861515

PLACER DEVELOPMENT LIMITED

MEMORANDUM:

TO: D.C. Rotherham/D.A. Howard   DATE: March 19th, 1979

FROM: C.C. Rennie   FILE: Venture 164

RE: Adanac - Ruby Creek - Drilling

A relevant set of maps and sections of the Adanac Ruby Creek deposit have been assembled and reviewed. Copies of Climax and Johns Manville drill logs, and plant and damsite drill logs have been obtained for our files. A set of 1"=100' computer ore block sections have been printed and stage 1 and stage 2 pits outlined on them as calculated for the preliminary evaluations. Block grades have been coloured on the sections to illustrate the grade distribution.

A review of the computer ore reserve calculation has indicated:

(1) According to Michel David the geostatistics indicate that vertical variations are 12 times more rapid than horizontal ones. Placer's computer program for the preliminary reserve calculation uses a filter that is one 40 ft. bench high with 200' search radius so that no effect of assays above or below is taken into account. The computer calculation is essentially a bench by bench polygonal calculation.

(2) There are twenty-two holes outlining the majority of the stage 1 reserves and thirty seven holes (including the ones that penetrate both stage 1 and stage 2) outlining the stage 2 reserves. When core assays are composited for each bench and each bench calculated separately independent of values on benches above and below by our present computer program there are effectively only 22 samples to provide the grade of ore on the stage 1 benches and 37 for the stage 2. These are insufficient for any accurate prediction of grade.

(3) The stage 1 and stage 2 pits provide the payback cash flow. On a .10% MoS_2 cutoff to the mill stage 1 contains 8,949,000 tons of .193% and stage 2 15,546,000 tons of .152%, for a total of 24,495,000 tons of .167% MoS_2.

...2

(4) David concluded that from geostatistics that considering blocks 400'x400'x40' that each block will be known with a precision of 5% with a 50' drilling grid, 10% with a 100' grid, 20% with a 200' grid and 43% with a 400' grid. Since most of stage 1 and 2 is drilled on a 200' grid we have a ±20% confidence in the grade, which at 15,000 TPD and nominal .19 mill heads in stage 1 represents a plus or minus 4 million pounds of MoS_2 per year or plus or minus 2.4 million pounds of Mo per year. At $7.00 US per pound Mo and .85 US to Canadian dollar exchange rate this represents plus or minus approximately 20 million Canadian dollars per year. Obviously we need more information to improve the predictability in the payback period.

(5) An inspection of the drill sections indicates that the highest grade continuous mineralization is on the sections with the most drill holes and particularly in the vicinity of the underground workings. If the arguments for upgrading are ignored there still remains the distinct possibility that in the central portion of the zone the grade may be higher than is indicated by the limited sampling - essentially 22 samples per bench in stage 1.

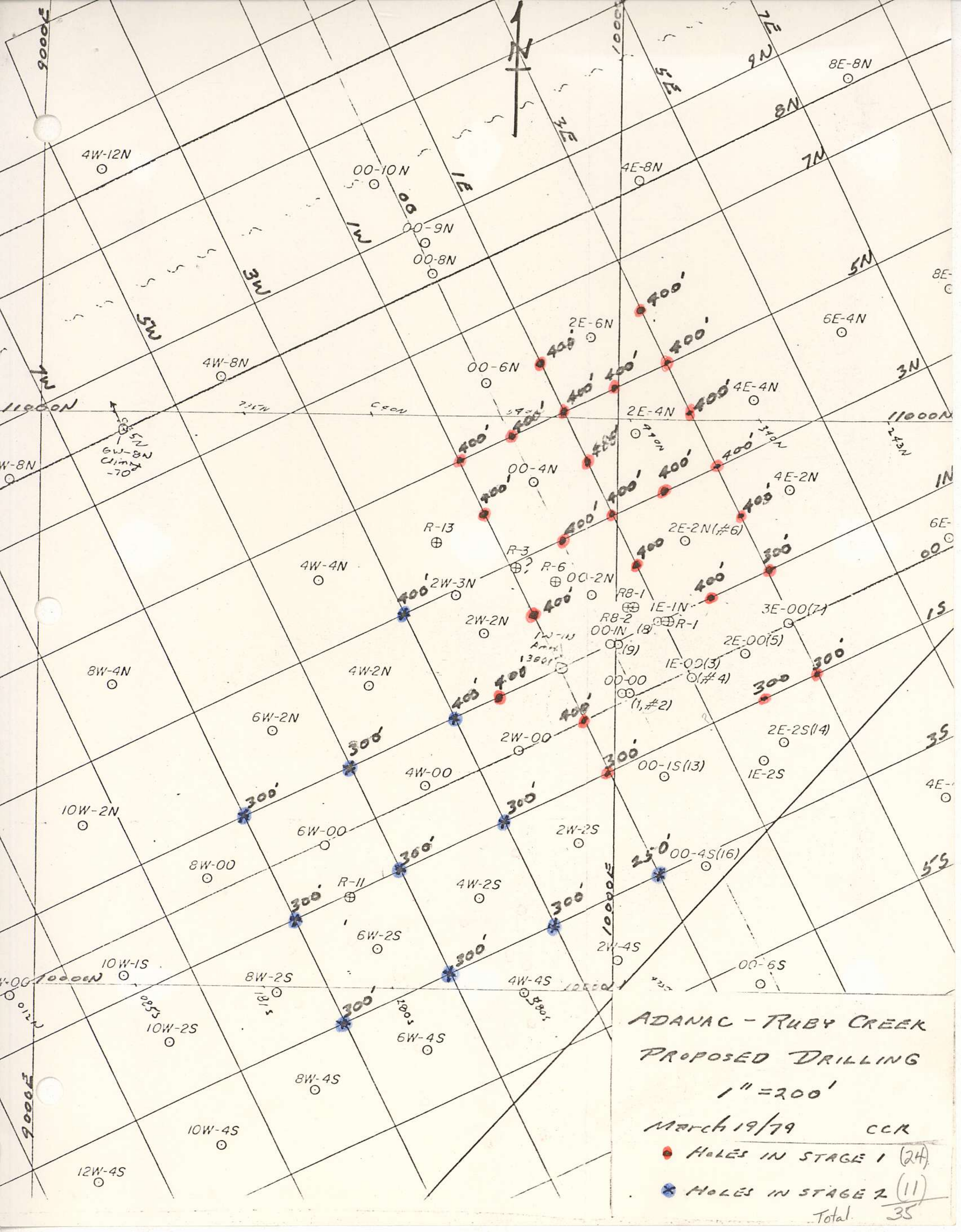
A pattern of fill in drilling is proposed to the bottom of stage 2 with holes at regular 100' spacing in the stage 1 area and 140' diagonal spacing in stage 2. This drilling will total 12,650' in 35 holes essentially doubling the number of holes in the stage 1 and 2 pit areas. (Appendix 1 and 2). This program, exclusive of any plant or tailings site investigation, and exclusive of exploration of surrounding areas is estimated to cost $400,000.00 (appendix 3).

Once the drill core has been logged in detail and photographed it should be all sent for assay or further metallurgical testing. There should be ample sample available for any bench scale metallurgical testing required. Total weight of sample to be shipped to Vancouver would be 38500 lbs. (17,500 Kg.).

The road and camp should be opened in May with the drilling to start in late May or early June. Engineering are requesting that a yet unspecified plant - tailings site program be carried out first by the same contractor. No provision has been made in the $400,000 estimate for this cost.

C.C. Rennie

CCR/cs
c.c. L. Adie/H.J. Matheson
E. Lonergan
S. Tennant
Engineering
Computers


ADANAC - RUBY CREEK
PROPOSED DRILLING
1" = 200'
March 19/79
CCR
HOLES IN STAGE 1 (24)
HOLES IN STAGE 2 (11)
Total 35
9000E
10000E
11000N
10000N
7E
9N
5E
8N
3E
7N
1E
5N
00
3N
1W
1N
3W
1S
5W
3S
7W
5S
8E-8N
4W-12N
00-10N
4E-8N
00-9N
00-8N
8E-
2E-6N
6E-4N
4W-8N
00-6N
4E-4N
2E-4N
W-8N
6W-8N
00-4N
4E-2N
R-13
2E-2N(#6)
6E-
R-3
R-6
4W-4N
2W-3N
00-2N
R8-1
1E-1N
R8-2
R-1
3E-00(7)
2W-2N
00-1N
(8)
(9)
2E-00(5)
8W-4N
4W-2N
1E-00(3)
(#4)
00-00
(1,#2)
6W-2N
2W-00
2E-2S(14)
4W-00
00-1S(13)
1E-2S
10W-2N
4E-
6W-00
2W-2S
8W-00
00-4S(16)
R-11
4W-2S
6W-2S
2W-4S
10W-1S
00-6S
8W-2S
4W-4S
10W-2S
6W-4S
8W-4S
10W-4S
12W-4S
400'
300'
250'

APPENDIX 2

Adanac - Proposed Drilling

Section	Northern	Footage
3E	6N	400'
	5N	400'
	4N	400'
	3N	400'
	2N	400'
	1N	300'
	1S	300'
2E	5N	400'
	3N	400'
	1N	400'
	1S	300'
1E	6N	400'
	5N	400'
	4N	400'
	3N	400'
	2N	400'
00E	5N	400'
	3N	400'
1W	5N	400'
	4N	400'
	2N	400'
	0N	400'
	1S	300'
	3S	250'

Section	Northing	Footage
2W	1N	400'
3W	3N	400'
	1N	400'
	1S	300'
	3S	300'
5W	1N	300'
	1S	300'
	3S	300'
7W	1N	300'
	1S	300'
	3S	300'
		12650'

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APPENDIX 3

Cost Estimate - Adanac Drill Program

Mobilization and Demob. of 2 rigs, crew and tractor	$25,000
Drill 12,650' @ $17.00/ft.	215,000
Moves 35 @ $400.00/move	14,000
Tractor time (guestimate)	8,000
Camp charges: Camp refurbishing 5000	
Camp operation 2 mo.@ 7500/mo 15000	
	20,000
Geology - 2 geologists, 2 months @ $2,500/mo.	10,000
- student labour, 2 for 2 months @ $1000/mo.	4,000
Vehicle charges	3,000
Surveying (questimate)	5,000
Freight on samples 1200 @ $10.00/sample	12,000
Sample preparation 1,700 @ $3.00/sample	3,600
Assaying 1,700 @ $7.00/sample	8,400
Probing holes for radioactivity	5,000
Computer data	10,000
Airfares	2,000
Supervision	3,000
	$348,000
Contingencies @ 15%	52,000
	$400,000

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I would agree that the raises should give better sampling than the drill holes but since the seven raises in the main part of the zone (excluding 4E-2N)which is only 28 ft. long) range in assays for the total lengths in fresh rock from .136 to .301 and the corresponding drill hole lengths range in grade from .090 to .328 I can only conclude that these are insufficient samples on which to base an ore reserve, or to argue any comparison for up-grading purposes.

Placer Computer Group point out that the accuracy of prediction of ore block grade depends on drill hole spacing and I would agree with this conclusion. For confirmation of ore reserve grade in the Adanac Ruby Creek deposit I would much rather have more NQ holes (with recovery maximized) than the equivalent cost but fewer PQ holes or raises. For this reason I would propose a program of 20 NQ fill-in drill holes at 100 ft. spacing within the stage 1 pit bottom area and drilled to the bottom of stage 2 pit, plus 14 NQ holes at 200 ft. spacing in the stage 2 pit extension to the southwest. This would total 12,050 ft. in 34 holes. If budgetary considerations limit the expenditure below the estimated $500,000 for this program the number of holes in the stage 2 pit extension area should be reduced.

If coincident holes and coincident drill holes and raises are each considered one sampling point, there are at present 17 vertical sampling points within the stage 1 pit bottom area. The above program proposes 20 additional sampling points within the same area which should markedly improve the confidence level of the reserve calculation.

The final mining reserve calculations for feasibility study should be based on all available data with no attempt at up-grading. The fact that the raises did average 10% higher grade in the fresh rock than the corresponding drill holes should suggest to most people that the deposit should mine out at a grade not lower than the ore reserve grade; and the proposed additional drilling should enhance the confidence in the reserve grade.

CCR:mg

C. C. RENNIE.

cc: D. C. Rotherham/D. A. Howard
J. H. Eastman/T. L. Horsley

PLACER DEVELOPMENT LIMITED

MEMORANDUM:

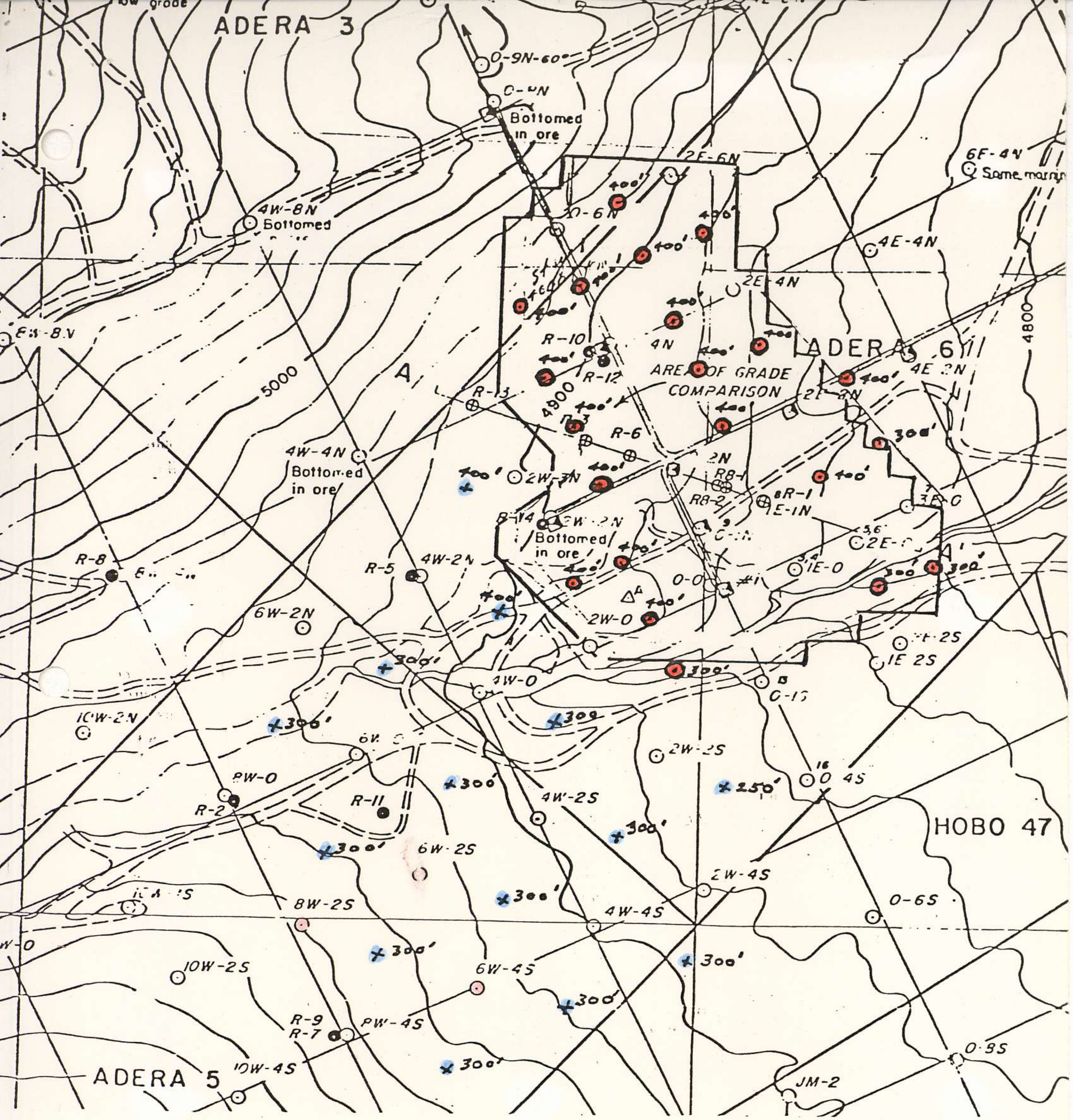
TO:	L. Adie/H. J. Matheson	DATE:	13 December 1978
FROM:	C. C. Rennie	FILE:	Grid 104-N-11
RE:	ADANAC'S RUBY CREEK MOLYBDENUM DEPOSIT RESERVES.		

The January 1978 reserve calculation of Ruby Creek molybdenum reserves by the Placer Computer Group used all available data with no up-grading and produced the following mining reserve (in short tons x 1000):

Pit	Cut-off Gr.	Ore Tons	Grade	Waste Tons	Total Tons	Strip Ratio
Stage 1	.07	10,207	.179	8,139	18,346	.80:1
Stage 2	.07	20,783	.135	15,964	36,747	.77:1
Ultimate	.07	35,603	.111	47,009	82,612	1.32:1
Total	.07	66,593	.129	71,112	137,705	1.07:1

Much has been written by CW&G and Equity about the possible up-grading of the reserves that has supposedly been indicated by a comparison of the bulk sampling of eight raises with the coincident drill core results. Two detailed statistical studies by Climax and by Placer's computer group tend to refute this up-grading by showing that the sample results from each method of sampling are in the same population groups. In my opinion the introduction of the up-grading argument has only served to cloud the issue and has psychologically reduced the confidence in the ore reserve grade to the point where more data is required before any engineering group would be happy predicating production on the data available.

It has been suggested that a program of PQ ($3\frac{11}{32}$") drilling within the pit area would provide more accurate sampling than NQ ($1\frac{7}{8}$") drilling. While this may be theoretically correct the relative volume of any size drill hole to the tonnage that it represents is so small that it would be very fortuitous if a drill hole, or in fact a raise, represented the grade of the surrounding tonnage exactly. It has been agreed that the raises, because of their larger size and more accurate sampling procedures, better represent the grade of the deposit than do the NQ drill core, particularly in the leached zone where drill core recovery was not as good as in the fresh rock. However, one BQ hole at 00N-00E with 90% core recovery gave slightly higher assays than the corresponding raise length, whereas the NQ hole at 00N-00E assayed only 66% of the raise assays.



ADANAC RUBY CREEK MOLYBDENUM

PROPOSED NQ FILL-IN DRILLING

1" = 200'

DEC/78 CCR.

⊙ PROPOSE HOLES – STAGE 1 PIT
20 HOLES = 7700'

× " " – STAGE 2 PIT
14 HOLES = 4350'

ST/C... file

PLACER DEVELOPMENT LIMITED

MEMORANDUM:

TO: D.C. Rotherham DATE: March 5th, 1979

FROM: E.S. Holt FILE: Venture 164

RE: ADANAC EXPLORATION DRILLING

During the period 1973 and 1974 Climax Molybdenum Corporation drilled nine diamond drill holes and deepened two others in the immediate vicinity of the Ruby Creek deposit. Two of these holes encountered significant molybdenite mineralization in areas which were previously unexplored.

Hole 6W-8N was collared on the south side of the Adera Fault and drilled at a shallow angle through the fault. It intersected 1,500 feet of material averaging .132% MoS_2 which included a 400 foot section assaying .200% MoS_2. Most of the better grade material was from within the broad fault zone.

The other hole of particular interest was collared at 36W-4N which is 1000 feet west of any previous drilling. The last 80 feet of this hole, from 1,020 to 1,100 feet averaged .229% MoS_2.

Both of the holes described above are isolated intersections which may or may not represent significant tonnage. Most importantly from the exploration standpoint, they demonstrate that reserve grade mineralization either extends beyond the presently known deposit or more probably they represent the discovery of other molybdenum concentrations.

Due in part to the depth of the intersections the possibility of either representing material which would be mined during the early operating years, must be regarded as remote. They do however, have the potential to significantly expand the ultimate reserves and could play an important role in overall planning.

Two new holes along strike from 6W-8N and the deepening of hole 36W-4N are recommended as an initial drilling program to determine the possible significance of the targets. Holes to the east and west of 6W-8N at 0-8N and 12W-8N will test the along strike potential of the initial intersection and provide pit slope data in the vicinity of the fault. They should be drilled to a depth of 2000 feet at a bearing of N30°W with a -70° dip.

...2/

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Hole 36W-4N should be deepened to beyond any significant mineralization (say 900 feet to a total depth of 2000 feet). Additional drilling would be contingent on the results of these holes and the significance they could have on the project.

Detail of holes 6W-8N and 36W-4N are appended.

It is of interest to note that by drilling 9 holes Climax came up with two promising exploration targets. This speaks well for the general exploration potential of the Ruby Creek area.

Respectfully submitted

E.S. Holt

ESH/cs

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DETAIL OF HOLE 6W-8N

Drill hole 6W-8N was collared approximately 200 feet south of the Adera fault and was drilled at a -70° dip toward the fault. It initially encountered significant fault gouge and broken rock at 450 feet and then remained in fairly continuous , incompetent and often badly broken materail with various degrees of shearing and slickensiding, to the end of the hole at 2000 feet.

A summary of the assay results are:

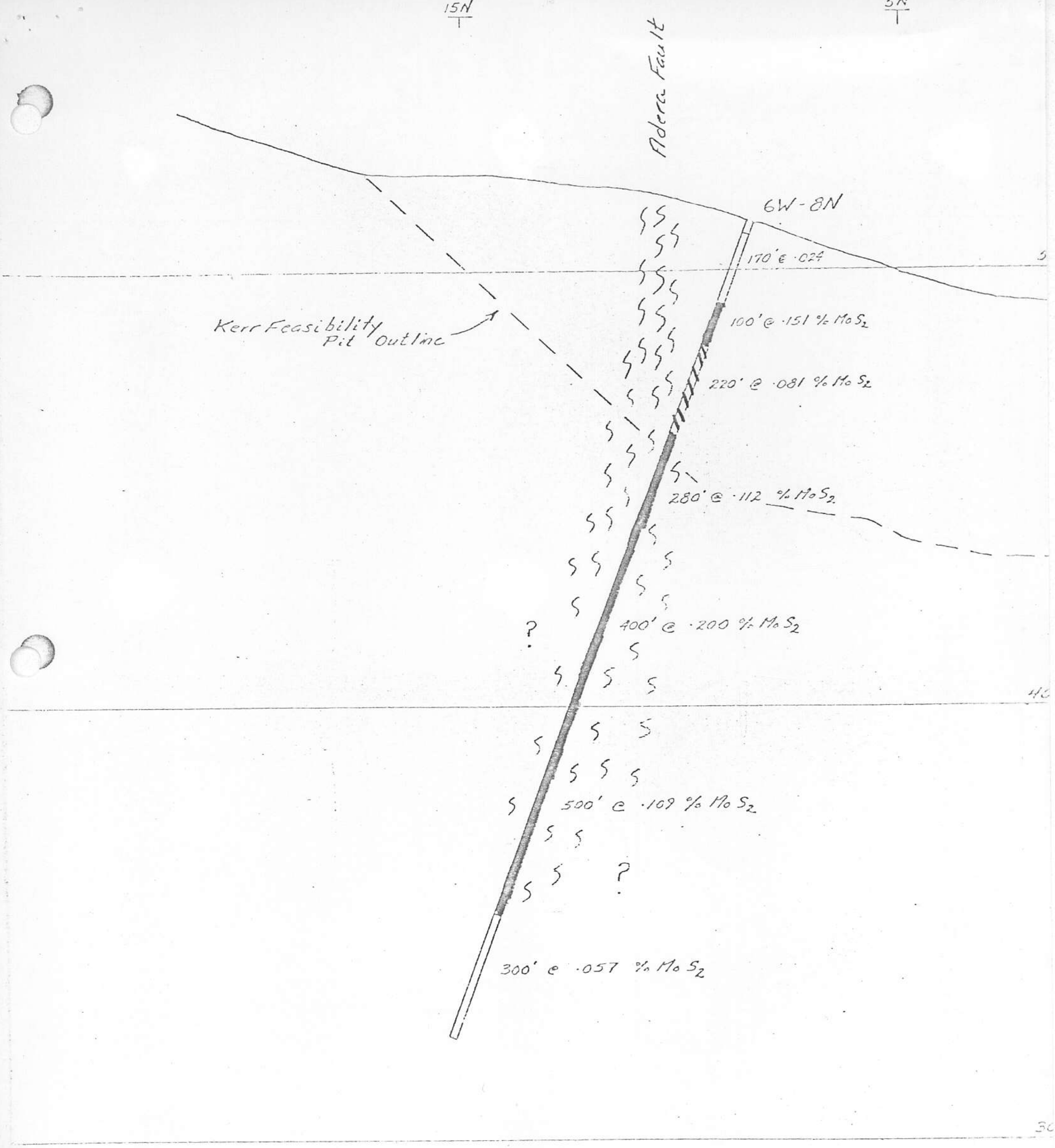
30 to 200 ft.	170 ft. @ .024% MoS_2
200 to 300 ft.	100 ft. @ .151% MoS_2
300 to 520 ft.	220 ft. @ .081% MoS_2
520 to 800 ft.	280 ft. @ .112% MoS_2
800 to 1200 ft.	400 ft. @ .200% MoS_2
1200 to 1700 ft.	500 ft. @ .109% MoS_2
1700 to 2000 ft.	300 ft. @ .057% MoS_2

Core recoveries apparently were not determined. Some visual estimates and other comments were recorded in the geologic logs which indicate that local portions had very low core recovery. Most of the core was soft and badly broken with slickensiding and fault gouge common. Some sections were reported as recovering "only sand", which in all probability meant that almost everything other than the quartz grains had been washed away, including a disproportionate portion of the molybdenite.

With regard to evaluation of the intersection, the width of the "mineralized fault zone" is open to speculation. Dip tests are not available for the drill hole and the fault zone itself is equally ill defined. Assuming the fault is verticle and the hole ran true at -70°, the intersection would have a width of approximately 400 feet, and could represent significant tonnage. Each 5 degrees of flattening or steepening would add or subtract approximately 100 feet from the true width of the intersection.

Only one other hole, 0-9N, intersected the Adera fault zone. It had a similar -70° dip and north 30° west bearing. It intersected the fault zone much nearer surface and contained much lower grade molybdenite mineralization. It also encountered a broad zone of faulting, but not to the extent of 6W-8N. In 0-9N the bulk of the faulting was within a 400 foot interval, while in 6W-8N it extended over 1200 feet. Possible explanations for the apparently much broader zone in the deeper hole are:

1. Horsetailing of the main fault zone.
2. Widening of the zone with depth
3. Deviation of the drill hole parallel to the fault zone.
4. Warping of the fault zone to closely correspond with the dip of the drill hole.



Section Through 6W
Looking East

Scale : 1 inch = 300 ft

Situations 1 or 2 above, could result in significant tonnage potential, while 3 and 4 would minimize the zones width. In all probability additional drilling will be required in order to evaluate the potential of the zone. Careful study of the drill core may help to determine the angle at which the drill hole intersected the fault zone and tropari test down the hole would provide accurate survey data regarding deviation from the initial bearing and dip.

The lower molybdenite content in hole 0-9N, which also cut the Adera fault zone could be the result of near surface leaching as noted in the underground bulk sampling results. The molybdenite content was often much lower in the upper 100 feet of bedrock. In the case of the broken fault zone the leached portion would be expected to extend deeper. Additional drilling to test the significance of the intersection in hole 6W-8N may therefore have to cut the fault zone at considerable depth in order to accurately assess the grade potential.

A detailed geologic log and an assay log have been provided to Adanac. The core was sampled over ten foot intervals and assayed at Skyline Labs.Inc. of Colorado. Detail of the assay results are appended.

DETAIL OF HOLE 36W-4N

This hole was drilled 1000 feet west of any previous holes at Ruby Creek. As will be noted on plan, it was collared near the divide at the headwaters of Ruby Creek and was drilled vertically to a depth of 1100 feet.

The hole has been logged as coarse alaskite over almost its entire length with a few short intervals of fine alaskite and a section from 950 to 1020 containing rock described as MCA ?; possibly medium coarse alaskite. The upper 1000 feet of the hole is visually described as being essentially barren with rare disseminated MoS_2, infrequent quartz filled fracturing and weak alteration. The most notable change in the vicinity of 1000 feet, where the MoS_2 grade dramatically increases is the much more broken nature of the rock and the appearance of MCA noted above. The final 80 feet which average .229% MoS_2 is described as coarse alaskite. Although this section is generally badly broken, one interval from 1050 to 1060, which assayed .416% MoS_2, is noted to be very competent and unbroken.

The location of hole 36W-4N, within a tight valley, with 1000 feet of barren material overlying the mineralized section, eliminates any open pit potential in that immediate area. This fact does not detract from its overall importance however, in that it has demonstrated that reserve grade mineralization at Ruby Creek is not limited to the presently outlined deposit. This feature dramatically enhances the exploration potential of the area.

ADANAC

Drill Hole Number: 36W - 4N

Dollar Coordinates: 6562E 9410N

Collar Elevation: 5160 feet

Bearing: ---

Dip: Vertical

Length: 1100 feet

Key:

Footage	Sample Number	$\%MoS_2$	
90 - 980	No assays made		
980 - 990	A-74-347	.027	
990 - 1000	A-74-348	.131	
1000 - 1010	A-74-349	.035	
1010 - 1020	A-74-350	.036	
1020 - 1030	A-74-351	.284	
1030 - 1040	A-74-352	.107	
1040 - 1050	A-74-353	.377	
1050 - 1060	A-74-354	.416	0.229% MoS_2
1060 - 1070	A-74-355	.091	
1070 - 1080	A-74-356	.042	
1080 - 1090	A-74-357	.019	
1090 - 1100	A-74-358	.494	

Replicates:

None

ADANAC

Drill Hole Number: 6W - 8N

Collar Coordinates: 9150E 10980N

Collar Elevation: 5110 feet

Bearing: N30W

Dip: -70°

Length: 2000 feet

Key:

Footage	Sample Number	% MoS_2
30 - 40	A-73-1	.017
40 - 50	A-73-2	.013
50 - 60	A-73-3	.023
60 - 70	A-73-4	.022
70 - 80	A-73-5	.026
80 - 90	A-73-6	.017
90 - 100	A-73-7	.0090
100 - 110	A-73-8	.0085
110 - 120	A-73-9	.010
120 - 130	A-73-10	.0020
130 - 140	A-73-11	.0055
140 - 150	A-73-12	.0050
150 - 160	A-73-13	.075
160 - 170	A-73-14	.036
170 - 180	A-73-15	.035
180 - 190	A-73-16	.051
190 - 200	A-73-17	.049
200 - 210	A-73-18	.170
210 - 220	A-73-19	.110
220 - 230	A-73-20	.102
230 - 240	A-73-21	.087
240 - 250	A-73-22	.103
250 - 260	A-73-23	.369
260 - 270	A-73-24	.075
270 - 280	A-73-25	.076
280 - 290	A-73-26	.355
290 - 300	A-73-27	.059

ADANAC
Drill Hole No. 6W - 8N

Footage	Sample Number	% MoS_2
300 - 310	A-73-28	.040
310 - 320	A-73-29	.054
320 - 330	A-73-30	.182
330 - 340	A-73-31	.072
340 - 350	A-73-32	.099
350 - 360	A-73-33	.082
360 - 370	A-73-34	.158
370 - 380	A-73-35	.032
380 - 390	A-73-36	.125
390 - 400	A-73-37	.071
400 - 410	A-73-38	.111
410 - 420	A-73-39	.096
420 - 430	A-73-40	.084
430 - 440	A-73-41	.042
440 - 450	A-73-42	.061
450 - 460	A-73-43	.096
460 - 470	A-73-44	.128
470 - 480	A-73-45	.044
480 - 490	A-73-46	.026
490 - 500	A-73-47	.071
500 - 510	A-73-48	.045
510 - 520	A-73-49	.060
520 - 530	A-73-50	.270
530 - 540	A-73-51	.197
540 - 550	A-73-52	.231
550 - 560	A-73-53	.058
560 - 570	A-73-54	.054
570 - 580	A-73-55	.052
580 - 590	A-73-56	.063
590 - 600	A-73-57	.170
600 - 610	A-73-58	.045
610 - 620	A-73-59	.034
620 - 630	A-73-60	.047
630 - 640	A-73-61	.049
640 - 650	A-73-62	.047
650 - 660	A-73-63	.100
660 - 670	A-73-64	.029
670 - 680	A-73-65	.228
680 - 690	A-73-66	.118
690 - 700	A-73-67	.066
700 - 710	A-73-68	.092
710 - 720	A-73-69	.173

ADANAC
Drill Hole No. 6W - 8N

Footage	Sample Number	% MoS_2
720 - 730	A-73-70	.082
730 - 740	A-73-71	.113
740 - 750	A-73-72	.147
750 - 760	A-73-73	.148
760 - 770	A-73-74	.100
770 - 780	A-73-75	.172
780 - 790	A-73-76	.128
790 - 800	A-73-77	.113
800 - 810	A-73-78	.615
810 - 820	A-73-79	.097
820 - 830	A-73-80	.080
830 - 840	A-73-81	.049
840 - 850	A-73-82	.280
850 - 860	A-73-83	.028
860 - 870	A-73-84	.108
870 - 880	A-73-85	.161
880 - 890	A-73-86	.465
890 - 900	A-73-87	.031
900 - 910	A-73-88	.265
910 - 920	A-73-89	.118
920 - 930	A-73-90	.084
930 - 940	A-73-91	.319
940 - 950	A-73-92	.142
950 - 960	A-73-93	.086
960 - 970	A-73-94	.327
970 - 980	A-73-95	.229
980 - 990	A-73-96	.228
990 - 1000	A-73-97	.028
1000 - 1010	A-73-98	.334
1010 - 1020	A-73-99	.217
1020 - 1030	A-73-100	.233
1030 - 1040	A-73-101	.474
1040 - 1050	A-73-102	.112
1050 - 1060	A-73-103	.029
1060 - 1070	A-73-104	.017
1070 - 1080	A-73-105	.023
1080 - 1090	A-73-106	.012
1090 - 1100	A-73-107	.101
1100 - 1110	A-73-108	.035
1110 - 1120	A-73-109	1.01
1120 - 1130	A-73-110	.040

ADANAC
Drill Hole No. 6W - 8N

Footage	Sample Number	% MoS_2
1130 - 1140	A-73-111	.015
1140 - 1150	A-73-112	.012
1150 - 1160	A-73-113	.553
1160 - 1170	A-73-114	.309
1170 - 1180	A-73-115	.487
1180 - 1190	A-73-116	.211
1190 - 1200	A-73-117	.039
1200 - 1210	A-73-118	.035
1210 - 1220	A-73-119	.045
1220 - 1230	A-73-120	.539
1230 - 1240	A-73-121	.047
1240 - 1250	A-73-122	.022
1250 - 1260	A-73-123	.018
1260 - 1270	A-73-124	.111
1270 - 1280	A-73-125	.071
1280 - 1290	A-73-126	.090
1290 - 1300	A-73-127	.153
1300 - 1310	A-73-128	.019
1310 - 1320	A-73-129	.084
1320 - 1330	A-73-130	.074
1330 - 1340	A-73-131	.375
1340 - 1350	A-73-132	.062
1350 - 1360	A-73-133	.057
1360 - 1370	A-73-134	.241
1370 - 1380	A-73-135	.175
1380 - 1390	A-73-136	.034
1390 - 1400	A-73-137	.023
1400 - 1410	A-73-138	.148
1410 - 1420	A-73-139	.062
1420 - 1430	A-73-140	.082
1430 - 1440	A-73-141	.112
1440 - 1450	A-73-142	.171
1450 - 1460	A-73-143	.048
1460 - 1470	A-73-144	.186
1470 - 1480	A-73-145	.068
1480 - 1490	A-73-146	.084
1490 - 1500	A-73-147	.019
1500 - 1510	A-73-148	.055
1510 - 1520	A-73-149	.080
1520 - 1530	A-73-150	.054
1530 - 1540	A-73-151	.111

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Footage	Sample Number	% MoS_2
1540 - 1550	A-73-152	.160
1550 - 1560	A-73-153	.049
1560 - 1570	A-73-154	.173
1570 - 1580	A-73-155	.115
1580 - 1590	A-73-156	.068
1590 - 1600	A-73-157	.095
1600 - 1610	A-73-158	.024
1610 - 1620	A-73-159	.086
1620 - 1630	A-73-160	.028
1630 - 1640	A-73-161	.035
1640 - 1650	A-73-162	.246
1650 - 1660	A-73-163	.072
1660 - 1670	A-73-164	.146
1670 - 1680	A-73-165	.100
1680 - 1690	A-73-166	.153
1690 - 1700	A-73-167	.076
1700 - 1710	A-73-168	.343
1710 - 1720	A-73-169	.065
1720 - 1730	A-73-170	.054
1730 - 1740	A-73-171	.027
1740 - 1750	A-73-172	.034
1750 - 1760	A-73-173	.058
1760 - 1770	A-73-174	.067
1770 - 1780	A-73-175	.034
1780 - 1790	A-73-176	.034
1790 - 1800	A-73-177	.051
1800 - 1810	A-73-178	.065
1810 - 1820	A-73-179	.046
1820 - 1830	A-73-180	.106
1830 - 1840	A-73-181	.061
1840 - 1850	A-73-182	.050
1850 - 1860	A-73-183	.048
1860 - 1870	A-73-184	.075
1870 - 1880	A-73-185	.088
1880 - 1890	A-73-186	.037
1890 - 1900	A-73-187	.054
1900 - 1910	A-73-188	.125
1910 - 1920	A-73-189	.058
1920 - 1930	A-73-190	.057
1930 - 1940	A-73-191	.036
1940 - 1950	A-73-192	.028

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Footage	Sample Number	% MoS_2
1950 - 1960	A-73-193	.032
1960 - 1970	A-73-194	.019
1970 - 1980	A-73-195	.033
1980 - 1990	A-73-196	.018
1990 - 2000	A-73-197	.017

Replicates:

Sample Number	Replicate of:	% MoS_2
A-73-5X	A-73-5 from 3rd split @ 65 mesh.	.026
A-73-10X	A-73-10 from 2nd split @ 65 mesh.	.0014
A-73-15X	A-73-15 from 1st split @ 65 mesh.	.036
A-73-20X	A-73-20 from 1st split @ 10 mesh.	.108
A-73-25X	A-73-25 from 3rd split @ 65 mesh.	.076
A-73-30X	A-73-30 from 2nd split @ 65 mesh.	.180
A-73-35X	A-73-35 from 3rd split @ 65 mesh.	.031
A-73-40X	A-73-40 from 1st split @ 10 mesh.	.085
A-73-45X	A-73-45 from 3rd split @ 65 mesh.	.043
A-73-50X	A-73-50 from 2nd split @ 65 mesh.	.274
A-73-55X	A-73-55 from 1st split @ 65 mesh.	.053
A-73-60X	A-73-60 from 1st split @ 10 mesh.	.047
A-73-65X	A-73-65 from 3rd split @ 65 mesh.	.225
A-73-70X	A-73-70 from 2nd split @ 65 mesh.	.083
A-73-75X	A-73-75 from 1st split @ 65 mesh.	.173
A-73-80X	A-73-80 from 1st split @ 10 mesh.	.081
A-73-85X	A-73-85 from 3rd split @ 65 mesh.	.159
A-73-90X	A-73-90 from 2nd split @ 65 mesh.	.084
A-73-95X	A-73-95 from 1st split @ 65 mesh.	.230
A-73-100X	A-73-100 from 1st split @ 10 mesh.	.223
A-73-105X	A-73-105 from 3rd split @ 65 mesh.	.023
A-73-110X	A-73-110 from 2nd split @ 65 mesh.	.038
A-73-115X	A-73-115 from 1st split @ 65 mesh.	.471
A-73-120X	A-73-120 from 1st split @ 10 mesh.	.546
A-73-125X	A-73-125 from 3rd split @ 65 mesh.	.070
A-73-130X	A-73-130 from 2nd split @ 65 mesh.	.072
A-73-135X	A-73-135 from 1st split @ 65 mesh.	.177
A-73-140X	A-73-140 from 1st split @ 10 mesh.	.081
A-73-145X	A-73-145 from 3rd split @ 65 mesh.	.077
A-73-150X	A-73-150 from 2nd split @ 65 mesh.	.056
A-73-155X	A-73-155 from 1st split @ 65 mesh.	.115

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Sample Number	Replicate of:	% MoS_2
A-73-160X	A-73-160 from 1st split @ 10 mesh.	.027
A-73-165X	A-73-165 from 3rd split @ 65 mesh.	.097
A-73-170X	A-73-170 from 2nd split @ 65 mesh.	.054
A-73-175X	A-73-175 from 1st split @ 65 mesh.	.032
A-73-180X	A-73-180 from 1st split @ 10 mesh.	.107
A-73-185X	A-73-185 from 3rd split @ 65 mesh.	.088
A-73-190X	A-73-190 from 2nd split @ 65 mesh.	.053
A-73-195X	A-73-195 from 1st split @ 65 mesh.	.032