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825951

REPORT OF FIELD PROGRAM

MATAJUR AND EL NINIO CLAIM GROUPS

Queen Charlotte Islands, B.C.

February, 1990

for:

DOROMIN RESOURCES LTD.
827 W. Pender St.
Vancouver, B.C.

R. F. McIntyyre, B.Sc., Geologist
J. F. McIntyre, B.Sc., P.Eng.

February 28, 1990

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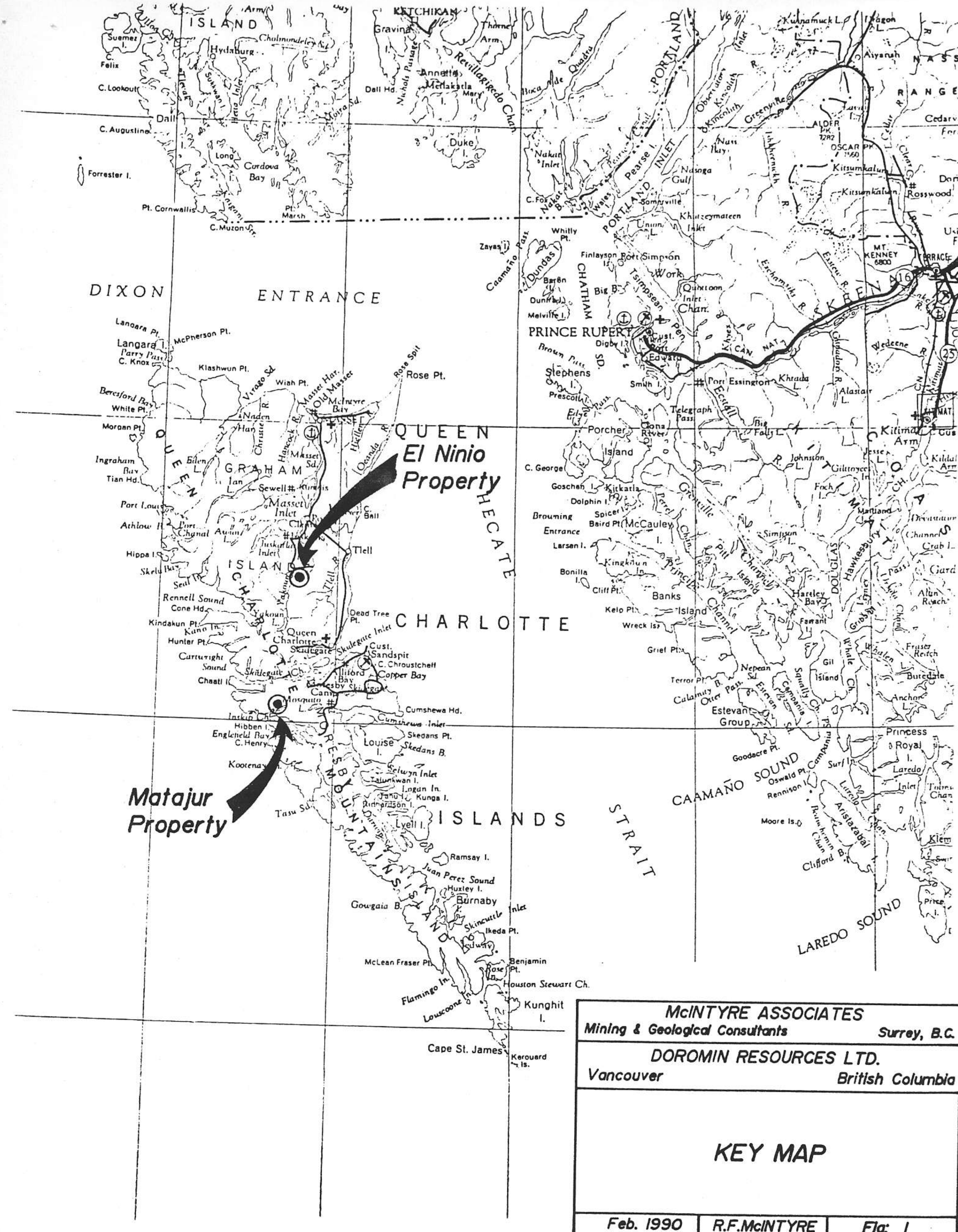
ILLUSTRATIONS



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Mining & Geological Consultants — *Surrey, B.C.*

DOROMIN RESOURCES LTD.
Vancouver — *British Columbia*

KEY MAP

Feb. 1990 | R.F.McINTYRE | Fig: 1

INTRODUCTION

The authors were commissioned by Mr. Marino Specogna of Doromin Resources Ltd., a Vancouver company, to conduct a field program on their El Ninio and Matajur claim groups, located on the Queen Charlotte Islands, British Columbia.

These properties have received only minor exploration effort in the past so the work conducted was of a preliminary nature, designed to investigate several mineralized showings and to test the efficacy of the exploration methods under local property conditions. To this end reconnaissance silt sampling was carried out on both properties, a small scale soil sampling grid was established and sampled over a known mineralized zone on the El Ninio property, two massive sulphide showings were located, sampled and investigated by geophysical means on the Matajur property and the area of the soils grid on the El Ninio property tested by the same geophysical methods.

The program was completed in a timely manner with only minimal delays due to weather conditions. However snow cover prevented geological examination of showings on the El Ninio property and restricted the scope of activities on the Matajur property. The work was conducted entirely in the month of February, 1990.

PROPERTIES

The February 1990 field work was divided between two properties, both owned by Doromin Resources Ltd., located on the Queen Charlotte Islands, B.C.

The first, the El Ninio property consists of the El Ninio claim, an eight unit 4-post mineral claim, record #7749, and an adjoining fractional mineral claim, the El Nino fraction, #7914. This property is located in the east-central portion of Graham Island, at Lat. 53° 28' N, Long. 132° 10' W. It lies approximately 7 km to the southeast of the Cinola gold deposit, a property containing over 40 million tonnes of mineable reserves.

There is presently no road access to the El Ninio property, however a good logging road runs to within 2 km of the southwest corner of the property and additional bulldozer trails exist to the west of the property at similar or shorter distances. Completion of a road to the property would greatly facilitate future exploration efforts. The short distance involved ensures that the cost would be minimal, fully balanced by the savings of helicoptor transportation charges and other support costs during even a modest exploration program.

The Matajur property consists of four contiguous 4-post mineral claims totalling 76 units. The claim names are the Matajur 1, #7672, the Matajur 2, #7673, the Matajur 3, #7674, and the Matajur 4, #7675. As the four claims were staked from a common Legal Corner Post no gaps or fractions exist.

The Matajur claims are located on the northwest corner of Moresby Island at Lat. 53° 03' N, Long. 132° 19' W. Road access exists to within approximately 3 km of the claim boundary and 5 km of tidewater at Security Cove. Future activity might justify construction of an access road to this latter point. The steep topography of the property would make road building to other areas of the claims difficult, and the expense would have to be justified by a more pressing need.

The Matajur claims lie immediately west of the Cimadoro property, also owned by Doromin Resources Ltd. The Cimadoro main showing has returned assays of up to 1.3 oz./ton of gold.

GEOLOGY

The geological settings of the two properties are quite different. No small scale geological maps of either area have been published. Also, large areas of the eastern portions of the Islands are blanketed by thick sections of recent alluvium.

The El Ninio property appears to have very little bedrock exposure, being mainly covered by swamp and varying amounts of overburden. Some two feet of snow blanketed the property during the February 12 - 25 period of field work so the authors were unable to examine any outcrops or showings. Based on large scale published maps the property is underlain by middle Jurassic andesites and agglomerates of the Yakoun Group. Some portions of the property, particularly on the north end, may be underlain by Cretaceous sedimentary rocks of the Queen Charlotte Group. On a previous, brief visit to the claim (January 28/90) less snow was present and some bedrock was visible in the banks of Canyon Creek. These were fine grained, buff weathered volcanic rocks considerably oxidized and clay-altered, and obviously highly pyritic. As well, soils in the area were stained dark red and appear to be very iron-rich. Float found in the creek contained several percent pyrite as well as fine grained bornite, and possibly some barite as well. This area was therefore chosen for more intense examination and is the site of the geochemical/geophysical grid.

The Matajur property is dominated by sharp topographic relief, numerous cliffs and bluffs and little overburden above the valley floors. Much of the property is underlain by basalts of the Karmutsen Formation, along with minor limestone lenses within the volcanic sequence. These rocks are prominent along the shoreline. However, several cliffs located to the northeast of MacKenzie Cove and along the north side of Security Inlet reveal thick sequences of light colored, thinly bedded sedimentary rocks. The authors did not examine these but large scale map information suggests that they are limestones and argillites of the Triassic and Jurassic Kunga Formation, a rock unit which is known to occur near the Matajur property on the northwest portion of Moresby Island.

Two showings were located by the R.F. McIntyre in the area of Mackenzie Cove. These had previously been examined by J. F. McIntyre in 1963, along with other showings located on property adjacent to the Matajur claims. All of these are massive sulphide occurrences within the Karmutsen volcanic rocks.

The locations of the two showings are shown on Figure 4. They were sampled as shown on Figure 5 with chip samples taken across outcrops and float samples taken wherever significant quantities were found. Details are as follows:

TABLE 1

Rock Samples - Mackenzie Cove - Matajur Property

Sample #	Type	Length	Cu%	Zn ppm	Ag ppm	Au ppb	Hg ppb
A Zone							
D1	Float	-	0.41	36	0.6	3	230
D2	Float	-	0.30	12	0.9	1	4300
D3	Channel	1.3 m	1.44	252	1.1	1	1800
D4	Chip	5 m	0.37	55	0.7	1	220
D5	Float	-	0.45	67	0.5	3	630
B Zone							
D6	Chip	1.5 m	0.01	234	0.1	1	50
D7	Chip	10 m	1.47	298	2.5	1	200
D8	Chip	5 m	0.91	49	0.6	4	180

The westerly showing, herein termed the "A" zone, was found in a small, steep gully beginning just above sea level on the west side of MacKenzie Cove. The gully is formed by a fault striking 160° and dipping 70° E. The lower part of the area is covered by slide debris and the upper part is steep and un-vegetated. The topography of the area consists entirely of steep slopes and broken cliffs.

Float boulders consisting of massive pyrrhotite with minor chalcopyrite were found at locations D1, D2 and D5. No outcrop occurrence with this characteristic was seen though a mineralized pod about 1.3 x 2.0 m was sampled at D3 and a much large pyritized zone, at least 5m x 15 m in extent, was sampled at D4. This zone appears to continue on the cliff face for a considerble distance to the southwest, but could not be reached for examination. A massive pyrrhotite were not visited due to rough sea conditions and shortage of time. Prospecting of these areas to re-locate the showings is recommended.

It is apparent from past work in the area of the Matajur property and work on adjoining properties such as the Cimadoro that the geological setting is very favorable for the discovery of mineralization, particularly massive sulphide deposits. The authors believe that a thorough program of prospecting this large area would result in the discovery of additional showings. The remote location, steep topography and often inclement weather conditions have limited past efforts, much of which were confined to near-shore regions. Extension of efforts to more inland sections would likely result in additional discoveries. It should be noted that the geological setting of Westmin's Lynx, Myra and H W deposits on Vancouver Island is substantially the same as that of northwestern Moresby Island.

GEOCHEMISTRY

The bulk of fieldwork consisted of three phases of geochemical investigations. These were; (a) establishment of a grid and detailed soil sampling of a portion of the El Ninio property, (b) reconnaissance silt sampling of the El Ninio property and (c) reconnaissance silt sampling of the Matajur property. Partial results are presented on Figures 2, 3 and 4 respectively. Samples were subjected to a 30 element I.C.P. analysis by Acme Analytical Laboratories Ltd. of Vancouver, B.C. and atomic absorbtion assays for mercury, gold and barite. The full results are tabulated in Appendix I.

The soil sample grid on the El Ninio property was established from a baseline cut along the western boundary of the El Ninio claim commencing at the Legal Corner Post on the northwest corner of the claim. Stations were placed every 50 m along the baseline for 2000 m south of the L.C.P. Distances were measured with a 100 m nylon chain. All claimposts along the west boundary were located.

A detailed grid was established from stations 1000 m S to 1500 m S inclusive. Cross lines were run from each 50 m station for 100 m to the west and 300 m to the east of the baseline, with flagged sampling sites established every 20 m. As well, sample sites were established every 25 m along the baseline. Lines 1450 S and 1500 S were not run to the west of the baseline. Line 1000 S was run to 1000 m E with sample sites established every 50 m from 300 m E to 1000 m E. The resulting grid totals some 231 sample sites, as shown on Figure 2.

Because of thick snow cover and the prevalent swampy, organic soils, only 150 samples of mineral soil were collected. Future soil sampling could obtain a higher percentage of successfully taken samples if (a) a soil sampling auger is employed to reach greater depths and (b) sampling is conducted when the ground is clear of snow.

Silt samples were taken from 45 locations on two drainages on the El Ninio property. Results are presented on Figure 3. With additional time and absence of snow cover the silt sampling program can be extended beyond the areas covered in the February field program.

A similar silt sampling program totalling 61 samples was conducted on the two main drainages of the Matajur property, as shown on Figure 4. The locations shown are approximate. Many areas were not reached because of time constraints. There are numerous small streams flowing into the major watercourses which could be sampled if an extended effort was made. Such a program would provide better information in most areas than soil sampling, and at much lower cost. The authors recommend that an extensive program of detailed stream silt sampling be carried out over the entire Matajur property as a primary component of the next phase of exploration.

Results of the silt and soil assays show no anomalous values in Mo, Cu, Zn, Pb, Ba, Ag, Cd, Ni or Co. on either property. Values of As above 40 ppm were found in the Matajur silt samples only. Elevated values of Mn and Fe ranging from 5000-26,000 ppm Mn and 10-36% of Fe occur in both silts and soils, though the I.C.P. digest is incomplete for these elements and accuracy is therefore questionable. As well, anomalous values of Hg were found in all three sampling categories. These warrant further discussion.

Separate background cutoff values of Hg were chosen for the three sample categories. For the El Ninio soil samples a figure of 300 ppb was used, in line with work done by others in the area. For the El Ninio silt samples a cutoff figure of 200 ppb was chosen, as the authors feel this more accurately reflects the distribution of silt sample values. For the Matajur silt samples the statistical technique of "probability plot partitioning" was used to separate background from anomaly populations. The cumulative probability graph is included in Appendix 1.

From this it is clear that both background and anomaly values are much higher than those of the El Ninio. The author attributes this to the mineralogically richer volcanic geological environment of the Matajur property and its relative lack of glacially derived overburden. There is little overlap of background and anomaly populations. A cutoff figure of 900 ppb of Hg was selected which will exclude about 96% of background values while including some 99% of anomalous values. Eleven of these samples are anomalously high in Hg.

In several areas anomalous samples are clustered. On the El Ninio property silts E38, E44 & E45 are all anomalous in Hg and form a target for future investigation. The Matajur silts form several clusters of which M23 - M30 is a large Hg anomaly. Follow-up work in this area is strongly recommended.

A cluster of anomalous gold assays occurs at E1, E6 and E11 on Figure 3. A large cluster of anomalous gold values occurs in the northwest corner of the soil sample grid on Figure 2. These include the six highest gold values found. Considering the inherent difficulties of soil sampling for gold and the fact that these values are 4 - 8 times the normal background level this is a significant anomaly. The authors recommend follow-up work in this area. In addition, a series of anomalous Hg values runs diagonally across the northern portion of Figure 2. Anomalous Hg and Au have not been found in any one sample, indeed there are no noticeable correlations among anomalous values of any of the elements tested. It appears that Au and Hg mineralization are unrelated and the anomalies identified herein constitute distinctly different exploration targets.

GEOPHYSICS

Geophysical investigation of portions of the Matajur and El Ninio properties was carried out by Strato Geological Engineering Ltd. of Surrey, B.C. under the direction of the authors. Work was carried out from Feb. 22 to 25 inclusive and consisted of ground based magnetometer and V.L.F.-EM surveys.

On the El Ninio property the entire geochemical grid was surveyed, with readings taken every 10 m on the crosslines. On the Matajur property test lines were run across the "A" and "B" zones to determine their geophysical responses. (See Figure 5).

A single line bearing approximately 030° was run for 70 m south and 100 m north of sample location D1. This roughly paralleled the shore at 10 - 50 feet above sea level. Due to very steep terrain no other lines could be run across the "A" zone.

On the "B" showings a short baseline was established between the sites of samples D7 and D8 on a bearing of 050°. From this, two perpendicular lines were run crossing each showing and extending 100 m southeast and 100 m northwest along a bearing of 140°.

No response was seen across the "A" zone. However significant responses were found at the "B" zone. Time limitations prevented extension of this work.

The El Ninio survey revealed several magnetometer anomalies, some of which coincide with weak VLF-EM anomalies. Two of these correspond roughly to the gold anomaly in the northwest corner of the grid and with a cluster of high Hg and Fe values on the west side of the grid. Since the geological features producing these anomalies have not yet been defined the significance of the geophysical results remains unclear.

Complete results of the geophysical survey are present in a separate report by Strato Geological Engineering Ltd. entitled Geophysical Report on the Matajur and El Ninio Properties, Skeena Mining Division, B.C. and dated February 28, 1990.

CONCLUSIONS AND RECOMMENDATIONS

The preliminary field program conducted on the El Ninio and Matajur properties produced significant results. A considerable body of information has been gathered to guide future exploration efforts. The silt and soil sampling, though limited in extent, identified several areas with anomalously high levels of gold (El Ninio) and mercury (Matajur and El Ninio). Two massive sulphide showings were found and sampled (Matajur) and two additional showing have been tentatively identified from previous work. Both properties have merit and should be more intensively explored.

The authors recommend that a two phase exploration program be conducted.

During the first phase, the El Ninio silt sampling, gridding, soil sampling and ground geophysical surveys should be extended to cover the entire property, and an access road should be constructed to facilitate this work. On the Matajur claims the entire property should be thoroughly prospected and silt sampled. Anomalous areas should receive local griding and soil sampling where terrain permits to better define the anomalies. The entire property should receive an airborne geophysical survey.

Conditional on positive results from Phase 1 the authors recommend that anomalies be further tested by a series of short diamond drill holes totalling 1000 meters split between the two properties.

Work on Graham Island can be based in Queen Charlotte city, eliminating the need for a camp, however extensive work on the Matajur claims will require camp facilities, local water transportation and servicing by sea. Work should be planned in such a way as to eliminate dependence on helicopter transport.

Respectfully submitted

R. F. McIntyre, B.Sc. Geologist

J. F. McIntyre, B.Sc. P.Eng.

APPENDIX 1

Sample Assay Sheets

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

Doromin Resources Ltd. File # 90-0514 Page 1

827 W. Pender St., Vancouver BC V6C 3G8

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppb
E 1 P	1	12	17	65	.1	3	24	3174	9.50	9	5	ND	1	33	1	2	2	124	.24	.034	2	16	.97	63	.19	6	1.97	.04	.04	1	90
E 2	1	6	13	46	.1	1	41	6456	6.13	17	5	ND	1	39	1	2	2	109	.24	.030	2	13	.63	83	.15	2	1.52	.02	.03	1	80
E 3	1	19	23	72	.2	9	11	970	5.75	7	5	ND	1	63	1	2	2	128	.33	.036	2	22	1.16	99	.18	5	3.27	.02	.03	1	130
E 4	1	14	15	78	.1	7	13	1227	5.00	9	5	ND	1	96	1	2	2	154	.46	.029	2	25	1.78	102	.24	2	3.50	.03	.04	1	80
E 5 P	1	18	16	74	.2	8	13	1382	5.98	3	5	ND	1	66	1	2	2	155	.45	.033	2	24	1.78	84	.23	2	2.99	.04	.05	1	90
E 6	2	9	20	53	.1	5	5	479	1.34	2	5	ND	1	58	1	2	2	49	.36	.023	2	15	.77	124	.17	4	1.74	.02	.03	1	130
E 7	1	10	23	59	.1	6	18	2896	3.69	2	5	ND	1	118	1	2	2	85	.66	.028	2	19	1.11	133	.19	2	2.51	.03	.04	1	80
E 8	1	12	11	67	.1	9	14	1311	5.15	4	5	ND	1	105	1	2	2	125	.60	.031	2	21	1.53	107	.23	2	2.84	.03	.05	1	90
E 9	1	14	18	51	.1	9	10	693	2.96	2	5	ND	1	110	1	2	2	91	.52	.033	2	21	1.15	111	.18	3	3.44	.03	.04	2	480
E 10	1	12	14	45	.2	5	8	579	3.29	3	5	ND	1	104	1	2	3	99	.49	.031	2	18	.87	110	.17	4	2.31	.03	.04	1	100
E 11	1	22	20	68	.2	8	14	1691	4.46	3	5	ND	1	94	1	2	2	130	.67	.031	3	23	1.29	114	.21	4	3.23	.04	.05	1	140
E 12 P	1	30	12	123	.2	16	21	2632	6.91	6	5	ND	1	94	1	2	2	139	.63	.043	3	27	1.96	126	.20	4	4.09	.05	.07	1	90
E 13	1	26	9	129	.3	17	25	4454	7.03	6	5	ND	1	99	1	2	2	143	.60	.036	3	29	1.64	174	.17	2	4.89	.03	.06	1	100
E 14	1	26	8	125	.2	13	22	3233	6.68	6	5	ND	1	91	1	2	2	142	.70	.035	3	28	1.75	133	.18	4	4.35	.04	.06	1	80
E 15	1	25	10	115	.1	13	21	3163	5.97	3	5	ND	1	94	1	2	2	133	.67	.040	3	26	1.55	139	.17	2	4.12	.03	.05	1	60
E 16	1	28	17	138	.3	15	23	3390	6.68	4	5	ND	1	99	1	2	2	137	.73	.038	3	28	1.73	146	.17	2	4.61	.04	.06	1	80
E 17	1	28	10	137	.4	14	23	3719	7.14	3	5	ND	1	89	1	2	2	139	.66	.037	3	28	1.78	145	.18	2	4.46	.04	.06	1	60
E 18	1	25	12	135	.3	15	23	3726	6.77	5	5	ND	1	92	1	4	2	136	.64	.036	3	29	1.71	146	.17	3	4.38	.04	.05	1	70
E 19 P	1	22	2	110	.1	13	18	1950	5.35	2	5	ND	1	64	1	2	2	126	.47	.030	3	23	1.64	104	.17	2	3.49	.04	.07	1	60
E 20 P	1	21	14	115	.1	12	17	1117	5.46	2	5	ND	1	66	1	2	2	126	.43	.029	3	22	1.56	114	.16	7	3.75	.05	.07	1	80
E 21 P	1	25	14	120	.2	13	19	2221	5.89	5	5	ND	1	74	1	2	2	129	.50	.034	3	25	1.75	115	.19	7	3.69	.05	.07	1	70
E 22 P	1	21	7	116	.1	11	20	3535	5.82	2	5	ND	1	64	1	2	2	120	.44	.031	3	21	1.51	122	.15	2	3.60	.04	.07	1	80
E 23 P	1	17	15	103	.1	11	16	2011	5.13	2	5	ND	1	47	1	2	2	108	.28	.027	2	20	1.36	118	.10	6	3.51	.03	.08	1	60
E 24 P	1	19	4	98	.1	12	15	1568	4.99	2	5	ND	1	57	1	2	2	110	.33	.030	2	22	1.32	134	.10	3	3.68	.03	.08	1	50
E 25 P	1	20	11	95	.1	8	14	1531	4.57	2	5	ND	1	34	1	2	2	108	.25	.026	2	18	1.26	96	.10	2	2.93	.02	.08	1	60
E 26 P	1	23	11	100	.1	9	16	2372	5.00	3	5	ND	1	35	1	2	2	105	.29	.031	3	17	1.31	115	.09	8	3.10	.03	.11	1	70
E 27 P	1	19	15	97	.2	7	15	2320	5.01	2	5	ND	1	33	1	2	2	99	.28	.033	2	16	1.33	99	.06	6	3.00	.03	.10	1	50
E 28 P	1	41	9	61	.2	15	32	1122	7.91	2	5	ND	1	28	1	2	2	78	.42	.036	3	19	1.43	44	.03	5	2.84	.03	.10	1	100
E 29 P	1	29	15	87	.1	9	15	1637	5.42	3	5	ND	1	45	1	2	2	109	.51	.042	3	18	1.76	75	.09	6	3.17	.04	.10	1	70
E 30 P	1	23	8	95	.2	8	16	1750	5.18	2	5	ND	1	37	1	2	2	106	.40	.033	3	21	1.74	77	.09	2	3.33	.04	.10	1	50
E 31 P	1	20	12	94	.1	9	14	1518	4.63	3	5	ND	1	39	1	2	2	99	.37	.030	3	18	1.66	79	.08	4	3.35	.03	.10	1	60
E 32 P	1	21	6	107	.2	12	17	1944	5.43	6	5	ND	1	56	1	3	2	122	.43	.030	3	21	1.64	93	.17	3	3.26	.04	.08	1	120
E 33 P	1	22	4	112	.1	10	17	2075	5.50	3	5	ND	1	57	1	2	2	119	.43	.031	3	20	1.68	97	.16	3	3.35	.04	.08	1	50
E 34 P	1	26	16	110	.1	11	17	2111	5.40	2	5	ND	1	55	1	2	2	119	.43	.028	3	23	1.52	112	.15	2	3.17	.04	.08	1	70
E 35 P	1	20	8	105	.2	11	16	1926	5.08	5	5	ND	1	59	1	2	2	115	.42	.028	2	20	1.53	105	.14	7	3.32	.04	.07	2	80
E 36 P	1	20	16	105	.2	11	16	1976	5.03	6	5	ND	1	54	1	3	2	114	.42	.027	3	23	1.50	103	.14	6	3.19	.04	.08	2	70
STD C	17	57	38	127	6.6	70	29	937	3.87	42	18	8	36	47	18	15	18	56	.45	.094	36	56	.89	173	.06	37	1.83	.06	.14	12	1300

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: P1-P9 Soil P10 Rock HG ANALYSIS BY FLAMELESS AA.

P - PULVERIZED

DATE RECEIVED: FEB 28 1990 **DATE REPORT MAILED:** March 8/90 **SIGNED BY**..........D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

Doromin Resources Ltd. FILE # 90-0514

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppb
E 37 P	1	19	13	100	.1	10	16	2047	5.17	2	5	ND	1	51	1	2	2	116	.42	.029	2	23	1.52	95	.15	2	3.23	.04	.08	1	80
E 38 P	1	18	13	100	.1	9	16	2277	5.11	2	5	ND	1	53	1	2	2	123	.41	.027	2	24	1.41	93	.16	2	3.10	.04	.07	1	230
E 39 P	1	23	10	94	.2	8	16	3025	5.24	2	5	ND	1	50	1	2	2	132	.45	.028	3	25	1.37	93	.17	2	2.92	.04	.08	1	80
E 40 P	1	21	10	94	.1	9	16	1918	5.05	2	5	ND	1	52	1	2	2	120	.43	.029	2	22	1.44	91	.15	2	3.08	.04	.07	1	90
E 41 P	1	26	4	93	.1	10	19	2798	5.86	7	5	ND	1	53	1	2	2	133	.44	.036	3	26	1.48	95	.18	2	3.17	.05	.07	1	80
E 42 P	1	27	7	87	.1	9	19	3168	5.55	7	5	ND	1	62	1	2	2	138	.48	.034	3	25	1.35	105	.19	7	3.13	.05	.08	1	100
E 43 P	1	25	4	96	.1	10	19	2980	5.83	2	5	ND	1	46	1	2	2	125	.36	.031	2	25	1.42	99	.15	2	3.17	.04	.07	1	90
E 44 P	1	12	10	47	.1	6	11	1094	3.65	2	5	ND	1	38	1	2	2	101	.23	.019	2	19	1.06	80	.15	2	2.46	.03	.06	1	620
E 45 P	1	17	8	80	.2	7	16	1800	5.33	4	5	ND	1	38	1	2	2	121	.27	.030	2	22	1.31	77	.15	9	2.63	.03	.07	1	340
G 1 P	1	33	6	71	.1	21	15	664	3.65	7	5	ND	1	39	1	2	2	77	.63	.055	3	41	1.39	52	.15	3	2.02	.03	.09	1	520
G 2 P	1	37	6	73	.1	24	17	595	3.95	6	5	ND	1	35	1	2	2	82	.58	.051	3	42	1.42	58	.15	7	2.03	.03	.09	1	350
G 3 P	1	37	10	60	.1	18	20	863	5.34	11	5	ND	1	33	1	2	2	121	.41	.036	4	55	1.19	46	.16	3	3.21	.03	.08	1	210
G 4 P	1	30	2	58	.1	23	12	413	3.22	5	5	ND	1	39	1	2	2	79	.45	.047	4	49	1.40	35	.14	2	2.32	.03	.10	1	320
G 5 P	1	26	9	57	.1	18	12	466	3.04	4	5	ND	1	25	1	2	2	63	.54	.059	4	32	1.20	37	.13	5	1.64	.03	.07	2	400
G 6 P	1	45	11	113	.1	24	17	644	3.72	9	5	ND	1	57	1	3	2	82	1.02	.077	3	44	1.64	34	.18	5	2.34	.05	.06	1	280
G 7 P	1	24	6	71	.2	19	14	613	3.42	6	5	ND	1	47	1	2	3	78	.81	.065	2	38	1.49	25	.18	5	2.04	.04	.06	1	180
G 8 P	1	29	11	50	.1	21	21	654	4.50	3	5	ND	1	42	1	2	2	114	.70	.058	2	45	1.40	16	.22	4	2.14	.05	.05	1	130
G 9 P	1	19	11	50	.1	19	19	972	4.17	2	5	ND	1	54	1	2	2	91	.64	.048	2	42	1.28	19	.18	2	2.02	.04	.04	1	320
G 10 P	1	27	13	93	.3	13	18	1430	5.47	6	5	ND	1	47	1	2	2	115	.48	.044	3	31	1.60	73	.18	5	2.94	.04	.08	1	160
G 11 P	1	41	13	84	.1	24	17	675	4.07	6	5	ND	1	38	1	2	2	84	.62	.056	3	45	1.49	51	.15	5	2.16	.03	.09	1	350
G 12 P	1	33	4	71	.1	20	15	600	3.56	7	5	ND	1	32	1	2	2	70	.61	.062	3	37	1.37	45	.14	5	1.84	.03	.07	1	310
G 13 P	1	65	112	401	.2	33	20	634	4.24	8	5	ND	1	49	1	3	2	92	.70	.053	2	64	2.06	38	.17	2	2.77	.03	.07	1	240
G 14 P	1	74	37	527	.2	39	23	667	4.80	3	5	ND	1	67	2	5	2	103	.86	.073	2	70	2.18	42	.15	2	2.80	.03	.06	1	11000
G 15 P	1	55	20	180	.1	35	17	483	3.47	2	5	ND	1	66	1	2	2	69	1.22	.101	2	60	2.06	14	.17	8	2.38	.04	.03	1	150
M 1	2	37	15	38	.4	9	41	3557	13.16	41	5	ND	1	35	1	2	2	122	.57	.059	3	33	.70	102	.09	3	2.58	.02	.03	1	2500
M 2	1	33	3	41	.1	15	12	440	3.88	8	5	ND	1	43	1	2	2	88	.72	.037	2	31	1.00	61	.15	6	2.17	.02	.03	1	1600
M 3	1	32	6	45	.1	15	14	670	3.93	11	5	ND	1	40	1	2	2	92	.64	.041	2	33	1.02	62	.13	2	2.19	.02	.03	1	780
M 4	7	36	7	49	.1	19	13	367	3.39	4	5	ND	1	65	1	2	2	70	1.24	.068	2	35	1.26	36	.14	7	2.37	.02	.05	1	270
M 5	2	9	4	36	.1	13	14	993	2.34	5	5	ND	1	16	1	2	2	69	.30	.041	3	33	.62	23	.02	2	1.37	.01	.05	2	5200
M 6	1	5	10	26	.1	16	8	242	1.74	2	5	ND	1	15	1	2	2	51	.54	.027	2	38	1.22	15	.14	5	1.52	[illegible]	.02	1	330
M 7	1	9	5	23	.1	8	5	166	1.17	2	5	ND	1	9	1	2	2	40	.25	.017	2	24	.88	8	.16	2	1.02	.02	.02	2	110
M 8	1	33	10	66	.1	22	23	1638	4.72	12	5	ND	1	33	1	2	3	105	.55	.047	3	45	1.22	73	.11	2	2.53	.02	.04	1	380
M 9	1	29	7	69	.1	26	23	1898	5.02	7	5	ND	1	25	1	2	3	106	.40	.041	3	53	1.37	74	.10	9	2.35	.02	.05	1	230
M 10	1	23	3	73	.2	22	32	8262	5.18	43	5	ND	1	31	1	2	2	109	.60	.044	3	48	1.23	158	.10	7	2.37	.02	.05	1	540
M 11	1	28	9	49	.1	19	16	949	4.68	7	5	ND	1	17	1	2	2	106	.27	.036	4	41	1.07	43	.05	2	2.03	.01	.05	1	610
M 12	1	14	4	54	.2	18	18	1947	3.42	8	5	ND	1	21	1	2	2	87	.35	.035	2	46	1.14	46	.09	4	1.99	.02	.04	1	160
STD C	18	57	41	128	6.9	67	31	959	3.97	40	17	7	36	47	19	15	19	57	.45	.094	37	58	.87	174	.07	39	1.93	.06	.14	11	1300

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SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppb
M 13	1	28	13	58	.1	21	26	2620	5.27	10	5	ND	1	24	1	2	2	106	.37	.043	3	42	1.18	75	.07	2	2.31	.02	.06	1	250
M 14 P	1	28	5	65	.1	20	16	846	4.29	3	5	ND	1	57	1	2	2	89	.86	.046	2	34	1.30	110	.16	3	2.32	.03	.07	1	480
M 15	1	47	4	79	.1	33	25	1869	6.01	9	5	ND	1	28	1	2	2	110	.49	.058	4	50	1.40	144	.07	3	2.76	.01	.09	1	400
M 16	1	55	8	87	.2	37	27	1744	5.86	9	5	ND	1	31	1	2	2	113	.57	.064	4	55	1.52	177	.08	4	2.94	.02	.10	1	760
M 17	1	65	15	59	.1	23	20	909	5.72	8	5	ND	1	20	1	2	2	136	.23	.044	6	54	1.02	55	.08	3	3.47	.02	.05	1	650
M 18	1	39	7	51	.1	14	20	1743	5.90	13	5	ND	1	39	1	2	2	109	.63	.064	4	36	.85	104	.09	2	2.59	.02	.03	1	6200
M 19 P	1	32	7	66	.1	22	21	1701	6.74	11	5	ND	1	39	1	2	2	107	.63	.055	3	37	1.24	70	.13	4	2.43	.04	.08	1	720
M 20	1	37	11	60	.1	13	18	1018	4.62	14	5	ND	1	44	1	3	2	100	.67	.041	3	32	1.11	58	.14	5	2.56	.02	.03	1	570
M 21	1	38	10	54	.1	13	17	1037	4.41	12	5	ND	1	48	1	2	2	99	.76	.043	3	31	1.13	68	.15	4	2.52	.02	.03	1	260
M 22	1	34	2	40	.1	16	15	323	3.34	11	5	ND	1	45	1	2	2	98	.64	.038	4	32	1.05	27	.14	4	3.15	.02	.03	1	760
M 23 P	1	31	8	69	.1	17	15	788	4.30	9	5	ND	1	62	1	2	2	92	.93	.045	2	32	1.41	96	.18	7	2.52	.03	.06	1	950
M 24	2	78	14	105	.3	11	21	899	13.09	63	5	ND	1	31	1	2	2	149	.27	.050	5	46	1.55	24	.13	7	4.11	.01	.03	1	250
M 25	1	65	12	111	.1	16	21	1684	6.27	21	5	ND	1	49	1	2	2	120	.65	.056	4	39	1.79	62	.16	8	3.28	.01	.04	1	210
M 26 P	1	26	3	49	.1	16	14	631	3.93	11	5	ND	1	60	1	2	2	84	1.03	.046	2	30	1.24	141	.18	6	2.31	.04	.06	1	180
M 27	1	30	6	34	.1	14	14	558	3.75	11	5	ND	1	51	1	2	2	88	.81	.036	2	27	.97	97	.15	3	2.15	.02	.03	2	6600
M 28	1	32	4	35	.1	14	13	571	3.51	10	5	ND	1	48	1	2	2	84	.81	.039	3	27	.92	99	.14	6	2.14	.02	.03	3	2300
M 29	1	36	9	39	.1	16	16	633	3.88	12	5	ND	1	50	1	2	3	92	.89	.042	2	29	.95	95	.15	7	2.25	.02	.03	2	12000
M 30	1	36	11	36	.1	14	14	582	3.64	8	5	ND	1	46	1	2	2	90	.85	.040	2	26	.89	81	.15	6	2.21	.02	.03	1	4300
M 31	8	77	8	83	.2	35	30	2047	6.35	33	7	ND	1	47	1	2	2	139	.96	.072	6	59	1.61	46	.26	4	3.01	.02	.06	1	60
M 32	1	34	6	95	.1	29	27	4026	7.25	115	5	ND	1	57	1	2	2	108	1.14	.071	6	51	1.32	233	.19	4	2.49	.01	.05	1	80
M 33	3	60	4	71	.1	31	24	1348	5.50	17	5	ND	1	61	1	2	2	123	.86	.070	5	53	1.55	23	.25	7	2.63	.07	.07	1	1100
M 34	2	70	10	69	.1	30	21	519	5.02	11	5	ND	1	45	1	3	2	126	.87	.054	6	55	1.57	19	.26	5	2.95	.04	.06	1	180
M 35	1	69	5	100	.1	47	24	312	4.16	23	5	ND	1	26	1	2	2	139	.38	.063	13	81	1.82	95	.16	8	3.87	.02	.14	1	110
M 36	1	55	9	54	.1	34	36	2131	5.23	12	5	ND	1	23	1	2	2	117	.24	.058	8	80	1.61	37	.14	5	3.21	.02	.07	1	120
M 37 P	1	31	10	65	.1	33	17	956	5.61	7	5	ND	1	45	1	2	2	105	1.02	.071	4	50	1.64	52	.30	2	2.34	.02	.05	1	30
M 38 P	1	13	2	3	.5	1	4	2411	36.39	12	5	ND	1	42	1	2	2	128	.67	.347	2	29	.12	99	.02	3	.33	.01	.02	1	120
M 39 P	1	31	10	64	.1	20	16	1083	5.66	16	5	ND	1	62	1	2	2	116	1.83	.068	5	45	1.27	126	.18	8	2.54	.02	.06	1	130
M 40	1	68	11	71	.1	31	17	524	5.50	11	5	ND	1	39	1	2	2	123	.88	.050	5	54	1.57	28	.29	4	2.84	.02	.05	1	220
M 41	1	71	9	93	.2	42	24	874	6.21	6	5	ND	1	35	1	2	2	129	.86	.055	4	63	2.00	47	.31	3	3.09	.01	.05	1	140
M 42	1	38	12	90	.2	39	23	698	5.08	11	5	ND	1	35	1	2	2	106	.55	.042	7	64	1.70	72	.15	3	3.15	.01	.12	1	80
M 43	1	44	20	134	.1	55	32	488	5.66	9	5	ND	1	30	1	4	3	115	.46	.075	9	79	2.21	60	.16	3	3.79	.01	.10	1	130
M 44	1	57	6	84	.2	31	23	1362	6.02	13	5	ND	1	50	1	2	2	121	1.07	.072	5	52	1.59	71	.22	5	2.57	.01	.04	1	1600
M 45	1	54	19	187	.1	31	26	1488	6.65	24	5	ND	1	36	1	2	2	116	.65	.066	9	54	1.52	83	.13	3	2.89	.01	.08	1	120
M 46	1	49	4	94	.2	68	28	922	5.80	19	5	ND	1	49	1	2	2	98	.75	.072	5	88	2.02	70	.17	2	2.58	.01	.12	2	90
M 47	1	61	8	84	.2	52	25	1044	5.50	12	5	ND	1	39	1	2	2	112	.78	.049	5	86	2.05	64	.21	5	2.96	.01	.06	1	110
M 48	1	76	15	84	.5	32	25	1177	5.67	22	5	ND	1	34	1	4	2	127	.82	.056	5	56	1.59	61	.26	5	2.88	.01	.05	1	200
STD C	18	57	42	132	7.0	67	31	950	3.97	41	23	6	36	47	19	15	21	56	.46	.094	36	55	.84	174	.07	38	1.92	.06	.14	11	1400

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppb
M 49 ρ	1	65	8	75	.4	39	20	736	6.61	5	5	ND	1	36	1	4	2	127	1.05	.058	5	57	1.77	45	.35	5	2.62	.02	.06	1	180
M 50 ρ	1	38	8	81	.3	45	22	758	5.31	4	5	ND	1	39	1	2	2	107	.72	.061	4	74	2.76	39	.27	6	2.92	.02	.08	1	80
M 51	1	87	10	86	.5	34	26	1365	6.13	17	5	ND	1	32	1	2	3	138	.77	.050	6	58	1.43	60	.26	5	3.02	.01	.04	1	500
M 52 ρ	1	71	12	83	.3	38	21	732	5.44	10	5	ND	1	35	2	2	2	127	1.08	.045	4	53	1.74	44	.36	3	2.66	.02	.05	1	260
M 53 ρ	1	66	2	73	.3	32	18	644	4.91	13	5	ND	1	20	1	2	2	113	.81	.050	4	45	1.49	54	.31	4	2.18	.03	.06	1	190
M 54	1	73	6	90	.4	40	24	1127	6.09	15	5	ND	1	31	1	2	2	125	.83	.047	4	56	1.73	62	.29	3	2.75	.01	.05	1	200
M 55	1	86	12	75	.5	28	55	1237	11.79	28	5	ND	1	27	1	2	2	139	.61	.053	6	62	1.28	53	.25	5	2.80	.01	.04	1	230
M 56	1	37	14	92	.5	23	24	1850	5.76	34	5	ND	1	23	1	3	2	132	.49	.035	4	45	1.55	45	.24	7	2.37	.01	.04	1	60
M 57	1	35	11	97	.4	19	23	2271	5.69	40	5	ND	1	22	1	2	2	138	.42	.033	4	42	1.53	45	.22	9	2.38	.01	.04	1	80
M 58	1	57	16	77	.5	24	26	2987	5.40	21	5	ND	1	35	1	2	2	131	.65	.042	5	51	1.21	75	.29	7	2.58	.01	.04	1	90
M 59	1	46	18	83	.2	22	28	3299	5.94	27	5	ND	1	30	1	2	3	129	.56	.042	5	50	1.37	86	.26	6	2.60	.01	.04	1	80
M 60	1	71	14	88	.4	35	23	1139	5.76	12	5	ND	1	32	1	2	2	127	.86	.052	5	56	1.72	55	.31	8	2.69	.01	.04	1	160
M 61	1	77	14	97	.3	41	24	971	6.23	10	5	ND	1	29	1	2	2	132	.77	.050	4	65	2.00	51	.29	6	3.02	.01	.05	1	190
STD C	18	57	45	130	6.9	67	30	942	3.97	42	21	8	37	47	19	14	19	57	.46	.100	37	57	.87	174	.06	38	1.92	.06	.14	11	1300

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppb
L1000S 100W	1	11	14	13	.1	4	3	154	1.97	2	5	ND	1	24	1	2	2	133	.06	.018	2	15	.34	81	.22	2	1.87	.01	.03	2	110
L1000S 80W	1	17	11	30	.1	7	4	220	2.25	2	5	ND	1	25	1	2	2	152	.07	.019	2	18	.47	88	.23	2	2.48	.01	.03	1	180
L1000S 40W	1	14	14	13	.1	4	4	192	3.29	3	5	ND	1	39	1	2	2	144	.05	.010	2	17	.20	93	.23	5	3.08	.01	.04	1	150
L1000S 20W	1	18	7	23	.1	6	5	222	4.95	2	5	ND	1	23	1	2	2	162	.05	.016	2	20	.27	96	.21	5	4.23	.01	.04	1	190
L1000S BL	1	3	14	1	.1	1	1	78	.29	2	5	ND	1	28	1	2	2	37	.06	.012	2	6	.04	78	.15	2	.70	.01	.02	1	30
L1000S 40E	1	17	8	40	.1	5	6	331	6.12	7	5	ND	1	14	1	3	2	290	.02	.009	2	20	.07	48	.30	3	.68	.01	.02	3	30
L1000S 60E	1	13	11	34	.2	8	7	277	5.97	7	5	ND	1	43	1	2	3	129	.09	.013	2	22	.60	130	.14	5	3.29	.03	.04	1	150
L1000S 80E	1	27	2	104	.3	12	18	1850	5.58	4	5	ND	1	66	1	2	2	125	.50	.030	3	27	1.50	109	.18	4	3.51	.05	.08	1	100
L1000S 120E	1	5	2	8	.3	2	41	5025	8.13	2	5	ND	1	27	1	2	2	96	.06	.074	5	12	.14	84	.06	2	2.12	.01	.03	1	200
L1000S 140E	1	8	11	6	.1	3	3	214	2.69	5	5	ND	1	14	1	2	2	164	.04	.015	2	12	.19	61	.23	2	1.05	.01	.02	1	60
L1000S 180E	1	9	2	23	.2	4	3	265	1.85	2	5	ND	1	26	1	2	4	91	.18	.019	2	6	.16	26	.09	2	.43	.01	.03	2	130
L1000S 200E	1	21	17	23	.2	7	5	212	8.02	3	5	ND	1	26	1	2	2	157	.05	.025	2	31	.19	103	.19	2	7.70	.01	.02	2	220
L1000S 280E	1	11	5	23	.1	5	3	115	1.41	2	5	ND	1	25	1	2	2	27	.24	.069	2	7	.16	43	.03	3	.97	.02	.04	1	180
L1000S 367E	1	33	9	54	.2	15	14	529	5.39	2	5	ND	1	45	1	3	2	114	.13	.020	4	29	.83	233	.14	5	6.62	.02	.03	1	200
L1000S 400E	1	17	6	40	.1	4	8	422	6.51	2	5	ND	1	36	1	2	2	130	.17	.020	2	16	.56	91	.03	2	3.74	.02	.03	1	120
L1000S 550E	1	9	13	49	.2	4	13	3667	7.33	7	5	ND	1	59	1	2	2	106	.40	.045	3	17	.56	96	.06	5	2.45	.02	.03	1	110
L1000S 600E	1	6	10	18	.7	3	6	280	20.63	7	5	ND	1	15	1	2	2	274	.03	.024	2	14	.26	46	.07	2	1.82	.01	.04	1	880
L1000S 750E	1	7	9	17	.1	3	6	433	4.18	2	5	ND	1	19	1	2	2	119	.06	.011	3	12	.35	70	.07	3	2.15	.01	.07	1	70
L1000S 800E	1	3	16	3	.1	3	5	478	1.44	4	5	ND	1	35	1	2	2	40	.05	.015	3	5	.13	74	.05	4	1.22	.01	.04	1	50
L1025S BL	1	21	10	13	.1	5	4	212	2.49	3	5	ND	1	14	1	2	3	138	.04	.017	2	14	.27	55	.21	2	1.26	.01	.03	1	60
L1050S 100W	1	4	6	7	.3	1	1	81	.20	2	5	ND	1	22	1	2	2	6	.06	.028	2	3	.11	13	.01	8	.15	.02	.03	1	130
L1050S 80W	1	5	5	1	.3	1	1	25	.46	2	5	ND	1	16	1	2	2	11	.02	.044	2	2	.06	46	.02	7	.41	.01	.02	1	110
L1050S 40W	1	17	11	22	.3	6	5	247	6.95	5	5	ND	1	29	1	2	2	195	.33	.017	2	22	.23	50	.25	4	1.84	.01	.04	1	100
L1050S 20W	1	18	2	17	.1	4	6	248	4.78	6	5	ND	1	12	1	2	2	267	.06	.005	2	14	.07	31	.28	2	.65	.01	.02	1	30
L1050S BL	1	9	4	9	.6	2	2	92	2.55	7	5	ND	1	22	1	2	2	139	.04	.014	2	5	.06	63	.16	5	.50	.02	.02	1	80
L1050S 20E	1	20	11	32	.1	5	4	224	6.79	6	5	ND	1	19	1	2	2	263	.09	.012	2	16	.19	69	.29	4	.89	.02	.03	1	50
L1050S 40E	1	17	9	72	.1	9	17	2719	4.90	6	5	ND	1	64	1	2	2	120	.27	.026	4	23	.85	123	.13	2	3.30	.03	.03	1	100
L1050S 60E	1	9	13	26	.3	5	5	382	6.29	7	5	ND	1	40	1	2	2	115	.09	.030	2	14	.30	86	.10	5	2.04	.02	.03	1	130
L1050S 80E	1	3	8	2	.1	2	1	58	.58	2	5	ND	1	19	1	2	2	21	.16	.023	2	2	.07	22	.03	2	.16	.01	.03	1	90
L1050S 120E	1	16	11	26	.1	6	5	224	5.47	3	5	ND	1	22	1	2	2	176	.04	.016	2	21	.20	67	.20	2	3.03	.01	.02	1	260
L1050S 160E	1	11	6	36	.1	4	7	1571	6.89	8	5	ND	1	27	1	2	2	103	.09	.101	4	10	.17	95	.02	2	2.00	.01	.03	1	180
L1050S 180E	1	15	3	48	.3	3	27	4123	13.66	3	5	ND	1	33	1	2	3	140	.11	.091	6	19	.30	123	.03	4	3.65	.02	.02	1	110
L1050S 240E	1	4	4	8	.1	1	4	686	1.02	2	5	ND	1	21	1	2	2	18	.09	.092	2	1	.04	51	.01	5	.51	.01	.03	1	220
L1050S 280E	2	8	8	13	.1	3	3	215	2.40	3	5	ND	1	36	1	2	3	81	.09	.033	2	11	.22	79	.10	2	1.22	.01	.03	2	130
L1050S 300E	4	16	11	31	.3	5	6	279	7.61	10	5	ND	1	25	1	2	3	207	.02	.013	2	22	.19	104	.22	4	2.14	.01	.02	1	110
L1075S BL	1	10	7	17	.1	3	3	133	3.05	8	5	ND	1	19	1	2	2	178	.06	.009	2	9	.07	60	.19	3	.99	.01	.02	1	60
STD C	18	57	37	129	6.7	67	30	944	4.03	43	17	7	36	47	19	15	18	58	.46	.094	37	55	.87	173	.07	36	1.87	.06	.14	13	1400

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppb
L1100S 80W	1	12	9	21	.1	3	4	174	3.68	12	5	ND	1	32	1	2	2	117	.09	.029	6	13	.26	80	.15	2	1.68	.01	.05	1	120
L1100S 40W	1	22	16	26	.1	4	5	219	6.59	10	5	ND	1	16	1	2	2	300	.02	.014	2	18	.11	75	.30	2	1.58	.01	.02	1	110
L1100S 20W	1	24	6	31	.3	5	6	298	8.04	7	5	ND	1	23	1	2	2	302	.11	.014	2	24	.17	56	.36	2	1.76	.01	.02	1	120
L1100S BL	1	21	8	83	.1	11	21	3425	5.04	8	5	ND	1	87	1	2	2	120	.46	.042	5	22	.91	146	.13	8	3.80	.04	.03	1	140
L1100S 20E P	1	26	15	109	.2	11	19	2305	6.15	2	5	ND	1	44	1	2	2	119	.32	.033	2	20	1.41	121	.11	2	3.94	.03	.08	1	60
L1100S 40E	1	6	11	18	.1	2	4	453	3.04	2	5	ND	1	53	1	2	2	148	.13	.014	2	9	.27	89	.15	2	1.60	.02	.03	1	320
L1100S 180E P	1	24	3	101	.2	10	18	2454	5.88	3	5	ND	1	40	1	2	2	112	.27	.027	2	19	1.30	122	.08	2	3.77	.02	.07	1	60
L1100S 200E P	1	26	10	112	.2	9	18	2313	5.93	7	5	ND	1	39	1	3	2	116	.29	.030	2	19	1.47	115	.09	2	4.05	.03	.10	1	40
L1100S 220E	1	17	6	20	.2	3	4	176	5.11	5	5	ND	1	33	1	2	2	141	.07	.028	2	17	.15	78	.18	9	3.81	.02	.02	1	280
L1100S 240E	1	18	5	20	.3	3	4	140	4.96	4	5	ND	1	39	1	2	2	134	.06	.028	2	18	.15	79	.18	2	4.26	.01	.02	1	300
L1100S 300E	1	18	8	21	.4	4	5	189	5.01	3	5	ND	1	32	1	2	2	139	.07	.028	2	19	.23	77	.18	2	4.21	.01	.02	1	270
L1125S BL P	1	22	5	68	.2	8	8	637	2.16	5	5	ND	1	71	1	2	2	71	.38	.107	6	19	.61	128	.08	2	3.95	.03	.04	1	210
L1125S BL (A)	1	4	12	11	.1	1	20	4242	3.55	2	5	ND	1	48	1	2	2	97	.05	.034	3	14	.12	109	.07	2	1.61	.01	.03	1	90
L1150S 100W	1	15	17	19	.2	1	5	321	5.40	5	5	ND	1	21	1	2	2	249	.05	.016	2	12	.24	79	.26	2	1.23	.01	.03	1	100
L1150S 80W	1	29	16	32	.5	4	7	377	5.86	8	5	ND	1	9	1	3	2	249	.03	.012	2	19	.44	93	.21	2	3.57	.01	.04	2	230
L1150S 60W P	1	4	2	6	.8	1	1	78	.40	2	5	ND	1	20	1	2	2	21	.03	.019	2	3	.10	34	.02	2	.28	.01	.02	1	200
L1150S 40W	1	30	20	49	.4	7	8	339	7.42	8	5	ND	1	23	1	3	2	229	.05	.015	2	22	.57	195	.21	2	3.73	.02	.03	1	110
L1150S 20W	1	18	2	78	.2	11	18	1108	5.72	2	5	ND	1	87	1	2	2	136	.44	.026	3	23	.92	150	.15	2	4.05	.04	.04	1	150
L1150S BL	1	5	7	19	.1	3	5	233	3.63	6	5	ND	1	49	1	2	2	129	.06	.008	3	11	.27	115	.10	2	2.17	.02	.05	1	60
L1150S 20E P	1	11	11	15	.4	2	10	1714	3.00	2	5	ND	1	40	1	2	2	132	.19	.111	4	9	.10	82	.03	2	1.49	.02	.04	1	190
L1150S 100E	1	5	6	8	.1	3	12	4304	5.86	2	5	ND	1	32	1	2	2	78	.09	.097	4	6	.05	86	.02	2	1.22	.01	.08	1	300
L1150S 160E P	1	3	2	8	.4	1	1	25	.62	2	5	ND	1	17	1	2	2	12	.08	.070	2	3	.03	25	.01	2	.38	.01	.04	1	130
L1150S 280E	1	27	14	107	.4	10	21	3657	6.85	6	5	ND	1	54	1	2	2	116	.43	.041	3	20	1.21	144	.09	2	4.15	.02	.06	1	90
L1150S 260E	1	11	6	17	.1	3	2	188	2.69	3	5	ND	1	40	1	2	3	55	.12	.021	4	10	.13	84	.07	2	1.92	.01	.03	1	120
L1150S 280E	1	8	10	13	.2	3	2	113	2.28	4	5	ND	1	41	1	3	2	51	.12	.029	4	10	.08	85	.05	2	1.84	.01	.03	1	150
L1150S 300E	1	32	11	65	.2	12	13	1355	2.63	5	5	ND	1	55	1	5	2	72	.28	.047	3	23	.86	167	.11	2	4.77	.02	.03	1	170
L1200S 40E	1	14	14	61	.1	12	8	267	2.00	5	5	ND	1	78	1	2	2	65	.16	.030	4	21	.71	146	.14	2	4.31	.02	.07	2	190
L1200S 60E	1	19	10	61	.1	17	10	331	3.18	7	5	ND	1	76	1	2	2	85	.17	.031	3	28	.98	159	.16	2	5.22	.02	.10	1	140
L1200S 180E	1	24	13	36	.2	7	6	263	9.58	4	5	ND	1	19	1	2	2	199	.04	.021	3	32	.36	92	.19	2	5.66	.01	.03	1	480
L1200S 200E	1	22	4	32	.2	7	6	244	8.66	4	5	ND	1	14	1	2	2	189	.03	.019	2	31	.31	83	.19	2	5.07	.01	.02	1	450
L1200S 220E	1	26	12	78	.2	8	18	2537	5.00	2	5	ND	1	54	1	2	2	110	.37	.045	4	21	.93	147	.07	2	4.15	.02	.04	1	100
L1200S 260E	1	3	8	13	.1	2	1	135	3.44	7	5	ND	1	25	1	2	2	81	.04	.043	2	2	.10	45	.03	2	1.16	.01	.04	1	80
L1200S 300E	1	8	12	33	.1	3	9	1981	4.77	3	5	ND	1	60	1	2	2	73	.27	.030	2	10	.54	75	.14	2	1.77	.03	.04	2	110
L1225S BL	1	7	2	22	.2	2	17	1891	10.99	2	5	ND	1	39	1	2	2	136	.21	.057	4	13	.16	71	.05	4	1.68	.02	.02	1	150
L1250S 100W P	1	41	6	86	1.0	6	13	1321	6.54	8	5	ND	1	83	1	7	2	185	1.35	.028	2	22	2.02	76	.15	11	5.76	.04	.11	1	560
L1250S 80W	1	19	12	40	.3	8	8	534	4.49	6	5	ND	1	40	1	3	2	144	.13	.032	3	22	.31	117	.16	7	7.11	.02	.03	1	130
STD C	19	57	41	131	6.9	68	30	1010	3.99	41	21	7	36	47	19	14	22	59	.47	.094	37	55	.84	174	.07	32	1.96	.06	.14	11	1400

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppb
L1250S 60W	1	21	24	49	.4	11	9	551	5.40	3	5	ND	1	41	2	7	2	166	.11	.029	3	27	.31	129	.19	4	7.55	.02	.03	2	220
L1250S 40W	1	20	28	43	.8	6	6	250	9.36	2	5	ND	2	20	1	6	2	157	.05	.022	2	37	.24	101	.20	3	9.19	.01	.02	3	300
L1250S 20E	1	24	21	60	.6	14	10	515	6.43	5	5	ND	1	42	1	7	2	191	.22	.042	3	30	.97	110	.16	2	4.62	.02	.04	1	230
L1250S 40E	1	14	8	45	.3	11	13	829	7.30	2	5	ND	1	32	1	5	2	234	.07	.020	2	29	.75	94	.23	3	2.80	.01	.09	1	100
L1250S 80E	1	6	13	18	.4	2	4	568	2.56	2	5	ND	1	42	1	4	2	52	.09	.056	3	8	.08	87	.05	2	1.21	.01	.04	1	130
L1250S 100E	1	4	14	18	.2	2	3	201	2.89	5	5	ND	1	49	1	3	3	79	.06	.015	2	9	.17	121	.11	2	1.26	.01	.03	2	40
L1250S 160E	1	11	21	44	.1	8	6	238	2.27	4	5	ND	1	47	2	4	2	79	.13	.018	2	14	.47	158	.16	2	2.59	.02	.05	1	60
L1250S 180E	1	8	12	45	.2	1	2	126	1.70	2	5	ND	1	12	1	2	2	82	.04	.018	2	10	.06	42	.14	3	.60	.01	.02	1	70
L1250S 200E	1	23	17	70	.4	11	15	2131	6.72	8	5	ND	1	30	1	6	2	150	.08	.027	3	29	.55	144	.14	2	6.53	.01	.03	1	150
L1250S 220E	1	19	11	72	.7	10	19	5011	13.86	5	5	ND	1	55	1	8	2	170	.25	.041	3	26	.80	141	.09	2	3.56	.02	.04	1	80
L1250S 240E	1	4	3	16	.2	2	2	435	5.03	2	5	ND	1	26	1	2	2	46	.18	.081	2	1	.06	47	.01	2	.77	.01	.03	1	130
L1250S 300E	1	4	7	13	.6	1	2	42	1.32	2	5	ND	1	31	1	2	2	29	.15	.129	2	2	.05	52	.01	2	.68	.01	.04	1	230
L1275S BL	1	3	14	17	.3	1	2	115	3.01	7	5	ND	1	40	1	4	2	69	.06	.021	3	6	.07	82	.06	2	1.16	.01	.03	1	70
L1300S 80W	1	14	14	43	.8	9	16	2335	9.61	10	5	ND	1	65	1	6	2	164	.26	.086	6	32	.39	108	.07	2	4.47	.02	.03	1	260
L1300S 40W	1	4	2	15	.7	5	17	7750	7.73	2	5	ND	1	22	1	5	2	106	.03	.115	7	8	.05	87	.02	3	1.30	.01	.07	1	180
L1300S 20E	1	18	23	43	.4	12	7	280	5.31	2	5	ND	1	28	1	8	2	93	.09	.041	3	30	.56	131	.15	4	7.54	.01	.08	3	160
L1300S 100E P	1	4	5	16	.4	1	1	141	.16	2	5	ND	1	19	1	2	2	4	.31	.054	2	2	.06	16	.01	5	.15	.02	.09	1	270
L1300S 120E P	1	7	8	19	.2	3	4	355	1.19	2	5	ND	1	36	1	2	2	36	.21	.065	2	7	.14	90	.03	2	1.43	.02	.04	1	230
L1300S 140E	2	22	5	30	.4	6	5	198	7.18	5	5	ND	1	30	1	5	2	160	.05	.028	3	28	.20	153	.12	2	4.59	.01	.02	1	150
L1300S 160E	1	16	7	30	.2	5	7	301	5.05	7	5	ND	1	19	1	5	4	274	.03	.011	3	15	.07	89	.23	2	.83	.01	.03	1	40
L1300S 180E P	1	20	11	106	.4	7	18	2749	6.46	4	5	ND	1	33	1	3	2	105	.35	.038	3	19	1.28	93	.05	2	3.14	.02	.10	1	20
L1300S 200E	1	6	7	13	.2	1	2	113	2.51	2	5	ND	1	31	1	4	2	77	.08	.045	2	7	.09	81	.06	2	1.48	.01	.03	1	80
L1300S 220E P	1	6	13	11	.5	3	4	1107	1.06	4	5	ND	1	31	1	2	2	49	.12	.113	3	12	.10	91	.02	2	1.90	.01	.04	1	260
L1300S 280E P	1	5	6	6	.4	3	1	40	.86	2	5	ND	1	28	1	2	2	29	.13	.124	2	5	.05	54	.01	2	.95	.01	.02	1	180
L1325S BL	1	11	12	31	.3	7	6	418	2.81	5	5	ND	1	49	1	4	2	93	.17	.037	4	17	.45	94	.08	2	2.59	.01	.03	1	170
L1350S 80W	1	6	13	16	.1	2	3	299	1.73	4	5	ND	1	41	1	3	2	70	.09	.014	3	10	.14	94	.11	2	1.35	.01	.03	1	40
L1350S 60W	1	5	10	7	.1	2	2	205	1.12	2	5	ND	1	37	1	3	2	57	.07	.009	3	8	.10	87	.11	2	1.05	.01	.03	1	30
L1350S 40W P	1	8	10	25	.4	6	7	653	2.12	5	5	ND	1	45	1	2	3	59	.14	.101	3	14	.21	94	.05	2	1.95	.02	.05	1	230
L1350S 100E	1	26	17	62	.5	14	16	1216	4.64	5	5	ND	1	91	1	6	2	106	.37	.066	4	25	.97	142	.11	2	4.35	.02	.04	1	180
L1350S 140E	1	6	9	10	.3	1	2	149	.54	2	5	ND	1	41	1	3	2	26	.14	.034	2	6	.06	73	.02	2	.95	.01	.02	1	130
L1350S 180E	1	17	4	25	.2	6	7	294	5.05	3	5	ND	1	20	1	6	3	258	.05	.006	2	16	.06	66	.25	2	.46	.01	.01	1	20
L1350S 200E P	1	25	14	103	.4	8	20	2738	6.60	2	5	ND	1	41	1	8	2	105	.37	.044	2	18	1.62	143	.05	2	3.44	.04	.11	1	10
L1350S 240E	1	29	12	82	.1	17	18	703	3.90	4	5	ND	1	76	1	7	2	111	.25	.048	4	44	1.49	133	.09	2	5.35	.02	.04	1	100
L1350S 260E	1	25	2	34	.1	6	7	278	6.53	9	5	ND	1	13	1	7	2	283	.01	.043	2	18	.07	48	.17	4	.89	.01	.02	1	20
L1350S 280E	1	24	19	33	.1	10	4	171	1.48	5	5	ND	1	54	1	6	2	110	.08	.047	4	27	.39	137	.12	2	4.45	.01	.03	3	160
L1350S 300E P	1	18	2	92	.5	9	19	4666	6.97	7	5	ND	1	45	1	7	2	109	.38	.033	3	19	1.23	103	.10	14	3.29	.04	.09	1	30
STD C	18	57	37	129	7.5	69	31	1023	4.06	41	17	8	36	47	19	15	21	58	.48	.095	36	55	.85	173	.07	41	1.86	.06	.14	13	1300

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppb
L1400S 100W P	1	5	5	26	.6	5	64	26210	5.21	7	5	ND	1	37	1	3	7	72	.09	.042	3	19	.13	210	.11	6	2.00	.02	.07	1	180
L1400S 60W	1	4	13	22	.1	3	6	837	1.36	3	5	ND	1	57	1	2	2	66	.10	.013	2	13	.20	90	.08	2	1.81	.01	.05	1	60
L1400S 20E	1	9	5	22	.4	4	21	9058	4.13	6	5	ND	1	74	1	3	2	77	.75	.088	9	11	.17	175	.02	2	2.42	.01	.04	1	280
L1400S 40E	1	10	23	18	.7	4	29	2138	7.81	5	5	ND	1	30	1	4	2	127	.07	.022	4	19	.19	76	.12	5	2.88	.01	.04	1	130
L1400S 80E	1	13	11	24	.1	4	5	223	6.47	6	5	ND	1	19	1	6	8	301	.04	.015	2	15	.28	73	.22	2	2.25	.01	.04	1	60
L1400S 100E	1	16	11	29	.2	2	9	1053	8.39	7	5	ND	1	24	1	6	5	277	.10	.016	2	15	.37	57	.17	2	1.68	.01	.03	1	30
L1400S 160E	1	21	17	144	.7	10	34	9549	9.44	5	5	ND	1	48	1	8	2	126	.49	.046	3	23	1.06	162	.06	2	3.95	.02	.04	1	60
L1400S 180E	1	23	25	41	.4	5	6	277	9.95	5	5	ND	1	21	1	7	7	190	.04	.023	2	36	.25	83	.19	2	5.75	.01	.04	2	120
L1400S 220E	1	27	13	37	.6	6	7	256	8.72	8	5	ND	1	14	1	8	2	209	.05	.029	2	30	.17	87	.20	2	5.35	.01	.03	1	650
L1400S 240E	1	22	14	37	.1	10	6	342	2.96	8	5	ND	1	51	1	8	2	141	.16	.035	3	25	.56	89	.14	2	4.26	.01	.04	3	180
L1400S 260E	1	18	16	90	.4	9	19	4884	5.36	6	5	ND	1	56	1	7	2	96	.55	.041	3	15	.98	92	.08	2	3.49	.02	.04	1	100
L1400S 280E	1	19	16	87	.4	9	20	6284	5.27	10	5	ND	1	65	1	5	2	92	.60	.044	3	18	.88	108	.07	4	3.60	.02	.04	1	130
L1400S 300E	1	18	20	42	.4	6	6	256	6.95	5	5	ND	1	19	1	7	3	145	.05	.034	2	27	.43	112	.14	2	5.15	.01	.04	1	110
L1450S BL	1	20	34	41	.5	8	6	199	7.08	3	5	ND	1	16	1	10	3	151	.04	.034	2	28	.31	90	.16	3	6.71	.01	.04	3	200
L1450S 20E	1	8	25	35	.1	7	5	606	3.19	6	5	ND	1	43	1	4	2	133	.09	.024	4	20	.42	104	.16	2	3.07	.01	.04	1	100
L1450S 40E	1	14	17	34	.5	8	6	650	2.93	6	5	ND	1	45	1	4	2	90	.17	.077	6	22	.34	89	.08	2	4.11	.02	.03	1	220
L1450S 80E	1	3	8	10	.1	3	1	44	.38	2	5	ND	1	79	1	2	2	24	.29	.063	3	9	.10	104	.05	2	1.36	.01	.05	1	130
L1450S 100E	1	23	17	36	.3	11	7	235	7.11	2	5	ND	1	28	1	4	2	146	.08	.026	3	29	.38	107	.21	2	7.31	.02	.04	2	190
L1450S 140E	1	18	11	113	.4	8	21	1949	8.84	9	5	ND	1	46	2	5	2	138	.41	.056	4	23	.95	127	.06	2	4.02	.01	.03	1	90
L1450S 160E	4	2	13	21	.1	1	4	287	1.35	2	5	ND	1	8	1	2	6	30	.09	.006	2	2	.13	25	.02	2	1.18	.01	.01	18	130
L1450S 180E	1	2	2	13	.1	2	3	120	.78	2	5	ND	1	5	1	2	2	22	.06	.002	2	3	.07	18	.02	2	1.02	.01	.01	1	50
L1450S 200E	1	11	9	24	.1	6	8	546	5.55	15	5	ND	1	17	2	8	2	106	.15	.017	2	16	.28	60	.08	2	3.56	.01	.02	1	60
L1450S 240E	1	16	19	103	.6	7	28	7695	7.84	3	5	ND	1	63	1	7	2	114	.96	.037	3	20	1.15	106	.08	2	4.05	.02	.06	1	40
L1450S 300E	1	6	16	25	.2	5	5	754	1.65	6	5	ND	1	41	1	3	2	65	.11	.022	3	13	.25	79	.05	2	2.39	.01	.04	1	70
L1500S 20E	1	8	23	42	.7	4	18	5268	20.62	3	5	ND	1	23	2	6	2	240	.04	.046	4	31	.34	70	.14	2	5.09	.01	.04	1	170
L1500S 40E P	1	5	2	10	.2	1	2	1246	.17	2	5	ND	1	14	1	2	2	5	.30	.036	2	2	.04	12	.01	8	.10	.02	.03	1	400
L1500S 60E	1	7	7	14	.1	1	3	204	2.31	3	5	ND	1	18	1	3	3	134	.04	.009	3	9	.06	39	.19	3	.49	.01	.02	1	80
L1500S 120E P	1	10	8	29	.2	3	10	4665	2.63	2	5	ND	1	40	1	4	2	78	.21	.066	5	13	.16	97	.06	2	2.01	.02	.04	1	160
L1500S 140E P	1	13	13	52	.4	12	10	959	5.81	2	5	ND	1	52	1	5	2	124	.20	.036	3	22	.64	123	.12	2	2.89	.02	.05	1	80
L1500S 180E	1	4	27	33	.3	3	7	892	6.25	12	5	ND	1	28	1	5	2	154	.12	.023	2	15	.26	129	.05	2	3.11	.01	.04	1	50
L1500S 200E	1	8	6	49	.5	5	15	2268	10.79	4	5	ND	1	22	1	5	2	173	.11	.046	3	21	.29	80	.03	4	3.79	.01	.03	1	110
L1500S 220E	4	26	8	38	.4	2	5	226	9.97	6	5	ND	1	14	1	7	3	162	.03	.044	2	21	.28	56	.02	2	4.48	.01	.05	2	130
L1500S 240E	1	58	18	71	.3	15	21	580	3.75	4	5	ND	1	89	1	9	2	116	1.08	.032	3	20	1.14	375	.12	3	7.11	.03	.08	1	30
L1500S 260E	1	39	32	60	.6	7	8	380	8.26	9	5	ND	1	15	1	9	2	106	.08	.039	2	24	.62	71	.06	2	9.38	.01	.04	4	140
L1500S 200E	1	18	11	29	.2	5	6	215	6.12	9	5	ND	1	15	1	5	2	245	.05	.010	2	15	.10	30	.16	11	1.22	.01	.02	1	30
L1500S 300E	1	7	17	19	.4	3	5	775	2.15	5	5	ND	1	30	1	3	2	86	.10	.033	3	11	.15	64	.05	2	1.69	.01	.04	1	100
STD C	18	57	41	132	7.3	67	31	1012	4.04	42	18	8	36	47	20	15	20	58	.48	.094	37	55	.85	173	.07	39	1.83	.06	.14	11	1400

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppb
BL 1250S 20C	1	7	7	8	.9	1	76	16106	19.02	5	6	ND	1	7	1	6	5	218	.01	.113	5	14	.01	57	.03	2	2.20	.01	.04	1	180
BL 1300S 25C	1	9	13	28	.2	4	5	638	7.19	2	5	ND	1	30	1	6	5	128	.11	.034	4	12	.29	62	.07	6	2.27	.01	.03	1	70
BL 1350S 30C	1	8	17	25	.2	5	21	1580	3.58	4	5	ND	1	36	1	3	2	92	.06	.017	3	17	.25	124	.11	2	2.43	.01	.04	1	150
BL 1375S 50C	1	33	5	80	.1	17	17	598	3.08	3	5	ND	1	56	2	6	2	101	.32	.052	4	30	1.40	119	.10	3	4.68	.02	.03	1	340
BL 1400S 50C	2	9	12	32	.7	1	10	4097	15.60	7	5	ND	1	9	1	5	3	267	.02	.081	13	30	.24	70	.09	2	6.52	.01	.13	1	250
BL 1500S 50C	1	20	23	37	.1	13	6	199	2.30	5	5	ND	1	25	2	5	2	108	.05	.038	4	39	.57	121	.12	2	8.29	.01	.03	2	80
STD C	17	58	43	129	7.3	66	31	969	4.02	43	19	7	35	46	19	14	21	57	.45	.094	36	55	.88	173	.07	40	1.92	.06	.14	13	1300

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Hg ppb
D 1	1	4074	13	36	.6	10	127	241	32.18	27	5	ND	3	2	1	2	2	17	.52	.035	2	1	.23	3	.01	2	.48	.01	.02	2	230
D 2	22	2955	4	12	.9	29	321	246	21.33	43288	5	ND	2	7	1	2	2	20	.53	.013	2	8	.29	4	.02	2	.37	.01	.01	1	4300
D 3	1	14446	7	252	1.1	24	281	189	26.66	1001	5	ND	2	14	2	2	2	20	.44	.057	2	9	.46	2	.04	2	.68	.01	.01	1	1800
D 4	1	3669	2	55	.7	4	25	831	7.28	114	5	ND	1	4	1	2	2	7	1.33	.032	2	2	.18	4	.02	6	.26	.01	.01	1	220
D 5	1	4521	7	67	.5	8	65	1295	32.64	21	5	ND	3	2	2	2	2	26	3.09	.041	2	1	.13	4	.01	2	.66	.01	.01	13	630
D 6	1	95	2	234	.1	4	17	6730	5.16	23	5	ND	1	26	1	2	2	9	1.63	.019	2	1	.42	25	.02	2	.58	.01	.01	1	50
D 7	1	14690	2	298	2.5	5	61	398	16.04	66	5	ND	1	2	1	2	2	3	.85	.010	2	1	.07	7	.01	2	.17	.01	.01	1	200
D 8	1	9053	2	49	.6	14	305	226	18.84	37	5	ND	1	16	1	2	2	18	.33	.022	2	2	.35	6	.04	2	.70	.01	.01	1	180
STD C	18	56	38	132	6.6	67	31	942	3.92	43	20	7	37	48	19	15	21	58	.44	.096	38	56	.88	172	.07	39	1.85	.06	.13	11	1300

ACME ANALYTICAL LABORATORIES LTD.
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
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DATE RECEIVED: MAR 8 1990
DATE REPORT MAILED: ....

GEOCHEMICAL ANALYSIS CERTIFICATE

Doromin Resources Ltd. FILE # 90-0514R Page 1
827 W. Pender St., Vancouver BC

SAMPLE#	AU* ppb	BA* ppm
E 1	10	904
E 2	5	1004
E 3	5	672
E 4	3	697
E 5	2	871
E 6	11	964
E 7	3	834
E 8	4	778
E 9	4	671
E 10	3	717
E 11	10	727
E 12	1	843
E 13	2	692
E 14	5	740
E 15	8	718
E 16	5	785
E 17	10	794
E 18	5	803
E 19	6	904
E 20	2	855
E 21	3	908
E 22	7	843
E 23	1	743
E 24	1	754
E 25	2	714
E 26	2	751
E 27	2	614
E 28	4	455
E 29	3	658
E 30	5	679
E 31	2	677
E 32	2	960
E 33	1	929
E 34	2	878
E 35	1	839
E 36	2	886

- SAMPLE TYPE: P1-P9 Soil Pulp P10 Rock Pulp
AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.
BA* .1 GM SAMPLES FUSED WITH .6 GM LIBO2 DISSOLVED IN HNO3 ANALYSED BY ICP.

SIGNED BY........... D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

Doromin Resources Ltd. FILE # 90-0514R Page 2

SAMPLE#	AU* ppb	BA* ppm
E 37	1	927
E 38	5	896
E 39	1	926
E 40	3	940
E 41	2	916
E 42	3	943
E 43	1	920
E 44	1	893
E 45	2	983
G 1	1	521
G 2	4	513
G 3	2	506
G 4	4	427
G 5	1	515
G 6	3	388
G 7	1	399
G 8	1	260
G 9	1	268
G 10	3	819
G 11	1	477
G 12	5	510
G 13	1	360
G 14	2	265
G 15	3	179
M 1	3	281
M 2	3	350
M 3	2	325
M 4	1	306
M 5	1	148
M 6	4	201
M 7	5	196
M 8	5	306
M 9	2	275
M 10	3	397
M 11	4	226
M 12	1	258

SAMPLE#	AU* ppb	BA* ppm
M 13	1	235
M 14	1	380
M 15	1	335
M 16	7	375
M 17	2	234
M 18	1	301
M 19	3	280
M 20	1	454
M 21	1	327
M 22	3	269
M 23	1	402
M 24	2	235
M 25	1	296
M 26	2	476
M 27	2	358
M 28	3	364
M 29	1	376
M 30	2	318
M 31	2	373
M 32	1	520
M 33	1	331
M 34	3	341
M 35	4	366
M 36	7	288
M 37	1	394
M 38	1	160
M 39	2	368
M 40	3	358
M 41	6	405
M 42	1	426
M 43	5	385
M 44	9	361
M 45	8	385
M 46	1	338
M 47	2	362
M 48	18	401

SAMPLE#	AU* ppb	BA* ppm
M 49	2	388
M 50	1	351
M 51	5	398
M 52	2	424
M 53	4	513
M 54	5	445
M 55	2	364
M 56	9	408
M 57	1	400
M 58	1	383
M 59	1	437
M 60	4	420
M 61	2	454

SAMPLE#	AU* ppb	BA* ppm
L1000S 100W	19	857
L1000S 80W	17	928
L1000S 40W	16	824
L1000S 20W	9	694
L1000S BL	43	1071
L1000S 40E	8	547
L1000S 60E	24	709
L1000S 80E	1	909
L1000S 120E	8	353
L1000S 140E	2	643
L1000S 180E	3	137
L1000S 200E	5	403
L1000S 280E	1	130
L1000S 367E	1	698
L1000S 400E	3	485
L1000S 550E	9	510
L1000S 600E	1	419
L1000S 750E	1	708
L1000S 800E	1	663
L1025S BL	5	590
L1050S 100W	7	37
L1050S 80W	3	207
L1050S 40W	1	561
L1050S 20W	31	852
L1050S BL	4	493
L1050S 20E	7	623
L1050S 40E	7	661
L1050S 60E	2	459
L1050S 80E	2	64
L1050S 120E	6	514
L1050S 160E	1	283
L1050S 180E	1	312
L1050S 240E	1	104
L1050S 280E	4	516
L1050S 300E	7	473
L1075S BL	10	596

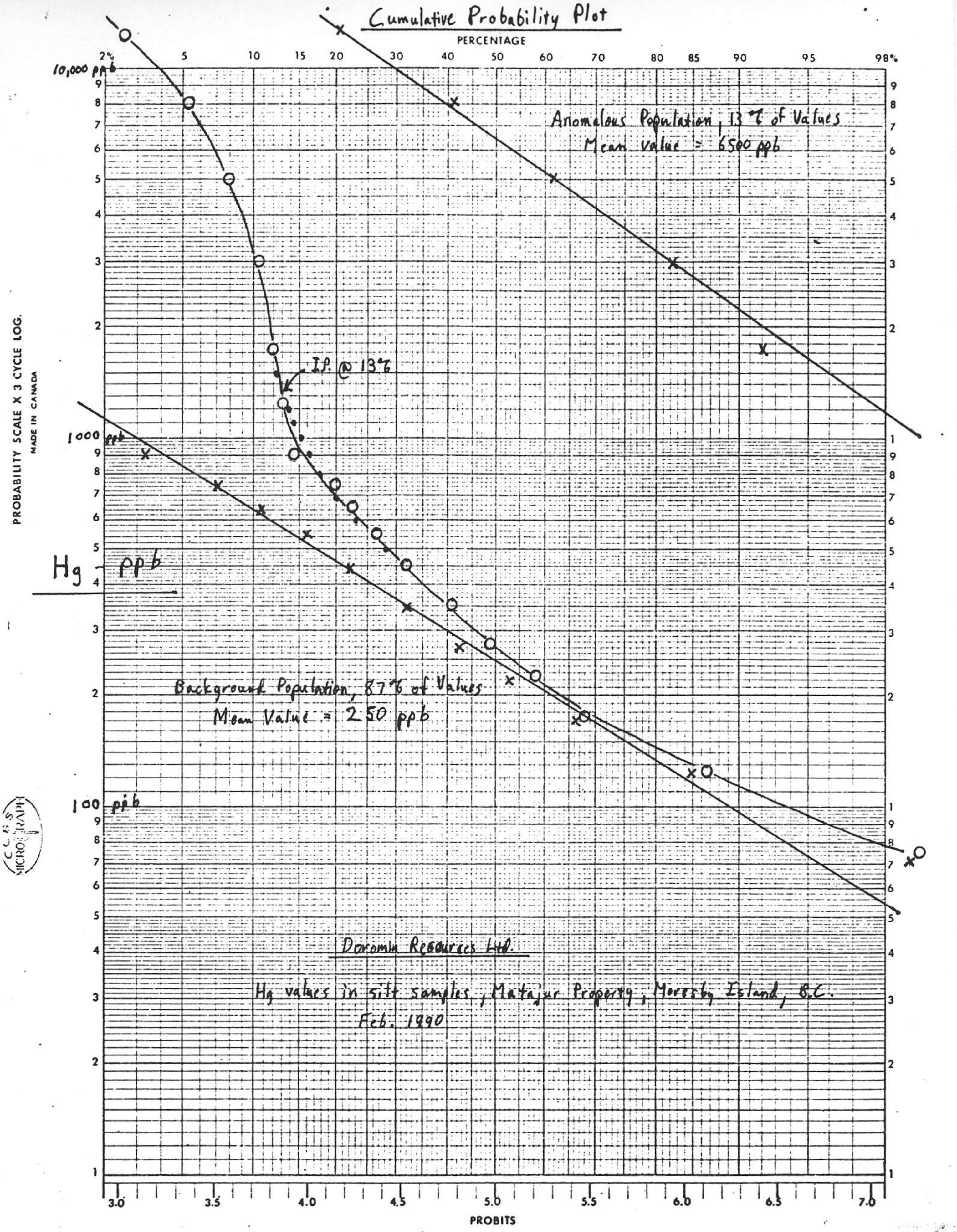
SAMPLE#	AU* ppb	BA* ppm
L1100S 80W	19	715
L1100S 40W	13	592
L1100S 20W	2	450
L1100S BL	2	644
L1100S 20E	5	684
L1100S 40E	3	762
L1100S 180E	5	714
L1100S 200E	3	666
L1100S 220E	4	311
L1100S 240E	3	282
L1100S 300E	3	306
L1125S BL	1	489
L1125S BL (A)	7	550
L1150S 100W	6	937
L1150S 80W	1	1170
L1150S 60W	3	152
L1150S 40W	1	1001
L1150S 20W	1	700
L1150S BL	1	780
L1150S 20E	2	343
L1150S 100E	3	237
L1150S 160E	1	67
L1150S 200E	1	636
L1150S 260E	1	583
L1150S 280E	1	540
L1150S 300E	3	677
L1200S 40E	3	787
L1200S 60E	6	778
L1200S 180E	1	401
L1200S 200E	1	427
L1200S 220E	5	629
L1200S 260E	6	437
L1200S 300E	11	647
L1225S BL	1	373
L1250S 100W	5	473
L1250S 80W	1	434

SAMPLE#	AU* ppb	BA* ppm
L1250S 60W	1	451
L1250S 40W	1	374
L1250S 20E	4	674
L1250S 40E	1	651
L1250S 80E	1	519
L1250S 100E	1	642
L1250S 160E	1	882
L1250S 180E	4	541
L1250S 200E	1	560
L1250S 220E	1	568
L1250S 240E	1	266
L1250S 300E	4	195
L1275S BL	3	581
L1300S 80W	3	455
L1300S 40W	1	244
L1300S 20E	1	519
L1300S 100E	4	53
L1300S 120E	3	583
L1300S 140E	1	551
L1300S 160E	2	422
L1300S 180E	1	636
L1300S 200E	1	531
L1300S 220E	1	330
L1300S 280E	1	187
L1325S BL	10	658
L1350S 80W	2	1013
L1350S 60W	1	1084
L1350S 40W	1	481
L1350S 100E	1	603
L1350S 140E	1	770
L1350S 180E	1	444
L1350S 200E	1	667
L1350S 240E	1	604
L1350S 260E	1	535
L1350S 280E	1	702
L1350S 300E	1	721

SAMPLE#	AU* ppb	BA* ppm
L1400S 100W	8	603
L1400S 60W	6	714
L1400S 20E	5	367
L1400S 40E	1	548
L1400S 80E	3	686
L1400S 100E	5	1504
L1400S 160E	4	569
L1400S 180E	3	387
L1400S 220E	1	408
L1400S 240E	1	546
L1400S 260E	1	486
L1400S 280E	1	483
L1400S 300E	1	437
L1450S BL	2	434
L1450S 20E	2	542
L1450S 40E	6	388
L1450S 80E	1	505
L1450S 100E	1	408
L1450S 140E	1	497
L1450S 160E	1	471
L1450S 180E	1	421
L1450S 200E	1	446
L1450S 240E	7	490
L1450S 300E	1	656
L1500S 20E	1	357
L1500S 40E	1	48
L1500S 60E	1	322
L1500S 120E	1	416
L1500S 140E	1	597
L1500S 180E	1	520
L1500S 200E	1	405
L1500S 220E	1	275
L1500S 240E	2	937
L1500S 260E	3	358
L1500S 280E	2	289
L1500S 300E	5	527

SAMPLE#	AU* ppb	BA* ppm
BL 1250S 20C	1	115
BL 1300S 25C	4	790
BL 1350S 30C	2	575
BL 1375S 50C	1	555
BL 1400S 50C	3	340
BL 1500S 50C	4	391

SAMPLE#	AU* ppb	BA* ppm
D 1	3	814
D 2	1	614
D 3	1	309
D 4	1	180
D 5	3	107
D 6	1	65
D 7	1	22
D 8	4	41



Cumulative Probability Plot
PERCENTAGE
2% 5 10 15 20 30 40 50 60 70 80 85 90 95 98%
10,000 ppb
1000 ppb
100 ppb
PROBABILITY SCALE X 3 CYCLE LOG.
MADE IN CANADA
Hg - ppb
Anomalous Population, 13 % of Values
Mean Value = 6500 ppb
I.P. @ 13 %
Background Population, 87 % of Values
Mean Value = 250 ppb
Doromin Resources Ltd.
Hg values in silt samples, Mattajur Property, Moresby Island, B.C.
Feb. 1990
3.0 3.5 4.0 4.5 5.0 5.5 6.0 6.5 7.0
PROBITS