underground Mine Figures (5 pages)
3. Various recent photos

MAX Molybdenum Project

BC Small Mine Permit Schedule

Production Estimate Summary

	PrePro	Year 1 (Monthly Production Estimates)											
Name	Aug	Sep	Oct	Nov	Dec	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug
Mine Development Schedule													
Development Metres	69 m	105 m	231 m	132 m	177 m	159 m	156 m	122 m	91 m	105 m	99 m	103 m	84 m
Waste Tonnes	2,952 t	4,775 t	13,978 t	7,975 t	10,713 t	9,662 t	9,757 t	7,541 t	5,737 t	6,357 t	5,974 t	6,259 t	5,244 t
Raise Metres	-	22 m	9 m	4 m	-	-	43 m	19 m	38 m	17 m	-	-	40 m
Development Ore Tonnes	-	147 t	5,519 t	1,615 t	3,081 t	3,115 t	3,085 t	2,674 t	844 t	2,019 t	2,550 t	2,671 t	2,115 t
Diluted Stope Tonnes	-	-	-	4,295 t	1,424 t	-	-	1,352 t	10,066 t	-	16,885 t	12,136 t	4,001 t
All Ore Tonnes	-	147 t	5,519 t	5,910 t	4,505 t	3,115 t	3,085 t	4,027 t	10,910 t	2,019 t	19,435 t	14,808 t	6,116 t
Diluted MoS_2	-	1.72%	1.13%	1.15%	1.47%	1.77%	1.95%	2.01%	2.04%	1.74%	1.74%	1.96%	1.93%
ORE Stockpiled/developed	-	147 t	5,666 t	-0 t	0 t	3,115 t	6,200 t	-0 t	0 t	2,019 t	9,454 t	12,261 t	7,378 t
Average Grade Stockpile (%)			1.14%				1.86%			1.74%	1.74%	1.79%	1.79%
Concetrator Schedule													
Cummulative ORE Tonnes	-	147 t	5,666 t	11,576 t	4,505 t	3,115 t	6,200 t	10,227 t	10,910 t	2,019 t	21,454 t	24,261 t	18,378 t
Operating Periods				Mill Trials				Start Mill			Start Mill		End Year 1
Mill Production (12,000 max)	-	-	-	11,576 t	4,505 t	-	-	10,227 t	10,910 t	-	12,000 t	12,000 t	11,000 t
Cummulative Mill Production (Tonnes)				11,576 t	16,081 t	16,081 t	16,081 t	26,308 t	37,218 t	37,218 t	49,218 t	61,218 t	72,218 t
												Project Total	**72,218**
Concentrate Production													
Average Grade (MoS_2 %)				1.14%	1.47%			1.92%	2.04%		1.74%	1.96%	1.96%
MoS2 Conc Production (kg)		-	-	121,938	60,938	-	-	180,492	205,223	-	191,637	216,109	198,352
Mo contained in Conc (kg)		-	-	73,151	36,557	-	-	108,277	123,113	-	114,963	129,644	118,991
Mo contained in Conc (lbs)		-	-	161,268	80,593	-	-	238,708	271,415	-	253,448	285,813	262,328

Year 1 Total Mo Production (kg)	704,696
(lbs)	1,553,572

MAX Molybdenum Project

BC Small Mine Permit Schedule

Production Estimate Summary

Name	Year 2 (Monthly Production Estimates)											
	Sep	Oct	Nov	Dec	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug
Mine Development Schedule												
Development Metres	50 m	54 m	2 m	-	-	-	-	-	-	-	-	-
Waste Tonnes	3,325 t	3,303 t	299 t	38 t	-	-	-	-	-	-	-	-
Raise Metres	36 m	1 m	35 m	4 m	10 m	6 m	10 m	6 m	-	-	-	-
Development Ore Tonnes	2,059 t	2,255 t	68 t	-	-	-	-	-	-	-	-	-
Diluted Stope Tonnes	639 t	13,250 t	11,154 t	11,000 t	12,449 t	11,500 t	13,986 t	7,334 t	7,134 t	10,000 t	1,550 t	-
All Ore Tonnes	2,697 t	15,505 t	11,222 t	11,000 t	12,449 t	11,500 t	13,986 t	7,334 t	7,134 t	10,000 t	1,550 t	-
Diluted MoS_2	1.57%	1.94%	1.76%	1.72%	1.23%	0.86%	1.42%	1.77%	1.95%	1.95%	1.95%	0.00%
ORE Stockpiled/developed	10,075 t	13,580 t	12,802 t	11,802 t	24,251 t	35,752 t	37,738 t	33,072 t	28,206 t	38,206 t	39,756 t	39,756 t
Average Grade Stockpile (%)	1.73%	1.78%	1.78%	1.78%	1.50%	1.29%	1.30%	1.30%	1.30%	1.47%	1.49%	1.49%
Concetrator Schedule												
Cummulative ORE Tonnes	10,075 t	25,580 t	24,802 t	23,802 t	24,251 t	35,752 t	49,738 t	45,072 t	40,206 t	38,206 t	39,756 t	39,756 t
Operating Periods		Start Mill					Start Mill					**End Year 2**
Mill Production (12,000 max)	-	12,000 t	12,000 t	12,000 t	-	-	12,000 t	12,000 t	12,000 t	-	-	-
Cummulative Mill Production (Tonr	-	12,000 t	24,000 t	36,000 t	36,000 t	36,000 t	48,000 t	60,000 t	72,000 t	72,000 t	72,000 t	72,000 t
											Project Total	**144,218**
Concentrate Production												
Average Grade (MoS_2 %)		1.94%	1.76%	1.78%			1.42%	1.59%	1.69%			
MoS2 Conc Production (kg)	-	214,176	194,304	196,512	-	-	156,544	175,211	186,160	-	-	-
Mo contained in Conc (kg)	-	128,484	116,563	117,888	-	-	93,911	105,109	111,677	-	-	-
Mo contained in Conc (lbs)	-	283,256	256,975	259,895	-	-	207,036	231,723	246,204	-	-	-

Year 2 Total Mo Production		
	(kg)	673,632
	(lbs)	1,485,089

MAX Molybdenum Project
BC Small Mine Permit Schedule
Production Estimate Summary

Name	Year 3 (Monthly Production Estimates) Sep	Oct	Nov	Dec
Mine Development Schedule				
Development Metres	-	-	-	-
Waste Tonnes	-	-	-	-
Raise Metres	-	-	-	-
Development Ore Tonnes	-	-	-	-
Diluted Stope Tonnes	-	-	-	-
All Ore Tonnes	-	-	-	-
Diluted MoS_2	0.00%	0.00%	0.00%	0.00%
ORE Stockpiled/developed	27,756 t	15,756 t	3,756 t	0 t
Average Grade Stockpile (%)	1.49%	1.49%	1.49%	1.49%
Concetrator Schedule				
Cummulative ORE Tonnes	39,756 t	27,756 t	15,756 t	3,756 t
Operating Periods	Start Mill			
Mill Production (12,000 max)	12,000 t	12,000 t	12,000 t	3,756 t
Cummulative Mill Production (Tonr	12,000 t	24,000 t	36,000 t	39,756 t
			Project Total	**183,974**
Concentrate Production				
Average Grade (MoS_2 %)	1.49%	1.49%	1.49%	1.49%
MoS2 Conc Production (kg)	164,323	164,323	164,323	51,433
Mo contained in Conc (kg)	98,577	98,577	98,577	30,855
Mo contained in Conc (lbs)	217,324	217,324	217,324	68,022

Year 3 Total Mo Production (	326,587
(lbs)	719,994