

860737

GEOLOGICAL, GEOCHEMICAL and GEOPHYSICAL REPORT

on the

TWIN PROPERTY

Kamloops Mining Division

British Columbia

Claim Name:	TWIN 1	Record No.	2403
	TWIN 2		2404
	TWIN 3		2405

Latitude: 51° 08' North Longitude: 119° 47' West

N.T.S. 82 M / 4 W

OWNERS: LINCOLN RESOURCES INC. and APEX ENERGY CORP.

Suite 450 - 800 West Pender Street
Vancouver, B.C. V6C 2V6
(604) 684-2710

OPERATOR: LINCOLN RESOURCES INC.

Suite 450 - 800 West Pender Street
Vancouver, B.C. V6C 2V6
(604) 684-2710

CONTRACTOR: MINOREX CONSULTING LTD.

Suite 200A - 156 Victoria Street
Kamloops, B.C. V2C 1Z7
(604) 372-2181

February 24, 1987

J. D. Blanchflower, F.G.A.C.
Geologist

Z. Doborzynski, P. Eng.
Geophysicist

TABLE OF CONTENTS

	Page No.
INTRODUCTION.....	1
SUMMARY.....	1
RECOMMENDATIONS.....	5
GENERAL DESCRIPTION.....	6
Location and Access.....	6
Physiography.....	6
Claim Ownership.....	6
History.....	8
GEOLOGIC SETTING.....	9
RESULTS OF PREVIOUS EXPLORATION WORK.....	13
1986 EXPLORATION PROGRAM.....	15
Survey Control Grid.....	16
Geological Survey.....	16
Geochemical Surveys.....	16
Soil Geochemical Survey.....	16
Lithogeochemical Survey.....	17
Geophysical Survey.....	18
Fixed Source Genie Electromagnetic Survey....	18
Trenching Program.....	18
RESULTS OF THE 1986 EXPLORATION PROGRAM.....	18
Geological Survey.....	18
Lithology.....	19
Structure.....	21
Alteration.....	22
Mineralization.....	22

TABLE OF CONTENTS

	Page No.
Geochemical Surveys.....	23
Soil Geochemical Survey.....	23
Lithogeochemical Survey.....	26
Geophysical Survey.....	26
Fixed Source Genie Electromagnetic Survey....	26
Trenching Program.....	27
DISCUSSION OF THE EXPLORATION RESULTS.....	29
EXPLORATION POTENTIAL.....	31
CONCLUSIONS.....	33
STATEMENTS OF QUALIFICATIONS.....	35
STATEMENT OF COSTS.....	38
BIBLIOGRAPHY.....	40

APPENDICES

Appendix I:	Geophysical Report on the TWIN Property
Appendix II:	Fixed Source Genie Electromagnetic Survey Survey Data and Profiles
Appendix III:	Acme Analytical Laboratories Ltd. Soil Geochemical Results
Appendix IV:	Acme Analytical Laboratories Ltd. Lithogeochemical Results
Appendix V:	Soil Geochemical Statistics
Appendix VI:	Lithogeochemical Statistics
Appendix VII:	Lithogeochemical Sample Descriptions

LIST OF ILLUSTRATIONS

Figure No.		Page No.
1	Location Map, 1 inch = 64 miles.....	2
2	Claim Map, 1 : 50,000.....	7
3	Regional Geology Map, 1 : 200,000.....	10
4	Geological Plan, 1 : 5,000.....	In Pocket
5	Soil Geochemical Plan, Gold (p.p.b.), 1 : 5,000.....	In Pocket
6	Soil Geochemical Plan, Silver (p.p.m.), 1 : 5,000.....	In Pocket
7	Soil Geochemical Plan, Copper (p.p.m.), 1 : 5,000.....	In Pocket
8	Soil Geochemical Plan, Lead (p.p.m.), 1 : 5,000.....	In Pocket
9	Soil Geochemical Plan, Zinc (p.p.m.), 1 : 5,000.....	In Pocket
10	Soil Geochemical Plan, Arsenic (p.p.m.), 1 : 5,000.....	In Pocket
11	Soil and Lithogeochemical Plan, Barium (p.p.m.), 1 : 5,000.....	In Pocket
12	Geophysical Plan, Electromagnetics Survey, Frequency Ratio 112/37, 1 : 5,000.....	In Pocket
13	Geophysical Plan, Electromagnetics Survey, Frequency Ratio 337/37, 1 : 5,000.....	In Pocket
14	Geophysical Plan, Electromagnetics Survey, Frequency Ratio 1012/37, 1 : 5,000.....	In Pocket
15	Geophysical Plan, Electromagnetics Survey, Frequency Ratio 3037/37, 1 : 5,000.....	In Pocket
16	Trenching Plan, 1 : 1,000.....	In Pocket
17	Compilation Plan, Geology, Geochemistry, Geophysics and Trenching, 1 : 5,000.....	In Pocket

INTRODUCTION

Lincoln Resources Inc. and Apex Energy Corp. of Vancouver, B.C. jointly own the TWIN property. This property is comprised of three M.G.S. mineral claims, totalling 39 units; all situated in the Kamloops Mining Division of British Columbia.

This report documents the results of the geological, geochemical and geophysical surveys, and trenching that were carried out on behalf of Lincoln Resources Inc. during the 1986 field season.

The 1986 exploration program included: relabelling a portion of the existing control grid (14.0 line-km.), establishment of additional control grid (15.15 line-km.), geological mapping at a scale of 1:5,000, soil and lithogeochemical sampling (361 soil and 63 rock samples), geophysical surveying (fixed source Genie electromagnetic survey, 17.75 line-km.), and trenching (300 metres). This work was carried out between October 16 and December 16, 1986. The report and accompanying plans were prepared after all the analytical and statistical data were received, plotted, interpreted and evaluated.

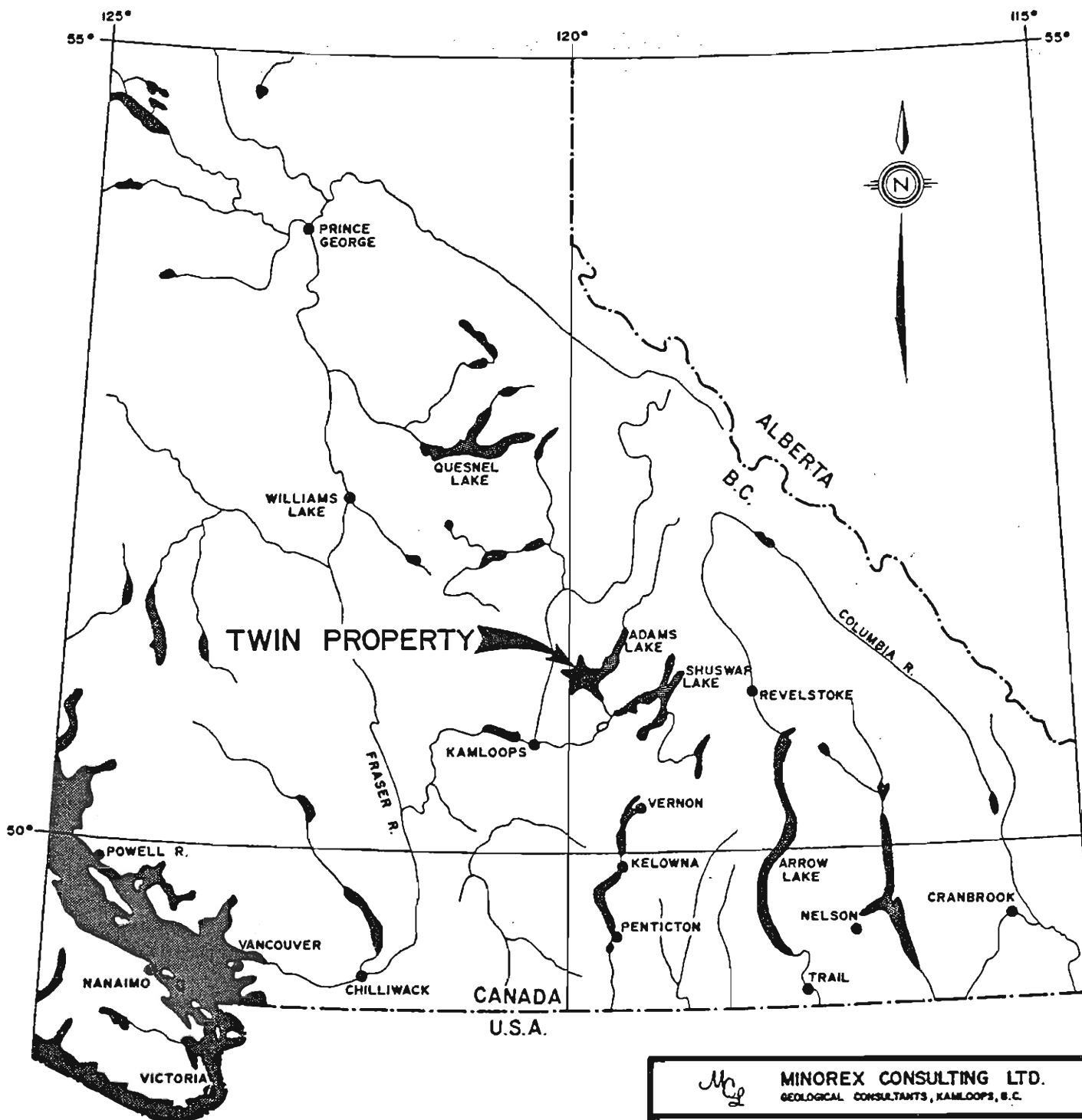
The writers supervised all phases of exploration, and wrote this report which documents its results and those of the previous work by Austin Resources Inc., Corporation Falconbridge Copper and Spirex Geoservices Ltd.

SUMMARY

The TWIN property is situated on the southeastern slopes of Samatsum Mountain, within the Interior Plateau of southcentral British Columbia. Its geographic coordinates are 51° 08' North latitude by 119° 47' West longitude (N.T.S. 82M/4W). The claim group is located 25 kilometres east-southeast of the town of Barrriere, or 60 kilometres north-east of the city of Kamloops.

Vehicular access is possible from Kamloops via either Highway 5 northward to Louis Creek, thence eastward to Skwaam Bay on Adams Lake; or eastward on Highway 1 to Squilax, then northward to Skwaam Bay. At Skwaam Bay a well maintained logging haulage road (Adams West) leads northward along the western side of Adams Lake. The 3,000 logging road joins the Adams West road 8 kilometres north of Skwaam Bay. This seasonal gravel logging road leads northwesterly up the southern slopes of Samatsum Mountain and joins the 3,200 logging road which crosses the claim group. It is approximately 130 kilometres by road from Kamloops.

Elevations within the property range from 4,400 to 5,600 feet A.M.S.L. The climate is moderate with temperatures ranging from -25° C. to +30° C. Precipitation is usually moderate to heavy.



J.D. Blanchflower

To accompany a report by J.D. Blanchflower.

Mc

MINOREX CONSULTING LTD.
GEOLOGICAL CONSULTANTS, KAMLOOPS, B.C.

LINCOLN RESOURCES INC.
VANCOUVER, BRITISH COLUMBIA

LOCATION MAP

TWIN PROPERTY
KAMLOOPS MINING DIVISION, B.C.

DATE: AUG. 18/86

SCALE: 1" = 64 mi.

DWN. BY: T.Q./T.

DWG. NO.: 1

The exploration season may extend from May to November.

The property comprises three M.G.S. mineral claims (39 units), called the TWIN 1 to 3. It is currently owned jointly by Lincoln Resources Inc. (51%) and Apex Energy Corp. (49%).

The first documented work on the property is reported in the 1936 B.C. Minister of Mines Annual Report (p. D 39). Trenching had traced a silver and base metal-bearing 'dolomite' zone for approximately 4,600 feet with an average width of 9 to 20 feet. The government geologist reported results of six samples ranging from: trace to 0.50 oz./ton gold, trace to 5.0 oz./ton silver, nil to 36.50 % lead, and nil to 3.7 % zinc.

The 'Twin Mountain' property was optioned to Camoose Mines Limited by C.C. Keller of Louis Creek in 1952. A 7.5-mile access road was built from Skwaam Bay that fall; and in 1953, two exploration tunnels were driven, 330 and 440 feet. In 1967 and 1968, Sinmax Mines conducted a detailed exploration program which included: linecutting, geochemical and geophysical surveying, and some underground mapping and sampling (Read, 1968). Sinmax Mines prospected their claim holdings, excavated 15 trenches, and mapped the surface showings and underground workings in 1969. In 1981 and 1982, Apex Energy Corp. conducted geological, geochemical and geophysical surveying over the known base metal showings.

In December, 1983, Austin Resources Inc. negotiated an option agreement with Apex Energy Corp. A preliminary control grid was established and limited soil geochemical sampling was conducted that field season.

Corporation Falconbridge Copper (C.F.C.), the operator of the adjoining Rea (AR/HN) property, explored the Twin property in 1984 with: geological mapping (1:2,500), soil and rock geochemical sampling, geophysical surveying (V.L.F.-EM and Max-Min II), and drilling (2 holes). After Corporation Falconbridge Copper terminated their option in April, 1985, Lincoln Resources Inc. conducted fill-in soil geochemical sampling.

The property is dominantly underlain by volcanic and volcanoclastic units belonging to the Eagle Bay Formation of Late Devonian to Early Mississippian age. They include ash- to agglomerate-size tuffs, locally pyritized with fine-grained disseminations and veinlets. All lithologies have experienced regional greenschist metamorphism which has produced a strong penetrative foliation and widespread chloritization of the more mafic members. These units have been structurally inverted by a combination of isoclinal folding and repetitive faulting.

The stratigraphy trends northwesterly and dips northeasterly. Bedding attitudes show that the lithologies dip from -44° to -60° northeastward. Faults are common in this region, often parallel with or perpendicular to the schistosity.

The 1986 exploration program included: relabelling a portion

of the existing control grid (14.0 line-km.), establishment of additional control grid (15.15 line-km.), geological mapping at a scale of 1:5,000, soil and lithogeochemical sampling (361 soil and 63 rock samples), geophysical surveying (fixed source Genie electromagnetic survey, 17.75 line-km.), and trenching (300 metres). This work was carried out between October 16 and December 16, 1986. The report and accompanying plans were prepared after all the analytical and statistical data were received, plotted, interpreted and evaluated.

Geological results show that the southern portion of the property is dominantly underlain by older mafic volcanic and volcanoclastic rocks of the Eagle Bay Formation. These rocks are repetitively bedded as a rather thick volcanic pile with no obvious hiatuses in volcanism. Such a setting is indicative of an ancient volcanic seamount deposited during a period of relatively rapid and continuous volcanism with few, if any, periods of quiescence, sedimentation or sulphide deposition.

Trenching in the northwestern portion of the property exposed graphitic argillites with intercalated very fine-grained epiclastic and tuffaceous sediments. These thinly-bedded rocks appear to conformably overlie lapilli tuffs and argillaceous 'muddy' tuffs of the volcanic sequence.

A total of 2,611 B-horizon soil geochemical samples have now been collected from this property. Their analytical results indicate three dominant geochemical trends. These trends are:

- 1) Twin Mountain Trend (L 60+00 East by 3+00 North to L 73+00 East by 2+00 North) - reflects the known mineralization at the 'Twin Mountain' lead-zinc-silver prospect. The linear lead, zinc, silver and copper anomalies appear to be off-set northeasterly as they trend northwestward from the Twin Mountain silver-lead-zinc showings.
- 2) Ridge Trend (L 60+00 East by 2+50 South to L 83+00 East by 1+00 North) - has a very strong silver, gold and copper response and it is underlain by mafic volcanic and volcanoclastic rocks which are locally altered. The alteration zones are silicified, pyritized and sparingly mineralized with chalcopyrite, galena, sphalerite, magnetite and hematite; and
- 3) Homestake Trend (L 83+00 East by 1+00 South to L 76+00 East by 1+50 South) - is reflected by anomalous arsenic, gold and lead soil geochemistry. It overlies the stratigraphic contact between the major volcanic and sedimentary units, and appears to be truncated by an apparent northeasterly trending fault zone along the Homestake Creek.

The highest metal values from all of the lithogeochemical sampling are: 260 p.p.b. gold, 2.8 p.p.m. silver, 316 p.p.m. copper, 4,567 p.p.m. lead and 7,252 p.p.m. zinc. No economic mineralization was discovered.

The results of the interpreted geophysical survey data indicate ten electromagnetic conductors with weak to relatively high responses. All of these conductors trend northwestward, paralleling the stratigraphy.

Five conductors appear to be reflecting lithologic changes (e.g. Conductors 'C', 'E', 'F', 'G' and 'J') and one conductor appears to be reflecting the stratigraphic contact between the volcanic and sedimentary units (e.g. Conductor 'D').

The most interesting conductors include: Conductor 'A', which is probably responding to underlying carbonaceous sedimentary rocks, although, it does occur in an area through which the 'Discovery' horizon is inferred to occur; Conductor 'H', which is interesting in that it overlies a mapped dioritic intrusion with abundant pyritization and local copper soil geochemistry; and Conductor 'I', which reflects the 'Twin Mountain' lead-zinc mineralization and was the best conductor of the survey.

It is the writer's opinion that further exploration work is warranted, but this work should be directed at evaluating specific exploration targets.

RECOMMENDATIONS

The highest priority target is undoubtedly the geological, geochemical and/or geophysical anomalies in the northwestern corner of the claim group. This target, called the 'Homestake' trend, will require an extensive trenching and/or diamond drilling program.

The 'Twin Mountain' silver-lead-zinc showings should be re-examined. Recent exploration work at the 'Silver Zone', on the Rea property, shows that there is late-stage or post-metamorphic veining superimposed on a syngenetic sulphide-bearing horizon. Perhaps past exploration efforts on the 'Twin Mountain' prospect might not have recognized such a geologic setting.

The dioritic intrusion with its attendant copper geochemical response, northwest of the 'Twin Mountain' prospect, should be examined to see if there is a potential there for contact metasomatic mineralization.

The 'Twin Mountain' and dioritic intrusion targets will require detailed geological mapping, lithogeochemical sampling and 'fill-in' geophysical surveying. Trenching and diamond drilling might follow this work when the 'Homestake' target is evaluated.

GENERAL DESCRIPTION

Location and Access

The TWIN property is located in the Kamloops Mining Division of southcentral British Columbia. It is situated approximately 25 kilometres east-southeast of the town of Barriere or 60 kilometres north-east of the city of Kamloops. The geographic coordinates are $51^{\circ} 08'$ North latitude by $119^{\circ} 47'$ West longitude; N.T.S. 82M / 4W.

Vehicular access is possible from Kamloops via either Highway 5 northward to Louis Creek, thence eastward to Skwaam Bay on Adams Lake; or eastward on Highway 1 to Squilax, then northward to Skwaam Bay. At Skwaam Bay, a well maintained logging haulage road (Adams West) leads northward along the western side of Adams Lake. The 3,000 logging road joins the Adams West road 8 kilometres north of Skwaam Bay. This seasonal gravel logging road leads northwesterly up the southern slopes of Samatosum Mountain and joins the 3,200 logging road which crosses the claim group. It is approximately 130 kilometres by road from Kamloops.

Physiography

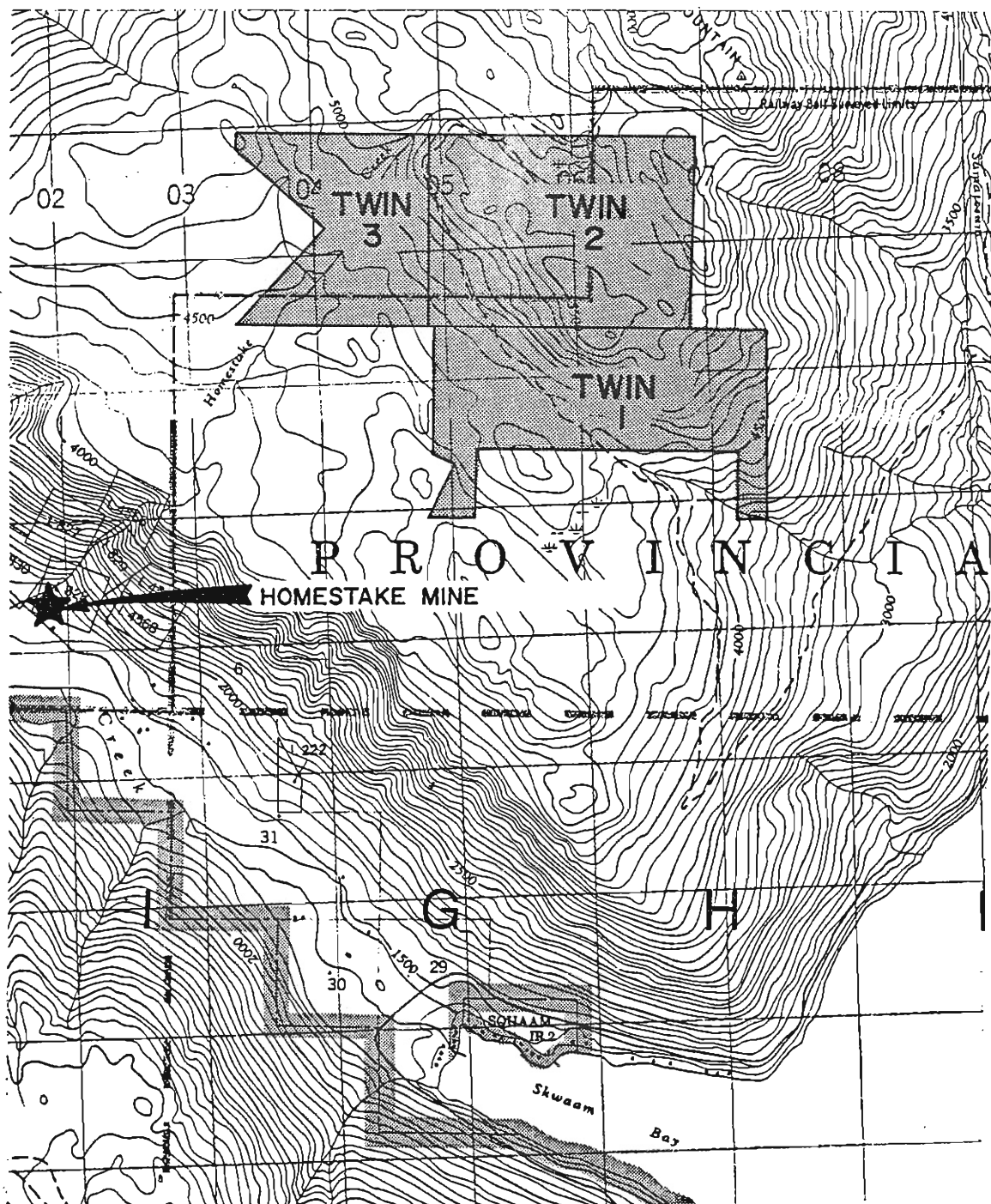
The claims cover the southwestern slopes of Samatosum Mountain within the Interior Plateau. Elevations within the claims range from 4,400 to 5,600 feet A.M.S.L. The climate is moderate with temperatures ranging from -25° C. to $+30^{\circ}$ C. Precipitation is usually moderate to heavy. The exploration season may extend from May to November.

Several areas within the property have been clear-cut logged; however, elsewhere there is a moderate to thick growth of pine, fir, cedar and aspen. The drainage pattern is either westward to Homestake Creek or southward to Adams Lake. Bedrock exposures are scarce except in areas of logging roadcuts or high relief.

Claim Ownership

The property is comprised of three M.G.S. mineral claims, totalling 39 units. The location and configuration of these claims are shown on Figure 2. The following table summarizes all pertinent claim data for the TWIN claim group (Notice of Grouping No. 1849, January 27, 1981).

Claim Name	Units	Record Number	Record Date	Expiry Year
TWIN 1	18	2403	Feb. 13/80	1988
TWIN 2	12	2404	Feb. 13/80	1988
TWIN 3	9	2405	Feb. 13/80	1988
	39 units			



J.D. Blanchflower



To accompany a report by J.D. Blanchflower.

After B.C.M.M. Claim Map 82M/4.

MCL

MINOREX CONSULTING LTD.
GEOLOGICAL CONSULTANTS, KAMLOOPS, B.C.

LINCOLN RESOURCES INC.
VANCOUVER, BRITISH COLUMBIA

CLAIM MAP
TWIN PROPERTY
KAMLOOPS MINING DIVISION, B.C.

DATE:	AUG. 18/86	SCALE:	1: 50,000
DWN. BY:	T.Q./T.	DWG. NO.:	2

All three TWIN mineral claims were staked by Mr. C. Graf of Vancouver, B.C. All interests in these claims were sold to Mr. John K. Ralfs of Vancouver, B.C. on March 5, 1981 (Bill of Sale No. 2494). On February 26, 1982, Mr. Ralfs sold all interest in these claims to Apex Energy Corp. (Bill of Sale No. 2595).

In late 1983, Austin Resources Inc. (Lincoln Resources Inc.) negotiated an option agreement with Apex Energy Corp.

On March 7, 1984, Corporation Falconbridge Copper acquired all interests in the property under the terms of a joint option agreement with Austin Resources Inc. (Lincoln Resources Inc.) and Apex Energy Corp. (Bill of Sale No. 2961). When this option agreement was terminated on April 11, 1985, Apex Energy Corp. re-acquired a 100% interest in the claims (Bill of Sale No. 3069). Apex Energy immediately assigned a 51% interest in the property to Lincoln Resources Inc. on April 11, 1985 (Bill of Sale No. 3070). Thus, the property is currently owned jointly by Lincoln Resources Inc. (51%) and Apex Energy Corp. (49%).

History

The Barriere Lakes - Adams Plateau region has received intermittent exploration interest since the 1920's. Early workers concentrated their efforts on exploring and developing several of the stratabound base-metal occurrences known throughout the region. One of these prospects is the 'Twin Mountain' silver-lead-zinc showing situated within the subject property.

The first documented work on this property is reported in the 1936 B.C. Minister of Mines Annual Report (p. D 39). Trenching traced a 'dolomite' zone for approximately 4,600 feet with an average width of 9 to 20 feet.

The 'dolomite' zone was reported to occur in rocks of quartz-sericite to greenstone schist composition. Galena, sphalerite, pyrite and chalcopyrite mineralization was reportedly hosted by both the 'dolomite' zone and 'quartz-lenses'. The government geologist reported results of six samples ranging from: trace to 0.50 oz./ton gold, trace to 5.0 oz./ton silver, nil to 36.50 % lead, and nil to 3.7 % zinc (B.C.M.M.A.R., 1936, p. D 39).

The property was optioned to Camoose Mines Limited by C.C. Keller of Louis Creek in 1952. A 7.5-mile access road was built from Skwaam Bay that fall; and in 1953, two exploration tunnels were driven, 330 and 440 feet. The western tunnel intersected a mineralized vein and it was drifted on for 100 feet northwesterly and 110 feet southeasterly.

The property was restaked in 1966 by C.C. Keller, as the 'Star', 'Max' and 'Hope' mineral claims, and optioned to Sinmax Mines Ltd. In 1967 and 1968, Sinmax Mines conducted a detailed exploration program which included: linecutting, geochemical and geophysical surveying, and some underground mapping and sampling

(Read, 1968). During the 1969 field season, Sinmax Mines prospected their claim holdings, excavated 15 trenches, and mapped the surface showings and underground workings. The results of this work discovered that the 'Twin Mountain' lead and zinc-bearing vein structure could be traced over a strike length of 4 miles, but the low silver and moderate lead and zinc values were erratically distributed within it (Dawson, 1969).

In 1980, Mr. C. Graf staked the TWIN 1 to 3 mineral claims to cover the 'Twin Mountain' silver-lead-zinc vein on the slopes of Samatosum Mountain, west of the mineral claims owned by Kamad Silver Co. Ltd. At that time, Kamad Silver was exploring and developing their Homestake Mine, located just 4 kilometres southwest of the Twin Mountain showing. In 1981 and 1982, Mr. Graf and his associates conducted geological, geochemical and geophysical surveying over the reported base metal showings.

In October, 1983, Rea Gold Corporation announced the discovery of gold-bearing massive sulphide mineralization on their adjoining AR and HN mineral claims. This announcement caused a staking rush in the region and prompted Austin Resources Inc. (Lincoln Resources Inc.) to negotiate an option agreement with Apex Energy Corp. A preliminary control grid was established and limited soil geochemical sampling was completed by December.

Corporation Falconbridge Copper (C.F.C.), the operator of the Rea (AR/HN) property, explored the TWIN mineral claims during the 1984 field season with: geological mapping (1:2,500), soil and rock geochemical sampling, geophysical surveying (VLF-EM and Max-Min II), and drilling (2 holes). After Corporation Falconbridge Copper terminated their option in April, 1985 Lincoln Resources Inc. conducted fill-in soil geochemical sampling.

GEOLOGIC SETTING

The Barriere Lakes - Adams Plateau region has been recently mapped by several government geologists. The most definitive geological reports include those by: T. Hoy and R. Goutier (1986), P.A. Schiarizza and V. Preto (1984), V. Preto and P.A. Schiarizza (1985), and G.P.E. White (1985). Much of the following text is based on the results of these recent works.

This region is underlain by a weakly to moderately metamorphosed assemblage of sedimentary and volcanic rocks belonging to the Late Devonian to Early Mississippian-age Eagle Bay Formation. The Eagle Bay Formation appears to stratigraphically overlie volcanic rocks of the Late Devonian Fennell Formation. These formations have been intruded by granodiorite orthogneiss to biotite quartz monzonite ranging in age from Late Devonian to Cretaceous. The strata and intrusions are locally overlain by olivine basalt flows of Pleistocene to Recent age.



Mr

REGIONAL GEOLOGY
TWIN PROPERTY
KAMLOOPS MINING DIVISION, B.C.

DWG. NO.:	3
-----------	---

A horizontal scale bar with alternating black and white segments. It is marked with '0' at the left end, '5000' in the middle, and '10,000 (meters)' at the right end.

LEGEND

UPPER TRIASSIC AND LOWER JURASSIC NICOLA GROUP (?)

UPPER TRIASSIC OR LOWER JURASSIC

Xjv AUGITE PORPHYRY BRECCIA

UPPER TRIASSIC

Xi DARK GREY LIMESTONE

DEVONIAN TO PERMIAN

ALLOCHTHONOUS INTERNALLY IMBRICATED OCEANIC ASSEMBLAGE

FENNELL FORMATION

UPPER STRUCTURAL DIVISION

uFb GREY AND GREEN PILLOWED AND MASSIVE METABASALT; MINOR AMOUNTS OF BASALTIC BRECCIA, TUFF, DIABASE, GABBRO, AND CHERT

uFc GREY AND GREEN BEDDED CHERT

LOWER STRUCTURAL DIVISION

IFc GREY AND GREEN BEDDED CHERT, CHERTY ARGILLITE, SLATE, AND PHYLLITE

IFb GREY AND GREEN PILLOWED AND MASSIVE METABASALT; MINOR AMOUNTS OF BASALTIC BRECCIA AND TUFF

IFg GABBRO, DIORITE, DIABASE

IFp LIGHT TO MEDIUM GREY QUARTZ-FELDSPAR PORPHYRY RHYOLITE

IFs LIGHT TO DARK GREY SANDSTONE, SILTSTONE, SLATE, PHYLLITE, AND QUARTZITE; MINOR AMOUNTS OF LIMESTONE AND CHERT; IN PLACES INCLUDES GREY TO GREEN QUARTZOSE AND FELDSPATHIC PHYLLITE (METATUFF)

IFcg INTRAFORMATIONAL CONGLOMERATE; CLASTS DERIVED EXCLUSIVELY FROM FENNELL FORMATION LITHOLOGIES

IFu UNDIVIDED; MAINLY IFc, IFg, and IFb, BUT MAY INCLUDE ANY OR ALL OF ABOVE ROCK TYPES

DEVONO-MISSISSIPPIAN AND OLDER PARAUTOCHTHONOUS ROCKS (EBU TO SDQ)

EAGLE BAY FORMATION (EBF TO EBG)

MISSISSIPPIAN

EBP DARK GREY PHYLLITE AND SLATE WITH INTERBEDDED SILTSTONE, SANDSTONE, AND GRIT; MINOR AMOUNTS OF CONGLOMERATE, LIMESTONE, AND METATUFF; **EBM**-LIMESTONE; **EBv**-METAVOLCANIC BRECCIA AND TUFF

DEVONIAN AND/OR MISSISSIPPIAN

EBF LIGHT TO MEDIUM GREY, RUSTY WEATHERING FELDSPATHIC PHYLLITE AND FRAGMENTAL PHYLLITE DERIVED FROM INTERMEDIATE TO FELSIC TUFF AND VOLCANIC BRECCIA; MINOR AMOUNTS OF DARK GREY PHYLLITE AND SILTSTONE; **EBFq**-LIGHT GREY MASSIVE "CHERTY QUARTZITE" (SILICEOUS EXHALITE?)

DEVONIAN

EBA LIGHT SILVERY GREY TO MEDIUM GREENISH GREY SERICITE-QUARTZ PHYLLITE AND SERICITE-CHLORITE-QUARTZ PHYLLITE DERIVED FROM FELSIC TO INTERMEDIATE VOLCANIC AND VOLCANICLASTIC ROCKS INCLUDING PYRITIC, FELDSPATHIC, AND COARSELY FRAGMENTAL VARIETIES; LESSER AMOUNTS OF DARK GREY PHYLLITE, SILTSTONE, AND GREEN CHLORITIC PHYLLITE; INCLUDES BIOTITE-FELDSPAR-QUARTZ SCHIST AND GNEISS, BIOTITE-QUARTZ HORNFELS AND AMPHIBOLITE ADJACENT TO BALDY BATHOLITH; **EBAI**-FELDSPAR PORPHYRY, FELDSPATHIC PHYLLITE, PYRITIC SERICITE-FELDSPAR-QUARTZ PHYLLITE, METAVOLCANIC BRECCIA; **EBAI**-SERICITIC QUARTZ-FELDSPATHIC SCHIST AND GNEISS DERIVED FROM FELSIC INTRUSIVE ROCKS; **EBAu**-UNDIVIDED EBA and EBAI

DEVONIAN (?) AND/OR OLDER (?) (UNITS EBU TO EBG)

EBU LIGHT TO DARK GREEN CHLORITIC PHYLLITE, DARK GREY PHYLLITE AND SILTSTONE, LIMESTONE, QUARTZITE

EBM GREY AND GREEN VESICULAR AND PILLOWED METABASALT, GREENSTONE, CHLORITE SCHIST; MINOR AMOUNTS OF BEDDED CHERT, SILICEOUS PHYLLITE AND FINE-GRAINED QUARTZITE

EBK Banded LIGHT GREY AND GREEN ACTINOLITE-QUARTZ SCHIST AND EPIDOITE-ACTINOLITE-QUARTZ ROCK; LESSER AMOUNTS OF GARNET-EPIDOITE SKARN, CHLORITIC SCHIST, AND SERICITE-QUARTZ SCHIST

DEVONIAN (?) AND/OR OLDER (?) (UNITS EBU TO EBG) (CONTINUED)

EBL CALCAREOUS BLACK PHYLLITE, DARK GREY LIMESTONE AND ARGILLACEOUS LIMESTONE

EBS GREY AND GREEN PHYLLITIC SANDSTONE AND GRIT, PHYLLITE, AND QUARTZITE; LESSER AMOUNTS OF LIMESTONE, DOLOSTONE, GREEN CHLORITIC PHYLLITE, SERICITE-QUARTZ PHYLLITE, AND FELDSPATHIC SERICITE-QUARTZ PHYLLITE; **EBSq**-LIGHT GREY TO WHITE QUARTZITE; **EBSc**-LIMESTONE, DOLOSTONE, MARBLE; **EBSb**-GREENSTONE, PILLOWED METABASALT, CHLORITIC PHYLLITE; **EBSg**-CONGLOMERATE; **EBSp**-GREY PHYLLITE AND SILTSTONE; **EBSi**-SIDERITE-SERICITE-QUARTZ PHYLLITE AND FELDSPATHIC PHYLLITE (METATUFF); **EBSa**-PYRITIC SERICITE-QUARTZ PHYLLITE AND CHLORITOID-SERICITE-QUARTZ PHYLLITE

EBG MEDIUM TO DARK GREEN CALCAREOUS CHLORITE SCHIST AND FRAGMENTAL SCHIST DERIVED LARGE-ly FROM MAFIC TO INTERMEDIATE VOLCANIC AND VOLCANICLASTIC ROCKS; LESSER AMOUNTS OF LIMESTONE AND DOLOSTONE; MINOR AMOUNTS OF QUARTZITE, GREY PHYLLITE, AND SERICITE-QUARTZ PHYLLITE; **EBGc**-LIMESTONE, DOLOSTONE, MARBLE; **EBGi**-TSHINAKIN LIMESTONE MEMBER-MASSIVE, LIGHT GREY FINELY CRYSTALLINE LIMESTONE AND DOLOSTONE; **EBGs**-DARK TO LIGHT GREY SILICEOUS AND/OR GRAPHITIC PHYLLITE, CALCAREOUS PHYLLITE, LIMESTONE, CALC-SILICATE, CHERTY QUARTZITE; MINOR AMOUNTS OF GREEN CHLORITIC PHYLLITE AND SERICITE-QUARTZ PHYLLITE; **EBGq**-LIGHT TO MEDIUM GREY QUARTZITE; **EBGo**-DARK GREY PHYLLITE, CALCAREOUS PHYLLITE AND LIMESTONE; MINOR AMOUNTS OF RUSTY WEATHERING CARBONATE-SERICITE-QUARTZ PHYLLITE (METATUFF?); **EBGg**-POLYMICTIC CONGLOMERATE

SPARKLE CREEK-DEADFALL CREEK SUCCESSION (SDQ)

LOWER CAMBRIAN (?) AND/OR HADRYNIAN (?)

SDQ LIGHT TO DARK GREY QUARTZITE, MICACEOUS QUARTZITE, GRIT, AND PHYLLITE; LESSER AMOUNTS OF CALCAREOUS PHYLLITE, CARBONATE, AND GREEN CHLORITIC SCHIST; NORTHEASTERN EXPOSURES INCLUDE STAUROLITE-GARNET-MICA SCHIST, CALC-SILICATE SCHIST, AND AMPHIBOLITE

TERTIARY OR QUATERNARY

Tb OLIVINE BASALT

MIOCENE OR PLOCENE

mTb PLATEAU LAVA: OLIVINE BASALT

Eocene

KAMLOOPS GROUP

eTs SKULL HILL FORMATION AND RELATED ROCKS; ANDOSITE AND BASALT; INCLUDES MINOR AMOUNTS OF MUOSTONE AND SHALE IN THE VICINITY OF ALEX AND HAGGARD CREEKS

eTc CHU CHUA FORMATION: SANDSTONE, SHALE, CONGLOMERATE, COAL

CRETACEOUS OR TERTIARY

qp QUARTZ-FELDSPAR PORPHYRY

BALDY BATHOLITH, RAFT BATHOLITH, AND RELATED ROCKS

Kg GRANITE AND GRANODIORITE

AGE UNKNOWN

di FOLIATED DIORITE, QUARTZ DIORITE, AND GABBRO

ub SERPENTINITE

LATE DEVONIAN

Dgn GRANITE AND GRANODIORITE ORTHOGNEISS; **Ognp**
INCLUDES SILLIMANITE-BEARING PARAGNEISS

SYMBOLS

GEOLOGICAL CONTACT: DEFINED, APPROXIMATE, ASSUMED	
BEDDING, TOP KNOWN: INCLINED, OVERTURNED	
BEDDING, TOP UNKNOWN: HORIZONTAL, INCLINED, VERTICAL	
FACING DIRECTION OF PILLOWED BASALT: INCLINED, OVERTURNED	
SYNMETAMORPHIC SLATY CLEAVAGE, SCHISTOSITY, OR GNEISSOSITY: HORIZONTAL, INCLINED, VERTICAL	
MINERAL LINEATION	
POSTMETAMORPHIC CRENUATION CLEAVAGE: INCLINED, VERTICAL	
CRENUATION LINEATION	
MESOSCOPIC FOLD AXIS: SYNMETAMORPHIC, POSTMETAMORPHIC, LATE KINK	
AXIAL TRACE OF SYNMETAMORPHIC FOLD: OVERTURNED ANTICLINE, OVERTURNED SYNCLINE: ESTABLISHED, INFERRED	
AXIAL TRACE OF POSTMETAMORPHIC FOLD: ANTIFORM, SYNFORM	
LATER (SYN OR POSTMETAMORPHISM) WEST TO SOUTHWESTERLY DIRECTED THRUST FAULT; TEETH ON UPPER PLATE: DEFINED, APPROXIMATE, ASSUMED	
EARLY (PRE FOLDING AND METAMORPHISM) EASTERLY DIRECTED THRUST FAULT; TEETH ON UPPER PLATE: DEFINED, APPROXIMATE, ASSUMED	
FAULT; DOT ON DOWNTHROWN SIDE, ARROWS INDICATE SENSE OF STRIKE SLIP MOVEMENT: DEFINED, APPROXIMATE, ASSUMED	
CONODONT FOSSIL LOCALITY: MISSISSIPPIAN, PENNSYLVANIAN, PERMIAN	
LOCATION OF RADIOMETRICALLY DATED SAMPLE (Pb/U ON ZIRCONS AND Rb/Sr WHOLE ROCK): INDICATE A DEVONIAN AGE FOR UNIT EBA AND FOR UNIT IFp	
MINERAL OCCURRENCE	
LIMIT OF GEOLOGICAL MAPPING OR OUTCROP	
LINE OF GEOLOGICAL CROSS-SECTION	
TOPOGRAPHICAL CONTOUR (200-METRE INTERVAL)	

MINERAL OCCURRENCES

MINERAL OCCURRENCES			Minfile				
				17	BROKEN RIDGE	Pb, Zn, Cu	82M-130
				18	HARPER	Cu, Pb, Zn	82M-60
1	REXSPAR	U, F	82M-21	19	EBL	Cu	82M-51
2	FOGHORN (CHIOGRINI)	Ag, Pb, Zn, Cu	82M-40	20	KAJUN (JUNE)	Ag, Pb, Zn, Cu	82M-58
3	LYDIA	Pb, Ag, Cu	82M-8	21	TWIN MOUNTAIN	Pb, Zn, Cu, Ag, Au, barite	82M-20
4	JUDY	Mo, Cu	92P-36	22	REA	Au, Ag, Pb, Zn, Cu	82M-191
5	WINDPASS	Au, Cu, Bi, Ag	92P-39	23	HOMESTAKE	Ag, Pb, Zn, Au, Cu, barite	82M-25
6	SWEET HOME	Au, Cu, Bi	92P-40	24	BECA (TOM)	Cu, Pb, Zn, Au, Ag	82M-55
7	GOLD HILL	Au, Pb, Cu, Zn, Ag	92P-41	25	JOE (GLEN)	Cu, Pb, Zn	82M-54
8	QUEEN BESS	Pb, Zn, Ag	92P-42	26	ELSIE	Pb, Zn, Ag, Au	82M-12
9	CC (CHU CHUA)	Cu, Zn	92P-140	27	LUCKY COON	Pb, Zn, Ag, Au, As	82M-12
10	ENARGITE	Pb, Zn	82M-65	28	KING TUT	Ag, Pb, Zn, Au	82M-13
11	FORTUNA 1	Pb	82M-72	29	SPAR	Pb, Au, Ag, Cu	82M-17
12	FORTUNA 2	Pb	82M-70	30	PET	Pb, Zn	82M-143
13	COPPER CLIFF	Pb, Zn, Cu	82M-67	31	MOSQUITO KING	Pb, Zn, Ag	82M-16
14	RAINBOW	Cu, Pb, Zn	82M-67	32	BC (CUSH)	Cu, Pb, Zn	82M-139
15	C-C	Cu, Pb, Zn	82M-67	33	SPARKS	Cu, Pb, Zn, Ag	82M-14

Structural features of the region include, at least, two periods of folding and faulting. An early period of folding, west to northwest trending with axes plunging north to northwest, has deformed the strata prior to later folding with fold axes plunging gently north.

There are numerous base-metal occurrences known throughout the region, many of which are stratabound massive sulphide deposits syngenetic with their host rocks. Such polymetallic deposits, commonly with associated barite and precious-metal values, are most abundant in the Birk Creek - North Barriere Lake, Johnson Lake - Sinmax Creek and Adams Plateau areas. See Figure 3 for a map of the regional geology and locations of the known mineral occurrences.

RESULTS OF PREVIOUS EXPLORATION WORK

Survey Control Grid

Over the last six years there have been four control grids established over portions of the property. The first control grid was established by Apex Energy Corp. over the 'Twin Mountain' showing and its strike extensions. Austin Resources Inc. (Lincoln Resources Inc.) established another survey grid over the northwestern portion of the property in 1983. A third control grid was later established at an orientation of 132° by Corporation Falconbridge Copper for their geological, geochemical and geophysical surveying during the 1984 field season. In 1985, Quest Canada Exploration Services Inc. did detailed surveying over a portion of the 1984 control grid, establishing 12.5 sample stations along 50-metre grid lines.

Geology

The property is underlain by volcanic and volcanoclastic units of the Late Devonian to Early Mississippian-age Eagle Bay Formation. The oldest units comprise a complex succession of mafic to felsic(?) volcanics and pyroclastics (Units 1 to 3) that lie at the structural top of the assemblage. The volcanic basement rocks are dominated by mafic flows and pyroclastics, including ash- to agglomerate-size tuffs. All lithologies have experienced regional greenschist metamorphism which has produced a strong penetrative foliation and widespread chloritization of the more mafic members. These units have been structurally inverted by a combination of isoclinal folding and repetitive faulting (Hoy and Goutier, 1986).

Three linear, dioritic to gabbroic intrusives have been mapped by Corporation Falconbridge personnel, at coordinates: L 72 N. by 3+50 E., L 72 N. by 12+00 E., and L 66 N. by 15+50 E.

The stratigraphy trends northwesterly and dips northeasterly. Bedding attitudes show that the lithologies dip from -44° to -60° northeastward.

Faults are common in this region, often parallel with or perpendicular to the schistosity. The northwesterly fractures in the vicinity of the old 'Twin Mountain' showing, at grid coordinates L 61 E. by 2+50 N., and the Homestake Creek fault are examples of each of the above fracture patterns.

The "Twin Mountain" silver-lead-zinc prospect is the only known mineralization. There are, however, the 'Silver' and 'Discovery' sulphide-bearing horizons on the adjacent Kamad and Rea properties that may trend through the claim group.

Geochemistry

Three soil geochemical surveys have been undertaken recently. These were carried out by: Austin Resources Inc. (Lincoln Resources Inc.) in 1983, Corporation Falconbridge Copper in 1984, and Quest Canada Exploration Services Inc. for Lincoln Resources Inc. and Apex Energy Corp. in 1985.

Austin Resources Inc. undertook a limited soil geochemical survey over the northcentral portion of the property. A total of 304 B-horizon soil samples was collected at 25-metre intervals along grid lines 130 metres apart. The control grid was orientated with a baseline at 115° and grid lines at 025° . Austin Resources analysed their samples for gold, silver, copper, lead and zinc.

Corporation Falconbridge Copper surveyed the northern half of the property. A total of 930 B-horizon soil samples was collected at 50-metre intervals along grid lines 100 metres apart. Selective soil sampling was also carried out over anomalous targets at 25-metre intervals. This survey extended from grid coordinates L 60 E. to L 79 E., inclusive. Their samples were analysed for gold, silver, copper, lead, zinc and arsenic.

Quest Canada Exploration Inc. contracted fill-in sampling at 12.5-metre intervals along grid lines L 60 E. to L 79 E., inclusive. Intermediate grid lines from L 59+50 E. to L 82+50 E. were established to give a sample density of 50 by 12.5 metres. A total of 1016 B-horizon soil samples was collected and analysed for gold, silver, copper, lead, zinc and arsenic.

Corporation Falconbridge Copper collected approximately 300 rock geochemical samples during their geological survey in 1984. These samples were analysed for copper, zinc, barium, sodium, calcium, magnesium, silica and titanium. The barium results have been plotted with those of the 1986 soil geochemical survey as Figure 11 of this report.

Geophysics

In 1984, Spirex Geoservices Ltd. (Quest Canada Exploration Services Inc.) conducted VLF-EM surveying on behalf of Corporation Falconbridge Copper. The survey covered an area from L 60 E. to L 79 E. and 6+50 N. to 29+90 N. (47 line-km.) along lines 100 metres apart with readings taken every 25 metres. A Geonics EM-16 VLF instrument was used for the survey to receive the Annapolis, Maryland (21.4 hz.) transmitter station.

Prior to drilling, Corporation Falconbridge Copper undertook a Max-Min II survey over a portion of the property. The data from this survey are not available, just the plotted axes of their conductors (C.F.C., 1984).

Diamond Drilling

Corporation Falconbridge Copper tested their survey results with diamond drilling in 1984. The first drill hole was collared near grid coordinates L 65 by 2+00 S., on the site of a very high gold-in-soil anomaly. This hole is not shown on any of the C.F.C. plans so it has not been plotted on the figures accompanying this report; however, it reportedly intersected a carbonitized zone with white quartz veining and fracture filling (Oliver, 1986). A second drill hole was collared to test the southeastern extension of the Discovery Zone. According to Mr. J. Oliver (1986), this hole did not intersect any economic mineralization.

1986 EXPLORATION PROGRAM

This program was supervised by Mr. D. Windsor and the writers. It included: relabelling a portion of the existing control grid (14.0 line-km.), establishment of additional survey control grid (15.15 line-km.), geological mapping at a scale of 1:2,500, soil and lithogeochemical sampling (361 soil and 63 rock samples), geophysical surveying (fixed source Genie electromagnetic, 17.75 line-km.), and trenching (300 metres). This work was carried out between October 16 and December 16, 1986. This report and its accompanying plans were prepared after all of the analytical and statistical data were received and plotted.

Amex Exploration Services Ltd. of Kamloops, B.C. was contracted to relabel a portion of the existing survey control grid and establish additional survey control grid. The writer and Mr. D. Windsor, an experienced and qualified geotechnologist / geophysical operator, mapped the western portion of the property which had not yet been surveyed. Mr. Neil Martin, an experienced geological/geochemical assistant employed by Minorex Consulting Ltd., collected the soil geochemical samples under the supervision of Mr. Windsor and the writer. Messrs. Windsor and Martin

carried out the geophysical survey under the supervision of Mr. Z. Doborzynski. The trenching program was undertaken under the supervision of Mr. Windsor and the report writers.

The Statements of Qualifications for Mr. Windsor and the writers accompany this report.

Survey Control Grid

The control grids that were established by Corporation Falconbridge Copper in 1984 and Spirex Geoservices Ltd. in 1985 required relabelling, particularly in areas of recent clearcut logging. In addition, these grids had to be extended to cover the western and southwestern portions of the property. Field personnel of Amex Exploration Services Ltd. were contracted to carry out this work.

The existing control grid was reflagged, reblazed and relabelled with metal station labels at 25-metre intervals. The grid lines were 'brushed out' and cleared during this work for later geophysical surveying. In total, 14.0 line-kilometres of existing grid were re-established.

Additional control grid was established between the existing grid and the western boundary of the property. This control grid was established at an orientation of 225° with a line spacing of 100 metres and station interval of 25 metres. In total, 15.15 line-kilometres of control grid were established.

Geological Survey

The geology of this property was mapped in detail by Corporation Falconbridge Copper personnel in 1984. However, this surveying did not extend to the extreme western and southwestern portions of the claim group. Soil geochemical and geophysical surveying since then have shown that the two sulphide-bearing horizons, known as the 'Rea' and 'Silver' Zones, probably underlie the western portion of the property; thus, geological surveying was extended to cover this area.

Mr. D. Windsor and the writer undertook the geological survey. Figure 4 of this report is a compilation of previous geological data (C.F.C., 1984) and the results of the 1986 survey.

Geochemical Surveys

Soil Geochemical Survey

Soil geochemical samples were collected using a grub hoe. Survey notes on the sample character (i.e. active, dry, or swamp), texture (i.e. organic, clay, silt, sand, or gravel), origin (i.e. residual, colluvial, alluvial, or glacial), horizon,

depth, colour, and location were taken at each sample location. From these notes, the soil geochemical samples were dominantly a mixture of clay, silt and sand from the residual, alluvial and glacial overburden. The 'B' soil horizon was sought for the survey, usually 5 to 10 centimetres beneath the surface to minimize any organic matter.

The samples were placed in kraft paper envelopes, field dried, and delivered for analysis to Acme Analytical Laboratories Ltd. in Vancouver, B.C. A total of 361 soil samples were collected by Mr. N. Martin during a 5.5-day period.

At Acme Analytical Laboratories Ltd. the samples were dried at 60° C. and sieved to -80 mesh. All samples were analysed for 31 elements, including: molybdenum, copper, lead, zinc, silver, nickel, cobalt, manganese, iron, arsenic, uranium, thorium, strontium, cadmium, antimony, bismuth, vanadium, calcium, phosphorus, lanthanum, chromium, magnesium, barium, titanium, boron, aluminum, sodium, potassium, tungsten and gold. The first 30 elements were analysed by inductively coupled argon plasma (ICP) methods. The gold analyses were carried out using conventional atomic absorption methods. All analyses were conducted under the supervision of professional assayers.

At the writer's request Acme Analytical Laboratories Ltd. undertook a statistical analysis of the results using a microcomputer and a conventional statistical software programme. Mean, standard deviation and frequency percent data were calculated for copper, lead, zinc, silver, arsenic, strontium, nickel, cobalt, barium and gold.

Lithogeochemical Survey

The lithogeochemical samples were collected by the Mr. D. Windsor during the geological survey and later trenching program. All samples were properly described, labelled and delivered for analysis to Acme Analytical Laboratories Ltd. in Vancouver, B.C. A total of 63 samples were analysed, 8 surface and 55 trench samples.

At Acme Analytical Laboratories Ltd. the samples were ground to -100 mesh, and a 0.500 and 10 gram fraction of each were digested for either ICP or atomic absorption analysis, respectively. The surface samples were analysed for 31 elements, including: molybdenum, copper, lead, zinc, silver, nickel, cobalt, manganese, iron, arsenic, uranium, thorium, strontium, cadmium, antimony, bismuth, vanadium, calcium, phosphorus, lanthanum, chromium, magnesium, barium, titanium, boron, aluminum, sodium, potassium, tungsten and gold. The first 30 elements were analysed by inductively coupled argon plasma (ICP) methods. The gold analyses were carried out using conventional atomic absorption methods. All analyses were conducted under the supervision of professional assayers.

At the writer's request Acme Analytical Laboratories Ltd. undertook a statistical analysis of the results using a microcomputer and a conventional statistical software programme. Mean, standard deviation and frequency percent data were calculated for copper, lead, zinc, silver, arsenic, strontium, nickel, cobalt, barium and gold.

Geophysical Survey

Fixed Source Genie Electromagnetic Survey

A fixed source Genie electromagnetic survey was carried out by Messrs. D. Windsor and N. Martin under the supervision of Mr. Z. Doborzynski, a highly qualified geophysicist employed by ESSO Minerals Canada. It was undertaken during and shortly after the geological and geochemical surveys.

All aspects of this survey are thoroughly discussed in the 'Geophysical Report on the TWIN Property', Appendix I of this report. Appendix II contains the electromagnetic data and computer generated profiles. Figures 12 to 15 document the results of this survey work, and Figure 17 correlates the results of the geophysical survey with those of the geological and geochemical surveys.

Trenching Program

On December 9th, Holdings Lumber Company of Chase was contracted to clear the access roads of snow, and a Caterpillar 225 excavator was contracted from Brentwood Enterprises Ltd. of Kamloops to carry out the trenching work. Eleven individual trenches at seven locations were excavated, mapped, sampled and surveyed. A total of 300 metres of trenching was completed from December 12th to 16th.

RESULTS OF THE 1986 EXPLORATION PROGRAM

The results of the geological, soil geochemical and geophysical surveys are very encouraging; however, the lithogeochemical results are generally quite low. Nevertheless, the field work did show that the geology is considerably more complex than previously thought, and that there is still potential for discovering volcanogenic massive sulphide mineralization.

Geological Survey

The results of the 1986 and 1984 geological surveys accompany this report as Figure 4. This plan is a compilation of the

detailed mapping results reported by Corporation Falconbridge Copper (1984), and those from the work undertaken by Messrs. D. Windsor and J. D. Blanchflower during 1986. The stratigraphic and lithologic correlations established by Corporation Falconbridge Copper personnel have been retained for the purposes of this report.

1) Lithology

The claims are dominantly underlain by volcanic and volcanoclastic units of the Late Devonian to Early Mississippian-age Eagle Bay Formation. The oldest units comprise a complex succession of mafic to intermediate or felsic(?) volcanics and pyroclastics (Units 1 to 3) that lie at the structural top of the assemblage. The volcanic basement rocks are dominated by mafic flows and pyroclastics, including ash- to agglomerate-size tuffs. These rocks are locally pyritized with fine-grained disseminations and veinlets. More massive 'greenstone' units are probably original mafic flows.

Three linear intrusive bodies (Units 4.1 and 4.2) have been mapped by Corporation Falconbridge personnel, at grid coordinates: L 72 N. by 3+50 E., L 72 N. by 12+00 E., and L 66 N. by 15+50 E. These intrusives are of dioritic to gabbroic composition. It is not known whether these intrusions reflect synvolcanic intrusive centres, or if they were emplaced along zones of structural weakness during or after regional metamorphism. Many of the small basic stocks in the area have discordant contacts, unaltered compositions and lack metamorphic fabric.

A sequence of fine- to coarse-grained sedimentary rocks (Unit 6) is the youngest unit within the property. It comprises laminated carbonaceous argillite, siltstone, grit and wacke, and poorly sorted conglomerate with both sedimentary and volcanic clasts. Graded bedding is common.

The lithologic units have been described and correlated stratigraphically, in order of decreasing age, as follows.

LATE DEVONIAN TO EARLY MISSISSIPPIAN

EAGLE BAY FORMATION

1 Mafic Volcanics -

1.1 Mafic Flow - medium to dark green, massive homogeneous mafic flow, poorly bedded but quite schistose. Locally altered to epidote, chlorite, quartz, magnetite and iron-rich carbonates near fault and shear zones which have been infilled by quartz, calcite (+/- pyrite). Pyritized with fine-grained disseminations and microveinlets.

1.2 Pillowed Flow and Breccia - like the mafic flows in

outcrop. Vague primary structures indicating rapid cooling in a submarine environment. Breccia fragments are usually monolithic, subangular and poorly sorted.

- 1.3 Mafic Ash Tuff - slightly finer-grained equivalent of Unit 1.4.
- 1.4 Mafic Lapilli Tuff - medium to dark green, schistose lapilli pyroclastic. Lapilli fragments are usually elongate. Locally altered to epidote, chlorite, quartz, magnetite and iron-rich carbonates near fault and shear zones which have been infilled by quartz, calcite (+/- pyrite). Pyritized with fine-grained disseminations and micro-veinlets.
- 1.5 Agglomerate - similar in outcrop to Unit 1.2, except displays sedimentary features. Clasts range from 1 to more than 64 centimetres.
- 1.6 Mafic Tuff Breccia - similar to Units 1.3 and 1.4 with primary depositional breccia features.
- 1.7 Laharic (Debris) Flow - medium to dark green, poorly sorted and poorly bedded synvolcanic unit.

2 Intermediate Volcanics -

- 2.1 Intermediate Flow - fine-grained dacitic volcanic flow. Quartz eyes are less than 3 percent of volume. Massive, light to medium green, schist.
- 2.2 to 2.7 - Intermediate equivalents of Units 1.2 to 1.7.

3 Felsic Volcanics -

- 3.1 Felsic Flow - light grey to green, quartz-rich flow. Quartz eyes greater than 5 percent of volume.
- 3.2 to 3.7 - felsic equivalents of Units 1.2 to 1.7. Quartz-feldspar segregations are common.

4 Mafic Intrusions -

- 4.1 to 4.3 Diorite, Gabbro and Diabase - weakly foliated and altered intrusives with rare to less than 3 percent quartz crystals. Appear to be syn- or post-volcanic features; although, they often have disconformable contacts and appear quite fresh.

5 Felsic Intrusions -

- 5.1 Quartz-Feldspar Porphyry - small, quartz and plagioclase-rich intrusions which may post-volcanic or post-metamorphic features.

6 Sediments -

- 6.1 Chert, Ribbon Chert and Chert Breccia - relatively unaltered, grey to black, massive and poorly bedded chert often contains less than 3 percent sulphides. Chert breccias are related to tectonic versus depositional processes.
- 6.2 Chert Argillite - pale buff to grey chert with less than 1 cm. thick argillaceous interbeds. May have graphitic partings.
- 6.3 Quartzitic Argillite (Wacke) - well sorted, fine- to medium-grained quartz-rich sediments and grits with graphitic partings. Distinctive blue-grey quartz grains.
- 6.4 Quartz Pebble Conglomerate (Heterolithic Wacke) - poorly sorted, medium- to coarse-grained sediment. Distinctive talcose mudchips, chert pebbles, argillite fragments, quartz pebbles and minor volcanic clasts contained within a dark grey, fine-grained matrix.
- 6.5 Argillite - Phyllite - uniform, very fine- to fine-grained, black clastic. Often very graphitic with 1mm. to 1cm. carbonaceous partings.
- 6.6 Limestone - light to dark grey, massive limestone.
- 6.7 Greywacke - similar to Unit 6.3.
- 6.8 Limestone Cobble Breccia - a sedimentary or tectonic breccia with limestone cobble-size clasts.
- 6.9 Coarse Wacke - coarser-grained equivalent of Units 6.3 and 6.7.
- 6.0 Multilithic Pebble Conglomerate - similar to Unit 6.4.

2) Structure

The stratigraphy trends northwesterly and dips northeasterly. Bedding attitudes show that the lithologies dip from -44° to -60° northeastward. These attitudes are consistent with the stratigraphy of the Rea property. According to Hoy and Goutier (1986), the volcanic succession has been structurally overturned.

Faults are common in this region, often parallel to and crosscutting the schistosity. There seems to be a number of northwesterly fractures in the vicinity of the old 'Twin Mountain' showing at grid coordinates L 61 E. by 2+50 N.

Recent mapping and trenching results show several northwesterly trending fault and shear structures paralleling the stratigraphy. The siliceous and pyritized zones at grid coordinates L 62 E. by 4+00 S. and L 57 E. by 5+50 S. appear to have infilled syn-metamorphic fault structures. Other shear structures are obviously much younger, lithologically-controlled features.

3) Alteration

All lithologies have experienced regional greenschist metamorphism which has produced a strong penetrative foliation and widespread chloritization of the more mafic members. The principle hydrothermal alteration assemblages are characterized by:

- 1) carbonitization - generally as small ovoids within the mafic matrix to complete carbonitization (80% dolomite, iron-rich magnesite, and/or calcite) of the mafic rocks;
- 2) pyritization - as disseminations, veinlets, and discontinuous streaks parallel to foliation, increases from 1 to 10%;
- 3) sericitization - produces weak to moderate compositional layering with pyrite-rich sections; and
- 4) silicification - introduction is most frequent as lamellae, 1 to 4 cm. in thickness, parallel to foliation.

4) Mineralization

The lithogeochemical results from the geological survey and trenching program are generally quite low. Except for local zones of silicification with associated pyritization and minor galena, sphalerite, chalcopyrite and magnetite mineralization, no significant zones of sulphide mineralization were discovered.

Pyrite mineralization, with or without associated minor galena, sphalerite and chalcopyrite, occurs locally within the metamorphosed mafic volcanics and volcanoclastics. Fine-grained disseminations and/or microveinlets often occur in or near zones of more intense shearing with associated silicification, sericitization and epidote, chlorite, carbonate and mariposite alteration envelopes.

Magnetite disseminations occur locally, often associated with mafic flows and flow breccias. It also occurs as an alteration product within structurally-controlled zones of higher-grade propylitic alteration.

The fine-grained, graphitic sediments host abundant diagenetic, euhedral to subhedral pyrite disseminations. Pyrite mineralization may locally exceed 10 to 12 percent of the rock volume.

Geochemical Surveys

Soil Geochemical Survey

The soil geochemical results accompany this report as Appendix III, and Appendix V contains the statistical data. Figures 5 to 11 show the plotted and contoured gold-, silver-, copper-, lead-, zinc-, arsenic- and barium-in-soil results.

The writer has plotted both the 1986 results and those of the 1984 and 1985 soil geochemical surveys to present a compilation of the property's soil geochemistry. The statistical data for ten elements is summarized in the following table.

Element	Minimum Value(ppm)	Maximum Value(ppm)	Mean (ppm)	Standard Deviation
Gold	1.0*	320.0*	6.0*	24.0
Silver	0.1	2.6	0.4	0.4
Copper	1.0	173.0	38.0	31.0
Lead	2.0	2,091.0	42.0	114.0
Zinc	22.0	569.0	124.0	70.0
Strontium	4.0	298.0	24.0	27.0
Arsenic	2.0	250.0	23.0	26.0
Cobalt	1.0	52.0	14.0	8.0
Nickel	3.0	247.0	51.0	36.0
Barium	22.0	528.0	142.0	72.0

Total number of samples: 361 * parts per billion (p.p.b.)

These soil geochemical results have been correlated with the geological and geophysical results as Figure 17. The following observations are evident from the gold-, silver-, copper-, lead-, zinc-, arsenic-, and barium-in-soil results(see Figures 5 to 11).

1. Gold

The various soil geochemical surveys have identified several local gold-in-soil anomalies (greater than or equal to 50 p.p.b.). Most of the anomalous results occur only at single sites; however, there is a four-site anomaly at grid coordinates L 64 to 65 East by 1+75 to 2+50 South. This anomaly overlies the area which Corporation Falconbridge Copper tested with their first 1984 diamond drill hole.

The most important feature of the gold-in-soil results is the apparent trend of the single-site anomalies. One can see

that, aside from those located within seasonal drainages, the anomalies closely parallel the stratigraphic trend. This feature may be fortuitous if the glacial movement was solely southeastward or northwestward; however, the results also seem to be spatially and, possibly, genetically related to locally altered and pyritized mafic flows and pyroclastics.

It should be noted that most of the high gold-in-soil results occur along a ridge which trends northwesterly from L 60+00 East by 2+50 South to L 83+00 East by 1+00 North. Along this ridge, the overburden depth is minimal; thus, the gold geochemical results appear to be more continuous than those located in areas of deep overburden.

2. Silver

The silver-in-soil anomalies (greater than or equal to 2.5 p.p.m.) occur along two relatively distinct trends - L 61+00 East by 1+75 South to L 81+00 East by 0+75 North, and L 61+00 East by 2+50 North to L 64+00 East by 2+50 North. The former trend correlates well with the trend of the gold- and arsenic-in-soil anomalies, termed the 'Ridge' trend. The latter trend, termed the 'Twin Mountain' trend, lies within a very large, northwesterly lead- and zinc-in-soil anomaly which reflects the surface trace and workings of the 'Twin Mountain' lead-zinc-silver prospect (see History section).

The anomalous silver results, like those of gold, seem to reflect a close spatial relationship with the more intensely altered and pyritized mafic volcanics and volcaniclastics. There is only one single-site silver anomaly southwest of the main access road, an area of deep overburden and poor drainage. One might have expected that the silver-in-soil results would have reflected a more southwesterly dispersion pattern, given the solubility of silver.

3. Copper

The copper-in-soil anomalies (greater than or equal to 150 p.p.m.) seem to have a similar distribution as silver, but copper appears to be more widely dispersed between the 'Twin Mountain' and 'Ridge' trends. The wider dispersion pattern appears to be related to the southwesterly drainage pattern from the 'Twin Mountain' structure.

It is interesting to note that there is an apparent peripheral dispersion pattern southwest and northeast of the 'Twin Mountain' structure, and that there is a local copper-in-soil anomaly over the dioritic intrusion at grid coordinates L 72+00 East by 4+00 North. The anomalous copper soil geochemistry along this trend may be related to contact metamorphism or remobilized copper mineralization genetically

associated with the structurally controlled syn- or post-volcanic intrusions.

There are no copper-in-soil anomalies southwest of the main access road which, like silver, would be a likely dispersion area for water-soluble copper ions.

4. Lead

The lead-in-soil anomalies (greater than or equal to 200 p.p.m.) indicate three zones of mineralization. The first and largest anomaly overlies the 'Twin Mountain' structure, discussed above. The second anomalous trend coincides with the 'Ridge' zone, reflected by high gold, silver, copper and arsenic soil geochemistry. The third anomalous trend occurs between grid coordinates L 78+00 East by 2+50 South to L 82+00 East by 1+50 South. It is located in the extreme northwestern corner of the property, an area of relatively deep overburden and poor bedrock exposure.

The results of the trenching program, discussed in the following text, indicate that the northwestern corner of the property is underlain by a major stratigraphic contact between the dominantly volcanic sequence, which underlies most of the claim group, and a younger fine-grained sedimentary succession. The high lead-in-soil results in this area seem to be reflecting this lithologic contact and/or possible sulphide mineralization deposited along this contact. If this is the case, then it is interesting to note that the anomalous lead values occur with other anomalous arsenic, gold and zinc soil values.

5. Zinc

There are two, very large zinc-in-soil anomalies (greater than or equal to 500 p.p.m.) overlying the strike of the 'Twin Mountain' structure. Within the larger, more dispersed zinc anomalies, there are several lead, silver and minor copper soil anomalies. The other zinc soil anomalies are very local, commonly near or in seasonal drainages.

Along the 'Ridge' trend there are several single-site anomalies with coincident high lead, silver, and/or copper soil geochemistry.

6. Arsenic

The arsenic-in-soil geochemistry is very interesting, especially with regard to further exploration. The anomalous arsenic soil values (greater than or equal to 100 p.p.m.) occur dominantly in the northwestern portion of the claim group, southwest of the baseline and northwest of Homestake

Creek. It is in this area that trenching exposed the fine-grained epiclastic sedimentary sequence of rocks overlying the mafic volcanic units.

It is very interesting to note that the anomalous arsenic soil values, from L 83+00 East by 1+00 South to L 76+00 East by 1+50 South, terminate at Homestake Creek. The drainage course of this creek appears to be reflecting a major northeasterly trending fault. If this is the case, then the stratigraphic contact between the mafic volcanic and sedimentary rocks may be offset by right lateral movement along the Homestake Creek fault.

7. Barium

It is very difficult to comment on the anomalous barium-in-soil values (greater than or equal to 300 p.p.m.) since only the 1986 soil samples were analysed for barium. The previous work by Corporation Falconbridge Copper analysed lithogeochemical samples; thus, there are two different sample populations. Nevertheless, it appears from the 1986 sampling that the anomalous barium values are underlain by highly fractured, altered and pyritized zones within the mafic volcanic rocks (Units 1.1 and 1.4).

Lithogeochemical Survey

During the geological survey, seventy hand specimens of the mapped outcrops were collected. Of these specimens, eight were submitted for lithogeochemical analysis (8614-1 to 8). During the later trenching program, fifty-five lithogeochemical samples were collected from the exposed bedrock.

The lithogeochemical results accompany this report as Appendix IV, and Appendix VI contains the statistical data. Figures 4 and 16 show the sample locations and analytical results. Appendix VII contains the lithogeochemical sample descriptions.

The highest metal values from all of the lithogeochemical samples were: 260 p.p.b. gold, 2.8 p.p.m. silver, 316 p.p.m. copper, 4,567 p.p.m. lead and 7,252 p.p.m. zinc. It is obvious from these results that no economic mineralization was discovered.

Geophysical Survey

Fixed Source Genie Electromagnetic Survey

All aspects of this survey are thoroughly discussed in the 'Geophysical Report on the TWIN Property', Appendix I of this report. Appendix II contains the electromagnetic data and computer generated profiles. Figures 12 to 15, and 17 document the results of this survey work.

Trenching Program

Figure 16 of this report shows the location, shape and size of each trench. The geological and lithogeochemical results for this work are also shown on this plan. Figure 17 shows the locations of the trenches with respect to other geological, geochemical and geophysical results. Lithogeochemical sample descriptions appear in Appendix VII.

The location, dimensions and geology of the individual trenches are discussed in the following text.

Trench 1 - L 78+00 East by 1+50 to 1+78 South

This trench is 28 metres long with an overburden depth of 1 to 3 metres. It was excavated to test a coincident horizontal loop electromagnetic and gold-in-soil geochemical anomaly. The bedrock is light green, well foliated, mafic lapilli tuff with numerous quartz-carbonate veinlets and stringers hosting local and minor galena and hematite mineralization. Pyrite is ubiquitous, as fine-grained disseminations representing 1 to 7 percent of the rock volume.

Lithogeochemical results (samples 8614-21 to 37) were of low to background levels, except sample 8614-24 which returned 492 p.p.m. lead.

Trench 2 - L 78+80 East by 2+50 to 2+68 South and 2+75 to 2+87.5 South

Three individual trenches were excavated at this site (see Figures 16 and 17). The most northern trench did not reach bedrock and was abandoned after 5 metres in length. The second trench, between 2+50 to 2+68 South, was then excavated near the access road to expose the lithology without disturbing the nearby forest cover. The third trench at this site was dug south of the access road.

From 2+50 to 2+68 South, medium green, poorly altered lapilli tuffs underlie the overburden. No significant mineralization was observed.

The third trench, from 2+75 to 2+87.5 South, exposed a one-metre wide fault zone with altered, mylonitic material. Light brown, 'muddy' tuffs (i.e. argillaceous tuff) occur on both sides of the structure. These tuffs host local quartz veins measuring up to 0.3 m. wide with associated local pyrite disseminations (less than or equal to 2 %) and malachite. Lapilli tuff occurs in stratigraphic contact with the 'muddy' tuff unit halfway along the third trench, at approximately 2+81 South. The lapilli tuff hosts quartz fracture fillings, up to 7 cm. wide, with associated pyrite disseminations and minor malachite. Argillite with intercalated tuffaceous beds occurs at the southern end of the third trench at 2+85 South. None of the lithogeochemical samples (8614-14 to 20) returned values of economic interest.

Trench 3 - L 71+00 East by 3+40 to 3+70 South

This trench was excavated for 30 metres with an overburden depth of 1 to 3 metres. It was sited to test an alteration zone in mafic volcanics with an electromagnetic response.

From 3+40 to 3+53 South, the trench exposed light green to brown, silicified mafic tuff hosting 2 to 5 percent pyrite disseminations. An ankeritic alteration zone was exposed from 3+53 to 3+70 South. This zone has local mariposite alteration with the more silicic and pyritic sections.

All lithogeochemical samples (8614-57 to 60) returned low to background metal values.

Trench 4 - L 67+00 East by 3+39 to 3+53 South and 3+74 to 4+06 South

Two individual trenches were excavated at this site for a total length of 46 metres. They were dug to test a barium-in-soil anomaly on strike with a mapped alteration zone.

The first trench, from 3+39 to 3+53 South, exposed pale green, poorly altered mafic lapilli tuff. The tuff becomes more chloritic southward.

The second trench, from 3+85 to 4+06 South, exposed mafic volcaniclastics with abundant mariposite, and pyrite disseminations.

Lithogeochemical samples (8614-38 to 55) returned generally low values, except sample 8614-40 located midway along the second trench. This sample returned values of 2.8 p.p.m. silver, 13 p.p.b. gold, 316 p.p.m. copper, 4,567 p.p.m. lead and 7,552 p.p.m. zinc.

Trench 5 - L 65+00 East by 2+43 to 3+06 South and 3+42 to 3+52 South

Two trenches were excavated at this site to test a multi-element soil geochemical anomaly. Silicified and pyritized lapilli tuff was exposed from 2+46 to 2+55 South.

The second trench, from 3+42 to 3+52 South, exposed 6 metres of pale green, fine-grained mafic flow. This rock is pyritized and altered with abundant carbonate and mariposite.

Lithogeochemical samples (8614-9 to 13) returned quite low values in all metals.

Trench 6 - L 80+00 East by 2+31 to 2+89 South and 3+14 to 3+22 South

Two trenches were excavated at this site to test a fixed source Genie electromagnetic anomaly. The northern trench, from

2+31 to 2+89 South, exposed the stratigraphic contact between the dominantly volcanic and epiclastic sedimentary sequences. There is a one-metre fault zone between the two major units which appears to correlate well with the fault encountered in Trench 2.

The northern trench exposed altered mafic tuffs from 2+31 to 2+69 South, then there is an 8-metre section of deep overburden. On the other side of the overburden, 'muddy' or argillaceous tuff occurs in conformable contact with graphitic argillite, immediately north of the fault zone. A mineralized zone could exist in the section where the deep overburden was encountered since it is at the correct stratigraphic position for the deposition of syngenetic sulphide mineralization.

A test pit was excavated south of the first trench, from 3+14 to 3+22 South. This pit exposed finely-laminated, dark grey to black argillite at a depth of 5 metres. The foliation attitude of the argillite is 155° by -52° northeastward.

None of the lithogeochemical samples (8614- 26 to 31, and 46 and 47) returned any values of interest.

Trench 7 - L 81+00 East by 2+85 to 2+95 South

This trench was excavated for 10 metres in overburden of 7 to 8 metres deep. It was dug to test for the strike extensions of the volcanic-sedimentary contact encountered at Trenches 2 and 6. Graphitic argillite was exposed and sampled. The two lithogeochemical samples (8614-32 and 33) did not return any values of significance.

DISCUSSION OF EXPLORATION RESULTS

Geology

Geological survey results show that the southern portion of the property is dominantly underlain by older mafic volcanic and volcanoclastic rocks of the Eagle Bay Formation. These rocks are repetitively bedded as a rather thick volcanic pile with no obvious hiatuses in volcanism. Such a setting is indicative of an ancient volcanic seamount deposited during a period of relatively rapid and continuous volcanism with few, if any, periods of quiescence, sedimentation or sulphide deposition.

Trenching in the northwestern portion of the property exposed graphitic argillites with intercalated very fine-grained epiclastic sediments and tuffaceous laminae. These thinly-bedded sediments, although commonly in fault contact, appear to conformably overlie the lapilli tuffs and argillaceous 'muddy' tuffs of the volcanic sequence.

The local stratigraphy appears to be changing along strike, in a northwesterly direction, from a dominantly volcanic sequence to one of a volcanic succession conformably overlain by exhalative and epiclastic sedimentary rocks. If this is the case, then the most favourable setting for syngenetic massive sulphide deposition would be in the northwestern corner of the claim group.

Geochemistry

Soil Geochemistry

The soil geochemical results, combined with those of previous exploration programs, indicate three dominant geochemical trends.

The first trend, from L 60+00 East by 3+00 North to L 73+00 East by 2+00 North, reflects the known mineralization at the 'Twin Mountain' lead-zinc-silver prospect. This prospect has been discussed thoroughly in the History section of this report.

The second trend, along a ridge from L 60+00 East by 2+50 South to L 83+00 East by 1+00 South, has a very strong silver, gold and copper response. This 'Ridge' zone is underlain by mafic volcanic and volcanoclastic rocks which host local structurally controlled alteration zones. These alteration zones are silicified, pyritized and sparingly mineralized with chalcopyrite, galena, sphalerite, magnetite and hematite. Lithogeochemical results from samples taken along this zone returned rather low precious- and base-metal values.

The third trend, from L 83+00 East by 1+00 South to L 76+00 East by 1+50 South, is reflected by anomalous arsenic, gold and lead soil geochemistry. This trend overlies the stratigraphic contact between the major volcanic and sedimentary units. It appears to be truncated by an apparent northeasterly trending fault zone along the Homestake Creek drainage.

Lithogeochemistry

The highest gold lithogeochemical result was obtained from Sample 8614-6, located at grid coordinates 57+50 East by 0+35 South. This sample was collected from a silicified and pyritized zone in a mafic volcanic flow. This rock is locally well fractured and veined with quartz, calcite and pyrite.

The highest silver (2.8 p.p.m.), copper (316 p.p.m.), lead (4,567 p.p.m.), and zinc (7,252 p.p.m.) values were returned from Sample 8614-40, located in trench 4 at grid coordinates L 67+00 by 4+90 South. The host rock of this mineralization is highly altered mafic flow and lapilli tuff with pyrite, galena, malachite and chalcopyrite mineralization associated with quartz, calcite and mariposite fracture fillings.

Geophysics

The results of the interpreted geophysical survey data indicate ten electromagnetic conductors with weak to relatively high responses. All of these conductors trend northwestward, paralleling the stratigraphy.

Five conductors appear to be reflecting lithologic changes (e.g. Conductors 'C', 'E', 'F', 'G' and 'J') and one conductor appears to be reflecting the stratigraphic contact between the volcanic and sedimentary units (e.g. Conductor 'D').

The three most interesting conductors include: Conductor 'A', which is probably responding to underlying carbonaceous sedimentary rocks, although, it does occur in an area through which the 'Discovery' horizon is inferred to occur; Conductor 'H', which is very interesting in that it overlies a mapped dioritic intrusion with abundant pyritization and local copper soil geochemistry; and Conductor 'I', which reflects the 'Twin Mountain' silver-lead-zinc mineralization and was the best conductor of the survey.

EXPLORATION POTENTIAL

The exploration potential of this property is still quite good. Recent exploration has shown that in the northwestern corner of the property the mafic volcanic sequence is overlain by fine-grained marine sediments, indicating a period of sedimentation and possible syngenetic sulphide deposition. This stratigraphic contact occurs on strike with the projected trends of both the Discovery and Silver Zone horizons on the adjacent Rea and Kamad properties.

Mineral exploration work on the adjoining Rea Gold property has tested the Discovery Zone horizon and is currently being carried out on the Silver Zone horizon. Detailed surveying, trenching and drilling over the last three years have delineated three gold-bearing massive sulphide lenses within the Discovery Zone horizon over a strike length of 350 metres and to a depth of 100 metres.

The three gold-bearing massive sulphide lenses are called the 'L 100', 'L 98' and 'L 97' lenses. These volcanogenic sulphide lenses occur near the stratigraphic top of a highly altered tuff and exhalative chert sequence called the 'Rea chert' horizon. This member lies above a thicker sequence of mafic ash, crystal, and lapilli tuffs. The lenses are underlain by a footwall feeder and alteration zone, characterized by intense silicification, pervasive pyrite, and sericite development, indicative of silica, iron and potassium metasomatism. The southern two lenses, L 98 and L 97, are 'capped' by a layer of sulphide-bearing barite. All

lenses are stratigraphically overlain by a thin sequence of mafic tuff, called the 'muddy' tuff, which grades up into argillites, wackes, and grits (Hoy and Goutier, 1986).

Deposition of sulphides and barite occurred near the end of a cycle of explosive volcanism. Intense regional deformation and greenschist facies regional metamorphism have altered the host rocks to produce a succession of sheared chlorite phyllites, quartz-sericite schists, and chert (Hoy and Goutier, 1986). The drill indicated reserves of these three lenses are reported to be 267,720 tons grading 0.190 oz./ton gold, 2.14 oz./ton silver, 2.247 % zinc, 2.14 % lead and 0.527 % copper at a cut-off grade of 0.05 oz./ton gold (G.C.N.L., No. 131, 1986).

The Silver Zone horizon has much the same geologic setting as the Discovery horizon, perhaps the same lithologic succession has been structurally repeated. The main difference between the reported mineralization of these two horizons seems to be that the Silver Zone mineralization has a much higher silver to gold ratio, in the order of 800 to 1. This discrepancy may be due to a late-stage or post-metamorphic, fault controlled vein structure which subparallels the sulphide-bearing horizon in the vicinity of the exploration trenches. The writer observed in outcrop that some of the primary sulphide mineralization has been remobilized and recrystallized within the fault/vein structure as semi-massive to massive tetrahedrite mineralization (Blanchflower, 1986). Although there are no published reserves, drilling by Corporation Falconbridge Copper and announcements by Rea Gold Corporation indicate that their Silver Zone hosts values of up to 0.037 oz./ton gold, 28.8 oz./ton silver, 1.07 % copper, 5.03 % zinc and 3.72 % lead over a drill intercept of 4.20 metres (G.C.N.L., No. 153, p. 1).

Further exploration for syngenetic sulphide mineralization on the TWIN property should be concentrated in the northwestern portion of the claim group where the geological, geochemical and geophysical results show that the Discovery and/or Silver Zone horizons may exist.

The 'Twin Mountain' silver-lead-zinc showings should be re-evaluated in light of the recent exploration results from the Silver Zone of the adjoining Rea property. Perhaps past exploration work by Sinmax Mines and Apex Energy Corp. did not recognize the economic potential of late-stage or post-metamorphic veining when it is superimposed on a syngenetic sulphide-bearing horizon.

The dioritic intrusion, northwest of the 'Twin Mountain' prospect at grid coordinates L 72+00 East by 4+00 North, should also be re-examined to see if there is a potential here for contact metasomatic mineralization.

CONCLUSIONS

The geological results indicate that the local stratigraphy undergoes a facies change along strike, in a northwesterly direction, from a dominantly volcanic sequence to one of a volcanic succession conformably overlain by exhalative and epiclastic sedimentary rocks. If this is the case, then the most favourable geologic setting for syngenetic massive sulphide deposition would be in the northwestern corner of the claim group.

Future geological surveying must be directed toward locating and defining the top of the 'Rea chert' horizon, for it is within this volcanogenic member that the gold-bearing sulphide mineralization is situated. Massive sulphide lenses may develop at different levels within the chert horizon and they may be locally discordant within this unit, but the known mineralization on the Rea property is both genetically and spatially associated with it.

A total of 2,250 B-horizon soil geochemical samples has been collected over the property. Their results indicate three dominant geochemical trends. These trends are:

- 1) Twin Mountain Trend (L 60+00 East by 3+00 North to L 73+00 East by 2+00 North) - reflects the known mineralization at the 'Twin Mountain' lead-zinc-silver prospect. This linear lead, zinc, silver and copper anomaly appears to be off-set northeasterly as it trends northwestward from the Twin Mountain silver-lead-zinc showings. It strengthens in a southeasterly direction within the property where the anomaly overlies highly fractured and altered mafic volcanic flows and volcanoclastics;
- 2) Ridge Trend (L 60+00 East by 2+50 South to L 83+00 East by 1+00 North) - It has a very strong silver, gold and copper response and is underlain by mafic volcanic and volcanoclastic rocks which host local structurally controlled alteration zones. These alteration zones are silicified, pyritized and sparingly mineralized with chalcopyrite, galena, sphalerite, magnetite and hematite; and
- 3) Homestake Trend (L 83+00 East by 1+00 South to L 76+00 East by 1+50 South) - This trend is reflected by anomalous arsenic, gold and lead soil geochemistry. It overlies the stratigraphic contact between the major volcanic and sedimentary units, and it appears to be truncated by an apparent northeasterly trending fault zone underlying Homestake Creek.

The highest metal values that analysed from all of the litho-geochemical samples are 260 p.p.b. gold, 2.8 p.p.m. silver, 316 p.p.m. copper, 4,567 p.p.m. lead, 7,252 p.p.m. zinc. It is obvious from these results that no economic mineralization was discovered during the litho-geochemical sampling or trenching programs.

The geophysical survey discovered ten electromagnetic conductors, three of which are certainly worthy of further investigation. These three conductors are supported by positive and coincident geological and/or geochemical anomalies.

It is the writer's opinion that further exploration work is warranted, but this work should be directed at evaluating specific exploration targets.

The highest priority target is undoubtedly the geological, geochemical and/or geophysical anomalies in the northwestern corner of the claim group. This target will require an extensive trenching program and/or diamond drilling program.

The 'Twin Mountain' silver-lead-zinc showings should be re-evaluated because past exploration efforts might not have recognized the economic potential of late-stage or post-metamorphic veining when it is superimposed on a syngenetic sulphide-bearing horizon, like the 'Silver Zone' on the Rea property.

The dioritic intrusion with its attendant copper geochemical response, northwest of the 'Twin Mountain' prospect, should be re-examined to see if there is a potential there for contact metasomatic mineralization.

Submitted By,

MINOREX CONSULTING LTD.

A handwritten signature in cursive script, reading "J. D. Blanchflower". The signature is written in dark ink and is positioned above the printed name and title.

J. D. Blanchflower, F.G.A.C.
Consulting Geologist

STATEMENT OF QUALIFICATIONS

I, J. DOUGLAS BLANCHFLOWER, of the City of Kamloops, Province of British Columbia, DO HEREBY CERTIFY THAT:

- 1) I am a Consulting Geologist with a business office at Suite 200A - 156 Victoria Street, Kamloops, British Columbia, V2C 1Z7; and President of Minorex Consulting Ltd.
- 2) I am a graduate in geology with a Bachelor of Science, Honours Geology degree from the University of British Columbia in 1971.
- 3) I am a Fellow of the Geological Association of Canada.
- 4) I have practised my profession as a geologist for the past fifteen years.

Pre-Graduate experience in Geology, Geochemistry and Geophysics in British Columbia, Yukon and Northwest Territories (1966 to 1970).

Three years as Geologist with the British Columbia Ministry of Energy, Mines and Petroleum Resources (1970 to 1972).

Seven years as Exploration Geologist with Canadian Superior Exploration Limited (1972 to 1979).

Three years as Exploration Geologist with Sulpetro Minerals Limited (1979 to 1982).

Four years as Consulting Geologist with Minorex Consulting Ltd. (1982 to 1986).

Active mineral exploration and development experience throughout Western North America.

- 5) I own no direct, indirect or contingent interest in the subject claims, nor shares in or securities of LINCOLN RESOURCES INC. or APEX ENERGY CORP.
- 6) I supervised the geological and geochemical surveys and wrote those sections of this report which documents their results.
- 7) I consent to the use of this report in a Prospectus or Statement of Material Facts.



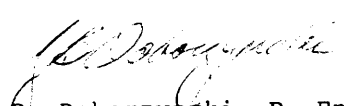
J. D. Blanchflower, F.G.A.C.

Dated at Kamloops, B. C. this 24th day of February, 1987.

CERTIFICATION

I, Zbigniew B. Doborzynski of 871 Tudor Avenue in the city of North Vancouver, in the Province of British Columbia, do hereby certify that:

1. I graduated from McGill University with a B.Eng. in Mining Engineering and Applied Geophysics in 1971;
2. I received an M.Sc. in Applied Geophysics, also from McGill University in 1974;
3. I am a registered member of the Association of Professional Engineers of the Province of Ontario, the Society of Exploration Geophysicists and B.C. Geophysical Society;
4. I am employed as an Exploration Geophysicist with Esso Minerals Canada;
5. I have been practicing my profession for the past thirteen years.


Z. B. Doborzynski, P. Eng.
Geophysicist
ESSO MINERALS CANADA

-STATEMENT OF QUALIFICATIONS-

I, DWAYNE M.J. WINDSOR, of the City of Kamloops, Province of British Columbia, DO HEREBY CERTIFY THAT:

1) I am a Consulting Geological Technologist with a business office at 1013 Dundas Street, Kamloops, British Columbia, V2B 2T1; and President of Tarnex Geoservices.

2) I am a graduate Geotechnologist with a diploma from Sir Sandford Fleming College in 1978.

3) I have practised my profession for the past eleven years:

Pre-Graduate experience in Geology, Geochemistry and Geophysics in Quebec and Saskatchewan (1976 to 1977).

Nine years as a Geophysical and Geological Technologist with Novamin Resources (formerly Sulpetro Minerals Limited) in British Columbia, Yukon Territory, Northwest Territories, Ontario, Quebec and Nova Scotia.

One year as a Consulting Geological Technologist with Tarnex Geoservices.

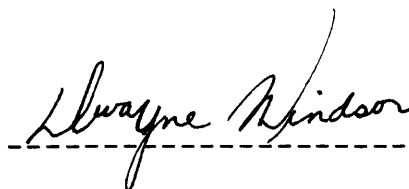
4) I own no direct, indirect or contingent interest in the subject claims, nor shares in or securities of LINCOLN RESOURCES INC.

5) I carried out a Geological Survey of the TWIN Property under the supervision of Mr. J. D. Blanchflower, F.G.A.C.

I carried out a fixed source Genie electromagnetic survey under the supervision of Mr. Z. Doborzynski and

I supervised the trenching program on the TWIN Property.

6) This work was carried out between October 16th and December 16th, 1986.



Dwayne M. Windsor

Dated at Kamloops, B.C., this 24th day of February, 1987.

STATEMENT OF COSTS

Re: Relabelling existing control grid (14.0 line-km.),
Establishment of additional control grid (15.15 line-km.),
Geological mapping at a scale of 1:5,000,
Soil and lithogeochemical sampling, and analysis (361 soil
and 63 rock samples),
Geophysical surveying (fixed source Genie electromagnetic
survey, 17.75 line-km.),
Trenching (300 metres), and
Collation, plotting drafting, interpretation and documenta-
tion of all survey data from the 1986, 1985 and 1984 explora-
tion programs.

FIELD EXPENSES - October 16 to December 16, 1986

1. **Personnel**

D. Windsor - 33 days @ \$200.00/day	\$ 6,600.00
D. Blanchflower - 13 days @ \$300.00/day	3,900.00
N. Martin - 27.5 days @ \$150.00/day	4,125.00
S. Lowe - 8 days @ \$150.00/day	1,200.00
2. **Room and Board**

Room and board for D. Windsor, N. Martin and S. Lowe at Johnson Lake Fishing Lodge - 66.5 man days @ \$ 27.296/man day	1,815.17
Room and board for S. Lowe (mob & demob) - 3 days @ \$43.903/man day	131.71
3. **Geophysical Equipment Rental**

ESSO Minerals Canada - 13 days @ \$ 136.30/day	1,771.83
--	----------
4. **Generator Rental**

Minorex Consulting Ltd. - 6 days @ \$ 10.00/day	60.00
---	-------
5. **Snowmobile Rental**

Prop and Track and Interior Motorcycles (2 sleds) 15 days @ \$ 50.00/day plus fuel and tax	818.76
---	--------
6. **Vehicle Expenses**

Tarnex Geoservices and Minorex Consulting Ltd. Two 4WD 1/2 ton P/U trucks 40 days @ \$ 35.00/day plus 2,328 km. @ \$ 0.35/km.	2,214.78
--	----------

7. Geochemical Analyses (Acme Analytical)	
Sample preparation, analysis and statistics	
Soil geochemical samples - 31 elements	3,880.75
Rock geochemical samples - 31 elements	700.00
Shipping rx samples (Kam - Van)	74.50
8. Linecutting and Grid Relabelling	
Amex Exploration Services	6,953.15
9. Snow Plowing (Holdings Lumber Company Ltd.)	
Grader - 10 hrs @ \$93.00/hr.	930.00
10. Trenching	
Brentwood Enterprises Ltd. - 38.6 hrs @ \$97./hr	3,741.00
11. Miscellaneous Field Supplies	
Flagging, soil bags, tags, etc.	453.51
12. Miscellaneous Expenses	
Expended snowshoes, hay wire, sacks, etc.	<u>187.60</u>
Total Field Expenses	\$ 39,557.76

OFFICE EXPENSES - February 14 to 24, 1987

1. Report and Map Preparation	
J.D. Blanchflower - 4.5 days @ \$ 300.00/day	\$ 1,350.00
D. Windsor - 61 hrs. @ \$ 18.00/hr.	1,098.00
2. Drafting and Reproductions	
Drafting (T.P. Quinn) - 62 hrs. @ \$ 15./hr.	930.00
Universal Reproductions - report and map reproduction and copying	1,090.93
3. Shipping and Courier Charges	
Loomis, P.W.A., and Greyhound Bus Lines	51.67
4. Management Fee	
C.E.C. Engineering Ltd. (Vancouver)	<u>3,100.00</u>
Total Office Expenses	\$ 7,620.60

TOTAL COST OF PROJECT	<u>\$ 47,178.36</u>
------------------------------	----------------------------

BIBLIOGRAPHY

- B.C. Ministry of Energy,
Mines and Pet. Res., 1983: Minfile; No. 082M 020; pp. 2956-57.
- B.C. Minister of Mines: Annual Report, 1936, p. D 39.
- Blanchflower, J.D., 1986: Exploration Report on the Twin Property, Kamloops Mining Division, British Columbia; private report to Lincoln Resources Inc., pp. 24.
- Blanchflower, J.D., 1986: Evaluation of the Silver Zone mineralization on the Rea (AR/HN) Property, Kamloops Mining Division, B.C.; private report to Rea Gold Corporation.
- Blanchflower, J.D., 1986: Exploration Report on the Rea (AR/HN) Property, Kamloops Mining Division, British Columbia; private report for Rea Gold Corporation.
- Campbell, R.B., 1963: Adams Lake, G. S. C. Map 48 - 163.
- Corporation Falconbridge
Copper, 1984: Geological, Geochemical and Geophysical Data; private company reports and maps.
- ESSO Minerals Canada, 1986: Geochemical and Geophysical Data; private company reports and data.
- Dawson, J.M., 1969: Geological Report on the Twin Mountain Property, Adams Lake Area, Kamloops Mining Division, British Columbia; Assessment Report No. 2093.
- George Cross News Letter,
1986: March 21, 1986, No. 57, p. 1.
May 28, 1986, No. 102, p. 2.
July 9, 1986, No. 131, p. 2.
July 15, 1986, No. 135, p. 1.
August 11, 1986, No. 153, p. 1.
- Goutier, F., Godwin, C. Mineral Deposits of the Birk Creek Area: An Introduction to a Metallogenic Study of the Adams Plateau - Clearwater Area (B2M); B.C. Ministry of Energy, Mines and Pet. Res., Geological Fieldwork, 1984, Paper 1985-1, pp. 67-76.

- Hoy, T., and Goutier, F., 1986: Rea Gold (Hilton) and Homestake Volcanogenic Sulphide-Barite Deposits, Southeastern British Columbia, 82M/4W; B.C. Ministry of Energy, Mines and Pet. Res., Geological Fieldwork, 1985; Paper 1986-1; pp.59-68.
- Lincoln Resources Inc., 1986: Geological, Geochemical and Geophysical Data; private company data.
- Oliver, J., 1986: Personal Communications.
- Preto, V.A. and Schiarizza, P.A., 1985: Geology and Mineral Deposits of the Adams Plateau - Clearwater Region; Geol. Soc. Am., Cordilleran Section Meeting, Guidebook, Field Trip No. 16, pp. 16-1 to 16-11.
- Read, W.S., 1968: Geochemical and Geophysical Report, STAR 1-14 and adjoining claims, report for Sinmax Mines Ltd.; Assessment Report No. 1783.
- Schiarrizza, P.A., and Preto, V.A., 1984: Geology of the Adams Plateau - Clearwater Area; B. C. Ministry of Energy, Mines and Pet. Res., Preliminary Map 56.
- White, G.P.E., 1985: Hilton Massive Sulphide Discovery (Rea Gold), Johnson Creek - Adams Lake Area (82M/4W); B.C. Ministry of Energy, Mines and Pet. Res., Geological Fieldwork, 1984, Paper 1985-1, pp. 77-83.

APPENDIX I

GEOPHYSICAL REPORT ON THE TWIN PROPERTY

APPENDIX I

FIXED SOURCE GENIE SURVEY ON THE TWIN PROPERTY KAMLOOPS MINING DIVISION - NTS 82M/4W

Introduction

A fixed source GENIE electromagnetic survey has been carried to explore the west side of the property and to locate the southeast extensions of both the Rea and Silver horizons.

17.75 line kilometers of surveying was completed.

Description of the GENIE system

GENIE is an acronym for "GEometry Normalised In-Phase Electromagnetometer". It is manufactured by Scintrex.

Field procedure consists of laying out a large loop of insulated wire (Fig. 1) and energising it with current from a transmitter which is powered by a 2.5 kW motor-generator. The transmitter loop is usually laid out on the footwall side of the target with its long sides oriented parallel to the geological strike in the area. Measurements are taken along lines laid out perpendicular to the long sides of the loop.

The transmitter unit is capable of simultaneously energising the loop with very stable sinusoidal current waveforms at five frequencies - 37.5, 112.5, 337.5, 1012.5 and 3037.5 Hz. The frequencies to be transmitted can be selected. The fewer frequencies chosen, the higher the output at those frequencies that are transmitted.

FIXED SOURCE GENIE

LARGE LOOP ON SURFACE

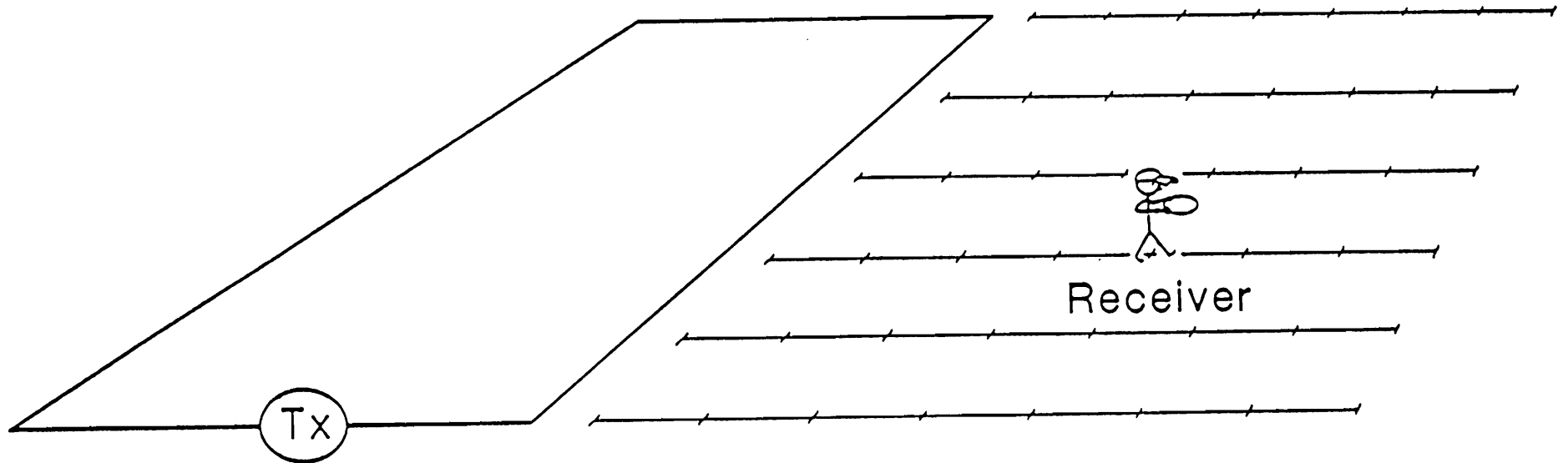


Figure 1

The receiver unit can either be the analog SE-88 console and sensor or the newer IGS data acquisition system with EM4 module and sensor. Either unit simultaneously measures the vertical magnetic field amplitudes at two frequencies, calculates the amplitude ratio and displays the result as a percentage value. One frequency is called the "reference". It is normally 37.5 Hz and as a result is relatively unaffected by all but the most conductive features. The other, referred to as the "signal" is at a much higher frequency (112.5, 337.5, 1012.5 or 3037.5). In barren areas, the normalised amplitudes at these two frequencies are the same whereas in conductive areas, the "signal frequency" amplitude is significantly different from the "reference" to be detected.

In this survey four amplitude ratios were measured - 3037.5/37.5, 1012.5/37.5, 337.5/37.5 and 112.5/37.5. Measurements were taken at 25 m intervals.

Figure 2 shows the fixed source GENIE response to a vertical conductor. The quality of this conductor is indicated by the responses at different frequency ratios. A weaker conductor will only be detected by the 3037.5/37.5 Hz ratio, while a much better conductor will have similar responses at all four frequency ratios.

A common procedure in processing the results is to Fraser filter the data, thus converting the crossover response (Fig. 2a) to a peak response (Fig. 2b), allowing contouring of the results.

**Theoretical Response To A Vertical Thin Sheet Conductor
In A Resistive Half Space**

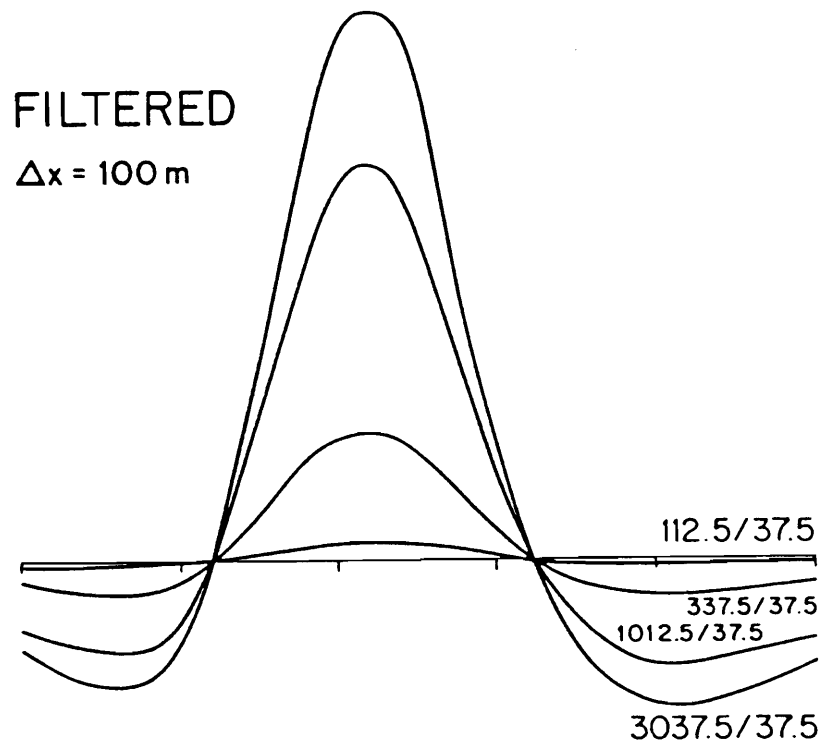
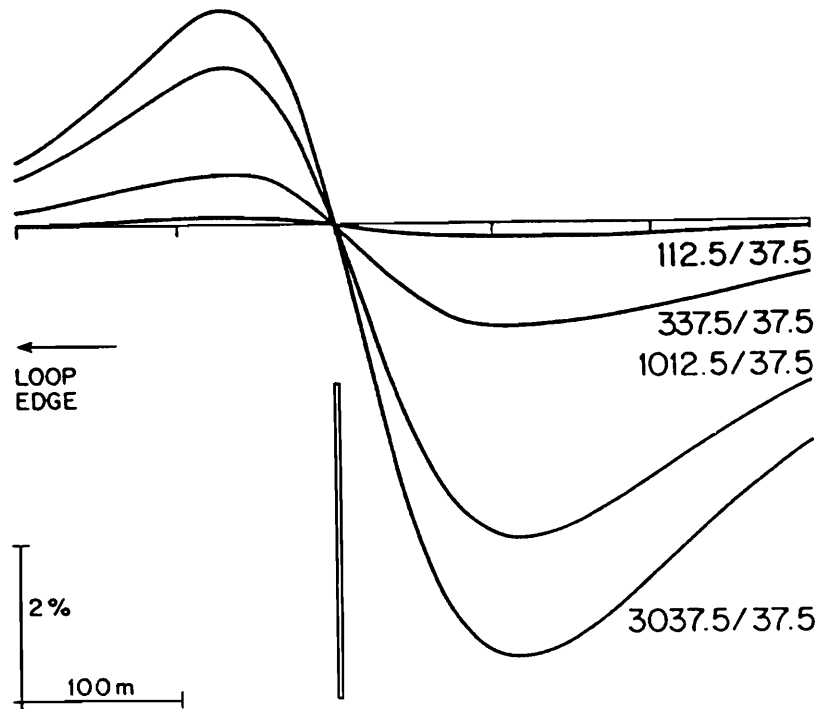


Figure 2

Data Presentation

The raw field data, Fraser filtered results as well as the calculated Hjelt filter, in a pseudo-section format, are presented in Appendix II. Contoured Fraser filtered results for the four frequency ratios are presented on Figures 12 to 15. The interpreted EM anomalies are presented jointly with geology, geochemistry and trenching results on the Compilation Map (Fig. 17).

All maps discussed in this section are at a scale of 1:5000.

The Fraser filter is a commonly used procedure to transform VLF-EM and now GENIE data into a form that allows contouring of the results. It is obtained by taking four equally spaced readings - R_{i-1} , R_i , R_{i+1} and R_{i+2} and performing the following calculation:

$$F.F_{i+1/2} = (R_{i-1} + R_i - R_{i+1} - R_{i+2})$$

The result is plotted midway between the positions of R_i and R_{i+1} . A complete description of this procedure can be found in an article written by Fraser (1969).

An extension of this filter process is given by Karous and Hjelt (1983) in which they convert EM data into equivalent current densities as a function of depth. In effect, this procedure simulates electrical current flow in the subsurface that would be required to produce the measured values. This filter uses six equally spaced readings in the following calculation:

$$I_J = -0.102 R_{J-3} + 0.059 R_{J-2} - 0.561 R_{J-1} + 0.561 R_{J+1} \\ - 0.059 R_{J+2} + 0.102 R_{J+3}$$

where I_J is the equivalent current density for station "J" at a depth equal to the station interval. Equivalent current densities at greater depths are calculated by using values at proportionately greater intervals. The result is the pseudo-section presentation found in Appendix II.

Discussion of Results

Ten conductive zones have been outlined. These are shown on Figure 17 and are labelled zones A to J. Most are weak conductors as they are detected by the 3037/37 and 1012/37 frequency ratios only (Fig. 12 and 13). Zone A and parts of zones H, I and J are more conductive as evidenced by the fact that they have also been detected by the 337/37 frequency ratio (Fig. 14). The responses at the 112/37 frequency ratio (Fig. 15) are very weak, indicating that none of these zones can be classed as very good conductors. Comments on the individual zones are given in the following paragraphs.

Zone A - Line 83E to 78E at about 800S

This zone is open both to the east and west. Its average conductance is about 10 Siemens (S) indicating that cause of this anomaly is a good quality, buried conductor whose top is within 25 m of surface.

This zone occurs within a wide sedimentary unit and is probably caused by conductive sediments within it.

Zone B - Line 83E to 80E at about 650S

This is a very weak conductor whose conductance is less than 1 S. It may be caused by a resistivity contrast between the sedimentary unit which hosts zone A and mafic volcanics to the north of it.

Zone C - Line 83E to 75E at 400S

The strongest response is on line 83E. On adjacent lines, responses are progressively weaker. This zone is not detected on line 79E but recurs between lines 78E and 75E. Its average conductance is less than 1 S, again indicating a change in lithology.

Zone D - Line 83E to 64E at about 300S

The strongest responses are on lines 83E to 75E where estimated conductivities range from 3 to 12 S. The source is near surface. Trenching in the area of the EM anomalies on lines 81E and 80E has exposed graphitic argillites at the contact between sediments and altered mafic volcanics.

East of 75E, responses are significantly weaker; giving conductance estimates in the 1 S range. Between lines 71E and 64E the anomaly coincides with a road which could be considered as the source, however trenches north of the anomaly, on lines 71E and 67E, have exposed altered mafic volcanics containing pyrite and malachite. The source of this anomaly is probably the contact between these volcanics and sediments to the south.

Zone E - Line 79E to 70E at about 200S

Conductance estimates are variable along this trend, ranging from less than 1 to 8 siemens, indicating a weak to fair conductor. The source is shallow. A trench on line 78E and north of of the conductor encountered altered mafic volcanics containing between 1 to 10% pyrite suggesting that the cause of this anomaly may also be a lithologic contact.

Zone F - Line 83E to 71E at about 100S

The conductivity of this zone is variable along strike. The strongest responses are between lines 83E and 80E and also between 77E and 73E.

A multi-element geochemical anomaly roughly correlates with this conductor, between lines 83E and 80E.

Zone G and J - Line 79E to 60E between 50N and 100N

These two zones appear to be faulted portions of the same feature. The fault is located between lines 68E and 69E. The most conductive portions of these zones are located between lines 76E and 74E and also between 71E and 66E. The responses indicate that Zone J is the shallowest of the two. There is no indication as to the cause of these anomalies.

Zone H - Lines 74E and 60E at about 300N

This zone may consist of two enechelon conductors located between lines 74E and 70E, and 64E and 62E. Conductance estimates for both zones are in the 10 S range, indicating good quality conductors. There is no source that can explain the whole trend however between line 72E and 69E the conductor coincides with the exposed contact between a diorite intrusion and mafic volcanics. This contact is reported to be strongly mineralized with pyrite.

Zone I - Line 76E to 60E at about 450N

GENIE responses along this zone are the strongest and most consistent of the survey. This zone has been traced for a distance of 1.6 km. It weakens to the east but is open to the west. The Twin Mountain showing is located just north of it on line 71E at 500N. Moreover, this year's geochemical survey has outlined a coincident strong multi-element anomaly (Pb, Zn, Ag). The source appears to be within a sericitized and pyritized altered mafic volcanic.

Conclusion

Three different, though potentially significant, conductor trends have been outlined:

1. Weak to very weak conductors, probably caused by a change in lithology. These anomalies may represent similar geological settings to the Rea and Silver horizons.

Zone D reflects one such setting based on trenching. This feature may be the SE extension of the "Silver" horizon. Zone B which is located 300 m to the south may, as a result, be the expression of the "Rea" horizon. Zones C, E, F and possibly G and J have similar EM signatures and should be checked.

2. Fair to good conductors, bordering an intrusion.

Zone H borders an exposed diorite intrusion between lines 69E and 72E and may be caused by sulphide mineralization at the contact between this intrusion and mafic volcanics. If there is potential for precious metals in this setting, then two areas along this trend should be explored - between lines 75E and 71E and lines 64E and 62E where the strongest responses were obtained.

3. Long strike length good quality conductors

Zone I extends from line 76E to 60E. Its average conductance is about 15 Siemens. The Twin Mountain Pb/Zn showing is located in the immediate vicinity. Furthermore, a strong Pb/Zn/Ag geochemical anomaly is associated with this trend. This area should be further prospected, particularly in the area of an old trench which crosses line 71E at 500N (Fig. 17). This trench may have been stopped just north of the interpreted location of this EM trend. If possible, this trench should be extended further south to cross this conductor.

Z. Doborzynski
Geophysicist, P. Eng.
ESSO MINERALS CANADA

References

Fraser, D.C., 1969: Contouring of VLF-EM data: Geophysics, 34, pp 958-967

Karous, M. & Hjelt, S.E., 1983: Linear filtering of VLF dip angle measurement: Geophysical Prospecting, 31, pp 782-794

APPENDIX II

FIXED SOURCE GENIE ELECTROMAGNETIC SURVEY

Survey Data and Profiles

TWIN GRID - LARGE LOOP EM

LINE 5300E

DATE 11/30/86

OPERATOR N.M. Nparm=4

STATION	112/37	337/37	1012/3	3037/3	FF1	FF2	FF3	FF4
-200.0	6.5	13.8	20.3	15.4	*	*	*	*
-175.0	7.2	15.1	22.3	16.9	-1.9	-4.6	-6.2	-2.2
-150.0	7.6	16.2	23.4	16.8	-1.6	-4.4	-7.2	-3.4
-125.0	8.0	17.3	25.4	17.7	-1.8	-4.3	-7.5	-3.5
-100.0	8.4	18.4	27.5	19.4	-2.1	-4.0	-6.4	-2.3
-75.0	9.0	19.4	28.8	18.6	-2.5	-5.1	-8.4	-7.3
-50.0	9.5	20.3	30.5	20.8	-2.7	-6.5	-12.5	-13.1
-25.0	10.4	22.6	34.2	24.5	*	*	*	*
0.0	10.8	23.6	37.6	28.0	*	*	*	*

TWIN GRID - LARGE LOOP EM LINE 5400E
DATE 11/30/86 OPERATOR N.M. Nparm=4

STATION	112/37	337/37	1012/3	3037/3	FF1	FF2	FF3	FF4
-300.0	4.4	9.0	13.5	13.6	*	*	*	*
-275.0	5.0	9.9	15.1	14.1	-1.7	-3.9	-5.6	-2.3
-250.0	5.4	11.0	16.6	15.2	-1.4	-3.9	-4.9	-0.5
-225.0	5.7	11.8	17.6	14.8	-1.7	-3.9	-5.0	0.2
-200.0	6.1	13.0	19.0	15.0	-1.9	-3.7	-4.9	1.5
-175.0	6.7	13.7	20.2	14.8	-1.6	-3.8	-5.0	1.6
-150.0	7.0	14.8	21.3	13.5	-1.5	-4.0	-6.2	-2.2
-125.0	7.4	15.7	22.9	14.7	-1.9	-4.2	-7.5	-4.7
-100.0	7.8	16.8	24.8	15.8	-2.0	-5.2	-9.8	-9.4
-75.0	8.5	17.9	26.9	17.1	-1.7	-5.9	-12.0	-14.8
-50.0	8.7	19.8	30.6	22.8	-1.9	-4.8	-9.0	-7.4
-25.0	9.3	20.8	33.1	24.9	*	*	*	*
0.0	9.8	21.7	33.4	22.4	*	*	*	*

TWIN GRID - LARGE LOOP EM LINE 5500E
DATE 11/30/86 OPERATOR N.M. Nparm=4

STATION	112/37	337/37	1012/3	3037/3	FF1	FF2	FF3	FF4
-400.0	2.9	5.5	7.8	9.2	*	*	*	*
-375.0	3.2	6.1	8.9	9.8	-1.4	-3.3	-5.4	-3.8
-350.0	3.6	7.0	10.3	10.7	-1.4	-3.5	-5.6	-4.2
-325.0	3.9	7.9	11.8	12.1	-1.3	-3.3	-4.8	-2.0
-300.0	4.3	8.7	13.0	12.6	-1.3	-3.2	-4.1	0.8
-275.0	4.5	9.5	13.9	12.2	-1.6	-3.2	-4.2	1.7
-250.0	5.0	10.3	15.0	11.7	-1.6	-3.3	-5.0	0.2
-225.0	5.4	11.1	16.1	11.4	-1.4	-3.3	-5.0	-0.0
-200.0	5.7	12.0	17.8	12.3	-1.7	-3.6	-4.6	0.8
-175.0	6.1	12.7	18.3	10.8	-2.1	-4.5	-6.1	-2.8
-150.0	6.7	14.0	20.2	12.1	-1.8	-4.6	-7.3	-5.6
-125.0	7.2	15.2	22.0	13.8	-1.4	-4.1	-7.4	-5.9
-100.0	7.4	16.1	23.8	14.7	-1.8	-5.0	-10.0	-11.4
-75.0	7.9	17.2	25.8	17.1	-2.3	-6.1	-12.2	-14.5
-50.0	8.5	19.1	30.0	22.8	-2.2	-4.5	-6.8	-1.4
-25.0	9.1	20.3	31.8	23.5	*	*	*	*
0.0	9.5	20.5	30.8	17.8	*	*	*	*

TWIN GRID - LARGE LOOP EM

LINE 3600E

DATE 11/30/86

OPERATOR N.M. Nparm=4

STATION	112/37	337/37	1012/3	3037/3	FF1	FF2	FF3	FF4
-500.0	2.0	3.3	3.9	5.3	*	*	*	*
-475.0	2.3	4.0	5.3	7.5	-1.1	-2.4	-4.6	-5.2
-450.0	2.6	4.6	6.5	8.7	-0.9	-2.3	-4.0	-3.5
-425.0	2.8	5.1	7.3	9.3	-0.8	-2.4	-4.2	-3.3
-400.0	3.0	5.8	8.5	10.4	-0.8	-2.1	-3.8	-2.0
-375.0	3.2	6.3	9.5	10.9	-1.0	-2.3	-3.3	0.3
-350.0	3.4	6.7	10.1	10.8	-1.3	-3.1	-3.6	1.5
-325.0	3.8	7.7	11.2	10.2	-1.5	-3.3	-4.1	0.5
-300.0	4.1	8.4	12.0	10.0	-1.5	-3.2	-4.6	-0.5
-275.0	4.6	9.3	13.4	10.5	-1.3	-3.4	-5.5	-2.2
-250.0	4.8	10.0	14.4	10.2	-1.6	-3.8	-6.6	-5.1
-225.0	5.2	11.1	16.5	12.5	-2.0	-4.1	-7.0	-5.9
-200.0	5.8	12.0	17.9	13.3	-1.9	-4.3	-6.7	-3.9
-175.0	6.2	13.2	20.0	15.3	-1.5	-3.4	-4.3	1.2
-150.0	6.7	14.2	21.1	14.4	-1.5	-2.8	-3.4	1.4
-125.0	6.8	14.4	21.1	13.0	-1.9	-4.0	-6.7	-5.3
-100.0	7.6	15.8	23.4	15.3	-1.8	-5.0	-9.9	-10.4
-75.0	7.8	16.8	25.5	17.4	-1.8	-4.9	-9.2	-7.4
-50.0	8.4	18.4	28.9	21.3	-1.6	-3.2	-2.8	6.1
-25.0	8.8	19.1	29.2	18.8	*	*	*	*
0.0	9.0	19.3	28.0	13.8	*	*	*	*

TWIN GRID - LARGE LOOP EM LINE 5700E
 DATE 11/30/86 OPERATOR N.M. Nparm=4

STATION	112/37	337/37	1012/3	3037/3	FF1	FF2	FF3	FF4
-525.0	1.9	3.0	3.3	4.1	*	*	*	*
-500.0	2.1	3.6	4.5	6.2	-0.9	-2.4	-4.6	-6.4
-475.0	2.3	4.2	5.6	7.8	-1.0	-2.3	-4.5	-5.0
-450.0	2.6	4.8	6.8	8.9	-1.0	-2.3	-4.3	-3.9
-425.0	2.8	5.3	7.8	10.1	-1.0	-2.4	-4.2	-2.7
-400.0	3.1	6.0	8.9	10.5	-0.9	-2.3	-3.6	-0.7
-375.0	3.3	6.5	9.9	11.2	-0.9	-2.6	-3.3	1.0
-350.0	3.5	7.1	10.4	10.1	-1.2	-3.0	-3.9	-0.3
-325.0	3.8	8.0	11.7	10.6	-1.4	-2.9	-4.2	-1.3
-300.0	4.2	8.6	12.5	11.0	-1.3	-2.7	-4.1	-0.1
-275.0	4.5	9.4	13.8	11.0	-1.5	-3.0	-5.1	-2.3
-250.0	4.8	9.9	14.5	10.7	-1.9	-3.8	-6.8	-5.6
-225.0	5.4	11.1	16.9	13.6	-1.6	-3.9	-6.0	-3.4
-200.0	5.8	12.0	18.2	13.7	-1.0	-3.5	-4.6	-1.8
-175.0	6.0	12.9	19.2	14.0	-0.9	-3.6	-5.6	-3.8
-150.0	6.2	13.7	20.5	15.1	-1.5	-3.7	-6.4	-3.7
-125.0	6.5	14.8	22.5	16.4	-2.4	-4.0	-6.4	-2.8
-100.0	7.2	15.5	23.6	16.4	-2.3	-4.2	-6.2	-2.0
-75.0	7.9	17.0	25.8	17.9	-1.5	-2.5	-2.9	5.6
-50.0	8.1	17.5	26.5	16.9	-1.5	-2.1	0.0	13.0
-25.0	8.5	17.5	25.8	11.8	*	*	*	*
0.0	9.0	19.1	26.5	10.0	*	*	*	*

TWIN GRID - LARGE LOOP EM LINE 5800E

DATE 01 DEC. 1986 OPERATOR D.W. LOOP#3 LOOP 1100x750m Nparm=4

STATION	112/37	337/37	1012/3	3037/3	FF1	FF2	FF3	FF4
-525.0	2.0	3.0	3.3	3.7	*	*	*	*
-500.0	2.2	3.6	4.7	6.3	-1.1	-2.4	-4.6	-7.0
-475.0	2.5	4.2	5.8	8.1	-1.0	-2.4	-4.1	-4.2
-450.0	2.8	4.8	6.8	8.9	-0.7	-2.3	-3.9	-2.8
-425.0	2.9	5.4	7.8	9.7	-0.8	-2.3	-4.0	-2.1
-400.0	3.1	5.9	8.7	10.1	-1.1	-2.6	-4.4	-2.2
-375.0	3.4	6.6	9.9	10.6	-1.2	-2.8	-4.5	-2.5
-350.0	3.7	7.3	11.0	11.4	-1.2	-2.8	-4.4	-2.1
-325.0	4.0	8.0	12.1	11.8	-1.1	-2.9	-4.2	-1.2
-300.0	4.3	8.7	13.2	12.3	-1.2	-3.1	-3.9	-0.2
-275.0	4.5	9.5	14.1	12.1	-1.5	-3.5	-4.4	-0.6
-250.0	5.0	10.3	15.1	12.2	-1.4	-3.9	-5.6	-2.7
-225.0	5.3	11.4	16.6	12.8	-1.4	-3.7	-5.9	-3.3
-200.0	5.6	12.3	18.2	14.2	-1.5	-3.7	-6.8	-5.1
-175.0	6.1	13.1	19.4	14.1	-1.4	-4.2	-9.2	-10.2
-150.0	6.3	14.3	22.2	18.0	-1.9	-4.6	-9.3	-10.7
-125.0	6.8	15.3	24.6	20.5	-1.8	-3.8	-4.9	-2.4
-100.0	7.5	16.7	26.3	22.3	-0.9	-1.7	1.4	13.5
-75.0	7.4	16.7	25.4	18.6	-1.2	-1.3	2.3	19.8
-50.0	7.8	17.0	24.1	10.7	-2.0	-2.6	-1.1	10.6
-25.0	8.3	17.7	25.3	10.4	*	*	*	*
0.0	8.9	18.6	25.3	8.3	*	*	*	*

TWIN GRID - LARGE LOOP EM LINE 5800E
 DATE 02 DEC. 1986 OPERATOR S.L. LOOP# 4 Nparm=4

STATION	112/37	337/37	1012/3	3037/3	FF1	FF2	FF3	FF4
-1275.0	-2.9	-4.8	-5.8	-5.6	*	*	*	*
-1250.0	-4.3	-8.0	-10.2	-11.5	5.3	11.5	15.4	22.2
-1225.0	-5.7	-10.9	-14.0	-17.1	4.6	10.1	13.6	20.1
-1200.0	-6.8	-13.4	-17.4	-22.2	4.0	8.9	12.2	17.4
-1175.0	-7.8	-15.6	-20.4	-26.5	3.5	8.1	11.2	15.5
-1150.0	-8.7	-17.6	-23.2	-30.2	3.5	7.9	10.7	14.9
-1125.0	-9.4	-19.5	-25.8	-34.0	3.6	7.4	9.9	13.4
-1100.0	-10.6	-21.6	-28.5	-37.6	2.8	6.2	8.7	11.9
-1075.0	-11.1	-22.9	-30.4	-40.0	2.5	5.9	8.6	12.7
-1050.0	-11.7	-24.4	-32.6	-43.5	3.0	6.3	8.5	12.7
-1025.0	-12.5	-26.0	-34.9	-46.8	2.8	5.7	7.1	10.4
-1000.0	-13.3	-27.6	-36.6	-49.4	2.1	4.6	6.2	8.9
-975.0	-13.7	-28.5	-38.0	-51.3	1.8	4.1	5.8	8.3
-950.0	-14.2	-29.7	-39.7	-53.8	2.1	3.8	4.6	6.5
-925.0	-14.6	-30.5	-40.7	-55.2	1.9	3.3	3.4	4.5
-900.0	-15.4	-31.5	-41.6	-56.4	1.2	2.5	2.3	2.8
-875.0	-15.3	-32.0	-42.2	-57.1	1.5	2.1	2.0	2.2
-850.0	-15.9	-32.5	-42.4	-57.3	1.7	2.6	3.6	5.9
-825.0	-16.3	-33.1	-43.4	-58.4	1.4	3.3	6.1	11.7
-800.0	-16.6	-34.0	-44.8	-61.9	1.1	3.3	7.5	13.5
-775.0	-17.0	-34.9	-47.1	-65.5	0.8	2.7	6.5	11.2
-750.0	-17.0	-35.5	-48.6	-68.3	1.1	2.4	5.1	9.3
-725.0	-17.4	-36.1	-49.8	-70.3	1.4	2.9	4.5	7.6
-700.0	-17.7	-36.7	-51.0	-72.8	1.8	3.5	3.9	4.5
-675.0	-18.1	-37.8	-51.9	-73.4	1.9	3.0	3.2	2.8
-650.0	-18.8	-38.5	-52.8	-74.2	1.0	1.9	2.5	2.4
-625.0	-18.9	-39.0	-53.3	-74.8	1.0	1.6	3.4	1.9
-600.0	-19.0	-39.2	-53.9	-75.2	1.7	2.2	5.3	5.8
-575.0	-19.7	-39.9	-55.6	-75.7	1.6	2.8	5.1	10.0
-550.0	-19.9	-40.5	-56.9	-80.1	1.0	2.6	3.6	6.1
-525.0	-20.4	-41.4	-57.7	-80.8	0.3	1.7	2.6	2.6
-500.0	-20.2	-41.6	-58.4	-81.1	0.9	1.6	2.8	3.8
-475.0	-20.4	-42.0	-58.8	-82.4	2.2	2.8	4.4	3.5
-450.0	-21.1	-42.6	-60.1	-83.3	2.3	3.5	5.0	2.3
-425.0	-21.7	-43.8	-61.5	-83.7	*	*	*	*
-400.0	-22.1	-44.3	-62.4	-84.3	*	*	*	*

TWIN GRID - LARGE LOOP EM					LINE 5900E			
DATE 01 DEC. 1986					OPERATOR D.W. LOOP#3 LOOP 1100x750m Nparm=4			
STATION	112/37	337/37	1012/3	3037/3	FF1	FF2	FF3	FF4
-525.0	2.3	3.1	3.2	3.3	*	*	*	*
-500.0	2.2	3.5	4.5	6.0	-0.3	-2.2	-4.3	-6.6
-475.0	2.4	4.3	5.8	7.8	-0.8	-2.0	-3.7	-3.6
-450.0	2.4	4.5	6.2	8.1	-1.3	-2.5	-4.8	-3.9
-425.0	3.0	5.3	7.8	9.3	-1.1	-3.0	-5.1	-3.9
-400.0	3.1	6.0	9.0	10.5	-1.1	-2.9	-4.8	-2.2
-375.0	3.4	6.8	10.1	10.8	-1.5	-3.2	-5.1	-1.6
-350.0	3.8	7.4	11.5	11.2	-1.5	-3.3	-4.1	-0.7
-325.0	4.2	8.6	12.7	11.7	-1.2	-2.7	-3.0	0.8
-300.0	4.5	8.9	13.0	11.0	-1.1	-2.8	-4.0	-0.3
-275.0	4.7	9.8	14.2	11.1	-1.3	-3.3	-5.4	-3.6
-250.0	5.1	10.5	15.5	11.9	-1.5	-3.9	-7.0	-7.2
-225.0	5.4	11.5	17.1	13.8	-1.5	-4.4	-7.9	-7.4
-200.0	5.9	12.7	19.6	16.4	-1.3	-4.1	-6.5	-4.3
-175.0	6.1	13.7	20.9	16.7	-1.8	-3.9	-6.0	-4.4
-150.0	6.5	14.6	22.3	17.8	-2.3	-4.1	-6.6	-4.3
-125.0	7.3	15.7	24.2	19.7	-2.0	-3.4	-3.2	-6.0
-100.0	7.6	16.7	25.6	19.1	-1.5	-2.1	1.7	15.9
-75.0	8.2	17.0	24.1	12.4	-1.3	-2.4	0.4	12.1
-50.0	8.2	17.5	24.0	10.5	-0.6	-2.2	-1.2	10.0
-25.0	8.9	18.6	25.3	8.9	*	*	*	*
0.0	8.1	18.1	24.0	4.0	*	*	*	*

TWIN GRID - LARGE LOOP EM LINE 5900E
 DATE 02 DEC. 1986 OPERATOR S.L. LOOP# 4 Nparm=4

STATION	112/37	337/37	1012/3	3037/3	FF1	FF2	FF3	FF4
-1275.0	-2.7	-4.9	-6.1	-6.5	*	*	*	*
-1250.0	-4.5	-8.5	-11.1	-14.0	5.1	11.2	17.2	28.2
-1225.0	-5.6	-11.1	-15.2	-20.9	4.1	9.6	15.9	26.7
-1200.0	-6.7	-13.5	-19.2	-27.8	3.7	8.9	14.9	23.5
-1175.0	-7.5	-15.7	-23.0	-33.8	3.5	8.3	13.2	18.8
-1150.0	-8.5	-17.8	-26.3	-38.4	3.1	7.7	11.7	14.9
-1125.0	-9.2	-19.7	-29.1	-42.0	3.1	7.4	10.6	12.1
-1100.0	-9.9	-21.5	-31.9	-45.1	3.3	6.6	7.4	7.0
-1075.0	-10.9	-23.4	-34.1	-47.4	2.8	5.5	4.9	4.3
-1050.0	-11.5	-24.4	-34.3	-46.7	2.5	5.6	6.9	8.8
-1025.0	-12.1	-26.0	-36.6	-50.1	2.6	5.8	8.1	10.9
-1000.0	-12.8	-27.4	-38.7	-52.8	2.1	5.3	6.4	8.5
-975.0	-13.4	-28.8	-40.3	-54.9	1.8	4.5	5.0	6.7
-950.0	-13.6	-29.9	-41.4	-56.5	2.2	3.8	4.4	5.4
-925.0	-14.4	-30.8	-42.6	-57.9	1.8	3.6	3.8	5.1
-900.0	-14.8	-31.7	-43.5	-58.9	1.3	3.1	2.7	4.1
-875.0	-15.0	-32.6	-44.3	-60.6	1.8	2.7	2.4	2.7
-850.0	-15.5	-33.0	-44.5	-60.3	1.8	2.9	3.8	4.1
-825.0	-16.1	-34.0	-45.7	-61.9	1.3	2.9	4.5	6.5
-800.0	-16.2	-34.5	-46.9	-63.1	1.5	3.0	5.1	9.3
-775.0	-16.7	-35.4	-47.8	-65.6	1.2	2.9	6.0	10.9
-750.0	-17.1	-36.1	-49.9	-68.7	0.4	2.5	4.8	8.9
-725.0	-17.0	-36.7	-50.8	-70.9	1.5	2.5	3.8	6.6
-700.0	-17.2	-37.3	-51.7	-72.3	2.3	2.8	3.8	5.4
-675.0	-18.4	-38.0	-52.8	-73.9	1.5	2.9	3.3	4.2
-650.0	-18.1	-38.8	-53.5	-74.7	1.8	2.3	2.6	3.3
-625.0	-19.0	-39.4	-54.3	-75.7	1.7	2.1	3.0	3.9
-600.0	-19.3	-39.7	-54.6	-76.2	0.9	2.5	4.4	6.4
-575.0	-19.5	-40.6	-56.2	-78.1	1.1	2.3	4.6	6.4
-550.0	-19.7	-41.0	-57.1	-80.2	1.6	1.8	3.8	3.5
-525.0	-20.2	-41.6	-58.3	-80.5	1.5	1.4	2.8	2.7
-500.0	-20.6	-41.8	-58.8	-81.3	1.2	2.3	3.1	3.9
-475.0	-20.8	-42.2	-59.4	-82.1	1.4	3.4	4.1	5.1
-450.0	-21.2	-43.5	-60.8	-83.6	1.3	2.4	3.7	4.3
-425.0	-21.6	-43.9	-61.5	-84.9	*	*	*	*
-400.0	-21.7	-44.2	-62.4	-85.1	*	*	*	*

TWIN GRID - LARGE LOOP EM					LINE 6000E			
DATE 01 DEC. 1986		OPERATOR D.W.,S.L. LOOP#3 LOOP 1100x750m Nparm=4						
STATION	112/37	337/37	1012/3	3037/3	FF1	FF2	FF3	FF4
0.0	9.0	18.6	23.5	1.7	*	*	*	*
25.0	10.6	21.4	25.3	-1.4	0.0	0.9	6.6	16.1
50.0	9.5	19.6	22.4	-4.3	-0.7	2.5	12.6	27.2
75.0	10.1	19.5	19.8	-11.5	-1.8	0.8	12.1	29.7
100.0	10.7	19.0	15.3	-21.4	-0.9	-0.3	5.3	16.7
125.0	10.7	19.3	14.8	-24.1	-0.7	-0.3	3.2	13.6
150.0	11.0	19.5	15.0	-25.5	-0.7	1.2	9.6	23.8
175.0	11.1	19.1	11.9	-33.6	-0.6	1.6	13.1	22.2
200.0	11.3	18.5	8.3	-39.8	-1.0	-0.4	9.1	11.8
225.0	11.4	18.5	5.5	-41.5	-1.6	-2.3	2.8	6.7
250.0	12.0	19.5	5.6	-43.7	-2.6	-1.6	1.4	3.5
275.0	12.3	19.8	5.4	-44.3	-2.7	1.3	3.3	2.1
300.0	13.7	19.8	4.3	-44.4	-0.5	3.3	5.1	5.8
325.0	13.3	18.2	3.4	-45.7	-0.6	1.2	6.5	8.7
350.0	13.2	18.1	1.2	-48.8	-1.3	0.1	7.3	7.7
375.0	14.4	18.7	0.0	-50.0	0.2	2.2	7.9	8.4
400.0	13.4	17.5	-2.7	-52.2	-0.2	2.6	7.1	10.0
425.0	14.0	17.1	-4.0	-55.0	0.0	3.2	9.6	10.8
450.0	14.0	16.5	-5.8	-57.2	1.6	5.8	14.3	11.0
475.0	13.4	14.9	-10.5	-60.8	3.9	7.6	13.3	7.8
500.0	13.0	12.9	-13.6	-62.4	7.0	7.1	11.4	5.8
525.0	10.5	10.9	-16.0	-63.4	*	*	*	*
550.0	8.9	9.8	-19.5	-65.6	*	*	*	*

TWIN GRID - LARGE LOOP EM LINE 6000E

DATE 01 DEC. 1986 OPERATOR D.W., S.L. LOOP#3 LOOP 1100x750m Nparm=4

STATION	112/37	337/37	1012/3	3037/3	FF1	FF2	FF3	FF4
-525.0	-1.2	-0.9	-0.8	-0.7	*	*	*	*
-500.0	-1.0	-0.2	0.5	1.9	-1.0	-2.6	-4.9	-6.1
-475.0	-0.7	0.5	1.8	3.2	-1.1	-2.6	-4.6	-3.8
-450.0	-0.5	1.0	2.8	4.1	-1.0	-2.5	-4.1	-2.1
-425.0	-0.1	1.9	4.1	4.8	-0.8	-2.1	-3.4	-0.8
-400.0	-0.1	2.1	4.6	4.6	-1.2	-2.6	-3.8	-0.9
-375.0	0.3	2.9	5.7	5.1	-1.4	-2.9	-4.1	-0.9
-350.0	0.7	3.7	6.8	5.2	-1.2	-2.7	-4.2	-1.1
-325.0	0.9	4.2	7.6	5.4	-1.3	-3.4	-5.3	-2.7
-300.0	1.3	5.1	9.1	6.0	-1.5	-3.9	-5.6	-3.0
-275.0	1.6	6.2	10.6	7.3	-1.4	-3.2	-4.2	0.3
-250.0	2.1	7.0	11.7	7.1	-1.2	-2.6	-3.3	2.0
-225.0	2.2	7.5	12.2	5.9	-1.6	-3.2	-5.1	-2.4
-200.0	2.7	8.3	13.4	6.5	-1.9	-4.1	-7.1	-6.5
-175.0	3.2	9.4	15.6	8.9	-1.6	-4.2	-6.1	-3.9
-150.0	3.6	10.5	17.1	10.0	-1.3	-3.7	-4.6	1.2
-125.0	3.9	11.4	18.0	9.3	-1.5	-3.0	-3.2	4.5
-100.0	4.2	12.2	19.3	8.4	-1.8	-2.1	0.0	9.2
-75.0	4.8	12.7	19.0	6.4	-1.4	-1.6	2.2	14.4
-50.0	5.1	13.0	18.3	2.1	-1.0	-1.9	1.6	14.0
-25.0	5.3	13.5	17.8	-1.7	*	*	*	*
0.0	5.6	14.1	17.9	-3.8	*	*	*	*

TWIN GRID - LARGE LOOP EM LINE 6000E
 DATE 02 DEC. 1986 OPERATOR S.L. LOOP# 4 Nparm=4
 STATION 112/77 777/77 1012/3 3037/3 FF1 FF2 FF3 FF4

-1175.0	-7.9	-16.6	-29.0	-48.8	3.7	7.2	10.0	10.0
-1150.0	-8.9	-19.1	-33.2	-53.5	2.9	7.5	12.0	11.6
-1125.0	-9.5	-20.8	-35.8	-55.9	2.6	6.6	9.8	8.2
-1100.0	-10.2	-22.4	-38.4	-58.0	2.6	6.3	8.1	6.1
-1075.0	-10.8	-24.1	-40.4	-59.6	2.5	5.5	6.1	4.0
-1050.0	-11.5	-25.4	-41.9	-60.4	2.2	4.8	4.8	3.6
-1025.0	-12.0	-26.6	-43.0	-61.2	2.0	3.8	3.6	3.7
-1000.0	-12.5	-27.7	-44.1	-62.4	2.4	3.8	3.2	2.9
-975.0	-13.0	-28.1	-44.4	-62.9	2.7	5.5	4.5	2.3
-950.0	-13.9	-30.0	-45.9	-63.6	2.4	6.5	4.2	1.7
-925.0	-14.3	-31.3	-47.1	-64.0	2.3	5.8	2.3	1.3
-900.0	-15.0	-33.3	-47.4	-64.2	2.2	3.7	1.9	1.5
-875.0	-15.5	-33.8	-47.9	-64.7	1.6	2.3	2.2	2.5
-850.0	-16.0	-34.5	-48.5	-65.0	1.1	2.3	2.4	4.3
-825.0	-16.1	-34.9	-49.0	-66.4	1.3	2.5	3.2	5.5
-800.0	-16.5	-35.7	-49.8	-67.6	1.7	2.7	4.4	6.9
-775.0	-16.9	-36.2	-50.9	-69.3	1.7	3.4	4.8	8.2
-750.0	-17.4	-37.1	-52.3	-71.6	1.4	3.3	4.0	6.8
-725.0	-17.7	-38.2	-53.2	-73.5	1.2	2.2	3.5	5.2
-700.0	-18.0	-38.4	-54.0	-74.2	1.1	2.2	3.6	5.3
-675.0	-18.3	-39.1	-55.0	-76.1	1.3	2.6	3.3	3.8
-650.0	-18.5	-39.7	-55.8	-76.9	2.1	2.8	3.1	2.3
-625.0	-19.1	-40.4	-56.5	-77.2	2.3	2.6	2.7	2.9
-600.0	-19.8	-41.2	-57.4	-78.1	1.2	1.7	2.0	3.0
-575.0	-20.1	-41.5	-57.6	-78.9	0.7	1.5	3.0	2.4
-550.0	-20.0	-41.8	-58.3	-79.4	1.3	2.1	3.5	2.4
-525.0	-20.6	-42.4	-59.7	-80.0	1.3	2.4	2.8	2.8
-500.0	-20.8	-43.0	-59.7	-80.7	1.2	2.3	3.4	3.8
-475.0	-21.1	-43.6	-61.1	-81.5	1.4	2.3	3.8	5.7
-450.0	-21.5	-44.1	-61.7	-83.0	1.3	2.3	3.6	5.6
-425.0	-21.8	-44.8	-62.9	-84.9	*	*	*	*
-400.0	-22.1	-45.2	-63.5	-85.2	*	*	*	*

TWIN GRID - LARGE LOOP EM LINE 6100E
DATE 01 DEC. 1986 OPERATOR S.L. LOOP#3 LOOP 1100x750m Nparm=4

STATION	112/37	337/37	1012/3	3037/3	FF1	FF2	FF3	FF4
-525.0	-1.2	-0.8	-0.6	-0.3	*	*	*	*
-500.0	-0.9	0.0	0.9	2.4	-1.1	-2.7	-5.6	-7.9
-475.0	-0.6	0.6	2.4	4.3	-1.0	-2.8	-5.0	-6.0
-450.0	-0.4	1.3	3.5	5.7	-1.2	-3.1	-5.0	-4.9
-425.0	-0.1	2.1	4.8	7.0	-1.6	-3.2	-5.2	-3.0
-400.0	0.3	2.9	6.1	7.9	-1.5	-3.1	-4.7	-0.1
-375.0	0.8	3.7	7.4	7.8	-1.0	-2.9	-3.6	3.0
-350.0	0.9	4.4	8.2	7.2	-1.2	-2.9	-3.1	4.4
-325.0	1.2	5.1	8.9	5.5	-1.8	-3.4	-3.8	2.8
-300.0	1.7	5.9	9.8	5.1	-1.7	-3.5	-4.6	0.8
-275.0	2.2	7.0	11.1	4.8	-1.2	-2.9	-4.4	0.6
-250.0	2.4	7.5	12.2	5.0	-1.4	-3.0	-3.7	1.6
-225.0	2.7	8.3	13.1	4.3	-1.9	-3.6	-3.3	1.7
-200.0	3.3	9.2	13.9	3.9	-1.7	-3.8	-3.9	0.5
-175.0	3.7	10.2	14.7	3.7	-1.4	-3.4	-4.6	0.0
-150.0	4.0	11.1	16.2	4.0	-1.2	-3.2	-3.7	1.4
-125.0	4.4	11.7	17.0	3.6	-1.5	-3.9	-3.9	1.1
-100.0	4.5	12.8	17.6	2.7	-2.1	-3.9	-5.2	-0.8
-75.0	5.4	13.9	19.5	3.8	-1.8	-2.7	-3.2	3.9
-50.0	5.6	14.5	20.3	3.3	-1.4	-1.8	0.1	10.0
-25.0	6.1	14.9	20.0	-0.7	-1.7	-2.8	2.2	13.5
0.0	6.3	15.3	19.7	-2.2	-2.2	-2.2	6.4	23.2
25.0	7.1	16.9	18.4	-8.7	-1.7	0.9	10.8	30.2
50.0	7.5	15.5	14.9	-17.4	-0.9	0.4	9.3	24.8
75.0	7.6	15.8	12.4	-23.7	-1.2	-1.4	5.3	16.5
100.0	7.9	16.2	11.6	-27.2	-1.3	0.1	6.1	15.1
125.0	8.4	16.5	10.4	-30.4	-0.6	1.9	9.2	17.7
150.0	8.4	15.4	7.5	-35.6	-0.4	1.4	10.1	19.5
175.0	8.5	15.4	5.3	-39.7	-0.6	0.8	8.5	19.1
200.0	8.7	15.1	2.5	-45.8	-1.1	0.1	4.0	11.0
225.0	8.8	14.9	1.8	-48.6	-2.3	-1.9	0.6	1.6
250.0	9.5	15.5	2.0	-47.9	-2.2	-2.2	0.4	-0.9
275.0	10.3	16.4	1.7	-48.1	-0.3	0.1	3.0	1.1
300.0	10.2	16.2	1.7	-47.5	0.5	2.1	7.9	6.7
325.0	9.9	15.6	-1.0	-49.6	0.4	3.6	9.6	10.7
350.0	10.1	14.9	-3.5	-52.7	0.8	4.3	7.4	10.5
375.0	9.6	13.3	-5.4	-55.1	0.3	3.0	7.1	10.6
400.0	9.6	12.9	-6.5	-57.7	0.0	2.3	9.7	9.3
425.0	9.8	12.3	-9.5	-60.7	0.3	2.9	10.3	6.2
450.0	9.4	11.6	-12.1	-61.4	0.0	3.8	9.9	6.6
475.0	9.7	10.7	-14.2	-63.2	0.5	4.3	10.0	7.7
500.0	9.5	9.4	-17.3	-65.5	0.8	3.4	8.0	5.4
525.0	9.1	8.6	-19.0	-66.8	*	*	*	*
550.0	9.3	8.1	-20.5	-67.3	*	*	*	*

TWIN GRID - LARGE LOOP EM LINE 6100E
 DATE 12/3/86 OPERATOR S.L. LOOP# 4 Nparm=4
 STATION 112/37 337/37 1012/3 3037/3 FF1 FF2 FF3 FF4

-1025.0	-11.3	-25.7	-45.8	-68.4	2.3	6.0	6.0	3.5
-1000.0	-11.9	-27.4	-47.4	-69.3	2.6	5.6	4.9	2.6
-975.0	-12.5	-28.6	-48.5	-69.9	2.9	5.6	4.3	1.9
-950.0	-13.3	-30.1	-49.6	-70.4	2.8	5.6	3.0	-0.6
-925.0	-14.0	-31.5	-50.6	-70.7	2.5	5.6	1.4	-2.8
-900.0	-14.6	-32.8	-50.5	-69.0	2.2	5.3	1.9	-0.7
-875.0	-15.2	-34.4	-51.1	-69.3	2.0	3.9	2.6	1.7
-850.0	-15.6	-35.2	-51.9	-69.7	1.8	2.6	2.1	2.8
-825.0	-16.2	-35.9	-52.3	-70.3	1.5	2.5	2.7	4.5
-800.0	-16.4	-36.3	-52.8	-71.5	1.8	3.3	4.1	5.8
-775.0	-16.9	-37.3	-54.1	-73.0	2.2	3.5	3.9	5.5
-750.0	-17.5	-38.2	-55.1	-74.6	1.9	2.8	2.7	4.3
-725.0	-18.0	-38.9	-55.7	-75.4	1.4	2.3	2.6	3.7
-700.0	-18.3	-39.4	-56.2	-76.5	1.2	2.4	3.1	3.8
-675.0	-18.6	-40.0	-57.2	-77.2	1.4	2.5	2.8	3.7
-650.0	-18.9	-40.7	-57.8	-78.5	1.8	2.3	2.6	3.0
-625.0	-19.4	-41.2	-58.4	-78.9	1.8	1.8	2.5	2.0
-600.0	-19.9	-41.8	-59.2	-79.8	1.5	1.6	1.5	0.1
-575.0	-20.2	-41.9	-59.5	-79.6	1.4	2.0	0.9	-0.1
-550.0	-20.6	-42.7	-59.6	-79.2	1.1	2.2	1.7	2.9
-525.0	-20.9	-43.0	-60.0	-80.1	0.7	2.2	2.6	4.4
-500.0	-21.0	-43.8	-60.8	-81.6	0.8	2.2	3.3	3.6
-475.0	-21.2	-44.1	-61.4	-82.1	2.0	2.1	3.8	3.2
-450.0	-21.5	-44.9	-62.7	-83.2	3.1	3.7	3.2	2.5
-425.0	-22.7	-45.1	-63.3	-83.7	*	*	*	*
-400.0	-23.1	-47.6	-64.0	-84.1	*	*	*	*

TWIN GRID - LARGE LOOP EM					LINE 6200E			
DATE 11/30/86		OPERATOR S.L.			LOOP#3	LOOP	1100x750m	Nparm=4
STATION	112/37	337/37	1012/3	3037/3	FF1	FF2	FF3	FF4
-525.0	-1.1	-0.6	-0.2	0.4	*	*	*	*
-500.0	-0.9	0.1	1.3	2.9	-0.9	-2.8	-5.1	-5.6
-475.0	-0.7	0.7	2.4	4.0	-1.4	-3.3	-5.4	-4.0
-450.0	-0.4	1.6	3.8	4.9	-1.6	-3.1	-5.0	-2.4
-425.0	0.2	2.5	5.3	6.0	-1.3	-2.8	-4.0	-0.4
-400.0	0.3	2.9	5.9	5.3	-1.2	-3.0	-3.6	0.7
-375.0	0.8	4.0	7.2	6.0	-1.1	-2.8	-2.8	3.8
-350.0	0.9	4.4	7.6	4.6	-1.3	-3.0	-2.2	6.5
-325.0	1.3	5.3	8.3	2.9	-1.7	-3.2	-2.8	5.1
-300.0	1.7	6.1	8.7	1.2	-1.7	-2.9	-3.7	2.0
-275.0	2.2	6.8	10.0	1.2	-1.4	-3.0	-3.4	1.5
-250.0	2.5	7.5	10.7	0.9	-1.5	-2.7	-3.1	2.9
-225.0	2.8	8.4	11.4	0.0	-1.8	-2.8	-3.9	2.2
-200.0	3.4	8.6	12.4	-0.8	-1.5	-4.0	-4.1	0.9
-175.0	3.7	10.1	13.6	-0.5	-1.5	-4.0	-3.9	1.3
-150.0	4.0	10.9	14.3	-1.2	-1.9	-3.5	-3.7	2.1
-125.0	4.6	11.8	15.6	-1.4	-1.8	-3.6	-4.0	1.3
-100.0	5.0	12.7	16.0	-2.4	-1.7	-4.2	-5.6	-3.3
-75.0	5.4	13.6	17.9	-1.5	-1.7	-4.8	-6.1	-5.2
-50.0	5.9	15.1	19.3	1.0	-1.5	-3.0	-2.6	5.4
-25.0	6.2	16.0	20.7	0.3	-1.5	-0.6	4.5	20.4
0.0	6.6	15.7	19.1	-6.2	-1.6	-0.5	9.4	26.5
25.0	7.0	16.0	16.4	-12.9	-1.5	-0.1	9.8	25.4
50.0	7.4	16.2	14.0	-19.5	-1.3	0.7	8.3	21.3
75.0	7.7	15.6	11.7	-25.0	-1.1	0.7	6.1	17.1
100.0	8.0	15.9	10.4	-28.7	-0.8	1.4	6.3	16.7
125.0	8.2	15.2	9.2	-32.9	-0.3	1.6	8.6	19.9
150.0	8.3	14.9	6.6	-37.5	-0.3	1.1	9.9	21.2
175.0	8.2	14.6	4.4	-44.0	-0.7	0.9	9.7	17.1
200.0	8.6	14.4	1.5	-47.6	-0.8	0.9	7.4	14.0
225.0	8.6	14.2	-0.2	-51.0	-1.1	2.5	4.3	10.4
250.0	9.0	13.9	-1.3	-54.6	-1.6	1.3	2.3	2.9
275.0	9.3	12.2	-1.7	-54.4	-1.7	-3.2	2.3	0.3
300.0	9.9	14.6	-2.1	-54.1	-0.7	0.0	6.8	4.8
325.0	10.1	14.7	-3.2	-55.2	0.7	5.9	11.8	8.8
350.0	9.8	12.1	-7.4	-58.1	1.3	5.7	10.8	10.1
375.0	9.5	11.3	-9.7	-60.0	1.3	3.2	7.8	9.2
400.0	9.1	9.8	-11.7	-63.4	0.3	0.8	6.8	5.1
425.0	8.9	10.4	-13.2	-63.9	-1.3	1.6	6.7	4.5
450.0	9.4	9.9	-15.0	-64.6	-0.1	4.8	11.1	7.8
475.0	9.9	8.7	-16.6	-67.2	2.7	5.6	15.3	9.3
500.0	8.5	6.8	-22.7	-69.1	2.5	4.6	14.0	9.8
525.0	8.1	6.2	-24.2	-72.0	*	*	*	*
550.0	7.8	4.7	-29.1	-74.1	*	*	*	*

TWIN GRID - LARGE LOOP EM LINE 6200E
 DATE 03 DEC. 1986 OPERATOR S.L. LOOP# 4 Nparm=4
 STATION 112/37 337/37 1012/3 3037/3 FF1 FF2 FF3 FF4

-950.0	-12.9	-29.7	-52.6	-76.0	3.4	7.7	6.2	1.0
-925.0	-13.5	-31.3	-53.9	-75.9	2.9	6.0	3.8	0.3
-900.0	-14.3	-32.8	-54.8	-76.2	3.1	5.9	3.2	0.0
-875.0	-15.0	-34.2	-55.5	-76.0	3.3	5.9	3.3	-0.1
-850.0	-15.9	-35.8	-56.4	-76.1	2.6	4.8	2.6	0.1
-825.0	-16.7	-37.1	-57.2	-76.0	1.5	3.5	1.2	0.3
-800.0	-16.8	-37.7	-57.3	-76.2	1.3	3.4	1.2	1.3
-775.0	-17.3	-38.7	-57.5	-76.2	1.4	2.9	2.0	2.5
-750.0	-17.5	-39.5	-58.2	-77.3	1.7	2.3	1.9	2.6
-725.0	-18.0	-39.8	-58.6	-77.6	1.8	2.4	1.6	2.8
-700.0	-18.5	-40.7	-59.0	-78.5	1.6	2.4	1.8	3.2
-675.0	-18.8	-41.0	-59.4	-79.2	1.8	3.0	3.0	4.2
-650.0	-19.3	-41.9	-60.0	-80.1	2.4	3.8	4.2	4.6
-625.0	-19.8	-42.8	-61.4	-81.8	2.8	3.7	3.3	3.0
-600.0	-20.7	-43.9	-62.2	-82.1	2.2	2.5	1.5	0.9
-575.0	-21.2	-44.5	-62.5	-82.8	1.5	1.5	0.1	-1.0
-550.0	-21.5	-44.7	-62.6	-82.0	0.9	2.0	0.4	0.0
-525.0	-21.9	-45.2	-62.2	-81.9	0.6	2.5	3.0	3.4
-500.0	-21.7	-46.0	-63.3	-82.9	1.6	2.3	4.4	4.8
-475.0	-22.3	-46.4	-64.5	-84.4	1.1	1.9	3.0	3.5
-450.0	-22.9	-47.1	-65.4	-85.2	0.3	1.3	1.8	2.1
-425.0	-22.2	-47.2	-65.4	-85.6	*	*	*	*
-400.0	-23.3	-47.6	-66.3	-86.1	*	*	*	*

TWIN GRID - LARGE LOOP EM					LINE 6300E			
DATE 11/30/86		OPERATOR S.L.			LOOP#3	LOOP	1100x750m	Nparm=4
STATION	112/37	337/37	1012/3	3037/3	FF1	FF2	FF3	FF4
-525.0	-1.3	-0.8	-0.6	-0.9	*	*	*	*
-500.0	-1.1	-0.2	0.7	1.2	-1.5	-3.9	-7.1	-7.7
-475.0	-0.7	0.8	2.6	3.6	-2.1	-4.8	-7.4	-3.9
-450.0	-0.2	2.1	4.6	4.4	-2.4	-4.9	-6.6	-1.1
-425.0	0.5	3.3	6.1	4.3	-1.9	-4.4	-5.6	-0.8
-400.0	1.0	4.5	7.7	4.8	-1.5	-3.7	-4.5	0.1
-375.0	1.2	5.3	8.6	4.7	-1.8	-3.4	-3.6	3.1
-350.0	1.8	6.2	9.7	4.3	-1.8	-3.4	-3.2	4.5
-325.0	2.2	7.0	10.2	2.1	-1.4	-3.2	-2.9	3.0
-300.0	2.6	7.9	11.3	2.4	-1.7	-3.1	-2.6	3.3
-275.0	2.8	8.5	11.5	1.0	-2.2	-3.3	-3.3	3.4
-250.0	3.7	9.5	12.6	0.2	-1.6	-3.0	-3.5	3.1
-225.0	3.9	10.2	13.5	-0.2	-1.4	-3.1	-2.5	4.5
-200.0	4.2	10.8	14.1	-1.7	-1.6	-3.5	-1.9	4.7
-175.0	4.8	12.0	14.5	-2.8	-1.5	-3.5	-2.8	2.3
-150.0	4.9	12.5	15.0	-3.8	-1.9	-3.8	-4.2	-0.1
-125.0	5.6	13.8	16.4	-3.0	-2.0	-3.1	-4.7	-0.9
-100.0	6.0	14.5	17.3	-3.5	-2.1	-3.2	-6.2	-4.1
-75.0	6.5	14.9	18.8	-2.4	-2.5	-5.5	-8.3	-8.2
-50.0	7.2	16.6	21.1	0.0	-2.4	-5.3	-6.6	-3.4
-25.0	7.8	18.3	23.3	2.3	-1.9	-2.8	1.5	15.6
0.0	8.3	18.5	23.2	-1.3	-1.7	-0.7	8.2	28.6
25.0	8.6	19.2	19.7	-12.0	-1.6	0.7	7.4	23.8
50.0	9.2	18.3	18.6	-15.6	-0.5	1.1	9.3	21.8
75.0	9.3	18.7	16.9	-21.5	0.1	1.0	12.6	24.6
100.0	9.0	17.7	12.1	-27.9	-0.8	1.1	10.0	23.5
125.0	9.4	18.3	10.8	-33.8	-1.4	2.3	8.7	20.3
150.0	9.7	17.0	8.2	-39.1	-1.2	2.3	8.8	15.4
175.0	10.1	16.7	6.0	-42.9	-0.8	0.2	6.5	10.3
200.0	10.2	16.3	4.2	-45.4	-0.3	-0.9	4.0	8.5
225.0	10.4	17.2	3.5	-46.9	0.6	-0.3	3.5	8.6
250.0	10.2	16.7	2.7	-49.9	-0.1	1.0	4.6	6.6
275.0	9.8	17.1	1.5	-51.0	-1.5	3.6	7.9	6.0
300.0	10.9	15.8	0.1	-52.4	0.1	6.2	14.8	9.1
325.0	10.6	14.4	-3.8	-54.5	1.6	5.9	15.7	14.8
350.0	10.0	12.3	-9.4	-58.0	1.2	3.1	9.6	14.6
375.0	9.9	12.0	-10.0	-63.7	0.3	2.5	7.6	6.2
400.0	9.5	11.6	-12.8	-63.4	-0.0	3.1	6.3	2.6
425.0	10.1	10.2	-14.2	-64.5	0.9	1.5	6.7	3.7
450.0	9.3	10.3	-14.9	-65.2	0.9	3.4	11.8	6.3
475.0	9.4	10.0	-18.8	-66.4	2.3	10.2	16.2	10.3
500.0	9.1	7.1	-22.1	-69.6	*	*	*	*
525.0	7.3	3.0	-27.8	-72.3	*	*	*	*

TWIN GRID - LARGE LOOP EM LINE 6300E
 DATE 03 DEC. 1986 OPERATOR S.L. LOOP# 4 Nparm=4
 STATION 112/37 337/37 1012/3 3037/3 FF1 FF2 FF3 FF4

-800.0	-17.1	-38.7	-60.8	-80.7	2.4	3.8	1.4	-0.9
-775.0	-17.5	-39.6	-61.3	-80.2	2.3	3.6	1.3	0.6
-750.0	-18.3	-40.5	-61.6	-80.6	2.0	3.6	1.1	1.3
-725.0	-18.6	-41.4	-61.8	-80.9	2.0	3.1	1.8	-0.2
-700.0	-19.2	-42.3	-62.2	-81.2	2.0	2.3	2.0	-1.4
-675.0	-19.7	-42.7	-63.0	-80.1	1.5	2.5	1.0	0.9
-650.0	-20.1	-43.3	-63.0	-80.6	1.3	3.5	1.0	3.8
-625.0	-20.3	-44.2	-63.2	-81.6	1.6	3.3	1.8	3.1
-600.0	-20.8	-45.3	-63.8	-82.9	1.6	1.9	1.5	1.1
-575.0	-21.2	-45.5	-64.2	-82.4	1.3	1.2	0.9	0.5
-550.0	-21.5	-45.9	-64.3	-83.2	1.2	1.1	1.1	-0.8
-525.0	-21.8	-46.1	-64.6	-82.6	1.6	1.8	2.2	0.6
-500.0	-22.1	-46.4	-65.0	-82.2	2.2	3.2	3.5	4.0
-475.0	-22.8	-47.4	-66.1	-84.2	2.0	3.2	3.9	1.9
-450.0	-23.3	-48.3	-67.0	-84.6	1.5	2.1	3.1	-0.6
-425.0	-23.6	-48.7	-68.0	-83.7	*	*	*	*
-400.0	-24.0	-49.1	-68.2	-84.5	*	*	*	*

TWIN GRID - LARGE LOOP EM LINE 6400E
 DATE 11/30/86 OPERATOR S.L. Nparm=4

STATION	112/37	337/37	1012/3	3037/3	FF1	FF2	FF3	FF4
75.0	8.9	18.5	18.1	-16.4	*	*	*	*
100.0	8.5	18.4	13.8	-24.2	-1.8	1.8	12.4	26.2
125.0	9.3	18.0	11.3	-30.5	-1.1	2.5	11.5	23.5
150.0	9.9	17.1	8.2	-36.3	0.7	1.9	10.8	19.6
175.0	9.0	16.8	5.4	-41.9	-1.0	1.1	7.9	13.6
200.0	9.5	16.4	3.3	-44.5	-2.4	-0.1	3.4	8.6
225.0	10.4	16.4	2.4	-47.3	-1.1	-0.8	1.0	6.1
250.0	10.5	16.9	2.9	-47.7	-0.8	0.8	3.7	7.6
275.0	10.5	16.7	1.8	-50.2	-0.6	4.1	9.7	9.9
300.0	11.2	15.8	-0.2	-52.4	1.3	6.2	13.6	10.1
325.0	10.4	13.7	-4.8	-55.4	1.7	6.0	13.4	12.3
350.0	10.0	12.6	-7.2	-57.3	0.9	5.1	12.8	13.5
375.0	9.9	10.9	-11.2	-62.8	0.8	3.0	10.0	8.6
400.0	9.6	10.3	-13.6	-63.4	0.7	1.4	7.0	6.5
425.0	9.5	10.2	-14.8	-65.3	0.7	2.8	8.7	8.7
450.0	9.3	9.6	-17.0	-67.4	0.9	4.9	12.2	10.4
475.0	9.1	8.1	-20.1	-70.0	1.1	6.3	14.6	12.1
500.0	8.8	6.8	-23.9	-73.1	1.0	6.4	14.8	12.3
525.0	8.5	4.6	-27.8	-76.4	*	*	*	*
550.0	8.4	3.9	-31.0	-79.0	*	*	*	*

TWIN GRID - LARGE LOOP EM LINE 6400E
 DATE 03 DEC. 1986 OPERATOR N.M. LOOP# 4 Nparm=4
 STATION 112/37 337/37 1012/3 3037/3 FF1 FF2 FF3 FF4

-700.0	-17.2	-42.0	-64.9	-83.6	1.6	3.5	-0.2	-1.2
-675.0	-17.5	-42.8	-64.7	-83.3	2.0	4.0	1.1	0.7
-650.0	-18.0	-43.8	-64.9	-83.5	2.2	4.5	2.7	2.0
-625.0	-18.7	-45.0	-65.8	-84.1	1.8	3.4	1.9	2.1
-600.0	-19.0	-46.1	-66.5	-84.7	1.5	1.6	-0.3	0.3
-575.0	-19.5	-46.1	-66.1	-85.0	1.5	1.5	-0.4	-0.7
-550.0	-19.7	-46.6	-65.9	-84.1	1.8	1.7	1.4	1.7
-525.0	-20.3	-47.1	-66.3	-84.9	1.7	1.4	2.4	3.0
-500.0	-20.7	-47.3	-67.1	-85.9	1.3	1.4	1.8	2.1
-475.0	-21.0	-47.8	-67.5	-86.1	1.0	1.5	2.4	2.2
-450.0	-21.3	-48.0	-67.7	-86.8	1.4	1.7	5.0	3.3
-425.0	-21.4	-48.6	-69.3	-87.4	*	*	*	*
-400.0	-22.3	-48.9	-70.9	-88.8	*	*	*	*

TWIN GRID - LARGE LOOP EM LINE 65+00E
 DATE 10/25/86 OPERATOR D.M.W. Nparm=4

ELEVATION	112/37	337/37	1012/3	3037/3	FF1	FF2	FF3	FF4
-550.0	1.6	1.8	2.4	3.1	*	*	*	*
-525.0	1.6	2.1	3.0	3.5	-0.3	-1.3	-2.2	0.5
-500.0	1.7	2.4	3.6	3.5	-0.3	-1.2	-1.4	4.2
-475.0	1.8	2.8	4.0	2.6	-0.3	-0.9	-0.5	8.5
-450.0	1.8	2.9	4.0	0.2	-0.5	-1.1	-0.5	10.1
-425.0	2.0	3.2	4.1	-2.6	-0.6	-1.7	-1.3	8.0
-400.0	2.1	3.6	4.4	-4.7	-0.7	-1.9	-1.8	5.7
-375.0	2.3	4.2	5.0	-5.7	-0.7	-1.8	-1.6	5.6
-350.0	2.5	4.5	5.3	-7.3	-0.5	-1.9	-1.4	6.1
-325.0	2.6	5.1	5.7	-8.7	-0.6	-1.7	-1.3	6.6
-300.0	2.7	5.5	6.0	-10.4	-0.8	-1.6	-1.3	6.4
-275.0	3.0	5.8	6.3	-12.2	-0.5	-1.9	-1.1	5.8
-250.0	3.1	6.4	6.7	-13.3	-0.4	-1.6	-0.7	5.7
-225.0	3.1	6.8	6.7	-15.1	-0.8	-1.7	-1.6	4.2
-200.0	3.4	7.0	7.0	-16.1	-0.8	-2.4	-2.4	3.4
-175.0	3.6	7.9	8.0	-16.5	-1.2	-2.0	-1.6	4.6
-150.0	3.7	8.3	8.1	-18.1	-2.0	-2.0	-2.4	3.2
-125.0	4.5	8.6	8.5	-19.1	-0.8	-2.6	-2.9	2.1
-100.0	4.8	9.6	10.0	-18.7	0.7	-2.0	-2.1	3.3
-75.0	4.2	9.9	9.5	-20.6	-0.1	-2.7	-4.6	-0.3
-50.0	4.4	10.3	11.1	-20.5	-1.5	-4.6	-6.6	-4.2
-25.0	4.7	11.9	13.0	-18.5	-1.7	-3.7	-4.1	-0.6
0.0	5.4	12.9	14.2	-18.4	-0.9	-1.6	-0.8	4.5
25.0	5.4	13.0	14.0	-20.0	-0.5	-0.7	2.6	9.7
50.0	5.6	13.4	14.0	-21.4	0.0	1.9	10.0	19.9
75.0	5.7	13.2	11.6	-26.7	0.1	3.5	15.1	27.1
100.0	5.3	11.3	6.4	-34.6	-0.6	1.5	12.5	24.8
125.0	5.9	11.8	4.1	-40.6	-0.4	0.6	8.9	17.7
150.0	5.7	11.2	1.4	-45.5	-0.7	0.3	6.3	11.0
175.0	5.9	11.3	0.2	-47.4	-1.5	0.2	4.8	9.0
200.0	6.4	11.4	-1.0	-49.7	-0.7	0.4	2.6	7.0
225.0	6.7	10.9	-2.2	-52.2	0.9	1.0	3.5	6.8
250.0	6.3	11.4	-1.2	-51.9	1.0	2.6	8.2	10.1
275.0	5.9	9.9	-5.5	-56.8	-0.2	2.2	9.0	9.3
300.0	6.1	9.8	-6.1	-57.4	-0.5	2.1	9.8	9.4
325.0	6.3	9.3	-9.6	-60.6	-0.5	2.1	8.3	9.6
350.0	6.2	8.3	-11.8	-63.0	-0.3	2.0	6.0	8.3
375.0	6.7	8.7	-12.2	-64.6	0.5	3.9	9.2	8.7
400.0	6.1	6.9	-15.2	-67.3	1.1	4.4	12.0	8.2
425.0	6.3	6.2	-18.0	-69.0	1.9	4.9	13.2	9.1
450.0	5.4	5.0	-21.4	-71.1	1.6	7.5	16.0	12.6
475.0	5.1	3.2	-25.0	-74.3	0.6	9.3	17.3	7.9
500.0	5.0	0.5	-30.4	-78.4	0.5	8.1	15.5	4.8
525.0	4.9	-1.6	-33.3	-74.9	*	*	*	*
550.0	4.7	-2.8	-37.6	-82.6	*	*	*	*

7. TWIN GRID - LARGE LOOP EM LINE 6500E
 DATE 03 DEC. 1986 OPERATOR N.M. LOOP# 4 Nparm=4
 STATION 112/37 337/37 1012/3 3037/3 FF1 FF2 FF3 FF4

-600.0	-20.4	-47.9	-70.1	-88.0	2.8	2.8	1.2	0.0
-575.0	-21.1	-48.8	-70.4	-88.2	1.6	1.9	0.9	-2.3
-550.0	-21.5	-49.1	-70.5	-86.5	0.7	1.2	0.9	0.5
-525.0	-21.6	-49.5	-70.9	-87.4	0.9	1.4	0.8	2.9
-500.0	-21.7	-49.6	-70.9	-87.8	1.4	2.3	1.2	3.3
-475.0	-22.3	-50.4	-71.3	-89.0	1.2	2.7	1.4	2.7
-450.0	-22.4	-51.0	-71.7	-89.5	1.3	2.8	0.9	2.5
-425.0	-22.8	-51.7	-71.9	-90.0	*	*	*	*
-400.0	-23.2	-52.5	-72.0	-91.0	*	*	*	*

TWIN GRID - LARGE LOOP EM LINE 88+00E

DATE 10/25/86 OPERATOR D.M.W. Nparm=4

STATION	112/37	337/37	1012/3	3037/3	FF1	FF2	FF3	FF4
-525.0	1.6	2.1	3.4	5.2	*	*	*	*
-500.0	1.7	2.4	4.1	5.8	-0.2	-1.2	-2.3	-0.4
-475.0	1.7	2.8	4.9	6.9	-0.3	0.2	-0.7	6.5
-450.0	1.8	2.9	4.9	4.5	-0.4	0.4	1.0	13.6
-425.0	1.9	2.1	4.8	1.7	-0.4	-1.9	1.2	15.3
-400.0	2.0	3.2	4.0	-3.9	-0.5	-2.5	-0.3	10.9
-375.0	2.1	3.7	4.5	-5.2	-0.6	-1.8	-1.0	8.2
-350.0	2.3	4.1	4.6	-7.9	-0.7	-2.0	-1.5	6.3
-325.0	2.4	4.6	4.9	-9.4	-1.0	-2.2	-2.2	4.0
-300.0	2.7	5.2	5.7	-10.0	-1.0	-2.1	-2.1	4.5
-275.0	3.0	5.7	6.0	-11.3	-0.7	-1.7	-1.1	6.5
-250.0	3.1	6.2	6.7	-12.6	-0.5	-1.2	0.0	7.8
-225.0	3.3	6.4	6.1	-15.2	-0.4	-1.4	-1.1	5.7
-200.0	3.3	6.7	6.6	-16.5	-0.6	-1.9	-1.8	4.0
-175.0	3.5	7.3	7.3	-17.0	-0.6	-1.9	-1.3	4.4
-150.0	3.7	7.7	7.2	-18.7	-0.9	-2.4	-2.2	3.9
-125.0	3.7	8.2	8.0	-19.2	-1.4	-3.3	-3.0	3.1
-100.0	4.4	9.2	8.7	-20.4	-0.7	-2.8	-2.2	2.2
-75.0	4.4	10.0	9.5	-20.6	-0.5	-2.3	-2.5	1.0
-50.0	4.4	10.2	9.4	-21.2	-0.9	-2.6	-3.2	1.3
-25.0	4.9	11.3	11.3	-20.8	-0.7	-2.0	-1.6	3.4
0.0	4.8	11.5	10.8	-22.3	-0.5	-2.2	-2.5	3.1
25.0	5.2	12.0	11.5	-23.1	-0.2	-2.0	-1.5	4.6
50.0	5.0	13.0	13.1	-23.1	-0.3	-0.8	6.3	14.1
75.0	5.2	12.5	10.7	-26.9	-0.4	1.5	12.2	22.2
100.0	5.3	13.3	7.6	-33.4	-0.6	4.8	13.7	23.8
125.0	5.3	10.7	4.0	-38.8	-1.1	3.0	10.7	19.9
150.0	5.8	10.3	0.6	-45.3	-0.8	-0.2	5.2	12.1
175.0	5.9	10.7	0.3	-46.8	-0.1	0.5	4.6	8.9
200.0	6.0	10.5	-0.9	-49.4	0.2	0.6	5.0	7.4
225.0	5.8	10.0	-2.8	-51.6	-0.5	-0.5	2.5	4.6
250.0	5.9	10.6	-2.8	-52.0	-1.0	0.0	3.6	6.9
275.0	6.4	10.4	-3.4	-53.6	-0.3	1.2	7.8	10.6
300.0	6.3	10.2	-5.8	-56.9	0.2	2.2	9.0	11.1
325.0	6.3	9.6	-8.2	-59.3	0.3	3.6	9.3	10.6
350.0	6.2	8.8	-10.0	-62.3	0.4	4.5	9.6	9.3
375.0	6.1	7.4	-13.3	-64.5	-0.1	3.9	7.2	6.6
400.0	6.0	6.5	-14.5	-66.4	-0.4	3.2	7.3	5.1
425.0	6.4	5.8	-16.0	-67.0	0.6	5.0	12.7	9.1
450.0	6.1	4.9	-19.1	-69.0	1.5	7.5	17.8	14.7
475.0	5.7	2.4	-24.1	-73.5	1.8	8.1	19.6	15.4
500.0	5.3	0.8	-28.8	-77.2	1.7	7.8	17.9	8.6
525.0	4.7	-1.6	-34.0	-80.7	*	*	*	*
550.0	4.6	-3.0	-36.8	-78.6	*	*	*	*

TWIN GRID - LARGE LOOP EM LINE 6600E
 DATE 03 DEC. 1986 OPERATOR N.M. LOOP# 4 Nparm=4
 STATION 112/37 337/37 1012/3 3037/3 FF1 FF2 FF3 FF4

-600.0	-21.2	-51.0	-73.4	-88.6	2.1	3.3	2.5	1.8
-575.0	-21.8	-51.9	-74.2	-88.0	1.2	1.9	1.5	4.1
-550.0	-22.0	-52.2	-74.4	-90.0	1.1	1.4	0.8	3.7
-525.0	-22.2	-52.6	-74.7	-90.7	0.5	1.1	0.0	1.3
-500.0	-22.7	-52.9	-74.7	-91.0	0.6	0.9	-0.6	-2.3
-475.0	-22.0	-53.0	-74.4	-91.0	2.9	1.1	-0.6	-4.9
-450.0	-23.5	-53.4	-74.4	-88.4	2.9	1.0	-0.2	-0.2
-425.0	-24.1	-53.6	-74.1	-88.7	*	*	*	*
-400.0	-24.3	-53.8	-74.5	-90.5	*	*	*	*

TWIN GRID - LARGE LOG EN LINE 87+00E
 DATE 10/25/86 OPERATOR D.M.W. Nparm=4

TATION	112/37	337/37	1012/3	3037/3	FF1	FF2	FF3	FF4
-525.0	1.9	2.5	3.3	5.4	*	*	*	*
-500.0	2.0	2.7	3.9	5.8	-0.2	-1.2	-3.1	-3.9
-475.0	2.0	3.0	4.8	7.5	-0.3	-1.3	-2.2	0.7
-450.0	2.1	3.4	5.5	7.6	-0.2	-1.0	-0.2	10.9
-425.0	2.2	3.6	5.4	5.0	-0.2	-0.8	1.0	17.5
-400.0	2.1	3.8	5.1	-0.8	-0.6	-1.0	0.8	14.5
-375.0	2.4	4.0	4.8	-4.1	-0.6	-1.5	-0.5	8.8
-350.0	2.5	4.4	4.9	-6.2	-0.5	-1.5	-1.4	6.5
-325.0	2.6	4.9	5.5	-7.5	-0.5	-1.1	-0.7	6.9
-300.0	2.8	5.0	5.6	-9.3	-0.4	-1.1	0.3	7.8
-275.0	2.8	5.4	5.5	-11.3	-0.6	-1.3	0.2	7.4
-250.0	3.0	5.6	5.3	-13.3	-0.6	-1.5	-0.4	6.8
-225.0	3.2	6.1	5.6	-14.7	-0.3	-1.6	-0.5	7.0
-200.0	3.2	6.4	5.6	-16.7	-0.4	-2.1	-1.6	5.3
-175.0	3.3	6.9	5.8	-18.3	-0.9	-2.5	-2.7	3.4
-150.0	3.5	7.7	7.0	-18.4	-0.9	-1.6	-1.3	4.5
-125.0	3.9	8.1	7.1	-20.0	-0.3	-0.8	-0.1	5.2
-100.0	3.8	8.1	7.0	-21.2	-0.5	-1.8	-0.9	4.6
-75.0	3.9	8.5	7.2	-22.4	-0.9	-2.3	-0.8	5.1
-50.0	4.3	9.5	7.8	-23.4	-0.7	-1.7	-0.2	5.3
-25.0	4.3	9.4	7.2	-25.3	-0.6	-1.7	-0.7	4.3
0.0	4.6	10.3	8.0	-25.8	-0.8	-2.0	-1.5	3.1
25.0	4.6	10.3	7.7	-27.2	-1.2	-2.3	-1.9	2.6
50.0	5.1	11.4	9.0	-27.0	-0.7	-1.1	2.0	8.1
75.0	5.3	11.5	8.6	-28.6	0.5	1.1	7.9	16.8
100.0	5.1	11.3	6.1	-33.7	0.4	2.3	10.0	19.4
125.0	4.8	10.5	3.6	-38.7	-0.6	1.8	9.1	16.7
150.0	5.2	10.0	1.1	-43.0	-0.4	0.7	7.6	13.3
175.0	5.3	10.0	-0.5	-46.1	-0.2	-0.1	5.3	9.3
200.0	5.1	9.8	-2.4	-48.9	-0.6	0.7	4.4	8.0
225.0	5.6	10.3	-2.3	-49.5	-0.1	1.8	5.5	9.1
250.0	5.4	8.8	-5.0	-53.5	-0.3	0.9	5.3	8.0
275.0	5.4	9.5	-5.2	-54.0	-1.0	0.8	5.0	7.0
300.0	5.9	8.7	-7.4	-57.0	-0.2	1.6	5.2	6.7
325.0	5.9	8.8	-7.8	-57.5	-0.1	1.3	6.3	7.7
350.0	5.6	7.8	-10.0	-60.2	-0.7	0.9	6.9	7.6
375.0	6.3	8.4	-11.5	-62.0	0.5	2.6	6.2	5.8
400.0	5.9	7.3	-13.2	-63.3	1.3	4.0	6.3	5.4
425.0	5.5	6.3	-14.5	-64.7	0.7	3.7	9.8	7.6
450.0	5.4	5.4	-16.5	-66.0	1.0	5.7	17.0	13.4
475.0	5.3	4.5	-21.0	-69.6	1.9	9.6	22.1	17.8
500.0	4.6	1.5	-27.0	-74.5	1.9	9.9	21.0	15.9
525.0	4.2	-1.2	-32.6	-78.9	*	*	*	*
550.0	3.8	-2.7	-36.4	-81.1	*	*	*	*

TWIN GRID - LARGE LOOP EM LINE 6700E
 DATE 02 DEC. 1986 OPERATOR N.M. LOOP# 4 Nparm=4
 STATION 112/37 337/37 1012/3 3037/3 FF1 FF2 FF3 FF4

-675.0	-19.0	-51.3	-78.0	-90.0	4.1	9.1	0.9	4.7
-650.0	-20.2	-56.6	-78.0	-90.0	3.7	1.0	0.1	-3.9
-625.0	-21.0	-53.8	-78.5	-87.7	3.2	0.0	-1.4	-0.4
-600.0	-21.9	-55.1	-77.6	-88.4	2.9	2.6	-1.0	2.8
-575.0	-22.5	-55.3	-77.5	-88.9	2.8	2.1	0.2	3.7
-550.0	-23.3	-56.2	-77.6	-90.0	2.4	1.7	0.2	3.1
-525.0	-23.9	-56.3	-77.7	-91.0	1.7	1.4	-1.0	-2.3
-500.0	-24.3	-56.9	-77.6	-91.0	1.4	0.8	-2.5	-4.3
-475.0	-24.6	-57.0	-76.7	-87.7	1.6	0.5	-1.7	2.3
-450.0	-25.0	-57.0	-76.1	-90.0	1.7	1.3	0.9	4.3
-425.0	-25.5	-57.4	-76.5	-91.0	*	*	*	*
-400.0	-25.8	-57.9	-77.2	-91.0	*	*	*	*

TWIN GRID - LARGE LOOP EM LINE 88+002

DATE 10/24/86 OPERATOR D.M.W. Nparm=4

	112/37	337/37	1012/3	3037/3	FF1	FF2	FF3	FF4
-525.0	1.8	2.2	3.1	5.3	*	*	*	*
-500.0	1.8	2.4	4.0	7.5	-0.3	-1.4	-3.6	-5.9
-475.0	1.9	2.8	5.0	9.4	-0.3	-1.3	-2.5	0.5
-450.0	2.0	3.2	5.7	9.3	-0.3	-1.0	-0.2	12.8
-425.0	2.0	3.3	5.8	7.1	-0.5	-1.1	1.6	22.1
-400.0	2.2	3.7	5.1	-1.2	-0.5	-1.0	1.5	17.7
-375.0	2.3	3.9	4.8	-4.5	-0.5	-1.0	0.2	10.3
-350.0	2.4	4.1	4.6	-7.3	-0.6	-1.5	-1.0	7.2
-325.0	2.6	4.5	5.1	-8.7	-0.5	-1.6	-0.9	6.6
-300.0	2.7	5.0	5.3	-10.3	-0.6	-1.3	-0.4	7.3
-275.0	2.8	5.2	5.3	-12.3	-0.7	-1.3	-0.4	7.4
-250.0	3.1	5.6	5.5	-14.0	-0.3	-1.6	0.2	7.9
-225.0	3.1	5.9	5.5	-16.0	-0.3	-1.7	0.3	7.4
-200.0	3.1	6.5	5.1	-18.2	-0.7	-1.5	-1.1	5.2
-175.0	3.4	6.7	5.6	-19.2	-0.6	-1.4	-1.3	4.8
-150.0	3.5	7.2	6.1	-20.2	-0.4	-1.5	-0.7	5.6
-125.0	3.6	7.4	5.9	-22.0	-0.3	-1.5	-0.5	5.6
-100.0	3.7	8.0	6.5	-23.0	-0.8	-1.5	-0.1	5.4
-75.0	3.7	8.1	6.0	-24.8	-1.3	-1.8	-0.2	5.0
-50.0	4.4	8.8	6.5	-25.6	-0.9	-1.8	-1.3	2.9
-25.0	4.3	9.1	6.2	-27.2	-0.7	-1.7	-1.9	2.1
0.0	4.7	9.6	7.6	-26.1	-0.5	-1.0	1.9	8.1
25.0	4.7	10.0	7.0	-28.8	-0.1	0.0	5.8	13.2
50.0	4.8	9.7	4.9	-32.6	-0.1	0.0	5.3	12.8
75.0	4.7	9.9	3.9	-35.5	-0.6	0.1	4.8	11.9
100.0	4.9	9.8	2.7	-38.7	-0.6	1.1	6.1	12.1
125.0	5.2	9.7	1.3	-41.3	-0.3	1.6	6.2	11.9
150.0	5.0	8.9	-0.8	-45.0	-0.3	0.7	3.9	8.4
175.0	5.4	9.0	-1.4	-46.9	0.1	0.5	4.2	7.3
200.0	5.1	8.9	-2.0	-47.8	0.3	0.9	6.8	10.0
225.0	5.2	8.5	-4.4	-51.4	-0.7	-0.1	4.8	7.9
250.0	5.0	8.5	-5.8	-53.3	-1.5	-0.8	2.0	4.7
275.0	6.0	9.0	-5.4	-53.8	0.0	0.1	3.7	5.8
300.0	5.7	8.8	-6.8	-55.6	0.4	1.2	5.4	6.2
325.0	5.3	8.6	-8.1	-57.3	-0.5	2.2	7.8	7.4
350.0	6.0	8.0	-9.5	-58.3	0.2	3.1	8.9	8.9
375.0	5.5	7.2	-13.2	-62.0	0.6	3.9	7.3	7.9
400.0	5.6	6.3	-13.3	-62.5	0.1	3.7	9.2	8.8
425.0	5.3	5.0	-16.7	-65.7	-0.5	3.7	11.6	10.4
450.0	5.7	4.8	-19.0	-67.6	0.9	6.7	15.5	12.9
475.0	5.7	2.8	-22.6	-71.0	3.1	9.2	20.1	15.4
500.0	4.4	0.3	-28.6	-75.2	1.9	7.5	17.2	12.5
525.0	3.9	-1.9	-33.1	-78.8	*	*	*	*
550.0	4.3	-2.5	-35.3	-79.9	*	*	*	*

TWIN GRID - LARGE LOOP EM LINE 6800E
 DATE 02 DEC. 1986 OPERATOR N.M. LOOP# 4 LOOP 1100x600m. Nparm=4
 STATION 112/37 337/37 1012/3 3037/3 FF1 FF2 FF3 FF4

-725.0	-15.9	-50.0	-81.7	-92.0	7.1	8.7	2.9	2.0
-700.0	-17.8	-52.0	-82.4	-92.0	6.6	8.1	1.7	2.0
-675.0	-19.4	-54.2	-82.9	-93.0	5.5	6.9	0.1	0.0
-650.0	-20.9	-55.9	-82.9	-93.0	4.3	6.0	-1.1	-2.0
-625.0	-21.8	-57.2	-82.5	-92.0	3.9	5.5	-1.0	-1.0
-600.0	-22.8	-58.9	-82.2	-92.0	4.0	3.8	-0.9	-2.0
-575.0	-23.8	-59.7	-82.2	-92.0	3.7	2.6	-2.1	-5.0
-550.0	-24.8	-60.2	-81.6	-90.0	3.2	2.5	-2.8	-4.0
-525.0	-25.5	-61.0	-80.7	-89.0	2.7	1.7	-2.2	0.0
-500.0	-26.3	-61.4	-80.3	-89.0	1.2	-1.3	-2.9	2.0
-475.0	-26.7	-61.5	-79.8	-90.0	-0.5	-3.4	-3.6	2.0
-450.0	-26.3	-59.6	-78.3	-90.0	0.3	-1.2	-1.4	2.5
-425.0	-26.2	-59.9	-78.2	-91.0	*	*	*	*
-400.0	-27.1	-60.0	-78.5	-91.5	*	*	*	*

E	ATION	112/37	337/37	1012/3	3037/3	FF1	FF2	FF3	FF4
-525.0		1.8	2.3	3.4	6.7	*	*	*	*
-500.0		1.9	2.6	4.5	9.5	-0.4	-1.3	-3.9	-7.2
-475.0		2.0	3.0	5.5	11.1	-0.6	-1.3	-2.6	0.4
-450.0		2.1	3.2	6.3	12.3	-0.6	-1.3	-0.2	13.5
-425.0		2.4	3.7	6.3	7.9	-0.2	-0.8	1.8	20.6
-400.0		2.3	3.8	5.7	2.0	-0.3	-0.8	1.2	16.4
-375.0		2.4	3.9	5.1	-2.4	-0.6	-1.4	-0.1	11.2
-350.0		2.6	4.4	5.7	-4.1	-0.5	-1.4	0.3	10.9
-325.0		2.7	4.7	5.2	-7.5	-0.4	-1.0	0.7	10.5
-300.0		2.8	5.0	5.3	-9.9	-0.4	-0.9	0.5	9.0
-275.0		2.9	5.1	4.9	-12.2	-0.6	-1.4	-0.5	8.0
-250.0		3.0	5.5	5.1	-14.2	-0.7	-1.4	-0.4	7.8
-225.0		3.3	6.0	5.6	-15.9	-0.4	-1.2	0.6	7.9
-200.0		3.3	6.0	4.8	-18.3	-0.3	-1.6	-0.1	7.1
-175.0		3.4	6.7	5.3	-19.7	-0.6	-1.7	-0.9	6.1
-150.0		3.5	6.9	5.2	-21.6	-0.8	-1.6	-0.6	5.7
-125.0		3.8	7.5	5.8	-22.5	-0.6	-1.4	0.0	5.6
-100.0		3.9	7.7	5.3	-24.5	-0.5	-0.9	0.3	5.2
-75.0		4.0	8.1	5.7	-25.2	-0.9	-1.3	-1.0	3.8
-50.0		4.2	8.0	5.1	-27.0	-0.7	-2.0	-1.8	3.8
-25.0		4.6	9.1	6.9	-26.5	-0.0	-1.0	2.1	8.7
0.0		4.3	9.0	5.7	-29.5	-0.3	-0.1	5.1	11.9
25.0		4.5	9.1	4.2	-32.7	-0.9	0.3	5.2	11.9
50.0		4.7	9.1	3.3	-35.2	-0.3	1.7	7.8	14.3
75.0		5.0	8.7	1.4	-38.9	0.6	1.6	7.8	13.7
100.0		4.5	7.8	-1.7	-43.3	0.1	-0.2	4.1	9.1
125.0		4.6	8.4	-1.4	-44.5	-0.8	-0.6	2.7	6.4
150.0		4.8	8.3	-3.0	-46.8	-0.9	-0.8	0.5	3.9
175.0		5.1	8.5	-2.8	-47.4	-0.7	-1.0	-0.1	3.4
200.0		5.2	9.0	-2.1	-47.8	-0.5	-0.2	3.2	5.9
225.0		5.4	8.8	-3.6	-49.8	-0.1	0.1	4.7	6.9
250.0		5.4	8.9	-4.5	-51.3	0.4	0.6	4.9	6.9
275.0		5.3	8.8	-5.9	-53.2	-0.2	0.9	4.5	6.3
300.0		5.1	8.3	-7.1	-54.8	-0.3	3.0	7.1	8.2
325.0		5.8	8.5	-7.8	-56.0	0.7	5.3	11.3	10.9
350.0		4.9	5.6	-12.3	-60.2	0.3	2.2	8.6	8.1
375.0		5.3	5.9	-13.9	-61.5	-0.1	1.0	5.9	6.3
400.0		5.1	6.0	-14.8	-62.8	0.4	4.7	10.9	10.6
425.0		5.2	4.5	-17.3	-65.2	1.3	6.6	15.1	13.3
450.0		4.8	2.7	-22.3	-69.7	1.1	6.7	14.0	11.0
475.0		4.2	1.2	-24.9	-71.6	-0.9	6.2	13.6	10.3
500.0		4.7	-0.7	-28.7	-74.3	0.6	5.8	14.2	9.7
525.0		5.2	-1.6	-32.1	-77.3	*	*	*	*
550.0		3.1	-3.7	-35.7	-78.3	*	*	*	*

TWIN GRID - LARGE LOOP EM LINE 6900E
 DATE 02 DEC. 1986 OPERATOR N.M. LOOP# 4 LOOP 1100x600m. Nparm=4
 STATION 112/37 337/37 1012/3 3037/3 FF1 FF2 FF3 FF4

-600.0	-23.0	-61.6	-86.6	-92.0	5.1	4.6	-2.1	-1.5
-575.0	-24.5	-62.8	-85.3	-91.5	4.3	3.2	-3.5	-1.5
-550.0	-25.6	-63.7	-84.7	-91.0	2.8	2.2	-3.5	-0.5
-525.0	-26.2	-63.9	-83.7	-91.0	2.5	2.2	-4.2	0.0
-500.0	-26.7	-64.8	-82.8	-91.0	2.9	1.1	-4.1	0.0
-475.0	-27.6	-65.0	-81.4	-91.0	2.6	0.0	-2.2	0.0
-450.0	-28.2	-64.8	-81.0	-91.0	2.0	-0.2	-0.7	0.0
-425.0	-28.7	-65.0	-81.0	-91.0	*	*	*	*
-400.0	-29.1	-64.6	-80.7	-91.0	*	*	*	*

TWIN GRID - LARGE LOOP EM LINE L70+00E
 DATE 10/24/86 OPERATOR D.M.W. Nparm=4

STATION	112/37	337/37	1012/3	3037/3	FF1	FF2	FF3	FF4
-525.0	1.9	2.4	3.2	5.3	*	*	*	*
-500.0	2.0	2.8	4.5	8.3	-0.4	-1.6	-5.4	-13.0
475.0	2.2	3.2	5.9	11.9	-0.2	-1.5	-5.0	-11.1
-450.0	2.1	3.6	7.2	14.7	-0.5	-1.5	-3.5	-2.4
-425.0	2.3	3.9	8.2	16.6	-0.7	-1.3	0.4	16.8
400.0	2.5	4.4	8.4	12.4	-0.5	-0.7	3.6	27.8
375.0	2.6	4.4	6.6	2.1	-0.4	-0.6	2.7	20.1
-350.0	2.7	4.6	6.4	-0.9	-0.5	-0.8	1.5	13.8
325.0	2.8	4.8	5.9	-4.7	-0.6	-0.9	1.2	12.5
300.0	3.0	5.0	5.6	-7.9	-0.5	-1.2	0.5	10.4
-275.0	3.1	5.3	5.5	-10.2	-0.6	-1.5	0.3	10.4
250.0	3.2	5.7	5.5	-12.8	-0.6	-1.1	1.3	11.7
225.0	3.5	6.1	5.3	-15.7	-0.2	-0.2	2.4	11.5
-200.0	3.4	6.0	4.4	-19.0	0.0	-0.3	1.2	8.2
-175.0	3.5	6.0	4.0	-21.0	-0.3	-1.4	-0.7	5.1
150.0	3.4	6.4	4.5	-21.9	-1.2	-2.4	-1.7	4.2
-125.0	3.8	7.0	4.6	-23.2	-1.4	-2.8	-2.3	4.0
-100.0	4.3	7.8	5.6	-23.9	-0.3	-1.5	0.4	6.9
-75.0	4.3	8.4	5.8	-25.2	0.3	0.1	3.9	10.4
-50.0	4.1	7.9	4.0	-28.8	0.3	0.6	5.2	12.2
-25.0	4.2	8.2	3.5	-30.7	-0.0	0.8	4.9	12.0
0.0	3.9	7.5	1.1	-35.5	-0.7	-0.3	1.9	7.1
25.0	4.4	7.8	1.5	-36.0	-0.9	-0.9	1.9	6.3
50.0	4.4	8.2	1.2	-37.3	-0.7	0.0	5.0	10.8
75.0	4.8	8.0	-0.5	-40.5	0.0	1.5	7.8	13.2
100.0	4.7	8.0	-1.8	-43.6	0.3	1.6	6.6	10.7
125.0	4.5	6.7	-5.3	-47.4	-0.8	-1.5	-0.9	3.0
150.0	4.7	7.7	-3.6	-47.4	-1.4	-2.5	-2.3	1.4
175.0	5.3	8.5	-2.6	-46.6	-0.5	-0.8	1.7	5.5
200.0	5.3	8.4	-4.0	-49.6	0.1	-0.0	0.9	3.7
225.0	5.2	8.6	-3.9	-49.9	-0.4	0.0	0.4	1.7
250.0	5.3	8.3	-3.6	-50.0	-0.8	0.2	4.2	5.1
275.0	5.6	8.7	-4.7	-51.2	-0.3	1.3	8.2	9.9
300.0	5.7	8.0	-7.0	-53.8	0.4	2.7	10.3	12.3
325.0	5.5	7.7	-9.5	-57.3	0.4	4.1	10.0	10.8
350.0	5.4	6.3	-12.5	-60.0	0.3	4.2	8.9	8.0
375.0	5.4	5.3	-14.0	-61.9	0.6	4.6	10.6	8.0
400.0	5.2	4.5	-16.9	-63.4	1.4	6.1	14.4	10.7
425.0	5.0	2.5	-20.2	-66.5	1.5	4.8	14.7	11.9
450.0	4.2	1.2	-25.1	-69.5	0.5	3.9	11.1	10.2
475.0	4.5	1.0	-26.7	-72.3	0.1	5.6	11.4	8.8
500.0	4.2	-1.2	-29.7	-73.9	1.1	6.4	14.4	10.0
525.0	4.4	-2.2	-33.5	-76.7	*	*	*	*
550.0	3.2	-4.4	-37.3	-79.5	*	*	*	*

TWIN GRID - LARGE LOOP EM

LINE 71+00E

DATE 10/24/86 OPERATOR D.M.W. Nparm=4

STATION	112/37	337/37	1012/3	3037/3	FF1	FF2	FF3	FF4
-525.0	2.0	2.8	4.3	7.9	*	*	*	*
-500.0	2.1	3.0	5.0	9.1	-0.7	-1.3	-4.6	-10.1
-475.0	2.3	3.3	6.1	11.8	-0.6	-1.6	-5.3	-11.2
-450.0	2.5	3.8	7.8	15.3	-0.5	-1.8	-4.3	-5.4
-425.0	2.5	4.1	8.6	16.8	-0.5	-1.5	-1.8	6.2
-400.0	2.8	4.8	9.6	15.7	-0.2	-0.7	1.1	16.2
-375.0	2.7	4.6	8.6	10.2	-0.3	-1.0	0.8	15.3
-350.0	2.8	5.0	8.5	6.1	-0.5	-0.9	1.2	15.0
-325.0	3.0	5.4	8.9	4.5	-0.4	-0.4	3.4	20.5
-300.0	3.0	5.1	7.0	-3.2	-0.3	-0.7	3.5	19.8
-275.0	3.2	5.7	7.0	-6.7	-0.2	-0.5	3.3	16.6
-250.0	3.1	5.5	5.4	-11.8	-0.4	-0.7	2.2	13.7
-225.0	3.3	5.8	5.3	-14.7	-0.6	-1.4	0.9	10.7
-200.0	3.4	6.1	4.9	-17.5	-0.6	-1.6	0.1	8.3
-175.0	3.6	6.6	4.9	-19.7	-0.5	-1.4	0.0	6.9
-150.0	3.7	6.9	5.2	-20.8	-0.6	-1.2	0.8	7.5
-125.0	3.8	7.2	4.6	-23.3	-0.6	-0.4	2.1	9.0
-100.0	4.1	7.5	4.7	-24.7	-0.3	0.2	3.6	10.8
-75.0	4.0	7.0	3.0	-28.4	-0.5	-0.8	2.5	9.5
-50.0	4.2	7.5	2.7	-30.4	-0.6	-1.5	0.8	6.9
-25.0	4.4	7.8	2.5	-32.2	-0.8	-1.3	0.6	6.0
0.0	4.4	8.2	2.4	-33.5	-0.9	-0.9	1.5	6.5
25.0	5.0	8.4	2.2	-35.1	-0.5	-0.5	3.0	8.1
50.0	4.7	8.5	1.2	-37.1	-0.5	0.9	5.9	11.7
75.0	5.2	8.6	0.4	-39.6	-0.0	2.9	9.5	15.3
100.0	5.0	7.4	-2.9	-44.3	0.4	1.6	7.1	12.3
125.0	4.9	6.8	-5.0	-47.7	-0.2	-1.3	1.1	5.1
150.0	4.9	7.6	-4.6	-48.5	-0.6	-1.6	0.0	2.3
175.0	5.2	7.9	-4.4	-48.6	-0.6	-1.1	0.7	3.1
200.0	5.2	8.1	-5.2	-49.9	-0.9	-1.4	-0.9	2.0
225.0	5.5	8.5	-4.5	-50.3	-0.9	-0.6	1.1	3.0
250.0	5.8	8.9	-4.2	-50.2	-0.1	1.9	7.7	9.3
275.0	5.8	8.3	-6.6	-53.0	0.8	4.0	11.6	13.2
300.0	5.6	7.2	-9.8	-56.8	1.7	5.5	12.7	12.1
325.0	5.2	6.0	-12.6	-59.6	1.3	4.4	10.5	9.0
350.0	4.5	4.0	-16.5	-62.3	-0.9	1.3	6.3	6.7
375.0	5.0	4.8	-16.4	-63.1	-1.6	1.7	6.1	6.4
400.0	5.6	3.9	-19.0	-65.5	0.5	4.0	8.1	6.5
425.0	5.5	3.2	-20.0	-66.3	2.1	5.4	12.0	10.3
450.0	4.6	1.5	-23.5	-68.8	1.5	6.4	15.5	13.2
475.0	4.4	0.2	-27.5	-73.3	0.4	7.7	15.8	10.7
500.0	4.2	-1.9	-31.5	-75.0	0.3	5.8	12.0	6.2
525.0	4.4	-4.1	-35.3	-77.8	*	*	*	*
550.0	3.9	-3.4	-35.7	-76.7	*	*	*	*

TWIN GRID - LARGE LOOP EM LINE 72+00E
 DATE 10/24/86 OPERATOR D.M.W. Nparm=4

STATION	112/37	337/37	1012/3	3037/3	FF1	FF2	FF3	FF4
-525.0	2.3	3.1	3.8	5.8	*	*	*	*
-500.0	2.6	3.5	4.9	7.4	-0.7	-1.9	-5.0	-8.7
-475.0	2.7	4.0	6.1	9.8	-0.7	-2.0	-5.2	-7.7
-450.0	2.9	4.5	7.6	12.1	-0.8	-2.0	-5.0	-5.0
-425.0	3.1	5.0	8.6	12.8	-0.7	-1.7	-4.4	-2.8
-400.0	3.3	5.5	10.1	14.1	-0.3	-1.0	-2.5	1.2
-375.0	3.4	5.7	10.5	13.6	-0.1	-0.9	-1.6	3.6
-350.0	3.3	5.8	10.7	12.1	-0.5	-1.5	-1.9	4.9
-325.0	3.5	6.3	11.5	12.0	-0.5	-0.8	1.6	15.2
-300.0	3.7	6.7	11.6	8.8	-0.1	0.4	6.2	25.8
-275.0	3.6	6.2	9.0	0.1	-0.1	0.1	5.9	24.3
-250.0	3.7	6.4	7.9	-5.1	-0.5	-0.6	3.3	18.0
-225.0	3.7	6.4	6.8	-10.3	-0.8	-1.0	2.0	13.6
-200.0	4.1	6.8	6.8	-12.7	-0.4	-0.8	2.5	13.2
-175.0	4.1	7.0	5.9	-16.3	0.0	-0.3	3.7	14.9
-150.0	4.1	7.0	5.2	-19.9	-0.3	-0.8	3.3	13.6
-125.0	4.1	7.1	3.8	-24.0	-0.6	-1.1	2.0	10.5
-100.0	4.4	7.7	4.0	-25.8	-0.2	-0.1	2.8	10.3
-75.0	4.4	7.5	3.0	-28.6	0.1	0.4	3.9	10.8
-50.0	4.3	7.4	2.0	-31.5	-0.4	-0.2	3.0	9.1
-25.0	4.4	7.4	1.1	-33.7	-0.6	-0.5	2.7	8.5
0.0	4.7	7.7	0.9	-35.5	-0.2	0.0	4.0	10.2
25.0	4.6	7.6	-0.5	-38.2	-0.6	0.2	4.9	11.1
50.0	4.7	7.5	-1.5	-41.2	-1.0	0.2	5.4	10.2
75.0	5.2	7.6	-3.0	-43.6	-0.2	0.5	4.7	8.4
100.0	5.1	7.3	-4.4	-46.0	0.3	0.3	2.7	6.1
125.0	5.0	7.3	-4.8	-47.2	-0.1	0.0	3.2	6.1
150.0	5.0	7.3	-5.3	-48.5	-0.2	0.8	5.7	8.4
175.0	5.2	7.3	-7.1	-50.8	0.5	1.6	5.3	9.3
200.0	5.0	6.5	-8.7	-53.3	0.8	1.5	2.1	6.7
225.0	4.7	6.5	-9.0	-55.3	0.0	0.6	2.5	4.5
250.0	4.7	5.8	-8.9	-55.5	-0.4	0.5	7.5	7.4
275.0	5.0	6.6	-11.3	-57.6	0.3	2.8	10.3	10.8
300.0	4.8	5.2	-14.1	-60.6	0.6	4.0	10.4	10.0
325.0	4.6	4.4	-16.4	-63.3	0.0	3.5	8.2	6.5
350.0	4.6	3.4	-19.4	-64.9	-0.8	2.5	5.5	4.8
375.0	4.8	2.7	-19.3	-65.5	-0.3	2.2	7.3	6.3
400.0	5.2	2.6	-22.0	-67.5	0.7	3.6	9.9	7.5
425.0	4.5	1.3	-24.0	-69.2	1.1	6.4	13.5	10.2
450.0	4.8	0.4	-27.2	-71.3	2.0	8.2	15.1	11.2
475.0	3.8	-2.9	-32.3	-75.6	1.5	5.3	11.5	6.8
500.0	3.5	-3.6	-34.0	-76.1	1.5	3.7	10.0	5.0
525.0	3.6	-4.2	-37.0	-77.6	*	*	*	*
550.0	2.2	-6.0	-39.3	-79.1	*	*	*	*

TWIN GRID - LARGE LOOP EM

LINE 73+00E

DATE 10/23/86 OPERATOR D.M.W. Nparm=4

STATION	112/37	337/37	1012/3	3037/3	FF1	FF2	FF3	FF4
-525.0	2.1	2.6	3.5	4.7	*	*	*	*
-500.0	2.4	3.1	4.6	6.7	-1.4	-2.1	-4.6	-5.4
-475.0	2.7	3.6	5.7	8.0	-1.4	-2.5	-5.6	-5.3
-450.0	3.2	4.2	7.0	8.8	-0.8	-2.3	-5.8	-6.2
-425.0	3.3	5.0	8.9	11.2	-0.6	-1.7	-4.6	-3.6
-400.0	3.4	5.1	9.6	11.8	-0.9	-1.9	-3.9	0.4
-375.0	3.7	5.8	10.9	11.8	-0.8	-2.2	-3.9	0.6
-350.0	3.9	6.2	11.5	10.8	-0.4	-1.9	-3.0	1.4
-325.0	4.0	6.9	12.9	12.2	-0.1	-0.9	0.6	10.4
-300.0	4.0	7.0	12.5	9.0	0.0	-0.1	2.9	16.1
-275.0	4.0	7.0	11.3	3.6	-0.2	-0.3	2.0	14.1
-250.0	4.0	7.0	11.2	1.5	-0.2	0.1	5.3	22.0
-225.0	4.2	7.3	10.6	-3.0	0.2	1.5	11.0	32.6
-200.0	4.0	6.6	6.6	-13.9	0.2	1.0	9.2	26.3
-175.0	4.0	6.2	4.2	-20.2	0.1	-0.2	4.8	16.3
-150.0	4.0	6.7	3.8	-23.0	-0.3	-0.8	2.9	12.9
-125.0	3.9	6.3	2.2	-27.4	-0.8	-1.2	2.4	11.0
-100.0	4.4	7.4	2.9	-28.7	-0.4	0.4	5.0	12.2
-75.0	4.3	6.8	0.7	-32.7	0.1	1.9	6.8	13.8
-50.0	4.4	6.5	-0.6	-35.6	0.0	1.3	5.4	12.2
-25.0	4.2	5.8	-2.6	-39.6	-0.3	-0.4	3.0	8.7
0.0	4.5	6.2	-2.7	-40.9	-0.2	-0.4	3.2	8.3
25.0	4.4	6.5	-3.5	-43.0	-0.1	1.4	5.6	10.3
50.0	4.5	5.9	-5.0	-45.8	-0.2	0.8	4.3	8.6
75.0	4.5	5.4	-6.8	-48.4	-0.6	-1.1	2.0	6.5
100.0	4.6	6.2	-6.0	-49.0	-0.9	-0.9	4.2	8.1
125.0	5.0	6.2	-7.8	-51.7	0.1	1.7	8.5	11.4
150.0	5.0	6.3	-9.2	-53.8	1.0	4.4	11.3	13.3
175.0	4.5	4.4	-13.1	-58.3	0.6	3.0	7.8	9.6
200.0	4.5	3.7	-15.2	-60.5	0.1	-0.2	2.2	4.2
225.0	4.4	4.0	-14.9	-61.2	-0.4	-0.7	1.6	2.8
250.0	4.5	4.3	-15.6	-61.8	0.0	0.7	3.1	3.9
275.0	4.8	4.1	-16.1	-62.7	1.1	2.9	7.4	7.5
300.0	4.1	3.5	-17.5	-64.2	0.3	4.3	10.8	9.7
325.0	4.1	2.0	-21.6	-67.8	-0.7	3.0	6.8	6.9
350.0	4.5	1.3	-22.8	-68.8	-0.2	3.6	3.2	3.8
375.0	4.4	1.2	-23.1	-70.1	1.0	5.0	6.6	3.6
400.0	4.4	-1.5	-24.5	-70.3	1.7	3.9	13.9	7.5
425.0	3.5	-1.0	-28.0	-72.2	1.3	5.0	15.7	10.2
450.0	3.6	-3.2	-33.5	-75.7	1.1	5.7	10.5	7.1
475.0	3.0	-4.3	-34.7	-77.0	1.1	5.7	10.1	5.8
500.0	3.0	-5.6	-37.3	-78.0	1.7	6.3	12.3	6.5
525.0	2.5	-7.6	-41.0	-80.5	*	*	*	*
550.0	1.8	-8.6	-43.3	-81.0	*	*	*	*

TWIN GRID - LARGE LOOP EM LINE 74+00E
 DATE 10/23/86 OPERATOR D.M.W. Nparm=4

ELEVATION	112/37	337/37	1012/3	3037/3	FF1	FF2	FF3	FF4
-525.0	2.5	3.1	4.3	5.8	*	*	*	*
-500.0	3.3	4.3	6.7	9.2	-1.6	-2.5	-5.0	-2.5
-475.0	3.6	4.8	7.6	8.9	-0.9	-1.8	-4.0	-0.3
-450.0	3.8	5.1	8.4	8.6	-0.9	-2.6	-5.9	-4.2
-425.0	4.0	5.8	9.9	9.8	-0.6	-2.4	-6.0	-5.2
-400.0	4.3	6.7	12.0	11.9	-0.4	-1.8	-5.2	-3.9
-375.0	4.1	6.6	12.3	11.7	-0.6	-1.4	-2.7	3.7
-350.0	4.6	7.7	14.8	13.9	-0.5	-0.2	2.4	16.4
-325.0	4.4	7.0	12.2	6.0	-0.3	-0.2	3.6	19.1
-300.0	4.8	7.5	12.5	3.2	0.2	-0.3	2.9	15.0
-275.0	4.5	7.4	10.9	-2.4	0.3	0.4	4.1	15.2
-250.0	4.5	7.4	10.9	-3.4	0.0	0.7	7.1	23.3
-225.0	4.5	7.1	8.4	-11.0	-0.2	0.6	9.1	28.1
-200.0	4.5	7.0	6.3	-18.1	0.0	1.2	10.0	26.0
-175.0	4.7	6.9	3.9	-24.4	0.3	1.6	8.7	20.7
-150.0	4.3	6.0	0.8	-30.7	-0.2	0.4	4.4	13.0
-125.0	4.6	6.3	0.7	-32.5	-0.2	0.6	4.6	12.3
-100.0	4.6	6.2	-0.4	-35.6	0.6	1.7	7.4	14.9
-75.0	4.5	5.5	-2.7	-39.9	0.4	1.1	6.8	12.9
-50.0	4.1	5.3	-4.4	-43.1	-0.9	0.0	4.4	9.0
-25.0	4.6	5.3	-5.5	-45.3	-0.5	-0.1	3.7	7.6
0.0	4.9	5.5	-6.0	-46.7	0.6	1.3	5.9	9.7
25.0	4.3	5.2	-7.6	-49.3	-0.3	1.6	5.9	9.9
50.0	4.6	4.3	-9.8	-52.4	-1.0	-0.9	3.0	7.2
75.0	4.9	4.8	-9.7	-53.5	0.3	0.0	4.1	8.2
100.0	5.0	5.6	-10.7	-55.4	1.1	3.3	7.5	9.9
125.0	4.2	3.5	-12.9	-58.7	0.5	2.9	8.5	8.8
150.0	4.6	3.6	-15.0	-60.1	0.0	1.5	6.9	7.6
175.0	4.1	2.6	-17.1	-62.8	-0.5	0.3	3.8	5.4
200.0	4.7	3.0	-17.7	-63.6	-0.2	-0.2	2.2	3.5
225.0	4.5	2.9	-18.2	-64.7	0.7	0.8	3.9	3.8
250.0	4.5	2.9	-18.8	-65.2	1.1	2.0	7.0	5.8
275.0	4.0	2.2	-21.0	-66.9	0.6	2.0	7.9	6.7
300.0	3.9	1.6	-23.0	-68.8	-0.1	2.6	7.7	6.5
325.0	4.0	1.5	-24.7	-70.0	-0.3	3.2	6.7	5.4
350.0	4.0	-0.3	-27.0	-72.2	0.7	4.0	6.2	3.8
375.0	4.2	0.2	-27.4	-72.0	1.1	5.2	7.1	4.8
400.0	3.1	-3.0	-30.5	-74.0	0.2	3.9	8.3	6.5
425.0	4.0	-2.3	-31.0	-75.0	0.8	5.1	11.7	7.5
450.0	3.1	-4.4	-35.2	-77.5	1.9	7.4	12.9	6.9
475.0	3.2	-6.0	-38.0	-79.0	2.3	5.5	11.4	4.9
500.0	2.0	-8.1	-41.1	-80.4	1.2	3.7	10.0	4.2
525.0	2.0	-7.8	-43.5	-81.0	*	*	*	*
550.0	2.0	-10.0	-45.6	-82.6	*	*	*	*

TWIN GRID - LARGE LOOP EM LINE 7400E
 DATE 04 DEC. 1986 OPERATOR D.W. LOOP#5 LOOP 800x600m Nparm=4
 STATION 112/37 337/37 1012/3 3037/3 --- --- --- ---

✓ -575.0	-22.0	-60.3	-77.8	-87.0	2.2	1.8	2.3	2.5
-550.0	-22.3	-60.8	-78.4	-87.3	1.1	0.8	1.1	0.1
-525.0	-22.9	-61.3	-78.9	-88.0	-0.2	-0.7	0.1	-0.7
-500.0	-22.5	-60.6	-78.4	-86.4	-0.4	-0.3	1.3	2.5
-475.0	-22.5	-60.8	-79.0	-88.2	-0.2	0.2	2.2	-1.3
-450.0	-22.5	-60.8	-79.6	-88.7	-0.4	-0.1	1.9	-2.6
-425.0	-22.3	-60.8	-80.0	-84.6	*	*	*	*
-400.0	-22.3	-60.7	-80.5	-89.7	*	*	*	*

TWIN GRID - LARGE LOOP EM LINE 75+00E
DATE 11/04/86 OPERATOR D.M.W. Nparm=4

ELEVATION	112/37	337/37	1012/3	3037/3	FF1	FF2	FF3	FF4
-525.0	2.4	3.0	3.3	3.0	*	*	*	*
-500.0	2.4	3.0	3.7	3.9	-0.3	0.3	0.2	2.9
-475.0	2.5	2.9	3.6	3.2	-0.3	0.6	1.4	7.3
-450.0	2.6	2.8	3.2	0.8	0.0	1.4	2.0	8.3
-425.0	2.6	2.5	2.7	-1.0	0.1	1.8	1.1	5.2
-400.0	2.5	1.8	2.1	-3.3	0.0	1.1	-1.6	-3.0
-375.0	2.6	1.7	2.7	-2.1	0.3	1.0	-1.4	-2.9
-350.0	2.5	1.5	3.7	0.8	0.7	2.3	4.6	13.8
-325.0	2.3	1.0	2.5	-3.3	0.7	3.2	8.4	23.3
-300.0	2.1	-0.1	-0.7	-11.8	0.6	2.6	5.1	13.1
-275.0	2.0	-0.6	-1.5	-14.0	0.6	2.1	2.9	6.9
-250.0	1.8	-1.1	-1.8	-14.2	0.9	3.4	7.4	18.0
-225.0	1.7	-1.7	-3.3	-18.5	0.9	4.2	11.8	27.4
-200.0	1.2	-3.4	-7.4	-27.7	0.2	3.2	11.2	23.8
-175.0	1.4	-3.6	-9.5	-32.4	0.5	3.2	9.5	19.0
-150.0	1.3	-4.7	-12.4	-37.6	1.5	3.8	8.7	17.2
-125.0	0.8	-5.5	-14.0	-41.5	1.4	3.6	8.7	15.3
-100.0	0.4	-6.6	-16.6	-45.7	0.8	3.0	7.7	13.1
-75.0	0.3	-7.2	-18.5	-48.7	0.9	3.0	6.5	11.8
-50.0	0.1	-7.9	-19.8	-51.6	1.8	4.0	7.7	11.9
-25.0	-0.3	-8.9	-21.8	-54.6	1.9	3.6	7.5	9.7
0.0	-1.1	-10.2	-24.2	-57.6	0.9	1.8	4.7	6.6
25.0	-1.0	-10.2	-24.9	-58.3	0.7	2.2	5.0	8.3
50.0	-1.3	-10.7	-25.8	-60.5	1.3	3.6	7.8	10.4
75.0	-1.5	-11.9	-28.3	-63.7	0.8	2.2	6.0	7.1
100.0	-2.1	-12.6	-30.2	-65.5	0.4	1.0	3.1	4.3
125.0	-1.5	-12.2	-29.9	-65.8	1.4	2.3	4.7	5.8
150.0	-2.5	-13.3	-31.7	-67.7	0.7	2.0	4.6	5.5
175.0	-2.5	-13.8	-33.1	-69.4	-0.1	1.1	3.4	3.6
200.0	-2.2	-13.7	-33.1	-69.6	1.0	2.3	4.9	4.5
225.0	-2.7	-14.5	-35.1	-71.1	1.4	3.2	5.0	4.7
250.0	-3.0	-15.3	-36.0	-72.4	1.1	3.6	3.8	3.0
275.0	-3.3	-16.1	-37.2	-73.0	0.6	3.6	3.9	3.1
300.0	-3.5	-17.3	-37.7	-73.5	0.2	2.3	5.7	4.9
325.0	-3.4	-17.7	-39.4	-75.0	0.9	2.2	7.6	5.6
350.0	-3.6	-18.0	-41.2	-76.4	1.5	3.3	6.9	4.8
375.0	-4.2	-19.2	-43.5	-77.7	1.3	2.8	3.8	3.4
400.0	-4.3	-19.8	-44.0	-78.5	1.3	3.4	5.3	3.1
425.0	-4.8	-20.2	-44.5	-79.0	1.0	5.2	9.3	4.5
450.0	-5.0	-22.2	-48.3	-80.3	0.6	4.7	8.8	5.1
475.0	-5.1	-23.0	-49.5	-81.7	0.9	4.4	8.4	4.2
500.0	-5.3	-24.1	-52.1	-82.7	1.8	5.4	7.8	3.1
525.0	-5.7	-25.5	-54.1	-83.5	*	*	*	*
550.0	-6.5	-27.0	-55.3	-84.0	*	*	*	*

TWIN GRID - LARGE LOOP EM LINE 7500E
 DATE 05 DEC. 1986 OPERATOR D.W. LOOP#5 LOOP 800x600m Nparm=4
 STATION 112/37 337/37 1012/3 3037/3 FF1 FF2 FF3 FF4

-650.0	-17.0	-54.6	-75.1	-81.1	5.0	6.1	2.6	6.4
-625.0	-18.6	-56.2	-75.3	-83.6	4.3	4.4	2.0	7.9
-600.0	-19.6	-57.1	-75.8	-85.8	2.7	3.3	2.3	4.7
-575.0	-20.3	-58.1	-76.6	-86.8	1.6	1.3	0.6	1.5
-550.0	-20.6	-58.5	-76.8	-87.3	0.9	0.4	0.1	-0.3
-525.0	-20.9	-58.0	-76.2	-86.8	0.9	2.3	2.5	-4.5
-500.0	-20.9	-59.0	-77.3	-87.0	2.2	3.1	3.5	-6.6
-475.0	-21.5	-59.8	-78.2	-82.6	2.3	1.9	2.6	1.3
-450.0	-22.5	-60.3	-78.8	-84.6	0.2	0.6	1.9	6.6
-425.0	-22.2	-60.4	-79.3	-86.3	*	*	*	*
-400.0	-22.0	-60.3	-79.6	-87.5	*	*	*	*

TWIN GRID - LARGE LOOP EM LINE 76+00E
 DATE 11/04/86 OPERATOR D.M.W. Nparm=4

STATION	112/37	337/37	1012/3	3037/3	FF1	FF2	FF3	FF4
-525.0	2.2	2.9	3.2	3.0	*	*	*	*
-500.0	2.4	2.9	3.5	3.2	-0.7	0.0	0.5	5.9
-475.0	2.6	3.0	3.4	1.4	-0.4	0.4	1.7	8.3
-450.0	2.7	2.8	2.8	-1.1	-0.2	0.4	1.4	6.1
-425.0	2.7	2.7	2.4	-2.6	-0.3	0.4	0.5	3.3
-400.0	2.8	2.7	2.4	-3.2	-0.1	1.0	0.5	2.1
-375.0	2.9	2.4	2.3	-3.8	0.2	1.1	-0.5	-1.5
-350.0	2.7	2.0	2.0	-4.1	0.2	1.4	1.1	3.9
-325.0	2.8	2.0	3.2	-1.4	0.5	2.7	6.9	19.3
-300.0	2.6	1.0	0.0	-10.4	0.8	2.9	6.4	16.6
-275.0	2.4	0.3	-1.7	-14.4	0.5	1.7	0.6	2.0
-250.0	2.2	-0.2	-1.5	-14.0	0.5	1.8	1.8	4.3
-225.0	2.3	-0.2	-0.8	-12.8	0.7	3.0	8.7	20.5
-200.0	1.8	-1.5	-4.2	-19.9	0.6	3.4	11.9	28.4
-175.0	2.0	-1.9	-6.8	-27.4	1.2	4.1	11.6	25.0
-150.0	1.5	-3.2	-10.1	-33.7	1.4	4.4	10.8	20.9
-125.0	1.1	-4.3	-12.5	-38.6	1.0	3.7	9.8	18.3
-100.0	1.0	-5.2	-15.2	-43.4	1.0	3.9	9.3	16.9
-75.0	0.6	-6.0	-17.2	-47.2	0.9	4.3	9.4	15.9
-50.0	0.5	-7.4	-19.8	-51.7	1.2	4.0	9.1	14.2
-25.0	0.2	-8.1	-22.0	-54.8	1.3	3.6	8.1	12.2
0.0	-0.3	-9.3	-24.1	-58.3	0.9	2.7	6.4	9.3
25.0	-0.3	-9.8	-25.8	-60.4	1.1	1.8	5.0	7.1
50.0	-0.7	-10.3	-26.7	-62.0	1.3	1.9	5.5	6.7
75.0	-1.0	-10.6	-28.2	-63.8	1.0	2.6	6.0	6.1
100.0	-1.3	-11.4	-29.8	-65.3	0.4	2.7	4.7	4.9
125.0	-1.4	-12.1	-31.1	-66.6	0.5	2.5	3.7	4.7
150.0	-1.3	-12.6	-31.6	-67.4	0.9	2.8	4.7	6.0
175.0	-1.9	-13.4	-33.0	-69.2	1.0	2.4	5.6	6.5
200.0	-1.7	-14.1	-34.4	-70.8	1.1	2.0	5.0	4.6
225.0	-2.5	-14.3	-35.8	-72.3	0.5	2.3	3.6	2.5
250.0	-2.2	-15.2	-36.6	-72.3	0.9	2.2	3.7	3.1
275.0	-2.5	-15.5	-37.2	-73.3	1.4	2.3	4.2	3.4
300.0	-3.1	-16.2	-38.9	-74.4	0.9	2.4	3.5	2.5
325.0	-3.0	-16.8	-39.1	-74.6	1.5	2.8	4.5	3.7
350.0	-3.5	-17.3	-40.5	-75.6	1.9	2.7	6.7	5.7
375.0	-4.1	-18.5	-42.0	-77.1	1.5	3.2	7.3	5.6
400.0	-4.3	-18.3	-44.3	-78.8	1.2	6.1	7.5	5.1
425.0	-4.8	-20.7	-45.5	-79.5	0.9	5.8	8.5	5.9
450.0	-4.8	-22.2	-48.3	-81.5	1.6	2.5	8.4	4.8
475.0	-5.2	-22.6	-50.0	-82.7	*	*	*	*
500.0	-6.0	-22.8	-52.2	-83.1	*	*	*	*

TWIN GRID - LARGE LOOP EM LINE 7600E
 DATE 05 DEC. 1986 OPERATOR S.L. LOOP#5 LOOP 800x600m Nparm=4
 STATION 112/37 337/37 1012/3 3037/3 FF1 FF2 FF3 FF4
 -1100.0 -11.0 -40.3 -67.3 -78.2 9.1 18.3 8.8 5.2

-750.0	-11.0	-40.3	-67.3	-78.2	9.1	18.3	8.8	5.2
-725.0	-13.2	-45.5	-69.2	-79.7	10.3	17.1	8.4	5.2
-700.0	-16.3	-50.2	-71.7	-80.6	8.2	11.4	6.0	6.0
-675.0	-18.2	-52.7	-73.2	-82.5	6.1	7.9	3.7	6.7
-650.0	-19.5	-54.4	-73.7	-83.8	5.1	6.2	3.0	1.1
-625.0	-21.1	-56.4	-74.9	-86.0	3.3	3.8	2.5	-4.4
-600.0	-21.7	-56.9	-75.0	-81.4	2.1	2.6	3.1	2.5
-575.0	-22.2	-57.7	-76.1	-84.0	1.8	2.6	2.9	8.0
-550.0	-22.7	-58.2	-76.9	-85.9	1.4	3.0	1.9	6.3
-525.0	-23.0	-59.0	-77.1	-87.5	1.3	3.3	2.3	4.4
-500.0	-23.3	-59.9	-77.8	-88.7	1.5	3.1	2.9	2.8
-475.0	-23.7	-60.6	-78.5	-89.1	*	*	*	*
-450.0	-24.1	-61.4	-79.3	-89.9	*	*	*	*

TWIN GRID - LARGE LOOP EM

LINE 77+00E

DATE 11/04/86

OPERATOR D.M.W. Nparm=4

STATION	112/37	337/37	1012/3	3037/3	FF1	FF2	FF3	FF4
-525.0	2.6	3.5	3.7	3.3	*	*	*	*
-500.0	2.7	3.8	4.2	3.4	-0.8	-0.7	-0.6	3.2
-475.0	3.0	4.0	4.5	2.9	-0.6	0.1	1.7	8.6
-450.0	3.1	4.0	4.0	0.6	-0.5	0.8	3.3	11.8
-425.0	3.2	3.7	3.0	-2.9	-0.4	1.1	3.0	9.5
-400.0	3.4	3.5	2.2	-5.4	0.0	1.2	1.8	5.1
-375.0	3.3	3.1	1.8	-6.4	0.0	0.9	1.0	2.9
-350.0	3.3	2.9	1.6	-7.0	-0.0	1.1	2.5	7.0
-325.0	3.4	2.8	1.4	-7.7	0.4	2.1	4.6	12.0
-300.0	3.2	2.1	-0.5	-12.7	0.5	2.1	3.0	7.4
-275.0	3.1	1.5	-1.1	-14.0	0.3	1.3	0.3	0.5
-250.0	3.0	1.3	-1.0	-13.8	0.2	1.3	0.0	-0.6
-225.0	3.0	1.0	-0.9	-13.4	0.5	2.5	5.1	11.9
-200.0	2.9	0.5	-1.2	-13.8	1.0	3.5	12.3	29.8
-175.0	2.6	-0.7	-5.8	-25.3	1.1	3.8	13.6	31.6
-150.0	2.3	-1.3	-8.6	-31.7	1.1	4.8	13.2	27.5
-125.0	2.1	-2.7	-12.0	-39.0	1.1	5.2	13.4	25.4
-100.0	1.7	-4.1	-15.6	-45.5	1.0	4.4	11.3	20.7
-75.0	1.6	-5.1	-18.4	-50.6	1.5	4.3	9.9	16.8
-50.0	1.2	-6.1	-20.5	-54.6	1.8	4.5	9.8	13.8
-25.0	0.6	-7.4	-23.4	-58.3	1.3	3.8	8.3	10.8
0.0	0.4	-8.3	-25.3	-60.7	1.1	3.4	6.6	8.9
25.0	0.1	-9.0	-26.9	-63.0	1.2	3.7	6.7	8.3
50.0	-0.2	-10.1	-28.4	-64.9	1.1	3.2	7.2	8.0
75.0	-0.5	-10.9	-30.5	-67.1	0.8	2.4	5.5	6.3
100.0	-0.7	-11.4	-32.0	-68.8	1.2	2.7	3.5	3.4
125.0	-0.8	-12.0	-32.4	-69.5	1.6	3.1	3.1	1.4
150.0	-1.6	-13.0	-33.6	-69.8	0.9	1.9	3.0	1.7
175.0	-1.5	-13.5	-33.9	-69.9	0.4	0.6	3.6	3.4
200.0	-1.8	-13.4	-35.1	-71.1	0.7	1.8	4.5	4.4
225.0	-1.7	-13.7	-36.0	-72.0	1.3	3.5	5.0	4.4
250.0	-2.3	-15.0	-37.5	-73.4	1.5	3.8	5.3	4.3
275.0	-2.5	-15.6	-38.6	-74.1	1.3	3.5	4.1	3.7
300.0	-3.0	-16.9	-40.2	-75.6	1.1	2.1	2.9	2.2
325.0	-3.1	-17.2	-40.0	-75.6	1.3	2.0	4.3	2.3
350.0	-3.5	-17.4	-41.7	-76.3	1.6	3.6	5.9	3.8
375.0	-3.9	-18.7	-42.8	-77.2	1.2	3.7	6.6	4.3
400.0	-4.3	-19.5	-44.8	-78.5	0.6	3.9	6.4	3.7
425.0	-4.3	-20.3	-46.3	-79.3	1.4	3.7	6.1	3.4
450.0	-4.5	-21.8	-47.7	-80.1	*	*	*	*
475.0	-5.5	-21.7	-49.5	-81.1	*	*	*	*

TWIN GRID - LARGE LOOP EM LINE 7700E
 DATE 05 DEC. 1986 OPERATOR N.M. LOOP#6 LOOP 600x500m Nparm=4
 STATION 112/37 337/37 1012/3 3037/3 FF1 FF2 FF3 FF4

-775.0	-1.0	-14.1	-33.6	-42.6	4.4	12.2	14.8	11.8
-750.0	-2.0	-17.1	-36.9	-44.8	4.6	12.5	14.9	16.5
-725.0	-3.3	-20.3	-41.0	-49.5	4.5	11.8	13.8	18.5
-700.0	-4.3	-23.4	-44.4	-54.4	4.3	10.7	12.1	15.4
-675.0	-5.5	-25.8	-47.3	-58.4	3.9	10.6	11.1	9.6
-650.0	-6.4	-28.6	-50.2	-60.9	4.1	10.3	10.5	9.0
-625.0	-7.3	-31.2	-52.6	-61.5	4.4	8.9	9.5	13.5
-600.0	-8.7	-33.5	-55.4	-66.8	3.6	7.3	7.1	11.0
-575.0	-9.4	-35.2	-56.9	-69.1	3.0	6.2	5.0	5.8
-550.0	-10.2	-36.8	-58.2	-70.2	2.8	6.1	4.8	5.1
-525.0	-10.9	-38.1	-59.1	-71.5	2.7	6.3	5.8	5.2
-500.0	-11.5	-40.0	-60.8	-72.9	2.6	6.1	6.1	5.0
-475.0	-12.3	-41.2	-62.3	-74.0	2.1	6.0	5.8	5.3
-450.0	-12.7	-43.0	-63.7	-75.4	2.2	5.1	5.5	4.9
-425.0	-13.2	-44.2	-65.2	-76.8	*	*	*	*
-400.0	-14.0	-45.1	-66.3	-77.5	*	*	*	*

VIN GRID - LARGE LOOP EM

LINE L78E

DATE 11/6/86

OPERATOR D.M.W. Nparm=4

STATION	112/37	337/37	1012/3	3037/3	FF1	FF2	FF3	FF4
-525.0	2.8	4.0	4.9	5.7	*	*	*	*
-500.0	3.0	4.6	5.6	5.1	-1.0	-1.0	0.8	9.6
-475.0	3.3	4.8	5.2	2.3	-0.9	-0.1	2.7	12.5
-450.0	3.5	4.8	4.5	-1.1	-0.8	0.2	3.0	11.1
-425.0	3.7	4.7	3.6	-4.0	-0.6	0.4	2.8	8.9
-400.0	3.9	4.7	3.1	-5.9	-0.2	1.1	3.3	8.6
-375.0	3.9	4.4	2.2	-8.1	0.2	2.1	4.2	8.9
-350.0	3.9	3.9	1.2	-10.4	0.3	2.3	4.3	8.6
-325.0	3.7	3.1	-0.1	-12.5	0.1	1.6	3.1	7.0
-300.0	3.8	2.9	-0.8	-14.6	0.2	1.5	1.5	2.8
-275.0	3.7	2.5	-1.2	-15.3	0.4	1.6	0.3	-1.0
-250.0	3.6	2.0	-1.2	-14.6	0.5	2.2	4.4	9.3
-225.0	3.5	1.8	-1.1	-14.3	0.3	3.5	12.4	29.0
-200.0	3.3	0.5	-5.7	-24.9	0.0	3.8	14.2	33.2
-175.0	3.5	-0.2	-9.0	-33.0	0.5	3.9	11.9	26.0
-150.0	3.3	-1.3	-12.0	-39.4	0.9	3.8	10.3	20.1
-125.0	3.0	-2.3	-14.6	-44.5	0.8	3.4	9.4	17.1
-100.0	2.9	-3.0	-16.7	-48.0	1.0	3.9	9.8	17.4
-75.0	2.6	-4.0	-19.3	-53.0	1.6	4.5	9.3	14.7
-50.0	2.3	-5.2	-21.8	-56.9	2.1	4.5	8.1	10.3
-25.0	1.6	-6.3	-23.5	-58.8	1.7	3.7	6.5	7.9
0.0	1.2	-7.4	-25.7	-61.4	1.2	2.9	4.9	6.8
25.0	1.0	-7.8	-26.1	-62.2	1.4	3.2	6.0	7.7
50.0	0.6	-8.8	-28.0	-64.8	1.1	3.0	6.7	7.7
75.0	0.2	-9.6	-29.8	-66.5	0.3	2.3	5.5	6.1
100.0	0.3	-10.0	-31.0	-68.2	0.6	2.6	4.5	4.5
125.0	0.2	-10.7	-32.3	-69.2	1.4	2.8	3.7	3.6
150.0	-0.3	-11.5	-33.0	-70.0	1.5	2.5	3.7	3.4
175.0	-0.6	-12.0	-34.0	-71.0	1.6	3.0	4.3	3.2
200.0	-1.0	-12.7	-35.0	-71.6	1.5	3.6	5.3	3.9
225.0	-1.5	-13.8	-36.3	-72.6	1.3	3.8	6.7	4.8
250.0	-1.6	-14.5	-38.0	-73.9	2.1	5.0	7.4	4.8
275.0	-2.2	-15.8	-40.0	-75.1	2.4	5.2	6.5	3.8
300.0	-3.0	-17.5	-41.7	-76.2	0.8	3.4	5.5	2.5
325.0	-3.2	-18.0	-42.8	-76.6	0.2	2.6	5.1	1.6
350.0	-2.8	-18.7	-44.4	-77.2	*	*	*	*
375.0	-3.6	-19.4	-45.2	-77.2	*	*	*	*

TWIN GRID - LARGE LOOP EM

LINE 7800E

DATE 05 DEC. 1986

OPERATOR N.M.

LOOP#6

LOOP

600x500m Nparm=4

STATION	112/37	337/37	1012/3	3037/3	FF1	FF2	FF3	FF4
-875.0	4.2	8.1	8.1	7.9	*	*	*	*
-850.0	3.5	4.9	0.1	-6.3	3.0	15.4	33.0	48.9
-825.0	2.8	0.7	-8.7	-19.4	3.7	16.6	31.6	38.0
-800.0	1.9	-3.1	-16.1	-27.9	3.8	15.3	25.8	26.0
-775.0	0.7	-7.9	-24.1	-35.8	3.2	11.3	16.8	14.7
-750.0	0.2	-9.8	-26.5	-37.5	3.2	10.7	15.1	13.5
-725.0	-0.8	-12.5	-30.5	-40.9	3.3	11.9	16.3	17.2
-700.0	-1.5	-15.9	-35.2	-45.9	3.9	11.4	14.6	17.2
-675.0	-2.4	-18.3	-38.1	-49.7	4.1	11.1	13.9	15.3
-650.0	-3.8	-21.5	-42.2	-54.3	3.4	10.7	12.8	11.5
-625.0	-4.2	-23.8	-45.0	-56.6	4.3	11.6	13.5	12.2
-600.0	-5.4	-26.7	-48.1	-58.9	5.1	11.7	14.0	15.2
-575.0	-6.9	-30.2	-52.6	-64.2	4.0	8.8	9.9	11.7
-550.0	-7.8	-32.0	-54.5	-66.5	3.0	6.8	6.2	7.4
-525.0	-8.5	-33.7	-56.1	-68.3	3.2	7.2	6.7	8.0
-500.0	-9.2	-35.3	-57.2	-69.8	3.3	7.9	8.3	9.3
-475.0	-10.3	-37.6	-60.1	-73.0	2.3	6.7	6.7	7.1
-450.0	-10.7	-39.3	-61.5	-74.4	2.4	5.3	5.5	4.9
-425.0	-11.1	-40.3	-62.5	-75.5	*	*	*	*
-400.0	-12.3	-41.9	-64.6	-76.8	*	*	*	*

TWIN GRID - LARGE LOOP EM

LINE L79E

DATE 11/06/86

OPERATOR D.M.W. Nparm=4

STATION	112/37	337/37	1012/3	3037/3	FF1	FF2	FF3	FF4
-525.0	-0.6	0.0	0.2	-0.5	*	*	*	*
-500.0	-0.4	0.5	0.6	-3.4	-1.4	-1.9	-0.3	9.4
-475.0	0.0	1.0	0.7	-5.6	-1.3	-1.2	0.9	8.3
-450.0	0.4	1.4	0.4	-7.7	-0.9	-0.3	1.8	7.4
-425.0	0.5	1.3	0.0	-9.6	-0.7	0.3	2.5	6.7
-400.0	0.8	1.4	-0.7	-11.1	-0.4	0.9	2.9	6.6
-375.0	0.8	1.0	-1.4	-12.9	0.0	1.7	3.9	7.6
-350.0	0.9	0.8	-2.2	-14.4	0.0	2.6	5.5	10.4
-325.0	0.7	-0.1	-3.8	-17.2	-0.0	2.7	6.5	13.4
-300.0	1.0	-0.7	-5.3	-20.5	0.4	2.1	6.5	13.6
-275.0	0.6	-1.3	-7.2	-24.5	0.4	1.9	4.9	9.4
-250.0	0.7	-1.6	-8.4	-26.8	0.4	2.2	2.0	2.4
-225.0	0.5	-2.3	-9.0	-27.6	0.6	2.6	2.5	4.6
-200.0	0.4	-2.8	-8.6	-26.1	0.6	3.3	9.0	20.5
-175.0	0.2	-3.7	-11.3	-32.9	0.7	4.3	14.1	29.9
-150.0	0.1	-4.7	-15.3	-41.3	1.0	4.7	13.2	21.0
-125.0	-0.2	-6.1	-18.7	-47.6	1.2	4.5	10.7	15.3
-100.0	-0.5	-7.0	-21.1	-47.6	1.1	4.2	9.9	21.5
-75.0	-0.8	-8.3	-23.6	-56.6	1.5	4.2	10.0	19.4
-50.0	-1.0	-9.0	-26.1	-60.1	1.8	3.8	8.7	12.0
-25.0	-1.8	-10.5	-28.6	-63.5	1.2	2.5	6.2	9.3
0.0	-1.8	-10.6	-29.8	-65.2	0.9	2.5	5.7	8.0
25.0	-2.2	-11.4	-31.1	-67.7	0.6	3.6	6.3	6.6
50.0	-2.3	-12.2	-33.0	-69.0	1.0	3.9	5.5	5.0
75.0	-2.3	-13.4	-34.2	-70.5	2.2	3.3	4.9	4.6
100.0	-3.2	-14.1	-35.4	-71.2	2.1	3.0	5.1	4.1
125.0	-3.6	-14.8	-36.7	-72.9	1.7	3.6	5.5	2.3
150.0	-4.0	-15.7	-38.0	-72.9	1.6	3.9	5.2	2.5
175.0	-4.5	-16.8	-39.6	-73.5	0.8	2.9	3.5	3.4
200.0	-4.7	-17.6	-40.3	-74.8	0.7	1.6	3.1	2.3
225.0	-4.6	-17.8	-40.8	-75.0	1.5	0.4	2.4	2.5
250.0	-5.3	-18.2	-42.2	-75.6	1.1	2.0	2.8	3.1
275.0	-5.5	-17.6	-41.3	-76.7	*	*	*	*
300.0	-5.5	-20.4	-44.5	-77.0	*	*	*	*

TWIN GRID - LARGE LOOP EM LINE 7900E
DATE 05 DEC. 1986 OPERATOR N.M. LOOP#6 LOOP 600x500m Nparm=4

STATION	112/37	337/37	1012/3	3037/3	FF1	FF2	FF3	FF4
-925.0	4.2	10.1	15.9	23.5	*	*	*	*
-900.0	4.5	10.5	15.8	23.2	0.1	3.6	11.0	22.6
-875.0	4.4	9.5	13.1	17.9	1.0	7.9	21.0	41.1
-850.0	4.2	7.5	7.6	6.2	1.8	10.9	26.7	45.7
-825.0	3.7	4.6	0.3	-6.2	2.5	12.2	26.7	38.1
-800.0	3.1	1.5	-6.3	-15.4	2.7	12.5	25.3	31.0
-775.0	2.3	-1.6	-12.5	-22.7	2.5	12.6	24.2	28.2
-750.0	1.8	-4.8	-18.8	-29.9	2.5	12.1	21.4	25.2
-725.0	1.1	-7.9	-24.2	-36.4	2.7	11.1	18.2	21.7
-700.0	0.5	-10.6	-28.5	-41.4	2.9	10.6	16.3	19.2
-675.0	-0.3	-13.2	-32.7	-46.6	3.0	11.0	15.3	16.2
-650.0	-1.0	-15.9	-36.3	-50.4	3.0	11.1	14.7	13.5
-625.0	-1.8	-18.9	-40.2	-53.8	3.4	10.8	14.5	12.7
-600.0	-2.5	-21.3	-43.5	-56.7	4.6	11.3	14.6	10.2
-575.0	-3.7	-24.3	-47.5	-60.2	5.0	10.7	12.1	8.8
-550.0	-5.2	-27.2	-50.8	-60.5	3.8	8.9	9.2	13.5
-525.0	-6.0	-29.1	-52.3	-65.2	2.6	8.2	9.4	14.7
-500.0	-6.7	-31.3	-55.2	-69.0	2.4	8.1	8.4	9.9
-475.0	-7.1	-33.2	-57.3	-71.4	3.1	8.7	7.6	7.0
-450.0	-8.0	-35.3	-58.6	-72.7	3.5	8.5	8.6	7.0
-425.0	-8.9	-37.9	-61.5	-74.7	*	*	*	*
-400.0	-9.7	-39.1	-63.0	-76.4	*	*	*	*

TWIN GRID - LARGE LOOP EM					LINE 8000E			
DATE 05 DEC. 1986					OPERATOR D.W.			
					LOOP#6	LOOP	600x500m	Nparm=4
S	A	T	I	O	FF1	FF2	FF3	FF4
-025.0	-1.3	-0.5	0.3	0.2	*	*	*	*
-1000.0	-0.8	0.8	2.5	3.6	-1.3	-4.7	-8.9	-15.2
975.0	-0.7	1.7	4.4	6.8	-1.7	-5.3	-10.3	-18.7
950.0	-0.1	3.3	7.3	12.2	-2.0	-5.5	-10.5	-20.1
-925.0	0.3	4.5	9.9	16.9	-1.8	-4.8	-8.0	-13.8
-900.0	0.9	6.0	12.3	22.2	-1.3	-2.7	-3.4	-0.4
875.0	1.1	6.6	12.9	20.7	-0.9	0.3	3.7	11.6
-850.0	1.4	6.6	12.7	18.8	0.3	4.5	13.8	25.2
-825.0	1.5	5.7	8.8	12.5	1.8	9.1	22.7	39.6
800.0	0.7	3.0	3.0	1.8	1.6	10.8	26.7	43.7
775.0	0.4	0.2	-4.2	-10.1	1.6	11.3	27.2	38.9
-750.0	0.2	-2.3	-10.7	-19.3	2.6	11.5	25.4	32.2
725.0	-0.7	-5.8	-17.7	-27.9	2.3	9.9	21.3	25.6
700.0	-1.3	-7.8	-22.6	-33.7	1.7	9.3	18.7	24.5
-675.0	-1.5	-10.2	-27.1	-39.1	2.0	9.8	18.3	26.5
650.0	-2.2	-12.7	-31.9	-47.0	2.1	9.3	16.4	22.0
625.0	-2.6	-15.1	-36.1	-52.3	2.2	8.6	13.7	15.5
-600.0	-3.2	-17.1	-39.3	-55.8	2.3	8.6	12.0	11.7
-575.0	-3.8	-19.3	-42.4	-59.0	2.4	9.1	11.4	8.9
550.0	-4.3	-21.5	-45.0	-60.8	3.3	9.3	12.4	8.7
525.0	-5.1	-24.0	-48.1	-62.9	3.7	9.4	13.4	12.0
-500.0	-6.3	-26.1	-51.7	-65.6	2.7	8.4	11.2	12.9
475.0	-6.8	-28.8	-54.8	-70.1	2.0	6.7	7.7	8.7
450.0	-7.3	-29.7	-56.2	-71.3	3.3	7.8	7.2	6.3
-425.0	-7.8	-31.9	-58.0	-73.1	4.5	9.3	8.3	5.5
400.0	-9.6	-34.4	-60.2	-74.6	3.5	8.3	8.2	4.0
375.0	-10.0	-36.5	-62.3	-75.3	2.4	7.0	7.2	2.5
-350.0	-10.9	-38.1	-64.1	-76.4	1.9	6.5	6.1	-0.2
-325.0	-11.1	-39.8	-65.6	-76.0	2.2	5.9	5.2	2.6
300.0	-11.7	-41.3	-66.9	-75.5	2.9	5.4	5.4	8.8
-275.0	-12.5	-42.5	-68.0	-79.5	4.0	6.0	6.0	6.5
-250.0	-13.2	-44.0	-69.9	-80.8	4.5	6.3	5.4	2.7
225.0	-15.0	-45.8	-71.0	-80.7	2.7	4.9	4.3	3.8
200.0	-15.2	-47.0	-72.3	-82.3	1.8	3.9	4.0	1.9
-175.0	-15.7	-47.7	-72.9	-83.0	1.5	4.0	3.7	-1.4
150.0	-16.3	-49.0	-74.4	-81.9	0.4	2.8	1.8	-1.5
125.0	-16.1	-49.7	-74.5	-82.0	0.9	1.8	0.7	1.0
-100.0	-16.3	-49.8	-74.6	-81.4	3.9	3.0	1.1	4.4
-75.0	-17.0	-50.7	-75.0	-83.5	5.6	4.2	1.0	5.5
-50.0	-19.3	-51.8	-75.2	-84.3	3.1	4.4	1.3	0.5
-25.0	-19.6	-52.9	-75.4	-86.1	1.2	3.5	2.1	-4.6
0.0	-19.8	-54.0	-76.1	-82.2	2.0	2.5	3.9	2.5
25.0	-20.3	-54.2	-76.6	-83.6	3.3	25.8	5.0	9.2
50.0	-21.1	-55.2	-78.8	-87.2	*	*	*	*
75.0	-22.3	-78.8	-78.9	-87.8	*	*	*	*

LINE L81E								
OPERATOR D.M.W. Nparm=4								
STATION 112/37 337/37 1012/3 3037/3					FF1	FF2	FF3	FF4
-525.0	-0.8	-0.5	0.0	0.6	*	*	*	*
500.0	-0.3	1.2	2.9	4.5	-1.3	-3.5	-6.0	-7.8
475.0	-0.1	1.7	3.8	6.0	-1.5	-2.9	-3.9	-2.1
-450.0	0.3	2.5	5.1	6.9	-1.7	-2.6	-1.2	6.9
425.0	0.8	3.3	5.5	5.7	-1.2	-1.2	2.0	14.7
400.0	1.1	3.5	4.6	0.3	-0.9	-0.3	1.8	11.2
-375.0	1.2	3.5	4.0	-2.4	-1.3	-0.2	-0.2	1.3
350.0	1.6	3.6	4.3	-2.8	-0.9	0.8	3.1	6.6
325.0	2.0	3.6	4.5	-0.6	0.0	3.1	14.4	39.8
-300.0	1.7	2.7	0.7	-11.2	-0.1	4.4	21.5	59.2
-275.0	1.9	1.4	-6.3	-32.0	-0.2	3.9	16.4	37.1
250.0	1.9	0.5	-10.0	-39.0	0.5	3.9	8.9	12.5
-225.0	1.9	-0.3	-12.0	-41.3	1.2	3.9	4.3	2.9
-200.0	1.4	-1.7	-13.2	-42.2	0.9	2.8	1.5	-1.7
175.0	1.2	-2.0	-13.1	-41.0	0.3	2.9	2.4	1.1
150.0	1.2	-2.8	-13.6	-40.8	0.7	4.2	6.3	9.4
-125.0	1.1	-3.8	-15.1	-43.5	1.4	4.7	9.6	15.4
100.0	0.6	-5.2	-17.9	-47.7	1.1	4.3	9.9	16.6
-75.0	0.3	-6.1	-20.4	-52.0	0.7	3.8	9.0	14.6
-50.0	0.3	-7.2	-22.5	-55.8	0.9	3.1	7.8	10.9
-25.0	-0.1	-7.9	-24.8	-58.5	0.8	2.6	6.3	8.5
0.0	-0.2	-8.5	-25.9	-60.2	0.5	3.2	6.2	8.4
25.0	-0.4	-9.2	-27.7	-62.6	1.1	4.3	6.8	8.5
50.0	-0.4	-10.4	-29.2	-64.5	1.9	4.1	6.5	7.5
75.0	-1.3	-11.6	-31.2	-66.8	1.2	3.1	5.3	6.3
100.0	-1.4	-12.1	-32.2	-67.8	*	*	*	*
125.0	-1.5	-13.0	-33.5	-69.8	*	*	*	*

TWIN GRID - LARGE LOOP EM LINE 8100E
DATE 05 DEC. 1986 OPERATOR D.W. LOOP#6 LOOP 600x500m Nparm=4

STATION	112/37	337/37	1012/3	3037/3	FF1	FF2	FF3	FF4
-1000.0	-0.8	1.4	4.1	5.5	*	*	*	*
-975.0	-0.3	3.1	6.8	9.7	-2.4	-6.6	-10.8	-15.4
-950.0	0.6	5.1	10.0	14.2	-1.8	-5.2	-8.4	-10.1
-925.0	0.7	6.0	11.7	16.4	-1.7	-4.4	-6.4	-5.9
-900.0	1.4	7.4	13.5	17.6	-1.5	-3.3	-4.3	-4.8
-875.0	1.6	8.1	14.6	18.9	-0.6	-0.1	2.8	4.3
-850.0	2.0	8.6	14.9	19.9	0.7	5.8	16.9	29.2
-825.0	1.6	7.0	10.4	12.3	1.3	11.0	29.8	53.8
-800.0	1.3	3.9	2.2	-2.7	1.4	12.1	33.2	57.3
-775.0	1.0	0.7	-6.7	-18.9	1.8	10.9	28.6	42.5
-750.0	0.5	-1.9	-13.9	-28.8	1.8	10.3	23.8	29.6
-725.0	0.0	-4.4	-19.2	-35.3	1.5	9.9	22.1	25.0
-700.0	-0.3	-7.1	-25.2	-42.0	1.7	8.9	20.6	23.0
-675.0	-0.7	-9.1	-30.0	-47.1	2.1	9.0	18.4	22.0
-650.0	-1.3	-11.3	-35.0	-53.2	1.4	8.3	15.2	18.5
-625.0	-1.8	-13.9	-38.6	-57.9	0.8	6.6	12.6	13.6
-600.0	-1.6	-14.8	-41.6	-60.9	2.3	6.9	11.4	10.2
-575.0	-2.3	-17.0	-44.6	-63.8	2.6	7.9	10.4	7.7
-550.0	-3.4	-18.6	-47.0	-65.2	1.0	8.1	10.1	6.3
-525.0	-3.1	-21.1	-49.6	-67.2	1.8	8.1	9.8	5.2
-500.0	-3.6	-22.6	-52.1	-68.1	2.9	9.0	8.8	5.3
-475.0	-4.7	-25.2	-54.3	-69.5	2.5	9.2	8.8	6.5
-450.0	-4.9	-27.5	-56.2	-71.1	3.4	8.8	10.1	8.0
-425.0	-5.9	-29.5	-59.0	-73.0	*	*	*	*
-400.0	-7.1	-32.0	-61.6	-75.6	*	*	*	*

MAIN GRID - LARGE LOOP EM LINE L82E
 DATE 11/06/86 OPERATOR D.M.W. Nparm=4

STATION	112/37	337/37	1012/3	3037/3	FF1	FF2	FF3	FF4
-525.0	0.7	0.1	0.8	1.2	*	*	*	*
500.0	-0.5	1.0	3.0	5.7	-0.6	-4.9	-8.4	-11.2
475.0	0.2	2.6	5.5	8.1	-1.9	-3.9	-5.7	-5.7
-450.0	0.6	3.4	6.7	10.0	-1.8	-2.6	-2.6	2.4
425.0	1.0	4.1	7.5	9.5	-1.7	-1.3	1.3	14.5
400.0	1.6	4.5	7.3	6.2	-1.2	0.2	5.0	22.4
-375.0	1.7	4.3	5.6	-1.2	-0.8	1.1	5.7	18.5
350.0	2.1	4.1	4.2	-5.5	-0.3	2.2	7.4	17.7
325.0	2.0	3.6	3.0	-8.0	0.1	3.7	12.3	29.8
-300.0	2.1	2.6	-0.6	-16.4	0.3	4.4	14.1	35.4
-275.0	1.9	1.4	-4.5	-26.9	0.7	4.7	12.1	26.2
250.0	1.9	0.4	-7.2	-32.9	1.2	4.8	10.0	15.6
225.0	1.4	-1.1	-10.0	-36.6	0.9	4.0	7.7	10.0
-200.0	1.2	-1.9	-11.7	-38.8	0.4	3.8	6.4	8.1
175.0	1.2	-2.8	-13.2	-40.7	0.6	4.4	7.5	10.5
150.0	1.0	-4.0	-14.9	-42.8	1.0	5.1	10.9	16.4
-125.0	0.8	-5.1	-17.5	-47.2	1.5	5.2	12.0	18.2
100.0	0.4	-6.8	-21.5	-52.7	1.5	4.8	9.4	14.4
-75.0	-0.1	-7.5	-22.9	-55.5	1.0	4.3	8.1	11.3
-50.0	-0.2	-9.2	-25.5	-58.8	1.5	3.3	7.6	5.3
-25.0	-0.5	-9.4	-27.0	-60.7	*	*	*	*
0.0	-1.3	-10.6	-29.0	-58.9	*	*	*	*

TWIN GRID - LARGE LOOP EM LINE 8200E
DATE 05 DEC. 1986 OPERATOR D.W. LOOP#6 LOOP 600x500m Nparm=4

STATION	112/37	337/37	1012/3	3037/3	FF1	FF2	FF3	FF4
-950.0	1.0	6.9	13.4	17.0	*	*	*	*
-925.0	1.5	8.5	15.3	18.8	-2.4	-5.5	-7.1	-5.1
-900.0	2.2	9.8	17.2	19.9	-1.6	-3.6	-3.2	-0.9
-875.0	2.7	11.1	18.6	21.0	-0.3	0.9	6.2	11.6
-850.0	2.6	10.8	17.1	18.6	0.3	6.2	18.6	31.4
-825.0	2.6	9.2	12.5	10.7	1.2	11.3	31.4	52.2
-800.0	2.4	6.5	4.6	-2.5	2.5	13.9	36.3	57.4
-775.0	1.6	2.2	-6.4	-20.4	2.5	12.6	31.2	45.0
-750.0	0.9	-0.4	-12.8	-28.8	1.7	11.3	27.0	34.5
-725.0	0.6	-3.5	-20.2	-39.1	1.6	10.7	24.3	27.0
-700.0	0.2	-6.0	-26.0	-44.6	1.5	9.5	21.0	22.3
-675.0	-0.3	-8.6	-31.3	-50.3	1.2	8.1	17.7	20.1
-650.0	-0.4	-10.4	-35.9	-55.7	1.4	7.1	14.1	15.1
-625.0	-0.9	-12.3	-39.1	-59.3	1.4	6.7	12.2	11.7
-600.0	-1.2	-13.8	-42.2	-61.8	1.3	6.7	10.8	9.6
-575.0	-1.5	-15.6	-45.0	-64.9	1.2	6.5	9.5	5.9
-550.0	-1.9	-17.2	-47.1	-65.8	1.3	6.0	8.7	3.2
-525.0	-2.0	-18.7	-49.6	-66.8	1.9	6.3	7.8	1.9
-500.0	-2.7	-20.1	-51.2	-67.1	2.0	7.7	9.1	2.5
-475.0	-3.1	-22.1	-53.3	-67.4	1.8	9.3	10.3	4.8
-450.0	-3.6	-24.4	-56.6	-69.0	3.3	9.1	7.8	6.5
-425.0	-4.0	-27.1	-58.2	-70.3	*	*	*	*
-400.0	-6.0	-28.5	-59.5	-72.6	*	*	*	*

PIN GRID - LARGE LOOP EM LINE L83E
 DATE 11/06/86 OPERATOR D.M.W. Nparm=4

STATION	112/37	337/37	1012/3	3037/3	FF1	FF2	FF3	FF4
-525.0	-0.8	0.4	1.8	2.7	*	*	*	*
-500.0	0.2	2.5	5.3	7.4	-2.7	-5.7	-9.1	-11.3
-475.0	0.8	3.7	7.1	10.0	-2.2	-4.5	-6.5	-4.2
-450.0	1.3	4.9	9.1	11.4	-1.9	-2.8	-1.2	10.8
-425.0	1.9	5.8	9.8	10.2	-1.4	-0.4	5.4	26.8
-400.0	2.1	5.6	7.6	0.4	-0.8	1.4	7.8	27.2
-375.0	2.5	5.5	5.9	-5.6	-0.1	2.9	8.3	21.9
-350.0	2.3	4.5	3.7	-11.0	-0.4	3.2	8.1	18.5
-325.0	2.4	3.7	1.5	-16.1	-0.5	3.8	8.5	17.5
-300.0	2.8	3.1	0.0	-19.0	0.7	5.3	10.6	19.5
-275.0	2.4	1.3	-3.3	-25.6	1.0	4.4	8.3	15.5
-250.0	2.1	0.2	-5.8	-29.0	0.6	3.9	6.9	12.8
-225.0	2.1	-0.2	-5.8	-31.1	1.0	6.5	12.9	18.5
-200.0	1.8	-2.2	-10.2	-36.3	1.5	7.7	15.9	22.0
-175.0	1.4	-4.3	-14.3	-42.3	1.9	6.8	14.4	21.8
-150.0	1.0	-5.8	-17.6	-47.1	1.5	5.9	13.1	19.4
-125.0	0.3	-7.5	-21.3	-53.3	0.9	5.1	10.8	14.3
-100.0	0.6	-8.5	-23.7	-55.5	1.4	4.9	8.2	11.2
-75.0	-0.2	-9.9	-26.0	-59.2	*	*	*	*
-50.0	-0.3	-11.0	-27.2	-60.8	*	*	*	*

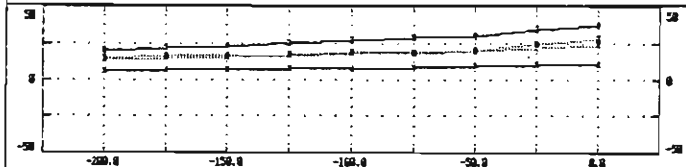
TWIN GRID - LARGE LOOP EM LINE 8300e
 DATE 12/06/86 OPERATOR D.M.W. Nparm=4

STATION	112/37	337/37	1012/3	3037/3	FF1	FF2	FF3	FF4
-950.0	1.9	10.0	16.4	14.4	*	*	*	*
-925.0	3.1	12.7	20.3	18.0	-2.2	-7.8	-10.6	-9.6
-900.0	3.1	14.3	22.3	19.7	-2.4	-6.3	-8.0	-6.5
-875.0	4.1	16.2	25.0	22.3	-2.2	-3.0	-0.8	4.8
-850.0	4.5	17.1	25.6	21.9	-0.5	3.6	13.3	26.7
-825.0	4.9	16.4	22.5	15.3	1.8	12.3	31.6	50.0
-800.0	4.2	13.3	14.8	2.2	3.6	19.7	46.7	64.8
-775.0	3.4	7.9	1.7	-15.0	3.7	21.4	49.2	63.5
-750.0	2.1	2.1	-11.1	-32.3	2.7	17.8	40.8	48.7
-725.0	1.8	-2.3	-21.6	-44.0	2.3	12.9	30.9	33.4
-700.0	1.0	-5.5	-28.6	-52.0	1.7	9.3	22.9	22.9
-675.0	0.6	-7.6	-35.0	-57.7	1.0	7.3	15.8	15.8
-650.0	0.5	-9.5	-38.1	-61.2	0.8	6.6	13.2	12.6
-625.0	0.1	-10.9	-41.3	-64.3	0.4	6.8	13.2	9.8
-600.0	0.2	-12.8	-45.0	-67.2	0.7	6.7	11.8	6.3
-575.0	0.0	-14.4	-47.6	-68.1	1.4	5.9	10.0	4.5
-550.0	-0.4	-16.0	-50.5	-69.7	1.7	5.6	7.7	1.5
-525.0	-0.8	-17.1	-52.1	-70.1	2.3	6.2	6.5	-1.1
-500.0	-1.3	-18.9	-53.7	-69.2	3.6	8.4	7.1	0.3
-475.0	-2.2	-20.4	-55.4	-69.5	4.2	10.6	8.6	2.9
-450.0	-3.5	-24.0	-57.5	-70.1	3.0	9.4	9.3	6.6
-425.0	-4.2	-25.9	-60.2	-71.5	*	*	*	*
-400.0	-4.5	-27.9	-62.0	-74.7	*	*	*	*

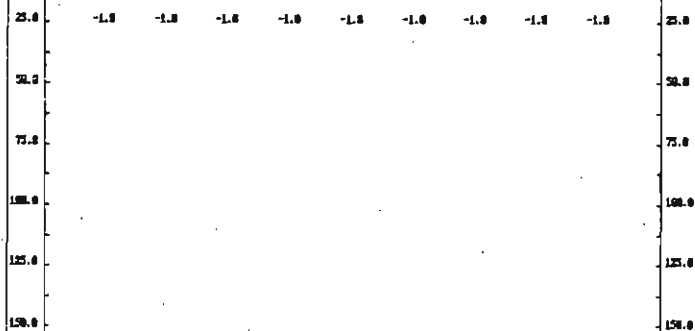
TWIN GRID - LARGE LOOP EM LINE 5380E

DATE 11/28/26 OPERATOR N.M. LOOP#3 LOOP 1180x752a

112/37	6.3	7.2	7.6	8.0	8.4	8.8	9.2	9.6	10.0
112/37/37		-1.3	-1.6	-1.8	-2.1	-2.3	-2.5	-2.7	
337/37	13.8	15.1	16.2	17.3	18.4	19.4	20.3	21.4	22.6
337/37/37		-4.4	-4.4	-4.3	-4.3	-5.1	-4.3		
1812/3	28.3	28.2	28.4	28.4	27.5	28.4	28.5	28.3	27.4
1812/3/37		-6.2	-7.2	-7.3	-6.4	-6.4	-12.5		
3837/3	15.4	16.7	16.3	17.7	15.4	12.6	22.8	24.3	22.8
3837/3/37		-2.2	-3.4	-3.5	-2.7	-7.3	-13.1		



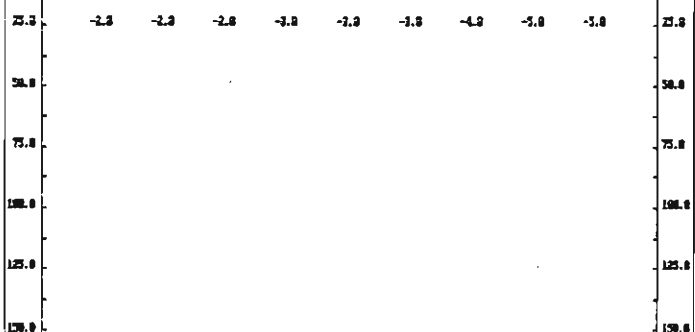
Pseudo-section of Filtered 112/37



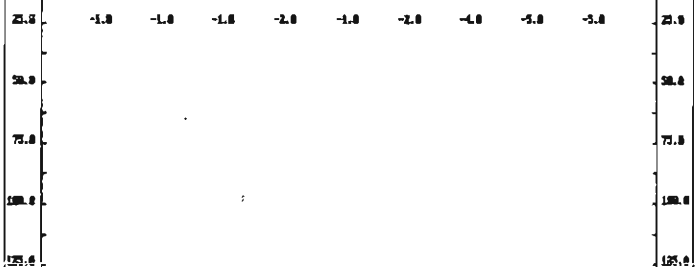
Pseudo-section of Filtered 337/37



Pseudo-section of Filtered 1812/3



Pseudo-section of Filtered 3837/3

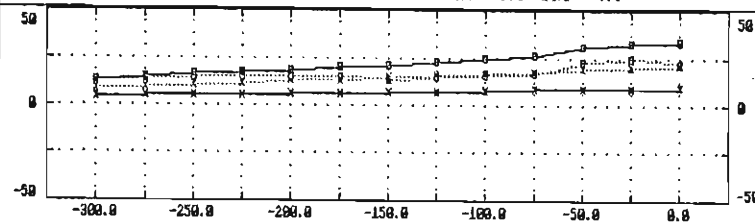


TWIN GRID - LARGE LOOP EM

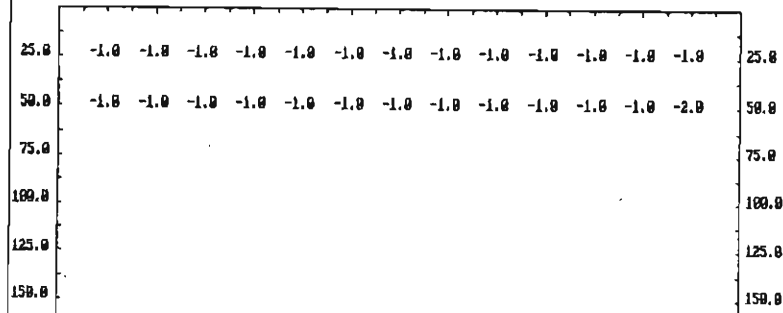
LINE 5400

DATE 11/30/86 OPERATOR N.M.

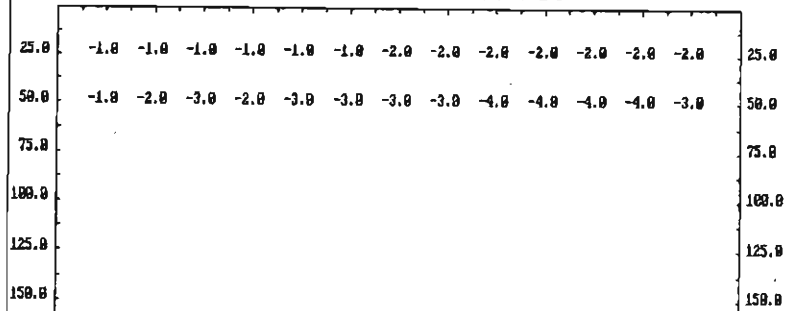
112/37	4.4	5.8	5.4	5.7	6.1	6.7	7.8	7.4	7.8	8.5	8.7	9.3	9.8
112/37:FF		-1.7	-1.4	-1.7	-1.9	-1.6	-1.5	-1.9	-2.8	-1.7	-1.9		
337/37	9.0	9.9	11.8	11.8	13.0	13.7	14.8	15.7	16.8	17.9	19.8	20.8	21.7
337/37:FF		-3.9	-3.9	-3.9	-3.7	-3.8	-4.8	-4.2	-5.2	-5.9	-4.8		
1012/3	13.5	15.1	16.6	17.6	19.0	20.2	21.3	22.9	24.0	26.9	30.6	33.1	33.4
1012/3:FF		-5.6	-4.9	-5.8	-4.9	-5.8	-6.2	-7.5	-9.8	-12.9	-9.8		
3037/3	13.6	14.1	15.2	14.8	15.8	14.8	13.5	14.7	15.8	17.1	22.8	24.9	22.4
3037/3:FF		-2.3	-0.5	0.2	1.5	1.6	-2.2	-4.7	-9.4	-14.8	-7.4		



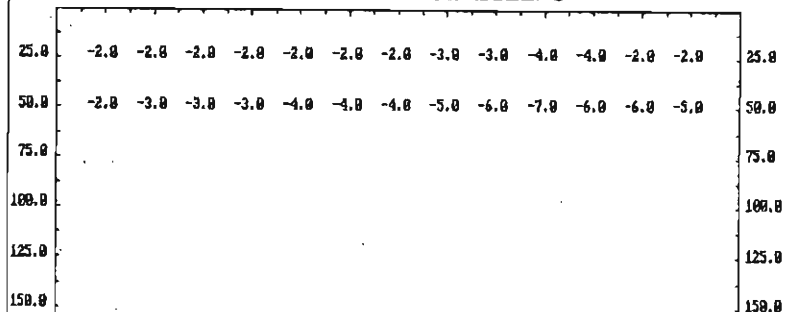
Pseudo-section of Filtered 112/37



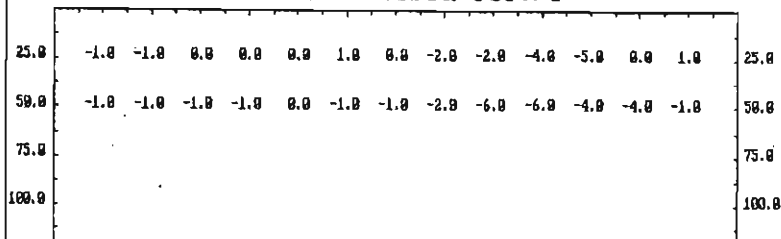
Pseudo-section of Filtered 337/37



Pseudo-section of Filtered 1012/3



Pseudo-section of Filtered 3037/3

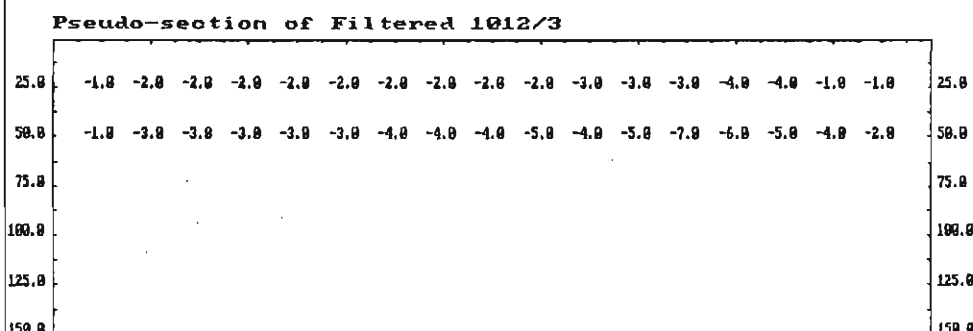
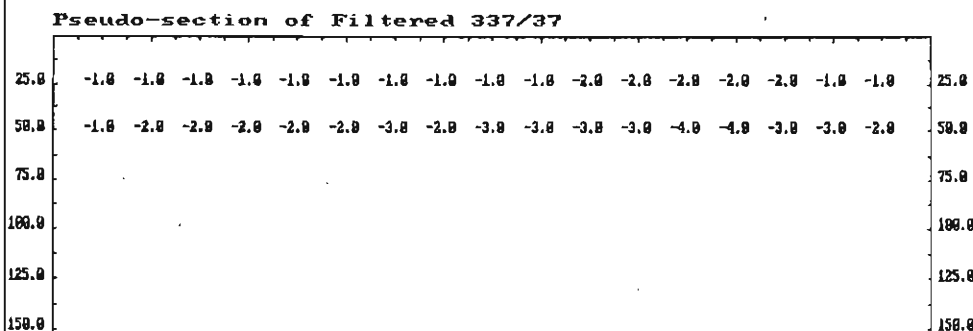
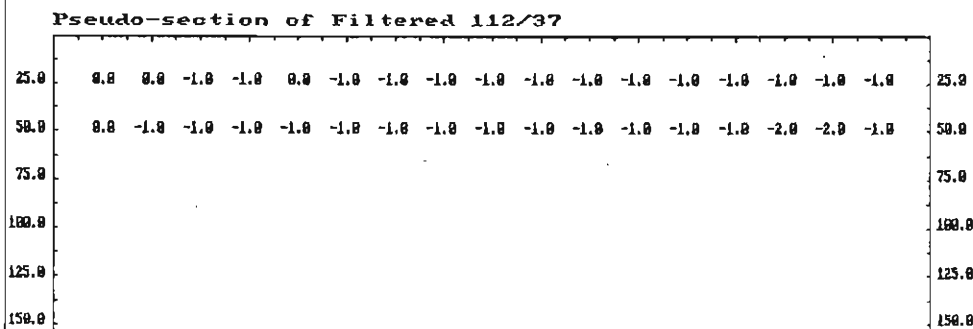
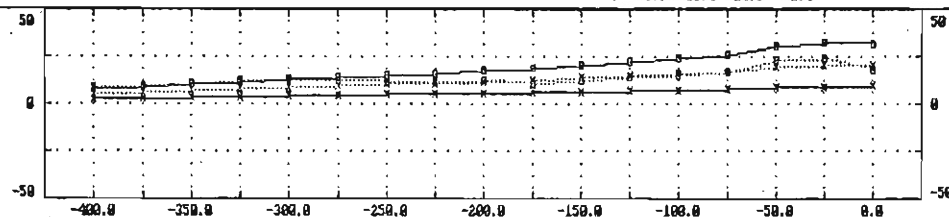


TWIN GRID - LARGE LOOP EM

LINE 5509E

DATE 11/30/86 OPERATOR N.M.

112/37	2.9	3.2	3.6	3.9	4.3	4.5	5.0	5.4	5.7	6.1	6.7	7.2	7.4	7.9	8.5	9.1	9.5
112/37:FF	-1.4	-1.4	-1.3	-1.3	-1.6	-1.6	-1.4	-1.7	-2.1	-1.8	-1.4	-1.8	-2.3	-2.2			
337/37	5.5	6.1	7.0	7.9	8.7	9.5	10.3	11.1	12.0	12.7	14.0	15.2	16.1	17.2	19.1	20.3	20.5
337/37:FF	-3.3	-3.5	-3.3	-3.2	-3.2	-3.3	-3.3	-3.6	-4.5	-4.6	-4.1	-5.0	-6.1	-4.5			
1012/3	7.8	8.9	10.3	11.8	13.0	13.9	15.0	16.1	17.0	18.3	20.2	22.0	23.8	25.8	30.0	31.8	30.8
1012/3:FF	-5.4	-5.6	-4.8	-4.1	-4.2	-5.0	-5.0	-4.6	-6.1	-7.3	-7.4	-10.0	-12.2	-6.8			
3037/3	9.2	9.8	10.7	12.1	12.6	12.2	11.7	11.4	12.3	10.8	12.1	13.8	14.7	17.1	22.8	23.5	17.8
3037/3:FF	-3.8	-4.2	-2.8	0.8	1.7	0.2	0.0	0.8	-2.8	-5.6	-5.9	-11.4	-14.5	-1.4			

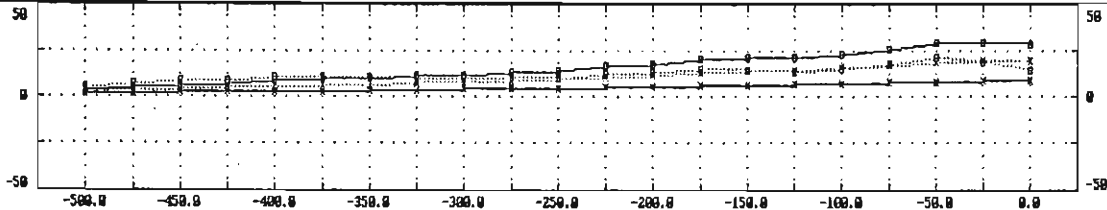


TWIN GRID - LARGE LOOP EM

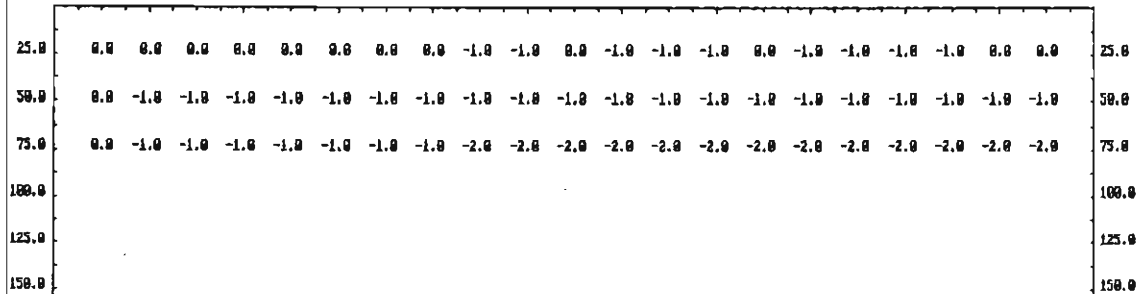
LINE 5600E

DATE 11/10/86 OPERATOR N.M.

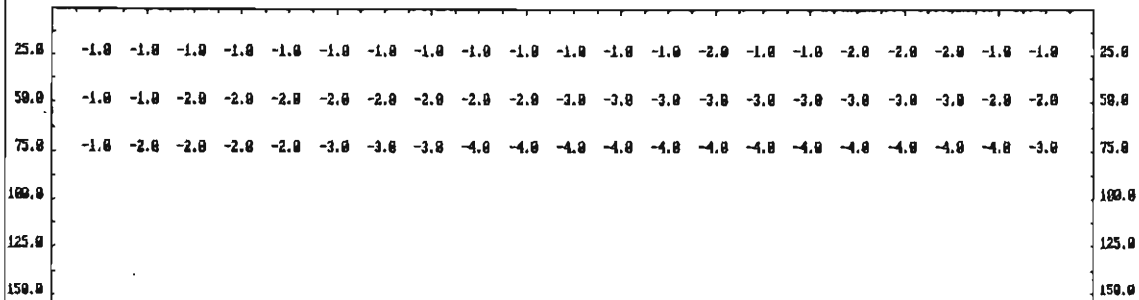
112/37	2.8	2.3	2.6	2.8	3.0	3.2	3.4	3.8	4.1	4.6	4.8	5.2	5.8	6.2	6.7	6.8	7.6	7.8	8.4	8.8	9.0
112/37:FF	-1.1	-0.9	-0.8	-0.8	-1.0	-1.3	-1.3	-1.5	-1.3	-1.6	-2.0	-1.9	-1.5	-1.5	-1.9	-1.8	-1.8	-1.6			
337/37	3.3	4.0	4.6	5.1	5.9	6.3	6.7	7.7	8.4	9.3	10.0	11.1	12.0	13.2	14.2	14.4	15.8	16.8	18.4	19.1	19.3
337/37:FF	-2.4	-2.3	-2.4	-2.1	-2.3	-3.1	-3.3	-3.2	-3.4	-3.8	-4.1	-4.3	-3.4	-2.8	-4.0	-5.8	-4.9	-3.2			
1012/3	3.9	5.3	6.5	7.3	8.5	9.5	10.1	11.2	12.0	13.4	14.4	16.5	17.9	20.0	21.1	21.1	23.4	25.5	28.9	29.2	28.0
1012/3:FF	-4.6	-4.0	-4.2	-3.0	-3.3	-3.6	-4.1	-4.6	-5.5	-6.6	-7.0	-6.7	-4.3	-3.4	-6.7	-9.9	-9.2	-2.0			
3037/3	5.3	7.5	8.7	9.3	10.4	10.9	10.8	10.2	10.0	10.5	10.2	12.5	13.3	15.3	14.4	13.0	15.3	17.4	21.3	19.8	13.8
3037/3:FF	-5.2	-3.5	-3.3	-2.0	0.3	1.5	0.5	-0.5	-2.2	-5.1	-5.9	-3.9	1.2	1.4	-5.3	-10.4	-7.4	6.1			



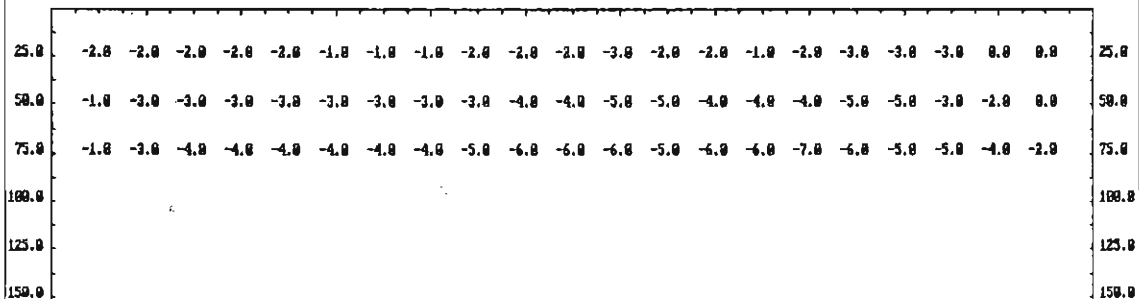
Pseudo-section of Filtered 112/37



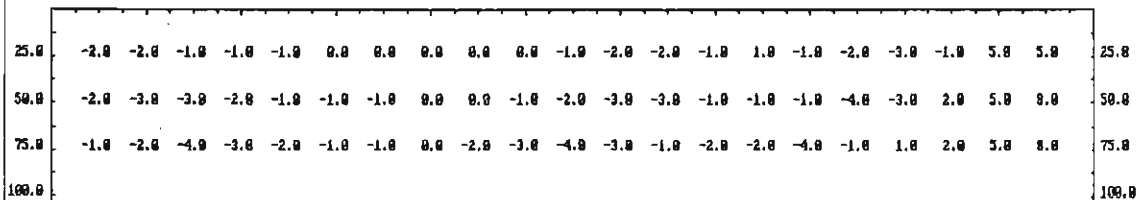
Pseudo-section of Filtered 337/37



Pseudo-section of Filtered 1012/3



Pseudo-section of Filtered 3037/3

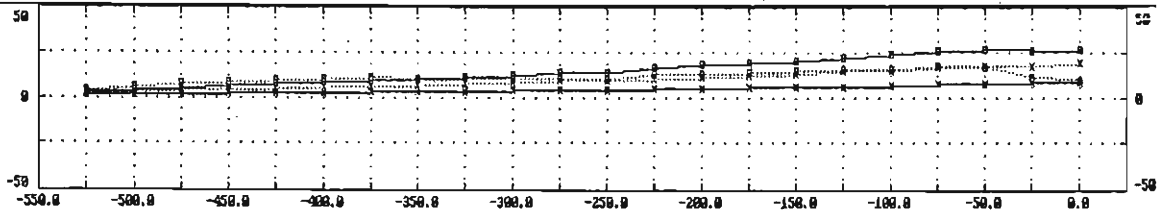


TWIN GRID - LARGE LOOP EM

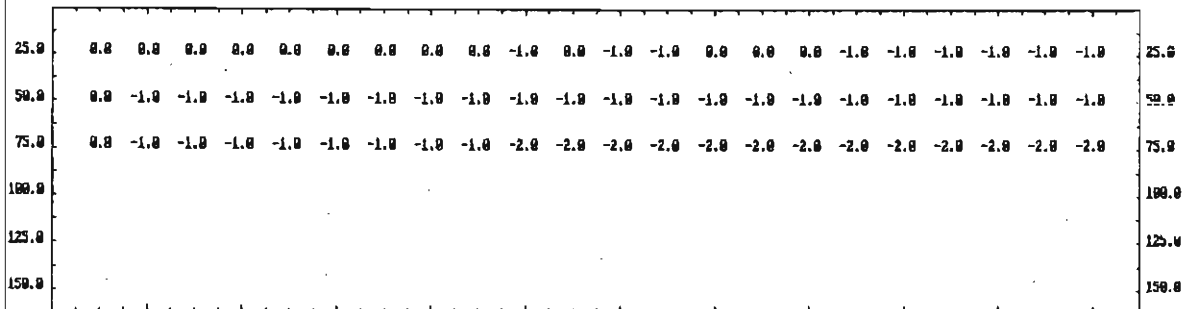
LINE 5700E

DATE 11/30/86 OPERATOR H.M.

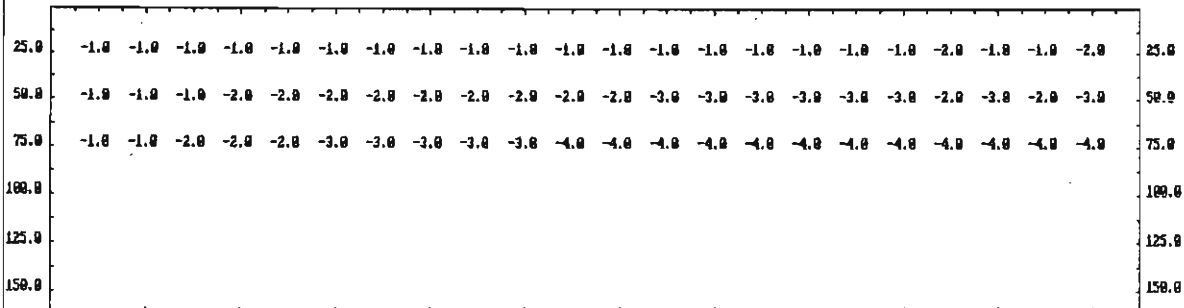
112/37	1.9	2.1	2.3	2.6	2.8	3.1	3.3	3.5	3.8	4.2	4.5	4.8	5.4	5.8	6.0	6.2	6.5	7.2	7.9	8.1	8.5	9.0
112/37:FF	-8.9	-1.0	-1.0	-1.0	-0.9	-0.9	-1.2	-1.4	-1.3	-1.5	-1.9	-1.6	-1.8	-0.9	-1.5	-2.4	-2.3	-1.5	-1.5			
337/37	3.0	3.6	4.2	4.8	5.3	6.0	6.5	7.1	8.0	8.6	9.4	9.9	11.1	12.0	12.9	13.7	14.8	15.5	17.0	17.5	17.5	19.1
337/37:FF	-2.4	-2.3	-2.3	-2.4	-2.3	-2.6	-3.0	-2.9	-2.7	-3.0	-3.0	-3.9	-3.5	-3.6	-3.7	-4.0	-4.2	-2.5	-2.1			
1012/3	3.3	4.5	5.6	6.8	7.8	8.9	9.9	10.4	11.7	12.5	13.0	14.5	16.9	18.2	19.2	20.5	22.5	23.6	25.8	26.5	25.8	26.5
1012/3:FF	-4.6	-4.5	-4.3	-4.2	-3.6	-3.3	-3.9	-4.2	-4.1	-5.1	-6.0	-6.0	-4.6	-5.6	-6.4	-6.4	-6.2	-2.9	0.0			
3037/3	4.1	6.2	7.0	8.9	10.1	10.5	11.2	10.1	10.6	11.0	11.0	10.7	13.6	13.7	14.0	15.1	16.4	16.4	17.9	16.9	11.0	10.0
3037/3:FF	-6.4	-5.0	-3.9	-2.7	-0.7	1.0	-0.3	-1.3	-0.1	-2.3	-5.6	-3.4	-1.8	-3.8	-3.7	-2.8	-2.0	3.6	13.0			



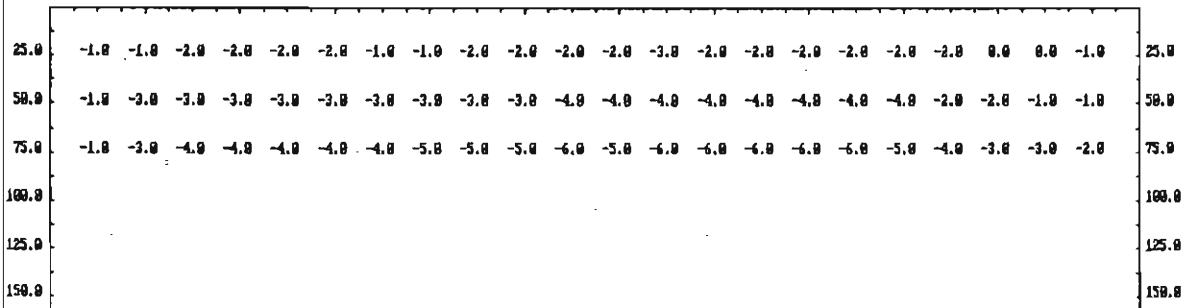
Pseudo-section of Filtered 112/37



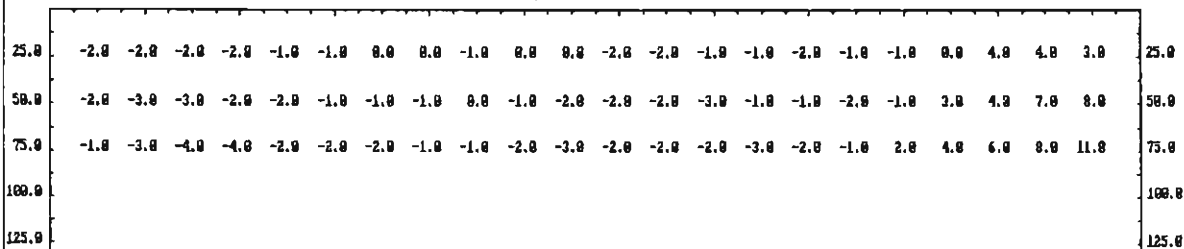
Pseudo-section of Filtered 337/37



Pseudo-section of Filtered 1012/3



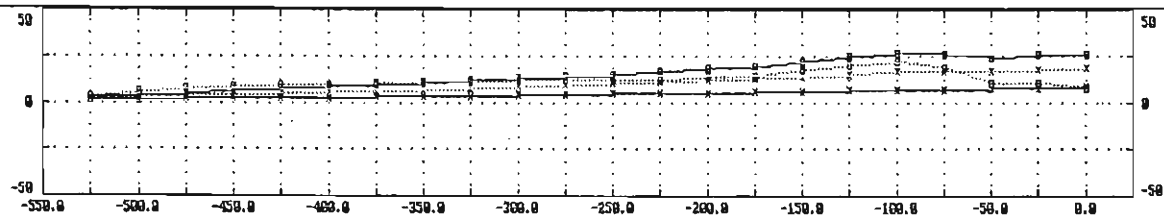
Pseudo-section of Filtered 3037/3



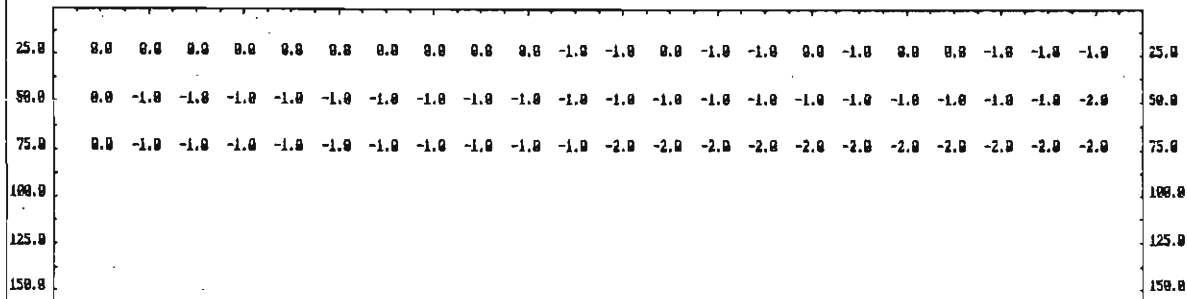
TWIN GRID - LARGE LOOP EM LINE 5800E

DATE 01 DEC. 1986 OPERATOR D.W. LOOP#3 LOOP 1100x750m

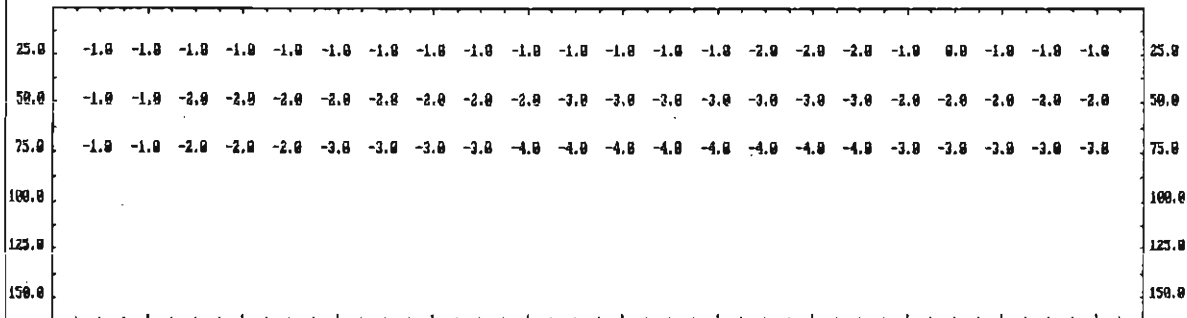
112/37	2.0	2.2	2.5	2.8	2.9	3.1	3.4	3.7	4.0	4.3	4.5	5.0	5.3	5.6	6.1	6.3	6.8	7.5	7.4	7.8	8.2	8.9
112/37:FF	-1.1	-1.8	-0.7	-0.8	-1.1	-1.2	-1.2	-1.1	-1.2	-1.5	-1.4	-1.4	-1.5	-1.4	-1.9	-1.8	-0.9	-1.2	-2.0			
337/37	2.0	2.6	4.2	4.8	5.4	5.9	6.6	7.3	8.0	8.7	9.5	10.3	11.4	12.3	13.1	14.3	15.3	16.7	16.7	17.0	17.7	18.6
337/37:FF	-2.4	-2.4	-2.3	-2.3	-2.5	-2.8	-2.8	-2.9	-3.1	-3.5	-3.9	-3.7	-3.7	-4.2	-4.6	-3.8	-1.7	-1.3	-2.6			
1012/3	3.3	4.7	5.8	6.8	7.8	8.7	9.9	11.0	12.1	13.2	14.1	15.1	16.6	18.2	19.4	22.2	24.6	26.3	25.4	24.1	25.3	25.3
1012/3:FF	-4.6	-4.1	-3.9	-4.0	-4.4	-4.5	-4.4	-4.2	-3.9	-4.4	-5.6	-5.9	-6.8	-9.2	-9.3	-4.9	1.4	2.3	-1.1			
3037/3	3.7	6.3	8.1	8.9	9.7	10.1	10.6	11.4	11.8	12.3	12.1	12.2	12.8	14.2	14.1	18.8	20.5	22.3	10.6	10.7	10.4	0.3
3037/3:FF	-7.8	-4.2	-2.8	-2.1	-2.2	-2.5	-2.1	-1.2	-0.2	-0.6	-2.7	-3.3	-5.1	-10.2	-10.7	-2.4	13.5	19.8	10.6			



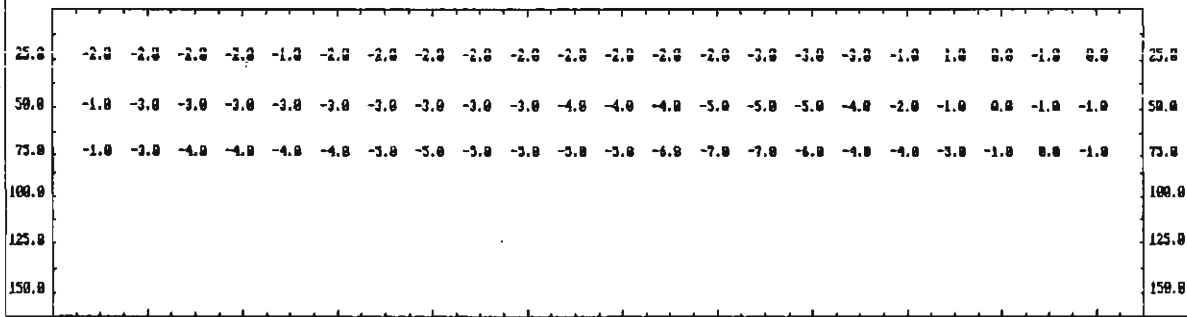
Pseudo-section of Filtered 112/37



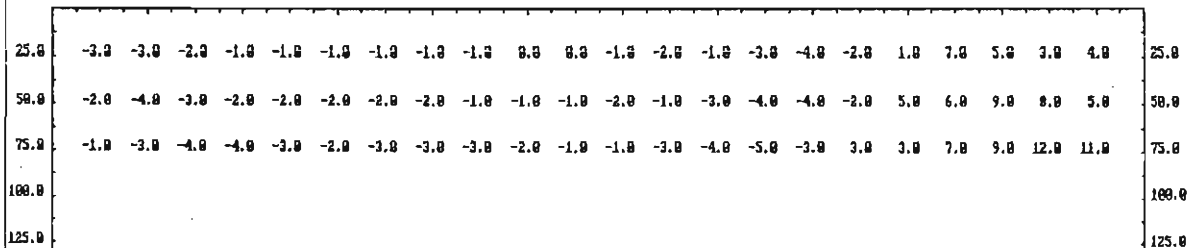
Pseudo-section of Filtered 337/37



Pseudo-section of Filtered 1012/3



Pseudo-section of Filtered 3037/3



TWIN GRID - LARGE LOOP EM

LINE 5800E

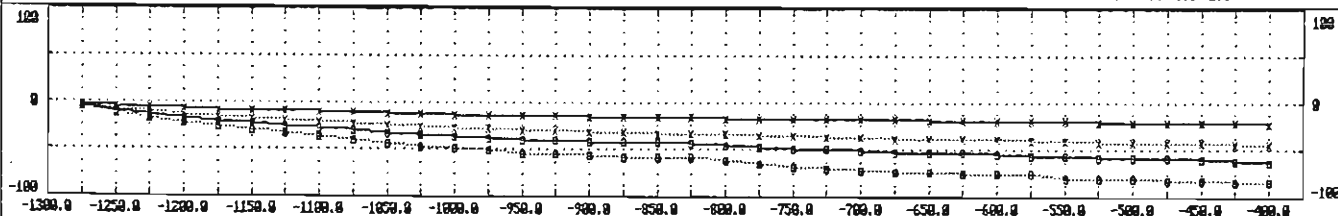
DATE 02 DEC. 1986 OPERATOR S.L. LOOP# 4

112/37 -2.9 -4.3 -5.7 -6.8 -7.8 -8.7 -9.4 -10.6 -11.1 -11.7 -12.5 -13.3 -13.7 -14.2 -14.6 -15.4 -15.3 -15.9 -16.3 -16.6 -17.0 -17.0 -17.4 -17.7 -18.1 -18.2 -18.3 -19.0 -19.7 -19.7 -19.9 -20.4 -20.4 -21.1 -21.7 -22.1
112/37:FF 5.3 4.6 4.0 3.5 3.5 3.6 2.8 2.5 3.0 2.8 2.1 1.8 2.1 1.9 1.2 1.5 1.7 1.4 1.1 0.8 1.1 1.4 1.8 1.9 1.9 1.9 1.7 1.6 1.0 0.3 0.9 2.2 2.3

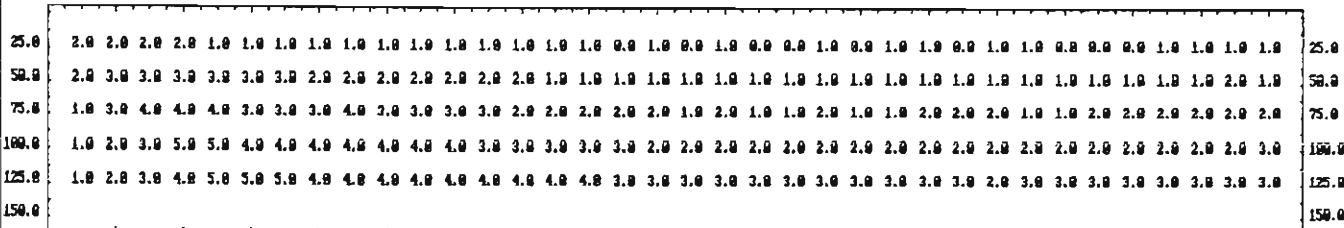
337/37 -4.8 -8.0 -10.9 -13.4 -15.6 -17.6 -19.5 -21.6 -22.9 -24.4 -26.0 -27.6 -28.5 -29.7 -30.5 -31.5 -32.0 -32.5 -33.1 -34.0 -34.9 -35.5 -36.1 -36.7 -37.0 -38.5 -39.0 -39.2 -39.9 -40.5 -41.4 -41.6 -42.0 -42.6 -43.8 -44.3
337/37:FF 11.5 10.1 8.9 8.1 7.9 7.4 6.2 5.9 6.3 5.7 4.6 4.1 3.8 3.3 2.5 2.1 2.6 3.3 3.3 2.7 2.4 2.9 3.5 3.0 1.9 1.6 2.2 2.8 2.6 1.7 1.6 2.8 3.5

1012/3 -5.0 -10.2 -14.0 -17.4 -20.4 -23.2 -25.8 -28.5 -30.4 -32.6 -34.9 -36.6 -38.0 -39.7 -40.7 -41.6 -42.2 -42.4 -43.4 -44.0 -47.1 -48.6 -49.9 -51.0 -51.9 -52.8 -53.3 -53.9 -55.6 -56.9 -57.7 -58.4 -58.8 -60.1 -61.5 -62.4
1012/3:FF 15.4 13.6 12.2 11.2 10.7 9.9 8.7 8.6 8.5 7.1 6.2 5.0 4.6 3.4 2.3 2.0 3.6 6.1 7.5 6.5 5.1 4.5 3.9 3.2 2.5 3.4 5.3 5.1 3.6 2.6 2.8 4.4 5.0

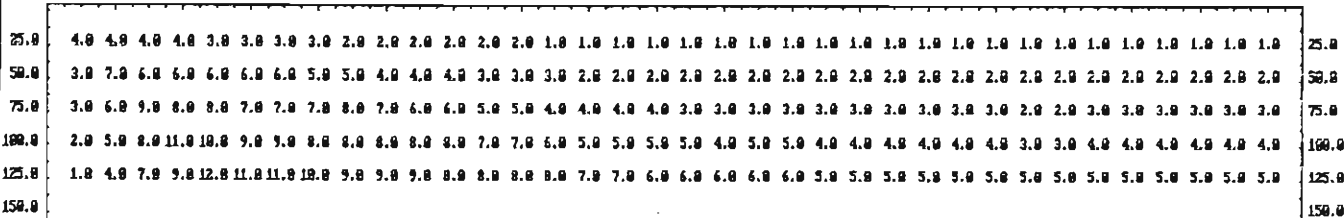
3037/3 -5.6 -11.5 -17.1 -22.2 -26.5 -30.2 -34.0 -37.6 -40.8 -43.5 -46.2 -49.1 -51.3 -53.0 -55.2 -56.4 -57.1 -57.3 -58.4 -61.9 -65.5 -68.3 -70.3 -72.0 -73.4 -74.2 -74.9 -75.2 -75.7 -78.1 -80.0 -81.1 -82.4 -83.3 -84.3
3037/3:FF 22.2 20.1 17.4 15.5 14.9 13.4 11.9 12.7 12.7 10.4 9.9 8.3 6.5 4.5 2.0 2.2 5.9 11.7 13.5 11.2 9.3 7.6 4.5 2.8 2.4 1.9 5.0 10.0 6.1 2.6 3.0 3.5 2.3



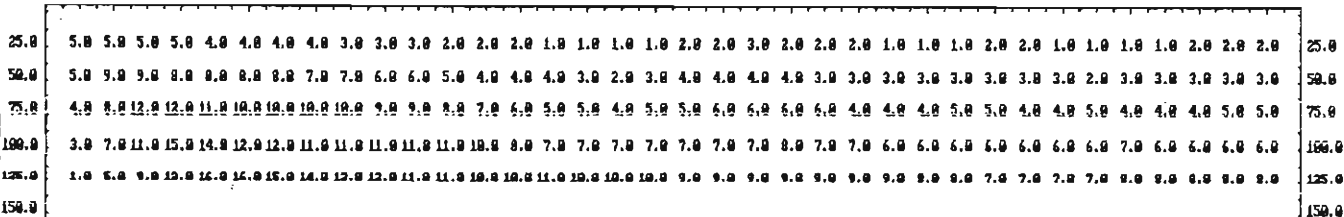
Pseudo-section of Filtered 112/37



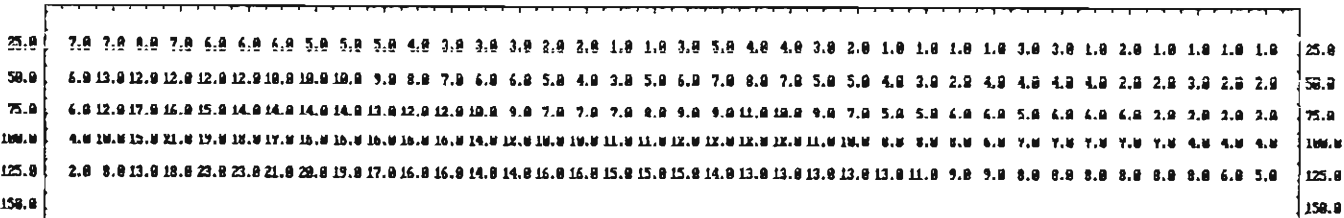
Pseudo-section of Filtered 337/37



Pseudo-section of Filtered 1012/3



Pseudo-section of Filtered 3037/3



TWIN GRID - LARGE LOOP EM

LINE 5900E

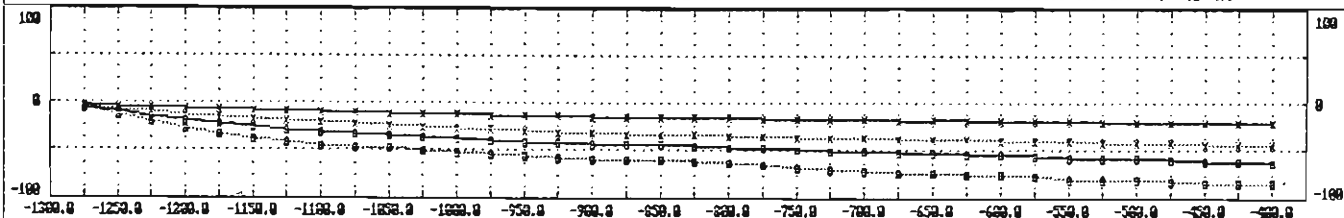
DATE 02 DEC. 1986 OPERATOR S.L. LOOP# 4

112/37 -2.7 -4.5 -5.6 -6.7 -7.5 -8.5 -9.2 -9.3 -10.9 -11.5 -12.1 -12.8 -13.4 -13.6 -14.4 -14.8 -15.0 -15.5 -16.1 -16.2 -16.7 -17.1 -17.8 -17.2 -18.4 -18.1 -19.0 -19.3 -19.5 -19.7 -20.2 -20.6 -20.8 -21.2 -21.6 -21.7
112/37:IT 5.1 4.1 3.7 3.5 3.1 3.1 3.3 2.8 2.5 2.6 2.1 1.8 2.2 1.8 1.3 1.8 1.8 1.3 1.5 1.2 0.4 1.5 2.3 1.5 1.8 1.7 0.9 1.1 1.6 1.5 1.2 1.4 1.3

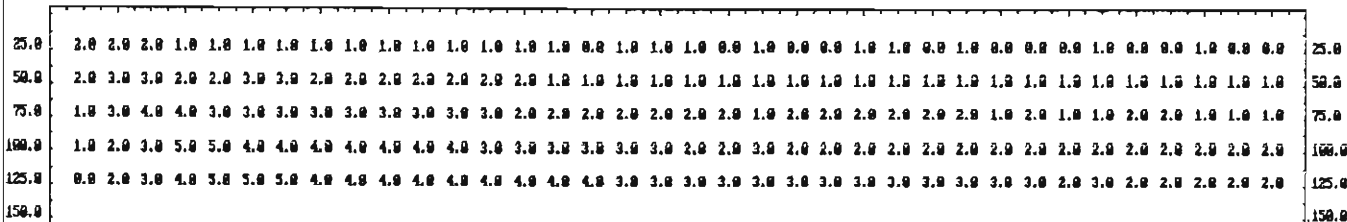
337/37 -4.9 -8.5 -11.1 -13.5 -15.7 -17.0 -19.7 -21.5 -23.4 -24.4 -26.0 -27.4 -28.9 -29.9 -30.9 -31.7 -32.6 -33.0 -34.0 -34.5 -35.4 -36.1 -36.7 -37.3 -38.0 -38.8 -39.4 -39.7 -40.6 -41.0 -41.6 -41.8 -42.2 -43.5 -43.9 -44.2
337/37:IT 11.2 9.6 8.9 8.3 7.7 7.4 6.6 5.5 5.6 5.8 5.3 4.5 3.8 3.6 3.1 2.7 2.9 2.9 3.0 2.9 2.5 2.5 2.8 2.9 2.3 2.1 2.5 2.3 1.8 1.4 2.3 3.4 2.4

1012/3 -6.1 -11.1 -15.2 -19.2 -23.0 -26.3 -29.1 -31.9 -34.1 -34.3 -36.6 -38.7 -40.3 -41.4 -42.6 -43.5 -44.3 -44.5 -45.7 -46.9 -47.0 -49.9 -50.8 -51.7 -52.0 -53.5 -54.3 -54.6 -56.2 -57.1 -58.3 -58.8 -59.4 -60.0 -61.5 -62.4
1012/3:IT 17.2 15.9 14.9 13.2 11.7 10.6 7.4 4.9 6.9 8.1 6.4 5.0 4.4 3.0 2.7 2.4 3.0 4.5 5.1 6.0 4.8 3.8 3.8 3.3 2.6 3.0 4.4 4.6 3.8 2.8 3.1 4.1 3.7

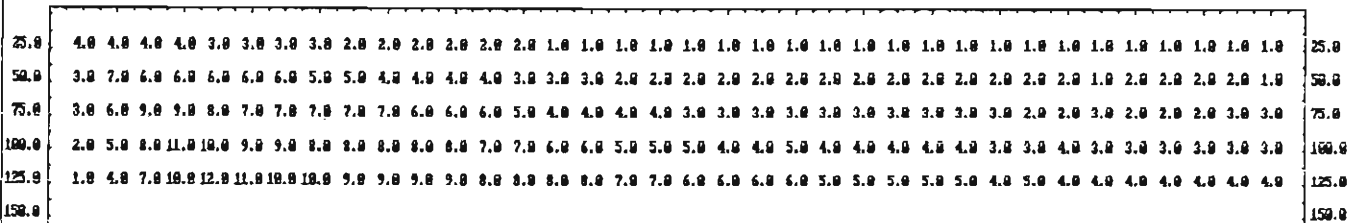
3037/3 -6.5 -14.2 -22.9 -27.0 -33.0 -38.4 -42.9 -45.1 -47.4 -46.7 -50.1 -52.0 -54.9 -56.5 -57.9 -58.9 -60.6 -60.3 -61.9 -63.1 -63.6 -64.7 -70.9 -72.3 -73.9 -74.7 -75.7 -76.2 -78.1 -83.2 -80.5 -81.3 -82.1 -83.6 -84.9 -85.1
3037/3:IT 20.2 26.7 23.5 18.2 14.9 12.1 7.0 4.3 8.0 10.9 8.5 6.7 5.4 5.1 4.1 2.7 4.1 6.5 9.3 10.9 8.9 6.6 5.4 4.2 3.3 3.9 6.4 6.4 3.5 2.7 3.9 5.1 4.3



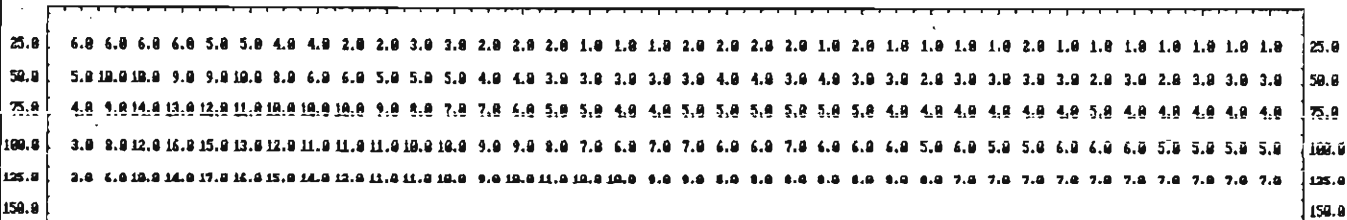
Pseudo-section of Filtered 112/37



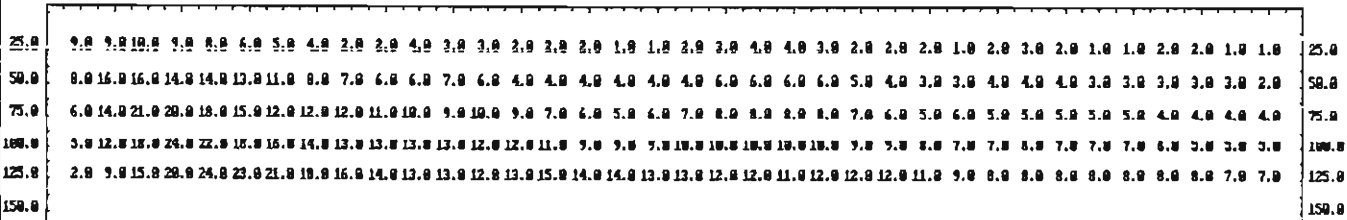
Pseudo-section of Filtered 337/37



Pseudo-section of Filtered 1012/3



Pseudo-section of Filtered 3037/3

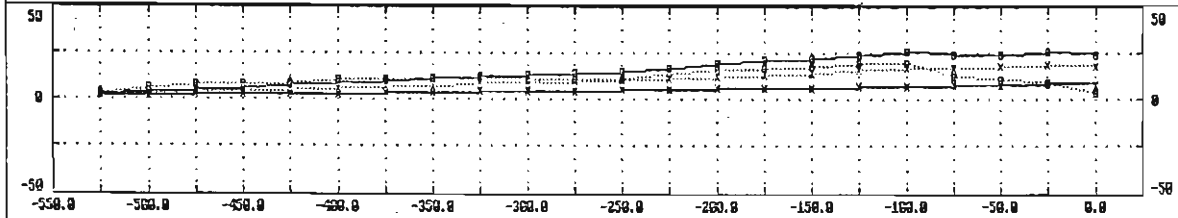


TWIN GRID - LARGE LOOP EM

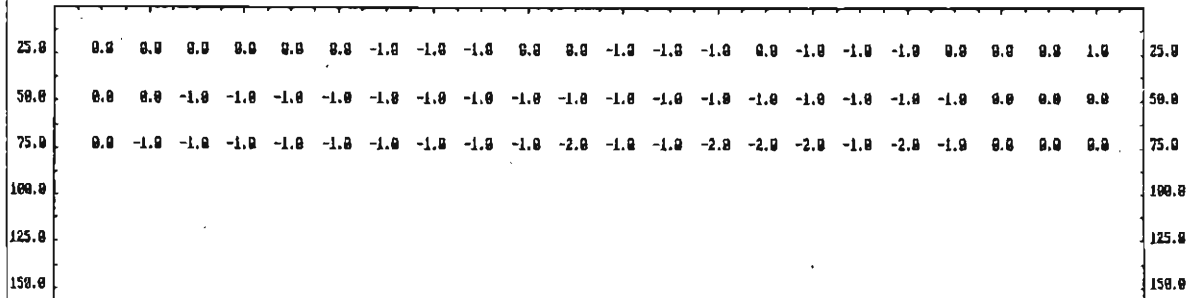
LINE 5900E

DATE 01 DEC. 1986 OPERATOR D.W. LOOP#3 LOOP 1100x750M

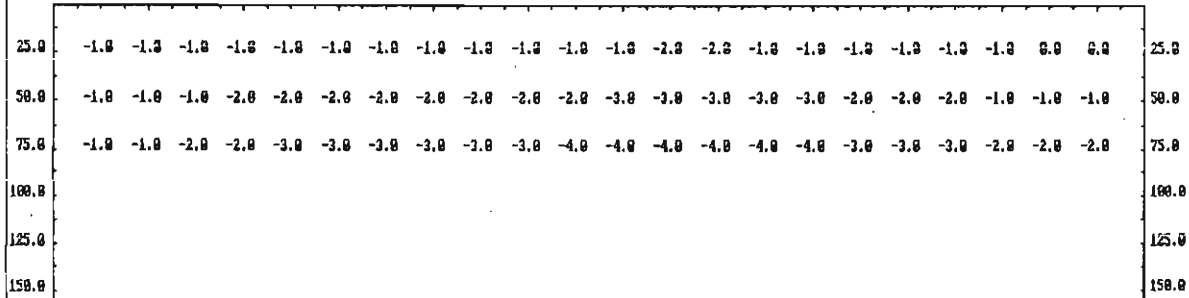
112/37	2.3	2.2	2.4	2.4	3.0	3.1	3.4	3.0	4.2	4.5	4.7	5.1	5.4	5.9	6.1	6.5	7.3	7.6	8.2	8.2	8.9	8.1
112/37:FF	-0.3	-0.8	-1.3	-1.1	-1.1	-1.5	-1.5	-1.2	-1.1	-1.3	-1.5	-1.5	-1.3	-1.8	-2.3	-2.0	-1.5	-1.3	-0.6			
337/37	3.1	3.5	4.3	4.5	5.3	6.0	6.8	7.4	8.6	8.9	9.8	10.5	11.5	12.7	13.7	14.6	15.7	16.7	17.8	17.5	18.6	18.1
337/37:FF	-2.2	-2.0	-2.5	-3.0	-2.9	-3.2	-3.3	-2.7	-2.8	-3.3	-3.9	-4.4	-4.1	-3.9	-4.1	-3.4	-2.1	-2.4	-2.2			
1012/3	3.2	4.5	5.8	6.2	7.8	9.0	10.1	11.5	12.7	13.8	14.2	15.5	17.1	19.6	20.9	22.3	24.2	25.6	24.1	24.0	25.3	24.8
1012/3:FF	-4.3	-3.7	-4.8	-5.1	-4.8	-5.1	-4.1	-3.0	-4.0	-5.4	-7.0	-7.9	-6.5	-6.8	-6.6	-3.2	1.7	0.4	-1.2			
3037/3	3.3	6.0	7.8	8.1	9.3	10.5	10.8	11.2	11.7	11.8	11.1	11.9	13.8	16.4	16.7	17.0	19.7	19.1	12.4	10.5	8.9	4.0
3037/3:FF	-6.6	-3.6	-3.9	-3.9	-2.2	-1.6	-0.7	0.0	-0.3	-3.6	-7.2	-7.4	-4.3	-4.4	-4.3	6.0	15.9	12.1	10.0			



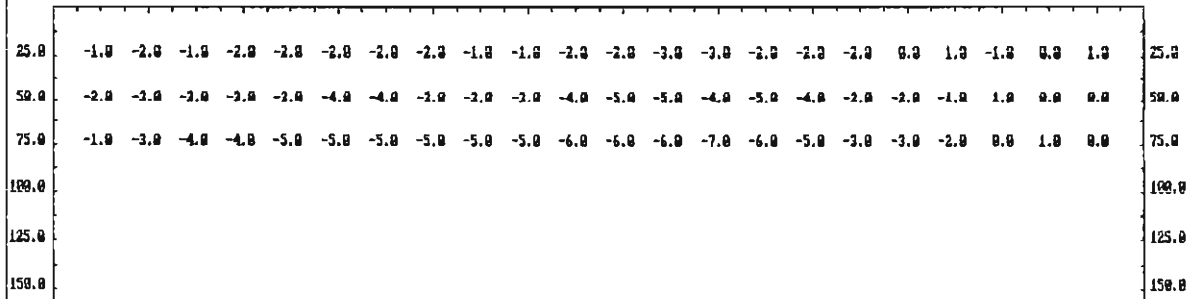
Pseudo-section of Filtered 112/37



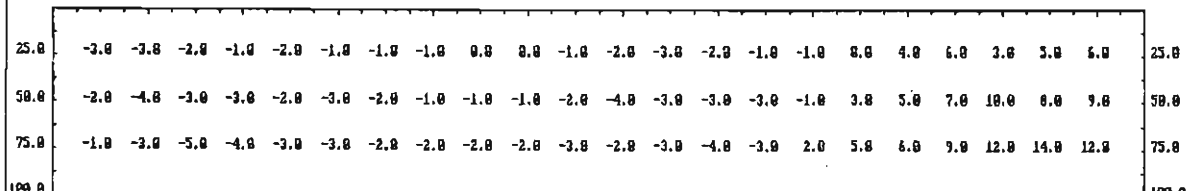
Pseudo-section of Filtered 337/37



Pseudo-section of Filtered 1012/3



Pseudo-section of Filtered 3037/3



TWIN GRID - LARGE LOOP EM

LINE 6000E

DATE 01 DEC. 1986 OPERATOR D.W. S.L. LOOP#3 LOOP 1180x750m Nparm=4

112/37 -1.2 -1.0 -0.7 -0.5 -0.1 -0.1 0.3 0.7 0.9 1.3 1.6 2.1 2.2 2.7 3.2 3.6 3.9 4.2 4.8 5.1 5.3 5.6

112/37:FF -1.0 -1.1 -1.0 -0.8 -1.2 -1.4 -1.2 -1.3 -1.5 -1.4 -1.6 -1.9 -1.6 -1.3 -1.5 -1.0 -1.4 -1.0

337/37 -0.9 -0.2 0.5 1.0 1.9 2.1 2.9 3.7 4.2 5.1 6.2 7.0 7.5 8.3 9.4 10.5 11.4 12.2 12.7 13.0 13.5 14.1

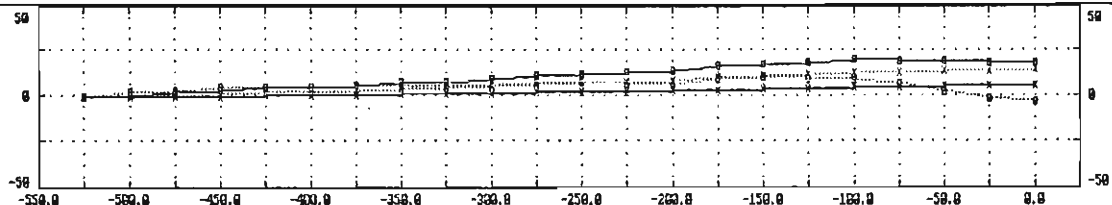
337/37:FF -2.6 -2.6 -2.5 -2.1 -2.6 -2.9 -2.7 -3.4 -3.9 -3.2 -2.6 -3.2 -4.1 -4.2 -3.7 -3.0 -2.1 -1.6 -1.9

1012/3 -0.8 0.5 1.0 2.0 4.1 4.6 5.7 6.8 7.6 9.1 10.6 11.7 12.2 13.4 15.6 17.1 18.0 19.3 19.8 18.3 17.8 17.9

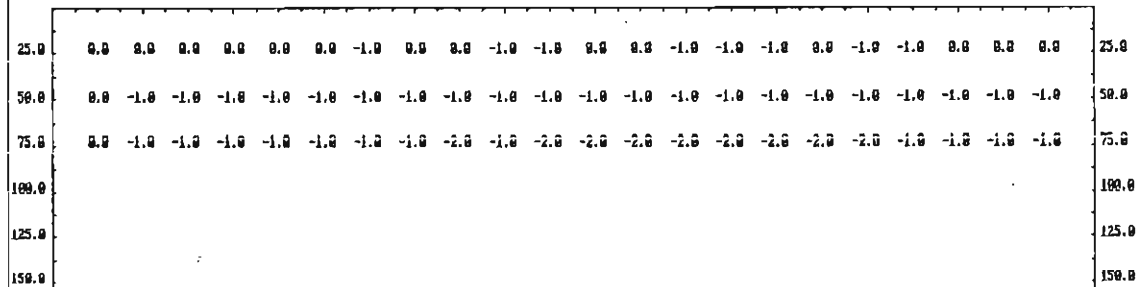
1012/3:FF -4.9 -4.6 -4.1 -3.4 -3.0 -4.1 -4.2 -5.3 -5.6 -4.2 -3.3 -5.1 -7.1 -6.1 -4.6 -3.2 0.0 2.2 1.6

3037/3 -0.7 1.9 3.2 4.1 4.8 4.6 5.1 5.2 5.4 6.0 7.3 7.1 5.9 6.5 8.9 10.0 9.3 8.4 6.4 2.1 -1.7 -3.0

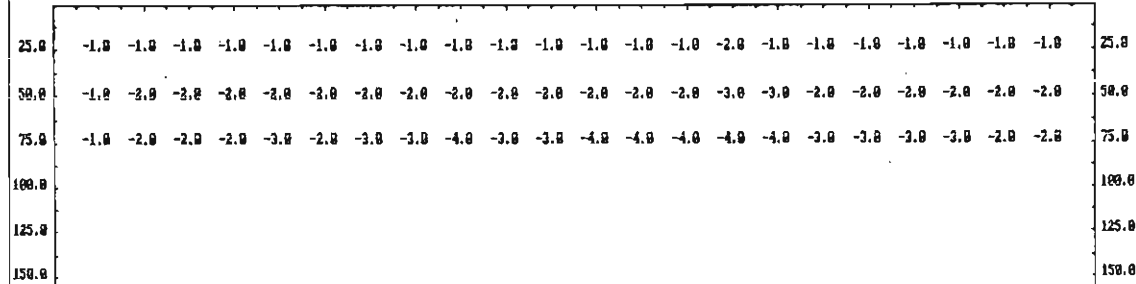
3037/3:FF -6.1 -3.0 -2.1 -0.8 -0.9 -0.9 -1.1 -2.7 -3.0 8.3 2.0 -2.4 -6.5 -3.9 1.2 4.5 9.2 14.4 14.0



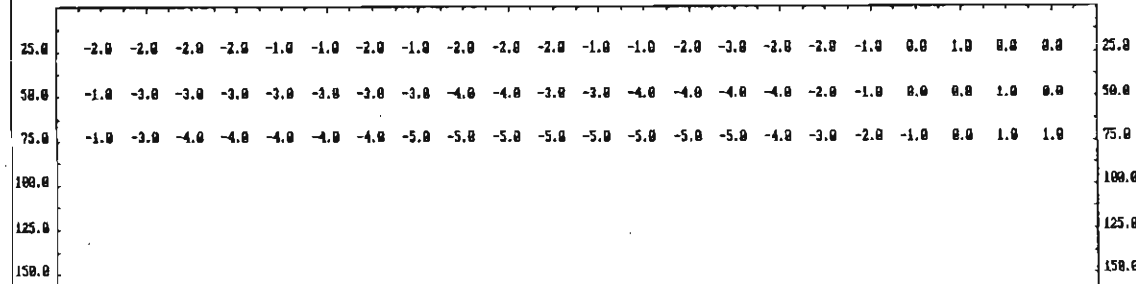
Pseudo-section of Filtered 112/37



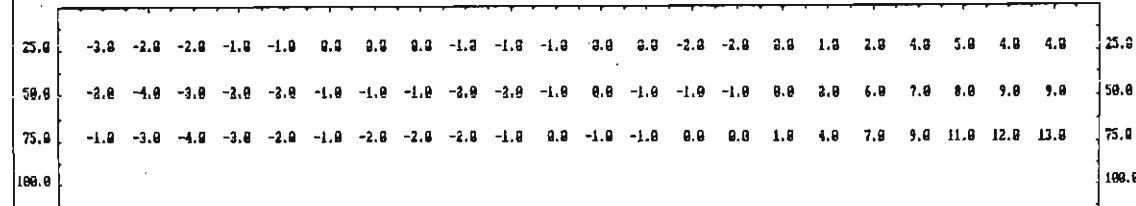
Pseudo-section of Filtered 337/37



Pseudo-section of Filtered 1012/3

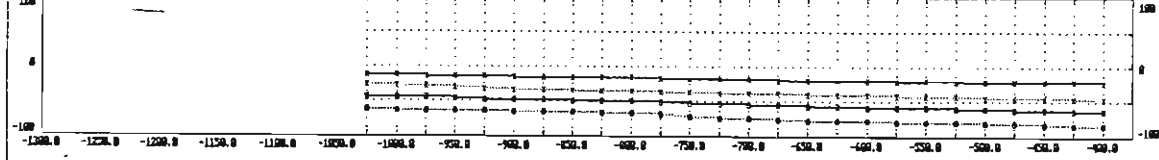


Pseudo-section of Filtered 3037/3



TWIN GRID - LARGE LOOP EM
DATE 02 DEC. 1956 OPERATOR S.L. LOOPE 4
LINE 6000E

112/77	8-12.5-13.0-13.5-14.3-15.0-15.5-16.0-16.1-16.5-16.9-17.4-17.7-18.0-18.3-18.5-19.1-19.0-20.1-20.0-20.4-20.0-21.1-21.5-21.0-22.1
112/77:17	2.0 2.4 2.7 2.4 2.3 2.3 1.6 1.5 1.3 1.7 1.7 1.4 1.3 1.3 2.1 2.3 1.2 0.7 1.3 1.3 1.2 1.4 1.3
337/77	4-27.7-28.1-28.0-28.2-28.3-28.5-28.7-28.2-28.4-29.1-29.7-29.4-29.2-29.3-29.4-29.4-29.7-29.7-29.7-29.7-29.7-29.7-29.7-29.7
337/77:17	3.8 3.8 3.5 3.5 3.8 2.7 2.3 2.3 2.5 2.7 3.4 3.3 2.2 2.3 2.6 2.8 2.6 1.7 1.5 2.3 2.4 2.7 2.3 2.3
1812/3	8-44.1-44.4-45.9-47.1-47.4-47.9-48.5-49.0-49.0-49.5-50.3-50.3-50.4-50.8-50.8-50.5-51.4-51.4-51.4-51.4-51.4-51.4-51.4-51.4
1812/3:17	3.6 2.3 4.5 4.2 2.3 1.9 2.2 2.4 2.2 4.4 4.0 4.0 3.5 3.4 2.3 2.1 2.7 2.0 3.0 2.5 2.0 3.4 3.0 3.4
3037/3	2-62.4-62.5-63.0-64.0-64.1-64.7-65.0-66.4-67.6-69.3-70.6-70.5-70.2-70.1-70.9-71.2-71.1-71.4-71.4-71.4-71.4-71.4-71.4
3037/3:17	3.7 2.9 2.3 1.7 1.3 1.5 2.5 4.3 3.5 4.9 3.2 4.8 5.2 5.3 3.0 2.3 2.9 3.0 2.4 2.4 2.0 3.0 3.7 3.4



Pseudo-section of Filtered 112/37

25.0	0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 0.0 1.0 1.0 1.0 0.0 0.0 1.0 1.0 0.0 0.0 1.0 0.0 1.0 1.0 0.0 0.0	25.0
50.0	0 2.0 2.0 2.0 2.0 2.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	50.0
75.0	0 3.0 3.0 3.0 3.0 3.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	75.0
100.0	0 4.0 4.0 4.0 4.0 4.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0	100.0
125.0	0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0	125.0
150.0		150.0

Pseudo-section of Filtered 337/37

25.0	0 1.0 2.0 2.0 2.0 2.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	25.0
50.0	0 4.0 4.0 4.0 4.0 4.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0	50.0
75.0	0 4.0 4.0 5.0 5.0 5.0 4.0 4.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0	75.0
100.0	0 9.0 9.0 7.0 7.0 6.0 5.0 5.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0	100.0
125.0	0 9.0 9.0 8.0 9.0 8.0 8.0 8.0 7.0 6.0 5.0 5.0 5.0 5.0 5.0 5.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0	125.0
150.0		150.0

Pseudo-section of Filtered 1812/3

25.0	1 1.0 1.0 2.0 1.0 1.0 1.0 1.0 1.0 2.0 2.0 1.0 1.0 1.0 1.0 1.0 1.0 2.0 1.0 1.0 1.0 1.0 1.0	25.0
50.0	1 3.0 3.0 3.0 3.0 3.0 2.0 2.0 2.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0	50.0
75.0	1 6.0 5.0 5.0 4.0 4.0 3.0 3.0 4.0 4.0 4.0 4.0 4.0 4.0 3.0 3.0 4.0 3.0 4.0 3.0 4.0 3.0 4.0	75.0
100.0	1 9.0 8.0 7.0 6.0 6.0 6.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0	100.0
125.0	1 8.0 8.0 8.0 9.0 9.0 8.0 8.0 7.0 7.0 7.0 7.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0	125.0
150.0		150.0

Pseudo-section of Filtered 3037/3

25.0	1 1.0 1.0 1.0 0.0 1.0 1.0 1.0 2.0 2.0 0.0 0.0 2.0 2.0 1.0 1.0 1.0 1.0 1.0 1.0 2.0 2.0 1.0	25.0
50.0	1 3.0 2.0 3.0 2.0 2.0 2.0 3.0 4.0 5.0 4.0 5.0 4.0 3.0 3.0 2.0 2.0 2.0 2.0 2.0 3.0 3.0 2.0	50.0
75.0	1 6.0 5.0 4.0 2.0 3.0 3.0 4.0 5.0 6.0 6.0 6.0 5.0 5.0 4.0 4.0 4.0 3.0 4.0 4.0 4.0 5.0 5.0	75.0
100.0	1 10.0 9.0 7.0 7.0 6.0 6.0 7.0 7.0 8.0 8.0 8.0 7.0 7.0 6.0 5.0 5.0 5.0 6.0 6.0 6.0 6.0 6.0	100.0
125.0	1 7.0 7.0 9.0 11.0 10.0 10.0 9.0 9.0 9.0 9.0 9.0 8.0 8.0 7.0 6.0 7.0 7.0 7.0 7.0 7.0 7.0 8.0	125.0
150.0		150.0

LINE 6100E

DATE 21 DEC. 1936 OPERATOR S.L. LOOPS 3 LOOP 1102x738m

112/77	-1.2	-0.9	-0.6	-0.4	-0.1	0.3	0.8	0.9	1.2	1.7	2.2	2.4	2.7	3.3	3.7	4.0	4.4	4.5	5.4	5.6	6.1	6.3	7.1	7.5	7.6	7.9	8.4	8.4	8.5	8.7	8.8	9.5	10.3	12.2	5.5	12.1	5.4	9.6	9.0	9.4	9.7	5.5	9.1	5.3
112/77:IT	-1.1	-1.0	-1.2	-1.6	-1.5	-1.0	-1.2	-1.8	-1.7	-1.2	-1.4	-1.9	-1.7	-1.4	-1.2	-1.5	-2.1	-1.8	-1.4	-1.7	-2.2	-1.7	-0.9	-1.2	-1.3	-0.6	-0.4	-0.6	-1.1	-2.3	-2.2	-0.3	0.5	0.4	0.8	0.3	0.8	0.3	0.8	0.5	0.8			
121/77	-0.8	0.0	0.6	1.3	2.1	2.9	3.7	4.4	5.1	5.9	7.0	7.5	8.3	9.2	10.2	11.1	11.7	12.0	13.9	14.5	14.9	15.3	16.9	15.5	15.8	16.2	16.5	15.4	15.4	15.1	14.9	15.5	16.4	16.2	15.6	14.9	13.9	12.9	12.3	11.6	10.7	9.4	0.6	8.1
121/77:IT	-2.7	-2.0	-3.1	-3.2	-3.1	-2.9	-3.0	-3.4	-3.5	-2.9	-3.0	-3.6	-3.8	-3.4	-3.2	-3.9	-3.9	-2.7	-1.8	-2.2	-2.2	0.9	0.4	-1.4	0.1	1.9	0.8	0.1	-1.5	-2.2	0.1	2.1	3.6	4.3	0.8	2.3	2.9	3.8	4.3	3.4				
1212/77	-4.6	0.9	2.4	2.5	4.8	6.1	7.4	8.2	9.9	9.0	11.1	12.2	12.4	13.9	14.7	16.3	17.0	17.1	19.5	20.3	20.0	19.7	18.4	16.9	14.8	13.6	12.0	9.5	6.3	3.5	1.0	3.0	1.7	1.7	-1.0	-3.6	-5.4	-6.5	-8.5	-12.1	-14.3	-17.3	-19.0	-20.5
1212/77:IT	-5.4	-5.0	-5.0	-5.2	-4.7	-3.6	-3.1	-3.8	-4.6	-4.4	-3.7	-3.3	-3.9	-4.6	-3.7	-3.9	-5.2	-3.2	0.1	2.2	6.4	10.8	1.4	6.4	9.2	10.1	1.5	0.8	0.6	4.0	2.0	7.0	7.4	7.1	9.7	10.9	9.9	10.0	5.8					
230/77	-0.3	2.4	4.3	5.7	7.0	7.9	7.8	7.2	5.5	5.1	4.2	5.0	4.3	3.8	4.2	3.6	2.7	3.8	3.7	-0.7	-2.2	-0.7	-17.4	-23.7	-27.2	-30.4	-33.6	-39.7	-45.0	-49.6	-47.9	-49.1	-47.5	-49.6	-52.7	-55.1	-57.7	-60.7	-61.4	-63.2	-65.5	-66.9	-67.3	
230/77:IT	-7.9	-5.8	-4.9	-3.8	-0.1	3.8	4.4	2.8	0.8	0.8	1.6	1.7	0.5	0.8	1.4	1.1	-0.8	1.9	10.0	13.5	23.2	30.0	24.8	15.5	15.1	17.9	19.5	19.1	11.8	1.6	-0.9	1.1	6.7	10.7	12.5	10.6	6.3	6.2	6.6	7.7	5.4			

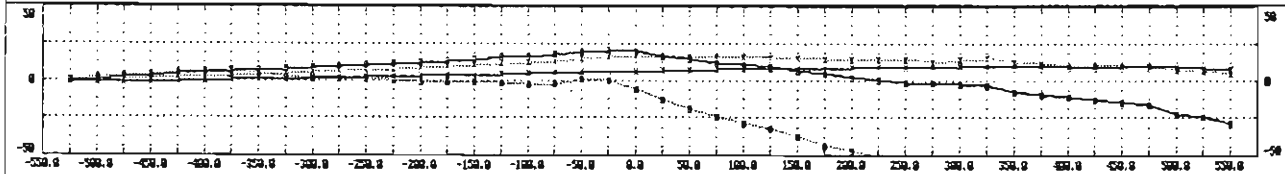
112/77 3-11.3-12.5-13.7-14.9-16.1-17.3-18.5-19.7-20.9-22.1-23.3-24.5-25.7-26.9-28.1-29.3-30.5-31.7-32.9-34.1-35.3-36.5-37.7-38.9-40.1-41.3-42.5-43.7-44.9-46.1-47.3-48.5-49.7-50.9-52.1-53.3-54.5-55.7-56.9-58.1-59.3-60.5-61.7-62.9-64.1-65.3-66.5-67.7-68.9-70.1-71.3-72.5-73.7-74.9-76.1-77.3-78.5-79.7-80.9-82.1-83.3-84.5-85.7-86.9-88.1-89.3-90.5-91.7-92.9-94.1-95.3-96.5-97.7-98.9-100.1-101.3-102.5-103.7-104.9-106.1-107.3-108.5-109.7-110.9-112.1-113.3-114.5-115.7-116.9-118.1-119.3-120.5-121.7-122.9-124.1-125.3-126.5-127.7-128.9-130.1-131.3-132.5-133.7-134.9-136.1-137.3-138.5-139.7-140.9-142.1-143.3-144.5-145.7-146.9-148.1-149.3-150.5-151.7-152.9-154.1-155.3-156.5-157.7-158.9-160.1-161.3-162.5-163.7-164.9-166.1-167.3-168.5-169.7-170.9-172.1-173.3-174.5-175.7-176.9-178.1-179.3-180.5-181.7-182.9-184.1-185.3-186.5-187.7-188.9-190.1-191.3-192.5-193.7-194.9-196.1-197.3-198.5-199.7-200.9-202.1-203.3-204.5-205.7-206.9-208.1-209.3-210.5-211.7-212.9-214.1-215.3-216.5-217.7-218.9-220.1-221.3-222.5-223.7-224.9-226.1-227.3-228.5-229.7-230.9-232.1-233.3-234.5-235.7-236.9-238.1-239.3-240.5-241.7-242.9-244.1-245.3-246.5-247.7-248.9-250.1-251.3-252.5-253.7-254.9-256.1-257.3-258.5-259.7-260.9-262.1-263.3-264.5-265.7-266.9-268.1-269.3-270.5-271.7-272.9-274.1-275.3-276.5-277.7-278.9-280.1-281.3-282.5-283.7-284.9-286.1-287.3-288.5-289.7-290.9-292.1-293.3-294.5-295.7-296.9-298.1-299.3-300.5-301.7-302.9-304.1-305.3-306.5-307.7-308.9-310.1-311.3-312.5-313.7-314.9-316.1-317.3-318.5-319.7-320.9-322.1-323.3-324.5-325.7-326.9-328.1-329.3-330.5-331.7-332.9-334.1-335.3-336.5-337.7-338.9-340.1-341.3-342.5-343.7-344.9-346.1-347.3-348.5-349.7-350.9-352.1-353.3-354.5-355.7-356.9-358.1-359.3-360.5-361.7-362.9-364.1-365.3-366.5-367.7-368.9-370.1-371.3-372.5-373.7-374.9-376.1-377.3-378.5-379.7-380.9-382.1-383.3-384.5-385.7-386.9-388.1-389.3-390.5-391.7-392.9-394.1-395.3-396.5-397.7-398.9-400.1-401.3-402.5-403.7-404.9-406.1-407.3-408.5-409.7-410.9-412.1-413.3-414.5-415.7-416.9-418.1-419.3-420.5-421.7-422.9-424.1-425.3-426.5-427.7-428.9-430.1-431.3-432.5-433.7-434.9-436.1-437.3-438.5-439.7-440.9-442.1-443.3-444.5-445.7-446.9-448.1-449.3-450.5-451.7-452.9-454.1-455.3-456.5-457.7-458.9-460.1-461.3-462.5-463.7-464.9-466.1-467.3-468.5-469.7-470.9-472.1-473.3-474.5-475.7-476.9-478.1-479.3-480.5-481.7-482.9-484.1-485.3-486.5-487.7-488.9-490.1-491.3-492.5-493.7-494.9-496.1-497.3-498.5-499.7-500.9-502.1-503.3-504.5-505.7-506.9-508.1-509.3-510.5-511.7-512.9-514.1-515.3-516.5-517.7-518.9-520.1-521.3-522.5-523.7-524.9-526.1-527.3-528.5-529.7-530.9-532.1-533.3-534.5-535.7-536.9-538.1-539.3-540.5-541.7-542.9-544.1-545.3-546.5-547.7-548.9-550.1-551.3-552.5-553.7-554.9-556.1-557.3-558.5-559.7-560.9-562.1-563.3-564.5-565.7-566.9-568.1-569.3-570.5-571.7-572.9-574.1-575.3-576.5-577.7-578.9-580.1-581.3-582.5-583.7-584.9-586.1-587.3-588.5-589.7-590.9-592.1-593.3-594.5-595.7-596.9-598.1-599.3-600.5-601.7-602.9-604.1-605.3-606.5-607.7-608.9-610.1-611.3-612.5-613.7-614.9-616.1-617.3-618.5-619.7-620.9-622.1-623.3-624.5-625.7-626.9-628.1-629.3-630.5-631.7-632.9-634.1-635.3-636.5-637.7-638.9-640.1-641.3-642.5-643.7-644.9-646.1-647.3-648.5-649.7-650.9-652.1-653.3-654.5-655.7-656.9-658.1-659.3-660.5-661.7-662.9-664.1-665.3-666.5-667.7-668.9-670.1-671.3-672.5-673.7-674.9-676.1-677.3-678.5-679.7-680.9-682.1-683.3-684.5-685.7-686.9-688.1-689.3-690.5-691.7-692.9-694.1-695.3-696.5-697.7-698.9-700.1-701.3-702.5-703.7-704.9-706.1-707.3-708.5-709.7-710.9-712.1-713.3-714.5-715.7-716.9-718.1-719.3-720.5-721.7-722.9-724.1-725.3-726.5-727.7-728.9-730.1-731.3-732.5-733.7-734.9-736.1-737.3-738.5-739.7-740.9-742.1-743.3-744.5-745.7-746.9-748.1-749.3-750.5-751.7-752.9-754.1-755.3-756.5-757.7-758.9-760.1-761.3-762.5-763.7-764.9-766.1-767.3-768.5-769.7-770.9-772.1-773.3-774.5-775.7-776.9-778.1-779.3-780.5-781.7-782.9-784.1-785.3-786.5-787.7-788.9-790.1-791.3-792.5-793.7-794.9-796.1-797.3-798.5-799.7-800.9-802.1-803.3-804.5-805.7-806.9-808.1-809.3-810.5-811.7-812.9-814.1-815.3-816.5-817.7-818.9-820.1-821.3-822.5-823.7-824.9-826.1-827.3-828.5-829.7-830.9-832.1-833.3-834.5-835.7-836.9-838.1-839.3-840.5-841.7-842.9-844.1-845.3-846.5-847.7-848.9-850.1-851.3-852.5-853.7-854.9-856.1-857.3-858.5-859.7-860.9-862.1-863.3-864.5-865.7-866.9-868.1-869.3-870.5-871.7-872.9-874.1-875.3-876.5-877.7-878.9-880.1-881.3-882.5-883.7-884.9-886.1-887.3-888.5-889.7-890.9-892.1-893.3-894.5-895.7-896.9-898.1-899.3-900.5-901.7-902.9-904.1-905.3-906.5-907.7-908.9-910.1-911.3-912.5-913.7-914.9-916.1-917.3-918.5-919.7-920.9-922.1-923.3-924.5-925.7-926.9-928.1-929.3-930.5-931.7-932.9-934.1-935.3-936.5-937.7-938.9-940.1-941.3-942.5-943.7-944.9-946.1-947.3-948.5-949.7-950.9-952.1-953.3-954.5-955.7-956.9-958.1-959.3-960.5-961.7-962.9-964.1-965.3-966.5-967.7-968.9-970.1-971.3-972.5-973.7-974.9-976.1-977.3-978.5-979.7-980.9-982.1-983.3-984.5-985.7-986.9-988.1-989.3-990.5-991.7-992.9-994.1-995.3-996.5-997.7-998.9-1000.1-1001.3-1002.5-1003.7-1004.9-1006.1-1007.3-1008.5-1009.7-1010.9-1012.1-1013.3-1014.5-1015.7-1016.9-1018.1-1019.3-1020.5-1021.7-1022.9-1024.1-1025.3-1026.5-1027.7-1028.9-1030.1-1031.3-1032.5-1033.7-1034.9-1036.1-1037.3-1038.5-1039.7-1040.9-1042.1-1043.3-1044.5-1045.7-1046.9-1048.1-1049.3-1050.5-1051.7-1052.9-1054.1-1055.3-1056.5-1057.7-1058.9-1060.1-1061.3-1062.5-1063.7-1064.9-1066.1-1067.3-1068.5-1069.7-1070.9-1072.1-1073.3-1074.5-1075.7-1076.9-1078.1-1079.3-1080.5-1081.7-1082.9-1084.1-1085.3-1086.5-1087.7-1088.9-1090.1-1091.3-1092.5-1093.7-1094.9-1096.1-1097.3-1098.5-1099.7-1100.9-1102.1-1103.3-1104.5-1105.7-1106.9-1108.1-1109.3-1110.5-1111.7-1112.9-1114.1-1115.3-1116.5-1117.7-1118.9-1120.1-1121.3-1122.5-1123.7-1124.9-1126.1-1127.3-1128.5-1129.7-1130.9-1132.1-1133.3-1134.5-1135.7-1136.9-1138.1-1139.3-1140.5-1141.7-1142.9-1144.1-1145.3-1146.5-1147.7-1148.9-1150.1-1151.3-1152.5-1153.7-1154.9-1156.1-1157.3-1158.5-1159.7-1160.9-1162.1-1163.3-1164.5-1165.7-1166.9-1168.1-1169.3-1170.5-1171.7-1172.9-1174.1-1175.3-1176.5-1177.7-1178.9-1180.1-1181.3-1182.5-1183.7-1184.9-1186.1-1187.3-1188.5-1189.7-1190.9-1192.1-1193.3-1194.5-1195.7-1196.9-1198.1-1199.3-1200.5-1201.7-1202.9-1204.1-1205.3-1206.5-1207.7-1208.9-1210.1-1211.3-1212.5-1213.7-1214.9-1216.1-1217.3-1218.5-1219.7-1220.9-1222.1-1223.3-1224.5-1225.7-1226.9-1228.1-1229.3-1230.5-1231.7-1232.9-1234.1-1235.3-1236.5-1237.7-1238.9-1240.1-1241.3-1242.5-1243.7-1244.9-1246.1-1247.3-1248.5-1249.7-1250.9-1252.1-1253.3-1254.5-1255.7-1256.9-1258.1-1259.3-1260.5-1261.7-1262.9-1264.1-1265.3-1266.5-1267.7-1268.9-1270.1-1271.3-1272.5-1273.7-1274.9-1276.1-1277.3-1278.5-1279.7-1280.9-1282.1-1283.3-1284.5-1285.7-1286.9-1288.1-1289.3-1290.5-1291.7-1292.9-1294.1-1295.3-1296.5-1297.7-1298.9-1300.1-1301.3-1302.5-1303.7-1304.9-1306.1-1307.3-1308.5-1309.7-1310.9-1312.1-1313.3-1314.5-1315.7-1316.9-1318.1-1319.3-1320.5-1321.7-1322.9-1324.1-1325.3-1326.5-1327.7-1328.9-1330.1-1331.3-1332.5-1333.7-1334.9-1336.1-1337.3-1338.5-1339.7-1340.9-1342.1-1343.3-1344.5-1345.7-1346.9-1348.1-1349.3-1350.5-1351.7-1352.9-1354.1-1355.3-1356.5-1357.7-1358.9-1360.1-1361.3-1362.5-1363.7-1364.9-1366.1-1367.3-1368.5-1369.7-1370.9-1372.1-1373.3-1374.5-1375.7-1376.9-1378.1-1379.3-1380.5-1381.7-1382.9-1384.1-1385.3-1386.5-1387.7-1388.9-1390.1-1391.3-1392.5-1393.7-1394.9-1396.1-1397.3-1398.5-1399.7-1400.9-1402.1-1403.3-1404.5-1405.7-1406.9-1408.1-1409.3-1410.5-1411.7-1412.9-1414.1-1415.3-1416.5-1417.7-1418.9-1420.1-1421.3-1422.5-1423.7-1424.9-1426.1-1427.3-1428.5-1429.7-1430.9-1432.1-1433.3-1434.5-1435.7-1436.9-1438.1-1439.3-1440.5-1441.7-1442.9-1444.1-1445.3-1446.5-1447.7-1448.9-1450.1-1451.3-1452.5-1453.7-1454.9-1456.1-1457.3-1458.5-1459.7-1460.9-1462.1-1463.3-1464.5-1465.7-1466.9-1468.1-1469.3-1470.5-1471.7-1472.9-1474.1-1475.3-1476.5-1477.7-1478.9-1480.1-1481.3-1482.5-1483.7-1484.9-1486.1-1487.3-1488.5-1489.7-1490.9-1492.1-1493.3-1494.5-1495.7-1496.9-1498.1-1499.3-1500.5-1501.7-1502.9-1504.1-1505.3-1506.5-1507.7-1508.9-1510.1-1511.3-1512.5-1513.7-1514.9-1516.1-1517.3-1518.5-1519.7-1520.9-1522.1-1523.3-1524.5-1525.7-1526.9-1528.1-1529.3-1530.5-1531.7-1532.9-1534.1-1535.3-1536.5-1537.7-1538.9-1540.1-1541.3-1542.5-1543.7-1544.9-1546.1-1547.3-1548.5-1549.7-1550.9-1552.1-1553.3-1554.5-1555.7-1556.9-1558.1-1559.3-1560.5-1561.7-1562.9-1564.1-1565.3-1566.5-1567.7-1568.9-1570.1-1571.3-1572.5-1573.7-1574.9-1576.1-1577.3-1578.5-1579.7-1580.9-1582.1-1583.3-1584.5-1585.7-1586.9-1588.1-1589.3-1590.5-1591.7-1592.9-1594.1-1595.3-1596.5-1597.7-1598.9-1600.1-1601.3-1602.5-1603.7-1604.9-1606.1-1607.3-1608.5-1609.7-1610.9-1612.1-1613.3-1614.5-1615.7-1616.9-1618.1-1619.3-1620.5-1621.7-1622.9-1624.1-1625.3-1626.5-1627.7-1628.9-1630.1-1631.3-1632.5-1633.7-1634.9-1636.1-1637.3-1638.5-1639.7-1640.9-1642.1-1643.3-1644.5-1645.7-1646.9-1648.1-1649.3-1650.5-1651.7-1652.9-1654.1-1655.3-1656.5-1657.7-1658.9-1660.1-1661.3-1662.5-1663.7-1664.9-1666.1-1667.3-1668.5-1669.7-1670.9-1672.1-1673.3-1674.5-1675.7-1676.9-1678.1-1679.3-1680.5-1681.7-1682.9-1684.1-1685.3-1686.5-1687.7-1688.9-1690.1-1691.3-1692.5-1693.7-1694.9-1696.1-1697.3-1698.5-1699.7-1700.9-1702.1-1703.3-1704.5-1705.7-1706.9-1708.1-1709.3-1710.5-1711.7-1712.9-1714.1-1715.3-1716.5-1717.7-1718.9-1720.1-1721.3-1722.5-1723.7-1724.9-1726.1-1727.3-1728.5-1729.7-1730.9-1732.1-1733.3-1734.5-1735.7-1736.9-1738.1-1739.3-1740.5-1741.7-1742.9-1744.1-1745.3-1746.5-1747.7-1748.9-1750.1-1751.3-1752.5-1753.7-1754.9-1756.1-1757.3-1758.5-1759.7-1760.9-1762.1-1763.3-1764.5-1765.7-1766.9-1768.1-1769.3-1770.5-1771.7-1772.9-1774.1-1775.3-1776.5-1777.7-1778.9-1780.1-1781.3-1782.5-1783.7-1784.9-1786.1-1787.3-1788.5-1789.7-1790.9-1792.1-1793.3-1794.5-1795.7-1796.9-1798.1-1799.3-1800.5-1801.7-1802.9-1804.1-1805.3-1806.5-1807.7-1808.9-1810.1-1811.3-1812.5-1813.7-1814.9-1816.1-1817.3-1818.5-1819.7-1820.9-1822.1-1823.3-1824.5-1825.7-1826.9-1828.1-1829.3-1830.5-1831.7-1832.9-1834.1-1835.3-1836.5-1837.7-1838.9-1840.1-1841.3-1842.5-1843.7-1844.9-1846.1-1847.3-1848.5-1849.7-1850.9-1852.1-1853.3-1854.5-1855.7-1856.9-1858.1-1859.3-1860.5-1861.7-1862.9-1864.1-1865.3-1866.5-1867.7-1868.9-1870.1-1871.3-1872.5-1873.7-1874.9-1876.1-1877.3-1878.5-1879.7-1880.9-1882.1-1883.3-1884.5-1885.7-1886.9-1888.1-1889.3-1890.5-1891.7-1892.9-1894.1-1895.3-1896.5-1897.7-1898.9-1900.1-1901.3-1902.5-1903.7-1904.9-1906.1-1907.3-1908.5-1909.7-1910.9-1912.1-1913.3-1914.5-1915.7-1916.9-1918.1-1919.3-1920.5-1921.7-1922.9-1924.1-1925.3-1926.5-1927.7-1928.9-1930.1-1931.3-1932.5-1933.7-1934.9-1936.1-1937.3-1938.5-1939.7-1940.9-1942.1-1943.3-1944.5-1945.7-1946.9-1948.1-1949.3-1950.5-1951.7-1952.9-1954.1-1955.3-1956.5-1957.7-1958.9-1960.1-1961.3-1962.5-1963.7-1964.9-1966.1-1967.3-1968.5-1969.7-1970.9-1972.1-1973.3-1974.5-1975.7-1976.9-1978.1-1979.3-1980.5-1981.7-1982.9-1984.1-1985.3-1986.5-1987.7-1988.9-1990.1-1991.3-1992.5-1993.7-1994.9-1996.1-1997.3-1998.5-1999.7-2000.9-2002.1-2003.3-2004.5-2005.7-2006.9-2008.1-2009.3-2010.5-2011.7-2012.9-2014.1-2015.3-2016.5-2017.7-2018.9-2020.1-2021.3-2022.5-2023.7-2024.9-2026.1-2027.3-2028.5-2029.7-2030.9-2032.1-2033.3-2034.5-2035.7-2036.9-2038.1-2039.3-2040.5-2041.7-2042.9-2044.1-2045.3-2046.5-2047.7-2048.9-2050.1-2051.3-2052.5-2053.7-2054.9-2056.1-2057.3-2058.5-2059.7-2060.9-2062.1-2063.3-2064.5-2065.7-2066.9-2068.1-2069.3-2070.5-2071.7-2072.9-2074.1-2075.3-2076.5-2077.7-2078.9-2080.1-2081.3-2082.5-2083.7-2084.9-2086.1-2087.3-2088.5-2089.7-2090.9-2092.1-2093.3-2094.5-2095.7-2096.9-2098.1-2099.3-2100.5-2101.7-2102.9-2104.1-2105.3-2106.5-2107.7-2108.9-2110.1-2111.3-2112.5-2113.7-2114.9-2116.1-2117.3-2118.5-2119.7-2120.9-2122.1-2123.3-2124.5-2125.7-2126.9-2128.1-2129.3-2130.5-2131.7-2132.9-2134.1-2135.3-2136.5-2137.7-2138.9-2140.1-2141.3-2142.5-2143.7-2144.9-2146.1-2147.3-2148.5-2149.7-2150.9-2152.1-2153.3-2154.5-2155.7-2156.9-2158.1-2159.3-2160.5-2161.7-2162.9-2164.1-2165.3-2166.5-2167.7-2168.9-2170.1-2171.3-2172.5-2173.7-2174.9-2176.1-2177.3-2178.5-2179.7-2180.9-2182.1-2183.3-2184.5-2185.7-2186.9-2188.1-2189.3-2190.5-2191.7-2192.9-2194.1-2195.3-2196.5-2197.7-2198.9-2200.1-2201.3-2202.5-2203.7-2204.9-2206.1-2207.3-2208.5-2209.7-2210.9-2212.1-2213.3-2214.5-2215.7-2216.9-2218.1-2219.3-2220.5-2221.7-2222.9-2224.1-2225.3-2226.5-2227.7-2228.9-2230.1-2231.3-2232.5-2233.7-2234.9-2236.1-2237.3-2238.5-2239.7-2240.9-2242.1-2243.3-2244.5-2245.7-2246.9-2248.1-2249.3-2250.5-2251.7-2252.9-2254.1-2255.3-2256.5-2257.7-2258.9-2260.1-2261.3-22

TWIN GRID - LARGE LOOP EM

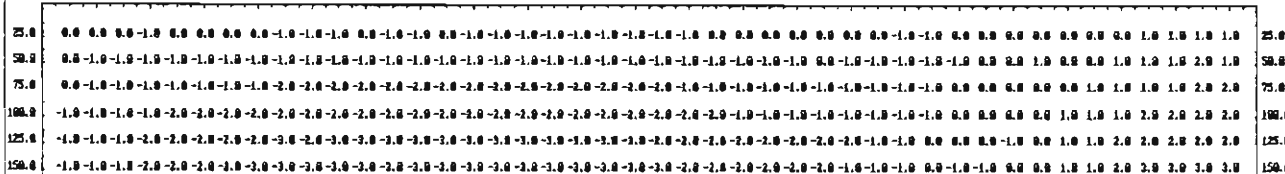
LINE 6200E

DATE 11/20/86 OPERATOR S.L. LOOP#3 LOOP 1180X750m

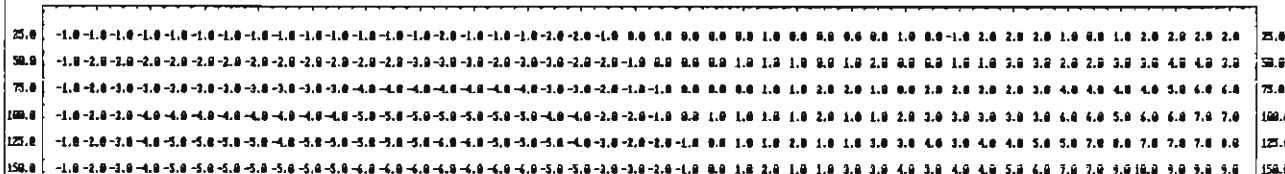
112/77 -1.1 -0.9 -0.7 -0.4 0.2 0.3 0.8 0.9 1.3 1.7 2.2 2.5 2.8 3.4 3.7 4.0 4.6 5.0 5.4 5.9 6.2 6.6 7.0 7.4 7.7 8.0 8.2 8.5 8.6 8.6 9.3 9.5 10.1 9.5 9.5 9.1 8.7 9.4 9.3 8.5 8.1 7.8
 112/77:77 -0.9 -1.4 -1.6 -1.3 -1.2 -1.1 -1.3 -1.7 -1.7 -1.4 -1.5 -1.8 -1.5 -1.5 -1.9 -1.8 -1.7 -1.7 -1.5 -1.5 -1.6 -1.3 -1.3 -1.1 -0.9 -0.3 -0.3 -0.7 -0.6 -1.1 -1.6 -1.7 -0.7 0.7 1.3 1.3 0.3 -1.3 -0.1 2.7 2.5
 337/77 -0.6 0.1 0.7 1.6 2.5 2.9 4.0 4.4 5.3 6.1 6.8 7.5 8.4 8.8 10.1 10.9 11.8 12.7 13.6 15.1 16.0 15.7 16.8 16.2 15.6 15.9 15.2 14.9 14.6 14.2 12.9 12.7 12.4 14.7 12.1 11.3 9.8 10.4 9.9 8.7 6.8 6.2 4.7
 337/77:77 -2.8 -2.3 -3.1 -2.8 -3.0 -2.8 -3.0 -3.2 -2.9 -3.0 -2.7 -2.8 -4.0 -4.0 -3.5 -3.6 -4.2 -4.0 -3.8 -4.6 -4.5 -0.1 0.7 0.7 1.4 1.6 1.1 8.9 8.9 2.5 1.3 -3.2 0.0 3.9 5.7 3.2 0.0 1.6 4.8 5.6 4.6
 1012/3 -0.2 1.3 2.4 3.0 3.3 5.9 7.2 7.6 8.0 8.7 10.0 10.7 11.4 12.4 13.4 14.3 15.4 16.0 17.9 19.3 20.7 19.1 16.4 14.0 11.7 10.4 9.2 6.6 4.4 1.5 -0.2 -1.3 -1.7 -2.1 -3.2 -7.4 -9.7 -11.7 -13.2 -15.0 -16.4 -22.7 -20.8 -25.1
 1012/3:77 -5.1 -5.4 -5.0 -4.0 -3.4 -2.9 -1.2 -1.0 -3.7 -3.4 -3.1 -2.9 -4.1 -3.9 -3.7 -4.0 -5.4 -4.1 -2.6 4.5 9.4 9.0 8.3 6.1 6.3 8.4 9.9 9.7 7.4 4.3 2.3 2.3 6.0 11.0 10.0 7.0 6.0 6.7 11.1 15.3 14.0
 3037/3 0.4 2.3 4.0 4.9 6.2 5.0 6.0 4.6 2.9 1.2 1.2 0.9 2.0 -0.8 -0.5 -1.2 -1.4 -2.4 -1.5 1.0 0.3 -4.2 -12.9 -19.9 -23.0 -22.7 -22.7 -37.5 -44.0 -47.6 -51.9 -54.6 -50.4 -54.2 -53.2 -38.1 -43.0 -43.0 44.3 9.4 -6.7 -2.4 -9.1 -17.2 -8.7 -4.1
 3037/3:77 -5.6 -4.0 -2.4 -0.4 0.7 3.0 6.5 5.1 2.0 1.5 2.9 2.2 0.7 1.3 2.1 1.1 -3.3 -5.2 5.4 28.4 25.5 25.4 21.3 17.1 15.7 15.5 21.2 17.1 14.0 10.4 2.9 0.3 4.0 0.0 10.1 9.2 5.1 4.5 7.8 9.3 9.8



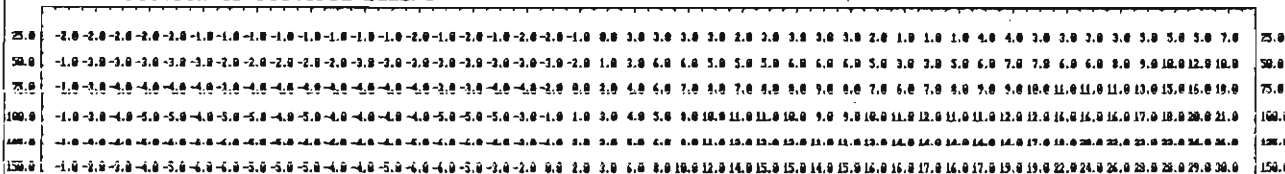
Pseudo-section of Filtered 112/37



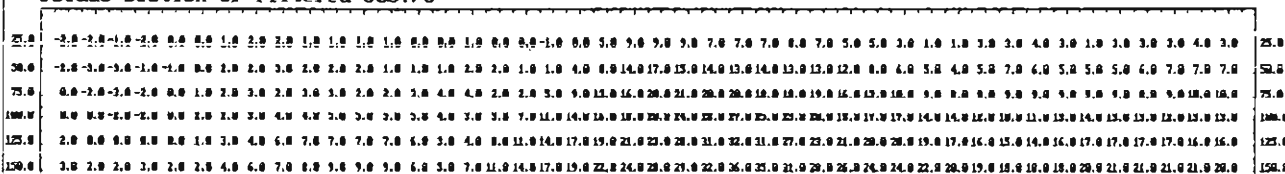
Pseudo-section of Filtered 337/37



Pseudo-section of Filtered 1012/3



Pseudo-section of Filtered 3037/3



LINE 6200E

DATE 25 DEC. 1986 OPERATOR I.L. LOOP# 4

11257

123:57

397/37

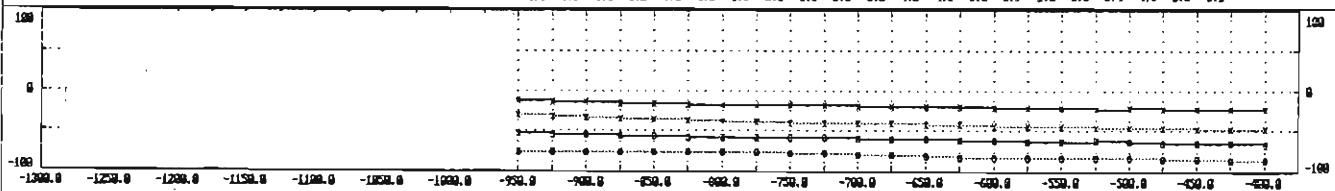
337/37:IT

1542/27

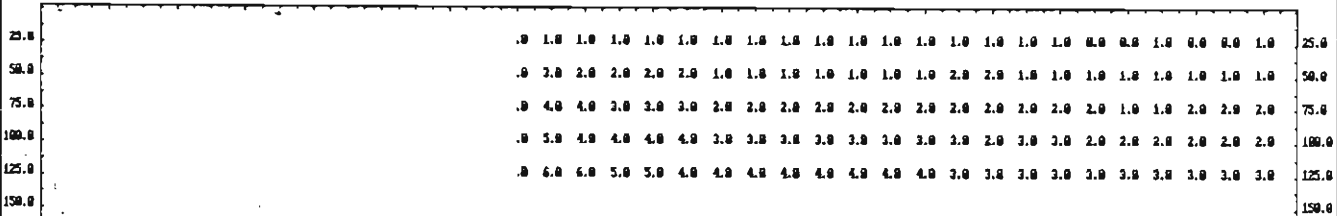
1012/3:57

3837/3

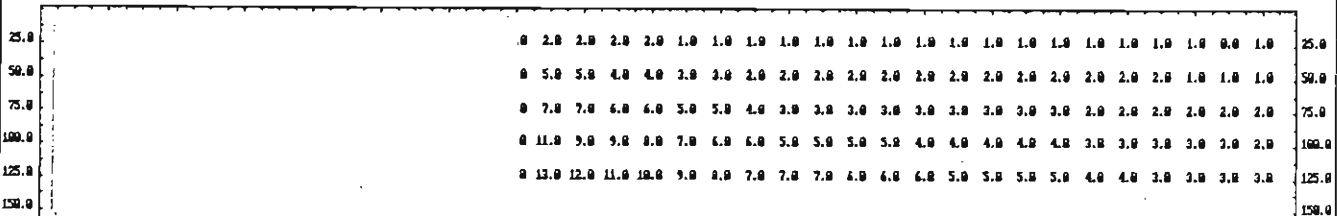
3077:5



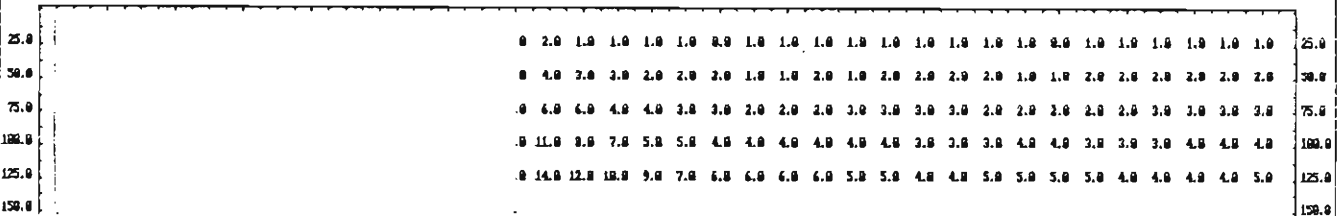
Pseudo-section of Filtered 112/37



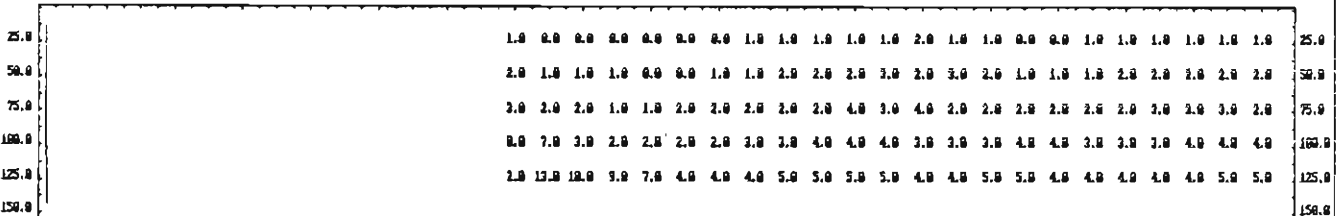
Pseudo-section of Filtered 337/37



Pseudo-section of Filtered 1012/3



Pseudo-section of Filtered SST/3

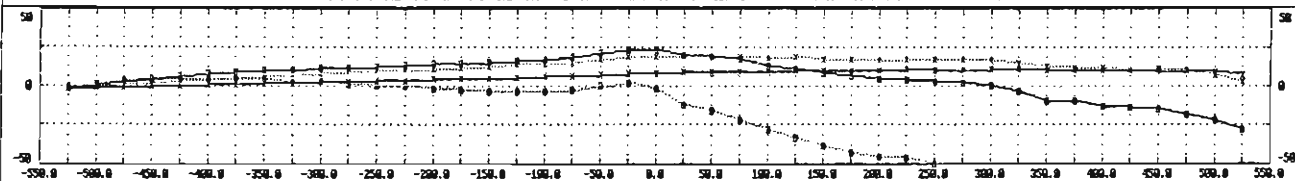


TWIN GRID - LARGE LOOP EM

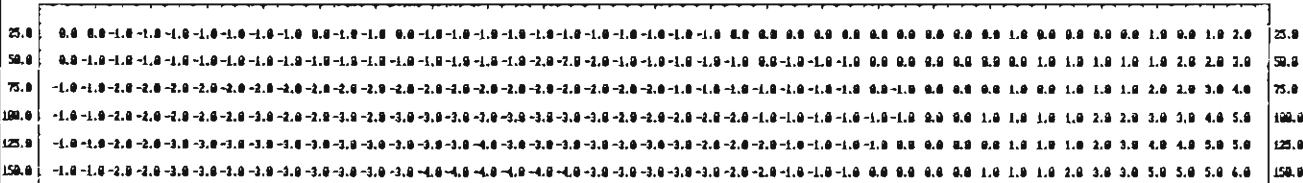
LINE 6300E

DATE 11/30/86 OPERATOR S.L. LOOP#3 LOOP (100x750m)

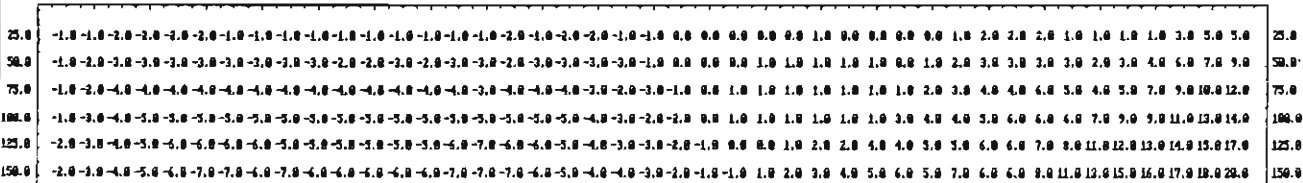
112/37 -1.3 -1.1 -2.7 -0.2 0.3 1.0 1.2 1.2 2.2 2.6 2.9 2.7 3.9 4.2 4.3 4.9 5.6 6.0 6.5 7.2 7.8 8.3 8.6 9.2 9.3 9.8 9.9 9.4 9.7 10.1 10.2 10.4 10.2 9.8 10.9 10.6 10.0 9.9 9.5 10.1 9.3 9.4 9.1 7.3
112/37:17 -1.5 -2.1 -2.4 -1.9 -1.5 -1.3 -1.0 -1.1 -1.7 -2.2 -1.6 -1.4 -1.6 -1.5 -1.9 -2.8 -2.1 -2.5 -2.4 -1.9 -1.7 -1.6 -0.5 0.1 -0.8 -1.4 -1.2 -0.8 -0.3 0.6 -0.1 -1.5 0.1 1.6 1.2 0.3 0.0 0.9 0.9 2.3
337/37 -0.0 -0.2 0.0 2.1 3.3 4.5 5.3 6.2 7.0 7.9 8.5 9.5 10.2 10.8 12.0 12.5 13.0 14.5 14.9 16.6 18.3 18.5 19.2 18.3 18.7 17.7 18.3 17.0 16.7 16.3 17.2 16.7 17.1 15.9 14.4 12.3 12.0 11.6 10.2 10.3 10.0 7.1 3.0
337/37:17 -3.5 -4.0 -4.9 -4.4 -3.7 -3.4 -3.4 -3.2 -3.1 -3.3 -3.0 -3.1 -3.5 -3.8 -3.1 -3.2 -5.5 -5.3 -2.0 -0.7 0.7 1.1 1.0 1.1 2.3 2.3 0.2 -0.9 -0.3 1.0 3.6 6.2 5.9 3.1 2.5 3.1 1.5 3.4 10.2
1012/3 -0.6 0.7 2.6 4.6 6.1 7.7 8.6 9.7 10.2 11.3 11.5 12.6 13.3 14.1 14.5 15.0 16.4 17.3 18.0 21.1 23.3 23.2 19.7 18.6 16.9 12.1 10.0 0.2 6.0 4.2 3.5 2.7 1.5 0.1 -3.0 -9.4 -10.0 -12.0 -14.2 -14.9 -18.0 -22.1 -27.0
1012/3:17 -7.1 -7.4 -6.6 -5.6 -4.5 -3.6 -3.2 -2.9 -2.6 -3.3 -3.5 -2.5 -1.9 -2.0 -4.2 -4.7 -6.2 -6.3 -6.6 1.5 8.2 7.4 9.3 12.4 10.0 8.7 9.8 6.5 4.0 3.5 4.6 7.9 14.0 15.7 9.6 7.6 6.3 6.7 11.0 16.2
3037/3 -0.9 1.2 3.6 4.4 6.3 6.8 4.7 4.3 2.1 2.4 1.0 0.2 -0.2 -1.7 -2.0 -3.0 -3.0 -3.5 -2.4 0.0 2.3 -1.3 -12.0 -15.6 -21.5 -27.9 -31.0 -37.1 -42.9 -45.9 -49.9 -51.0 -52.4 -54.5 -58.0 -63.7 -63.4 -64.5 -65.2 -66.4 -69.6 -72.3
3037/3:17 -7.7 -5.9 -1.1 -0.0 0.1 3.1 4.5 3.0 3.3 3.4 3.1 4.5 4.7 2.3 -0.1 -0.3 -4.1 -0.2 -3.4 15.6 20.6 22.0 21.0 24.6 23.5 20.3 15.4 10.3 8.5 8.6 6.6 6.0 9.1 14.0 14.6 6.2 2.6 3.7 6.3 10.3



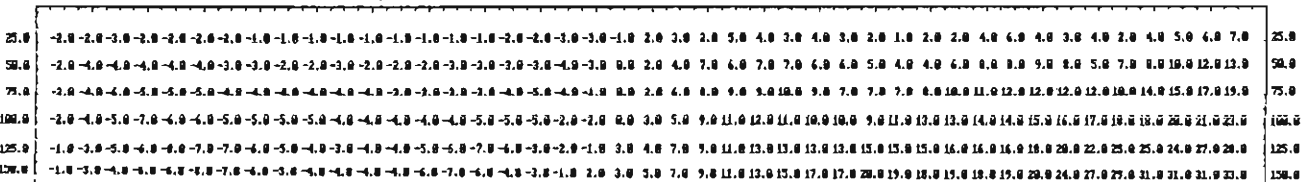
Pseudo-section of Filtered 112/37



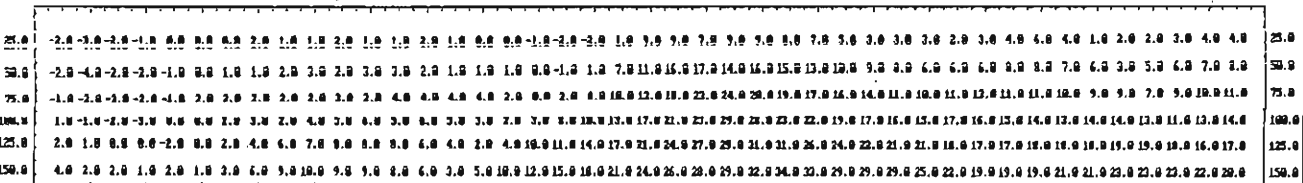
Pseudo-section of Filtered 337/37



Pseudo-section of Filtered 1012/3



Pseudo-section of Filtered 3037/3



LINE 6300E

DATE 03 DEC. 1986 OPERATOR S.L. LOOP# 4

1 -17.5 -18.3 -18.6 -19.2 -19.7 -20.1 -20.3 -20.8 -21.2 -21.5 -21.8 -22.1 -22.8

2.4 2.3 2.2 2.0 2.2 1.5 1.3 1.6 1.6 1.3 1.2 1.6 2.2

7 -39.6 -41.5 -41.4 -42.3 -42.7 -43.3 -44.2 -45.3 -45.5 -45.9 -46.1 -46.4 -47.4

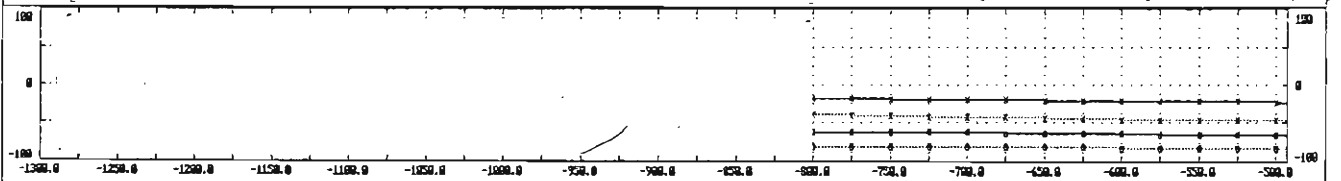
3.9	3.6	2.6	3.1	2.3	2.3	3.3	3.3	1.9	1.2	1.1	1.8	3.2
-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----

0	-41.2	-41.6	-41.8	-42.2	-42.8	-42.8	-42.8	-42.8	-44.2	-44.2	-44.6	-45.0	-46.1
---	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------

1.4	1.3	1.1	1.0	2.0	1.0	1.0	1.0	1.5	0.9	1.1	2.2	3.5
-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----

7 -33.2 -35.6 -33.3 -31.2 -33.1 -33.6 -31.6 -32.3 -32.4 -33.2 -32.6 -32.2 -32.2

-0.9	0.6	1.3	-0.2	-1.4	0.9	3.0	3.1	1.1	0.5	-0.0	0.6	4.0
------	-----	-----	------	------	-----	-----	-----	-----	-----	------	-----	-----

[illegible][illegible][illegible][illegible]

TWIN GRID - LARGE LOOP EM

LINE 6400E

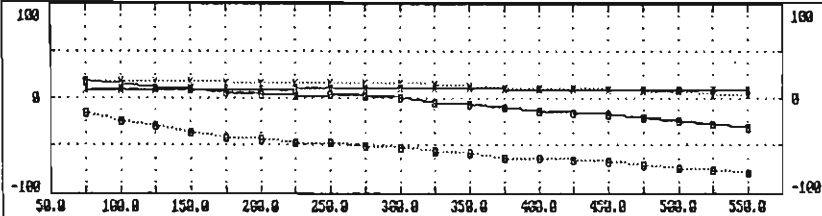
DATE 11/30/86 OPERATOR S.L. LOOP#3 LOOP 1188x750m

112/37 8.9 8.5 9.3 9.9 9.8 9.5 10.4 10.5 10.5 11.2 10.4 10.8 9.9 9.6 9.5 9.3 9.1 8.8 8.5 8.4
112/37:FF -1.8 -1.1 0.7 -1.0 -2.4 -1.1 -0.8 -0.6 1.3 1.7 0.9 0.8 0.7 0.7 0.9 1.1 1.8

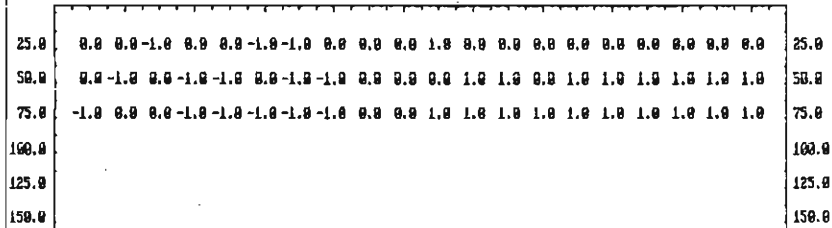
337/37 10.5 10.4 10.0 17.1 16.8 16.4 16.4 16.9 16.7 15.8 13.7 12.6 10.9 10.3 10.2 9.6 8.1 6.8 4.6 3.9
337/37:FF 1.8 2.5 1.9 1.1 -0.1 -0.8 0.8 4.1 6.2 6.8 5.1 3.8 1.4 2.8 4.9 6.3 6.4

1012/3 10.1 13.0 11.3 8.2 5.4 3.3 2.4 2.9 1.8 -0.2 -4.0 -7.2 -11.2 -13.6 -14.8 -17.0 -20.1 -23.9 -27.0 -31.0
1012/3:FF 12.4 11.5 10.0 7.9 3.4 1.0 3.7 9.7 13.6 13.4 12.0 10.8 7.0 8.7 12.2 14.6 14.8

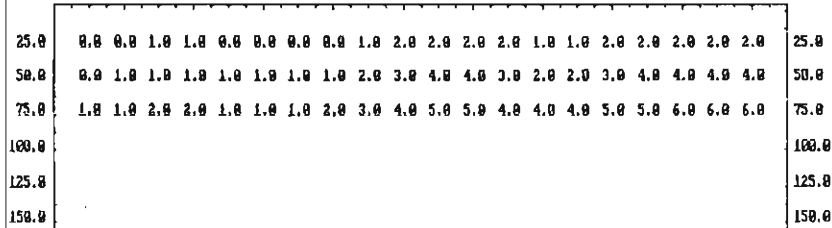
3037/3 -16.4 -24.2 -30.5 -36.3 -41.9 -44.5 -47.3 -47.7 -50.2 -52.4 -55.4 -57.3 -62.0 -63.4 -65.3 -67.4 -70.0 -73.1 -76.4 -79.8
3037/3:FF 26.2 23.5 19.6 13.6 8.6 6.1 7.6 9.9 10.1 12.3 13.5 8.6 6.5 8.7 10.4 12.1 12.3



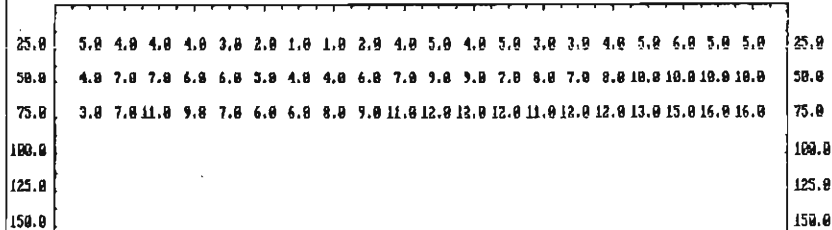
Pseudo-section of Filtered 112/37



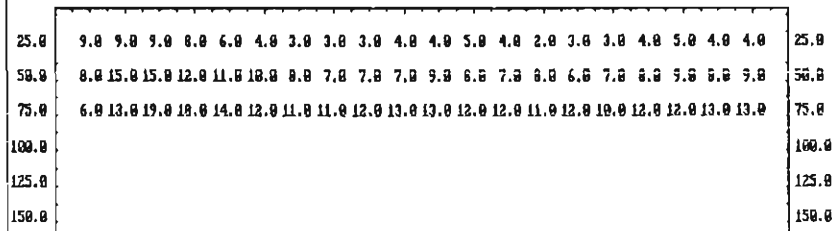
Pseudo-section of Filtered 337/37



Pseudo-section of Filtered 1012/3

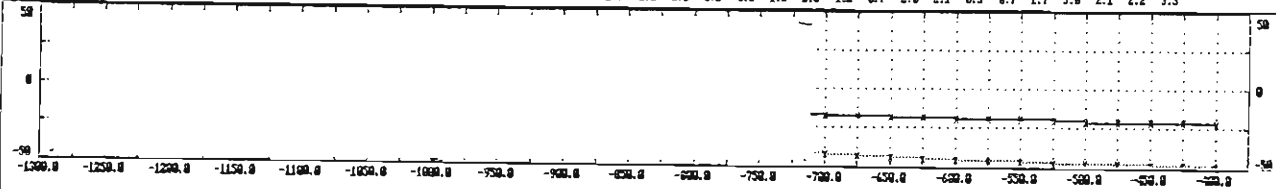


Pseudo-section of Filtered 3037/3

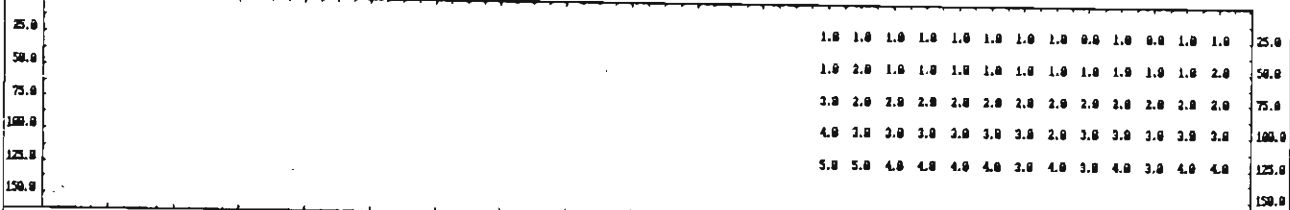


112/37	1.7	1.8	1.9	2.0	2.1	2.2	2.3	2.4	2.5	2.6	2.7	2.8	2.9	3.0	3.1	3.2	3.3	3.4	3.5	3.6	3.7	3.8	3.9	4.0	4.1	4.2	4.3	4.4	4.5	4.6	4.7	4.8	4.9	5.0	5.1	5.2	5.3	5.4	5.5	5.6	5.7	5.8	5.9	6.0	6.1	6.2	6.3	6.4	6.5	6.6	6.7	6.8	6.9	7.0	7.1	7.2	7.3	7.4	7.5	7.6	7.7	7.8	7.9	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	49.0	49.1	49.2	49.3	49.4	49.5	49.6	49.7	49.8	49.9	50.0	50.1	50.2	50.3	50.4	50.5	50.6	50.7	50.8	50.9	51.0	51.1	51.2	51.3	51.4	51.5	51.6	51.7	51.8	51.9	52.0	52.1	52.2	52.3	52.4	52.5	52.6	52.7	52.8	52.9	53.0	53.1	53.2	53.3	53.4	53.5	53.6	53.7	53.8	53.9	54.0	54.1	54.2	54.3	54.4	54.5	54.6	54.7	54.8	54.9	55.0	55.1	55.2	55.3	55.4	55.5	55.6	55.7	55.8	55.9	56.0	56.1	56.2	56.3	56.4	56.5	56.6	56.7	56.8	56.9	57.0	57.1	57.2	57.3	57.4	57.5	57.6	57.7	57.8	57.9	58.0	58.1	58.2	58.3	58.4	58.5	58.6	58.7	58.8	58.9	59.0	59.1	59.2	59.3	59.4	59.5	59.6	59.7	59.8	59.9	60.0	60.1	60.2	60.3	60.4	60.5	60.6	60.7	60.8	60.9	61.0	61.1	61.2	61.3	61.4	61.5	61.6	61.7	61.8	61.9	62.0	62.1	62.2	62.3	62.4	62.5	62.6	62.7	62.8	62.9	63.0	63.1	63.2	63.3	63.4	63.5	63.6	63.7	63.8	63.9	64.0	64.1	64.2	64.3	64.4	64.5	64.6	64.7	64.8	64.9	65.0	65.1	65.2	65.3	65.4	65.5	65.6	65.7	65.8	65.9	66.0	66.1	66.2	66.3	66.4	66.5	66.6	66.7	66.8	66.9	67.0	67.1	67.2	67.3	67.4	67.5	67.6	67.7	67.8	67.9	68.0	68.1	68.2	68.3	68.4	68.5	68.6	68.7	68.8	68.9	69.0	69.1	69.2	69.3	69.4	69.5	69.6	69.7	69.8	69.9	70.0	70.1	70.2	70.3	70.4	70.5	70.6	70.7	70.8	70.9	71.0	71.1	71.2	71.3	71.4	71.5	71.6	71.7	71.8	71.9	72.0	72.1	72.2	72.3	72.4	72.5	72.6	72.7	72.8	72.9	73.0	73.1	73.2	73.3	73.4	73.5	73.6	73.7	73.8	73.9	74.0	74.1	74.2	74.3	74.4	74.5	74.6	74.7	74.8	74.9	75.0	75.1	75.2	75.3	75.4	75.5	75.6	75.7	75.8	75.9	76.0	76.1	76.2	76.3	76.4	76.5	76.6	76.7	76.8	76.9	77.0	77.1	77.2	77.3	77.4	77.5	77.6	77.7	77.8	77.9	78.0	78.1	78.2	78.3	78.4	78.5	78.6	78.7	78.8	78.9	79.0	79.1	79.2	79.3	79.4	79.5	79.6	79.7	79.8	79.9	80.0	80.1	80.2	80.3	80.4	80.5	80.6	80.7	80.8	80.9	81.0	81.1	81.2	81.3	81.4	81.5	81.6	81.7	81.8	81.9	82.0	82.1	82.2	82.3	82.4	82.5	82.6	82.7	82.8	82.9	83.0	83.1	83.2	83.3	83.4	83.5	83.6	83.7	83.8	83.9	84.0	84.1	84.2	84.3	84.4	84.5	84.6	84.7	84.8	84.9	85.0	85.1	85.2	85.3	85.4	85.5	85.6	85.7	85.8	85.9	86.0	86.1	86.2	86.3	86.4	86.5	86.6	86.7	86.8	86.9	87.0	87.1	87.2	87.3	87.4	87.5	87.6	87.7	87.8	87.9	88.0	88.1	88.2	88.3	88.4	88.5	88.6	88.7	88.8	88.9	89.0	89.1	89.2	89.3	89.4	89.5	89.6	89.7	89.8	89.9	90.0	90.1	90.2	90.3	90.4	90.5	90.6	90.7	90.8	90.9	91.0	91.1	91.2	91.3	91.4	91.5	91.6	91.7	91.8	91.9	92.0	92.1	92.2	92.3	92.4	92.5	92.6	92.7	92.8	92.9	93.0	93.1	93.2	93.3	93.4	93.5	93.6	93.7	93.8	93.9	94.0	94.1	94.2	94.3	94.4	94.5	94.6	94.7	94.8	94.9	95.0	95.1	95.2	95.3	95.4	95.5	95.6	95.7	95.8	95.9	96.0	96.1	96.2	96.3	96.4	96.5	96.6	96.7	96.8	96.9	97.0	97.1	97.2	97.3	97.4	97.5	97.6	97.7	97.8	97.9	98.0	98.1	98.2	98.3	98.4	98.5	98.6	98.7	98.8	98.9	99.0	99.1	99.2	99.3	99.4	99.5	99.6	99.7	99.8	99.9	100.0	100.1	100.2	100.3	100.4	100.5	100.6	100.7	100.8	100.9	101.0	101.1	101.2	101.3	101.4	101.5	101.6	101.7	101.8	101.9	102.0	102.1	102.2	102.3	102.4	102.5	102.6	102.7	102.8	102.9	103.0	103.1	103.2	103.3	103.4	103.5	103.6	103.7	103.8	103.9	104.0	104.1	104.2	104.3	104.4	104.5	104.6	104.7	104.8	104.9	105.0	105.1	105.2	105.3	105.4	105.5	105.6	105.7	105.8	105.9	106.0	106.1	106.2	106.3	106.4	106.5	106.6	106.7	106.8	106.9	107.0	107.1	107.2	107.3	107.4	107.5	107.6	107.7	107.8	107.9	108.0	108.1	108.2	108.3	108.4	108.5	108.6	108.7	108.8	108.9	109.0	109.1	109.2	109.3	109.4	109.5	109.6	109.7	109.8	109.9	110.0	110.1	110.2	110.3	110.4	110.5	110.6	110.7	110.8	110.9	111.0	111.1	111.2	111.3	111.4	111.5	111.6	111.7	111.8	111.9	112.0	112.1	112.2	112.3	112.4	112.5	112.6	112.7	112.8	112.9	113.0	113.1	113.2	113.3	113.4	113.5	113.6	113.7	113.8	113.9	114.0	114.1	114.2	114.3	114.4	114.5	114.6	114.7	114.8	114.9	115.0	115.1	115.2	115.3	115.4	115.5	115.6	115.7	115.8	115.9	116.0	116.1	116.2	116.3	116.4	116.5	116.6	116.7	116.8	116.9	117.0	117.1	117.2	117.3	117.4	117.5	117.6	117.7	117.8	117.9	118.0	118.1	118.2	118.3	118.4	118.5	118.6	118.7	118.8	118.9	119.0	119.1	119.2	119.3	119.4	119.5	119.6	119.7	119.8	119.9	120.0	120.1	120.2	120.3	120.4	120.5	120.6	120.7	120.8	120.9	121.0	121.1	121.2	121.3	121.4	121.5	121.6	121.7	121.8	121.9	122.0	122.1	122.2	122.3	122.4	122.5	122.6	122.7	122.8	122.9	123.0	123.1	123.2	123.3	123.4	123.5	123.6	123.7	123.8	123.9	124.0	124.1	124.2	124.3	124.4	124.5	124.6	124.7	124.8	124.9	125.0	125.1	125.2	125.3	125.4	125.5	125.6	125.7	125.8	125.9	126.0	126.1	126.2	126.3	126.4	126.5	126.6	126.7	126.8	126.9	127.0	127.1	127.2	127.3	127.4	127.5	127.6	127.7	127.8	127.9	128.0	128.1	128.2	128.3	128.4	128.5	128.6	128.7	128.8	128.9	129.0	129.1	129.2	129.3	129.4	129.5	129.6	129.7	129.8	129.9	130.0	130.1	130.2	130.3	130.4	130.5	130.6	130.7	130.8	130.9	131.0	131.1	131.2	131.3	131.4	131.5	131.6	131.7	131.8	131.9	132.0	132.1	132.2	132.3	132.4	132.5	132.6	132.7	132.8	132.9	133.0	133.1	133.2	133.3	133.4	133.5	133.6	133.7	133.8	133.9	134.0	134.1	134.2	134.3	134.4	134.5	134.6	134.7	134.8	134.9	135.0</
--------	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	-------	---------

112/37 2.5 4.2 5.4 6.3 7.1 6.7 5.1 3.6 2.1 0.5 -2.5 -4.3 -6.2 -7.7 -9.2 -10.2 -11.4 -12.3 -13.9 -14.5 -15.3 -16.3 -16.7 -17.2 -17.5 -18.0 -18.7 -19.0 -19.5 -19.7 -20.3 -20.7 -21.0 -21.3 -21.4 -22.3
112/37:17 -3.9 -3.7 -2.1 1.4 3.1 5.1 6.1 7.7 9.4 9.5 7.1 6.2 5.3 4.9 4.5 4.6 4.7 3.5 3.2 3.2 2.3 1.7 1.6 2.0 2.2 1.8 1.5 1.3 1.3 1.7 1.3 1.0 1.4
337/37 7.0 9.4 12.2 14.7 17.7 16.5 9.1 2.0 -0.5 -4.5 -11.9 -16.2 -20.6 -24.1 -26.0 -29.6 -31.0 -31.0 -35.0777.9 -39.0 -40.4 -41.1 -42.0 -42.0 -42.0 -43.0 -45.1 -46.1 -46.6 -47.1 -47.3 -47.9 -48.0 -48.6 -48.9
337/37:17 -10.5 -10.0 -7.5 6.8 22.5 25.5 16.9 18.7 25.1 28.6 15.0 15.9 11.5 18.5 9.2 8.3787.3786.2835.2864.5 3.7 3.5 3.5 4.8 4.5 3.4 1.6 1.3 1.7 1.4 1.4 1.3 1.7
1012/3 12.1 14.9 17.7 21.7 28.4 23.0 -0.7 -17.3 -23.9 -30.9 -33.0 -30.4 -53.0 -56.0 -58.0 -59.9 -61.1 -62.2 -63.2 -64.0 -64.6 -65.0 -64.9 -64.9 -64.7 -64.9 -65.0 -66.5 -66.1 -65.9 -66.3 -67.1 -67.5 -67.7 -69.3 -70.9
1012/3:17 -12.4 -17.5 -12.0 27.0 70.2 64.3 36.0 32.7 36.6 27.5 17.6 12.6 8.9 7.0 5.4 4.4 2.9 3.2 2.4 1.3 0.2 -0.3 -0.2 1.1 2.7 1.9 -0.2 -0.4 1.4 2.4 1.0 2.4 5.0
3037/3 19.2 14.3 9.8 8.2 14.9 2.3 -27.1 -62.3 -67.3 -72.4 -83.3 -86.6 -88.0 -88.1 -77.0 -66.0 -66.0 -65.3 -65.0 -65.1 -64.7 -64.0 -64.4 -63.5 -63.3 -62.5 -64.1 -64.7 -65.0 -64.1 -63.9 -66.1 -66.0 -67.4 -68.0
3037/3:17 15.0 8.4 1.4 50.5 114.6 92.8 42.3 28.1 30.2 10.9 6.3 1.4 -2.4 -4.0 -2.5 -1.7 -1.2 -0.5 -0.6 -0.6 -1.5 -2.3 -1.2 0.7 2.0 2.1 0.3 -0.7 1.7 3.0 2.1 2.2 3.3



Pseudo-section of Filtered 112/37



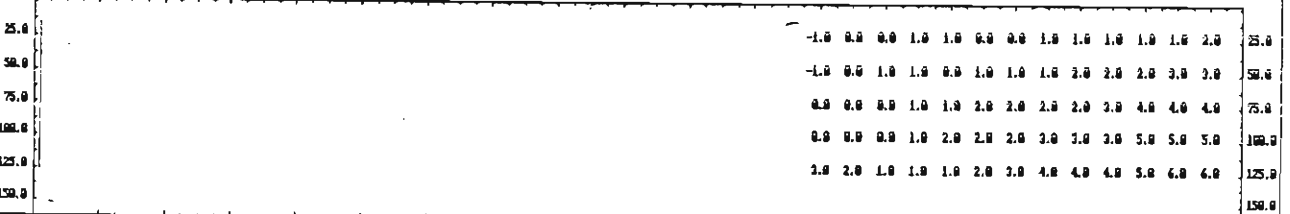
Pseudo-section of Filtered 337/37



Pseudo-section of Filtered 1012/3



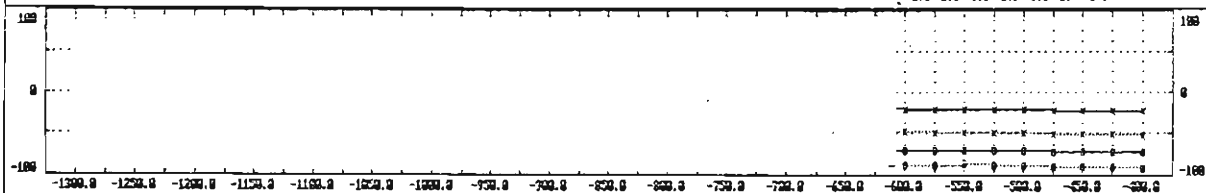
Pseudo-section of Filtered 3037/3



[illegible]

112/37
112/37:IT
337/37
337/37:IT
1012/3
1012/3:IT
3037/3
3037/3:IT

4-21.5-21.5-21.6-21.7-22.3-22.4-22.0-23.2
2.0 1.6 0.7 0.5 1.4 1.2 1.3
19-40.0-49.1-49.5-49.6-50.4-51.0-51.7-52.5
2.0 1.9 1.2 1.4 2.3 2.7 2.0
11-70.4-70.5-70.9-70.9-71.3-71.7-71.9-72.0
1.2 0.9 0.9 0.8 1.2 1.4 0.9
10-53.2-55.5-57.4-57.8-57.8-59.5-70.0-71.0
0.0-2.3 0.5 2.5 3.3 2.7 2.5



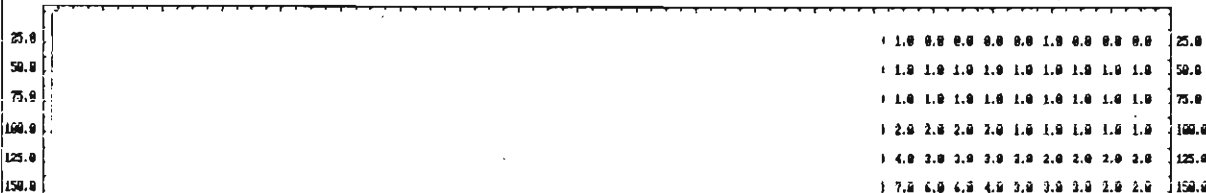
Pseudo-section of Filtered 112/37



Pseudo-section of Filtered 337/37



Pseudo-section of Filtered 1012/3



Pseudo-section of Filtered 3037/3

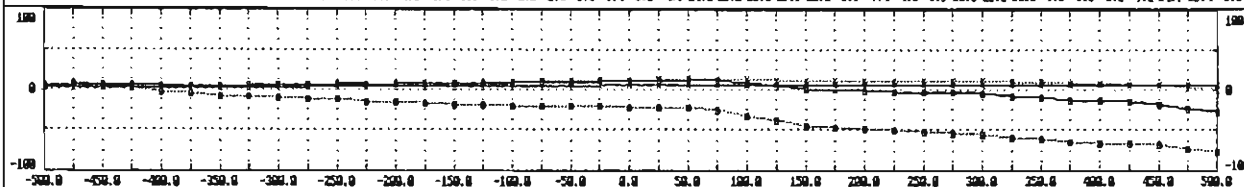


TWIN GRID - LARGE LOOP EM

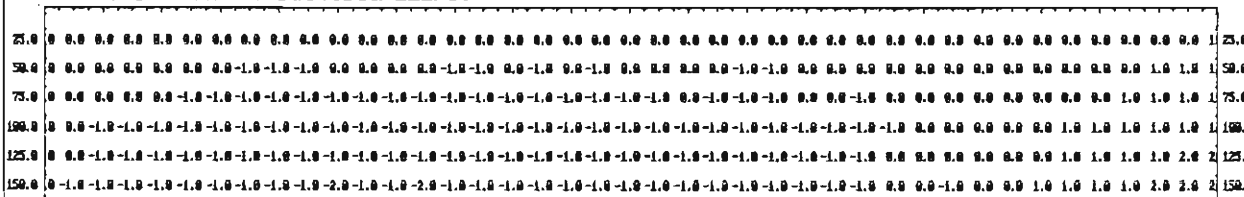
LINE 66+00E

DATE 10/25/86 OPERATOR D.N.M.

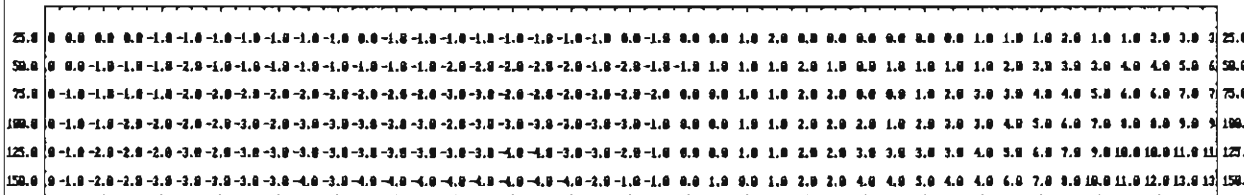
112/37: 1.7 1.9 1.9 2.0 2.1 2.3 2.4 2.7 3.0 3.1 3.3 3.3 3.5 3.7 3.7 4.4 4.4 4.4 4.9 4.8 5.2 5.0 5.2 5.3 5.3 5.8 5.9 6.0 5.8 5.9 6.4 6.3 6.3 6.2 6.1 6.0 6.4 6.1 5.7 5.3 4.7
112/37:HW2 -0.3 -0.4 -0.4 -0.5 -0.6 -0.7 -1.0 -1.0 -0.7 -0.5 -0.4 -0.6 -0.6 -0.9 -1.4 -0.7 -0.3 -0.5 -0.7 -0.5 -0.2 -0.3 -0.4 -0.6 -1.1 -0.8 -0.1 0.2 -0.3 -1.0 -0.3 0.2 0.3 0.4 -0.1 -0.4 0.6 1.5 1.0 1.7
337/37: 2.0 2.9 2.1 3.2 3.7 4.1 4.6 5.2 5.7 6.2 6.4 6.7 7.3 7.7 8.2 9.2 10.0 10.2 11.3 11.5 12.0 13.0 12.5 13.3 10.7 10.3 10.7 10.5 10.0 10.6 10.4 10.2 9.6 8.9 7.4 6.5 5.0 4.9 2.4 0.0 -1.6
337/37:HW2 0.2 0.4 -1.9 -2.5 -1.8 -2.0 -2.2 -2.1 -1.7 -1.2 -1.4 -1.9 -1.9 -2.4 -3.3 -2.0 -2.3 -2.6 -2.0 -2.2 -2.0 -0.8 1.5 4.0 3.0 -0.2 0.5 0.4 -0.5 0.0 1.2 2.2 3.6 4.5 3.9 3.2 5.0 7.5 8.1 7.0
1012/3: 4.9 4.9 4.0 4.0 4.5 4.6 4.9 5.7 6.0 4.7 6.1 6.6 7.3 7.2 8.0 8.7 9.5 9.4 11.3 10.8 11.5 13.1 10.7 7.6 4.0 0.6 0.3 -0.9 -2.0 -2.0 -3.4 -5.8 -0.2 -10.0 -13.3 -14.5 -16.0 -19.1 -24.1 -28.3 -34.0
1012/3:HW2 -0.7 1.0 1.2 -0.3 -1.0 -1.5 -2.2 -2.3 -1.1 0.0 -1.1 -1.0 -1.3 -2.2 -3.0 -2.2 -2.5 -3.2 -1.6 -2.5 -1.5 6.3 12.2 13.7 10.7 5.2 4.6 5.0 2.5 3.6 7.0 9.0 9.3 9.6 7.2 7.3 12.7 17.8 19.6 17.9
3037/3: 6.3 4.5 1.7 -3.5 -5.2 -7.9 -9.4 -10.0 -11.3 -12.6 -13.2 -16.5 -17.0 -18.7 -19.2 -20.4 -20.6 -21.2 -20.0 -22.3 -23.1 -23.1 -23.1 -26.9 -33.4 -30.0 -35.3 -46.0 -49.4 -51.6 -52.0 -53.6 -56.9 -59.3 -62.3 -64.5 -66.4 -67.0 -69.0 -70.5 -77.2 -80.7
3037/3:HW4 6.3 13.6 13.3 10.9 0.2 6.3 4.0 4.5 6.5 7.0 5.7 4.0 4.4 3.9 3.1 2.2 1.0 1.3 3.4 3.1 4.6 14.1 22.2 23.0 13.9 12.1 0.9 7.4 4.6 6.9 10.6 11.1 10.6 9.3 6.6 5.1 9.1 14.7 15.4 0.6



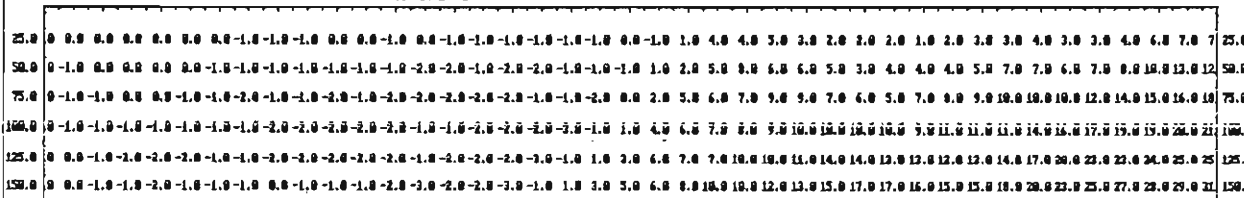
Pseudo-section of Filtered 112/37



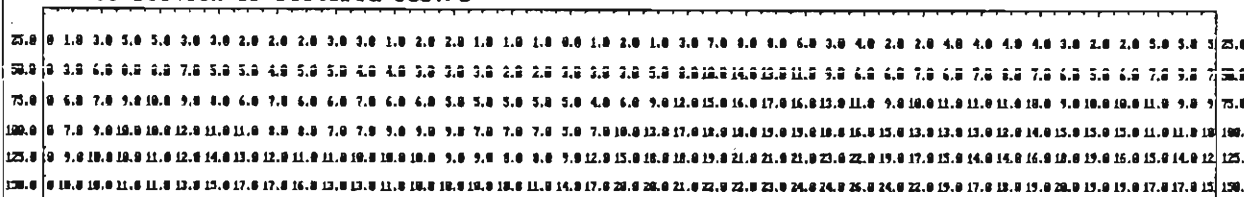
Pseudo-section of Filtered 337/37



Pseudo-section of Filtered 1012/3



Pseudo-section of Filtered 3037/3

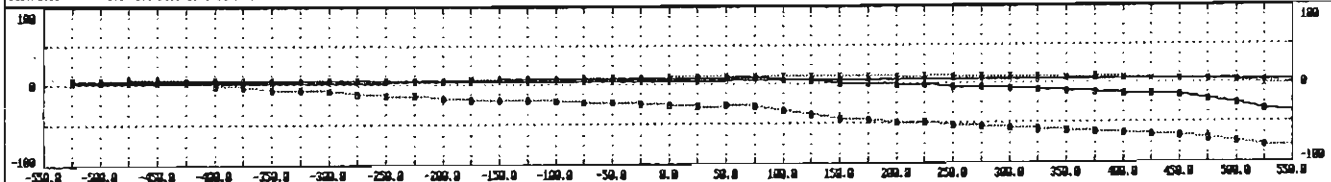


112/37 1.9 2.0 2.0 2.1 2.2 2.1 2.4 2.5 2.6 2.8 2.8 2.8 3.2 3.2 3.3 3.5 3.5 3.8 3.9 4.3 4.3 4.6 5.1 5.3 5.1 4.8 5.2 5.3 5.1 5.6 5.4 5.4 5.9 5.9 5.6 6.2 5.9 5.5 5.4 5.3 4.6 4.2 3.8
112/37:FF -0.2 -0.1 -0.2 -0.2 -0.1 -0.5 -0.5 -0.4 -0.6 -0.6 -0.3 -0.4 -0.5 -0.5 -0.3 -0.3 -0.9 -0.7 -0.6 -0.8 -1.2 -0.7 0.5 0.4 -0.6 -0.6 -0.2 -0.6 -0.1 -0.3 -1.0 -0.2 -0.1 -0.7 0.5 1.3 0.7 1.0 1.0 1.9

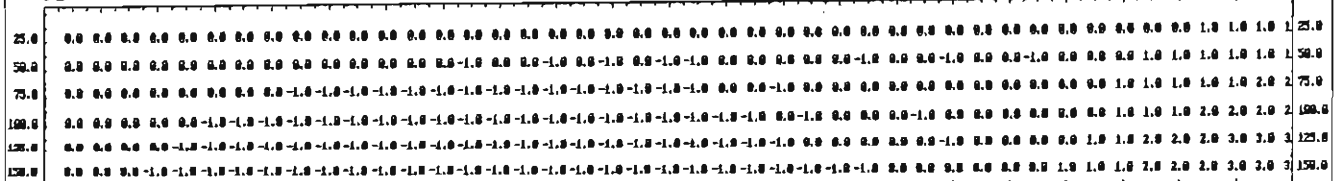
337/37 2.3 2.7 3.0 3.4 3.6 3.8 4.0 4.4 4.9 5.0 5.4 5.6 6.1 6.4 6.9 7.7 8.1 8.1 8.5 9.5 9.4 10.3 10.3 11.4 11.5 11.5 10.5 10.0 10.0 9.4 10.2 8.8 9.5 8.7 8.8 7.8 8.4 7.3 6.3 5.4 4.5 1.5 -1.2 -2.7
337/37:FF -1.2 -1.3 -1.0 -0.8 -1.0 -1.5 -1.5 -1.1 -1.1 -1.3 -1.5 -1.6 -2.1 -2.5 -1.6 -0.8 -1.0 -2.3 -1.7 -1.7 -2.0 -2.3 -1.1 1.1 2.3 1.9 0.7 -0.1 0.7 1.0 0.9 0.8 1.6 1.3 0.9 2.6 4.0 3.7 5.7 9.6 9.5

1012/3 3.3 3.9 4.0 3.5 5.4 5.1 4.8 4.9 5.5 5.6 5.5 5.3 5.6 5.6 5.8 7.0 7.1 7.0 7.2 7.8 7.2 8.0 7.7 9.0 8.6 6.1 3.6 1.1 -0.5 -2.4 -2.3 -5.0 -5.2 -7.4 -7.0 -10.0 -11.5 -13.2 -14.5 -16.5 -21.0 -27.0 -32.6 -36.4
1012/3:FF -3.1 -2.3 -0.2 1.0 0.6 -0.5 -1.4 -0.7 0.3 0.2 -0.4 -0.5 -1.6 -2.7 -1.3 -0.1 -0.9 -0.8 -0.2 -0.7 -1.5 -1.9 2.0 7.9 10.0 9.1 7.6 5.3 4.4 5.5 5.3 5.0 5.2 6.3 6.9 6.2 6.3 9.0 17.0 22.1 21.0

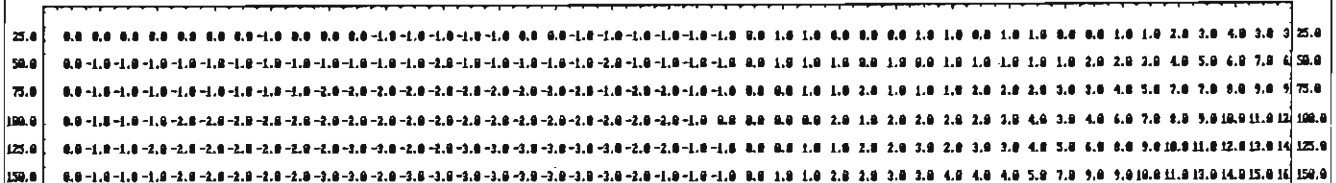
3037/3 5.4 5.8 7.5 7.6 5.8 -0.8 -4.1 -4.2 -7.3 -9.3 -11.3 -12.3 -14.7 -16.7 -18.3 -18.4 -20.0 -21.2 -22.4 -23.4 -25.3 -25.0 -27.2 -27.0 -28.6 -30.7 -30.7 -33.7 -30.7 -33.0 -46.1 -40.9 -49.5 -53.5 -54.0 -57.0 -57.0 -58.2 -62.0 -63.3 -64.7 -66.0 -69.6 -74.5 -79.9 -81.1
3037/3:FF -3.9 0.7 10.5 17.5 14.5 0.8 6.5 6.9 7.0 7.4 6.8 7.0 5.3 3.4 4.5 5.2 4.6 5.1 5.3 4.3 3.1 2.4 8.1 16.8 15.4 16.7 13.3 9.3 0.0 9.1 8.0 7.0 6.7 7.7 7.6 5.8 5.4 7.6 13.4 17.0 15.9



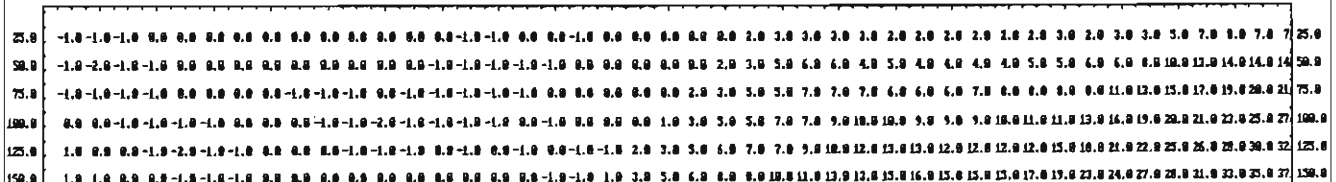
Pseudo-section of Filtered 112/37



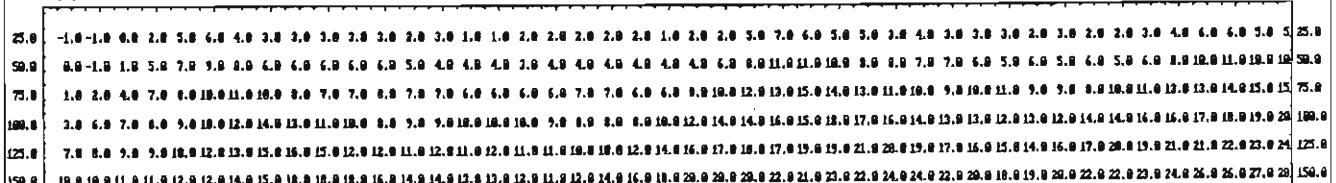
Pseudo-section of Filtered 337/37



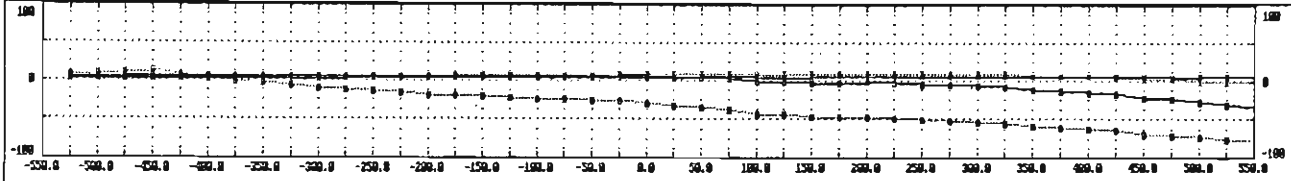
Pseudo-section of Filtered 1012/3



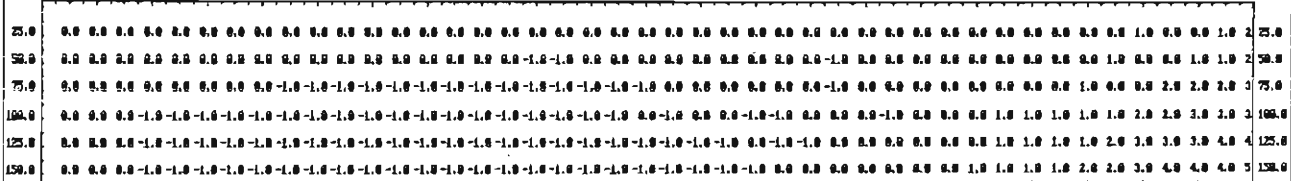
Pseudo-section of Filtered 3037/3



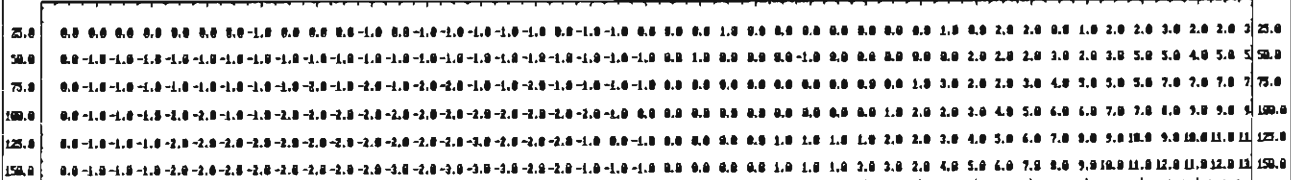
112/77 1.0 1.5 2.0 2.1 2.4 2.3 2.4 2.6 2.7 2.8 2.9 3.0 3.3 3.3 3.4 3.5 3.8 3.9 4.0 4.2 4.3 4.5 4.7 5.0 4.5 4.6 4.9 5.1 5.2 5.4 5.4 5.3 5.1 5.0 4.9 5.3 5.1 5.2 4.8 4.2 4.7 5.2 3.1
 112/77:IT -0.4-0.6-0.6-0.2-0.3-0.6-0.5-0.4-0.4-0.6-0.7-0.4-0.3-0.6-0.6-0.6-0.5-0.9-0.7 0.0-0.3-0.3-0.3 0.6 0.1-0.6-0.5-0.7-0.5-0.1 0.4-0.2-0.3 0.7 0.2-0.1 0.4 1.3 1.1-0.9 0.6
 337/77 2.3 2.6 3.0 3.2 3.7 3.8 3.9 4.4 4.7 5.0 5.1 5.5 6.0 6.0 6.7 6.9 7.5 7.7 8.1 8.0 9.1 9.0 9.1 9.1 8.7 7.8 8.4 8.3 8.5 9.0 8.8 8.9 8.0 8.3 8.5 5.4 5.3 6.0 4.5 2.7 1.2-0.7-1.6-0.7
 337/77:IT -1.3-1.3-1.3-0.8-0.8-1.4-1.4-1.0-0.9-1.4-1.4-1.2-1.6-1.7-1.6-1.4-0.9-1.3-2.0-1.0-0.1 0.3 1.7 1.6-0.2-0.6-0.8-1.0-0.2 0.1 0.6 0.5 3.0 5.2 2.2 1.0 4.7 6.6 6.7 6.2 5.0
 1012/3 2.4 4.5 3.5 6.3 6.3 5.7 5.1 5.7 5.2 5.3 4.9 5.1 5.6 4.8 5.3 5.2 5.0 5.3 5.7 5.1 6.9 5.7 4.2 3.3 1.4-1.7-1.4-3.0-2.0-2.1-3.6-4.5-5.9-7.1-7.0-12.3-13.9-14.9-17.9-22.3-24.9-26.7-32.1-35.7
 1012/3:IT -3.9-2.6-0.2 1.0 1.2-0.1 0.3 0.7 0.5-0.5-0.4 0.6-0.1-0.9-0.6 0.0 0.3-1.0-1.0 2.1 5.1 5.2 7.0 7.0 4.1 2.7 0.5-0.1 3.2 4.7 4.9 4.5 7.1 11.3 8.6 5.9 10.9 15.1 14.0 13.6 14.2
 3037/3 6.7 9.5 11.1 12.3 7.9 2.0-2.4-4.1-7.5-9.9-12.2-14.2-15.9-18.3-19.7-21.6-22.5-24.5-25.3-27.0-28.5-29.5-32.7-35.7-38.3-43.3-44.5-46.0-47.4-47.8-49.0-51.3-53.2-54.0-56.0-60.2-61.5-62.0-65.2-69.7-71.6-74.3-77.3-78.3
 3037/3:IT -7.2 0.4 13.5 20.6 16.4 11.2 10.9 10.5 9.0 0.0 7.0 7.5 7.1 6.1 5.7 5.6 5.2 3.8 3.0 0.7 11.9 11.9 14.3 13.7 9.1 6.4 3.5 3.4 5.9 6.9 6.9 6.3 0.2 10.9 0.1 6.3 10.6 13.3 11.0 10.3 9.7



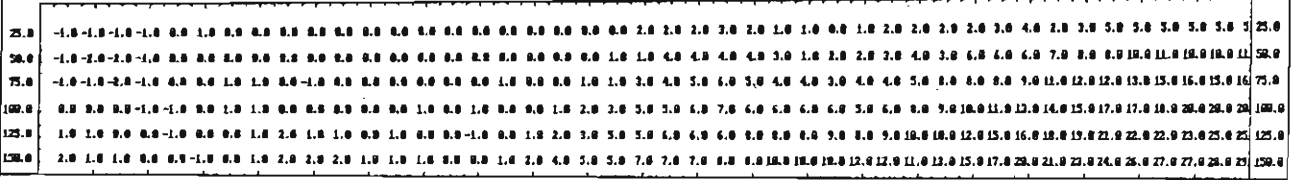
Pseudo-section of Filtered 112/37



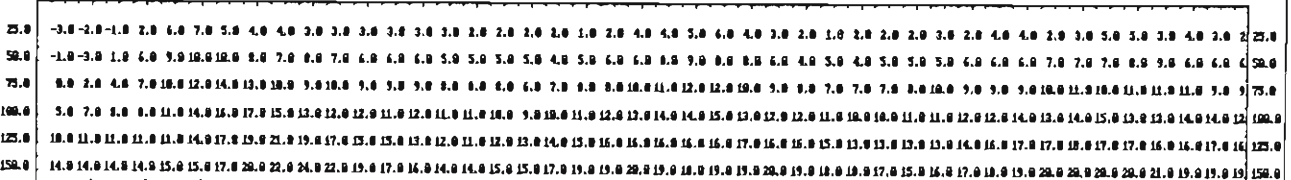
Pseudo-section of Filtered 337/37



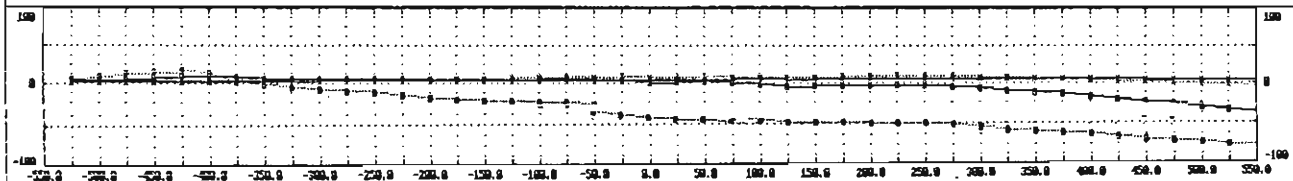
Pseudo-section of Filtered 1012/3



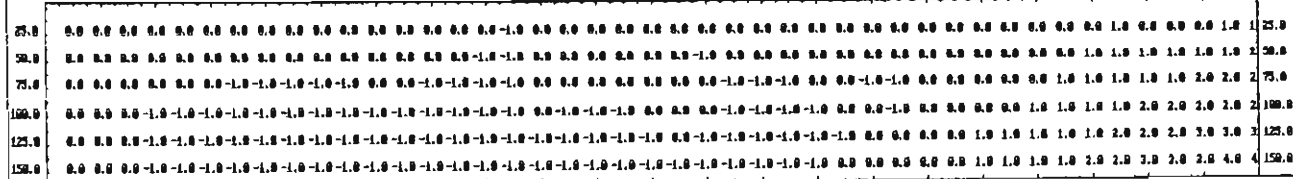
Pseudo-section of Filtered 3037/3



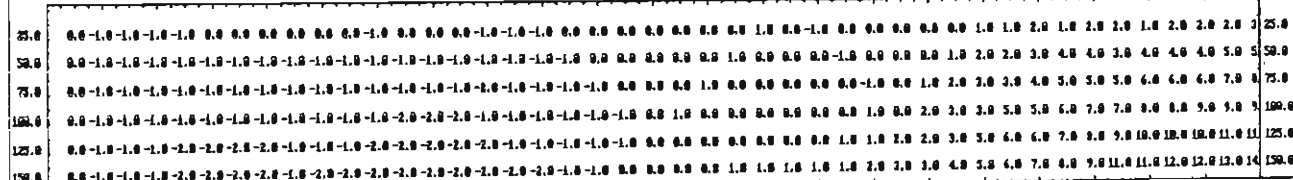
112/77 1.9 2.0 2.2 2.1 2.3 2.5 2.6 2.7 2.9 3.0 3.1 3.2 3.5 3.4 3.6 4.3 4.3 4.1 4.2 3.9 4.4 4.4 4.8 4.7 4.5 4.7 5.3 5.3 5.2 5.3 5.6 5.7 5.5 5.4 5.4 5.2 5.0 4.2 4.5 4.2 4.4 3.2
112/37:77 -0.4 -0.2 -0.5 -0.7 -0.5 -0.4 -0.5 -0.6 -0.5 -0.6 -0.2 0.0 -0.3 -1.2 -1.4 -0.3 0.3 0.3 0.0 -0.7 -0.9 -0.7 0.0 0.3 -0.0 -1.4 -0.5 0.1 -0.4 -0.3 -0.3 0.4 0.4 0.3 0.4 1.4 1.5 0.5 0.1 1.1
337/77 2.4 2.8 2.2 2.6 3.9 4.4 4.4 4.6 4.0 5.0 5.3 5.7 6.1 6.0 6.0 6.4 7.0 7.0 8.4 7.9 8.2 7.5 7.8 8.2 8.0 8.0 8.0 8.7 7.7 8.5 8.4 8.6 8.3 8.7 8.0 7.7 6.3 5.3 4.5 2.5 1.2 1.0 -1.2 -2.2 -4.4
337/37:77 -1.6 -1.5 -1.5 -1.3 -0.7 -0.6 -0.8 -0.5 -1.2 -1.5 -1.1 -0.2 -0.3 -1.4 -2.0 -2.0 1.5 0.1 0.6 0.0 -0.3 -0.9 0.0 1.5 1.6 -1.5 -2.5 -0.0 0.0 0.0 0.2 1.3 2.7 4.1 4.2 4.6 6.1 4.0 3.9 5.6 6.4
1012/7 3.2 4.3 5.9 7.2 8.2 8.4 6.6 6.4 5.9 5.6 5.5 5.3 4.4 4.0 4.5 4.6 5.6 5.8 4.0 3.5 1.1 1.5 1.2 -0.5 -1.0 -0.3 -3.4 -2.6 -4.0 -3.9 -3.4 -4.7 -7.0 -9.5 -12.5 -14.0 -16.9 -20.2 -25.1 -26.7 -29.7 -32.3 -37.3
1012/3:77 -0.4 -0.0 -0.5 0.4 3.6 2.7 1.5 1.2 0.5 0.3 1.3 2.4 1.2 -0.7 -1.7 -2.3 0.4 3.9 5.2 4.9 1.9 1.9 3.0 7.0 6.6 -0.9 -2.3 1.7 0.9 0.4 4.2 5.2 10.3 10.0 0.9 10.6 14.4 14.7 11.1 11.4 14.4
3037/3 5.3 0.3 11.9 16.7 16.6 12.4 2.1 -0.9 -4.7 -7.9 10.2 12.0 15.7 19.0 21.0 21.9 23.2 23.9 25.2 28.0 30.7 35.5 36.9 37.3 40.5 40.6 47.4 47.4 46.6 49.9 50.0 51.2 53.9 57.3 60.0 61.9 63.4 66.5 69.5 72.3 73.9 76.7 79.5
3037/3:77 -13.0 11.1 -2.4 16.8 27.3 20.1 13.0 12.5 10.4 10.4 11.7 11.5 0.2 5.1 4.2 4.0 6.9 10.4 12.2 12.0 7.1 6.3 10.8 13.2 10.7 3.0 1.4 5.5 3.7 1.7 3.1 9.9 12.3 10.0 0.0 0.0 10.7 11.9 10.2 0.0 10.0



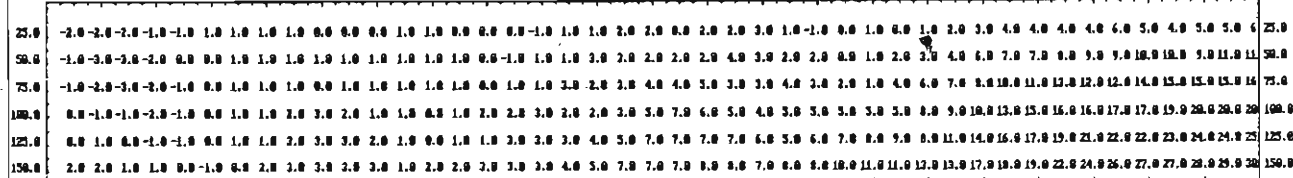
Pseudo-section of Filtered 112/37



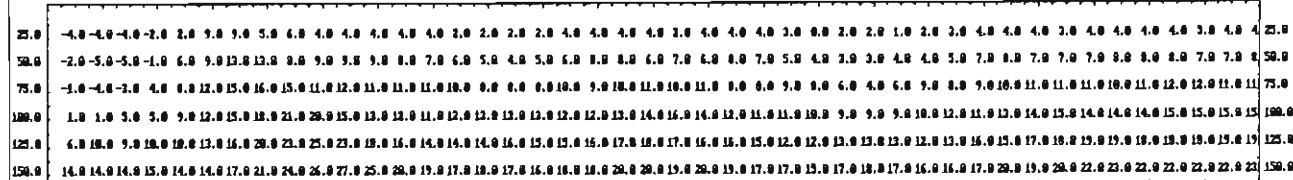
Pseudo-section of Filtered 337/37



Pseudo-section of Filtered 1012/3

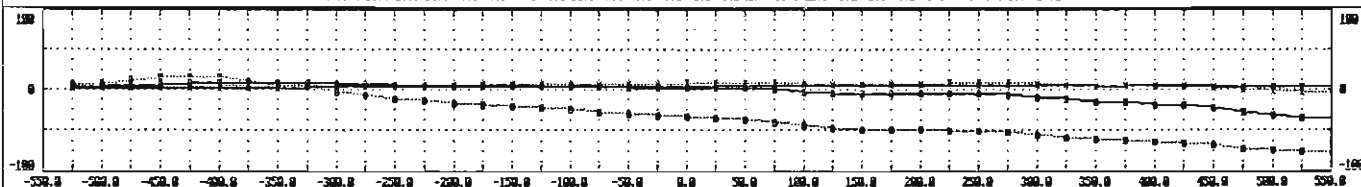


Pseudo-section of Filtered 3037/3

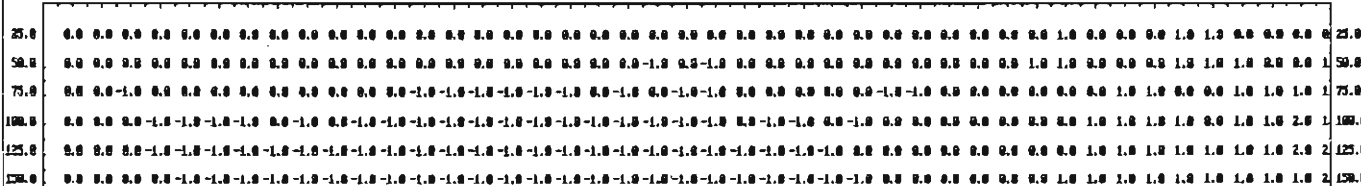


DATE 10/24/86 OPERATOR D.N.H.

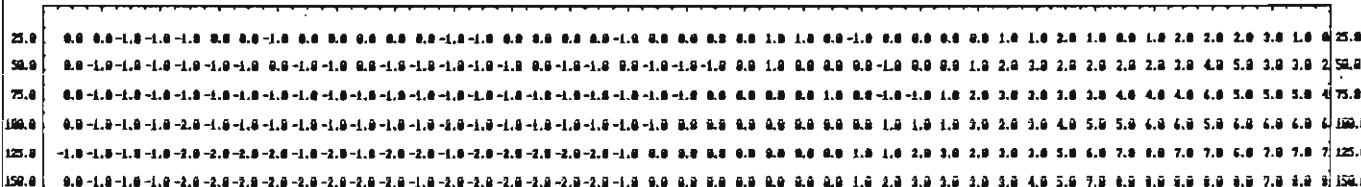
112/77 2.0 2.1 2.3 2.5 2.5 2.7 2.7 2.8 3.0 3.0 3.2 3.1 3.3 3.4 3.6 3.7 3.0 4.1 4.0 4.2 4.4 4.4 5.0 4.7 5.2 5.0 4.9 4.9 5.2 5.2 5.5 5.0 5.0 5.4 5.2 4.5 5.0 5.6 5.5 4.6 4.4 4.2 4.4 3.9
112/37:77 -0.7 -0.6 -0.5 -0.5 -0.2 -0.3 -0.3 -0.4 -0.3 -0.2 -0.4 -0.4 -0.4 -0.5 -0.4 -0.5 -0.3 -0.3 -0.6 -0.3 -0.5 -0.5 0.0 0.4 -0.2 -0.6 -0.6 -0.9 -0.1 0.0 1.7 1.3 -0.9 -1.6 0.5 2.1 1.5 0.4 0.3
337/77 2.0 3.0 3.3 3.0 4.1 4.0 4.6 5.0 5.4 5.1 5.7 5.5 5.0 6.1 6.6 6.9 7.2 7.5 7.0 7.5 7.0 8.2 8.4 8.5 8.6 7.4 6.8 7.6 7.9 8.1 8.5 8.9 8.3 7.2 6.8 4.0 4.8 3.9 3.2 1.5 0.2 -1.9 -4.1 -3.4
337/77:77 -1.3 -1.6 -1.8 -1.5 -0.7 -1.0 -0.9 -0.4 -0.7 -0.5 -0.7 -1.4 -1.6 -1.4 -1.2 -0.4 0.2 -0.8 -1.3 -1.3 -0.9 -0.5 0.9 2.9 1.6 -1.3 -1.6 -1.1 -1.4 -0.6 1.9 4.0 5.5 4.4 1.3 1.7 4.0 5.4 6.4 7.7 5.0
1012/3 4.3 5.0 6.1 7.0 6.6 9.6 0.6 0.5 0.9 7.0 7.0 3.4 3.3 4.9 4.9 5.2 4.6 4.7 3.0 2.7 2.5 2.4 2.2 1.2 0.4 -2.9 -5.0 -4.6 -4.4 -5.2 -4.5 -4.2 -4.6 -9.0 -12.6 -16.5 -16.4 -19.0 -20.0 -23.5 -27.5 -31.5 -33.7
1012/3:77 -4.6 -5.3 -4.3 -1.0 1.1 0.0 1.2 3.4 3.5 3.3 2.2 0.9 0.1 0.0 0.0 2.1 3.6 2.5 0.0 0.6 1.5 2.0 5.9 9.5 7.1 1.1 0.0 0.7 -0.9 1.1 7.7 11.6 12.7 10.5 6.3 6.1 0.1 12.0 15.5 15.0 12.0
3037/3 7.9 9.1 11.0 13.3 16.0 15.7 10.2 6.1 4.5 -3.2 -4.7 -11.0 -14.7 -17.5 -19.7 -20.0 -21.3 -24.7 -20.4 -30.4 -32.2 -33.5 -35.1 -37.1 -39.6 -46.3 -47.7 -40.5 -40.6 -49.9 -50.3 -50.2 -53.0 -56.0 -59.6 -62.3 -63.1 -65.5 -66.3 -68.0 -70.3 -75.0 -77.0 -76.7
3037/3:77 -10.1 -11.2 -5.4 6.2 16.2 15.3 13.0 20.5 19.0 16.6 13.7 10.7 0.3 6.9 7.5 9.0 10.0 9.5 6.9 6.0 6.5 8.1 11.7 15.3 12.3 5.1 2.3 3.1 2.0 3.0 9.3 13.2 12.1 9.0 6.7 6.4 6.5 10.3 13.2 10.7 6.2



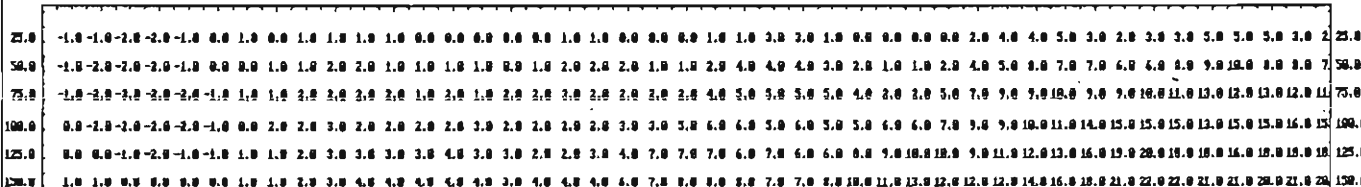
Pseudo-section of Filtered 112/37



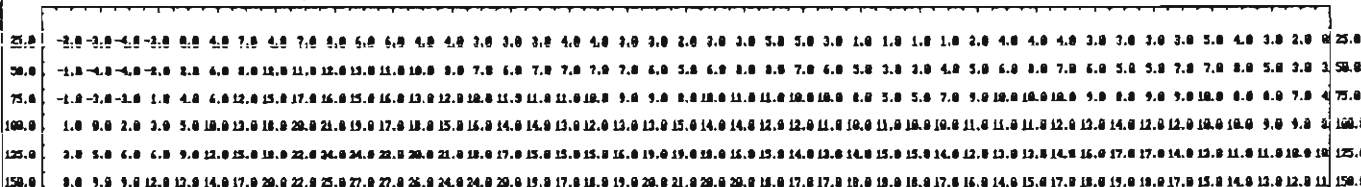
Pseudo-section of Filtered 337/37



Pseudo-section of Filtered 1012/3



Pseudo-section of Filtered 3037/3

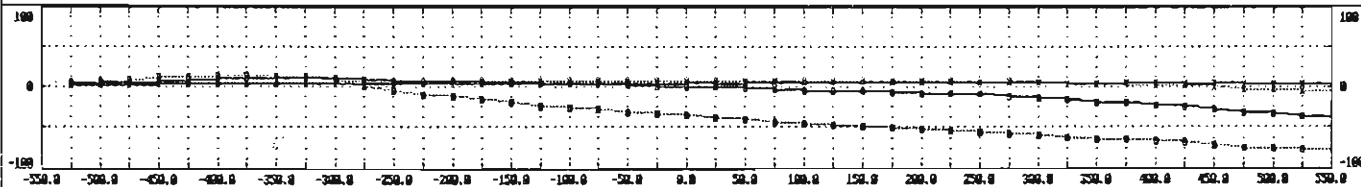


TWIN GRID - LARGE LOOP EM

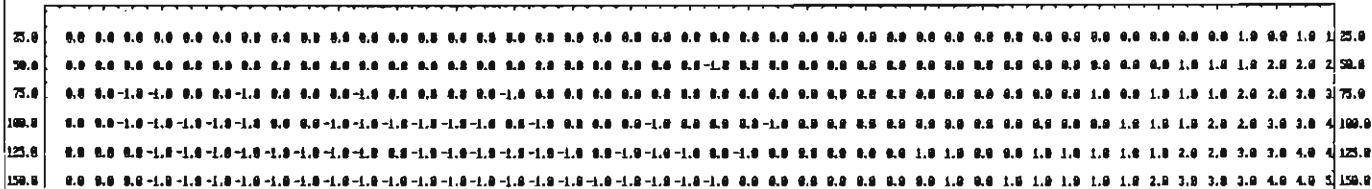
LINE 72+00E

DATE 10/14/86 OPERATOR D.M.H.

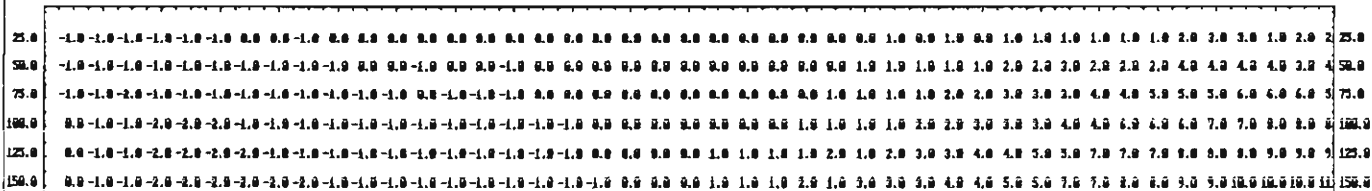
112/37 2.3 2.6 2.7 2.9 3.1 3.3 3.4 3.5 3.7 3.8 3.7 3.7 4.1 4.1 4.1 4.4 4.4 4.3 4.4 4.7 4.6 4.7 5.2 5.1 5.0 5.0 5.2 5.0 4.7 4.7 5.0 4.9 4.6 4.6 4.8 5.2 4.5 4.8 3.8 3.5 3.6 2.2
112/37:17 -0.7 -0.7 -0.8 -0.7 -0.3 -0.1 -0.5 -0.5 -0.1 -0.1 -0.5 -0.8 -0.4 0.0 -0.3 -0.6 -0.2 0.1 -0.4 -0.6 -0.2 -0.5 -1.0 -0.2 0.3 -0.1 -0.2 0.5 0.0 0.0 -0.4 0.3 0.6 0.0 -0.0 -0.3 0.7 1.1 2.0 1.5 1.5
337/37 3.1 3.3 4.0 4.5 5.0 5.5 5.7 5.8 6.3 6.7 6.2 6.4 6.4 6.8 7.0 7.0 7.1 7.7 7.5 7.4 7.4 7.7 7.6 7.5 7.6 7.3 7.3 7.3 6.5 6.5 5.8 4.6 5.2 4.4 3.4 2.7 2.6 1.3 0.4 -2.9 -3.6 -4.2 -6.0
337/37:17 -1.5 -2.0 -2.0 -1.7 -1.0 -0.9 -1.5 -0.8 0.4 0.1 -0.6 -1.0 -0.3 -0.0 -1.1 -0.1 0.4 -0.2 -0.5 0.0 0.2 0.2 0.5 0.3 0.0 0.0 1.6 1.5 0.6 0.5 2.0 4.0 3.5 2.5 2.2 3.6 6.4 0.2 5.3 3.7
1012/3 3.0 4.9 6.1 7.6 0.6 10.1 10.5 10.7 11.5 11.6 9.8 7.9 6.0 6.0 5.9 5.2 3.0 4.0 3.0 2.0 1.1 0.9 -0.5 -1.5 -3.0 -4.4 -4.0 -5.3 -7.1 -4.7 -9.0 -4.9 -11.3 -14.1 -16.4 -19.4 -19.3 -22.0 -24.0 -27.2 -32.3 -34.0 -37.0 -39.3
1012/3:17 -3.0 -5.2 -5.0 -4.4 -2.5 -1.6 -1.9 1.6 6.2 5.9 3.3 2.0 2.5 3.7 3.3 2.0 2.0 3.9 3.0 2.7 4.0 4.9 5.4 4.7 2.7 3.2 5.7 5.3 2.1 2.5 7.5 10.3 10.4 0.2 5.5 7.2 9.9 13.5 15.1 11.5 10.0
3037/3 5.0 7.4 9.0 12.1 12.0 14.1 13.6 12.1 12.0 0.0 0.1 -5.1 -10.3 -12.7 -16.3 -19.9 -24.0 -25.0 -28.6 -31.5 -33.7 -35.5 -38.2 -41.2 -43.6 -46.0 -47.2 -48.5 -50.0 -53.3 -55.3 -57.6 -60.6 -63.3 -64.9 -65.5 -67.5 -69.2 -71.3 -75.6 -76.1 -77.6 -79.1
3037/3:17 -0.7 -7.7 -5.0 -2.0 1.2 3.6 4.9 15.2 25.0 24.3 10.0 13.6 13.2 14.9 13.6 10.5 10.3 10.0 9.1 0.5 10.2 11.1 10.2 0.4 6.1 6.1 0.4 9.3 6.7 4.3 7.4 10.0 10.0 6.5 4.8 6.3 7.5 10.2 11.2 6.0 5.0



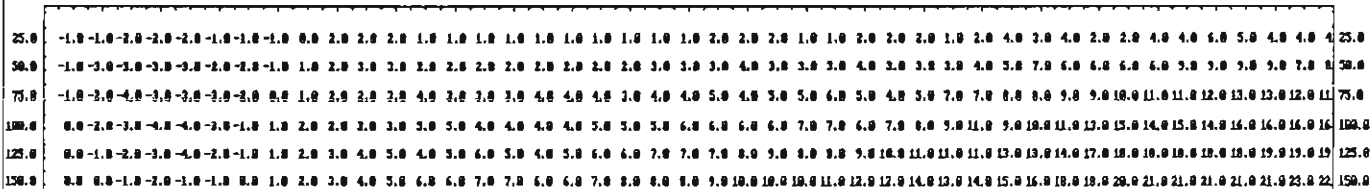
Pseudo-section of Filtered 112/37



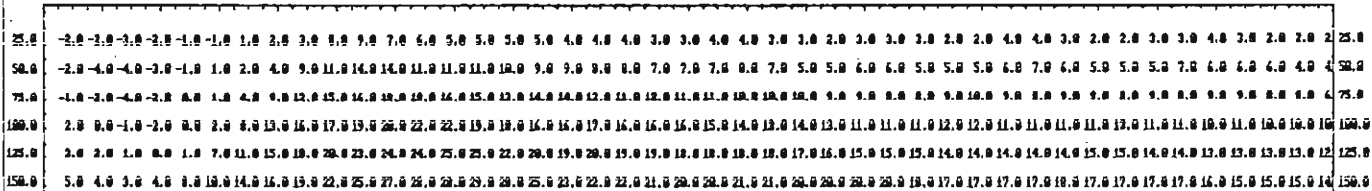
Pseudo-section of Filtered 337/37



Pseudo-section of Filtered 1012/3



Pseudo-section of Filtered 3037/3

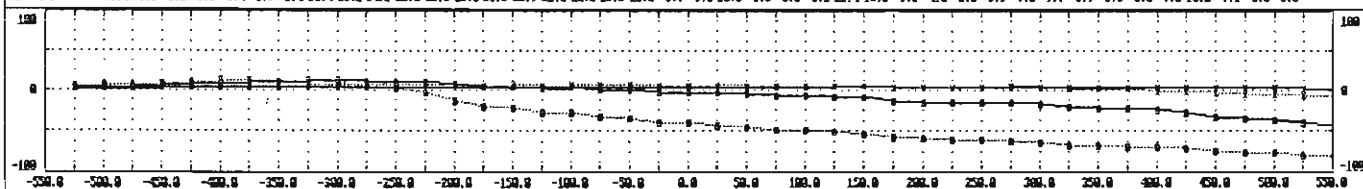


112/37 2.1 2.4 2.7 3.2 3.3 3.4 3.7 3.9 4.0 4.0 4.0 4.2 4.3 4.3 4.3 4.4 4.4 4.5 4.5 4.5 4.6 5.0 5.0 4.5 4.5 4.4 4.3 4.3 4.1 4.1 4.5 4.4 4.4 3.5 3.6 3.0 3.0 2.5 1.0
112/37:IT -1.4 -1.4 -2.5 -2.6 -2.9 -2.9 -2.4 -2.1 2.0 -2.2 -2.2 2.2 2.2 2.1 -2.3 -2.4 -2.4 2.1 2.0 -2.3 -2.2 -2.1 -2.2 -2.6 -2.9 2.1 1.8 2.6 2.1 -2.4 2.0 1.1 2.3 -2.7 -2.2 1.8 1.7 1.3 1.1 1.1 1.7

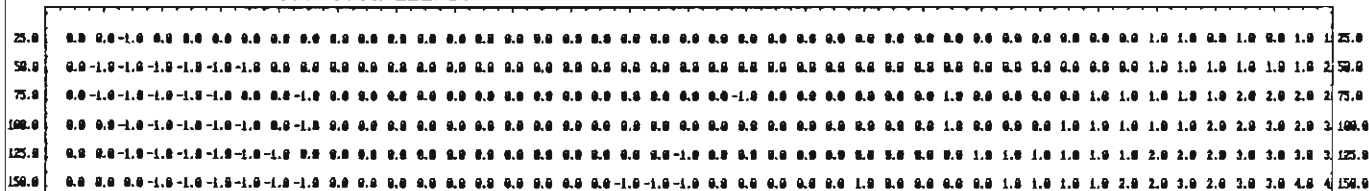
337/37 2.6 3.1 3.6 4.2 5.0 5.1 5.0 6.2 6.9 7.0 7.0 7.3 6.6 6.2 6.7 6.3 7.4 6.8 6.5 5.8 6.2 6.5 5.9 5.4 6.2 6.2 6.3 4.4 3.7 4.0 4.3 4.1 3.5 2.8 1.3 1.2 -1.5 -1.0 -3.2 -4.3 -5.6 -7.6 -8.6
337/37:IT -1.1 -2.3 -2.3 -1.7 -1.9 -2.2 -1.9 -2.9 -2.1 -2.3 2.1 1.5 1.0 -2.2 -2.0 -1.2 2.4 1.5 1.3 -2.4 -2.4 1.4 2.0 -1.1 -2.9 1.7 4.4 3.8 -2.2 -2.7 2.9 4.3 3.0 3.6 3.0 3.9 3.0 3.7 3.7 6.3

1012/3 3.5 4.6 5.7 7.0 8.9 9.6 10.9 11.5 12.9 12.5 11.3 11.2 10.6 6.6 4.2 3.0 2.2 2.9 0.7 -0.6 -2.6 -2.7 -3.5 -5.0 -4.8 -6.0 -7.0 -9.2 -13.1 -15.2 -14.9 -15.6 -16.1 -17.5 -21.6 -22.0 -23.1 -24.5 -28.0 -33.5 -34.7 -37.3 -41.0 -49.3
1012/3:IT -4.6 -5.6 -5.9 -4.6 -3.9 -3.9 -3.0 2.6 2.9 2.0 5.3 11.0 9.2 4.0 2.9 2.4 5.0 6.8 5.4 1.0 3.2 5.6 4.2 2.0 4.2 2.5 11.3 7.6 2.2 1.6 2.1 7.4 10.8 6.8 3.2 6.6 12.9 15.7 10.5 10.1 12.3

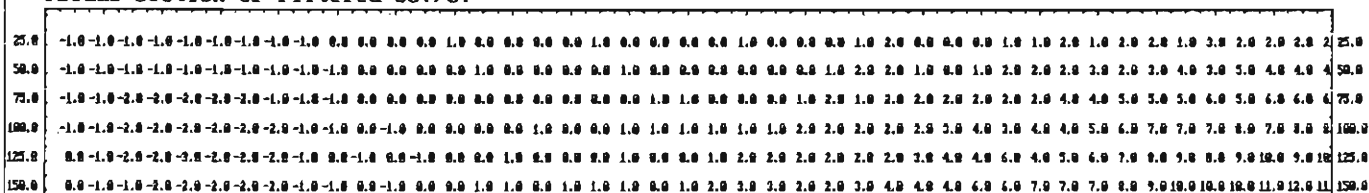
3037/3 4.7 6.7 8.0 9.0 11.2 11.8 11.0 10.8 12.2 9.0 7.6 1.5 -3.0 -12.9 -28.2 -23.0 -27.4 -28.7 -32.7 -35.6 -39.6 -40.9 -45.0 -46.4 -49.0 -51.7 -53.0 -58.3 -60.5 -61.2 -61.8 -62.7 -64.2 -67.0 -68.9 -70.1 -70.3 -72.2 -75.7 -77.0 -78.0 -80.5 -81.0
3037/3:IT -5.4 -5.3 -6.2 -5.6 9.4 8.6 1.4 10.4 16.1 14.1 22.0 32.6 26.3 16.3 12.9 11.0 12.2 13.8 12.2 9.7 9.3 10.3 8.6 6.3 8.1 11.4 13.3 9.6 4.2 2.8 3.5 7.5 9.7 6.9 3.8 3.6 7.5 10.2 7.1 5.0 6.5



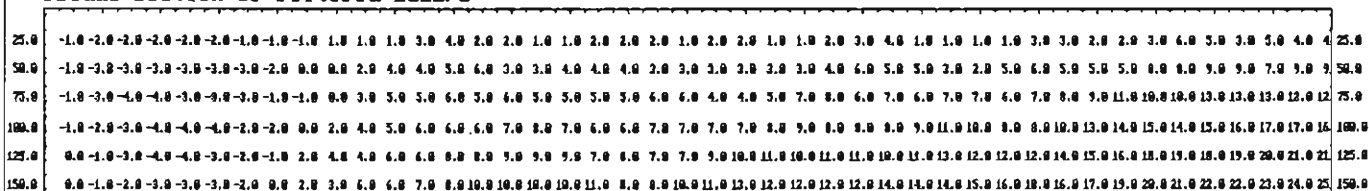
Pseudo-section of Filtered 112/37



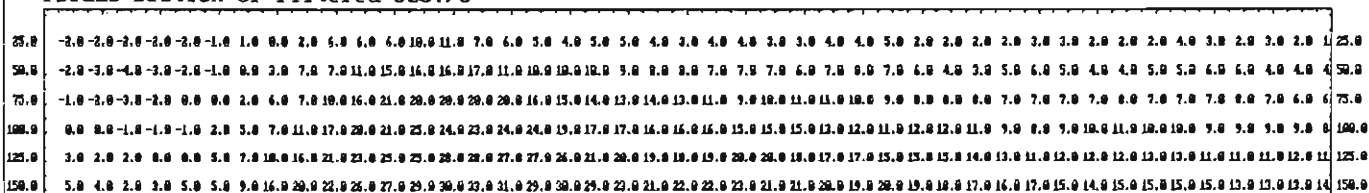
Pseudo-section of Filtered 337/37



Pseudo-section of Filtered 1012/3



Pseudo-section of Filtered 3037/3

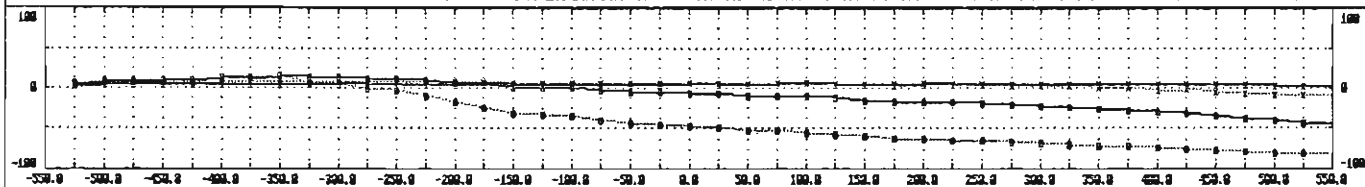


112/37 2.5 3.3 3.6 3.8 4.0 4.3 4.1 4.6 4.4 4.8 4.5 4.5 4.5 4.7 4.3 4.6 4.6 4.5 4.1 4.6 4.9 4.3 4.6 4.9 5.0 4.2 4.6 4.1 4.7 4.5 4.5 4.9 3.9 4.0 4.0 4.2 3.1 4.0 3.1 3.2 2.9 2.8 2.8
112/37:IT -1.6 -0.9 -0.9 -0.6 -0.4 -0.6 -0.3 -0.3 0.2 0.3 0.0 -0.2 0.0 0.3 -0.2 -0.2 0.6 0.4 -0.9 -0.5 0.6 -0.3 -1.0 0.3 1.1 0.5 0.0 -0.5 -0.2 0.7 1.1 0.6 -0.1 -0.3 0.7 1.1 0.2 0.3 1.9 2.3 1.2

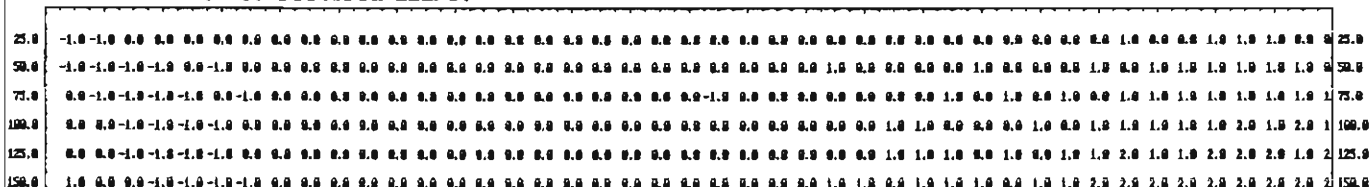
337/37 3.1 4.3 4.8 5.1 5.8 6.7 6.6 7.7 7.0 7.5 7.4 7.4 7.1 7.8 6.9 6.0 6.3 6.2 5.5 5.3 5.2 5.5 5.2 4.3 4.8 5.6 3.5 3.6 2.6 3.0 2.9 2.9 2.3 1.6 1.5 -0.3 0.1 -3.0 -2.3 -4.4 -6.0 -0.1 -7.0 -10.0
337/37:IT -2.5 -1.5 -2.6 -1.4 -1.8 -1.4 -0.2 -0.2 -0.3 0.4 0.7 0.6 1.2 1.6 0.4 0.6 1.7 1.1 0.0 -0.1 1.3 1.6 -0.9 0.0 1.3 2.9 1.5 0.3 -0.2 0.0 2.0 2.0 2.6 3.2 4.0 5.2 3.9 5.1 7.4 5.5 3.7

1012/3 4.3 6.7 7.4 9.4 9.9 12.0 12.3 14.0 12.2 12.5 10.9 10.9 0.4 6.2 1.9 0.9 0.7 -0.4 -2.7 -4.4 -5.5 -4.0 -7.6 -9.8 -9.7 -10.7 -12.9 -13.9 -17.1 -17.7 -10.2 -10.0 -21.0 -23.0 -24.7 -27.0 -27.4 -30.5 -31.0 -35.2 -38.0 -41.1 -42.5 -45.6
1012/3:IT -5.0 -4.0 -5.9 -4.0 -5.2 -2.7 2.4 3.6 2.9 4.1 7.1 9.1 10.0 0.7 4.4 4.6 7.4 6.8 4.4 3.7 5.9 5.9 3.0 4.1 7.5 8.5 6.9 3.0 2.2 3.9 7.0 7.9 7.7 6.7 6.2 7.1 0.3 11.7 12.9 11.4 10.0

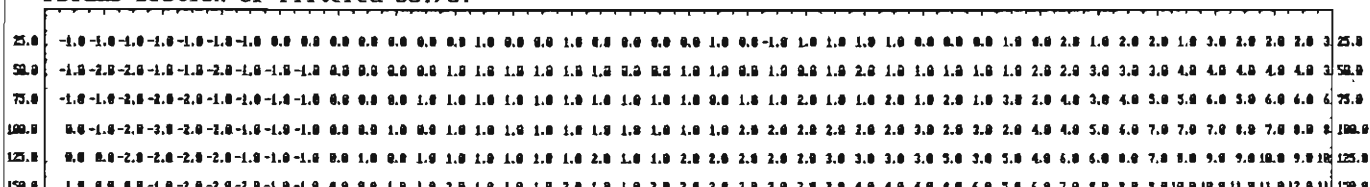
3037/3 5.8 9.2 0.9 0.6 9.0 11.9 11.7 13.9 6.0 3.2 -2.4 -3.4 -11.0 -10.1 -24.4 -30.7 -32.5 -35.4 -29.9 -43.1 -45.3 -46.7 -49.3 -32.4 -33.5 -35.4 -38.7 -60.1 -62.0 -63.6 -64.7 -65.2 -66.9 -68.0 -70.0 -72.2 -72.0 -74.0 -75.0 -77.5 -79.0 -80.4 -81.0 -82.6
3037/3:IT -2.5 -0.3 -4.2 -5.2 -3.9 3.7 16.4 19.1 15.0 15.2 23.3 28.1 26.0 28.7 13.0 12.3 14.9 12.9 9.0 7.6 9.7 9.9 7.2 0.2 9.5 0.0 7.6 5.4 3.5 3.0 5.0 6.7 6.5 5.4 3.8 4.8 6.5 7.5 6.9 4.9 4.2



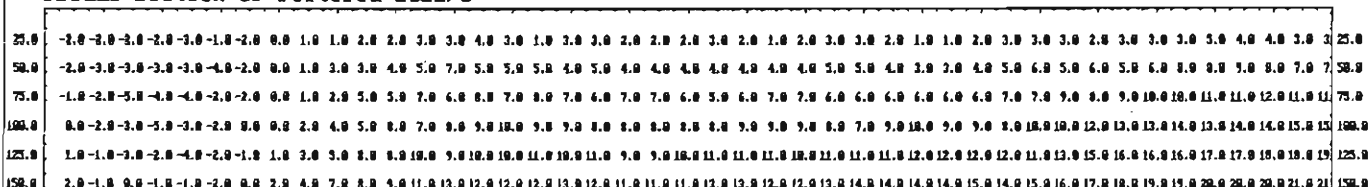
Pseudo-section of Filtered 112/37



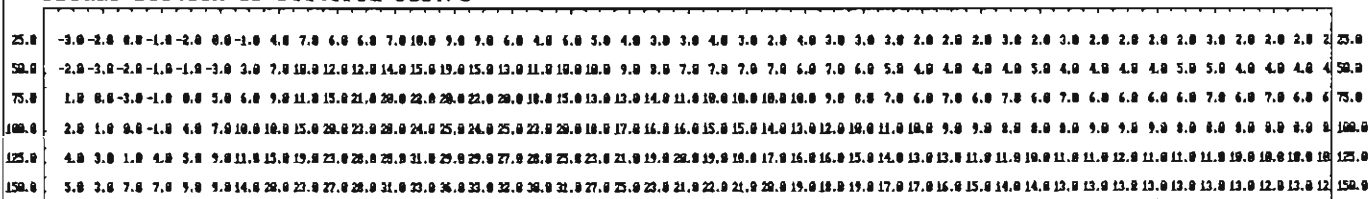
Pseudo-section of Filtered 337/37



Pseudo-section of Filtered 1012/3



Pseudo-section of Filtered 3037/3

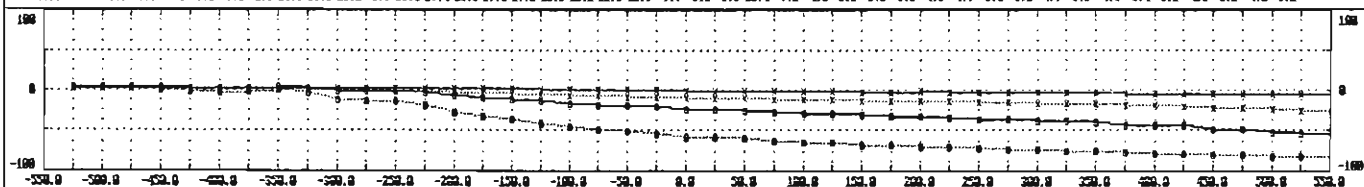


112/77 2.4 2.4 2.5 2.6 2.6 2.5 2.6 2.5 2.3 2.1 2.0 1.8 1.7 1.2 1.4 1.3 0.8 0.4 0.3 0.1 -0.2 -1.1 -1.0 -1.3 -1.5 -2.1 -1.5 -2.5 -2.5 -2.2 -2.7 -3.0 -3.1 -3.5 -3.4 -3.6 -4.3 -4.9 -5.0 -5.1 -5.3 -5.7 -6.5
112/77:17 -4.3 -4.3 0.0 2.1 2.0 2.3 2.7 0.7 0.6 0.6 0.5 0.5 0.2 2.5 1.5 1.6 0.8 0.9 1.3 1.3 0.9 0.7 1.3 2.8 0.4 1.4 0.7 -0.1 1.8 1.4 1.1 2.5 0.2 0.9 1.3 1.3 1.3 1.3 1.8 0.6 0.9 1.0

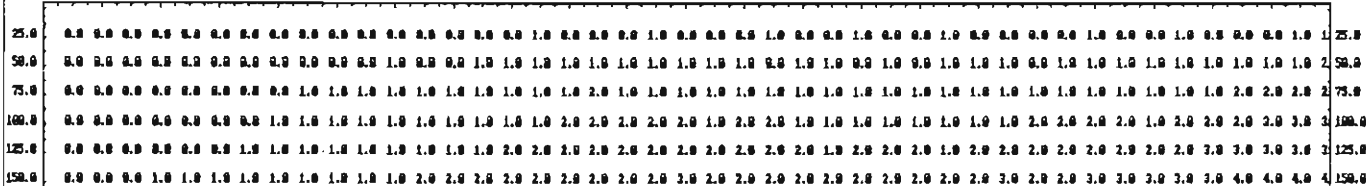
337/77 3.0 3.0 2.9 2.8 2.5 1.8 1.7 1.5 1.0 -0.1 -0.4 -1.1 -1.7 -3.4 -3.6 -4.7 -5.3 -6.4 -7.2 -7.9 -8.9 -10.2 -10.2 -10.7 -11.9 -12.6 -12.8 -13.3 -13.0 -13.7 -14.5 -15.3 -16.1 -17.3 -17.7 -18.2 -19.4 -20.2 -22.2 -23.0 -24.1 -25.5 -27.0
337/77:17 0.3 0.6 1.4 1.0 1.1 1.0 2.3 2.2 2.1 3.4 4.2 3.2 3.2 3.0 1.6 3.0 3.0 4.0 3.6 1.0 2.2 3.6 2.2 1.0 2.3 2.0 1.1 2.3 3.3 3.6 3.6 2.3 2.2 3.3 2.8 3.4 5.2 4.7 4.4 5.4

1012/7 3.3 3.7 3.6 3.2 2.7 2.1 2.7 3.7 2.3 -0.7 -1.5 -1.0 -3.3 -7.4 -9.5 -12.4 -14.0 -16.6 -18.5 -19.0 -21.0 -24.2 -24.9 -25.0 -28.3 -30.2 -29.9 -31.7 -33.1 -33.1 -35.1 -36.0 -37.2 -37.7 -39.4 -41.2 -43.5 -44.0 -44.5 -46.3 -45.5 -52.1 -54.1 -55.3
1012/7:17 0.2 1.4 2.0 1.1 -1.6 -1.4 4.6 0.4 5.1 2.9 7.4 11.4 11.2 9.5 0.7 0.7 7.7 6.5 7.7 7.5 4.7 5.0 7.0 6.0 3.1 4.7 4.6 3.4 4.9 5.0 3.8 2.9 5.7 7.6 6.9 2.0 5.3 9.3 0.0 0.4 7.0

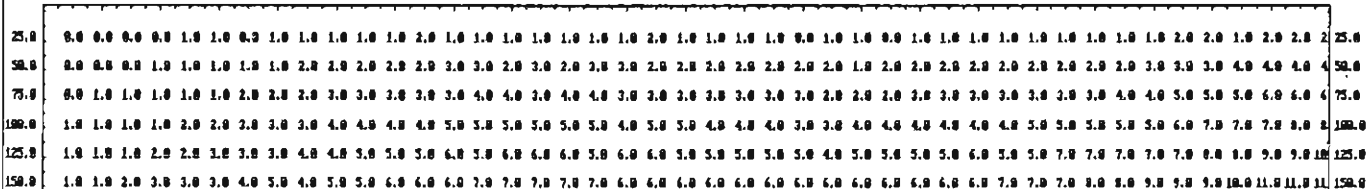
3037/7 3.0 3.3 3.2 0.0 -1.3 -3.3 -2.1 0.0 -3.3 -11.9 -14.0 -14.2 -18.5 -27.7 -32.4 -37.6 -41.5 -45.7 -50.7 -51.6 -54.6 -57.6 -58.3 -60.5 -63.7 -65.5 -65.8 -67.7 -69.4 -69.6 -71.1 -72.4 -73.0 -73.5 -75.0 -76.4 -77.7 -78.5 -79.0 -80.3 -81.7 -82.7 -83.5 -84.0
3037/7:17 2.9 7.3 0.3 5.2 -3.0 -2.9 13.8 23.3 13.1 6.5 10.0 27.4 23.0 19.0 17.2 15.3 13.1 11.0 11.9 9.7 6.6 0.3 10.4 7.1 4.3 5.0 5.5 3.6 4.5 4.7 3.0 3.1 4.9 5.6 4.8 2.4 3.1 4.5 3.1 4.2 3.1



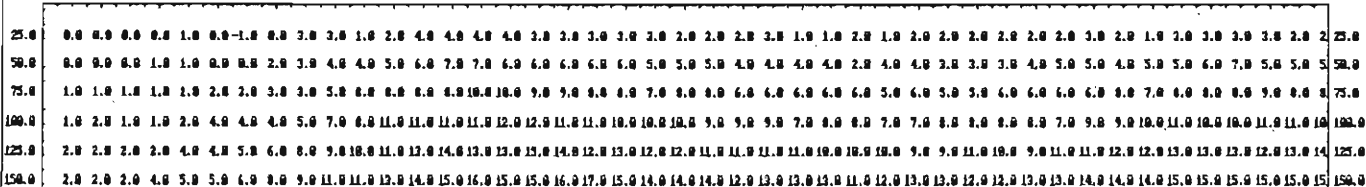
Pseudo-section of Filtered 112/37



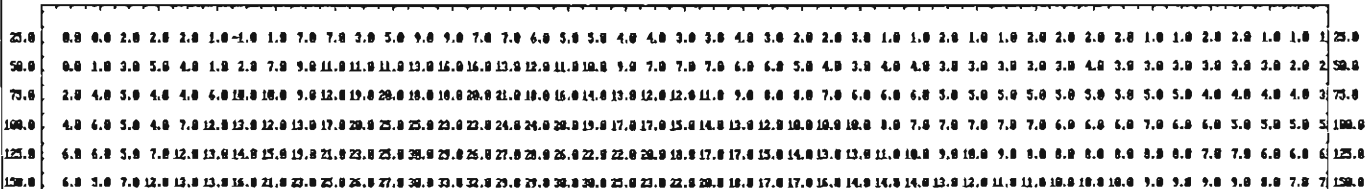
Pseudo-section of Filtered 337/37



Pseudo-section of Filtered 1012/3



Pseudo-section of Filtered 3037/3

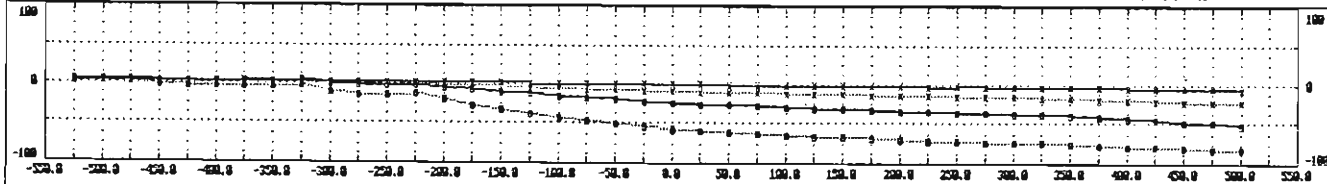


112/77 2.2 2.4 2.6 2.7 2.7 2.9 2.9 2.7 2.9 2.6 2.4 2.2 2.3 1.8 2.0 1.5 1.1 1.0 0.6 0.5 0.3 -0.3 -0.3 -0.7 -1.0 -1.3 -1.4 -1.3 -1.9 -1.7 -2.5 -2.2 -2.5 -3.1 -3.0 -3.5 -4.1 -4.3 -4.8 -5.2 -6.9
112/77:77 -0.7 -0.4 -0.2 -0.2 -0.1 0.2 0.2 0.5 0.8 0.5 0.3 0.7 0.4 1.2 1.4 1.0 1.0 0.9 1.2 1.3 0.5 1.1 1.3 1.0 0.4 0.5 0.9 1.0 1.1 0.5 0.9 1.4 0.9 1.5 1.5 1.5 1.2 0.9 1.6

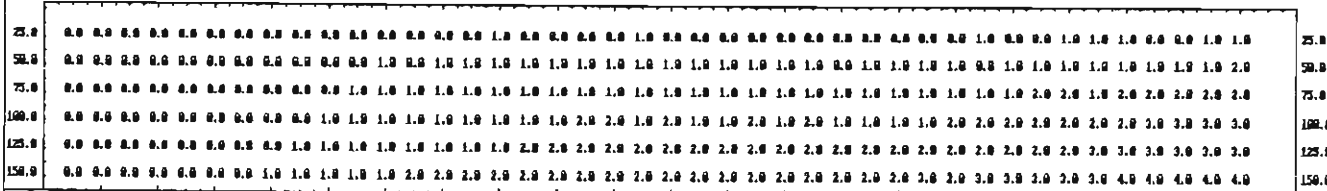
337/77 2.9 2.9 3.0 2.8 2.7 2.7 2.4 2.8 2.0 1.0 0.3 -0.2 -0.2 -1.5 -1.9 -3.2 -4.3 -5.2 -6.0 -7.4 -8.1 -9.3 -9.8 -10.3 -10.6 -11.4 -12.1 -12.6 -13.4 -14.1 -14.3 -15.2 -15.5 -16.2 -16.8 -17.3 -18.5 -18.3 -20.7 -22.2 -22.6 -22.8
337/77:77 0.0 0.4 0.4 0.4 1.0 1.1 1.4 2.7 2.9 1.7 1.0 2.0 3.4 4.1 4.4 3.7 3.9 4.3 4.0 3.6 2.7 1.0 1.9 2.6 2.7 2.5 2.0 2.4 2.0 2.3 2.2 2.3 2.4 2.0 2.7 3.2 6.1 5.0 2.5

1012/3 3.2 3.5 3.4 2.8 2.4 2.4 2.3 2.0 3.2 0.0 -1.7 -1.5 -0.8 -4.2 -6.0 -10.1 -12.5 -15.2 -17.2 -19.0 -22.3 -24.1 -25.0 -26.7 -28.2 -29.8 -31.1 -31.6 -33.0 -34.4 -35.9 -36.6 -37.2 -38.0 -39.1 -40.5 -42.0 -44.3 -45.5 -46.3 -50.0 -52.2
1012/3:77 0.5 1.7 1.4 0.5 0.5 -0.5 1.1 6.9 6.4 0.6 1.0 0.7 11.9 11.6 10.0 9.0 9.3 9.4 9.1 9.1 6.4 5.0 5.5 6.0 4.7 3.7 4.7 5.6 5.0 3.6 3.7 4.2 3.5 4.5 6.7 7.3 7.5 0.5 0.4

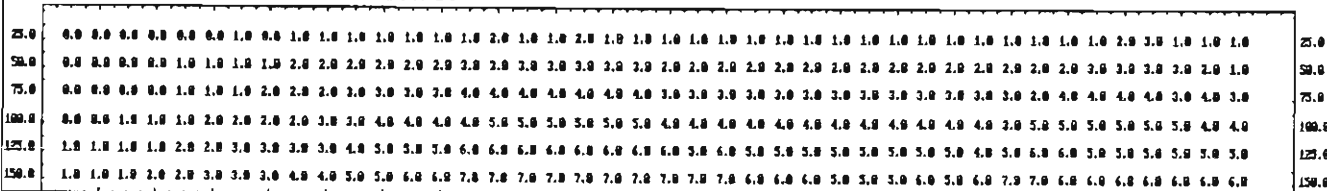
3037/3 3.0 3.2 1.4 -1.1 -2.6 -3.2 -3.8 -4.1 -1.4 -10.4 -14.4 -14.0 -12.3 -19.9 -27.4 -33.7 -38.4 -43.1 -47.2 -51.7 -54.8 -58.3 -60.4 -62.0 -63.8 -65.3 -66.6 -67.4 -69.2 -70.9 -72.3 -72.3 -73.3 -74.4 -74.6 -75.6 -77.1 -78.9 -79.9 -81.5 -82.7 -83.1
3037/3:77 5.9 0.3 6.1 3.3 2.1 -1.5 3.9 19.3 16.6 2.0 4.3 20.5 20.4 25.0 20.9 19.3 16.5 15.9 14.2 12.2 9.3 7.1 6.7 6.1 4.9 4.7 6.0 6.3 4.6 2.5 3.1 3.4 2.5 3.7 5.7 5.6 5.1 5.9 4.0



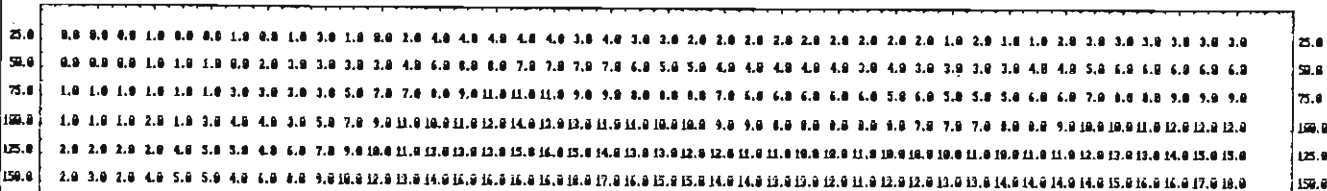
Pseudo-section of Filtered 112/77



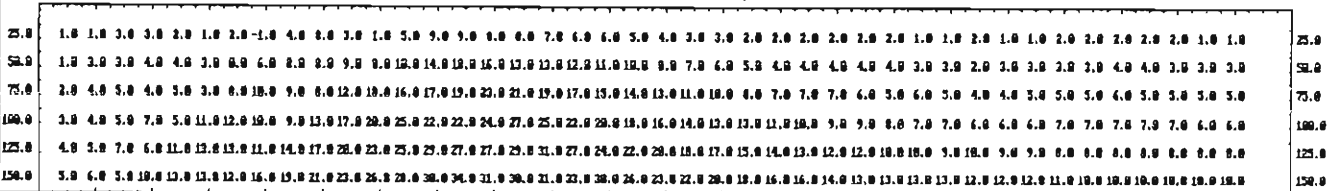
Pseudo-section of Filtered 337/77



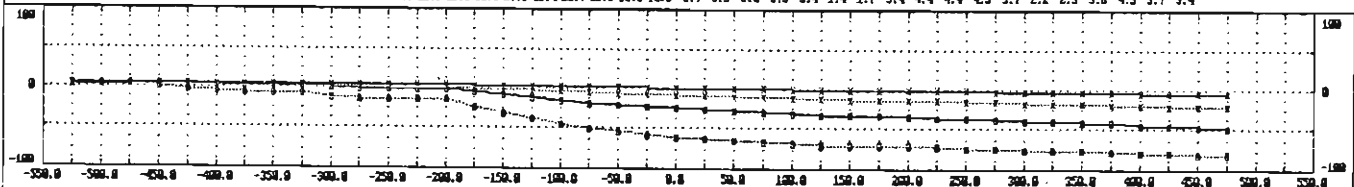
Pseudo-section of Filtered 1012/3



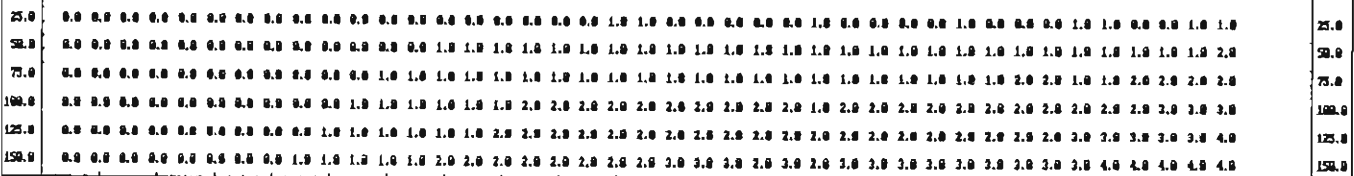
Pseudo-section of Filtered 3037/3



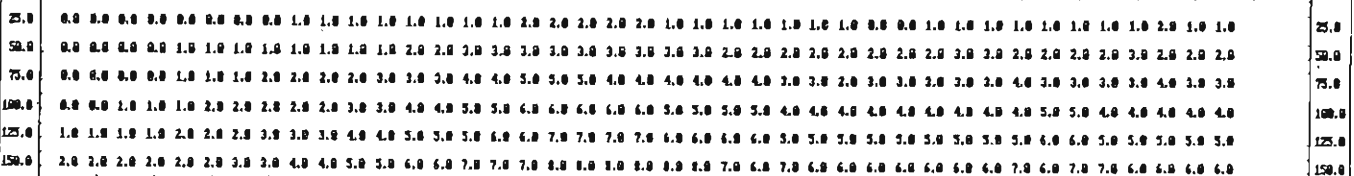
112/77 2.6 2.7 2.8 2.1 3.2 3.4 3.3 3.3 3.4 3.2 3.1 3.0 3.0 2.9 2.6 2.3 2.1 1.7 1.6 1.2 2.5 2.4 2.1 -0.2 -0.5 -0.7 -0.3 -1.6 -1.5 -1.3 -1.7 -2.3 -2.5 -3.0 -3.1 -3.5 -3.9 -4.2 -4.2 -4.5 -5.3
112/77:IT -0.3 -0.5 -0.5 -0.4 0.0 0.0 0.0 0.4 0.5 0.3 0.2 0.5 1.0 1.1 1.1 1.1 1.0 1.3 1.0 1.3 1.2 1.2 1.1 0.8 1.2 1.6 0.9 0.4 0.7 1.2 1.5 1.3 1.1 1.3 1.6 1.2 0.6 1.4
337/37 3.5 3.8 4.0 4.0 3.7 3.5 3.1 2.9 2.8 2.1 1.5 1.3 1.0 0.5 -0.7 -1.3 -2.7 -4.1 -5.1 -6.1 -7.4 -8.3 -9.0 -10.1 -10.5 -11.4 -12.0 -13.0 -13.5 -13.7 -13.7 -15.0 -15.6 -16.9 -17.2 -17.4 -18.7 -19.5 -20.3 -21.0 -21.7
337/37:IT -0.7 0.1 0.0 1.1 1.2 0.9 1.1 2.1 2.1 1.3 1.3 2.5 3.8 4.8 5.2 4.4 4.3 4.5 3.8 3.4 3.7 3.2 2.4 2.7 3.1 1.9 0.6 1.0 2.5 3.0 3.5 2.1 2.0 3.6 3.7 3.9 3.7
1012/3 2.7 4.2 4.5 4.8 3.0 2.2 1.9 1.6 1.4 -0.5 -1.1 -1.0 -0.9 -1.2 -1.4 -0.6 -12.0 -15.6 -18.4 -20.5 -22.4 -25.3 -26.9 -28.4 -30.5 -32.0 -32.4 -33.6 -33.9 -35.1 -36.0 -37.5 -38.6 -40.2 -40.0 -41.7 -42.0 -44.0 -46.3 -47.7 -49.3
1012/3:IT -0.6 1.7 3.3 3.0 1.0 1.0 2.5 4.6 3.0 0.3 0.0 5.1 12.2 12.6 13.2 13.4 11.3 9.9 9.0 8.3 6.6 6.7 7.2 5.5 3.5 3.1 3.0 3.6 4.5 5.0 5.3 4.1 2.9 4.3 5.9 6.6 6.4 6.1
3037/3 3.3 3.4 2.9 0.6 -2.5 -5.4 -6.4 -7.0 -7.7 -12.7 -14.0 -13.8 -13.4 -13.0 -25.3 -21.7 -19.0 -0.5 -5.0 -6.5 -6.0 -3.0 -2.7 -43.0 -44.9 -67.1 -68.2 -69.5 -69.8 -69.9 -71.1 -72.0 -73.4 -74.1 -75.6 -75.6 -76.3 -77.2 -78.5 -79.3 -80.1 -81.1
3037/3:IT 3.2 5.6 11.8 9.5 5.1 2.9 7.0 12.0 7.4 0.5 -0.6 11.9 29.8 31.6 27.5 25.4 20.7 16.8 13.0 10.0 8.9 8.3 8.0 6.3 3.4 1.4 1.7 3.4 4.4 4.4 4.3 3.7 2.2 2.3 3.0 4.3 3.7 3.4



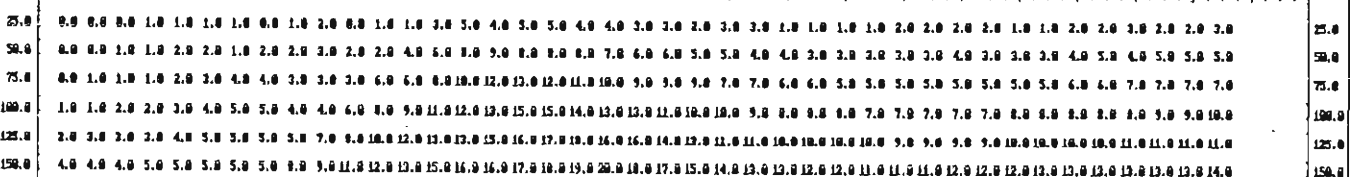
Pseudo-section of Filtered 112/37



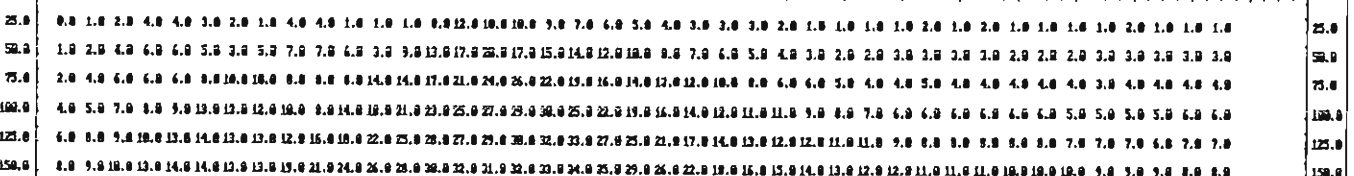
Pseudo-section of Filtered 337/37



Pseudo-section of Filtered 1012/3



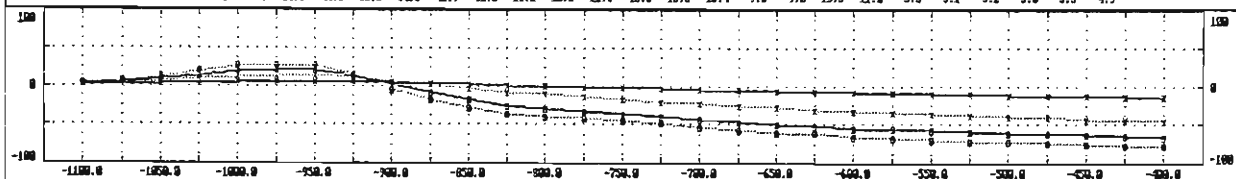
Pseudo-section of Filtered 3037/3



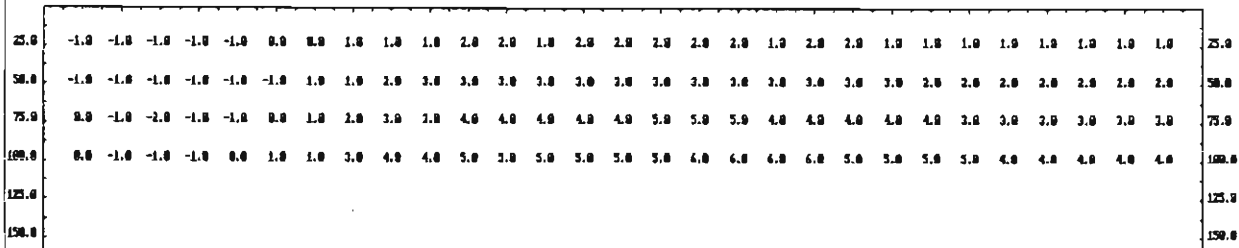
LINE 7700E

DATE 23 DEC, 1986 OPERATOR N.M. LOOP#6 LOOP 600x300m

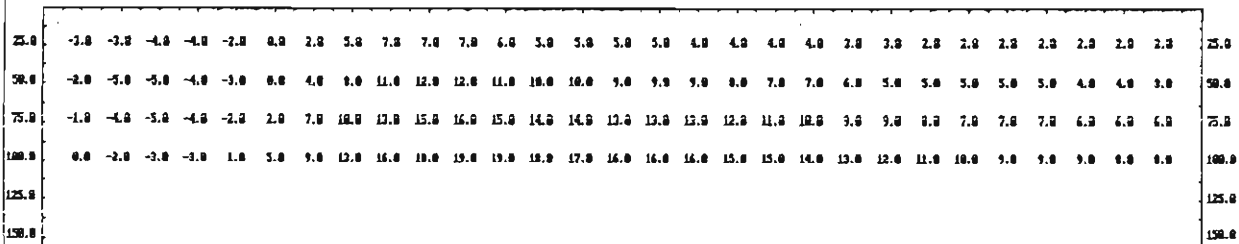
112/77	2.1	2.4	3.2	4.0	4.9	5.1	5.5	5.1	4.1	3.8	2.1	0.9	9.1	-1.8	-2.0	-3.3	-4.3	-5.3	-6.4	-7.3	-8.7	-9.4	-10.2	-10.9	-11.5	-12.3	-12.7	-13.2	-14.0
112/77:77		-2.7	-3.3	-2.8	-1.7	-0.6	1.4	3.3	4.1	4.1	4.1	3.9	0.0	4.4	4.6	4.3	4.3	3.9	4.1	4.4	3.6	3.8	2.8	2.7	2.6	2.1	2.2		
337/77	2.8	4.7	7.2	10.0	12.0	13.0	13.9	11.2	6.3	1.2	-3.0	-8.9	-11.1	-14.1	-17.1	-20.2	-22.4	-25.0	-28.6	-31.2	-33.5	-35.2	-36.0	-38.1	-40.0	-41.2	-43.0	-44.2	-45.1
337/77:77		-9.7	-10.9	-9.4	-4.9	1.5	10.2	17.4	19.3	18.5	17.3	14.2	12.1	12.2	12.5	11.8	10.7	10.4	10.3	8.9	7.3	6.2	6.1	6.3	6.1	6.8	5.1		
1062/2	9.0	6.3	10.0	15.3	10.0	4.1	20.3	19.1	1.4	-4.1	-14.7	-26.4	-30.0	-32.6	-36.0	-41.8	-47.0	-50.3	-53.5	-57.4	-61.0	-60.0	-59.3	-58.8	-57.0	-53.9	-49.8	-46.0	
1062/2:77		-16.4	-18.5	-15.9	-21.0	7.6	26.6	40.9	48.3	34.4	29.1	21.0	15.6	14.0	14.9	13.8	12.1	11.1	10.5	9.5	7.1	5.0	4.0	5.0	6.1	5.0	5.5		
3817/3	3.2	7.3	12.9	20.2	27.1	27.5	26.4	13.7	-4.4	-10.0	-27.3	-37.0	-39.9	-42.6	-44.0	-49.5	-54.4	-58.4	-60.9	-61.5	-64.0	-69.1	-70.2	-71.5	-72.9	-74.0	-75.4	-76.8	-77.5
3817/3:77		-22.6	-27.1	-21.5	-4.6	14.3	44.6	62.5	54.6	41.9	31.6	19.2	18.5	11.8	16.3	10.3	13.4	9.4	9.0	13.5	11.9	5.8	5.1	5.2	5.0	5.3	4.9		



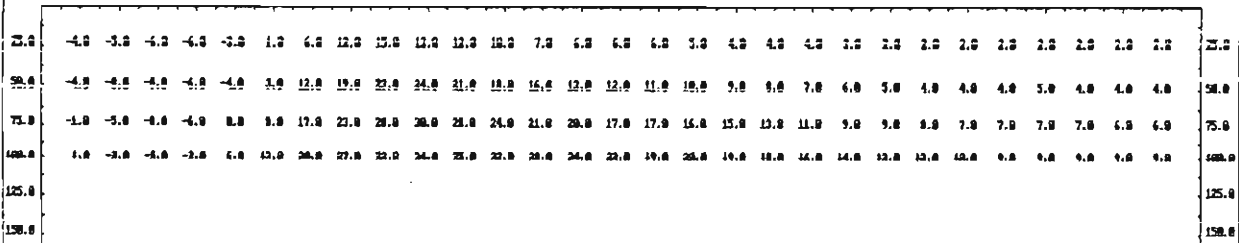
Pseudo-section of Filtered 112/37



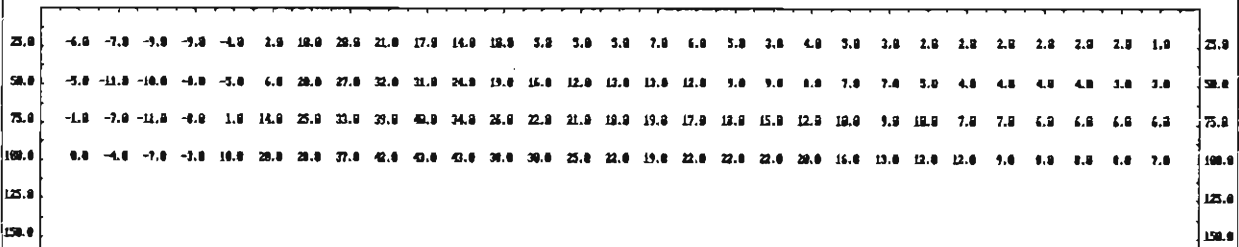
Pseudo-section of Filtered 337/37



Pseudo-section of Filtered 1012/3



Pseudo-section of Filtered 3037/3



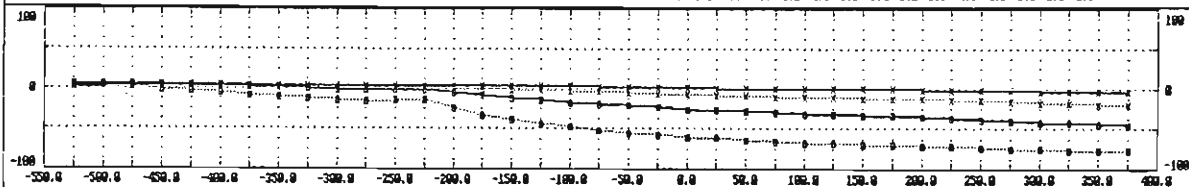
DATE 11/6/86 OPERATOR D.K.W.

112/37 2.8 3.8 3.3 3.5 3.7 3.9 3.9 3.9 3.7 3.8 3.7 3.6 3.5 3.3 3.5 3.2 3.8 2.9 2.6 2.3 1.6 1.2 1.8 0.6 0.2 0.3 0.2 -0.3 -0.6 -1.0 -1.5 -1.6 -2.2 -3.0 -3.2 -2.8 -3.6
112/37:17 -1.0 -0.9 -0.8 -0.6 -0.2 0.2 0.3 0.1 0.2 0.4 0.5 0.3 0.0 0.5 0.9 0.8 1.0 1.6 2.1 1.7 1.2 1.4 1.1 0.3 0.6 1.4 1.3 1.6 1.5 1.3 2.1 2.4 0.8 0.2

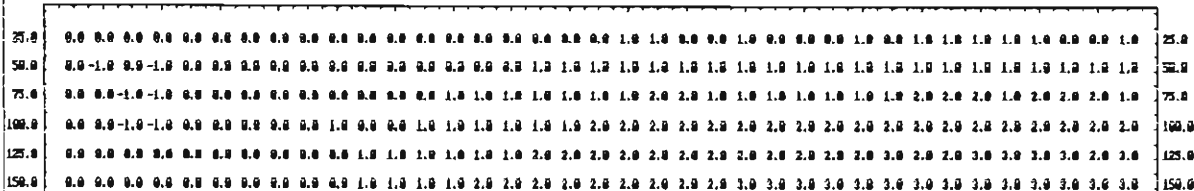
337/37 4.8 4.6 4.8 4.8 4.7 4.7 4.4 3.9 3.1 2.9 2.5 2.0 1.3 0.5 -0.2 -1.3 -2.3 -3.0 -4.0 -5.2 -6.3 -7.4 -7.8 -8.8 -9.6 -10.0 -10.7 -11.5 -12.0 -12.7 -13.0 -14.5 -15.0 -17.5 -18.0 -19.4
337/37:17 -1.0 -0.1 0.2 0.4 1.1 2.1 2.5 1.6 1.3 1.4 0.2 0.9 0.8 0.9 0.8 0.4 0.3 0.7 0.9 0.2 0.8 0.3 0.6 0.3 2.6 2.0 2.3 0.8 3.6 3.8 3.8 3.8 3.8 3.4 2.6

1012/3 4.5 5.6 5.2 4.5 3.6 3.1 2.2 1.2 -0.1 -0.8 -1.2 -1.2 -1.1 -3.7 -3.0 -12.0 -14.6 -16.7 -19.3 -21.0 -23.5 -25.7 -26.1 -28.0 -29.0 -31.0 -32.3 -33.0 -34.0 -35.0 -36.3 -38.0 -40.0 -41.7 -42.8 -44.4 -45.2
1012/3:17 0.8 2.7 3.0 2.8 3.3 4.2 4.3 3.1 1.5 0.3 4.4 12.4 14.2 11.9 10.3 9.4 9.0 9.3 8.1 6.5 4.9 6.0 6.7 5.5 4.5 3.7 3.7 4.3 5.3 6.7 7.4 6.5 5.5 5.1

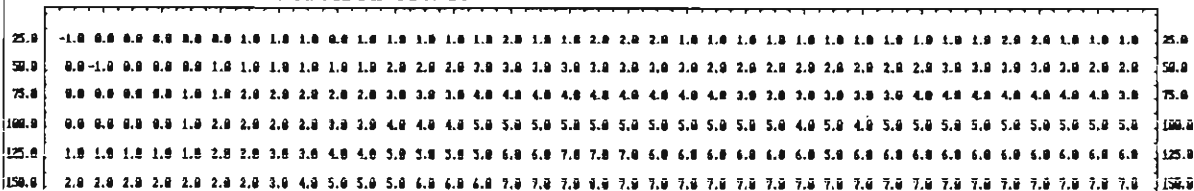
3037/3 5.7 5.1 2.3 -1.1 -4.0 -5.9 -4.1 -10.4 -12.5 -14.6 -15.3 -14.6 -14.3 -24.9 -33.0 -37.1 -44.5 -48.0 -53.0 -56.9 -58.9 -61.4 -62.2 -64.3 -66.5 -68.2 -69.2 -70.2 -71.0 -71.6 -72.6 -73.9 -75.1 -76.2 -76.6 -77.2 -77.2
3037/3:17 9.5 12.5 11.1 8.9 8.6 8.9 8.5 7.8 2.8 -1.8 9.3 25.8 23.2 26.8 28.1 17.1 17.4 14.7 19.3 7.9 5.8 7.7 7.7 6.1 4.5 3.6 3.4 3.2 3.9 4.8 4.8 3.8 2.3 1.6



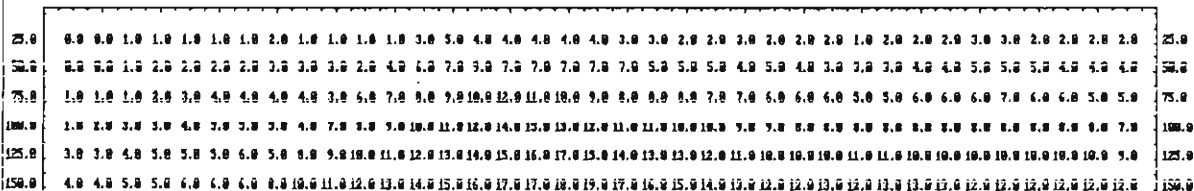
Pseudo-section of Filtered 112/37



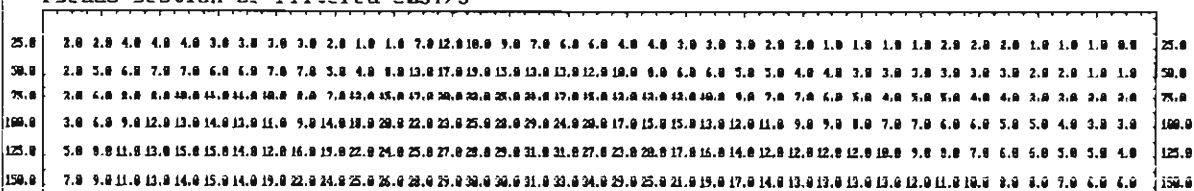
Pseudo-section of Filtered 337/37



Pseudo-section of Filtered 1012/3



Pseudo-section of Filtered 3037/3



TWIN GRID - LARGE LOOP EM

LINE 7800E

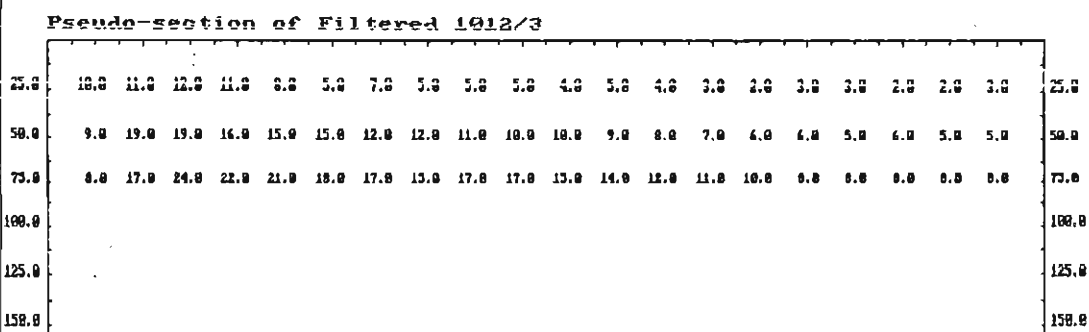
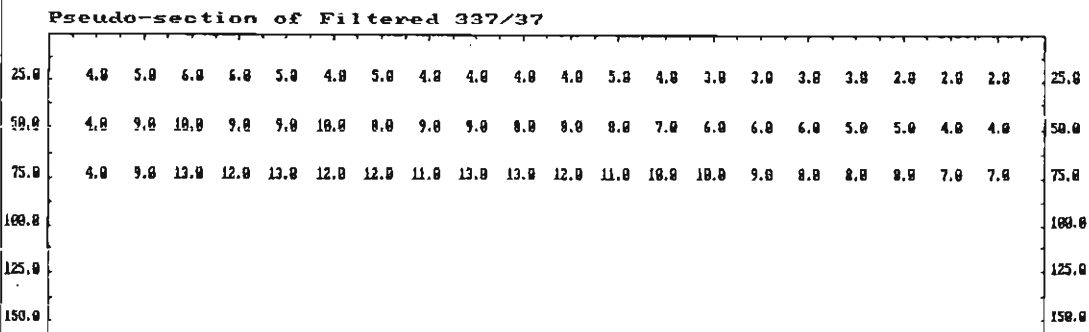
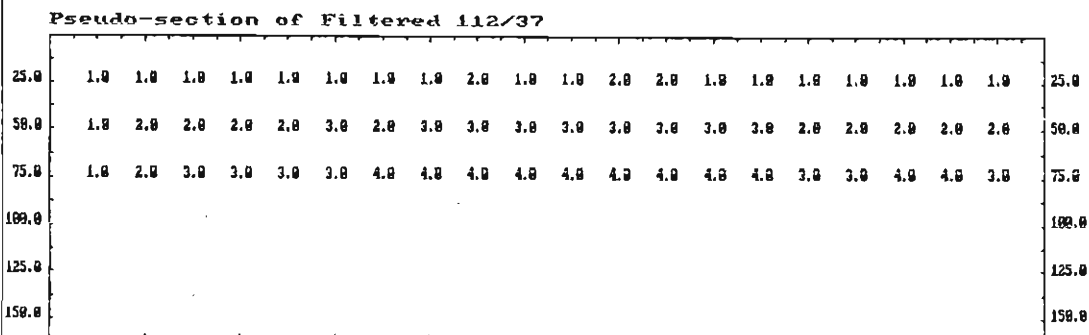
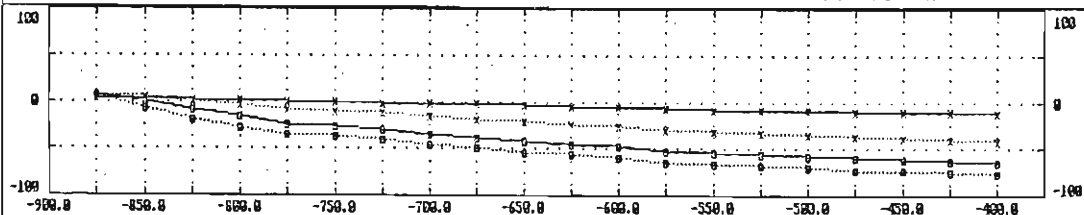
DATE 05 DEC. 1986 OPERATOR H.M. LOOP#6 LOOP 600x300m

112/37 4.2 3.5 2.8 1.9 0.7 0.2 -0.8 -1.5 -2.4 -3.8 -4.2 -5.4 -6.9 -7.8 -8.5 -9.2 -10.3 -10.7 -11.1 -12.3
112/37:FF 3.0 2.7 3.8 3.2 3.2 3.3 3.9 4.1 3.4 4.3 5.1 4.0 3.8 3.2 3.3 2.3 2.4

337/37 8.1 4.9 0.7 -3.1 -7.9 -9.8 -12.5 -15.9 -18.3 -21.5 -23.8 -26.7 -30.2 -32.0 -33.7 -35.3 -37.6 -39.3 -40.3 -41.9
337/37:FF 15.4 16.6 15.3 11.3 18.7 11.9 11.4 11.1 10.7 11.6 11.7 8.8 6.8 7.2 7.9 6.7 5.3

1012/3 8.1 8.1 -8.7 -16.1 -24.1 -26.5 -30.5 -35.2 -38.1 -42.2 -45.0 -48.1 -52.6 -54.5 -56.1 -57.2 -60.1 -61.5 -62.5 -64.6
1012/3:FF 33.0 31.6 25.0 16.8 15.1 16.3 14.6 13.9 12.8 13.5 14.0 9.9 6.2 6.7 8.3 6.7 5.5

3037/3 7.9 -6.3 -19.4 -27.9 -35.8 -37.5 -40.9 -45.9 -49.7 -54.3 -56.6 -58.7 -64.2 -66.5 -68.3 -69.8 -73.8 -74.4 -75.5 -76.8
3037/3:FF 42.9 38.8 25.9 14.7 13.5 17.2 17.2 19.3 11.5 12.2 15.2 11.7 7.4 9.0 9.3 7.1 4.9



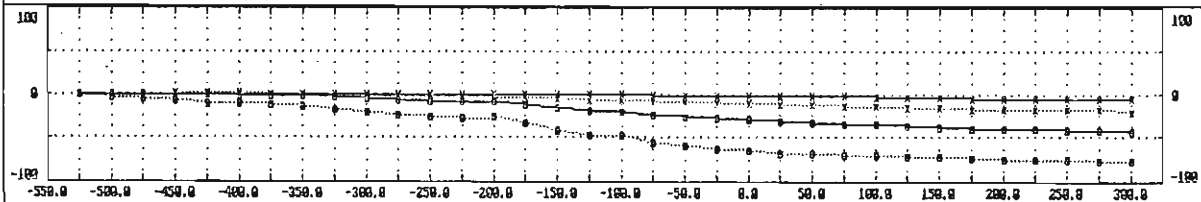
DATE 11/06/86 OPERATOR D.M.W.

112/37 -0.6-0.4 0.0 0.4 0.5 0.0 0.0 0.9 0.7 1.0 0.6 0.7 0.5 0.4 0.2 0.1 -0.2-0.5 -0.8 -1.0 -1.0 -1.0 -2.2 -2.3 -2.7 -3.2 -3.6 -4.0 -4.5 -4.7 -4.4 -5.3 -5.5 -5.5
112/37:FF -1.4-1.3 -0.9 -0.7 -0.4 0.0 0.0 0.0 0.4 0.4 0.4 0.6 0.6 0.7 1.0 1.2 1.1 1.5 1.8 1.2 0.9 0.6 1.0 2.2 2.1 1.7 1.6 0.8 0.7 1.5 1.1

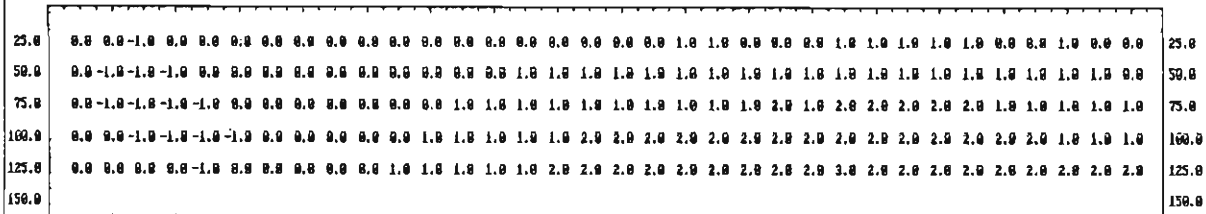
337/37 0.0 0.5 1.0 1.4 1.3 1.4 1.0 0.8 -0.1 -0.7 -1.3 -1.6 -2.3 -2.8 -3.7 -4.7 -6.1 -7.0 -8.1 -9.0-10.5-10.6-11.4-12.2-13.4-14.1-14.8-15.7-16.8-17.6-17.8-18.2-17.4-20.4
337/37:FF -1.9-1.2-0.3 0.2 0.9 1.7 2.6 2.7 2.1 1.9 2.2 2.6 3.3 4.5 4.7 4.5 4.2 4.2 3.8 2.5 2.5 2.6 3.9 3.3 3.8 3.4 3.9 2.9 1.6 0.4 2.0

1012/3 0.2 0.6 0.7 0.4 0.0-0.7 -1.4 -2.2 -3.0 -5.3 -7.2 -8.4 -9.0 -9.6-11.3-15.3-19.7-21.1-23.6-26.1-28.6-29.8-31.1-33.0-34.2-35.4-36.7-38.0-39.4-40.3-40.8-42.2-41.3-44.5
1012/3:FF -0.3 0.9 1.0 2.5 2.9 3.9 5.5 6.5 6.5 4.9 2.0 2.5 9.0 14.1 13.2 10.7 9.9 10.0 8.7 6.2 5.7 6.3 5.5 4.9 5.1 5.5 5.2 3.5 3.1 2.4 2.8

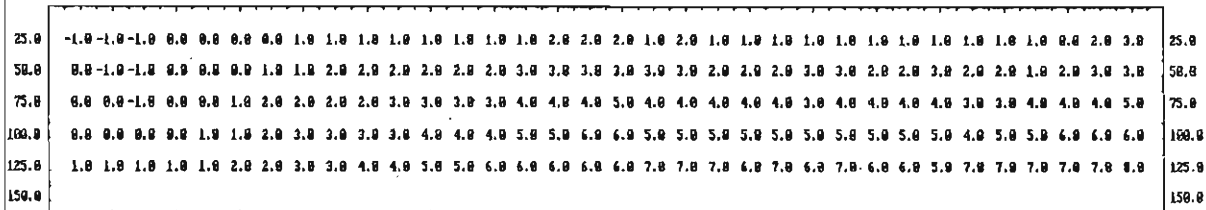
3037/3 -0.5 -1.4 -5.6 -7.7 -9.6-11.1-12.9-14.4-17.2-20.5-24.5-26.8-27.6-26.1-32.9-41.3-47.6-47.6-56.6-60.1-63.5-65.2-67.7-69.0-70.5-71.2-72.9-72.9-73.5-74.8-75.0-75.6-76.7-77.0
3037/3:FF 9.4 8.3 7.4 6.7 6.6 7.6 10.4 13.4 13.6 9.4 2.4 4.6 20.5 29.9 21.8 15.3 21.5 19.4 12.0 9.3 8.0 6.6 5.0 4.6 4.1 2.3 2.5 3.4 2.3 2.5 3.1



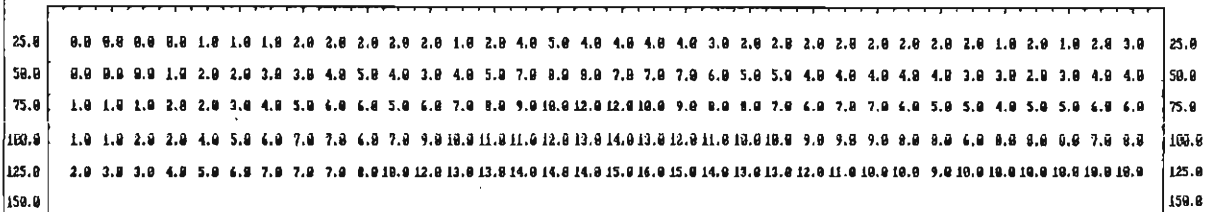
Pseudo-section of Filtered 112/37



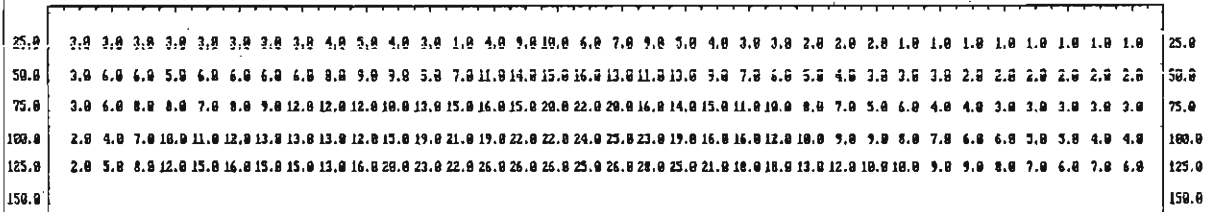
Pseudo-section of Filtered 337/37



Pseudo-section of Filtered 1012/3



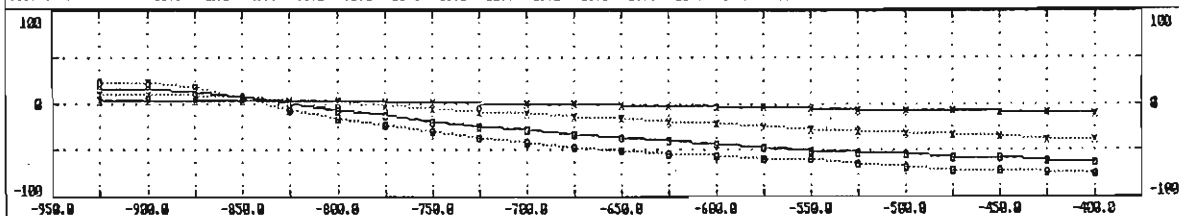
Pseudo-section of Filtered 3037/3



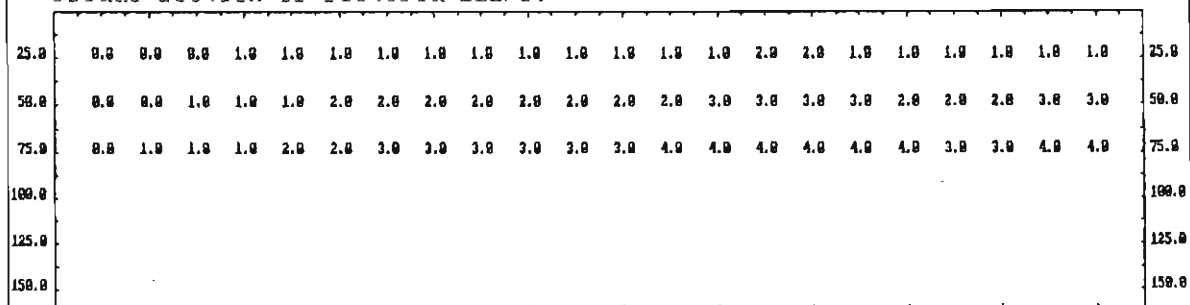
TWIN GRID - LARGE LOOP EM LINE 7900E

DATE 05 DEC. 1986 OPERATION N.M. LOOP#6 LOOP 600x500m

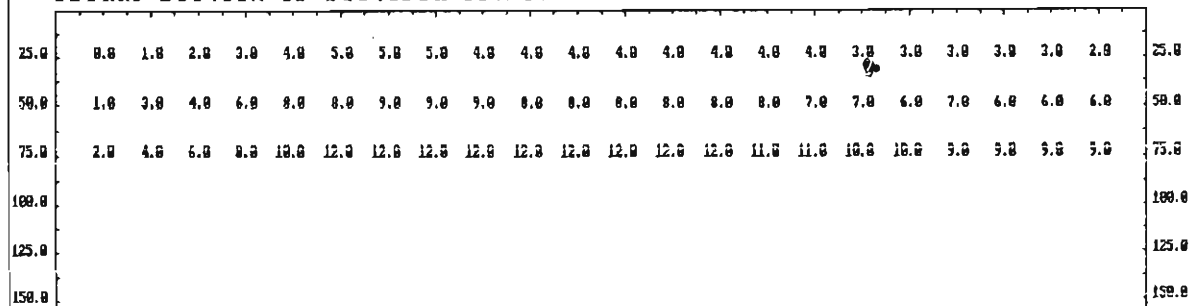
112/37	4.2	4.5	4.4	4.2	3.7	3.1	2.3	1.8	1.1	0.5	-0.3	-1.0	-1.8	-2.5	-3.7	-5.2	-6.8	-6.7	-7.1	-8.0	-8.9	-9.7
112/37:FF		0.1	1.8	1.8	2.5	2.7	2.5	2.5	2.7	2.9	3.0	3.0	3.4	4.6	5.8	3.8	2.6	2.4	3.1	3.5		
337/37	10.1	10.5	9.5	7.5	4.6	1.5	-1.6	-4.8	-7.9	-10.6	-13.2	-15.9	-18.9	-21.3	-24.3	-27.2	-29.1	-31.3	-33.2	-35.3	-37.9	-39.1
337/37:FF		3.6	7.9	10.9	12.2	12.5	12.6	12.1	11.1	10.6	11.9	11.1	10.2	11.3	10.7	8.9	8.2	8.1	8.7	8.5		
1012/3	16.0	16.8	13.1	7.4	0.3	-4.3	-10.6	-18.0	-24.3	-30.6	-32.7	-34.3	-40.2	-43.6	-47.6	-50.8	-53.8	-56.8	-57.8	-60.6	-61.8	-63.0
1012/3:FF		11.0	21.0	26.7	26.7	25.3	24.2	21.4	18.2	16.3	15.3	14.7	14.5	14.6	12.1	9.2	9.4	8.4	7.6	8.6		
3037/3	23.5	23.2	17.9	6.2	-4.2	-15.4	-22.7	-29.9	-36.4	-41.4	-46.6	-50.4	-53.8	-56.7	-60.2	-60.5	-65.2	-69.0	-71.4	-72.7	-74.7	-76.4
3037/3:FF		22.6	41.1	45.7	38.1	31.8	28.2	25.2	21.7	19.2	16.2	13.5	12.7	10.2	8.8	13.5	14.7	9.9	7.8	7.8		



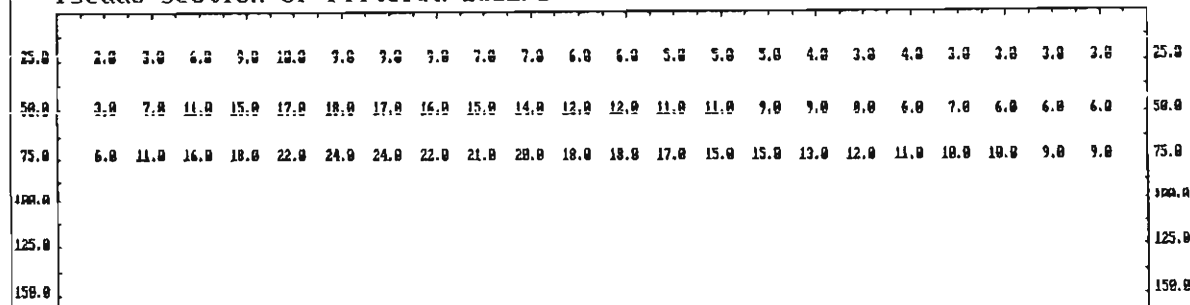
Pseudo-section of Filtered 112/37



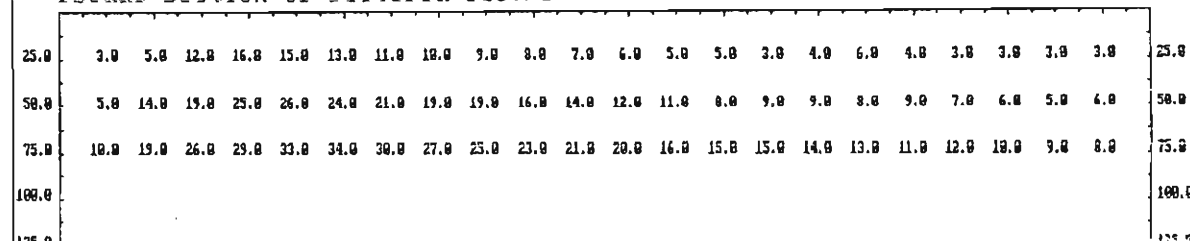
Pseudo-section of Filtered 337/37



Pseudo-section of Filtered 1012/3



Pseudo-section of Filtered 3037/3



[illegible]

Pseudo-section of Filtered 1012/3																																													
25.0	-3.0	-3.0	-4.0	-4.0	-3.0	-1.0	3.0	7.0	9.0	10.0	10.0	9.0	7.0	7.0	7.0	6.0	5.0	5.0	4.0	5.0	5.0	3.0	3.0	3.0	3.0	2.0	2.0	2.0	2.0	2.0	1.0	1.0	1.0	0.0	0.0	0.0	0.0	1.0	1.0	0.0	0.0	-7.0	-61.0	25.0	
50.0	-2.0	-5.0	-4.0	-5.0	-3.0	0.0	5.0	11.0	15.0	17.0	17.0	16.0	15.0	14.0	13.0	12.0	10.0	9.0	9.0	9.0	8.0	7.0	6.0	6.0	6.0	5.0	4.0	4.0	4.0	4.0	3.0	3.0	2.0	2.0	1.0	1.0	1.0	1.0	-4.0	-13.0	-11.0	-13.0	-66.0	-94.0	50.0
75.0	0.0	-3.0	-5.0	-4.0	-1.0	4.0	9.0	14.0	19.0	22.0	22.0	22.0	21.0	19.0	18.0	17.0	16.0	15.0	13.0	12.0	12.0	11.0	10.0	9.0	8.0	8.0	7.0	7.0	6.0	5.0	5.0	5.0	4.0	3.0	-7.0	-12.0	-17.0	-16.0	-17.0	-19.0	-72.0	-80.0	-28.0	75.0	
100.0	1.0	-2.0	-3.0	-2.0	2.0	7.0	12.0	19.0	22.0	25.0	28.0	28.0	26.0	24.0	22.0	21.0	20.0	20.0	19.0	18.0	17.0	16.0	15.0	14.0	12.0	10.0	10.0	10.0	9.0	8.0	8.0	7.0	-3.0	-4.0	-14.0	-19.0	-19.0	-21.0	-22.0	-25.0	-79.0	-85.0	-123.0	-61.0	100.0
125.0	2.0	0.0	1.0	2.0	4.0	11.0	16.0	24.0	24.0	28.0	31.0	32.0	30.0	27.0	26.0	24.0	22.0	21.0	20.0	20.0	19.0	18.0	16.0	15.0	12.0	12.0	12.0	2.0	-4.0	-10.0	-16.0	-21.0	-21.0	-24.0	-26.0	-28.0	-30.0	-44.0	-42.0	-82.0	-87.0	-84.0	125.0		
150.0	4.0	4.0	6.0	9.0	12.0	14.0	18.0	22.0	25.0	29.0	32.0	36.0	37.0	36.0	35.0	32.0	29.0	25.0	24.0	21.0	22.0	21.0	20.0	20.0	20.0	19.0	8.0	2.0	-4.0	-10.0	-16.0	-22.0	-22.0	-25.0	-28.0	-30.0	-32.0	-35.0	-49.0	-47.0	-85.0	-82.0	150.0		

[illegible]

TWIN GRID - LARGE LOOP EM

LINE L81E

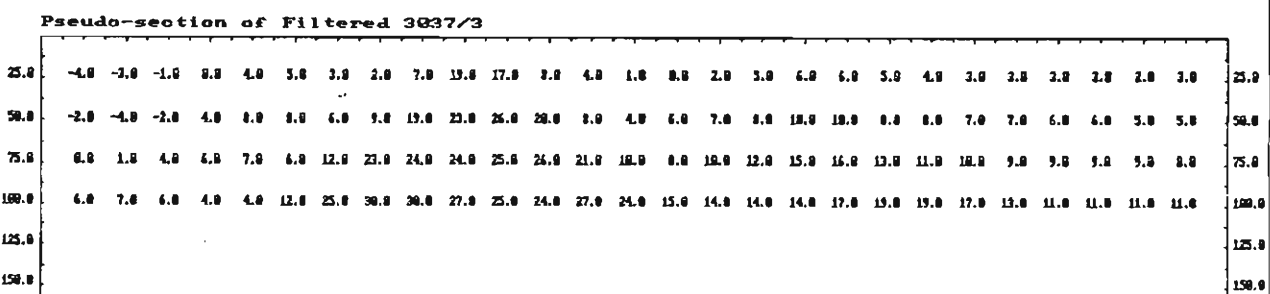
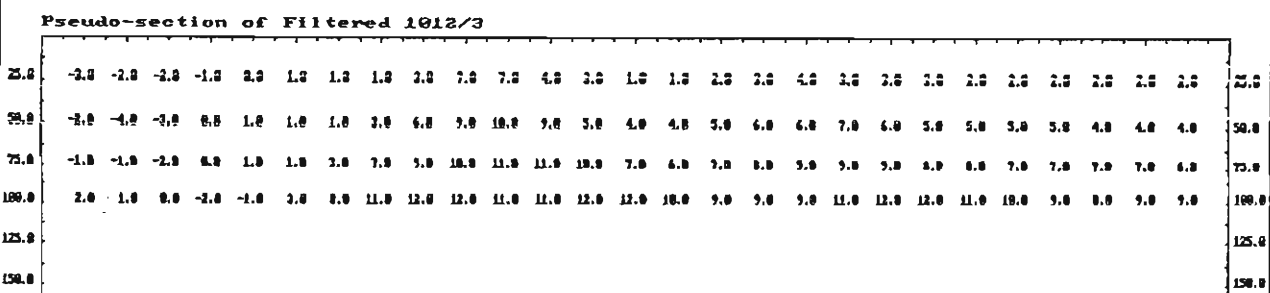
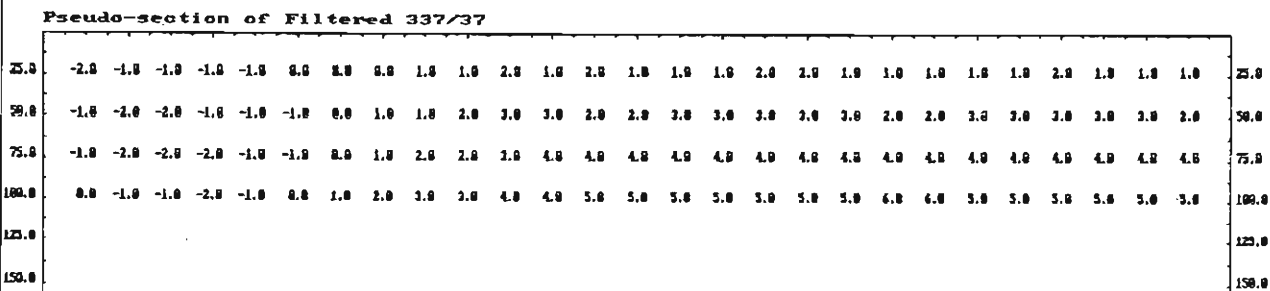
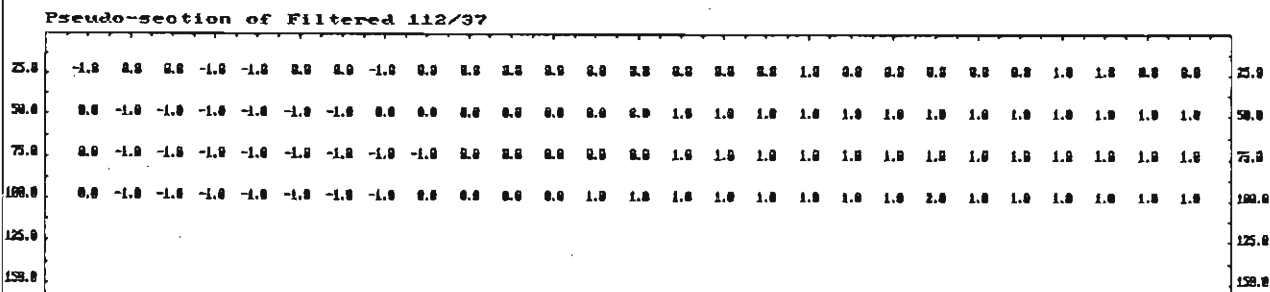
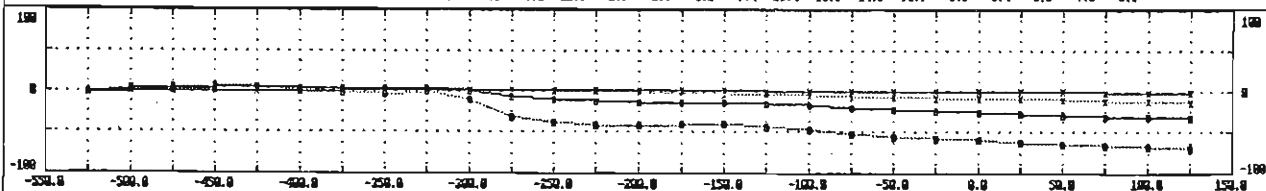
DATE 11/06/86 OPERATOR D.H.M.

112/37 -0.8 -0.3 -0.1 0.3 0.6 1.1 1.2 1.6 2.0 1.7 1.9 1.9 1.9 1.4 1.2 1.2 1.1 0.6 0.7 0.3 -0.1 -0.2 -0.4 -0.4 -1.3 -1.4 -1.5
112/37:FF -1.3 -1.5 -1.7 -1.2 -0.9 -1.3 -0.9 0.8 -0.1 -0.2 0.5 1.2 0.9 0.3 0.7 1.4 1.1 0.7 0.9 0.8 0.5 1.1 1.9 1.2

337/37 -0.5 1.2 1.7 2.5 3.3 3.5 3.5 3.6 3.6 2.7 1.4 0.5 -0.3 -1.7 -2.0 -2.0 -3.4 -5.2 -4.1 -7.2 -7.9 -4.3 -9.2 -10.4 -11.6 -12.1 -13.0
337/37:FF -3.5 -2.9 -2.6 -1.2 -0.3 -9.2 0.0 3.1 4.4 3.9 3.9 3.9 2.8 2.9 4.2 4.7 4.3 3.0 3.1 2.6 3.2 4.3 4.1 3.1

1012/3 0.0 2.9 3.0 5.1 5.5 4.6 4.0 4.3 4.5 0.7 -6.3 -10.0 -12.0 -13.2 -13.1 -13.6 -13.1 -17.9 -20.4 -22.5 -24.0 -25.9 -27.7 -29.2 -31.2 -32.2 -33.5
1012/3:FF -6.0 -3.9 -1.2 2.0 1.0 -0.2 3.1 14.4 21.5 16.4 0.9 4.3 1.5 2.4 6.3 9.6 9.9 9.0 7.0 6.3 6.2 6.0 6.5 5.3

3037/3 0.6 4.5 6.0 6.3 5.7 0.3 -2.4 -2.8 -0.6 -11.2 -32.0 -39.0 -41.3 -42.2 -41.0 -40.0 -40.5 -47.7 -52.0 -55.0 -52.5 -60.2 -62.6 -64.5 -66.8 -67.8 -69.0
3037/3:FF -7.0 -2.1 6.9 14.7 11.2 1.3 6.6 39.0 59.2 37.1 12.5 2.9 -1.7 1.1 9.4 15.4 16.6 14.6 10.9 0.5 0.4 0.5 7.5 6.3



TWIN GRID - LARGE LOOP EM

LINE 8100E

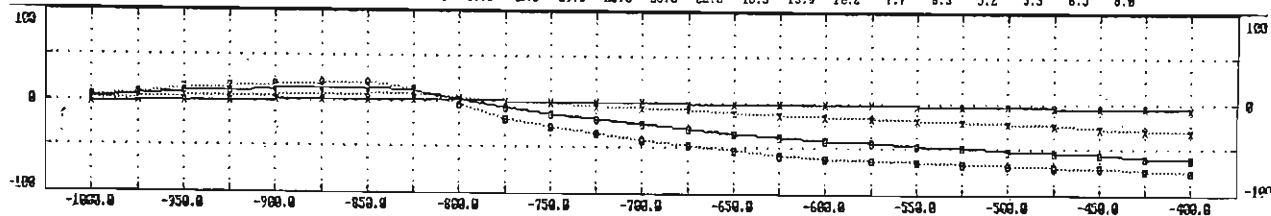
DATE 85 DEC. 1986 OPERATOR D.W. LOOP#6 LOOP 600x500m

112/37 -0.8 -0.3 0.6 0.7 1.4 1.6 2.0 1.6 1.3 1.0 0.5 0.0 -0.3 -0.7 -1.3 -1.8 -1.6 -2.3 -3.4 -3.1 -3.6 -4.7 -4.9 -5.9 -7.1
112/37:FF -2.4 -1.0 -1.7 -1.5 -0.6 0.7 1.3 1.4 1.0 1.8 1.5 1.7 2.1 1.4 0.8 2.3 2.6 1.0 1.8 2.9 2.5 3.4

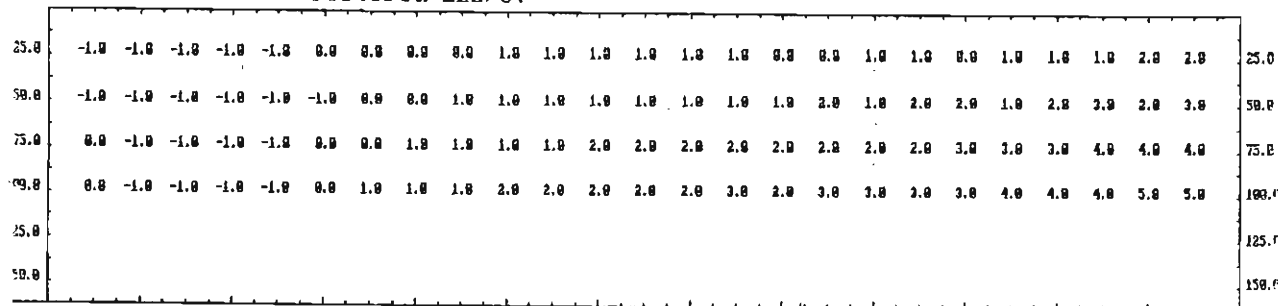
337/37 1.4 3.1 5.1 6.0 7.4 8.1 8.6 7.0 3.9 0.7 -1.9 -4.4 -7.1 -9.1 -11.3 -13.9 -14.0 -17.0 -18.6 -21.1 -22.6 -25.2 -27.5 -29.5 -32.0
337/37:FF -6.6 -5.2 -4.4 -3.3 -0.1 5.0 11.0 12.1 10.9 10.3 9.9 8.9 9.0 8.3 6.6 6.9 7.9 8.1 8.1 9.0 9.2 8.0

1012/3 4.1 6.0 10.0 11.7 13.5 14.6 14.9 10.4 2.2 -6.7 -12.9 -19.2 -25.2 -30.0 -35.0 -38.6 -41.6 -44.6 -47.8 -49.6 -52.1 -54.3 -56.2 -59.0 -61.6
1012/3:FF -10.0 -0.4 -6.4 -4.3 2.0 16.9 29.0 33.2 20.6 23.0 22.1 20.6 18.4 15.2 12.6 11.4 10.4 10.1 9.8 0.0 0.0 0.0 10.1

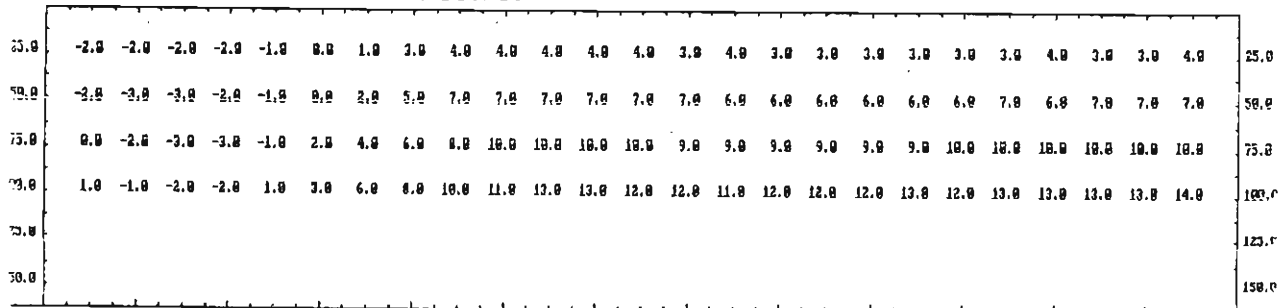
3037/3 5.5 9.7 14.2 16.4 17.6 18.9 19.3 12.3 -2.7 -10.9 -22.0 -35.3 -42.0 -47.1 -53.2 -57.9 -60.9 -63.8 -65.2 -67.2 -69.1 -69.5 -71.1 -73.0 -75.6
3037/3:FF -15.4 -10.1 -5.9 -4.0 4.3 29.2 53.0 57.3 42.5 29.6 25.0 23.0 22.0 18.5 13.6 10.2 7.7 6.3 5.2 5.3 6.5 8.0



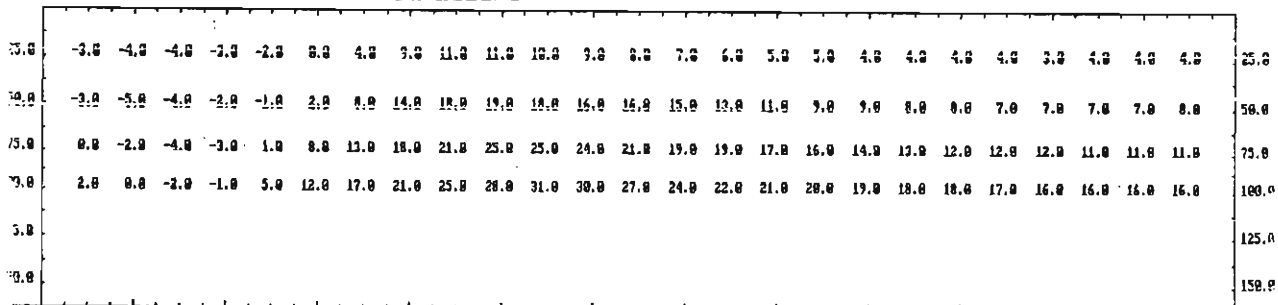
Pseudo-section of Filtered 112/37



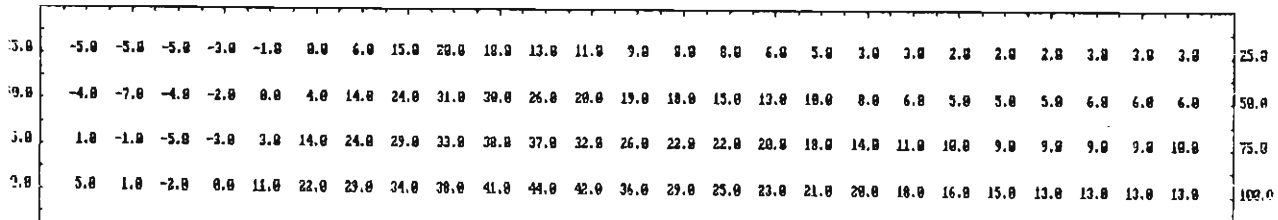
Pseudo-section of Filtered 337/37



Pseudo-section of Filtered 1012/3



Pseudo-section of Filtered 3037/3

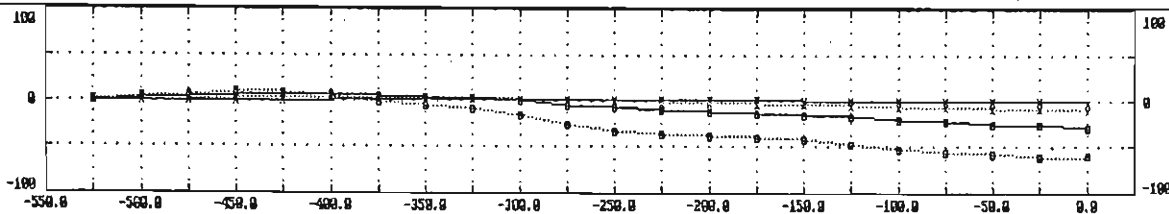


TWIN GRID - LARGE LOOP EM

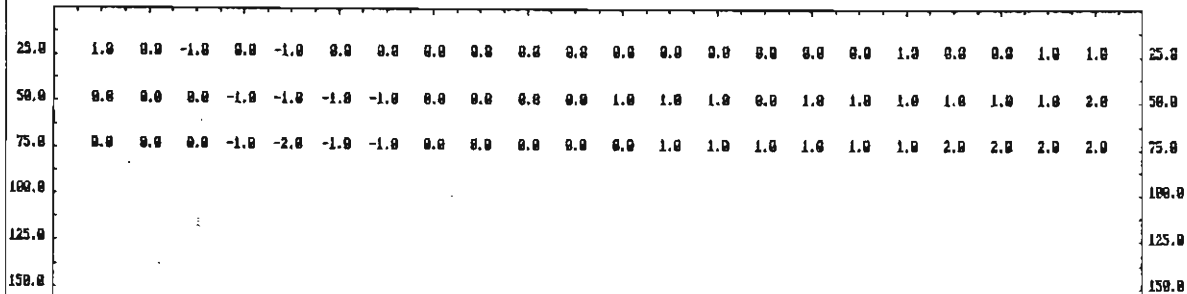
LINE L82E

DATE 11/06/86 OPERATOR D.M.W.

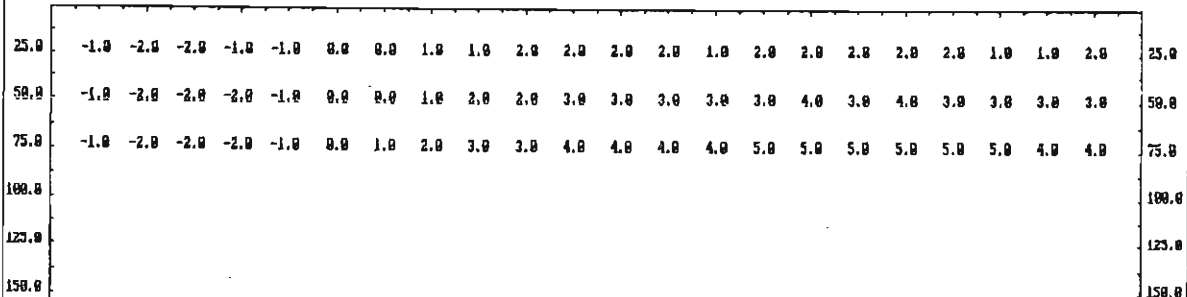
112/37 0.7 -0.5 0.2 0.6 1.0 1.6 1.7 2.1 2.0 2.1 1.9 1.9 1.4 1.2 1.2 1.0 0.8 0.4 -0.1 -0.2 -0.5 -1.1
112/37:FF -0.6 -1.9 -1.8 -1.7 -1.2 -0.8 -0.3 0.1 0.3 0.7 1.2 0.9 0.4 0.6 1.0 1.5 1.5 1.0 1.3
337/37 0.1 1.0 2.6 2.4 4.1 4.5 4.3 4.1 3.6 2.6 1.4 0.4 -1.1 -1.9 -2.0 -4.0 -5.1 -6.8 -7.5 -9.2 -9.4 -10.6
337/37:FF -4.9 -3.9 -2.6 -1.3 0.2 1.1 2.2 3.7 4.4 4.7 4.8 3.8 4.4 5.1 5.2 4.8 4.3 3.3
1812/3 0.0 2.0 5.5 6.7 7.5 7.3 5.6 4.2 3.0 -0.6 -4.5 -7.2 -10.0 -11.7 -13.2 -14.9 -17.5 -21.5 -22.9 -25.5 -27.0 -29.0
1812/3:FF -0.4 -5.7 -2.6 1.3 5.0 5.7 7.4 12.3 14.1 12.1 10.0 7.7 6.4 7.5 10.9 12.8 9.4 0.1 7.6
3037/3 1.2 5.7 0.1 10.0 9.5 6.2 -1.2 -5.5 -8.0 -16.4 -26.9 -32.9 -36.6 -38.0 -40.7 -42.8 -47.2 -52.7 -55.5 -58.8 -60.7 -50.9
3037/3:FF -11.2 -5.7 2.4 14.5 22.4 18.5 17.7 29.8 35.4 26.2 15.6 10.0 0.1 10.5 16.4 18.2 14.4 11.3 5.3



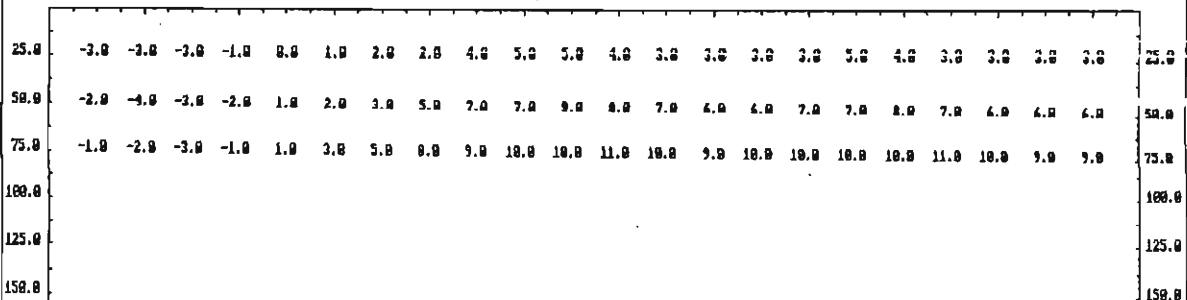
Pseudo-section of Filtered 112/37



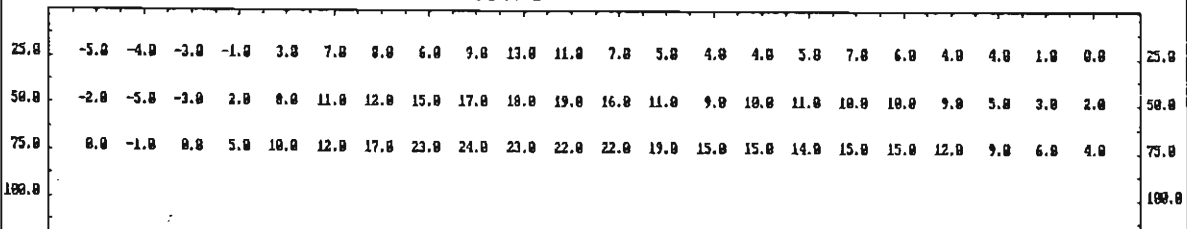
Pseudo-section of Filtered 337/37



Pseudo-section of Filtered 1812/3



Pseudo-section of Filtered 3037/3



TWIN GRID - LARGE LOOP EM

LINE 8200E

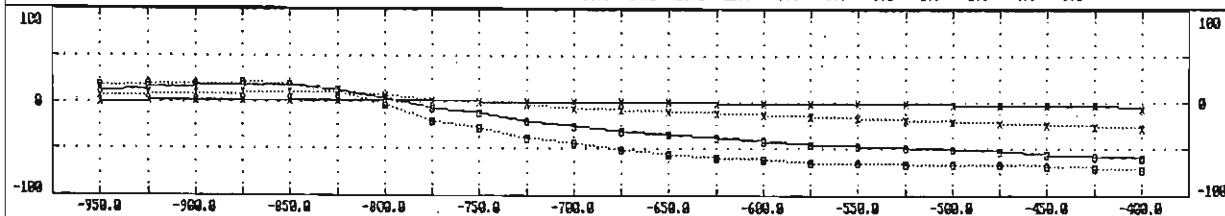
DATE 85 DEC. 1986 OPERATOR D.M. LOOP#6 LOOP 608x500m

112/37 1.0 1.5 2.2 2.7 2.6 2.6 2.4 1.6 0.9 0.6 0.2 -0.3 -0.4 -0.9 -1.2 -1.5 -1.9 -2.0 -2.7 -3.1 -3.6 -4.0 -4.0
112/37:FF -2.4 -1.6 -0.3 0.3 1.2 2.5 2.5 1.7 1.6 1.5 1.2 1.4 1.4 1.3 1.2 1.3 1.9 2.0 1.0 3.3

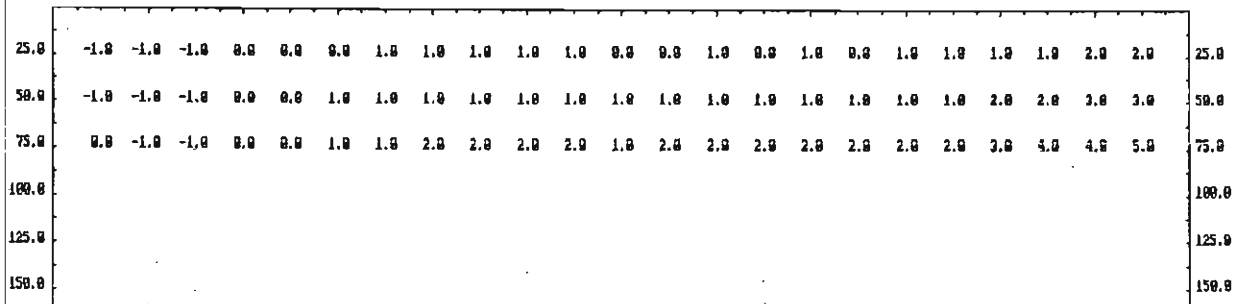
337/37 6.9 8.5 9.8 11.1 10.8 9.2 6.5 2.2 -0.4 -3.5 -6.0 -8.6 -10.4 -12.3 -13.0 -15.6 -17.2 -18.7 -20.1 -22.1 -24.4 -27.1 -29.3
337/37:FF -5.5 -3.6 0.9 6.2 11.3 13.9 12.6 11.3 10.7 9.5 8.1 7.1 6.7 6.7 6.5 6.0 6.3 7.7 9.3 9.1

1012/3 13.4 15.3 17.2 18.6 17.1 12.5 4.6 -6.4 -12.0 -20.2 -26.0 -31.3 -35.9 -39.1 -42.2 -45.0 -47.1 -49.6 -51.2 -53.3 -56.6 -58.2 -59.5
1012/3:FF -7.1 -3.2 6.2 10.6 31.4 36.3 31.2 27.0 24.3 21.0 17.7 14.1 12.2 10.0 9.5 8.7 7.8 9.1 10.3 7.8

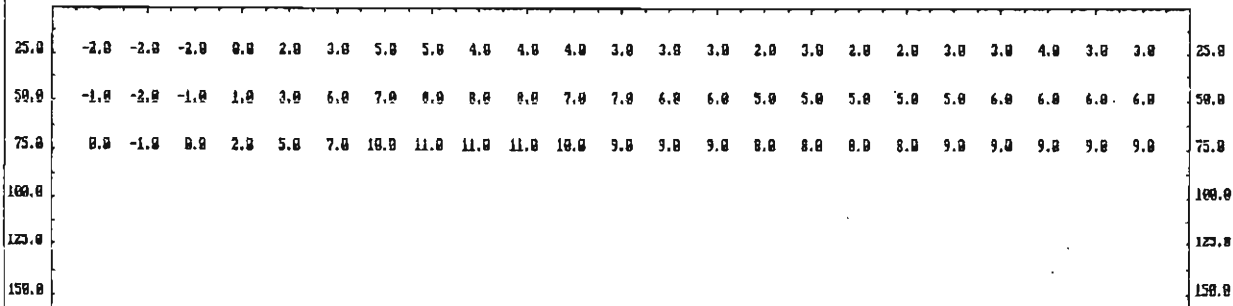
3037/3 17.0 18.0 19.9 21.0 10.6 10.7 -2.5 -20.4 -28.0 -33.1 -41.6 -50.3 -55.7 -59.3 -61.0 -64.9 -65.0 -66.0 -67.1 -67.4 -69.0 -70.3 -72.6
3037/3:FF -5.1 -0.9 11.5 31.4 52.2 57.4 45.0 34.5 27.0 22.3 20.1 15.1 11.7 9.6 5.9 3.2 1.9 2.5 4.0 6.5



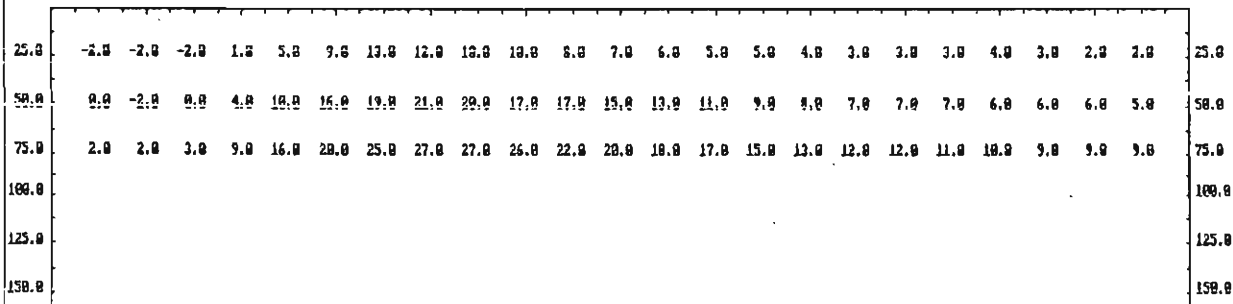
Pseudo-section of Filtered 112/37



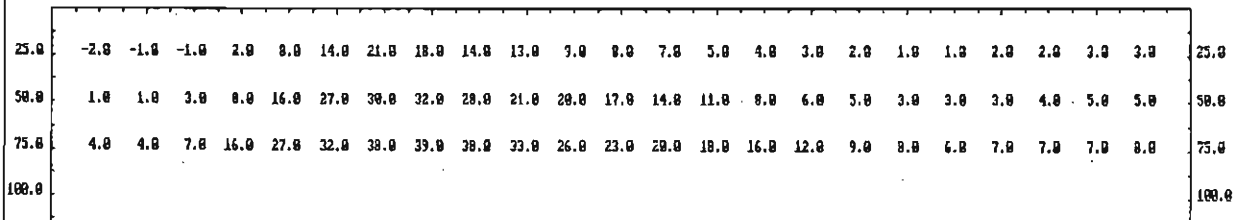
Pseudo-section of Filtered 337/37



Pseudo-section of Filtered 1012/3



Pseudo-section of Filtered 3037/3



TWIN GRID - LARGE LOOP EM

LINE L83E

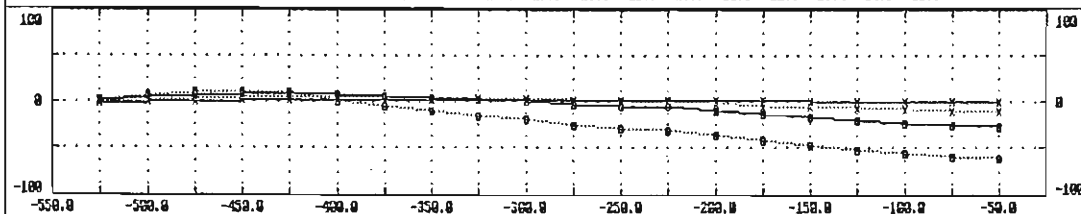
DATE 11/06/86 OPERATOR D.M.H.

112/37 -0.8 9.2 0.8 1.3 1.9 2.1 2.5 2.3 2.4 2.8 2.4 2.1 2.1 1.8 1.4 1.8 0.3 0.6 -0.2 -0.3
112/37:FF -2.7 -2.2 -1.9 -1.4 -0.8 -0.1 -0.4 -0.5 0.7 1.0 0.6 1.8 1.5 1.9 1.5 0.9 1.4

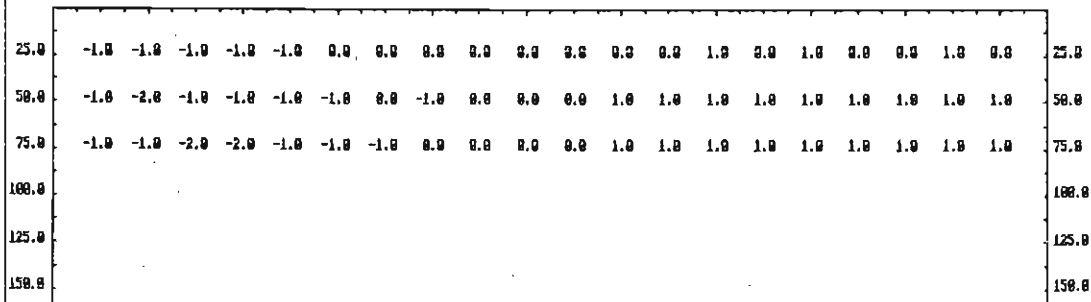
337/37 0.4 2.5 3.7 4.9 5.8 5.6 5.5 4.5 3.7 3.1 1.3 0.2 -0.2 -2.2 -4.3 -5.8 -7.5 -8.5 -9.9 -11.8
337/37:FF -5.7 -4.5 -2.8 -0.4 1.4 2.9 3.2 3.8 5.3 4.4 3.9 6.5 7.7 6.8 5.9 5.1 4.9

1012/3 1.8 5.3 7.1 9.1 9.8 7.6 5.9 3.7 1.5 0.8 -3.3 -5.8 -5.8 -10.2 -14.3 -17.6 -21.3 -23.7 -26.8 -27.2
1012/3:FF -9.1 -4.5 -1.2 5.4 7.8 0.3 0.1 0.5 10.6 0.3 6.9 12.9 15.9 14.4 13.1 10.8 0.2

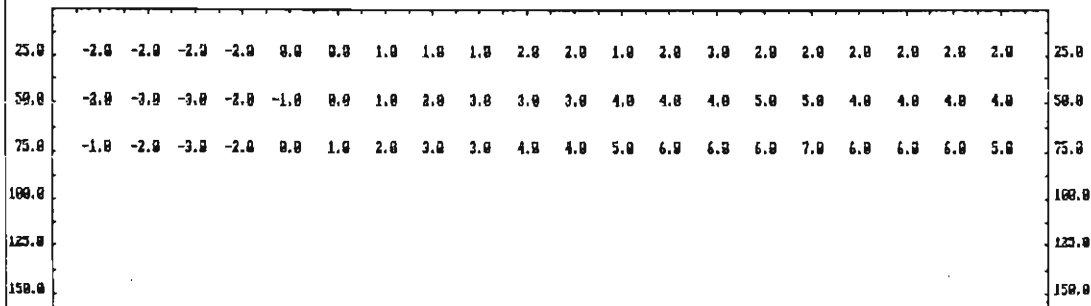
3037/3 2.7 7.4 10.0 11.4 10.2 0.4 -5.6 -11.8 -16.1 -19.0 -23.6 -29.0 -31.1 -36.3 -42.3 -47.1 -53.3 -55.5 -59.2 -60.8
3037/3:FF -11.3 -4.2 10.8 26.8 27.2 21.9 18.5 17.5 19.5 15.5 12.8 10.5 22.8 21.8 19.4 14.3 11.2



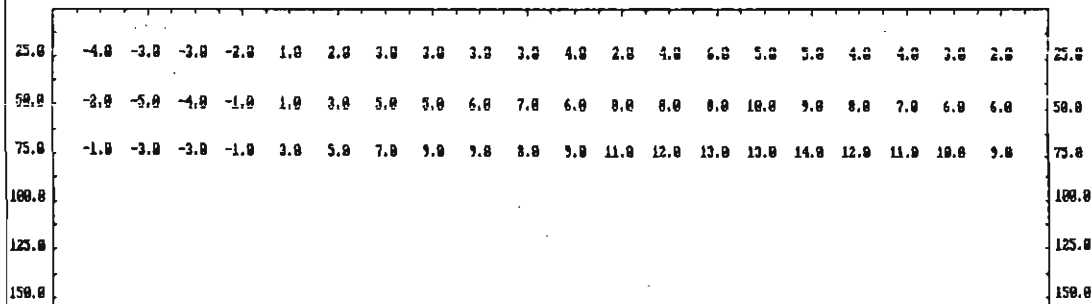
Pseudo-section of Filtered 112/37



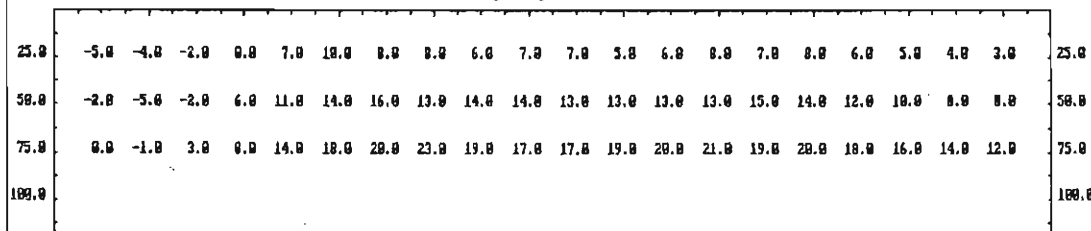
Pseudo-section of Filtered 337/37



Pseudo-section of Filtered 1012/3



Pseudo-section of Filtered 3037/3

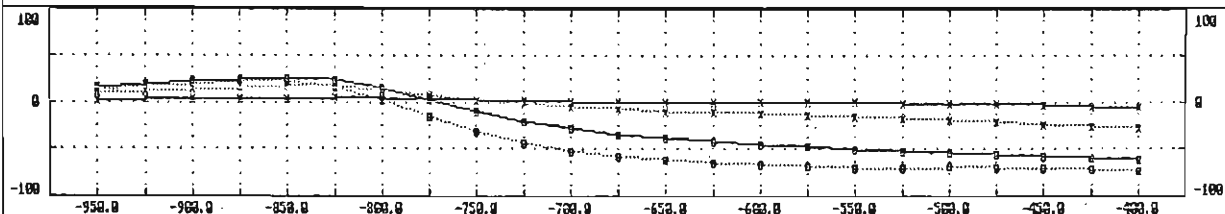


TWIN GRID - LARGE LOOP EH

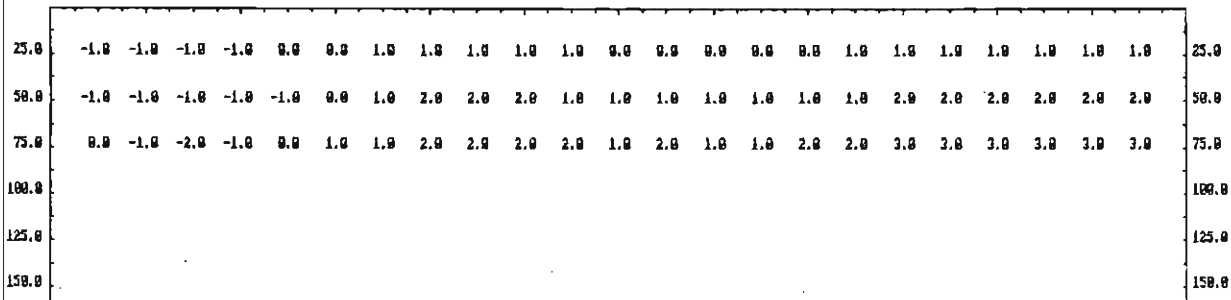
LINE 8300e

DATE 12/06/86 OPERATOR D.M.W.

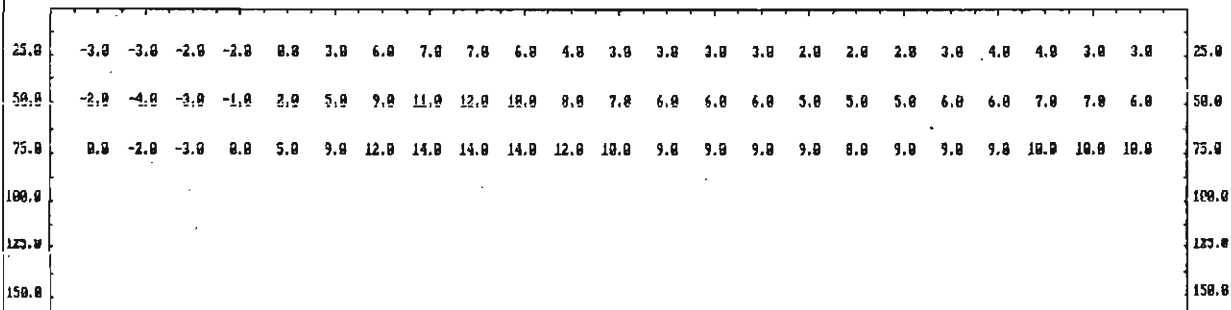
112/37	1.9	3.1	3.1	4.1	4.5	4.9	4.2	3.4	2.1	1.8	1.0	0.6	0.5	0.1	0.2	0.0	-0.4	-0.0	-1.3	-2.2	-3.5	-4.2	-4.5
112/37:FF	-2.2	-2.4	-2.2	-0.5	1.8	3.6	3.7	2.7	2.3	1.7	1.0	0.8	0.4	0.7	1.4	1.7	2.3	3.6	4.2	3.0			
337/37	10.0	12.7	14.3	16.2	17.1	16.4	13.3	7.9	2.1	-2.3	-5.5	-7.6	-9.5	-10.9	-12.8	-14.4	-16.0	-17.1	-18.9	-20.4	-24.0	-25.9	-27.9
337/37:FF	-7.0	-6.3	-3.0	3.6	12.3	19.7	21.4	17.0	12.9	9.3	7.3	6.6	6.8	6.7	5.9	5.6	6.2	8.4	10.6	9.4			
1012/3	16.4	20.3	22.3	25.0	25.6	22.5	14.8	1.7	-11.1	-21.6	-20.6	-35.0	-38.1	-41.3	-45.0	-47.6	-50.5	-52.1	-53.7	-55.4	-57.5	-60.2	-62.0
1012/3:FF	-10.6	-8.0	-0.8	13.3	31.6	46.7	49.2	40.0	30.9	22.9	15.8	13.2	13.2	11.8	10.0	7.7	6.5	7.1	0.6	9.3			
3037/3	14.4	18.0	19.7	22.3	21.9	15.3	2.2	-15.0	-32.3	-41.0	-52.0	-57.7	-61.2	-64.3	-67.2	-68.1	-69.7	-70.1	-69.2	-69.5	-70.1	-71.5	-74.7
3037/3:FF	-9.6	-6.5	4.8	25.7	50.0	64.0	63.5	40.7	33.4	22.9	15.0	12.6	9.8	6.3	4.5	1.5	-1.1	0.3	2.9	6.6			



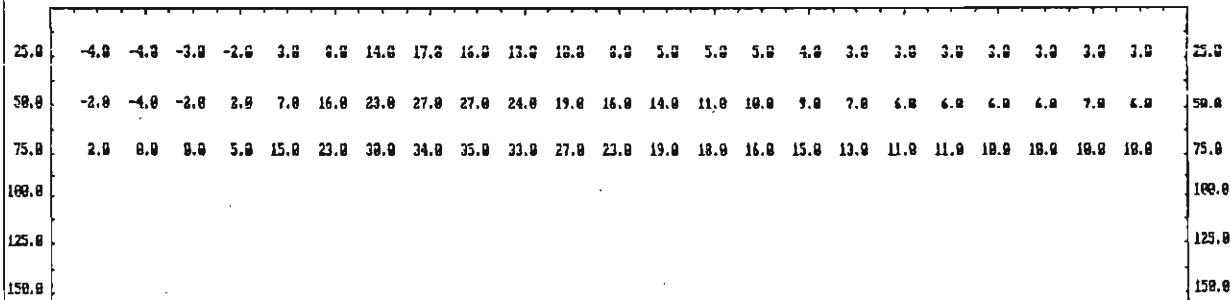
Pseudo-section of Filtered 112/37



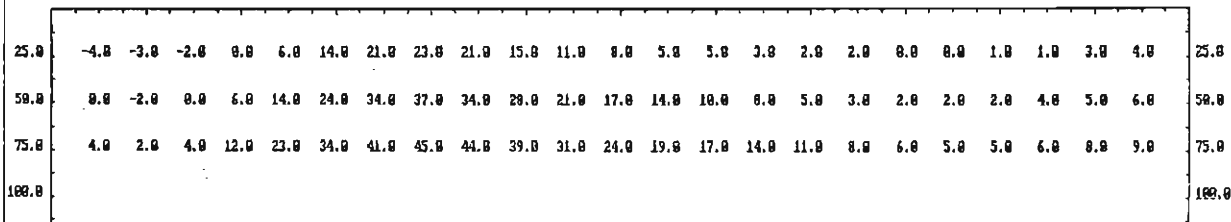
Pseudo-section of Filtered 337/37



Pseudo-section of Filtered 1012/3



Pseudo-section of Filtered 3037/3



APPENDIX III

ACME ANALYTICAL LABORATORIES LTD.

Soil Geochemical Results

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO₃-H₂O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN, FE, CA, P, CR, MG, BA, TI, B, AL, NA, K, W, SI, ZR, CE, SN, Y, NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: SOILS - BOMESH AU ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: NOV 11 1986 DATE REPORT MAILED: *Nov 14/86* ASSAYER: *D. J. Jepsen* DEAN TOYE. CERTIFIED B.C. ASSAYER.

C.E.C. ENGINEERING PROJECT-TWIN FB6-14 FILE# 86-3645

PAGE 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au1 PPB
52+00E 0+00S	1	165	68	163	.8	85	22	1886	3.04	13	5	ND	1	67	1	2	2	40	1.98	.117	11	97	.94	229	.04	6	2.05	.03	.02	1	3
52+00E 0+25S	1	64	94	148	.6	138	30	1869	6.97	32	5	ND	1	18	1	2	2	43	.54	.063	11	72	.55	326	.05	2	1.81	.01	.04	1	25
52+00E 0+50S	1	75	87	235	.3	130	29	1029	5.30	30	5	ND	2	12	1	2	2	71	.16	.057	14	151	1.60	255	.11	4	2.84	.01	.05	1	9
52+00E 0+75S	1	21	39	118	.4	104	22	343	4.11	13	5	ND	2	8	1	2	2	66	.12	.039	7	175	1.36	117	.10	2	2.48	.02	.03	1	3
52+00E 1+00S	1	12	56	81	.5	51	11	181	2.37	5	5	ND	1	9	1	2	2	35	.16	.037	8	46	.30	119	.08	2	2.09	.02	.02	1	1
52+50E 0+00S	1	32	75	199	.4	49	17	324	3.19	15	5	ND	1	41	1	2	2	39	.80	.030	9	63	.63	99	.10	2	2.65	.04	.02	1	1
53+00E 0+00S	1	59	74	245	.2	103	24	295	5.85	30	5	ND	2	30	1	2	2	79	.71	.031	13	147	1.59	127	.13	3	3.54	.01	.03	1	3
53+00E 0+25S	1	11	19	109	.3	24	10	219	2.34	7	5	ND	1	7	1	2	3	36	.10	.050	6	33	.28	91	.10	2	2.75	.02	.01	1	40
53+00E 0+50S	1	67	101	190	.8	104	25	1119	4.85	25	5	ND	2	20	1	2	2	55	.54	.085	8	111	1.11	223	.09	2	2.56	.01	.04	1	10
53+00E 0+75S	1	38	22	180	.3	160	34	360	5.67	13	5	ND	2	17	1	2	2	44	.27	.037	9	99	.47	500	.03	2	2.95	.01	.04	1	38
53+00E 1+00S	1	13	25	88	.3	13	8	184	2.33	8	5	ND	2	12	1	2	2	32	.15	.079	2	17	.12	77	.13	2	3.32	.03	.01	1	1
53+00E 1+25S	1	38	34	105	.4	69	13	1012	3.10	8	5	ND	3	32	1	2	2	43	.75	.081	22	71	.50	254	.17	2	3.84	.02	.04	1	1
53+00E 1+50S	1	6	11	22	.4	3	3	52	1.04	2	5	ND	1	9	1	2	2	19	.14	.022	6	8	.05	56	.07	2	1.56	.03	.02	1	1
53+00E 1+75S	1	12	15	80	.1	23	8	355	2.22	5	5	ND	1	7	1	2	2	34	.08	.131	5	29	.18	88	.14	3	3.08	.03	.02	1	5
53+00E 2+00S	1	6	15	46	.3	10	7	110	2.09	6	5	ND	1	7	1	2	2	35	.07	.056	5	17	.11	48	.10	2	2.34	.02	.02	1	1
53+50E 0+00S	2	53	102	202	.4	64	24	199	5.14	26	5	ND	3	12	1	2	2	42	.16	.049	10	60	.47	111	.15	4	3.68	.02	.02	1	3
54+00E 0+25S	2	91	59	147	1.0	66	15	2417	2.41	15	5	ND	1	93	2	2	2	35	2.54	.124	7	81	.83	190	.03	5	1.89	.03	.02	1	1
54+00E 0+50S	1	66	108	232	.7	99	27	641	4.99	35	5	ND	3	12	1	3	2	64	.21	.071	9	131	1.35	172	.12	2	2.64	.01	.05	1	50
54+00E 0+75S	1	35	39	141	2.6	35	9	337	2.42	14	5	ND	3	33	1	2	2	33	.67	.066	12	35	.37	164	.13	2	3.36	.05	.03	1	1
54+00E 1+00S	1	8	32	186	.6	25	13	409	3.80	15	5	ND	2	8	1	2	3	51	.10	.138	7	44	.29	108	.14	3	4.40	.02	.03	1	1
54+00E 1+25S	1	69	52	131	.8	99	18	1254	3.96	11	9	ND	1	35	1	2	2	36	.94	.050	6	42	.29	192	.07	2	2.01	.03	.03	1	19
54+00E 1+50S	2	145	29	158	.8	189	35	5349	4.78	24	5	ND	1	53	2	2	2	22	1.25	.068	12	27	.17	413	.06	2	2.13	.03	.04	1	21
54+00E 1+75S	1	36	34	153	.1	68	23	340	5.89	31	5	ND	2	8	1	2	2	54	.09	.069	9	62	.54	121	.09	2	2.38	.01	.04	1	4
54+00E 2+00S	1	49	33	112	.2	63	19	560	5.25	24	5	ND	4	11	1	2	3	55	.17	.076	13	57	.79	156	.08	5	2.65	.01	.06	1	1
54+00E 2+25S	1	23	19	91	.2	31	12	365	3.04	6	5	ND	2	9	1	2	2	44	.12	.101	7	46	.39	90	.12	2	2.93	.02	.03	1	4
54+00E 2+50S	1	16	45	90	.1	47	14	485	3.53	22	5	ND	1	11	1	2	3	56	.18	.041	7	68	.57	103	.11	2	2.45	.02	.03	1	1
54+00E 2+75S	1	62	75	150	.1	78	23	410	5.32	57	5	ND	6	13	1	2	2	64	.18	.043	16	96	1.17	155	.10	2	2.80	.01	.05	1	15
54+00E 3+00S	1	62	11	60	.2	18	7	367	1.64	5	5	ND	1	28	1	2	2	29	.74	.065	10	17	.18	137	.09	2	2.43	.06	.02	1	1
54+50E 0+00S	5	173	45	252	1.7	78	16	9641	1.79	12	5	ND	2	141	5	2	2	27	3.59	.157	11	71	.54	404	.03	7	2.03	.03	.03	1	4
55+00E 0+00S	1	17	57	187	.5	42	14	237	3.33	22	5	ND	2	17	1	2	2	45	.29	.034	6	61	.58	103	.14	2	3.13	.03	.02	1	1
55+00E 0+25S	1	80	76	284	.5	90	27	987	4.33	25	5	ND	3	45	1	2	4	54	.83	.043	10	127	1.36	339	.13	2	2.44	.03	.03	1	3
55+00E 0+50S	1	16	100	267	.9	50	17	250	3.86	18	5	ND	3	14	1	2	2	54	.19	.023	7	81	.77	68	.13	2	2.76	.03	.03	1	4
55+00E 0+75S	1	80	130	272	.3	130	30	429	5.63	27	5	ND	5	15	1	2	2	76	.24	.075	11	175	1.80	148	.18	2	3.24	.01	.05	1	1
55+00E 1+00S	2	38	62	167	.3	57	18	504	3.71	17	5	ND	5	9	1	2	4	53	.12	.086	10	76	.81	144	.11	2	2.85	.02	.04	1	3
55+00E 1+25S	1	125	51	146	.2	154	37	993	7.59	26	5	ND	3	7	1	2	5	63	.08	.043	17	137	.66	358	.02	2	3.50	.01	.06	1	1
55+00E 1+50S	2	98	71	176	.3	89	25	451	5.07	21	5	ND	8	10	1	2	3	63	.14	.068	14	116	1.50	200	.08	2	3.46	.01	.08	1	5
STD C/AU-S	21	58	39	134	7.0	69	30	1043	3.96	41	18	7	34	50	18	15	21	64	.48	.102	37	59	.88	184	.08	38	1.71	.07	.13	13	49

SAMPLE#	Mc PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mo %	Ba PPM	Ti %	P PPM	Al %	Na %	K %	M PPM	Au# PPB
55+00E 1+75S	1	41	11	64	1.7	15	4	684	1.09	2	5	ND	1	61	1	2	3	18	2.27	.102	6	15	.23	207	.06	10	1.88	.03	.02	1	1
55+00E 2+00S	1	12	17	56	.7	22	6	97	2.51	14	5	ND	1	23	1	2	2	37	.55	.049	4	27	.20	63	.09	3	2.95	.04	.02	1	1
55+00E 2+25S	2	30	28	77	.1	34	12	193	4.22	19	5	ND	2	12	1	2	2	54	.18	.045	7	40	.32	96	.12	8	3.54	.02	.01	1	5
55+00E 2+50S	1	10	11	91	.1	37	10	180	3.24	3	5	ND	1	6	1	2	2	52	.08	.038	2	51	.29	80	.09	5	1.83	.02	.02	1	1
55+00E 2+75S	1	28	17	70	.2	21	7	204	2.42	19	5	ND	1	9	1	2	2	38	.11	.060	4	30	.20	61	.10	4	2.36	.03	.02	1	9
55+00E 3+00S	2	54	18	107	.1	62	26	1199	4.84	13	5	ND	1	11	1	2	2	52	.17	.107	4	76	.50	162	.09	5	3.01	.03	.03	1	1
55+00E 3+25S	1	13	9	50	.1	15	5	449	2.11	6	5	ND	1	8	1	2	2	36	.10	.063	3	28	.19	78	.11	2	1.38	.03	.02	1	1
55+00E 3+50S	3	90	28	108	.3	49	15	1462	3.34	19	5	ND	4	19	1	2	2	39	.27	.140	21	44	.45	237	.14	7	3.76	.03	.05	1	1
55+00E 3+75S	2	72	37	120	.1	88	21	354	5.03	29	5	ND	6	17	1	2	2	60	.26	.061	15	93	1.23	192	.12	5	2.94	.02	.06	1	6
55+00E 4+00S	2	22	22	99	.3	51	12	565	3.31	19	6	ND	3	10	1	2	2	41	.13	.187	4	47	.45	128	.13	2	3.89	.02	.04	1	1
55+50E 0+00S	1	111	23	95	.6	33	10	538	2.05	8	5	ND	1	27	1	2	3	27	.62	.040	8	28	.25	120	.10	3	2.56	.05	.03	1	1
56+00E 0+00S	2	47	94	210	.9	56	17	415	3.14	23	5	ND	2	21	1	2	2	38	.50	.055	11	58	.53	149	.12	5	3.23	.03	.02	1	13
56+00E 0+25S	2	53	43	307	.3	71	16	2607	3.32	14	5	ND	1	27	2	2	2	43	.57	.051	6	75	.82	205	.13	2	2.98	.04	.03	1	12
56+00E 0+50S	1	134	39	264	1.8	53	12	724	2.84	14	5	ND	1	60	1	2	2	38	1.58	.105	16	50	.51	126	.08	4	3.00	.05	.03	1	2
56+00E 0+75S	2	64	94	240	.8	78	21	822	4.09	23	5	ND	3	14	1	2	2	55	.25	.082	9	91	1.08	170	.11	4	2.93	.01	.25	1	3
56+00E 1+00S	2	25	39	148	.4	56	14	427	3.34	14	5	ND	1	13	1	2	3	50	.21	.056	7	71	.65	125	.14	2	2.70	.03	.02	1	5
56+00E 1+25S	1	119	144	293	1.6	134	31	1204	5.69	45	5	ND	4	40	1	7	2	73	2.19	.069	9	163	2.18	232	.12	2	2.62	.02	.08	1	8
56+00E 1+50S	1	36	29	133	1.5	46	11	457	2.83	13	5	ND	2	27	1	2	2	41	.74	.049	10	59	.64	212	.09	4	2.70	.03	.04	1	1
56+00E 1+75S	2	24	26	130	2.0	42	11	192	3.81	13	5	ND	3	17	1	2	2	54	.27	.055	8	55	.58	195	.12	5	3.59	.02	.05	1	1
56+00E 2+00S	1	49	52	152	.2	122	26	338	5.29	28	5	ND	3	14	1	2	2	80	.30	.023	9	182	2.04	132	.12	2	2.78	.01	.05	1	2
56+00E 2+25S	1	9	12	48	.3	24	6	165	1.89	6	5	ND	2	9	1	2	2	39	.17	.027	9	39	.32	69	.05	4	.67	.01	.03	1	11
56+00E 2+50S	2	18	14	72	.2	26	10	513	2.92	9	5	ND	2	10	1	2	2	45	.13	.166	4	38	.32	75	.14	3	3.23	.02	.02	1	1
56+00E 2+75S	1	21	79	129	.1	28	10	1726	3.03	9	5	ND	1	10	1	2	2	51	.17	.117	4	42	.35	125	.11	5	2.05	.02	.03	1	1
56+00E 3+00S	1	4	13	36	.1	13	3	89	1.83	5	5	ND	1	5	1	2	2	40	.06	.019	2	20	.13	22	.11	3	.53	.02	.02	1	1
56+00E 3+25S	2	26	24	127	.4	79	9	2678	2.39	8	5	ND	1	30	1	2	2	30	.57	.088	7	22	.26	132	.11	4	2.55	.05	.03	1	3
56+00E 3+50S	1	1	13	44	.1	7	2	233	1.17	2	5	ND	1	5	1	2	3	31	.06	.023	3	13	.07	37	.08	5	.41	.02	.01	1	1
56+00E 3+75S	1	14	23	95	.2	32	15	1302	3.21	16	5	ND	1	12	1	2	3	48	.19	.118	3	43	.28	77	.09	3	1.78	.03	.03	1	4
56+00E 4+00S	1	3	7	32	.1	13	3	96	1.35	3	5	ND	1	5	1	2	2	32	.08	.015	3	17	.09	26	.07	3	.36	.02	.02	2	1
56+00E 4+25S	2	25	24	118	.1	80	18	523	4.49	17	5	ND	3	11	1	2	2	57	.16	.093	4	79	.77	136	.10	2	2.53	.02	.05	1	1
56+00E 4+50S	2	14	19	95	.1	81	17	620	3.21	9	5	ND	2	8	1	2	2	47	.11	.058	5	62	.32	84	.09	5	1.78	.02	.04	1	1
56+00E 4+75S	1	13	12	65	.3	31	12	768	2.82	7	8	ND	4	10	1	2	2	45	.18	.053	11	45	.57	113	.08	4	1.43	.01	.06	1	1
56+00E 5+00S	1	5	7	36	.1	11	4	121	1.81	5	5	ND	1	7	1	2	2	34	.07	.025	3	16	.13	58	.10	2	1.32	.03	.02	1	1
56+50E 0+00S	2	33	52	310	.8	67	16	770	3.44	24	5	ND	3	31	1	2	2	40	.70	.075	8	64	.75	160	.13	4	3.69	.03	.04	1	1
57+00E 0+00S	2	23	78	246	.4	47	18	286	4.00	35	5	ND	3	14	1	2	2	48	.26	.146	3	52	.55	75	.10	3	2.70	.02	.04	1	1
57+00E 0+25S	2	10	27	126	.9	33	9	196	2.57	13	5	ND	2	15	1	2	2	36	.23	.043	5	30	.30	92	.11	2	3.06	.03	.02	1	1
57+00E 0+50S	2	123	162	311	.6	155	38	1127	6.39	48	5	ND	5	30	1	2	2	74	.75	.061	12	174	2.35	457	.13	3	2.68	.02	.06	1	6
STD C/AU-S	21	58	39	130	7.0	69	28	1000	3.93	41	18	7	33	46	17	15	20	62	.48	.101	36	58	.88	175	.08	36	1.72	.06	.13	13	51

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Ri PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mo %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	M PPM	Au1 PPB
57+00E 0+75S	1	64	136	253	.7	81	19	590	4.16	27	5	ND	2	26	1	2	4	50	.52	.040	12	88	.94	192	.10	6	2.43	.02	.08	1	2
57+00E 1+00S	1	41	55	137	.4	71	18	338	3.81	17	5	ND	4	11	1	2	2	59	.18	.041	9	96	1.09	113	.11	6	2.50	.02	.04	1	1
57+00E 1+25S	1	51	53	184	.2	59	20	384	4.16	35	5	ND	4	8	1	4	2	53	.14	.054	7	80	.92	83	.10	2	1.83	.01	.03	1	1
57+00E 1+50S	1	33	35	183	.4	59	18	360	3.88	31	5	ND	3	13	1	2	2	53	.20	.025	8	73	.87	160	.10	3	2.01	.02	.03	1	1
57+00E 1+75S	1	19	41	143	.7	41	11	350	3.19	20	5	ND	3	20	1	2	2	41	.41	.057	8	51	.51	144	.14	3	3.43	.03	.04	1	
57+00E 2+00S	1	88	68	180	1.5	104	25	1060	4.84	29	6	ND	4	31	1	3	2	64	.78	.064	16	134	1.72	240	.11	9	2.80	.02	.08	1	11
57+00E 2+25S	1	68	90	164	.8	82	21	874	4.69	23	5	ND	4	28	1	2	2	70	.60	.052	16	119	1.76	222	.12	4	2.69	.02	.09	1	4
57+00E 2+50S	1	3	8	25	.2	7	3	68	.91	2	5	ND	2	4	1	2	4	20	.04	.023	5	10	.11	23	.05	4	.38	.02	.02	1	1
57+00E 2+75S	1	14	34	77	.1	40	10	185	3.68	25	5	ND	2	9	1	2	2	60	.17	.042	7	62	.63	69	.11	6	1.36	.02	.02	1	1
57+00E 3+00S	1	24	14	82	.2	31	11	952	2.62	6	5	ND	3	9	1	2	2	36	.14	.079	7	27	.21	89	.10	2	2.31	.03	.03	1	10
57+00E 3+25S	1	56	9	95	.3	240	38	824	5.09	15	6	ND	3	17	1	2	2	28	.33	.054	9	29	.32	109	.04	7	1.50	.02	.05	1	320
57+00E 3+50S	1	26	32	93	.1	74	17	354	4.13	26	5	ND	3	8	1	2	2	55	.13	.045	10	79	.98	83	.10	8	1.92	.01	.03	1	7
57+00E 3+75S	1	15	12	68	.2	26	9	565	2.40	6	5	ND	2	11	1	2	2	37	.17	.075	9	25	.27	72	.08	3	2.23	.03	.04	1	1
57+00E 4+00S	1	15	19	85	.1	36	11	204	3.12	10	5	ND	3	9	1	2	2	47	.12	.054	8	46	.58	77	.12	6	2.14	.02	.04	1	1
57+00E 4+25S	1	13	15	88	.2	14	8	360	2.73	14	5	ND	2	7	1	2	2	36	.08	.170	4	25	.17	78	.16	5	3.88	.02	.02	1	1
57+00E 4+50S	1	77	83	234	.3	95	28	369	5.77	79	5	ND	5	12	1	2	2	49	.17	.060	10	80	.84	124	.11	2	2.60	.01	.04	1	15
57+00E 4+75S	1	51	25	85	.1	102	25	865	4.93	24	5	ND	2	20	1	2	2	62	.33	.041	11	105	.86	165	.08	6	2.23	.02	.06	1	1
57+00E 5+00S	1	44	14	96	.3	36	10	2513	2.37	6	5	ND	2	26	1	2	2	33	.50	.028	13	34	.51	309	.10	5	2.21	.04	.05	1	2
57+00E 5+25S	1	25	13	79	.1	36	12	447	3.00	8	5	ND	5	12	1	2	2	42	.20	.057	12	46	.67	157	.11	5	2.54	.02	.05	1	1
57+00E 5+50S	1	43	24	96	.1	70	21	653	4.26	19	5	ND	3	12	1	2	2	54	.18	.053	7	85	.79	144	.12	5	2.24	.02	.04	1	8
57+00E 5+75S	1	33	32	120	.1	99	24	603	4.91	27	5	ND	3	17	1	2	2	65	.26	.042	10	127	1.35	150	.12	4	2.04	.01	.06	1	2
57+00E 6+00S	1	19	35	123	.1	44	16	368	3.55	26	5	ND	2	7	1	2	2	44	.09	.066	5	47	.45	83	.10	5	1.87	.02	.03	1	7
57+00E 6+00S	1	16	41	184	.6	20	7	1197	2.09	8	5	ND	1	18	1	2	2	33	.32	.064	6	20	.18	84	.10	2	1.99	.04	.02	1	2
58+00E 0+00S	1	57	71	203	.3	55	17	501	3.50	23	5	ND	4	14	1	2	2	48	.26	.034	10	66	.77	164	.10	5	1.94	.03	.05	1	1
58+00E 0+25S	1	96	110	277	1.0	83	23	1013	4.64	39	5	ND	3	25	1	2	2	52	.62	.047	13	95	1.11	191	.10	4	2.68	.02	.05	1	7
58+00E 0+50S	1	63	6	140	1.0	20	4	1607	.36	2	5	ND	2	174	3	2	3	5	6.19	.106	2	9	.20	185	.01	8	.38	.01	.02	1	1
58+00E 0+75S	1	58	5	49	.6	15	3	777	.38	2	5	ND	2	183	1	2	2	6	6.72	.109	3	4	.17	193	.01	7	.45	.01	.02	1	1
58+00E 1+00S	1	14	44	146	.6	42	15	362	3.56	15	5	ND	1	7	1	2	2	56	.11	.033	6	74	.75	74	.10	6	2.33	.01	.02	1	9
58+00E 1+25S	1	38	58	251	.6	65	21	664	4.44	42	5	ND	5	14	1	2	2	55	.20	.032	8	73	.91	174	.10	5	2.62	.02	.05	1	2
58+00E 1+50S	1	15	21	64	.6	18	11	314	2.35	10	5	ND	3	14	1	2	3	35	.18	.051	4	24	.24	53	.08	2	2.55	.04	.02	1	1
58+00E 1+75S	1	41	66	211	.8	69	21	524	5.16	55	5	ND	3	17	1	2	2	52	.28	.082	6	66	.68	175	.12	6	3.55	.02	.04	1	1
58+00E 2+00S	1	123	160	241	.8	99	40	1149	7.61	129	5	ND	5	14	1	4	2	54	.35	.076	14	87	1.00	157	.11	7	2.48	.01	.05	1	31
58+00E 2+25S	1	28	48	201	.3	45	20	381	5.67	44	5	ND	5	11	1	2	2	69	.12	.079	10	66	.74	161	.12	5	3.11	.02	.05	1	1
58+00E 2+50S	1	47	29	107	.5	62	18	814	3.56	15	5	ND	3	23	1	2	3	45	.53	.057	13	86	1.09	121	.11	3	2.41	.02	.04	1	1
58+00E 2+75S	1	45	59	132	.6	71	26	460	5.36	53	5	ND	3	13	1	2	3	55	.17	.054	9	99	.99	106	.13	4	2.28	.01	.03	1	1
58+00E 3+00S	1	21	47	126	.2	60	19	462	4.03	34	5	ND	2	9	1	2	4	38	.12	.069	6	47	.48	96	.10	4	2.69	.02	.03	1	1
STD C/AU-S	20	57	39	129	7.0	65	29	997	3.95	40	19	8	34	49	17	15	20	62	.48	.098	37	55	.88	184	.08	37	1.72	.07	.14	13	48

SAMPLE#	Mo PPH	Cu PPH	Pb PPH	Zn PPH	Ag PPH	Ni PPH	Co PPH	Mn PPH	Fe %	As PPH	U PPH	Au PPH	Th PPH	Sr PPH	Cd PPH	Sb PPH	Bi PPH	V PPH	Ca %	P %	La PPH	Cr PPH	Mg %	Ba PPH	Ti %	P PPH	Al %	Na %	F %	W PPH	Au1 PPB
58+00E 3+25S	1	43	65	138	.3	58	18	314	4.21	31	5	ND	5	12	1	2	2	48	.17	.069	10	70	.87	106	.08	2	2.62	.01	.04	2	2
58+00E 3+50S	1	21	16	101	.2	32	12	740	3.16	10	5	ND	3	14	1	2	2	42	.17	.120	10	41	.62	122	.07	6	2.34	.02	.04	2	1
58+00E 3+75S	1	10	9	68	.5	16	9	514	2.49	9	5	ND	3	10	1	2	2	35	.12	.128	7	24	.27	83	.10	2	2.43	.02	.03	1	1
58+00E 4+00S	1	12	22	92	.1	49	11	274	2.86	16	5	ND	3	11	1	2	2	38	.22	.052	6	33	.39	74	.10	2	2.71	.02	.03	2	1
58+00E 4+25S	1	24	23	106	.1	40	13	328	3.24	13	5	ND	6	13	1	2	2	38	.18	.080	10	41	.59	137	.12	6	3.68	.02	.05	2	1
58+00E 4+50S	1	17	13	77	.4	36	10	319	3.05	12	5	ND	3	12	1	2	2	44	.19	.046	7	41	.45	96	.10	2	2.10	.02	.04	2	1
58+00E 4+75S	1	17	15	74	.1	42	13	606	3.06	10	5	ND	2	9	1	2	2	43	.10	.037	7	50	.41	102	.08	4	1.27	.02	.03	2	2
58+00E 5+00S	1	39	29	101	.1	53	16	349	3.79	18	5	ND	4	13	1	2	2	49	.20	.078	10	65	.65	150	.10	6	2.86	.02	.04	2	1
58+00E 5+25S	1	27	27	113	.1	64	17	546	4.22	17	5	ND	4	10	1	2	2	55	.15	.089	7	85	.68	128	.15	2	2.25	.03	.04	2	1
58+00E 5+50S	1	42	45	149	.1	127	26	732	5.13	15	5	ND	2	16	1	2	2	70	.31	.041	7	157	1.41	186	.13	6	2.51	.02	.04	2	2
58+00E 5+75S	1	34	58	173	.2	112	25	565	4.86	31	5	ND	4	11	1	2	2	65	.15	.057	9	138	1.25	175	.12	2	2.98	.02	.05	2	51
58+00E 6+00S	1	13	22	98	.3	33	11	437	3.10	19	5	ND	4	16	1	2	2	36	.29	.040	9	42	.38	142	.13	2	3.11	.02	.03	2	1
58+00E 6+25S	1	43	6	56	.6	10	1	91	.28	2	5	ND	1	123	1	4	2	8	6.13	.122	2	12	.42	202	.01	13	.31	.01	.02	1	1
58+00E 6+50S	1	24	21	120	.3	43	13	233	3.46	12	5	ND	7	11	1	2	2	45	.14	.031	15	51	.72	133	.07	2	1.82	.01	.05	2	1
58+00E 6+75S	1	13	7	37	.1	26	7	312	2.19	2	5	ND	2	9	1	2	2	35	.15	.085	4	35	.15	47	.10	5	2.16	.03	.02	1	1
58+00E 7+00S	1	15	14	60	.1	47	13	887	6.36	2	5	ND	4	7	1	2	2	55	.07	.115	5	83	.35	76	.14	5	4.40	.01	.03	1	1
58+00E 7+25S	1	30	28	105	.2	59	16	327	3.76	29	5	ND	4	11	1	2	2	45	.13	.087	8	68	.80	158	.09	2	2.58	.02	.04	2	138
58+00E 7+50S	1	16	22	88	.3	34	11	231	3.17	14	7	ND	5	12	1	2	2	44	.17	.047	13	41	.66	146	.09	2	2.16	.02	.05	2	1
58+00E 7+75S	1	11	27	77	.3	33	11	340	2.84	22	5	ND	3	8	1	2	2	37	.10	.078	5	33	.34	87	.11	2	2.44	.02	.04	2	2
58+00E 8+00S	1	9	17	73	.4	14	5	87	2.58	10	5	ND	3	9	1	2	2	38	.11	.053	5	19	.16	92	.10	2	3.05	.02	.03	2	2
58+00E 8+25S	1	66	2	56	1.2	19	7	1762	1.22	6	5	ND	1	89	1	3	2	18	4.29	.148	14	22	.54	365	.02	6	1.17	.02	.04	1	8
58+00E 8+50S	1	39	11	75	.5	28	11	825	2.93	8	5	ND	3	35	1	2	2	40	.88	.040	15	38	.77	180	.07	2	2.30	.03	.06	2	1
58+00E 8+75S	1	31	20	101	.1	38	18	219	3.25	22	5	ND	9	9	1	2	5	41	.13	.047	15	47	.67	122	.11	2	2.88	.02	.05	2	1
58+00E 9+00S	1	87	53	127	.3	112	31	812	5.53	48	5	ND	3	27	1	2	2	55	.82	.101	12	122	1.53	103	.07	2	1.71	.02	.05	2	16
58+00E 9+25S	1	34	24	79	.5	32	11	307	3.16	18	5	ND	6	23	1	2	2	30	.45	.074	17	34	.29	140	.15	2	4.43	.02	.04	2	1
58+00E 9+50S	1	21	21	140	.4	38	13	230	3.80	15	5	ND	5	17	1	2	2	47	.27	.060	11	54	.65	156	.10	5	4.12	.02	.05	2	1
58+00E 9+75S	1	31	21	103	.4	45	15	216	3.48	19	5	ND	4	12	1	3	2	44	.16	.052	11	55	.66	89	.07	2	1.70	.02	.03	2	1
58+00E 10+00S	1	22	18	93	.3	32	10	163	3.39	18	5	ND	4	10	1	2	2	48	.14	.044	9	45	.47	94	.08	3	1.41	.02	.04	2	1
58+00E 10+25S	1	7	15	75	.3	15	7	348	2.25	5	5	ND	3	10	1	2	2	36	.13	.072	7	23	.25	95	.08	3	1.46	.02	.05	2	1
58+00E 10+50S	1	12	16	106	.4	21	9	313	2.67	13	5	ND	3	11	1	2	2	38	.17	.091	8	29	.26	76	.08	2	1.95	.02	.04	2	2
58+50E 0+00S	1	167	205	375	.8	140	44	1257	8.00	85	5	ND	5	16	1	2	2	64	.31	.057	11	130	1.62	209	.10	5	2.15	.01	.05	4	23
59+00E 0+00S	1	55	97	244	.7	81	20	946	3.93	26	5	ND	4	29	1	2	3	44	.87	.041	12	87	.94	125	.08	2	2.23	.02	.05	3	3
59+00E 0+25S	1	24	54	195	.9	40	13	733	2.93	14	7	ND	3	17	1	2	2	37	.39	.039	6	56	.52	85	.11	5	2.58	.02	.03	2	1
59+00E 0+50S	1	65	70	165	.3	100	20	399	4.49	27	5	ND	6	11	1	2	2	60	.23	.020	14	137	1.80	76	.09	2	2.02	.01	.04	2	2
59+00E 0+75S	1	77	13	86	.6	27	8	501	1.76	5	5	ND	1	78	1	2	3	19	3.26	.090	7	40	.34	95	.03	2	1.54	.03	.03	2	1
59+00E 1+00S	1	22	15	159	.7	26	9	1188	2.21	6	5	ND	1	38	1	2	2	27	1.01	.045	7	30	.41	91	.09	3	2.34	.04	.04	2	1
STD C/AU-S	20	55	36	129	6.9	66	28	994	3.96	37	17	7	34	48	17	16	17	62	.48	.097	36	58	.88	177	.08	35	1.71	.06	.13	13	51

SAMPLE#	Mc PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mo %	Ba PPM	Ti %	B PPM	Al %	Na %	I %	K PPM	Au1 PPM
59+00E 1+25S	1	90	55	201	.6	131	32	533	6.26	21	5	ND	6	33	1	2	2	58	.72	.038	10	109	1.34	211	.14	6	3.89	.03	.06	1	6
59+00E 1+50S	1	140	83	201	.6	109	36	1415	5.96	35	5	ND	4	36	1	2	2	60	.95	.039	18	114	1.61	195	.11	2	2.47	.02	.07	1	1
59+00E 1+75S	1	77	72	184	1.7	60	15	1381	2.82	14	5	ND	1	120	2	2	2	34	2.47	.081	7	61	.84	111	.04	2	1.77	.02	.03	1	1
59+00E 2+00S	1	86	114	287	.6	94	27	776	5.44	57	5	ND	3	21	1	2	2	58	.47	.055	11	103	1.22	157	.11	2	2.91	.02	.05	1	3
59+00E 2+25S	1	20	35	242	.2	63	19	253	4.51	29	5	ND	3	15	1	2	2	59	.26	.088	8	86	1.01	148	.14	5	3.49	.02	.03	1	1
59+00E 2+50S	1	19	35	104	.1	49	15	296	4.09	19	5	ND	1	16	1	2	2	56	.24	.032	10	73	.86	130	.15	2	2.85	.02	.02	1	1
59+00E 2+75S	1	25	35	164	.2	68	21	449	4.29	26	5	ND	3	11	1	2	2	56	.20	.050	9	91	.94	121	.14	2	2.69	.01	.03	1	1
59+00E 3+00S	1	73	121	229	.6	102	26	1207	5.26	49	5	ND	2	17	1	2	2	66	.26	.072	12	120	1.40	156	.11	2	2.43	.02	.04	1	8
59+00E 3+25S	1	47	141	186	.2	71	25	1411	5.06	69	5	ND	1	14	1	2	2	51	.21	.076	10	69	.70	123	.10	2	2.57	.02	.03	1	16
59+00E 3+50S	3	89	242	354	.1	107	43	658	8.61	169	5	ND	6	17	1	2	2	67	.26	.092	13	93	1.15	237	.11	4	3.76	.02	.06	1	17
59+00E 3+75S	1	41	52	182	.1	49	16	498	3.98	45	5	ND	3	11	1	2	2	50	.17	.050	12	51	.67	138	.10	2	2.27	.02	.04	1	4
59+00E 4+00S	1	9	22	119	.1	23	9	178	3.40	20	5	ND	2	12	1	2	2	41	.19	.064	6	27	.25	98	.15	3	4.29	.02	.02	1	1
59+00E 4+25S	1	48	47	142	.1	88	22	574	4.58	31	5	ND	4	17	1	2	2	50	.25	.088	8	81	.96	129	.12	3	3.22	.02	.05	1	1
59+00E 4+50S	1	43	14	203	.1	112	28	304	4.78	34	5	ND	2	14	1	2	2	38	.20	.043	8	56	.28	118	.06	2	2.11	.02	.04	1	1
59+00E 4+75S	1	44	27	103	.1	68	12	951	3.11	14	5	ND	4	23	1	2	3	35	.44	.044	15	37	.55	119	.14	2	3.55	.04	.05	1	5
59+00E 5+00S	1	24	25	126	.1	39	12	600	3.09	15	5	ND	2	10	1	2	2	37	.13	.084	6	33	.39	105	.13	2	3.38	.03	.04	1	1
59+00E 5+25S	1	7	19	66	.2	22	8	630	2.39	13	5	ND	1	10	1	2	2	41	.13	.036	3	27	.24	72	.10	2	1.24	.03	.02	1	3
59+00E 5+50S	1	23	23	106	.1	247	40	312	5.47	24	5	ND	1	10	1	2	2	53	.13	.042	9	219	.74	86	.10	5	2.34	.02	.04	1	1
59+00E 5+75S	1	17	22	150	.1	42	12	256	4.54	20	5	ND	4	12	1	2	3	68	.18	.043	14	58	.79	116	.12	3	2.42	.01	.04	1	1
59+00E 6+00S	1	21	41	112	.2	53	19	769	4.43	31	5	ND	2	12	1	2	2	47	.15	.109	7	51	.45	94	.13	3	3.36	.02	.03	1	2
59+00E 6+25S	1	24	20	72	.3	27	9	1146	2.65	18	5	ND	1	26	1	2	2	35	.72	.045	11	27	.31	130	.10	2	2.72	.05	.03	1	3
59+00E 6+50S	1	23	9	56	1.0	21	6	264	2.35	17	5	ND	1	26	1	2	2	26	.75	.034	13	22	.23	115	.12	5	3.71	.03	.02	1	1
59+00E 6+75S	1	27	30	188	.2	35	13	180	4.35	17	5	ND	5	26	1	2	2	53	.49	.030	15	40	.56	269	.07	2	2.73	.03	.05	1	7
59+00E 7+00S	1	13	22	77	.1	29	9	116	3.82	14	5	ND	2	12	1	2	2	48	.19	.038	7	39	.29	106	.11	3	2.15	.02	.04	1	1
59+00E 7+25S	1	17	28	107	.1	42	15	261	4.24	19	5	ND	2	13	1	2	2	58	.17	.068	8	57	.57	139	.14	2	3.61	.02	.03	1	3
59+00E 7+50S	1	70	13	55	1.3	22	7	1111	2.04	16	5	ND	1	38	1	2	2	27	1.11	.092	15	34	.34	198	.06	5	2.59	.05	.02	1	4
59+00E 7+75S	1	22	30	80	.1	34	10	145	3.69	26	5	ND	3	12	1	2	2	45	.18	.046	7	44	.49	111	.09	2	2.77	.02	.03	1	9
59+00E 8+00S	1	23	22	113	.1	44	12	206	4.00	21	5	ND	4	12	1	2	2	58	.14	.037	16	52	.75	181	.09	2	2.71	.02	.05	2	16
59+00E 8+25S	1	15	23	121	.3	43	13	460	3.54	16	5	ND	3	15	1	2	2	48	.22	.046	9	52	.54	156	.10	2	3.16	.02	.05	1	1
59+00E 8+50S	1	15	32	121	.6	15	7	167	2.47	33	5	ND	3	17	1	2	2	33	.25	.054	9	24	.23	101	.10	3	2.80	.04	.03	1	1
59+00E 8+75S	1	17	18	87	.1	23	9	249	2.36	11	5	ND	2	21	1	2	2	31	.39	.050	12	26	.35	109	.11	2	2.61	.04	.03	1	1
59+00E 9+00S	1	68	51	113	.1	81	27	1073	5.64	53	5	ND	4	30	1	2	2	53	.62	.072	19	85	1.10	192	.10	4	2.05	.03	.06	1	1
59+00E 9+25S	1	19	17	139	.1	40	14	316	4.03	15	5	ND	6	14	1	2	2	53	.20	.053	18	53	.93	215	.09	2	3.02	.02	.09	1	1
59+00E 9+50S	1	36	25	153	.9	51	16	397	3.86	17	7	ND	11	18	1	2	2	48	.34	.070	13	50	.73	267	.12	4	4.20	.02	.12	1	1
59+00E 9+75S	1	17	68	137	.5	34	15	467	3.35	23	5	ND	6	11	1	2	2	43	.16	.160	13	38	.57	125	.10	4	3.39	.02	.06	1	1
59+00E 10+00S	1	11	20	95	.3	27	8	167	3.11	18	5	ND	3	17	1	2	2	44	.27	.160	9	34	.39	97	.12	3	3.16	.02	.04	1	2
STD C/AU-S	20	58	42	127	7.0	67	29	968	3.94	41	19	7	33	46	16	15	20	60	.48	.094	34	54	.88	170	.08	36	1.71	.06	.13	13	47

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Hg %	Ba PPM	Ti %	F PPM	Al %	Na %	K %	W PPM	Au# PPB
59+50E 0+00S	1	124	104	269	.5	112	29	1098	5.84	31	5	ND	4	24	1	2	2	56	.65	.054	13	110	1.37	204	.11	5	2.55	.02	.05	1	3
60+00E 2+25S	1	43	39	159	.3	69	20	694	3.81	32	5	ND	2	8	1	2	2	43	.17	.094	6	80	.91	85	.10	4	1.90	.01	.03	1	2
60+00E 2+50S	1	76	9	50	.6	29	8	1280	1.53	6	5	ND	1	104	1	2	2	26	4.06	.129	6	25	.31	351	.03	9	1.10	.02	.01	1	1
60+00E 2+75S	1	14	19	70	.6	23	8	129	3.31	14	5	ND	2	15	1	3	2	48	.29	.037	6	44	.30	138	.14	5	3.34	.02	.02	1	1
60+00E 3+00S	1	25	39	170	.4	44	18	515	3.70	27	5	ND	3	9	1	3	2	38	.10	.092	7	52	.49	126	.12	4	3.96	.02	.02	1	2
60+00E 3+25S	1	24	32	175	.3	54	20	649	4.23	29	5	ND	3	12	1	2	3	47	.18	.073	6	68	.65	99	.10	4	3.08	.01	.03	1	3
60+00E 3+50S	1	27	48	173	.6	53	17	303	4.26	52	5	ND	3	10	1	2	2	50	.14	.079	4	62	.61	84	.11	5	2.55	.02	.03	1	3
60+00E 3+75S	1	23	14	94	.9	36	9	836	2.75	16	5	ND	3	22	1	3	4	30	.57	.072	13	39	.41	169	.15	5	4.31	.03	.02	1	2
60+00E 4+00S	1	34	24	147	.3	49	15	984	3.67	20	5	ND	4	10	1	2	2	43	.12	.110	7	50	.58	137	.10	6	3.04	.02	.04	1	1
60+00E 4+25S	1	9	16	54	.3	11	5	401	2.13	13	5	ND	1	5	1	2	2	32	.06	.097	4	14	.14	47	.09	4	1.33	.02	.03	1	1
60+00E 4+50S	1	48	43	141	.1	49	20	889	4.37	46	5	ND	3	10	1	2	2	51	.14	.051	9	53	.57	132	.07	6	2.09	.01	.03	1	5
60+00E 4+75S	1	37	60	130	.2	56	18	572	4.30	44	5	ND	3	12	1	2	2	53	.22	.048	4	61	.59	95	.07	3	1.62	.02	.03	1	24
60+00E 5+00S	1	139	39	185	.1	202	52	253	7.73	99	5	ND	2	16	1	2	2	54	.10	.068	6	137	1.07	151	.03	5	2.70	.01	.03	1	13
60+00E 5+25S	1	18	23	72	.3	33	10	178	2.91	17	5	ND	2	11	1	2	2	39	.14	.065	4	33	.26	69	.10	5	2.14	.02	.02	1	260
60+00E 5+50S	1	54	31	103	.2	76	17	354	3.79	24	5	ND	3	24	1	2	2	39	.50	.047	12	71	.94	79	.11	7	2.17	.02	.03	1	1
60+00E 5+75S	1	54	45	102	.6	63	15	538	3.62	16	5	ND	3	31	1	2	2	38	.68	.041	16	53	.63	91	.10	7	2.66	.03	.03	1	6
60+00E 6+00S	1	16	19	112	.4	55	16	160	4.06	14	5	ND	2	16	1	2	2	49	.27	.039	6	60	.52	88	.09	5	2.42	.03	.02	1	1
60+00E 6+25S	1	23	17	90	.5	46	11	691	3.03	13	5	ND	2	22	1	2	2	41	.44	.037	8	50	.60	129	.10	2	2.51	.03	.03	1	1
60+00E 6+50S	1	37	28	100	.6	58	15	398	3.94	24	6	ND	5	19	1	2	2	42	.36	.068	13	59	.60	159	.15	6	4.31	.03	.04	1	1
60+00E 6+75S	1	29	18	91	1.4	35	9	453	2.78	19	5	ND	3	16	1	2	2	30	.26	.058	10	33	.28	134	.14	6	3.78	.04	.03	1	1
60+00E 7+00S	1	98	2091	422	2.2	85	21	994	4.64	143	5	ND	4	30	1	2	2	49	.70	.069	12	81	.95	250	.09	5	2.99	.02	.04	1	39
60+00E 7+25S	1	79	63	82	1.0	46	13	351	2.98	32	5	ND	1	33	1	2	2	36	.86	.048	10	48	.50	189	.08	6	2.55	.03	.02	1	5
60+00E 7+50S	1	65	11	59	.5	22	6	407	1.88	7	5	ND	1	26	1	2	2	35	.60	.054	12	16	.21	63	.08	5	1.88	.05	.02	1	2
60+00E 7+75S	1	21	18	130	.2	25	12	331	3.85	17	6	ND	6	13	1	3	2	47	.18	.096	10	38	.55	150	.10	3	3.33	.02	.05	1	1
60+00E 8+00S	1	10	21	74	.3	29	11	236	3.04	16	5	ND	2	14	1	2	2	42	.20	.085	4	46	.41	77	.08	2	2.55	.02	.03	1	1
60+00E 8+25S	1	32	38	91	.1	49	12	217	3.51	37	5	ND	5	10	1	2	2	46	.11	.091	11	61	.72	118	.11	4	3.17	.02	.03	1	3
60+00E 8+50S	1	31	12	84	.3	25	10	2713	2.49	9	5	ND	1	83	1	2	2	24	3.05	.145	9	31	.65	292	.03	7	1.45	.02	.04	1	1
60+00E 8+75S	1	34	37	130	.3	58	18	300	3.90	31	5	ND	5	19	1	2	2	44	.46	.069	11	61	.69	151	.11	6	3.47	.02	.04	1	2
60+00E 9+00S	1	24	32	170	.3	59	18	256	4.48	36	5	ND	3	18	1	3	2	49	.33	.081	9	73	.69	155	.11	4	3.31	.02	.04	1	3
61+00E 3+75S	1	18	13	141	.9	22	10	168	3.91	16	8	ND	3	14	1	2	2	48	.30	.183	9	36	.45	128	.11	4	4.13	.01	.04	1	2
61+00E 4+00S	1	44	60	148	.4	46	14	228	4.77	42	5	ND	4	7	1	2	2	52	.10	.046	8	61	.80	72	.07	2	1.85	.01	.03	1	8
61+00E 4+25S	1	16	24	80	.3	25	8	110	3.09	13	5	ND	2	23	1	2	2	35	.64	.027	9	30	.28	78	.09	5	3.42	.02	.02	1	1
61+00E 4+50S	1	51	24	265	.9	75	15	1042	3.25	20	8	ND	3	24	2	2	2	32	.63	.056	12	45	.50	66	.13	4	3.23	.02	.03	1	5
61+00E 4+75S	1	13	26	72	.1	33	14	337	3.07	22	5	ND	2	9	1	3	2	35	.11	.091	4	40	.21	65	.13	4	3.82	.02	.02	1	2
61+00E 5+00S	1	12	15	72	.2	19	8	255	3.60	16	5	ND	4	7	1	2	2	52	.08	.163	6	33	.36	74	.11	5	2.48	.02	.03	1	1
61+00E 5+25S	2	36	35	72	1.8	57	15	444	3.38	30	41	3	9	22	1	27	6	38	.48	.053	6	66	.71	107	.11	9	3.15	.03	.10	9	1
STD C/AU-S	20	57	38	130	6.9	70	28	1002	3.96	39	20	7	32	48	17	15	19	62	.48	.099	37	57	.88	178	.08	35	1.71	.07	.12	12	49

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	R	Al	Na	F	W	Au#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
61+00E 5+50E	1	13	20	68	.1	22	9	155	3.25	10	5	ND	1	10	1	2	2	48	.13	.045	5	38	.31	7E	.10	2	2.84	.02	.02	1	2
61+00E 5+75S	1	38	29	119	.2	44	13	452	3.44	12	5	ND	7	16	1	3	2	37	.22	.070	13	37	.40	164	.14	2	4.45	.02	.05	1	3
61+00E 6+00S	1	17	26	68	.1	31	11	145	3.39	13	5	ND	2	9	1	2	2	45	.11	.076	6	42	.41	61	.12	4	3.28	.03	.02	1	13
61+00E 6+25S	1	21	16	85	.5	29	9	917	2.58	14	5	ND	3	21	1	2	2	36	.35	.066	12	26	.39	125	.11	6	2.96	.04	.04	1	1
61+00E 6+50S	1	49	34	92	.4	53	14	312	3.51	18	5	ND	3	17	1	2	2	43	.28	.072	14	60	.59	111	.13	3	3.48	.03	.03	1	29
61+00E 6+75S	1	36	11	60	.9	15	5	286	1.88	7	5	ND	1	31	1	2	2	33	.69	.062	16	16	.26	91	.08	2	2.12	.05	.02	1	1
61+00E 7+00S	1	14	8	76	.2	7	4	189	1.57	7	5	ND	1	22	1	2	2	24	.43	.039	6	8	.14	80	.09	3	2.01	.05	.01	1	1
61+00E 7+25S	1	103	21	76	.9	38	9	953	2.11	15	5	ND	1	43	1	2	2	26	1.23	.083	13	28	.42	185	.05	4	2.21	.04	.03	1	17
61+00E 7+50S	1	15	37	108	.2	24	12	247	3.89	30	5	ND	1	11	1	3	2	35	.17	.076	6	31	.22	107	.12	2	3.62	.02	.01	1	2
61+00E 7+75S	1	41	76	134	.9	39	11	1543	2.96	33	5	ND	1	21	1	2	2	35	.47	.074	13	24	.35	127	.13	4	3.00	.04	.03	1	1
61+00E 8+00S	1	25	25	112	.6	31	11	320	3.42	20	5	ND	4	22	1	2	2	39	.58	.071	14	34	.37	167	.14	6	4.50	.02	.03	1	1
61+00E 8+25S	1	43	155	265	.1	66	21	437	5.61	250	5	ND	2	11	1	2	2	57	.14	.050	12	67	.79	108	.08	2	2.15	.01	.04	1	6
61+00E 8+50S	1	11	13	43	.3	7	4	88	2.43	6	5	ND	1	11	1	2	2	37	.16	.029	6	17	.15	48	.11	2	2.27	.03	.02	1	2
61+00E 8+75S	1	36	37	110	.3	47	16	577	3.79	32	5	ND	5	15	1	2	2	48	.22	.063	16	58	.89	144	.10	2	2.41	.02	.06	1	10
62+00E 4+25S	1	88	113	193	.2	92	29	1266	5.05	61	5	ND	3	19	1	2	2	51	.67	.083	13	89	1.19	155	.09	3	2.18	.01	.04	1	30
62+00E 4+50S	1	27	19	121	.4	65	16	400	3.88	18	5	ND	3	11	1	2	2	52	.16	.124	13	94	1.21	94	.08	2	2.09	.01	.04	1	1
62+00E 4+75S	1	45	35	115	.4	63	17	504	3.25	13	5	ND	2	36	1	3	2	40	.90	.065	13	87	1.14	112	.06	2	1.60	.01	.04	1	3
62+00E 5+00S	1	48	21	185	2.0	30	8	1349	2.20	11	5	ND	1	62	1	2	2	26	2.27	.074	5	43	.62	159	.05	5	1.65	.02	.03	1	2
62+00E 5+25S	1	16	20	50	.2	14	4	1073	1.87	8	5	ND	1	14	1	2	2	28	.31	.073	9	16	.21	81	.10	4	2.00	.03	.02	1	1
62+00E 5+50S	1	29	32	169	.3	60	19	256	4.32	25	5	ND	5	16	1	2	2	53	.22	.046	13	75	.98	140	.09	2	2.88	.01	.03	1	3
62+00E 5+75S	1	13	33	122	.2	30	13	221	4.81	29	5	ND	3	9	1	2	2	55	.11	.100	5	51	.35	80	.14	2	3.44	.02	.02	1	1
62+00E 6+00S	1	49	25	162	.2	98	26	531	5.25	32	5	ND	4	22	1	2	2	65	.35	.049	12	118	1.43	215	.08	2	3.02	.01	.05	1	1
62+00E 6+25S	1	18	14	69	.6	33	9	264	2.87	17	5	ND	5	22	1	3	3	32	.49	.064	14	35	.44	118	.15	4	4.23	.03	.04	1	1
62+00E 6+50S	1	14	19	131	.6	27	8	442	2.74	11	5	ND	2	29	1	2	2	30	.64	.035	12	30	.45	136	.11	2	3.08	.04	.03	1	2
62+00E 6+75S	1	24	13	68	.8	15	6	313	2.07	6	5	ND	1	38	1	2	2	29	.93	.056	10	17	.34	138	.08	5	2.30	.05	.03	1	1
62+00E 7+00S	1	29	22	130	.3	27	8	203	2.77	8	5	ND	4	32	1	2	2	35	.74	.028	16	30	.54	201	.05	4	1.94	.02	.04	1	1
62+00E 7+25S	1	28	15	57	.6	13	7	348	2.02	12	5	ND	1	24	1	2	2	30	.51	.044	10	16	.18	127	.08	2	2.41	.05	.02	1	2
63+00E 4+50S	1	85	85	195	.5	111	30	1189	5.43	85	9	ND	5	67	1	2	2	53	5.34	.090	11	114	1.98	136	.09	3	1.62	.01	.06	1	28
63+00E 4+75S	1	23	34	114	.3	52	14	196	4.03	29	5	ND	2	15	1	2	2	52	.23	.058	7	68	.69	92	.11	6	2.40	.01	.03	1	1
63+00E 5+00S	1	41	51	160	.6	75	21	284	4.75	37	5	ND	5	13	1	2	2	52	.18	.060	10	81	1.04	169	.08	3	2.88	.01	.04	1	1
63+00E 5+25S	1	13	23	77	.5	28	10	312	2.68	15	5	ND	2	7	1	3	2	35	.09	.073	4	35	.29	60	.07	4	2.07	.02	.02	1	5
63+00E 5+50S	1	15	25	158	.2	33	10	183	3.75	14	5	ND	3	15	1	2	2	48	.23	.029	10	50	.60	141	.10	4	2.52	.01	.02	1	1
63+00E 5+75S	1	70	9	59	.5	16	6	804	1.16	2	5	ND	1	72	1	2	2	20	2.68	.140	8	32	.31	136	.03	6	1.23	.03	.01	1	1
63+00E 6+00S	1	29	17	106	.9	17	6	187	2.20	11	5	ND	2	29	1	2	2	23	.77	.059	13	20	.24	170	.12	3	3.49	.03	.03	1	2
63+00E 6+25S	1	20	17	78	.6	23	8	224	2.75	23	5	ND	2	20	1	2	2	36	.38	.050	5	28	.25	118	.09	2	2.95	.05	.02	1	1
63+00E 6+50S	1	14	10	67	.6	13	5	350	1.90	8	5	ND	1	21	1	2	2	30	.41	.047	7	12	.20	90	.10	6	2.14	.05	.02	1	1
STD C/AU-S	21	56	42	129	6.9	67	29	996	3.95	41	20	8	33	47	16	15	22	62	.48	.098	38	58	.88	176	.08	33	1.72	.06	.13	12	52

C.E.C. ENGINEERING PROJECT-TWIN P86-14 FILE# 86-3645

PAGE 8

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	F PPM	Al %	Na %	K %	W PPM	Au1 PPB
64+00E 4+75S	1	35	13	78	1.0	37	10	1325	2.38	13	5	ND	3	27	1	2	2	27	.51	.035	13	40	.56	182	.11	4	3.08	.04	.05	1	1
64+00E 5+00S	1	9	15	95	.3	20	5	105	3.06	9	5	ND	3	15	1	2	2	47	.23	.089	6	33	.38	86	.10	3	3.12	.02	.02	1	1
64+00E 5+25S	1	12	26	94	.2	34	10	196	3.42	24	5	ND	2	6	1	2	2	42	.07	.058	4	38	.36	59	.10	5	1.99	.02	.02	1	1
64+00E 5+50S	1	41	44	168	.2	101	25	309	5.06	38	5	ND	2	11	1	2	2	53	.18	.077	7	92	1.01	120	.09	2	2.66	.01	.03	1	2
78+00E 5+00S	1	19	62	179	.5	66	16	425	3.91	78	5	ND	2	9	1	2	2	40	.11	.097	5	38	.32	130	.09	5	2.33	.02	.03	1	1
78+00E 5+25S	1	13	38	226	.6	41	12	887	3.17	38	5	ND	1	9	1	2	2	31	.12	.080	2	27	.20	112	.10	3	2.66	.02	.03	1	1
78+00E 5+50S	1	11	81	159	.9	29	14	474	3.50	76	5	ND	1	10	1	2	2	35	.15	.096	3	27	.16	75	.09	3	2.32	.02	.02	1	88
78+00E 5+75S	1	89	124	569	.7	85	20	1080	4.34	69	6	ND	1	43	2	2	2	37	1.19	.106	7	81	.90	184	.04	3	1.68	.02	.03	1	11
78+00E 6+00S	1	10	36	146	.3	23	10	529	3.11	38	5	ND	2	11	1	2	2	34	.16	.128	3	26	.17	98	.11	4	3.12	.02	.03	1	1
78+00E 6+25S	1	6	25	96	.3	19	8	556	2.14	21	5	ND	1	11	1	2	2	27	.17	.088	3	16	.11	83	.08	6	2.20	.02	.03	1	1
78+00E 6+50S	1	55	67	194	.3	86	21	277	4.20	69	5	ND	1	9	1	2	2	36	.10	.068	5	44	.38	144	.08	4	2.51	.02	.03	1	10
78+00E 6+75S	1	39	50	222	.4	78	20	340	4.87	63	5	ND	2	14	1	2	2	53	.25	.091	8	84	.87	250	.12	4	3.16	.02	.05	1	1
78+00E 7+00S	1	27	30	102	.7	47	13	344	4.01	44	7	ND	3	8	1	2	2	45	.11	.113	9	53	.57	124	.10	4	2.69	.01	.05	1	1
78+00E 7+25S	1	16	41	121	.2	47	14	154	4.28	52	5	ND	2	12	1	2	2	48	.24	.171	8	57	.44	102	.10	6	3.41	.02	.03	1	1
78+00E 7+50S	1	10	13	79	.6	19	6	95	2.48	10	5	ND	3	9	1	3	2	35	.12	.065	7	23	.23	86	.10	3	2.57	.02	.04	1	1
78+00E 7+75S	1	17	20	60	.2	23	9	149	1.95	10	5	ND	2	8	1	2	2	25	.14	.018	7	22	.24	72	.07	3	1.26	.02	.03	1	2
78+00E 8+00S	1	34	23	75	.4	42	10	581	2.72	15	7	ND	1	51	1	2	2	29	1.54	.076	12	45	.74	189	.05	5	1.44	.02	.06	1	1
78+00E 8+25S	1	26	23	80	.4	54	15	259	3.46	31	5	ND	4	11	1	2	2	39	.16	.076	15	50	.53	108	.11	2	2.25	.01	.04	1	2
79+00E 5+00S	1	23	37	132	.7	53	12	671	3.03	45	5	ND	1	11	1	2	2	30	.19	.102	5	29	.25	140	.07	4	1.98	.02	.03	1	1
79+00E 5+25S	1	56	148	307	.6	70	20	1270	4.69	113	5	ND	1	21	1	2	2	37	.52	.060	4	51	.57	151	.07	2	2.08	.02	.04	1	11
79+00E 5+50S	1	82	122	209	.7	89	26	972	4.95	134	5	ND	5	23	1	2	3	45	.66	.094	16	80	1.28	143	.08	3	1.55	.02	.06	1	53
79+00E 5+75S	1	31	51	234	.4	102	24	419	4.73	37	5	ND	1	10	1	2	2	66	.19	.058	4	145	1.32	110	.13	2	2.27	.01	.03	1	1
79+00E 6+00S	1	7	26	88	.7	12	8	267	3.40	27	5	ND	2	10	1	2	2	48	.12	.234	2	23	.11	69	.17	2	4.28	.02	.02	1	2
79+00E 6+25S	1	27	26	199	.5	45	14	1686	3.48	28	5	ND	4	25	1	2	2	42	.56	.035	13	44	.85	251	.09	5	2.37	.03	.07	1	1
79+00E 6+50S	1	12	22	86	.4	22	8	189	2.64	14	5	ND	2	10	1	2	2	36	.14	.099	6	39	.32	99	.08	5	2.10	.02	.03	1	1
79+00E 6+75S	1	24	13	98	1.0	34	8	264	2.56	25	5	ND	2	24	1	2	2	29	.61	.046	11	29	.41	172	.11	2	3.09	.03	.05	1	2
79+00E 7+00S	1	5	5	71	.3	10	6	488	1.53	5	5	ND	1	10	1	2	2	24	.14	.081	3	12	.09	60	.08	6	1.95	.03	.01	1	1
79+00E 7+25S	1	15	23	104	.1	30	10	194	2.84	18	5	ND	2	9	1	2	2	38	.11	.035	6	33	.35	86	.09	3	1.38	.02	.02	1	1
79+00E 7+50S	1	24	18	62	.3	29	9	364	2.29	14	5	ND	2	71	1	2	2	25	2.53	.051	5	34	.56	183	.04	6	.97	.01	.03	1	1
79+00E 7+75S	1	18	12	60	.1	35	9	194	2.53	10	5	ND	4	10	1	2	2	33	.15	.091	12	44	.48	65	.09	2	1.52	.01	.03	1	2
79+00E 8+00S	1	20	29	67	.5	44	17	151	3.41	17	5	ND	5	10	1	2	2	37	.13	.089	6	46	.37	87	.12	2	3.38	.02	.05	2	1
79+00E 8+25S	1	13	11	81	.3	26	9	158	2.44	11	5	ND	2	11	1	2	2	34	.13	.071	7	23	.28	116	.11	4	2.81	.03	.04	1	1
79+00E 8+50S	1	12	18	74	.1	44	11	282	3.10	13	5	ND	1	12	1	2	2	47	.23	.081	9	61	.61	92	.12	2	2.26	.02	.03	1	1
79+00E 8+75S	1	37	27	99	.5	71	16	1135	3.83	20	5	ND	5	31	1	2	2	43	.47	.029	15	77	.88	335	.13	3	2.81	.03	.06	1	1
79+00E 9+00S	1	7	13	70	.4	14	6	120	1.73	3	5	ND	2	12	1	2	2	27	.21	.063	7	18	.21	96	.08	6	1.76	.03	.03	1	1
79+00E 9+25S	1	49	11	78	.5	38	10	1193	2.57	7	5	ND	3	36	1	2	2	24	.71	.044	14	28	.43	224	.12	4	2.82	.04	.06	1	2
STD C/AU-S	20	58	38	130	6.7	70	29	1001	3.95	39	17	7	32	48	16	15	19	62	.48	.101	35	58	.88	177	.08	33	1.72	.07	.13	13	53

C.E.C. ENGINEERING PROJECT - TWIN F86-14 FILE # 86-3645

PAGE 9

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Au PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mo %	Ba PPM	Ti %	R PPM	Al %	Na %	K %	W PPM	Au# PPB
80+00E 5+00S	2	75	162	283	.1	110	35	1863	9.89	187	5	ND	3	11	1	2	6	61	.11	.094	6	92	.79	176	.05	9	1.38	.01	.03	1	17
80+00E 5+25S	1	41	83	244	.2	75	21	566	5.42	91	5	ND	1	8	1	2	5	46	.09	.127	6	71	.59	93	.08	2	2.52	.01	.02	1	9
80+00E 5+50S	1	38	41	141	.6	59	14	281	4.09	45	5	ND	6	22	1	2	3	44	.47	.044	14	60	.67	271	.11	4	3.30	.02	.05	1	5
80+00E 5+75S	1	36	47	75	1.4	32	11	338	2.87	63	5	ND	2	31	1	3	3	23	.88	.056	10	32	.39	158	.10	7	3.08	.03	.03	2	13
80+00E 6+00S	1	16	18	102	.6	21	7	231	2.21	20	5	ND	2	25	1	2	2	26	.65	.038	10	19	.28	153	.10	7	2.74	.03	.03	1	1
80+00E 6+25S	1	60	29	85	.7	70	15	575	3.05	14	5	ND	1	46	1	2	4	34	1.28	.075	9	99	1.00	241	.06	5	2.27	.02	.04	1	2
80+00E 6+50S	1	80	16	71	.7	46	10	939	1.89	10	5	ND	1	61	1	2	2	24	2.08	.087	9	56	.60	206	.04	7	1.59	.02	.03	1	1
80+00E 6+75S	1	49	14	83	.5	27	8	663	2.15	9	5	ND	1	46	1	2	3	28	1.17	.058	8	28	.41	155	.07	2	1.90	.04	.03	1	1
80+00E 7+00S	1	17	19	118	.3	41	14	255	3.60	18	5	ND	3	17	1	2	3	50	.26	.048	10	52	.59	169	.12	5	2.68	.02	.05	1	1
80+00E 7+25S	1	22	14	89	.2	30	10	232	2.86	13	5	ND	4	18	1	2	2	37	.34	.101	9	35	.34	129	.11	2	3.33	.02	.04	1	1
80+00E 7+50S	1	19	14	61	.3	33	9	284	2.70	13	5	ND	3	21	1	2	3	34	.41	.065	6	41	.33	106	.09	7	2.92	.03	.04	1	2
80+00E 7+75S	1	13	9	70	.1	21	9	155	2.64	13	5	ND	4	11	1	2	4	35	.16	.187	9	26	.33	78	.14	3	3.37	.02	.04	1	1
80+00E 8+00S	1	5	13	60	.1	11	6	121	2.22	14	5	ND	2	10	1	3	2	34	.14	.197	3	18	.13	69	.12	2	2.61	.02	.02	1	1
80+00E 8+25S	1	22	9	57	.1	33	11	156	2.52	12	5	ND	4	18	1	2	2	34	.23	.037	10	37	.50	134	.09	3	1.80	.03	.03	1	1
80+00E 8+50S	1	14	20	97	.1	31	10	157	2.86	15	5	ND	3	15	1	2	2	40	.20	.091	9	41	.47	134	.09	4	2.16	.02	.03	1	1
80+00E 8+75S	1	16	15	57	.2	29	9	164	3.01	16	5	ND	3	21	1	2	2	37	.40	.139	11	34	.38	135	.12	5	3.38	.03	.04	1	1
80+00E 9+00S	1	43	26	90	.1	81	19	388	3.97	26	5	ND	5	20	1	2	3	53	.31	.035	23	110	1.33	92	.13	8	1.75	.01	.07	1	2
80+00E 9+25S	1	24	16	102	.2	55	16	293	3.22	12	5	ND	5	12	1	2	3	44	.19	.090	18	74	.86	115	.10	4	2.16	.01	.05	1	1
80+00E 9+50S	1	19	16	109	.2	33	12	401	2.93	13	5	ND	4	12	1	2	5	44	.16	.095	12	45	.55	167	.09	3	2.21	.02	.05	1	1
80+00E 9+75S	1	13	18	83	.4	26	10	157	2.97	12	5	ND	4	15	1	2	4	38	.20	.108	9	36	.42	143	.11	4	3.20	.02	.04	1	1
80+00E 10+00S	1	30	11	53	.7	23	6	496	1.94	7	5	ND	2	31	1	2	2	23	.61	.037	18	28	.32	205	.09	4	2.44	.04	.04	1	1
80+00E 10+25S	1	29	19	86	.1	44	13	301	3.33	14	5	ND	2	36	1	2	2	36	.71	.039	12	51	.75	267	.09	2	2.69	.03	.04	1	3
80+00E 10+50S	1	33	18	72	.7	31	8	368	2.20	9	5	ND	2	39	1	2	2	28	.68	.049	9	29	.38	205	.10	2	2.52	.05	.04	1	1
81+00E 5+25S	1	47	36	148	.4	49	16	1349	3.39	55	5	ND	4	38	1	2	3	40	1.04	.096	12	48	.67	300	.08	8	1.92	.07	.12	1	1
81+00E 5+50S	1	10	14	60	.2	16	7	130	2.45	13	5	ND	3	12	1	2	2	30	.14	.157	5	24	.22	66	.13	2	3.99	.02	.02	1	1
81+00E 5+75S	1	7	10	50	.1	10	8	200	2.58	8	5	ND	2	14	1	3	3	41	.16	.120	3	20	.15	30	.11	3	2.33	.03	.02	2	1
81+00E 6+00S	1	50	45	97	.1	102	22	341	4.50	28	5	ND	6	16	1	2	3	61	.27	.063	14	133	1.60	90	.15	3	1.98	.01	.04	1	3
81+00E 6+25S	1	33	27	81	.6	59	14	419	3.49	34	5	ND	5	21	1	2	4	38	.41	.044	13	62	.68	230	.14	2	3.48	.03	.05	1	1
81+00E 6+50S	1	43	13	85	.6	33	11	795	2.89	17	5	ND	1	46	1	2	4	34	1.12	.055	11	35	.51	232	.05	7	1.93	.02	.05	1	1
81+00E 6+75S	1	11	17	92	.3	31	9	152	3.36	18	5	ND	3	12	1	2	3	47	.17	.085	8	48	.50	77	.10	3	1.86	.01	.04	1	2
81+00E 7+00S	1	23	17	96	.2	50	13	192	3.82	19	5	ND	4	20	1	2	3	47	.36	.061	11	63	.72	168	.12	3	3.40	.02	.04	1	1
81+00E 7+25S	1	18	18	104	.2	55	15	248	3.78	17	5	ND	3	14	1	2	2	51	.20	.124	9	73	.79	116	.10	7	2.26	.01	.04	1	1
81+00E 7+50S	1	22	32	88	.2	39	13	267	4.31	22	5	ND	5	8	1	2	2	50	.10	.118	11	64	.74	61	.09	2	1.89	.01	.04	1	1
81+00E 7+75S	1	29	15	66	.6	25	8	1049	2.16	8	5	ND	1	41	1	2	2	30	.81	.047	13	24	.42	158	.08	6	2.13	.04	.04	1	1
81+00E 8+00S	1	50	8	37	.6	11	3	292	1.21	6	5	ND	1	70	1	2	2	21	1.87	.094	13	11	.25	139	.03	2	1.42	.04	.02	1	1
81+00E 8+25S	1	125	17	91	1.4	42	11	1517	1.86	8	8	ND	1	89	1	2	2	25	2.57	.088	25	38	.51	270	.04	3	1.76	.02	.04	1	1
STD C/AU-S	21	57	40	133	6.8	68	30	1017	3.96	43	18	7	33	49	17	16	19	63	.47	.099	36	58	.88	183	.08	34	1.72	.07	.13	14	51

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Ri	V	Ca	P	La	Cr	Mo	Ba	Ti	P	Al	Na	I	K	Au
PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
81+00E 8+50E	1	61	20	74	.4	47	9	648	2.66	9	6	ND	1	112	1	2	2	32	2.13	.124	16	61	.75	244	.04	4	2.12	.03	.05	1	1
81+00E 8+75S	1	34	14	55	.6	28	6	204	2.43	10	5	ND	2	32	1	2	2	26	.58	.045	15	31	.31	181	.11	3	2.74	.04	.05	1	1
81+00E 9+00S	1	69	11	60	.4	25	8	371	2.52	8	5	ND	1	52	1	2	2	35	1.27	.055	20	25	.36	275	.08	5	2.45	.04	.05	1	1
81+00E 9+25S	1	24	30	67	.5	31	8	588	2.64	11	5	ND	2	36	1	2	2	35	.73	.049	12	31	.44	212	.09	2	2.30	.06	.05	1	1
81+00E 9+50S	1	31	14	65	.1	32	9	478	2.72	9	5	ND	3	27	1	2	2	32	.55	.031	17	39	.60	186	.09	7	1.90	.03	.05	1	1
81+00E 9+75S	1	30	6	64	.1	26	7	572	2.52	4	5	ND	4	26	1	2	2	30	.51	.032	15	28	.44	217	.12	5	2.69	.04	.05	1	1
81+00E 10+00S	1	120	61	146	.1	190	37	592	7.03	21	5	ND	4	23	1	2	2	91	.44	.044	20	255	2.97	149	.18	3	3.07	.01	.06	1	10
82+00E 5+00S	1	29	31	155	.2	48	13	674	3.52	32	5	ND	5	19	1	2	2	45	.39	.035	16	48	.67	271	.10	2	2.61	.03	.06	1	1
82+00E 5+25S	1	29	29	108	.1	56	14	412	3.33	15	5	ND	5	20	1	2	2	44	.40	.044	16	65	.86	146	.11	2	2.05	.02	.05	1	1
82+00E 5+50S	1	22	26	118	.3	42	11	441	3.04	10	5	ND	2	21	1	2	2	39	.50	.074	10	42	.50	147	.11	3	3.03	.04	.06	1	3
82+00E 5+75S	1	29	23	135	.3	71	14	200	3.99	17	5	ND	3	18	1	2	2	60	.31	.037	10	97	.97	158	.11	5	2.27	.02	.05	1	1
82+00E 6+00S	1	40	60	143	.1	91	20	289	4.61	22	5	ND	3	19	1	2	2	60	.35	.076	11	119	1.33	171	.14	2	3.21	.02	.04	1	1
82+00E 6+25S	1	16	4	46	.3	10	4	450	1.46	5	5	ND	1	49	1	2	2	24	1.28	.063	5	12	.22	97	.05	2	1.63	.05	.03	1	1
82+00E 6+50S	1	24	18	119	.1	51	14	367	3.21	10	5	ND	4	16	1	2	2	45	.23	.041	12	64	.72	124	.11	2	2.06	.02	.05	1	2
82+00E 6+75S	1	5	7	54	.1	9	3	191	1.51	2	5	ND	1	6	1	2	2	30	.07	.027	5	16	.12	43	.08	4	.93	.02	.02	1	1
82+00E 7+00S	3	134	257	360	.1	139	41	719	7.27	72	5	ND	3	12	1	2	2	71	.20	.050	9	144	1.72	159	.10	2	3.03	.01	.04	1	7
82+00E 7+25S	1	34	11	56	.7	25	6	278	1.98	4	5	ND	2	32	1	2	2	26	.57	.052	16	22	.30	111	.10	3	2.61	.06	.04	1	4
82+00E 7+50S	1	34	9	37	.4	17	6	756	1.75	4	5	ND	1	36	1	2	2	29	.71	.044	14	16	.25	86	.07	2	1.65	.06	.03	1	1
82+00E 7+75S	1	77	18	65	.3	43	10	444	2.95	10	5	ND	1	43	1	2	2	36	.81	.047	21	43	.55	216	.10	5	2.88	.05	.05	1	1
82+00E 8+00S	1	60	14	81	.3	41	10	506	2.63	8	7	ND	1	43	1	2	2	36	.98	.048	13	49	.63	169	.08	2	1.97	.05	.04	1	1
82+00E 8+25S	1	43	25	117	.1	92	17	250	5.05	16	5	ND	4	22	1	2	2	73	.31	.028	17	132	1.55	162	.13	4	2.61	.01	.04	1	1
82+00E 8+50S	1	20	6	44	.3	13	5	298	1.87	2	5	ND	1	37	1	2	2	35	.68	.048	8	15	.22	77	.08	6	1.61	.07	.02	1	1
82+00E 8+75S	1	36	10	66	.5	25	8	789	2.45	7	5	ND	3	46	1	2	2	29	1.01	.051	8	23	.39	235	.12	7	2.90	.06	.05	1	1
82+00E 9+00S	1	25	11	93	.6	40	10	269	2.88	14	5	ND	3	29	1	2	2	38	.59	.068	11	40	.50	197	.11	3	3.05	.04	.06	1	1
83+00E 5+00S	1	13	12	38	.8	15	5	142	2.10	18	5	ND	3	22	1	2	2	19	.64	.064	9	15	.18	90	.14	5	3.95	.04	.03	2	1
83+00E 5+25S	1	27	20	102	.5	39	10	259	3.05	12	5	ND	3	25	1	2	2	30	.72	.118	16	41	.41	161	.13	6	4.22	.04	.06	1	1
83+00E 5+50S	1	20	20	83	.7	27	8	635	2.23	12	5	ND	1	30	1	2	2	30	.69	.037	7	33	.37	132	.10	5	2.16	.04	.03	1	2
83+00E 5+75S	1	9	23	74	.2	33	9	229	3.65	15	5	ND	3	15	1	2	2	49	.30	.165	8	53	.46	69	.14	6	2.99	.02	.04	1	1
83+00E 6+00S	1	27	13	77	.1	61	14	221	3.71	19	5	ND	5	17	1	2	2	51	.25	.023	18	73	.89	112	.15	9	1.78	.01	.04	1	1
83+00E 6+25S	1	89	32	182	.7	70	17	1022	4.85	19	5	ND	10	35	1	2	2	55	.41	.089	17	51	.61	528	.15	5	5.57	.03	.12	1	1
83+00E 6+50S	1	7	11	49	.3	13	6	274	2.04	4	5	ND	2	12	1	2	2	33	.16	.105	7	18	.16	54	.10	4	2.31	.03	.03	1	1
83+00E 6+75S	1	51	33	125	.1	98	22	705	4.41	23	5	ND	6	32	1	2	2	54	.60	.123	19	112	1.43	72	.16	4	1.49	.02	.04	1	6
83+00E 7+00S	1	19	14	80	.3	31	9	156	2.84	8	5	ND	3	16	1	2	2	38	.28	.049	9	33	.30	119	.11	2	2.65	.03	.04	1	1
83+00E 7+25S	1	32	20	79	.4	35	9	395	3.03	11	5	ND	5	24	1	2	2	42	.49	.037	16	35	.40	163	.14	7	3.38	.03	.06	1	1
83+00E 7+50S	1	74	12	56	.8	30	8	446	1.91	7	7	ND	1	71	1	2	2	26	2.03	.098	12	32	.43	240	.05	5	1.95	.04	.04	1	1
83+00E 7+75S	1	145	13	49	.6	35	7	663	.85	4	29	ND	3	298	1	2	2	9	6.57	.138	16	15	.35	296	.02	8	1.21	.01	.02	1	4
83+00E 8+00S	1	44	9	55	.5	16	8	427	2.06	2	8	ND	1	56	1	2	2	32	1.43	.069	11	15	.36	181	.06	3	1.84	.07	.04	1	1
STD C/AU-S	20	59	36	127	6.7	70	28	976	3.93	38	17	7	33	47	16	15	20	60	.48	.100	34	58	.88	172	.08	37	1.72	.06	.12	14	48

APPENDIX IV

ACME ANALYTICAL LABORATORIES LTD.

Lithogeochemical Results

ACME ANALYTICAL LABORATORIES LTD.

852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6

PHONE 253-3158

DATA LINE 251-1011

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO₃-H₂O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.

THIS LEACH IS PARTIAL FOR MN, FE, CA, P, CR, MG, BA, TI, B, AL, NA, K, W, SI, ZR, CE, SM, Y, NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.

- SAMPLE TYPE: ROCK CHIPS AU ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: NOV 24 1986 DATE REPORT MAILED: Nov 28/86 ASSAYER: D. J. J. DEAN TOYE, CERTIFIED B.C. ASSAYER.

CEC ENGINEERING PROJECT - TWIN 86-14 FILE # 86-3796

PAGE 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au PPB
86-14-1	2	141	16	105	.2	133	32	13415	7.51	34	24	ND	7	192	1	2	2	39	8.83	.025	2	80	1.88	137	.01	3	.85	.03	.02	1	1
86-14-2	1	211	27	79	.1	298	39	1337	8.44	43	6	ND	3	64	2	2	2	129	4.01	.071	5	442	4.33	33	.01	3	3.59	.02	.01	1	2
86-14-3	1	34	7	37	.1	84	15	974	3.53	2	10	ND	6	105	1	2	2	36	9.73	.024	3	124	3.82	34	.01	4	.89	.03	.02	1	2
86-14-4	1	33	4	43	.1	321	34	1530	3.83	6	12	ND	5	232	1	2	2	22	23.60	.013	2	436	2.89	13	.01	6	.99	.02	.02	1	4
86-14-5	1	33	5	28	.1	59	13	1014	3.73	4	5	ND	1	382	1	2	4	36	31.98	.047	4	53	.64	89	.04	2	.44	.01	.04	1	1
86-14-6	1	27	14	78	.1	220	32	645	5.73	16	9	ND	4	61	1	2	2	94	4.65	.047	2	338	4.08	42	.32	2	2.58	.05	.02	1	260
86-14-7	1	113	7	90	.1	194	33	1761	5.90	17	13	ND	7	109	1	2	2	41	9.38	.030	5	150	3.09	116	.01	5	1.94	.01	.08	1	2
86-14-8	1	44	17	101	.1	152	30	1797	6.29	77	6	ND	3	66	1	2	2	66	4.85	.086	2	171	5.14	74	.01	4	2.57	.01	.07	1	5

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO₃-H₂O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN, FE, CA, P, CR, MG, BA, TI, B, AL, NA, K, W, SI, ZR, CE, SM, Y, NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: ROCK CHIPS AU ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: DEC 22 1986 DATE REPORT MAILED: Jan 6/87 ASSAYER: *D. J. Toy* DEAN TOYE, CERTIFIED B.C. ASSAYER.

CEC ENGINEERING PROJECT - TWIN FILE # 86-4043

PAGE 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au PPM
86-14-9	1	86	13	82	.1	300	39	1155	6.48	162	5	ND	1	90	1	3	2	77	8.72	.038	2	369	4.79	133	.01	2	3.10	.10	.04	1	26
86-14-10	1	91	9	110	.3	273	38	1108	7.27	81	5	ND	1	80	1	3	2	46	9.38	.044	2	218	2.56	165	.01	2	2.09	.10	.09	1	14
86-14-11	2	73	198	4180	.5	126	23	2045	4.15	37	5	ND	1	202	11	5	2	55	12.87	.031	2	181	3.50	81	.02	2	1.39	.12	.02	1	11
86-14-12	1	69	8	67	.1	169	31	884	5.85	2	5	ND	2	205	1	2	2	105	11.44	.068	6	361	4.06	158	.02	2	3.23	.10	.01	1	1
86-14-13	1	92	8	86	.1	174	37	989	5.89	175	5	ND	1	106	1	2	2	18	11.01	.059	2	43	1.90	56	.01	2	.35	.15	.05	1	10
86-14-14	1	69	16	163	.1	178	26	1271	6.22	214	5	ND	1	114	2	2	2	25	7.53	.039	2	52	2.44	140	.01	2	.33	.12	.11	1	32
86-14-15A	1	220	140	268	.4	184	41	1447	6.72	146	5	ND	1	70	2	2	2	15	4.45	.057	2	38	1.97	159	.01	3	.38	.10	.11	1	46
86-14-15B	1	43	315	171	.5	51	12	2168	2.74	65	5	ND	1	192	1	9	2	10	13.15	.050	2	11	5.97	64	.01	4	.14	.11	.06	1	12
86-14-15C	2	38	76	115	.4	82	14	2196	4.12	81	5	ND	2	154	1	7	2	22	10.66	.050	2	17	4.55	115	.01	5	.28	.11	.13	1	19
86-14-16A	4	67	24	52	.3	59	17	1110	4.02	31	5	ND	3	78	1	2	2	9	3.14	.038	3	7	1.11	158	.01	15	.37	.08	.16	1	8
86-14-16B	1	64	14	135	.1	84	22	710	5.39	59	5	ND	4	47	1	2	2	23	1.37	.061	6	52	1.21	162	.01	8	1.21	.07	.20	1	15
86-14-17	1	54	5	88	.2	91	11	481	3.04	103	5	ND	3	36	1	2	2	23	1.06	.074	5	30	.67	138	.01	9	.74	.05	.13	1	2
86-14-18	1	102	9	86	.1	240	41	1217	6.49	13	5	ND	1	141	1	8	2	127	3.40	.044	3	388	6.79	91	.01	2	3.71	.09	.01	1	1
86-14-19	1	74	7	79	.1	210	33	1205	5.82	14	5	ND	1	144	1	6	3	120	3.59	.048	2	382	6.35	77	.01	2	3.35	.09	.01	1	1
86-14-20	1	84	15	91	.1	222	38	1257	6.06	16	5	ND	1	133	1	7	2	118	3.50	.052	2	355	6.45	54	.01	2	3.45	.09	.01	1	1
86-14-21	1	105	32	152	.2	248	45	1522	6.34	226	5	ND	1	76	1	2	2	73	4.08	.053	2	247	3.99	116	.01	2	2.49	.12	.04	1	47
86-14-22	1	66	19	143	.2	176	35	2178	6.02	128	5	ND	1	157	1	6	2	44	9.01	.042	2	140	4.88	139	.01	2	1.39	.12	.06	1	29
86-14-23	1	50	10	162	.1	153	30	1845	5.42	92	5	ND	1	157	1	2	2	31	7.99	.053	2	110	3.97	144	.01	3	1.04	.12	.06	1	22
86-14-24	1	107	492	207	.6	179	30	2238	5.62	148	5	ND	1	151	1	5	2	44	8.55	.048	2	153	4.77	184	.01	2	1.51	.13	.07	1	20
86-14-25	1	72	52	183	.2	209	39	1533	6.63	134	5	ND	1	95	1	2	2	69	4.97	.075	2	249	4.38	185	.01	2	2.44	.13	.05	1	24
86-14-26	10	45	43	71	.4	67	17	3017	4.54	53	5	ND	1	143	1	6	2	40	11.47	.101	2	26	5.20	58	.01	2	.39	.11	.08	1	11
86-14-27	1	37	10	115	.1	87	15	1627	4.64	59	5	ND	2	90	1	2	2	30	5.73	.071	2	51	3.59	62	.01	2	1.31	.09	.09	1	5
86-14-28	2	47	51	94	.4	43	11	3074	3.75	65	5	ND	2	186	1	10	2	12	14.31	.036	2	9	6.45	60	.01	2	.19	.11	.07	1	16
86-14-29	6	75	44	96	.8	28	4	2748	1.60	23	5	ND	2	196	1	16	4	63	18.82	1.427	6	21	6.60	134	.01	6	.39	.12	.11	1	2
86-14-30	3	26	13	73	.3	24	6	1842	2.02	70	5	ND	2	79	1	6	2	8	10.23	.039	2	6	4.51	78	.01	5	.14	.09	.06	1	9
86-14-31	1	51	6	97	.1	117	11	519	3.59	63	5	ND	2	47	1	2	2	20	2.77	.064	3	33	2.19	77	.01	3	.98	.07	.11	1	8
86-14-32	2	103	30	66	1.1	91	28	804	5.14	46	5	ND	4	46	1	4	2	20	3.51	.554	5	17	.91	43	.01	3	.53	.07	.20	1	13
86-14-33	13	42	30	141	.5	40	8	2837	3.09	38	5	ND	2	75	1	4	2	35	9.84	.073	3	8	4.20	67	.01	3	.19	.09	.10	1	6
86-14-34	1	60	82	153	.3	175	34	2072	6.17	143	5	ND	1	132	1	2	2	48	8.21	.080	2	134	4.31	157	.01	2	1.40	.15	.07	1	23
86-14-35	1	90	68	327	.4	260	48	1563	6.76	165	5	ND	1	119	1	2	2	44	6.68	.055	2	190	3.59	198	.01	2	1.35	.14	.07	1	26
86-14-36	1	77	66	342	.4	197	37	2029	5.92	206	5	ND	1	153	2	4	2	32	9.42	.048	2	121	4.43	144	.01	2	.87	.14	.05	1	32
86-14-37	1	89	152	859	.3	188	32	2264	5.78	286	5	ND	2	143	4	2	2	39	10.12	.065	2	112	4.00	237	.01	2	.84	.16	.06	1	12
86-14-38	1	84	11	104	.1	76	25	1138	5.52	23	5	ND	1	72	1	2	2	41	9.13	.082	2	55	1.03	327	.01	3	1.04	.14	.13	1	17
86-14-39	1	83	24	143	.3	100	35	1350	7.13	67	5	ND	1	61	1	2	2	38	4.22	.100	2	53	.51	326	.01	4	1.01	.13	.14	1	89
86-14-40	2	316	4567	7252	2.8	244	33	1878	7.06	167	5	ND	1	88	27	4	2	35	11.27	.038	2	86	1.67	314	.01	2	.64	.13	.06	1	13
86-14-41	1	70	64	236	.4	182	25	1247	5.99	58	5	ND	2	98	1	2	2	39	14.75	.034	2	87	1.72	239	.01	2	.58	.13	.06	1	4
STD C/AU-R	21	59	40	136	7.2	70	29	1036	3.95	38	17	7	34	49	18	16	19	65	.44	.106	36	59	.88	183	.08	37	1.72	.10	.13	12	505

CEC ENGINEERING PROJECT - TWIN FILE # 86-4043

PAGE 2

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mo %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au# PPB
86-14-42	1	71	68	142	.3	133	27	1392	5.38	144	5	ND	1	91	1	2	3	22	12.74	.042	2	41	2.15	74	.01	3	.26	.14	.06	1	5
86-14-43	1	98	13	143	.2	229	34	870	5.82	22	5	ND	1	86	1	2	3	36	10.83	.045	2	120	2.17	56	.01	3	.96	.13	.03	1	4
86-14-44	1	58	12	104	.3	213	33	918	5.96	3	5	ND	2	76	1	2	2	59	9.88	.044	2	189	2.45	48	.01	3	1.67	.12	.02	1	1
86-14-45	1	66	11	71	.3	198	34	1086	5.81	10	5	ND	1	72	1	2	2	33	10.34	.048	2	115	1.24	88	.01	2	.81	.13	.02	1	1
86-14-46	1	69	9	113	.2	200	30	1186	5.59	15	5	ND	1	110	1	3	3	106	5.14	.042	2	320	5.75	48	.01	2	3.03	.09	.01	1	11
86-14-47	1	70	9	91	.2	202	28	940	5.78	40	5	ND	1	150	1	7	2	88	5.69	.044	2	285	5.48	52	.01	2	3.03	.11	.03	1	1
86-14-48	1	80	7	137	.2	235	36	1005	5.56	11	5	ND	1	197	1	2	2	109	10.74	.045	4	351	2.96	36	.05	2	2.73	.10	.01	1	4
86-14-49	1	71	7	87	.1	221	35	914	6.32	8	5	ND	2	128	1	2	2	135	7.56	.048	5	385	3.71	54	.05	2	3.27	.10	.01	1	3
86-14-50	2	123	10	84	.2	226	37	951	6.18	11	5	ND	2	180	1	2	2	132	9.82	.041	3	359	3.44	206	.02	2	3.21	.11	.01	1	1
86-14-51	1	153	231	522	.4	228	34	1115	6.29	39	7	ND	2	149	2	2	2	62	9.05	.043	2	234	2.85	103	.01	2	2.43	.09	.11	1	13
86-14-52	2	103	11	118	.2	203	32	1009	5.95	9	5	ND	1	181	1	2	3	95	9.40	.038	4	277	3.16	66	.01	2	3.02	.09	.05	1	5
86-14-53	1	66	15	97	.1	262	39	938	6.48	10	5	ND	2	132	1	4	2	131	6.87	.048	5	382	3.62	47	.02	2	3.22	.10	.01	1	3
86-14-54	1	84	6	83	.2	240	38	927	6.32	7	5	ND	1	130	1	3	2	121	6.72	.050	5	380	3.42	105	.05	2	3.03	.10	.01	1	1
86-14-55	1	65	9	64	.3	229	33	838	5.54	7	5	ND	1	174	1	2	2	115	9.56	.046	4	359	2.44	64	.14	2	2.20	.11	.01	1	1
86-14-56	1	172	19	97	.3	155	24	1429	6.20	24	5	ND	1	169	1	2	2	51	10.82	.042	2	139	3.17	71	.05	2	1.64	.10	.04	1	14
86-14-57	1	101	43	216	.4	284	39	1254	6.93	71	7	ND	1	73	1	2	3	61	6.75	.064	2	228	1.93	146	.01	2	1.61	.14	.07	1	10
86-14-58	1	59	13	214	.1	315	36	1432	7.00	31	5	ND	1	121	1	2	2	63	9.73	.040	2	309	3.81	132	.01	2	1.71	.11	.02	1	4
86-14-59	1	41	30	247	.2	361	56	1388	5.35	59	5	ND	1	117	2	2	4	30	10.97	.056	2	307	3.22	172	.01	2	.65	.13	.04	1	6
86-14-60	1	34	12	231	.3	788	67	1606	7.52	194	6	ND	1	93	1	4	5	67	7.37	.061	4	1143	4.98	103	.01	2	2.57	.10	.01	1	11
STD C/AU-R	21	59	40	136	7.2	69	28	1012	3.98	40	17	8	34	48	18	16	18	1	.45	.105	36	58	.84	181	.08	37	1.72	.09	.13	11	510

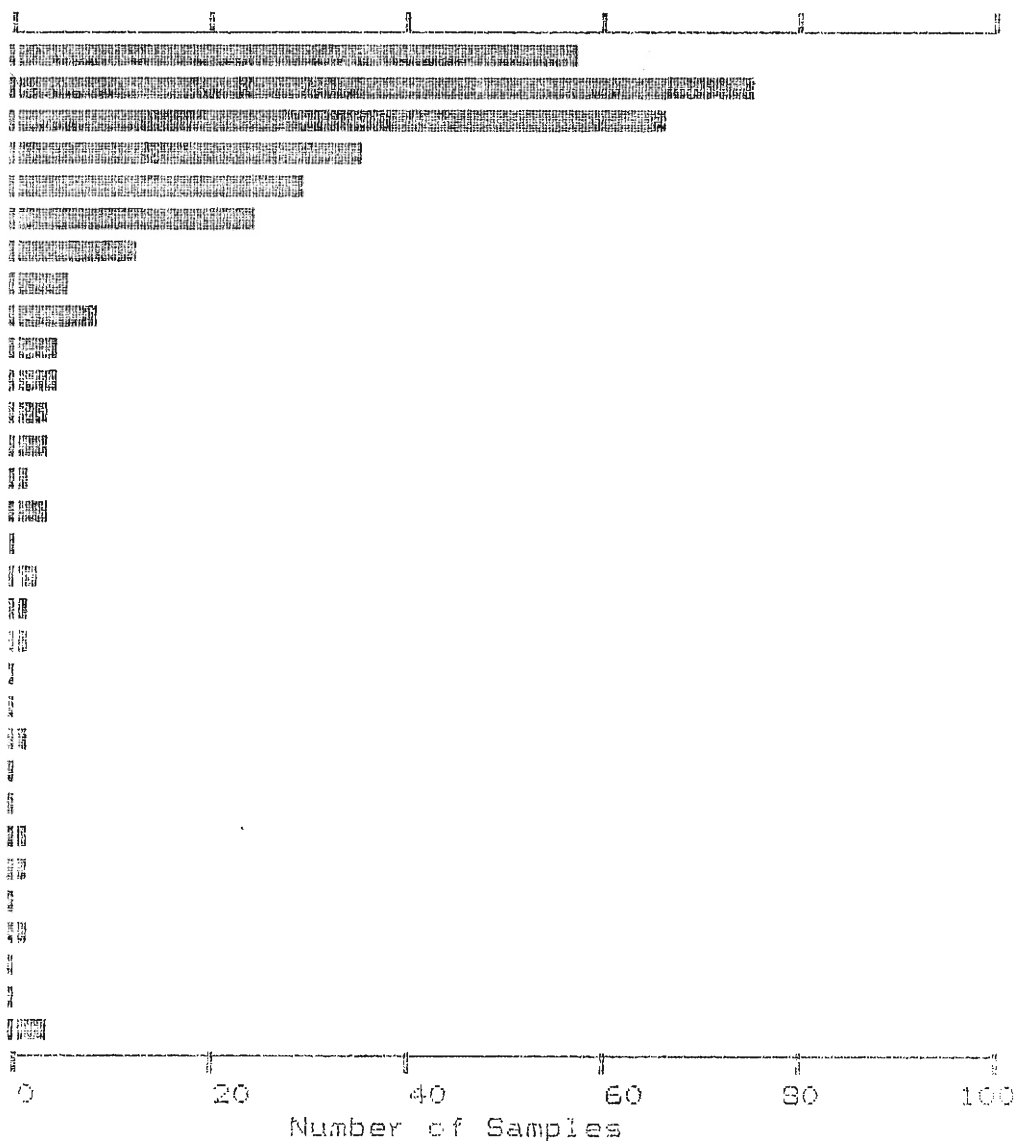
APPENDIX V

SOIL GEOCHEMICAL STATISTICS

C.E.C. ENGINEERING

5
(PPM)

5 (57)
10 (75)
15 (66)
20 (35)
25 (29)
30 (24)
35 (12)
40 (5)
45 (8)
50 (4)
55 (4)
60 (3)
65 (3)
70 (1)
75 (3)
80 (0)
85 (2)
90 (1)
95 (1)
100 (0)
105 (0)
110 (1)
115 (0)
120 (0)
125 (1)
130 (1)
135 (0)
140 (1)
145 (0)
150 (0)
Over (3)



361 Samples

Maximum: 250

Minimum: 2

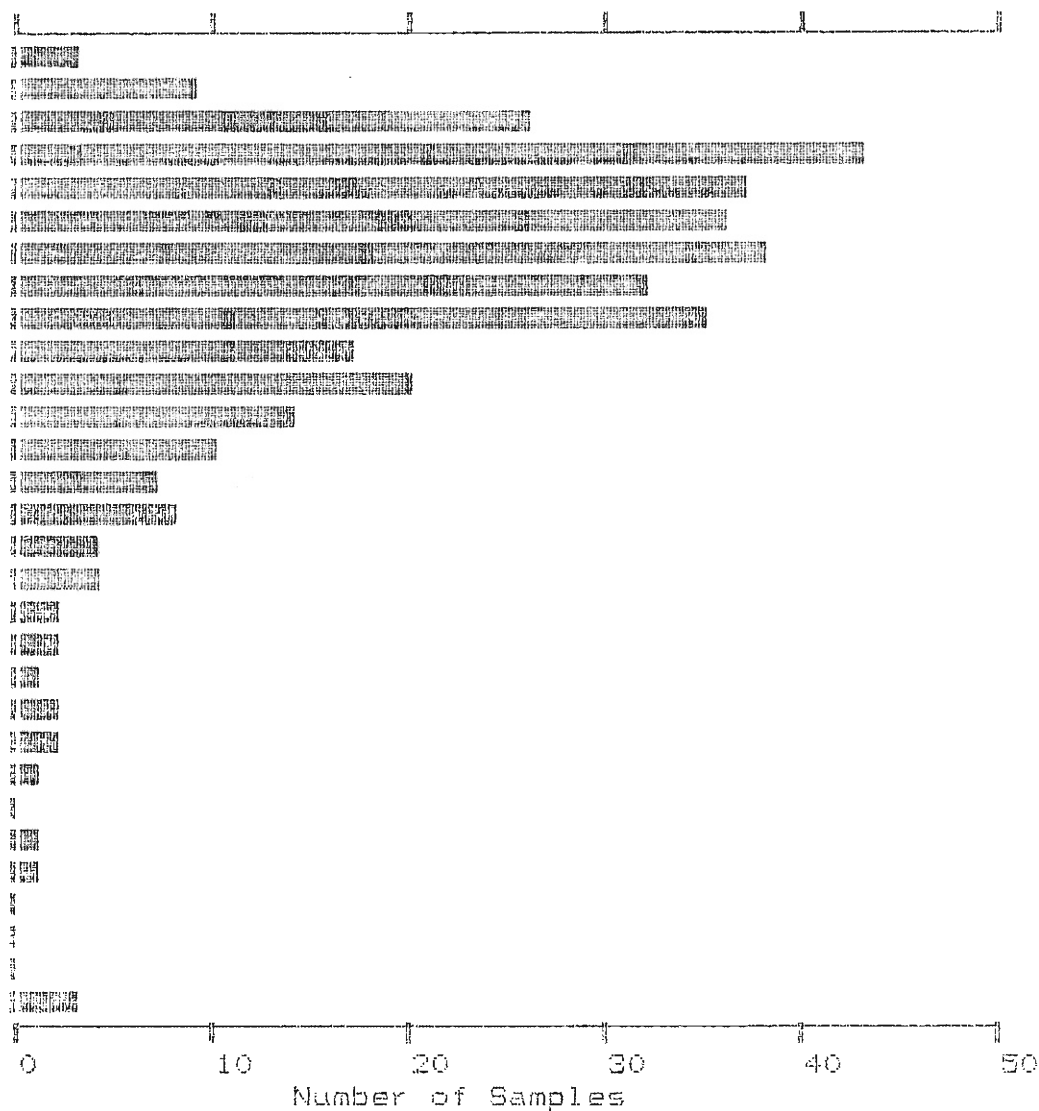
Mean: 23

Standard Deviation: 26

C.E.C. ENGINEERING

3A

(PPM)



361 Samples

Maximum: 528

Mean: 142

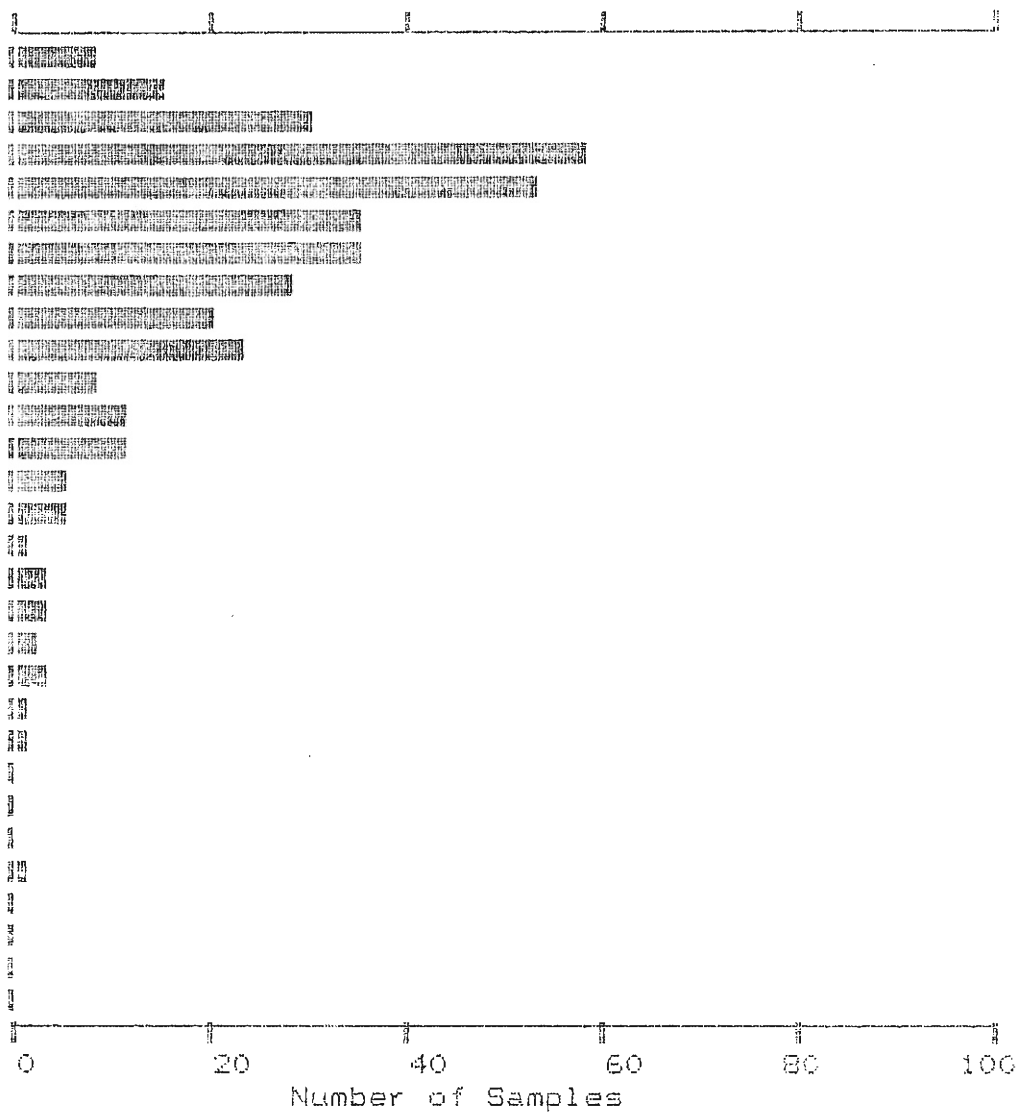
Minimum: 22

Standard Deviation: 72

C.E.C. ENGINEERING

(PPM)

2 (8)
4 (15)
6 (30)
8 (52)
10 (53)
12 (35)
14 (35)
16 (28)
18 (20)
20 (23)
22 (8)
24 (14)
26 (11)
28 (5)
30 (5)
32 (1)
34 (3)
36 (3)
38 (2)
40 (3)
42 (1)
44 (1)
46 (0)
48 (0)
50 (0)
52 (1)
54 (0)
56 (0)
58 (0)
60 (0)



361 Samples

Maximum:

52

Mean:

14

Minimum:

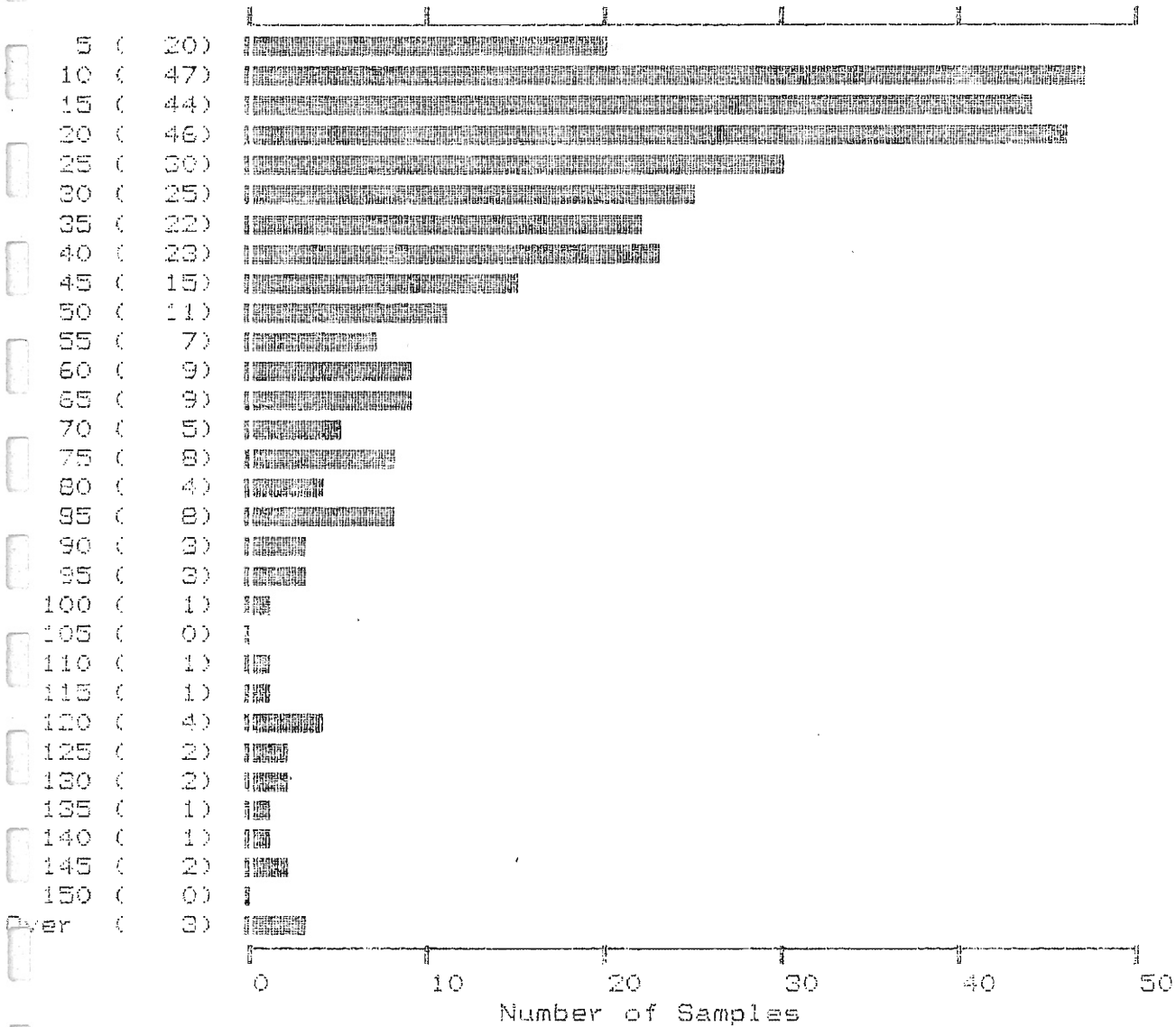
1

Standard Deviation:

8

C.E.C. ENGINEERING

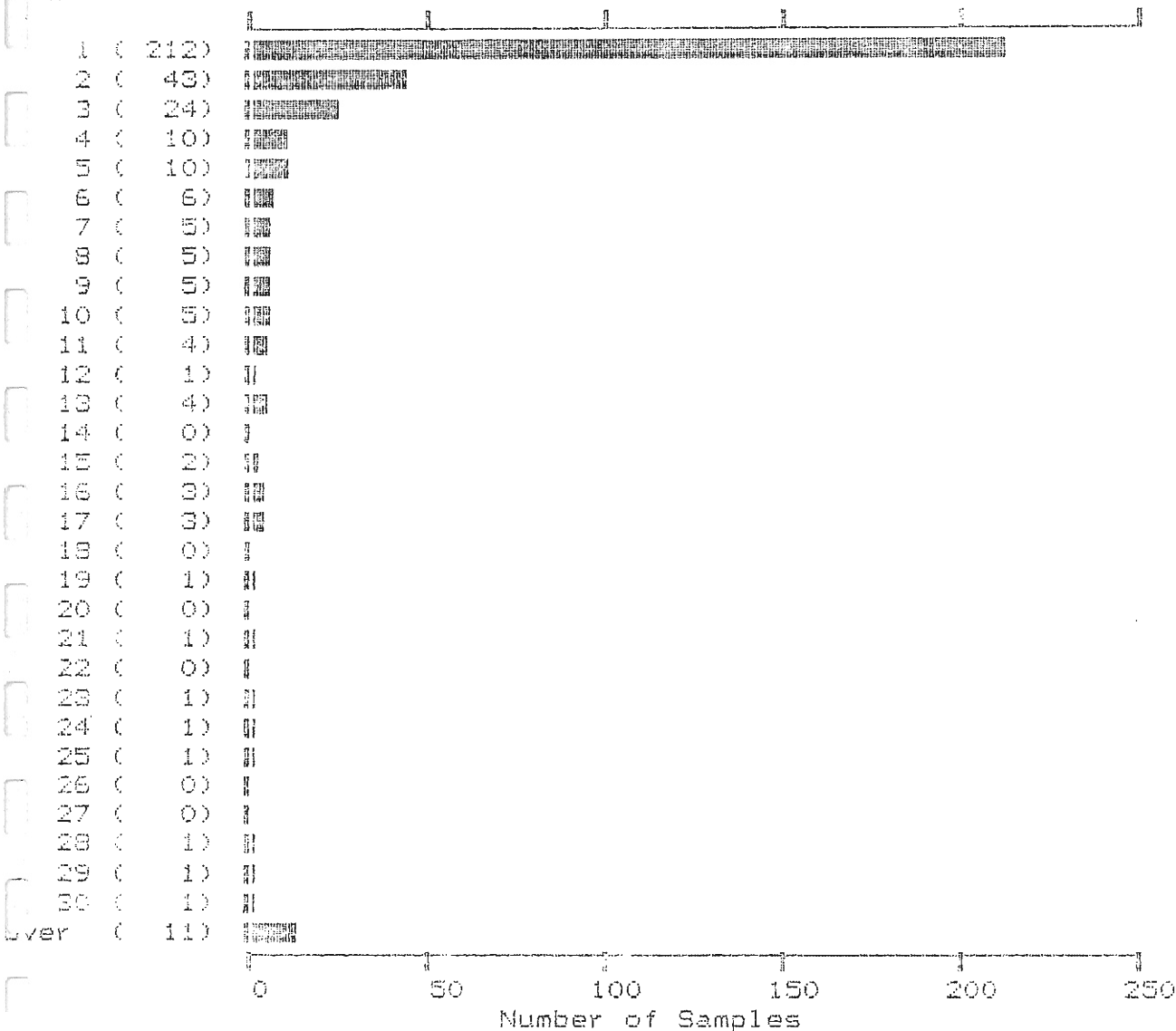
CU
(PPM)



361 Samples Maximum: 173 Mean: 38
 Minimum: 1 Standard Deviation: 31

C.E.C. ENGINEERING

AU-
(PPB)



361 Samples

Maximum:

320

Mean:

6

Minimum:

1

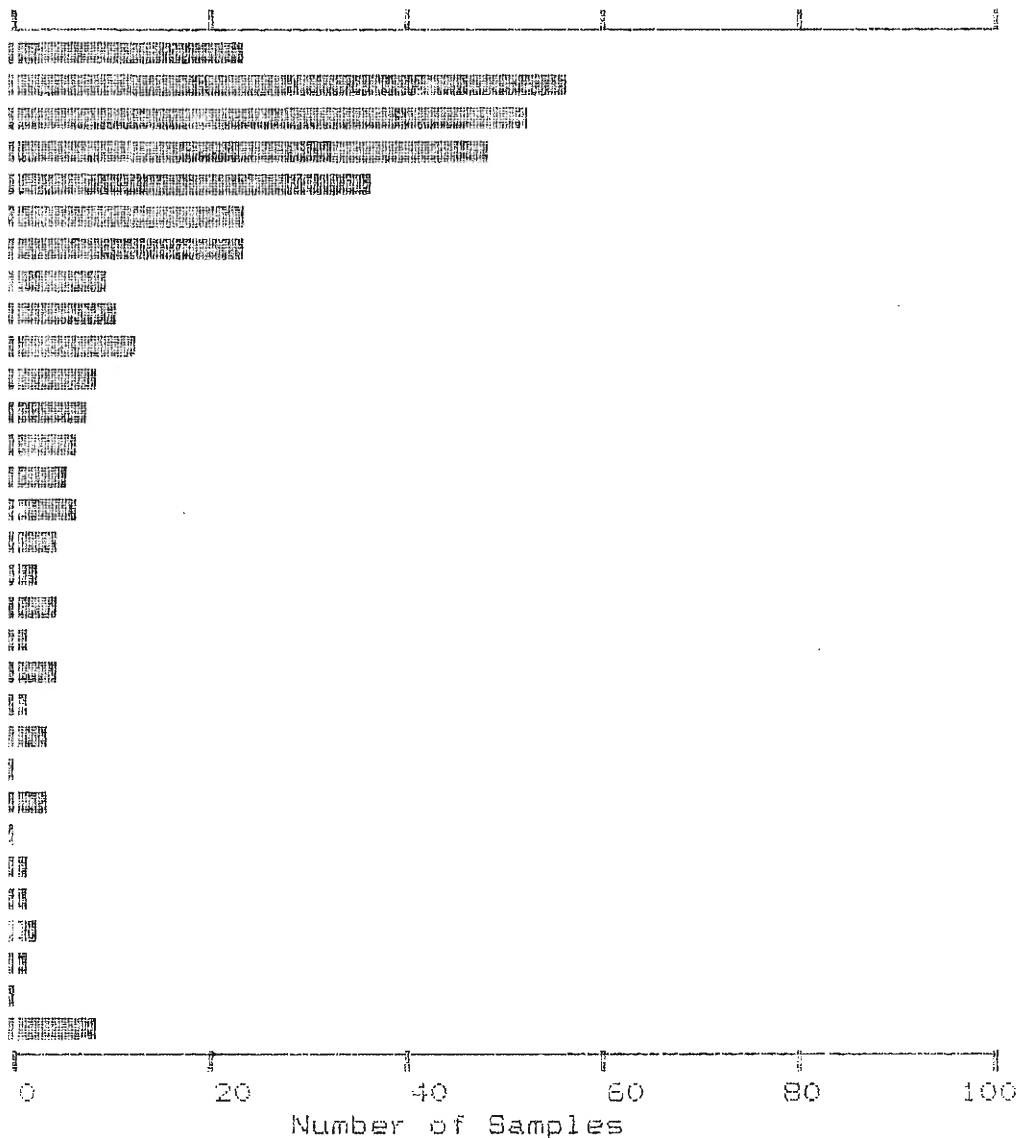
Standard Deviation:

24

C.E.C. ENGINEERING

(PPM)

5 (23)
10 (36)
15 (32)
20 (48)
25 (36)
30 (23)
35 (23)
40 (9)
45 (10)
50 (12)
55 (8)
60 (7)
65 (6)
70 (5)
75 (6)
80 (4)
85 (2)
90 (4)
95 (1)
100 (4)
105 (1)
110 (3)
115 (0)
120 (3)
125 (0)
130 (1)
135 (1)
140 (2)
145 (1)
150 (0)
Over (8)

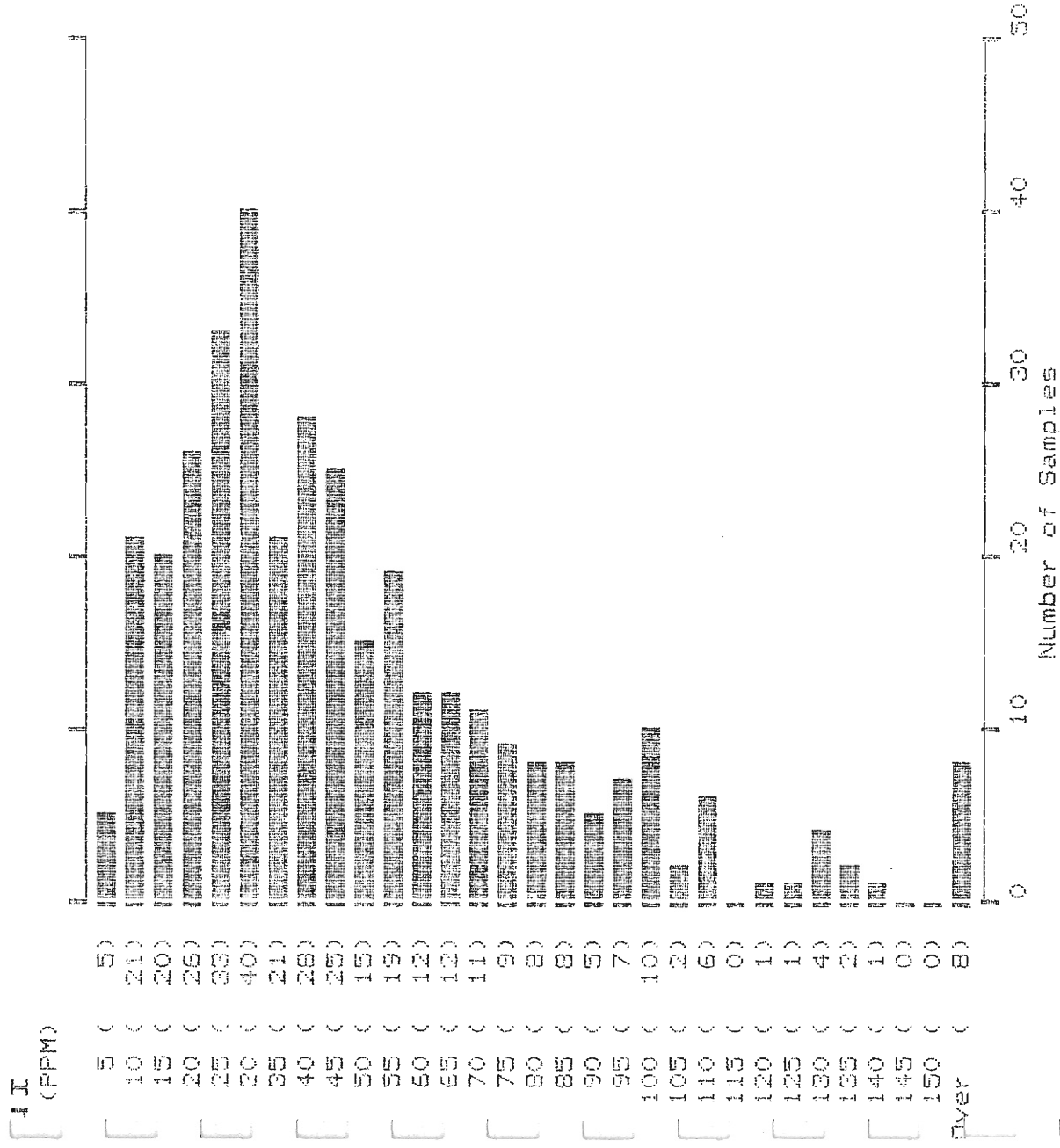


361 Samples

Maximum: 2091
Minimum: 2

Mean: 42
Standard Deviation: 114

C.E.C. ENGINEERING



361 Samples

Maximum: 247

Mean: 51

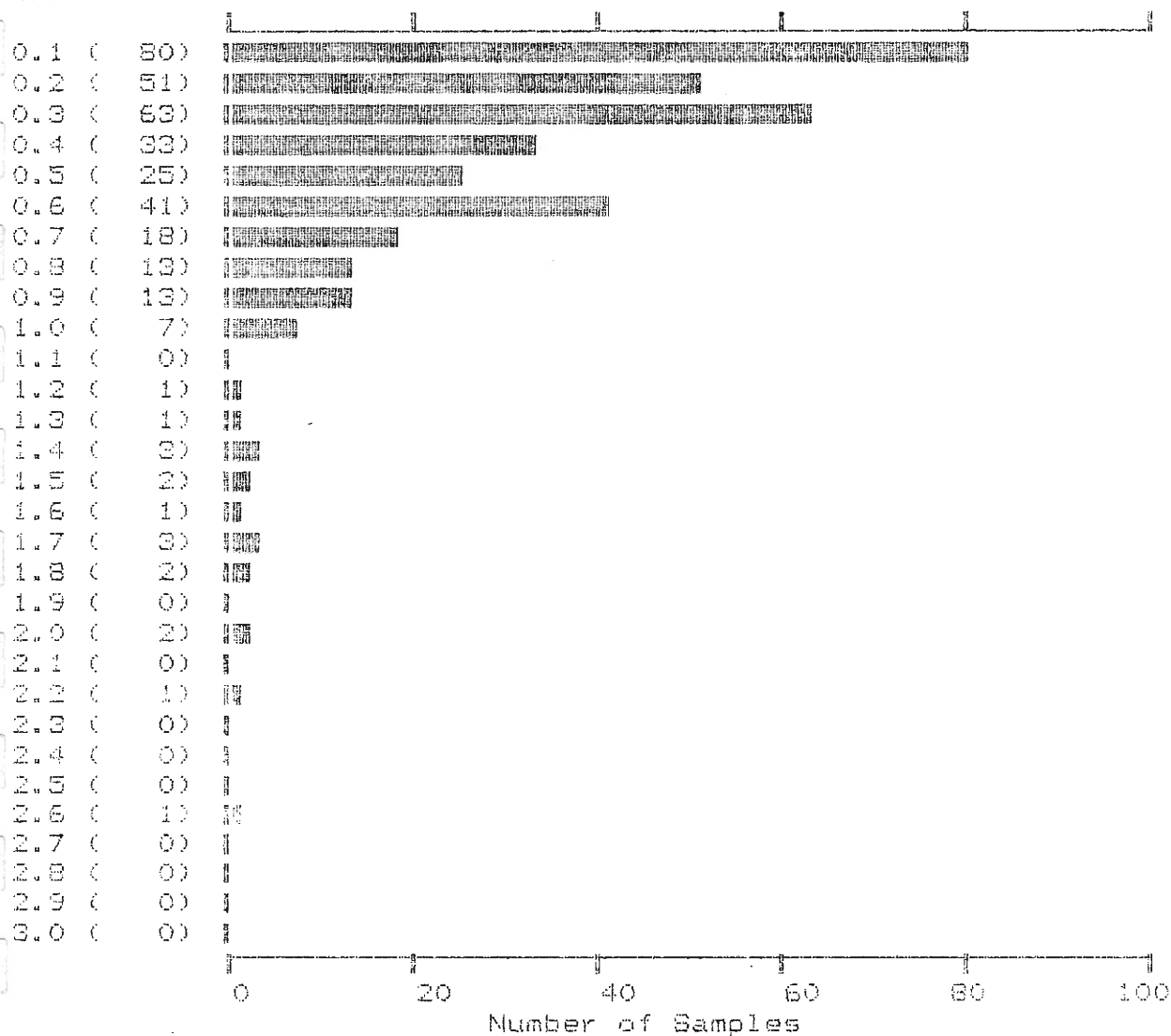
Minimum: 3

Standard Deviation: 36

36

C.E.C. ENGINEERING

US
(PPM)



361 Samples

Maximum: 2.6

Minimum: 0.1

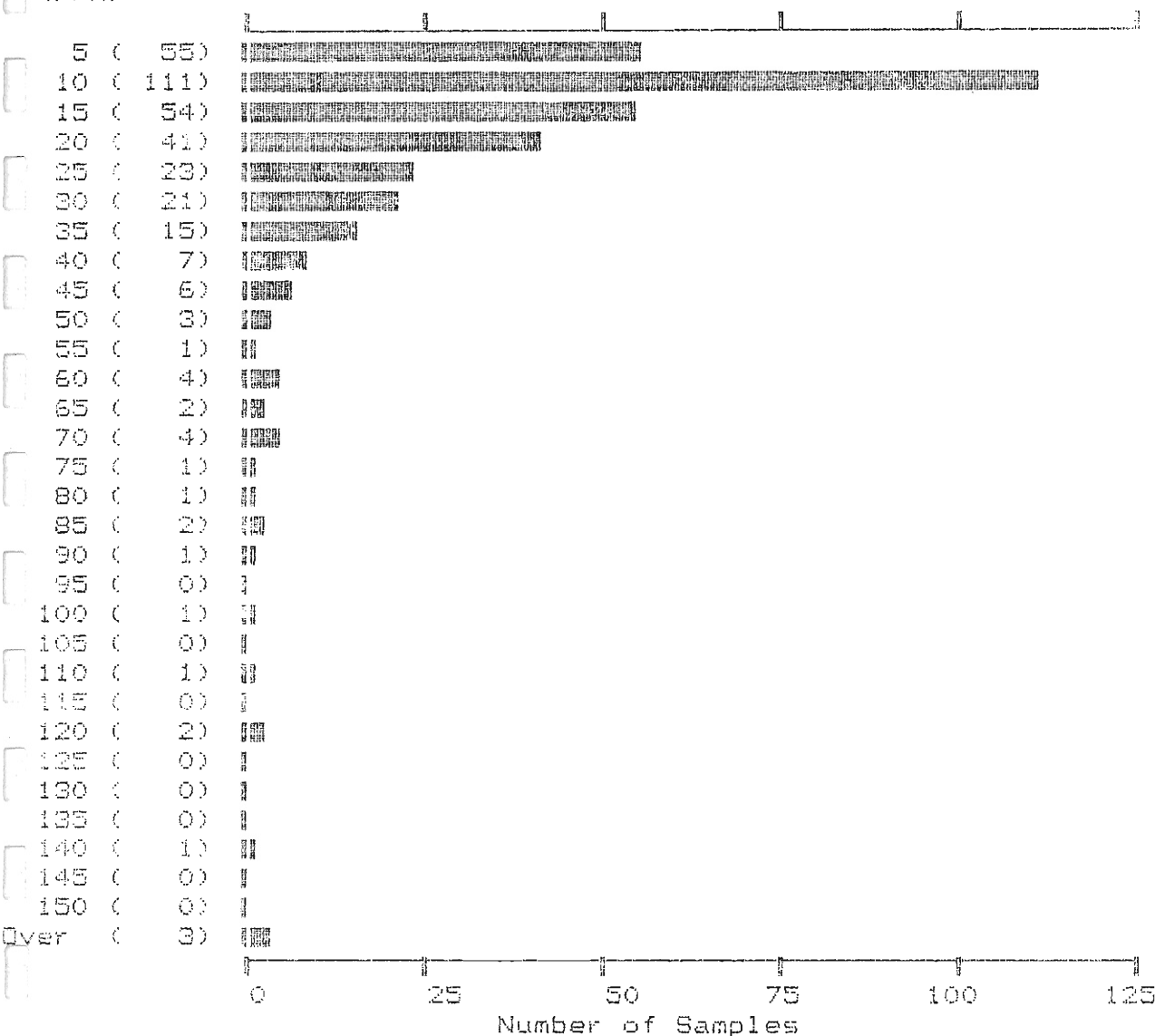
Mean: 0.4

Standard Deviation: 0.4

C.E.C. ENGINEERING

PR

(PPM)



361 Samples

Maximum:

298

Mean:

24

Minimum:

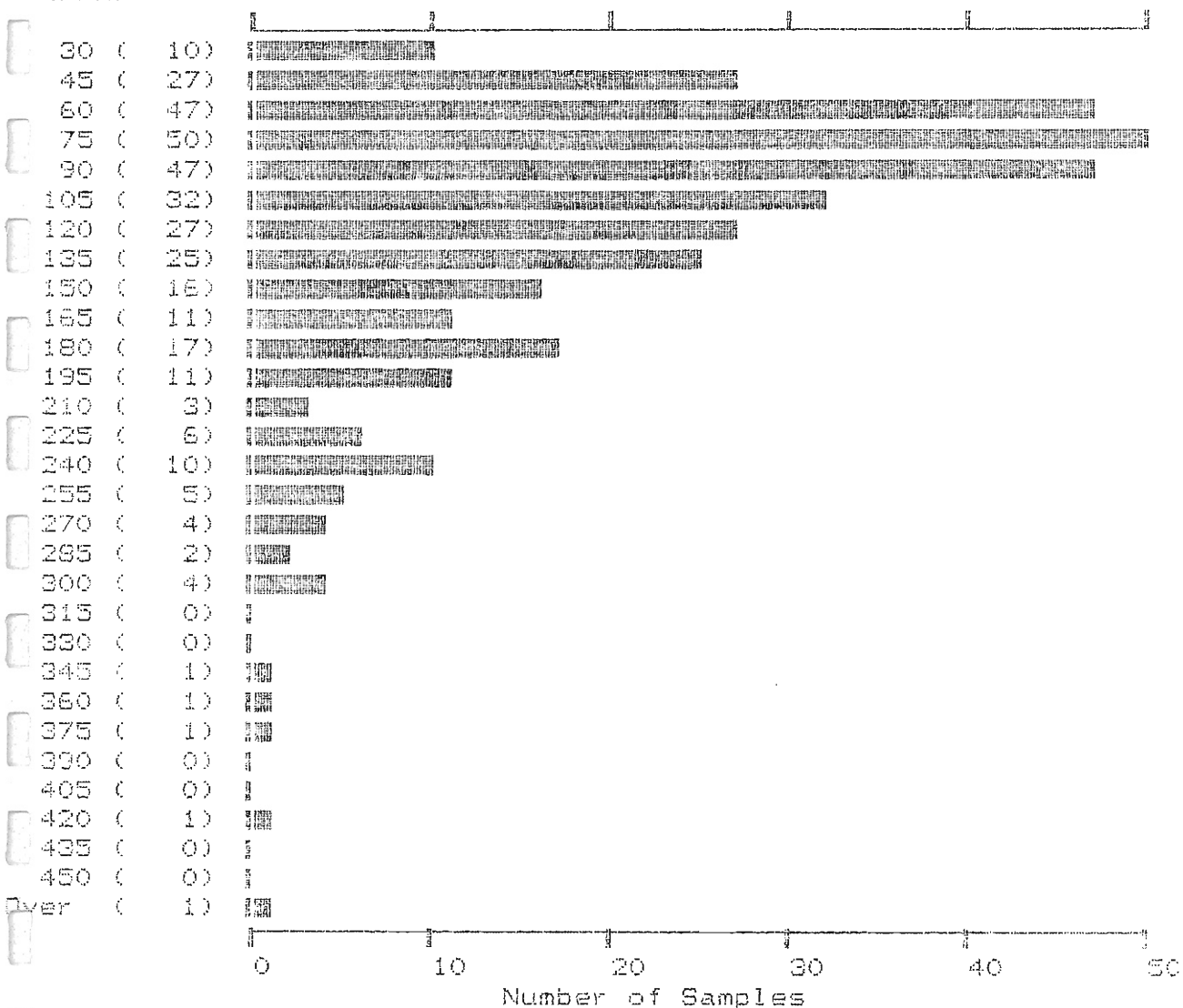
4

Standard Deviation:

27

C.E.C. ENGINEERING

IN
(PPM)



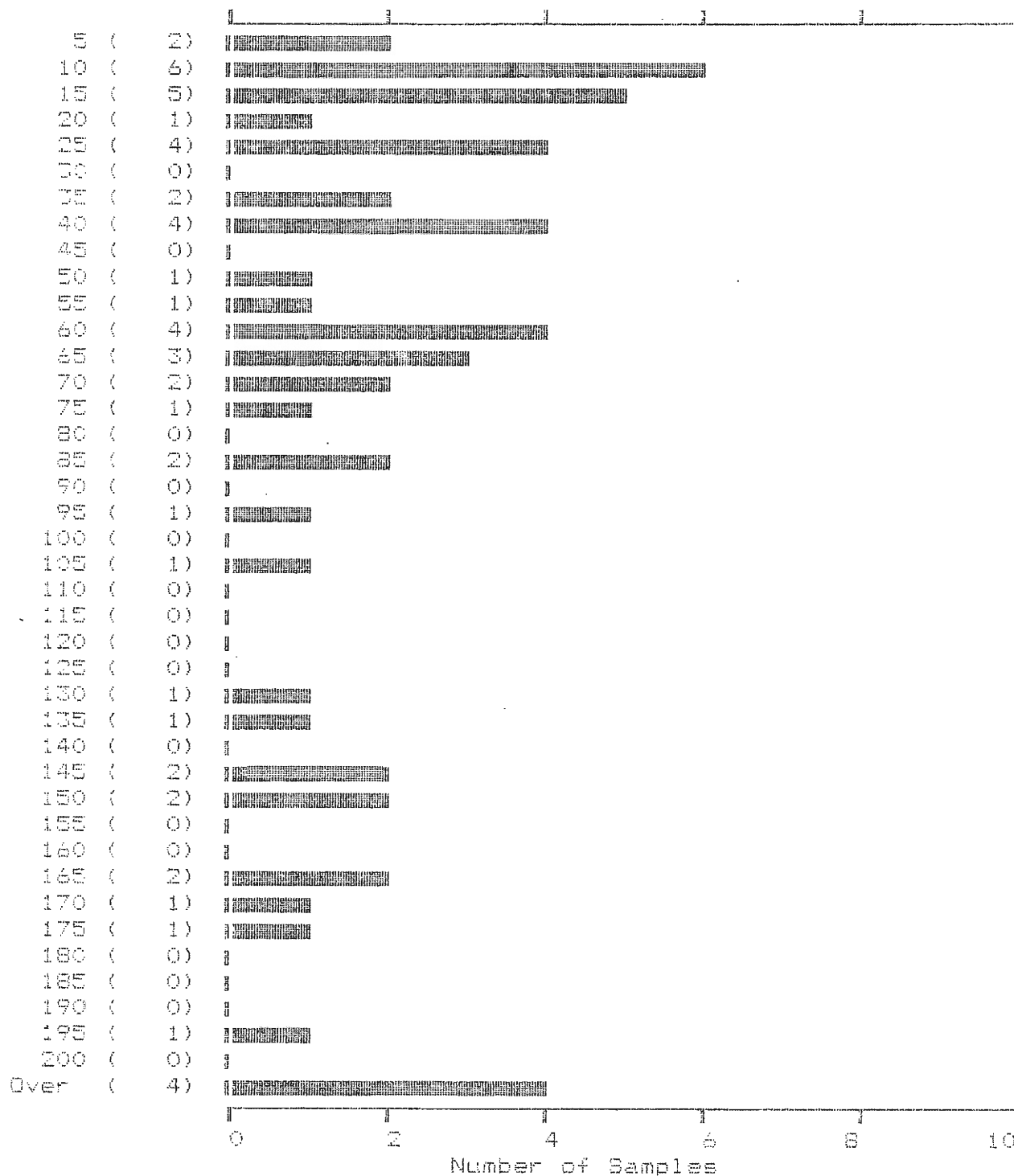
361 Samples	Maximum:	569	Mean:	124
	Minimum:	22	Standard Deviation:	70

APPENDIX VI
LITHOGEOCHEMICAL STATISTICS

C.E.C. ENGINEERING

AS

(PPM)



55 Samples

Maximum: 286

Minimum: 2

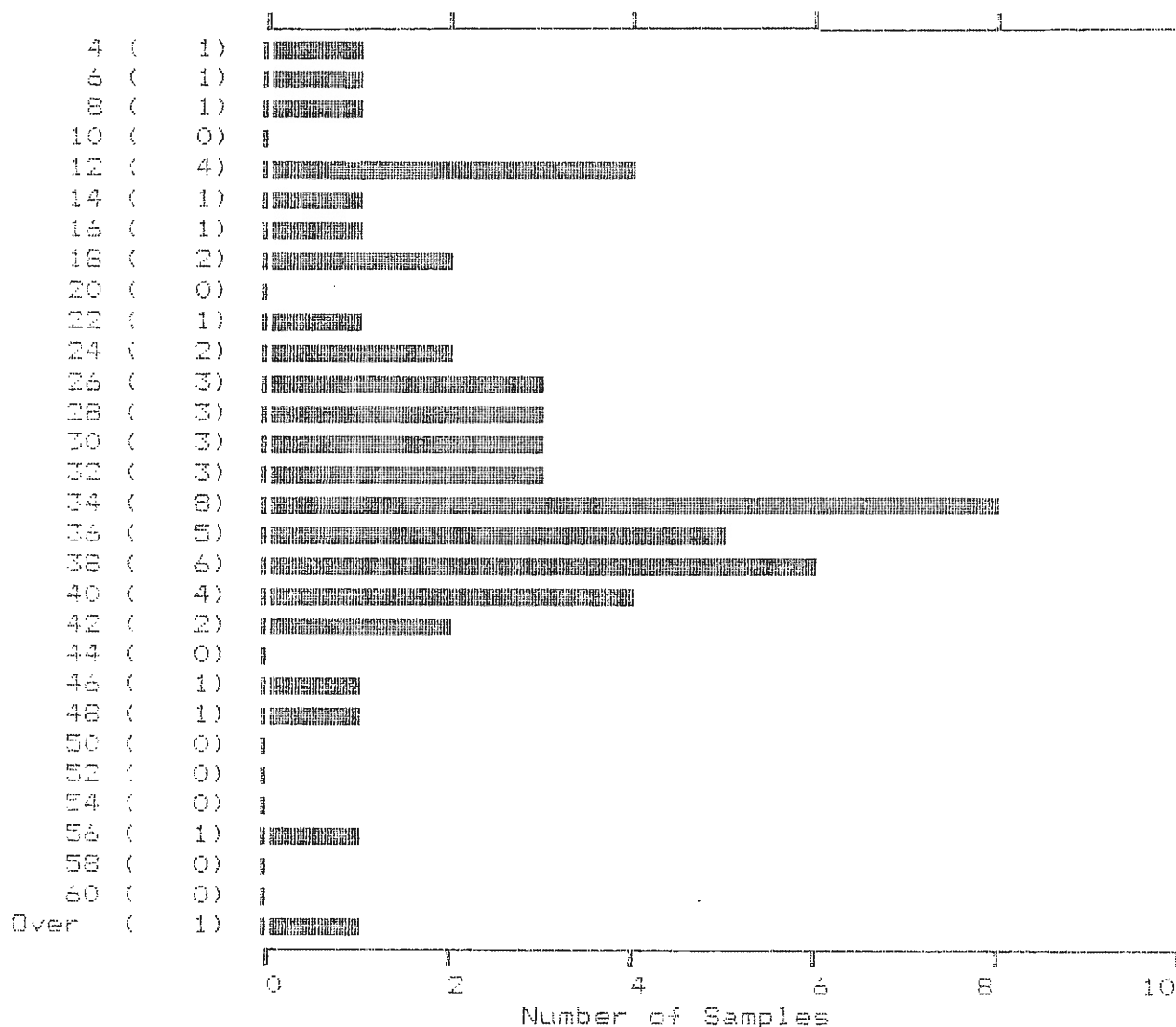
Mean: 76
Standard Deviation: 69

76
69

C.E.C. ENGINEERING

CO

(FPM)



55 Samples

Maximum:

67

Mean:

30

Minimum:

4

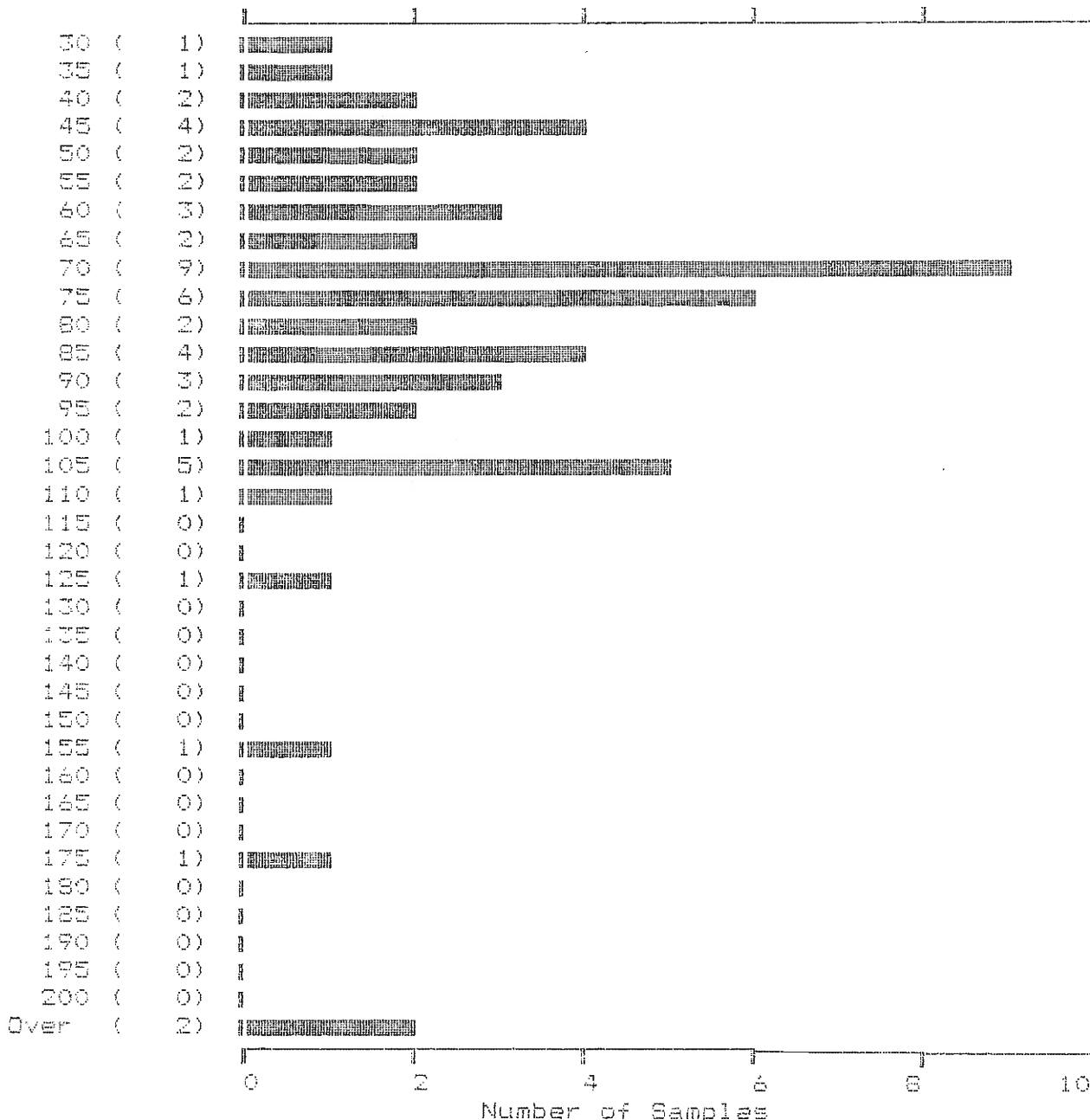
Standard Deviation:

12

C.E.C. ENGINEERING

CU

(PPM)



55 Samples

Maximum:

316

Mean:

82

Minimum:

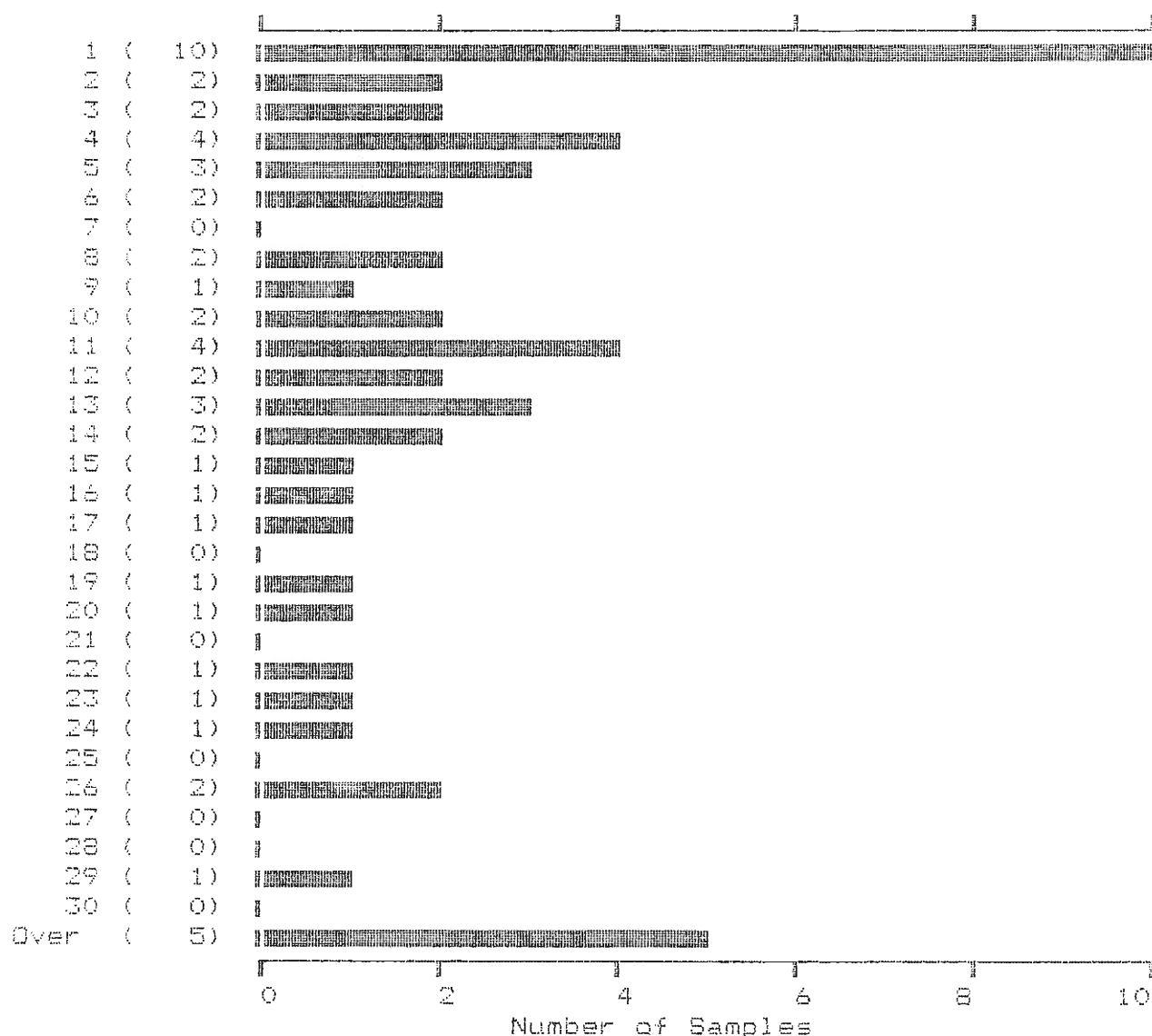
26

Standard Deviation:

46

C.E.C. ENGINEERING

ALJ
(PPB)



55 Samples

Maximum: 89

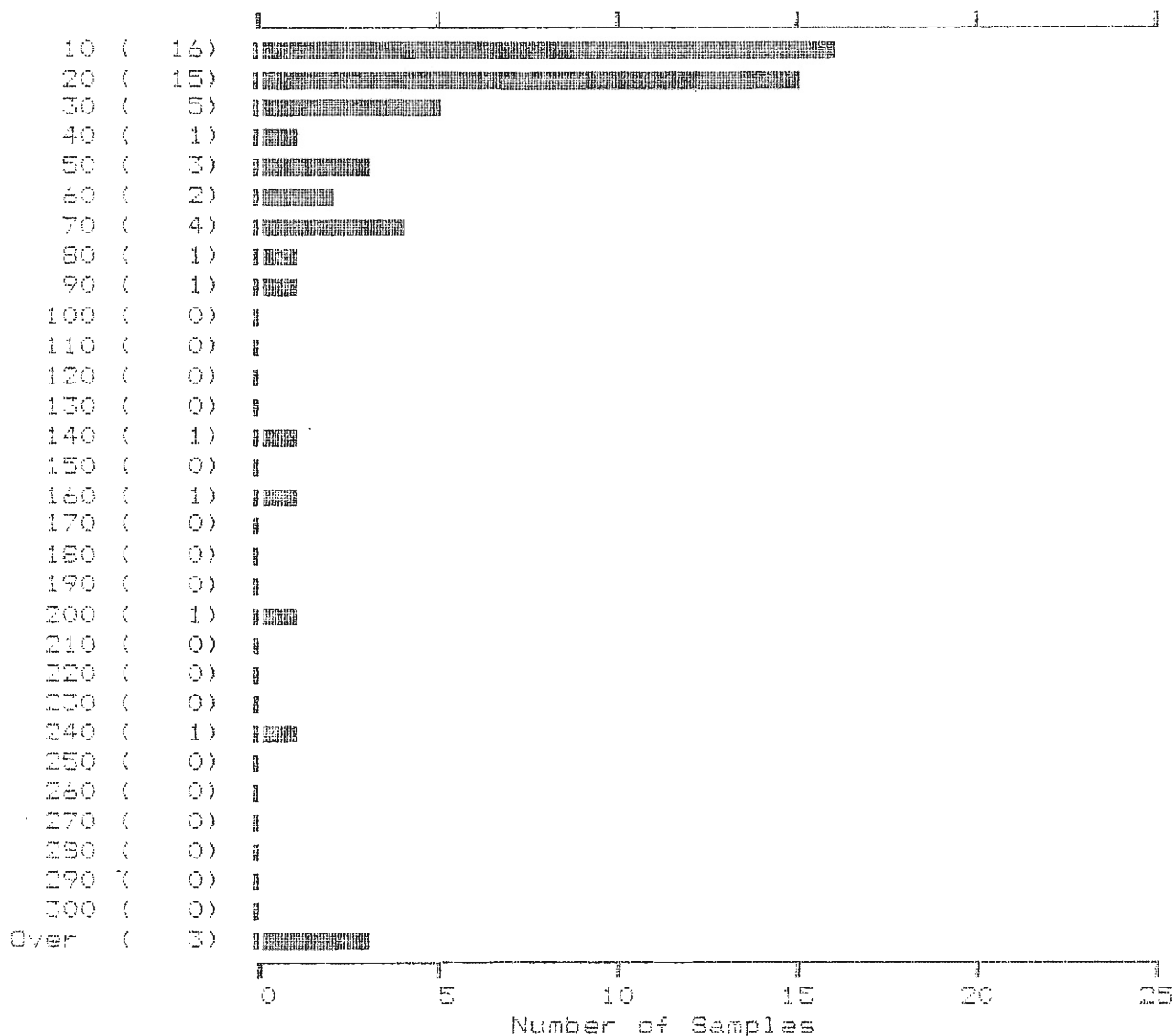
Mean: 13

Minimum: 1

Standard Deviation: 15

C.E.C. ENGINEERING

FB
(PPM)



55 Samples

Maximum: 4567

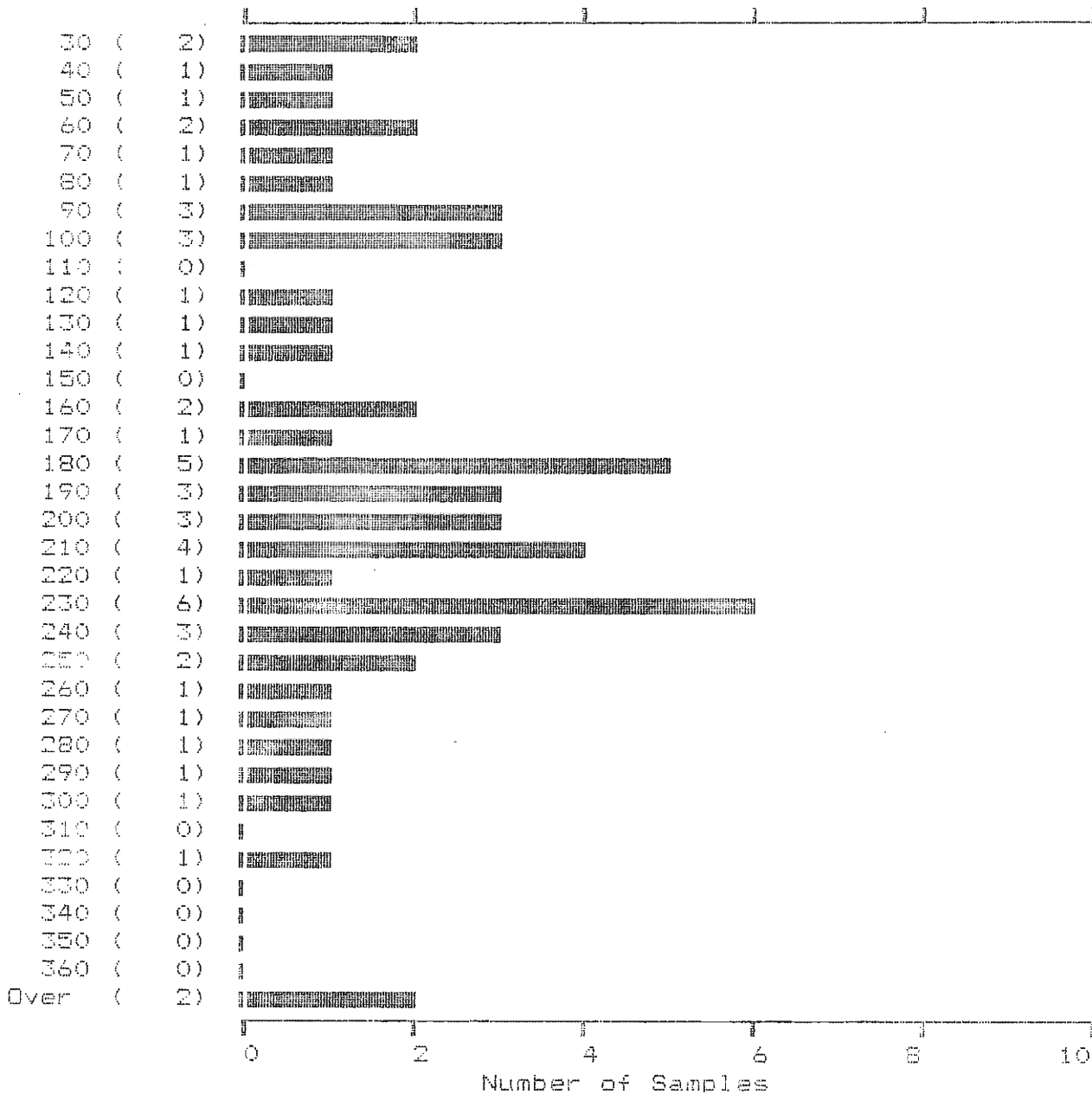
Mean: 132

Minimum: 5

Standard Deviation: 609

C.E.C. ENGINEERING

NI
(PPM)



55 Samples

Maximum: 788

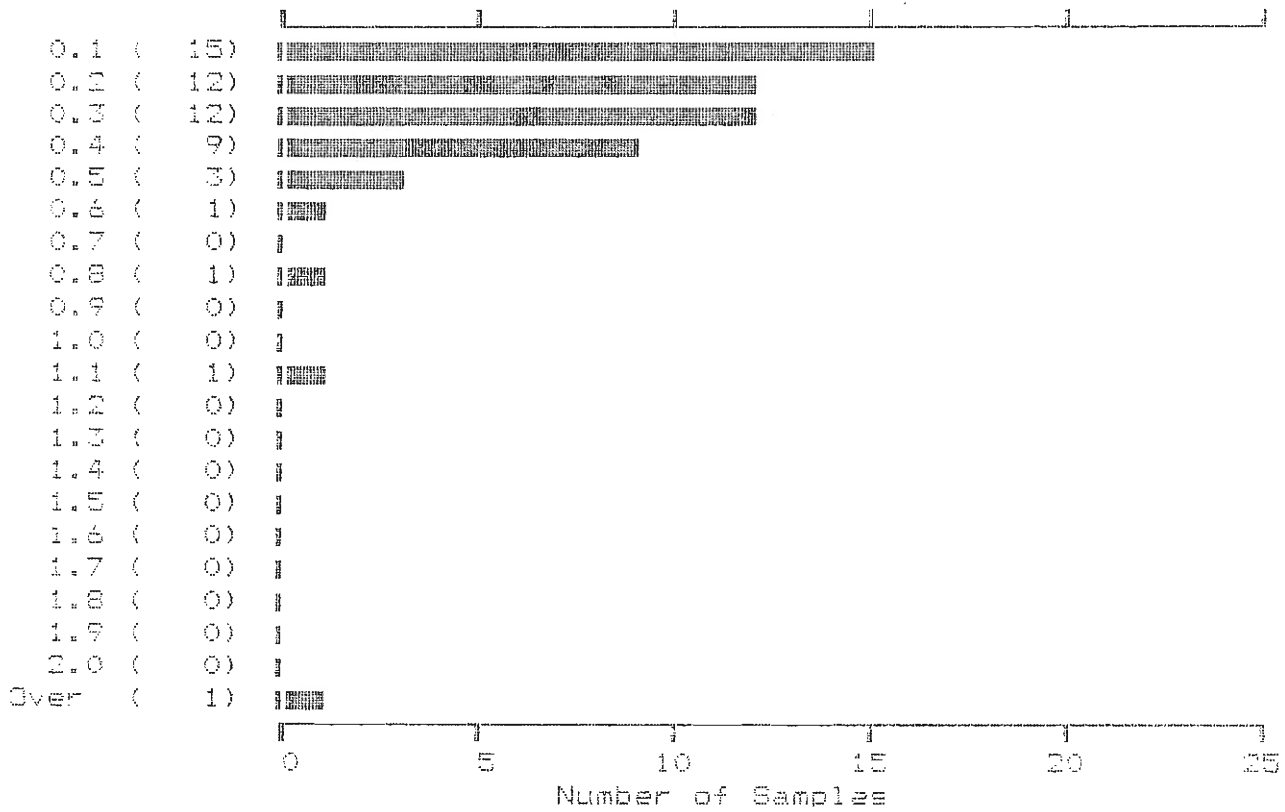
Mean: 186

Minimum: 24

Standard Deviation: 113

C.E.C. ENGINEERING

AS
(PPM)



55 Samples

Maximum: 2.6

Minimum: 0.1

Mean: 0.3

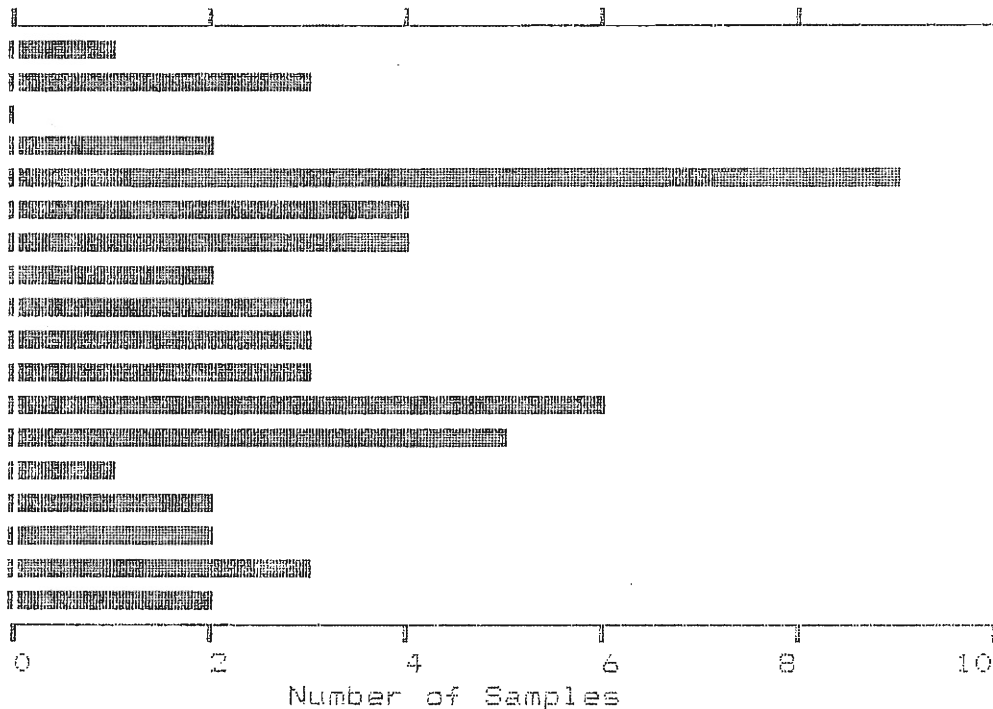
Standard Deviation: 0.4

C.E.C. ENGINEERING

SR

(PPM)

40 (1)
50 (3)
60 (0)
70 (2)
80 (9)
90 (4)
100 (4)
110 (2)
120 (3)
130 (3)
140 (3)
150 (6)
160 (5)
170 (1)
180 (2)
190 (2)
200 (3)
210 (2)



55 Samples

Maximum:

205

Mean:

120

Minimum:

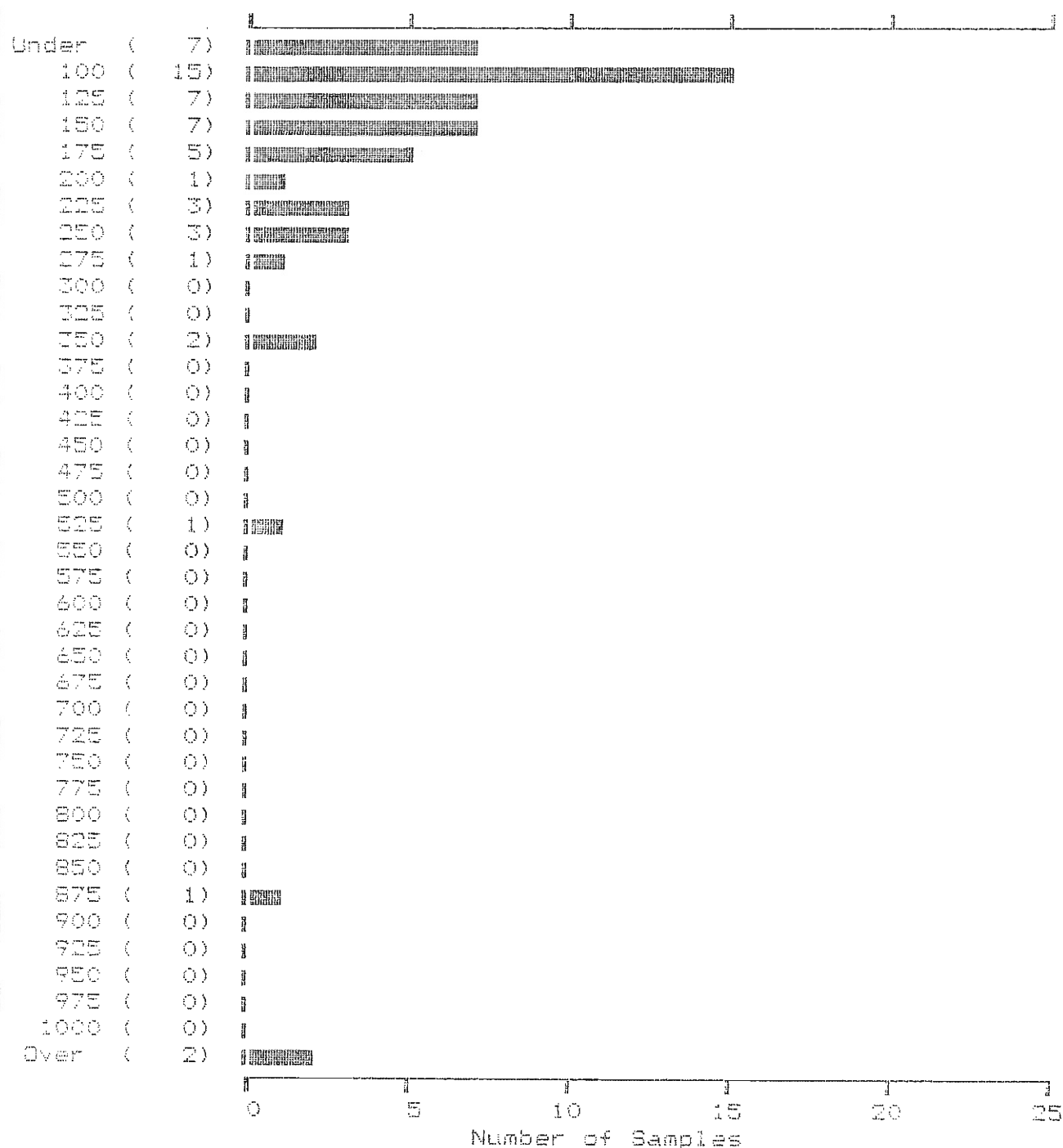
36

Standard Deviation:

45

C.E.C. ENGINEERING

ZIN
(PPM)



55 Samples Maximum: 7252 Mean: 357
 Minimum: 52 Standard Deviation: 1089

APPENDIX VII

LITHOGEOCHEMICAL SAMPLE DESCRIPTIONS

TWIN PROPERTY - LITHOGEOCHEMICAL SAMPLE DESCRIPTIONS

Project	Sample Grid	Coordinates		Description
Code	No.	Easting	Southing	
86-14	1	53+00	0+50	Fine-grained, silicified mafic volcanic flow with 5 to 10 pyrite disseminations.
86-14	2	60+00	5+00	Silicified lapilli tuff with 10 % pyrite disseminations.
86-14	3	59+00	7+75	Quartz, calcite veining in fault zone of massive mafic flow.
86-14	4	59+00	5+50	Quartz, carbonate, pyrite vein material in silicified mafic volcanic.
86-14	5	56+00	4+50	Pyritic vein material from a silicified lapilli tuff.
86-14	6	57+50	0+35	Massive, fine-grained mafic flow with 20% disseminated pyrite in quartz-calcite vein.
86-14	7	62+00	4+20	Quartz-sericite-carbonate vein material in altered fine-grained mafic volcanic.
86-14	8	80+00	4+65	Schistose mafic volcanic with more than 10% pyrite disseminations.
86-14	9	65+00	2+46.5	Silicified lapilli tuff - 3m. chip sample
86-14	10	65+00	2+49.5	Silicified lapilli tuff w/ 2 to 4% pyrite diss'ns. - 3m. chip sample
86-14	11	65+00	2+70	Till sample for geochem interpretation - 4 m. sample.
86-14	12	65+00	3+05	Grab sample of lapilli tuff.
86-14	13	65+00	3+50	Silicified, massive mafic flow or possible subvolcanic intrusive - 3 m. chip sample.
86-14	14	78+66	2+78	Fault zone. Light brown mylonitic material - 1 m. sample.
86-14	15A	78+66	2+79	Muddy tuff with local quartz-pyrite fracture fillings - 1 m. sample.
86-14	15B	78+66	2+80	Muddy tuff with local quartz-pyrite fracture fillings - 1 m. sample.
86-14	15C	78+66	2+81	Muddy tuff with local quartz-pyrite fracture fillings - 1 m. sample.
86-14	16A	78+66	2+82	Silicified lapilli tuff with 1 to 2% pyrite diss'ns. - 1 m. sample.
86-14	16B	78+66	2+83	Silicified lapilli tuff with 1 to 2% pyrite diss'ns. - 1 m. sample.
86-14	17	78+66	2+84	Schistose and talcose mafic lapilli tuff with thinly laminated argillite.
86-14	18	78+66	2+60	Relatively fresh but foliated mafic volcanics - 3 m. sample.
86-14	19	78+66	2+57	Relatively fresh but foliated mafic volcanics - 3 m. sample.
86-14	20	78+66	2+54	Relatively fresh but foliated mafic volcanics - 3 m. sample.
86-14	21	78+00	1+72	Siliceous lapilli tuff with less than 1 to 5% pyrite diss'ns - 3 m. sample.
86-14	22	78+00	1+69	Siliceous lapilli tuff with less than 1 to 5% pyrite diss'ns - 3 m. sample.
86-14	23	78+00	1+66	Siliceous lapilli tuff with less than 1 to 5% pyrite diss'ns - 3 m. sample.
86-14	24	78+00	1+63	Siliceous lapilli tuff with less than 1 to 5% pyrite diss'ns - 3 m. sample.
86-14	25	78+00	1+61	Siliceous lapilli tuff with 1% pyrite diss'ns - 3 m. sample.
86-14	26	80+00	2+67	Siliceous muddy tuff with 5% pyrite diss'ns - 2 m. sample.
86-14	27	80+00	2+69	Siliceous muddy tuff with 5% pyrite diss'ns - 2 m. sample.
86-14	28	80+00	2+71	Siliceous muddy tuff - 5 m. sample.
86-14	29	80+00	2+76	Siliceous muddy tuff - 6 m. sample.
86-14	30	80+00	2+82	Siliceous muddy tuff - 4 m. sample.
86-14	31	80+00	3+21	Black to dark grey, thinly laminated argillite - 2 m. sample.
86-14	32	81+00	2+97	Black to dark grey, thinly laminated, graphitic argillite - 2 m. sample.
86-14	33	81+00	3+01	Black to dark grey, thinly laminated, graphitic argillite - 2 m. sample.
86-14	34	78+00	1+58	Siliceous mafic volcaniclastic with 8 cm. qz vein, 10% pyrite and minor galena - 3 m. sample.
86-14	35	78+00	1+55	Siliceous mafic lapilli tuff with 2 % pyrite diss'ns. - 3 m. sample.
86-14	36	78+00	1+52	Siliceous mafic lapilli tuff with 2 % pyrite diss'ns. - 3 m. sample.
86-14	37	78+00	1+50	Siliceous mafic lapilli tuff with 2 % pyrite diss'ns. - 2 m. sample.
86-14	38	67+00	3+96	Well altered mafic tuff with py diss'ns. and mp alteration - 3 m. sample.
86-14	39	67+00	3+93	Well altered mafic tuff with py diss'ns. and mp alteration - 3 m. sample.
86-14	40	67+00	3+90	Same as 8614-38 with 5 cm. qz vein w/ py, gl, cp and sp diss'ns. in vein - 3 m. sample.
86-14	41	67+00	3+87	Same as 8614-38 - 3 m. sample.
86-14	42	67+00	3+84	Contact between mafic flow breccia and lapilli tuff - 3 m. sample.

TWIN PROPERTY - LITHOGEOCHEMICAL SAMPLE DESCRIPTIONS

=====				
Project	Sample	Grid	Coordinates	Description
Code	No.	Easting	Southing	

86-14	43	67+00	3+81	Foliated mafic tuff - 3 m. sample.
86-14	44	67+00	3+78	Foliated mafic tuff - 3 m. sample.
86-14	45	67+00	3+75	Foliated mafic tuff - 3 m. sample.
86-14	46	80+00	2+40	Relatively fresh mafic volcanic - 3 m. sample.
86-14	47	80+00	2+51	Relatively fresh mafic volcanic - 3 m. sample.
86-14	48	67+00	3+50	Light green, chloritic lapilli tuff - 3 m. sample.
86-14	49	67+00	3+47	Light green, chloritic lapilli tuff - 3 m. sample.
86-14	50	67+00	3+44	Light green, chloritic lapilli tuff - 3 m. sample.
86-14	51	67+00	3+41	Light green, chloritic lapilli tuff - 3 m. sample.
86-14	52	67+00	3+38	Light green, chloritic lapilli tuff - 3 m. sample.
86-14	53	67+00	3+35	Light green, chloritic lapilli tuff - 3 m. sample.
86-14	54	67+00	3+32	Light green, chloritic lapilli tuff - 3 m. sample.
86-14	55	67+00	3+29	Light green, chloritic lapilli tuff - 3 m. sample.
86-14	56	65+00	2+52.5	Siliceous lapilli tuff - 3 m. sample
86-14	57	70+30	3+53.5	Ankeritic volcanoclastic. Contact (122/48NE) between flow and tuff - 2.5 m. sample.
86-14	58	70+30	3+49.5	Light grn to brn silicified lapilli tuff with 2 to 5% py diss'ns. and ap - 3 m. sample.
86-14	59	70+30	3+46	Light grn to brn silicified lapilli tuff with 2 to 5% py diss'ns. and ap - 3.5 m. sample.
86-14	60	70+30	3+42	Light grn to brn silicified lapilli tuff with 2 to 5% py diss'ns. and ap - 4 m. sample.