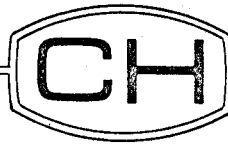


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CANNON-HICKS ASSOCIATES LTD.
SUITE 713-744 WEST HASTINGS ST.
VANCOUVER 1, B.C.

DUSTY MAC MINES LTD.

FEASIBILITY REPORT

BY

CANNON-HICKS ASSOCIATES LTD.

VANCOUVER, B.C.

FEBRUARY 24, 1971.

CANNON-HICKS ASSOCIATES LTD.

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February 24th, 1971.

Dusty Mac Mines Ltd.,
1710-1177 W.Hastings St.,
VANCOUVER, B.C.

Dear Sirs:

We present herewith our preliminary report on the feasibility of placing into production your Okanagan Falls property, pursuant to our proposal of December 17, 1970, and your acceptance thereof.

Our primary conclusion is that optimum profitability lies in shipment of the material as raw siliceous ore to Cominco Ltd., at Trail, B.C.

Cominco Ltd. have indicated to us the terms under which they may be prepared to accept the ore but are not prepared to offer a firm contract at this time. They have suggested that they may be in a position to do so in about one month from the date hereof.

Yours very truly,

CANNON-HICKS ASSOCIATES LTD.

H. Brodie Hicks
H. BRODIE HICKS, M. ENG. HICKS, ENG.
Consulting Engineer

HBH:mdc.
Encl.

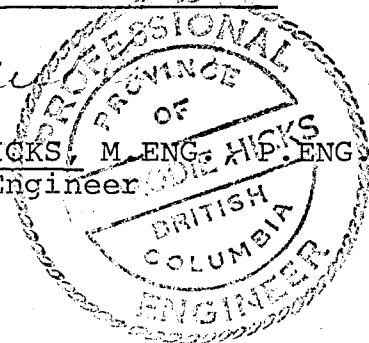


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CONCLUSIONS AND RECOMMENDATIONS:

1. Metal prices assumed herein are: gold - \$37.50 per ounce; silver - \$1.75 per ounce.
2. Ore reserves readily available by open pit mining are estimated at a minimum of 55,350 tons grading 0.23 oz/ton gold, 4.9 oz/ton silver, 80.4% silica, 5.9% alumina and 1.8% iron. Waste:ore ratio is 0.84:1. The reserves are classified as "probable".
3. These reserves may be profitably mined by (a) shipment as siliceous ore to Cominco Ltd. at Trail, B.C., (b) production of a flotation concentrate, or, (c) production of a cyanide precipitate.
4. The tables immediately following show cash flow projections for each of these alternatives. They may be summarised as follows:

	<u>Productive Life</u> <u>(Months)</u>	<u>Discounted</u> <u>Cash Flow</u>	<u>Capital</u> <u>Required</u>
Siliceous Ore	37 months	\$202,899	\$ 83,500
Flotation	18 "	189,139	331,000
Cyandiation	18 "	218,025	356,000

5. The last alternative, cyanidation, is not recommended because the anticipated difficulties of disposing of the cyanide residues would probably outweigh the small financial advantage.
6. Of the remaining alternatives, the production of raw siliceous ore is the more attractive. While requiring twice as long to mine out the orebody as in the case of flotation concentration, it will return an ultimately higher profit at much lower capital cost and risk.
7. It is therefore recommended that Dusty Mac Mines Ltd. proceed with planning for the production of raw siliceous ore for shipment to Cominco Ltd., at Trail, B.C.

CASH FLOW PROJECTIONS

	Alternative		
	a	b	c
Capital Costs			
Equipment	\$ ---	\$250,000	\$275,000
Preproduction	58,500	57,000	57,000
Working Capital	25,000	24,000	24,000
	83,500	331,000	356,000
Discounted Cash Value of Receipts	286,399	520,139	574,025
Discounted Cash Flow	\$202,899	\$189,139	\$218,025

Notes To Cash Flow Projections:

1. Operating income as follows:

Raw ore	\$ 6.78/ton
Flotation	\$ 9.90/ton
Cyanidation	\$10.80/ton

2. Present value of cash flow determined using an interest rate of 8%
(Reference: Mining Engineers' Handbook, 45-54)
3. Mining taxes estimated using B.C. Mining Tax Act.

COST FLOW PROJECTION

	RAW ORE (A)					FLOTATION (B)			CYANIDATION (C)		
	Present	Year 1	Year 2	Year 3	Year 4	Present	Year 1	Year 2	Present	Year 1	Year 2
Delivery-Tons	-	16,500	18,000	18,000	2,850	-	33,000	22,350	-	33,000	22,350
Operating Income	-	\$ 111,870	\$ 122,040	\$ 122,040	\$ 19,323	\$ -	\$ 323,400	\$ 219,030	\$ -	\$ 356,400	\$ 241,380
Taxes-Mining	-	-	12,665	13,952	14,899	-	-	36,580	-	-	41,725
-Federal	-	-	-	-	-	-	-	-	-	-	-
Capital Expen:											
Equipment	-	-	-	-	-	250,000	-	<75,000	275,000	-	<85,000
Preproduction	58,500	-	-	-	-	57,000	-	-	57,000	-	-
Working cap.	25,000	-	-	-	-	24,000	-	-	24,000	-	-
TOTAL	83,500	-	12,665	13,952	14,899	331,000	-	<38,420	356,000	-	<43,275
CASH FLOW	<83,500	111,870	109,375	108,088	4,424	<331,000	323,400	257,440	<356,000	356,400	284,655
DISCOUNTED VALUE:											
Investment	83,500					331,000			356,000		
Receipts		103,580	93,767	85,800	3,252		299,436	220,703		329,990	244,035
NET			202,899				189,139			218,025	



LOCATION AND SERVICES:

The property is situated immediately east of the village of Okanagan Falls and is comprised of 116 Mineral Claims, all held by Right of Location in the Osoyoos Mining Division of British Columbia. The orebody is located on the Joe #1 Claim, which is in good standing until August 1975. Surface rights to the immediate area are reported to have been acquired by the Company but this has not been authenticated by us.

A good gravel road leads to within a few hundred feet of the proposed mining site. Power, if required, would be brought from the substation of the West Kootenay Power and Light Co. at Okanagan Falls, a distance of approximately one and one quarter miles. Water sufficient for milling would probably have to be brought from Skaha Lake, a distance of 7,000 feet. Housing is available either at Okanagan Falls or at Penticton, some 12 miles north.

Disposal of tailings, should milling be adopted, could be carried out by damming one or more existing small draws and pot-holes in the immediate area. Because the property is centred in a farming and orchard area, unusual care would be required in dealing with effluent.

HISTORY:

There is no record of any substantial work on the property prior to its acquisition by Dusty Mac Mines in 1968.

Commencing late in 1968 and continuing through 1969, a programme of exploration was carried out under the direction of Cannon Engineering Ltd., and, later, of Cannon-Hicks

Associates Ltd. The work included surface trenching, geological mapping, diamond and percussion drilling and a limited underground programme and resulted in outlining the orebody substantially as it is now known. A report by Cannon-Hicks Associates Ltd., dated December, 1969, fully covers all results obtained.

Subsequently, the property was optioned to Noranda Exploration Ltd. which, in 1970, carried out a programme including extensive diamond drilling without adding substantially to the known ore. The option was allowed to lapse.

GEOLOGY:

The overall geology of the property is fully covered in the report of December, 1969 cited above.

Briefly, the ore is contained in a quartz breccia zone which extends over a length of 1,200 feet with widths up to 150 feet. This is generally underlain by an andesite porphyry breccia but tongues of the latter are occasionally found within the quartz mass. Structure is obscure. Metallic mineralisation consists of pyrite, sparse chalcopyrite, bornite and tetrahedrite together with occasional native gold and silver.

Ore occurrence is erratic and visual identification difficult. Careful mining control will be required.

ORE RESERVES:

Ore reserves are estimated at a minimum of 55,350 tons readily available by open-pit methods, grading 0.23 oz/ton gold, 4.9 oz/ton silver, 80.4% Silica, 5.9% alumina and 1.8% iron. Waste:ore ratio is 0.84:1.

Reserves are calculated from the results of cross-sectional drilling of the mineralised zone at 25-foot intervals. Both diamond and percussion drilling were employed. In addition, information was available from surface exposures and from sampling of an exploratory decline and raise.

Included herewith are a plan and 16 cross-sections showing the ore areas outlined as well as a longitudinal section of the underground work.

In consideration of the nature of the mineralisation and the type of information available, the reserves are categorized as "probable ore".

There are a number of ore-grade intersections in drill holes which are not included in this estimate because continuity with ore reserve blocks cannot be proved. It is possible, therefore, that ultimately a somewhat larger tonnage may be mined but for present purposes the figures quoted above are used.

MINING:

It is proposed to mine the deposit through three open pits designated Nos. 1, 2 and 3, opened respectively from the south, west and north and comprising respectively 7,350, 15,000

and 33,000 tons. Local topography lends itself to this approach which entails minimum removal of waste rock. The ore reserve plan herewith outlines the ore areas of the three pits.

Mining would commence in the #2 pit, which contains the best grade of ore and is more readily accessible than the #3 pit. The small #1 pit would be operated as a spare working place for otherwise idle equipment.

The most economical mining cost will be achieved by breaking and stockpiling a full years supply of ore in a single concentrated mining period of from two to three months duration, dependent on the production rate required. By this method, the necessary heavy equipment will be rented on a short-term basis without the necessity of tying up capital and senior supervision and engineering services will also only be required on the property for this limited term.

The overall cost of mining and stockpiling is estimated at \$3.00 per ton. Details are given in Table I herewith. Some explanatory details follow:

1. The mining rate is predicated on the preliminary Cominco proposal of accepting 1,500 tons per month of raw siliceous ore. This entails breaking of 18,000 tons of ore and 15,000 tons of waste annually.
2. In order to produce the size of material required by Cominco (maximum 12 inches) a large crusher would normally be required. Installed cost of a second-hand unit would be of the order of \$60,000

or in excess of \$1.00 per ton of reserves. As an alternative, it is proposed that a closer drilling pattern and higher explosive factor be adopted to break the ore to size in the pit at an approximate additional cost of \$0.36 per ton.

3. The erratic occurrence of mineralisation and the difficulty of recognizing ore visually renders it imperative to sample and assay much of the drill-hole cuttings. This will require an additional engineer's helper on the job as well as estimated assaying costs of \$5,000 annually.
4. Should circumstances permit a higher production rate, some improvement in costs would result but not of sufficient magnitude materially to affect the conclusions herein.

METALLURGICAL SAMPLE:

For purposes of metallurgical testing and determination of silica, alumina, and iron content, a new sample was selected making use of all available ore intersections from diamond drill holes. Percussion holes were not used because of a remote possibility of salting. The various intersections were weighted by length, holes were weighted into individual cross sections and these sections again weighted by ore reserve tonnages into a single composite.

Appendix "A" and attached tables give details of the procedure employed.

The single composite was made use of for metallurgical work while seven individual cross-section samples were assayed for silica, alumina and iron.

The metallurgical sample assayed 0.30 oz/ton gold and 6.1 oz/ton silver. This is higher than the ore reserve average because of the exclusion of percussion drilling results in certain lower-grade areas.

The silica, alumina and iron results are remarkably uniform as will be seen by reference to Table II. The weighted average is 80.4% silica, 5.9% alumina and 1.8% iron.

PRODUCTION OF RAW ORE:

Cominco Ltd. purchase siliceous material containing metallic values as siliceous ore. Tentative terms are set out in Appendix B.

At the moment of writing, Cominco have not confirmed these terms nor have they confirmed a delivery schedule although a maximum of 1,500 tons per month has been suggested. This proposed rate is made use of herein.

The net smelter return per ton of ore, based on the ore reserve grade of 0.23 oz/ton gold, 4.9 oz/ton silver, 80.4% silica, 5.9% alumina and 1.8% iron is \$17.62. This is before mining and shipping costs. Details of the calculation are set out in Appendix B(2).

Mining cost, as above, would be \$3.00 per ton delivered to a stockpile.

Loading, including rental of a small, second-hand loader, is estimated at \$0.60 per ton.

Hauling from a bin on the property to the delivery point at Trail has been quoted at \$6.40 per ton.

One part-time man at Okanagan Falls would be required at \$500 per month for ten months per year, or \$0.28 per ton.

Head office charges, engineering supervision and other overhead is estimated at \$1,000 per month for ten months per year or \$0.56 per ton.

In summary:		<u>Per Ton</u>
Net Smelter Return	-	\$17.62
Less, Mining	- \$3.00	
Loading	- 0.28	
Hauling	- 6.40	
Overhead	- 0.56	<u>10.84</u>
		Operating profit - \$6.78
		=====

Preproduction Expenditures

It is estimated that 6 weeks would be required after a decision to proceed before breaking commenced. During this period the economics of contracting vs. Company operation would be investigated and in the latter case equipment rented and personnel hired. A detailed pit design would be prepared.

Estimated cost:	\$3,000
Erection of a 100-ton bin	1,500
Mining and Stockpiling 18,000 tons	54,000
Payment by Cominco may be delayed up to two months. Hence, provision must be made for costs of delivery of 3,000 tons @ \$7.84, say -	25,000
	<u>\$83,500</u>
	=====

PRODUCTION OF A FLOTATION CONCENTRATE:

A copy of a metallurgical report prepared by Britton Laboratories is attached hereto as Appendix D.

The sample submitted was of somewhat higher grade than the ore reserve average, hence results are probably optimum.

By flotation, it is possible to recover 92.1% of the gold and 83.1% of the silver in a concentrate grading 14.5 oz/ton gold and 255.6 oz/ton silver. Ratio of concentration would be 52:1.

On the basis of a smelter schedule submitted by Cominco (Appendix C) and calculations therefrom (Appendix C(2)), the net smelter return per ton of ore is estimated at \$16.80.

Mining costs would remain at \$3.00 per ton and milling cost (see Table III) is estimated at \$4.00 per ton. Operating profit would thus be \$9.80 per ton.

A milling rate of 100 tons per day is suggested; thus, known ore reserves would be exhausted in approximately 18 months.

Capital cost of the mill is estimated at \$250,000, using second-hand equipment. The recoverable value, after exhaustion of the ore, is estimated at \$75,000. Capital costs are detailed in Table IV.

Preproduction Expenditures

It is estimated that four months would be required to achieve production and that a further two-months operating capital would be required thereafter. Mining would start one month before completion of the plant, but, in order to conserve funds, it is suggested that only 18,000 tons, or six-months supply, be broken during the first mining cycle.

Preproduction cash requirements would then be:

As per raw ore schedule, engineering	- \$ 3,000
As per raw ore schedule, mining, 18,000 tons	- 54,000
Mill	- 250,000
Two months working capital for mill, 6,000 tons @ \$4.00 per ton	- 24,000
	<hr/>
	\$331,000
	=====

PRODUCTION OF A CYANIDE PRECIPITATE:

Use of cyanidation as opposed to flotation would result in a higher per ton profit but it is our opinion that disposal of the cyanide residue in a settled agricultural area would increase costs to a still higher degree.

The Britton Report advises that, by cyanidation, 96.4% of the gold and 94.4% of the silver are recoverable in a precipitate.

The net smelter return per ton would be approximately \$1.50 higher than in the case of flotation. However, the capital cost would be increased by an estimated \$25,000 and operating cost by an estimated \$0.50 per ton. On this basis, operating profit would increase by \$0.50 per ton.

Preproduction expenditures, including working capital, would be of the order of \$360,000.

Before a decision to adopt cyanidation could be taken, lengthy negotiations with officials of the Pollution Board would be necessary.

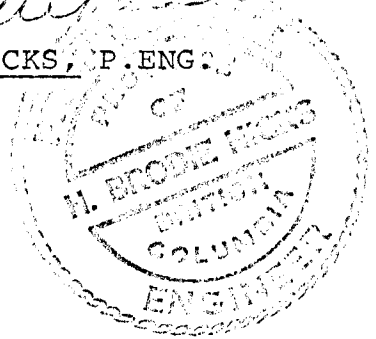
CONCLUSION:

We appreciate being entrusted with the preparation of this preliminary feasibility report. We will continue negotiations with Cominco in respect to their proposed raw siliceous ore schedule.

Respectfully submitted,

CANNON-HICKS ASSOCIATES LIMITED

H. Brodie Hicks
H. BRODIE HICKS, P. ENG.



:mdc.

TABLE IMINING COST

Basis is breaking of 18,000 tons of ore and 15,000 tons of waste on a once-a-year basis. On a two-shift schedule, 5 days per week, breaking 500 tons of rock per shift, this would require 6.6 weeks. With mobilization, etc. two months should be allowed.

A crew of two men plus one mechanic would suffice to drill and blast, including time for maintenance, moving and secondary blasting.

Supervision would include a project manager, a junior engineer and a helper-sampler. Because of the short term of employment, salaries would be above normal rates.

PARAMETERS:

Hole diameter - 3"
Hole pattern, ore - 5' x 5'
Hole pattern, waste - 6' x 6'
Drilling rate - 40 ft/hr.
Subgrade drilling - 10%
Rock density factor - 12 cu.ft/ton

Then, Yield/Ft. of Hole, ore - $\frac{5' \times 5'}{12} \times 90\% - 1.88$ tons

Yield/Ft. of Hole, waste $\frac{6' \times 6'}{12} \times 90\% - 2.70$ tons

Weighted Av. Yield/Ft. of Hole - 2.25 tons.

DRILLING COST: (Table I Cont'd)

Drill & Compressor Rental:		
\$3,000 mo/9,333	-	\$0.32
Fuel Oil, 8 g.p.h. @ \$0.20/gal.-		0.04
Lubricants	-	0.01
Repairs & Maintenance	-	0.14
Bits and Rods	-	0.11
		\$0.62

Whence, drilling cost/ton before labour charges - $\frac{\$0.62}{2.25}$ - \$0.28

Explosives - 0.15

Labour:

Driller/Shift inc. fringes		\$38.00
Helper / " " "		36.80
Mechanic/ " " "		40.00
		114.80

@ 500 tons/shift, cost/ton - $\frac{0.23}{\$0.66}$

COST/TON ORE BROKEN - \$0.66 x 1.84 - \$ 1.21

OVERHEAD CHARGES:

Supervision:

Project Manager, 2 months @ \$2,000	-	\$4,000
Junior Engineer, 2 " @ \$1,000	-	2,000
Helper-Sampler, 2 " @ 600	-	1,200
		\$7,200

Per Ton - $\frac{\$7,200}{18,000}$ - \$0.40

Assaying:

1,000 samples @ \$5.00 per sample - 0.28

Engineering & Administration: - $\frac{0.17}{0.85}$

LOADING, HAULING & STOCKPILING

Rental of 4 yd. loader & 25 ton truck @ \$2,500/mo. per ton	-	\$0.28
Load and Haul Ore, 1,000 ft.	-	0.20
Load and Haul Waste, 1,000 ft.	-	0.17
		0.65
		\$2.71
Contingencies, 10%		0.27
		0.27

GRAND TOTAL COST/TON ORE DELIVERED TO STOCKPILE \$2.98

say, \$3.00
=====

TABLE II
SILICA, ALUMINA AND IRON GRADES

<u>Section</u>	<u>Tons Assigned</u>	<u>SiO₂</u>	<u>Al₂O₃</u>	<u>Fe</u>
10,000	6,666	81.3	5.86	1.7
9,975	-	83.8	5.60	1.0
10,025	5,500	80.8	5.50	1.8
10,050	3,200	78.0	4.14	1.7
10,100	6,500	72.3	10.60	2.2
10,150	10,500	85.5	3.90	1.5
10,200	-	82.1	5.10	1.7
	<u>32,366</u>	<u>80.4</u>	<u>5.9</u>	<u>1.8</u>
	=====	=====	=====	=====

Subsequent to the selection of the above samples, a new ore reserve was calculated, based on a three-pit mining sequence and no reserves are now assigned to sections 9,975 and 10,200.

TABLE IIIMILLING COST

(Flotation @ 100 tons per day)

		<u>Per Ton</u>
Overall Supervision	-	\$ 0.67
Labour, 5 men @ \$35/shift	-	1.75
Sampling & Assaying	-	0.15
Reagents and steel	-	0.25
Operating & Maintenance Supplies	-	0.75
Power	-	0.30
Heat, Water, Tailings Disposal	-	0.10
		<hr/>
		\$3.97
	say,	\$4.00
		=====

TABLE IV

CAPITAL COST FLOTATION MILL

(100 tons per day)

Purchase, second hand equipment -	\$100,000
Delivery -	2,500
Housing -	25,000
Installation -	60,000
Design -	10,000
Electrics -	25,000
Water Supply -	20,000
	<hr/>
	\$242,500
say,	\$250,000
	=====

APPENDIX "A"SAMPLE SELECTIONFORMETALLURGICAL TESTINGANDDETERMINATION OF SiO_2 AND Al_2O_3

Ore reserves are based on the results of both diamond drill and percussion holes. Because there is a remote possibility of salting in the latter, only the diamond drill cores were used in compiling samples. Where assay office rejects were available these were taken; otherwise the remaining half cores were used.

Significant results are available on holes from sections 9,975, 10,000, 10,025, 10,050, 10,100, 10,150 and 10,200. Some additional samples were taken of ore-grade material from holes outside the ore-reserve boundaries to provide additional test material if required.

Table A-1 shows a list of sections with samples selected.

Samples for each of the seven significant sections were made up by combining the core from the various holes, weighted by length of ore intersection in each hole. Table A-2 gives details.

APPENDIX A (Cont'd)

The seven section samples were each assayed for silica and alumina. For purposes of metallurgical testing, however, all except the sample from section 9,975, which was too small, were combined into a single sample by weighting on the basis of ore-reserve tonnage calculated for each section. The weights assigned are shown in Table A-3.

Table A-4 sets out the calculations leading to an estimate of the average grade of each section and of the final metallurgical sample. This was expected to assay 0.32 oz/ton gold and 6.1 oz/ton silver. The actual values obtained were 0.30 oz/ton gold and 5.9 oz/ton silver. This is above the ore reserve grade due to the omission of the percussion hole samples but, is considered sufficiently close to be satisfactory for metallurgical investigations.

TABLE A - 1

METALLURGICAL SAMPLE LIST

<u>Line</u>	<u>D.D.H. Nos.</u>	<u>Footage</u>	<u>Tons Assigned</u>
9,800	Nil		170
9,825	Nil		3,170
9,850	Nil		1,570
9,875	Nil		2,470
9,900	Nil		2,790
9,925	Nil		2,170
9,950	61	5'	2,000
9,975	20	10'	5,180
10,000	1	35'	
	2	30'	
	3	30'	
	4	10'	8,600
	5	10'	
	6	30'	
	7	20'	
	45	5'	
10,025	9	20'	
	10	30'	6,900
	11	20'	
	12	35'	
	13	15'	
10,050	60	10'	8,300
	69	30'	
10,075	Nil		5,300
10,100	25	30'	
	26	15'	3,800
10,125	Nil		11,100
10,150	59	65'	14,100
10,175	Nil		12,200

METALLURGICAL SAMPLE LIST

<u>Line</u>	<u>D.D.H. Nos.</u>	<u>Footage</u>	<u>Tons Assigned</u>
10,200	30	5'	
	31	35'	6,100
	47	10'	
	58	10'	
10,300	35	10'	
	36	10'	Nil
	37	5'	
10,400	40	10'	Nil

TABLE A - 3

METALLURGICAL SAMPLE - Section Weighting

<u>Section</u>	<u>Assigned Tons</u>	<u>Weight</u> <u>%</u>
10,000	8,600	18
10,025	6,900	14
10,050	8,300	17
10,100	3,800	8
10,150	14,100	30
10,200	<u>6,100</u>	<u>13</u>
	<u>47,800</u>	<u>100</u>

METALLURGICAL SAMPLE - Grade Estimate

<u>Section</u>	<u>Hole No.</u>	<u>Grade</u>		<u>Weight</u> %	<u>Weighted Grade</u>	
		<u>Au oz/ton</u>	<u>Ag oz/ton</u>		<u>Au oz/ton</u>	<u>Ag oz/ton</u>
10,000	1	0.59	13.1	4		
	2	0.04	2.0	7		
	3	0.02	1.4	26		
	4	1.25	14.1	22	0.37	6.8
	5	0.50	11.9	7		
	6	0.24	15.7	7		
	7	0.08	2.7	22		
	45	0.12	3.1	5		
10,025	9	0.29	5.8	17		
	10	0.52	12.6	25		
	11	0.38	9.1	17	0.26	7.0
	12	0.02	3.0	29		
	13	0.09	3.2	12		
10,050	60	0.46	9.0	20	0.36	5.2
	69	0.34	4.3	80		
10,100	25	0.12	2.8	67	0.11	2.6
	26	0.08	2.1	33		
10,150	59	0.27	6.0	100	0.27	6.0
10,200	30	0.10	0.8	8		
	31	0.99	14.4	58	0.59	10.3
	47	0.02	8.7	17		
	58	0.08	2.1	17		

SUMMARY

METALLURGICAL SAMPLE

<u>Section</u>	<u>Grade</u>		<u>Weight</u> %	<u>Weighted Grade</u>	
	<u>Au oz/ton</u>	<u>Ag oz/ton</u>		<u>Au oz/ton</u>	<u>Ag oz/ton</u>
10,000	0.37	6.8	18		
10,025	0.26	7.0	14		
10,050	0.36	5.2	17	0.33	6.4
10,100	0.11	2.6	8		
10,150	0.27	6.0	30		
10,200	0.59	10.3	13		

APPENDIX B

TENTATIVE COMINCO TERMS FOR
PURCHASE OF SILICEOUS ORE

NOTE:

Cominco will purchase siliceous material either as flux or as siliceous ore. Terms are identical except that flux is not sampled and there is no payment for metallic content. Hence, for Dusty Mac, the material would have to be handled as siliceous ore.

PAYMENTS:

- Gold - Pay for 95% of contained gold with a minimum deduction of 0.03 oz/ton at London price less \$1.25/oz.
- Silver - Pay for 94% of contained silver with a minimum deduction of one oz/ton at Handy and Harmon unrefined quote less one cent/oz.
- Silica - Pay for 100% of contained silica at \$0.⁰⁸075/unit.

DEDUCTIONS:

- Silica: (100% - actual content %) x \$0.08
- Al₂O₃ : \$0.15/unit.
- Fe : \$0.50/unit.
- Handling: \$1.00 - \$2.50 (see below)

Over 6% Al₂O₃ is not desired. Individual lots carrying more than this would not be rejected, but this should be the cumulative target. The smelter has an overall limited

APPENDIX B (Cont'd)

capacity to absorb alumina.

QUANTITIES:

Would probably require 1,000 tons per month up to, depending on other deliveries of siliceous materials, a maximum of 1,500 tons per month.

LOTS:

For a continuous operation, 500-ton lots are optimum. This is the daily capacity of the larger crusher - sampling unit. Handling charges through this unit are \$1.00 per ton. Smaller lots are handled through a smaller unit with handling charges running up to \$2.50 per ton.

DELIVERY:

May be by truck or gondola rail car.

With trucks, loads are dumped in the yard until a lot (500 tons) has accumulated.

With cars, these are switched to a yard siding (with consequent demurrage) until a lot has accumulated.

LUMP SIZE:

The crushing and sampling plants are integral so all material must go through the crusher. There is no reduction in handling charges for pre-crushed material.

Maximum lump size is 12". Larger lumps are hand-broken at day-labour rates.

APPENDIX B(2)

NET SMELTER RETURN PER TON, RAW ORE

Using the January 1971 ore reserve calculation,
the overall grade may be cited as:

Gold	-	0.23 oz/ton
Silver	-	4.9 oz/ton
Silica	-	80.4%
Alumina	-	5.9%
Iron	-	1.8%

Payments:

Gold:	(0.23 x 95%) x \$37.50	- \$1.25	- \$7.92
Silver:	(4.9 x 94%) x \$ 1.75	- \$0.01	- 8.01
Silica:	80.4 x \$0.075	-	6.03
			<hr/>
			\$21.96

Less:

Silica:	(100.0 - 80.4) x \$0.08	- \$1.57
Alumina:	5.9 x \$0.15	- .87
Iron:	1.8 x \$0.50	- .90
Handling:		- <u>1.00</u> 4.34
Net Before Mining & Freight		- <u>\$17.62</u>
		<u>=====</u>

Siliceous Ore Settlement - Final



APPENDIX B

Our Serial No. **9573-C**
 In Account with **DUSTY MAC MINES LTD.**
c/o CANNON-HICKS ASSOCIATES LTD.
744 W. HASTINGS ST.
VANCOUVER, B.C.

Trail, B.C. **OCTOBER 1**, 19 **69**

For **Siliceous Ore** Lot No. **1** Car No. **2 trucks** Received **Sept. 8th**

Freight Value \$ _____ Freight Rate \$ _____

Scale Weight			Weight of Shipment				Moisture		Net Dry Weight		Dry Tons
Gross	Tare	Net	Gross	No. Sacks	Wt of Sacks	Net Wet Wt.	% H ₂ O	Net Dry Wt.	Dry Tons		
						53,710	.9	483	53,227	26.6135	
lbs.	lbs.	lbs.	lbs.		lbs.	lbs.	lbs.	lbs.			

Assays										
Gold	Silver	Wet Lead	Zinc	Sulphur	Silica	Iron	Lime	Arsenic	Alumina	Antimony
oz. per dry ton	oz. per dry ton	%	%	%	%	%	%	%	%	%
	1.1	.2	.1	.1	75.5	2.2	.4	.1	11.4	.1

Average Quotations		
Week Ending	Sept. 20	19 69
Exchange		

Gold	London Final Price \$	Less \$1.25	Net \$	oz.
S.	New York Price \$ 1.784	@ 7.78122	Less .04	Net \$ 1.88282 oz.
Lead	New York Price \$	C. lb.	Less	C. Net C. lb.
Zn PW	St. Louis Price \$	C. lb.	Less	C. Net C. lb.

Contents and Value			
Contents	Contents Paid for	Net Quotation	Value
29.27 Ozs. Gold	%	ozs. @ \$	/oz. \$
Oz. Silver	26.61 lbs. @ .15	ozs. @ \$ 1.88282	/oz. 5.01
Lbs. Lead	%	lbs. @	C./lb.
Lbs. Zinc	%	lbs. @	C./lb.
			\$ 5.01
* Credit @ \$			Details Below 16.16 Dr
Less: Trucking			Total Gross Value \$ 11.15 Dr
Switching			
Freight			
Less % Royalty on \$ _____ to _____			\$ 11.15 Dr

CREDIT		\$3.50 Cr	
Dr. Alumina	11.4 @ .15	1.71 *	11.15 Dr
Dr. Iron Fe ₂ O ₃	2.2 x 1.43 = 3.1 @ .15	.47	13.84 Cr
Dr. Lead as Pb 5	.2 x 1.15 = .2 @ .15	.03	
Dr. Zinc as Zn 5	.1 x 1.49 = .1 @ .15	.02	30.00
Arsenic			16.16 Dr
Moisture			
Truck Handling	Truck	.75	
Dr Dry Ton		.52 Cr	RH/bj

Siliceous Ore Settlement - Final



0-4410-7

Our Serial No. **237-C**
 In Account with **Dusty Mac Mines Ltd.**
c/o Cannon-Hicks Associates Ltd.
744 W. Hastings St.
Vancouver, B.C.

Trail, B.C. Jan. 15, 19 70

For **siliceous ore** Lot No. **2**

Car No. **CP 358405** Received **Dec. 12/69**

Freight Value \$ **64.04 per W.T.**
 Freight Rate \$ **13.08**

Scale Weight			Weight of Shipment						
Gross	Tare	Net	Gross	No. Sacks	Wt of Sacks	Net Wet Wt.	% H ₂ O	Net Dry Wt.	Dry Tons
214,160	48,340	165,820				165,820	3.5	160,016	80.008
lbs.	lbs.	lbs.	lbs.		lbs.	lbs.	lbs.	lbs.	

Assays										
Gold	Silver	Wet Lead	Zinc	Sulphur	Silica	Iron	Lime	Arsenic	Alumina	Antimony
.904	19.4	.2	.3	.2	85.9	1.8	.4	.1	5.9	.1
oz. per dry ton	oz. per dry ton	%	%	%	%	%	%	%	%	%

Average Quotations

Week Ending	Dec. 20, 19 69	Exchange
Gold	London Final Price \$ 35.052	@ 7.425
	New York Price \$ 1.745	"
Lead	New York Price \$	C. lb.
Zinc "PW"	St. Louis Price \$	C. lb.
		Less \$1.25
		Less \$.04
		Less
		Less
		Net \$ 36.40461
		Net \$ 1.83457
		C. Net
		C. Net
		C. Net
		C. lb.
		C. lb.

Contents and Value

Contents	Contents Paid for	Net Quotation	Value
72.327 Ozs. Gold	95 % 68.711	ozs. @ \$ 36.40461 /oz.	\$ 2,501.40
1,552.16 Oz. Silver	80.01 oz. M.D. 1,472.15	ozs. @ \$ 1.83457 /oz.	2,700.76
Lbs. Lead	%	lbs. @	C./lb.
Lbs. Zinc	%	lbs. @	C./lb.

* Treatment base \$2.13 Cr. x 80.008 = \$170.42*
 Breaking lumps 63.00
 Cr. \$107.42

Add: \$ 5,202.16
 Credit @ \$ 107.42 Cr.
 Less: Total Gross Value \$ 5,309.58
 Trucking
 Switching
 Freight \$13.08 x 82.91

Less % Royalty on \$ to

Silica	CREDIT	Dr. Alumina	Dr. Iron Fe ₂ O ₃	Dr. Lead as Pb 5	Dr. Zinc as Zn 5	Arsenic	Dr. Moisture	Dr. Extra Handling
	\$3.50	5.9 @ \$.15	1.8 x 1.43 = 2.6 @ \$.15	.2 x 1.15 = .2 @ \$.15	.3 x 1.49 = .4 @ \$.15			
		.89	.39	.03	.06			

\$ 4,225.12
 \$ 4,225.12

Net per Dry Ton \$ **2.13 Cr.**

/ag

APPENDIX C

TENTATIVE COMINCO TERMS FOR
PURCHASE OF HIGH GRADE CONCENTRATES

Gold - Pay for 95% of contained gold with a minimum deduction of 0.03 oz/ton at London price less \$1.25 oz.

Silver - Pay for 94% of contained silver with a minimum deduction of one oz/ton at Handy and Harman unrefined quote less one cent per ounce.

DEDUCTIONS:

- Treatment Charge - \$9.00 per dry ton.
- Container Handling - \$4.00 per dry ton.
- Sampling and Assaying - \$250.00/lot, maximum 15 tons (or \$16.67 per dry ton).
- Iron penalty - \$0.50/unit over 0.1%.
- Arsenic penalty - \$2.50/unit over 0.1%.

APPENDIX C(2)

NET SMELTER RETURN, FLOTATION CONCENTRATE

CONCENTRATE GRADE:

Gold	-	14.5 oz/ton.
Silver	-	255.6 oz/ton.
Iron	-	8.6%
Arsenic	-	0.05% (below penalty limit)

PAYMENTS:

Gold	-	(14.51 x 95%) x (\$37.50 - \$1.25)	-	\$499.34
Silver	-	(255.6 x 94%) x (\$1.75 x \$0.01)	-	\$418.06
				<u>\$917.40</u>
				=====

DEDUCTIONS:

Treatment	-	\$9.00	
Handling	-	4.00	
Sampling, etc.	-	16.67	
Iron Penalty	-	4.25	
Freight	-	<u>10.00</u>	<u>43.92</u>

NET SMELTER RETURN/TON CONCENTRATE		<u>\$873.48</u>	=====
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NET SMELTER RETURN/TON ORE - $\frac{\$873.48}{52}$	-	<u>\$16.80</u>	=====
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APPENDIX D

METALLURGICAL TESTS ON A SAMPLE OF

"DUSTY MAC" GOLD - SILVER ORE

submitted by

CANNON - HICKS ASSOCIATES LTD.

Our Project No: B300

Date: February 16, 1971

BRITTON RESEARCH LIMITED

1612 WEST THIRD AVENUE

VANCOUVER 9, B. C.

CANADA

BRITTON RESEARCH LIMITED

Consulting Metallurgists

1612 WEST THIRD AVENUE

VANCOUVER 9, B. C.

CANADA

JOHN W. BRITTON, A.R.S.M., B.Sc., P.Eng.
PRESIDENT

February 16, 1971.

PHONE: 738-7195
AREA CODE: 604

Mr. H. Brodie Hicks,
Cannon-Hicks Associates Ltd.,
714-744 West Hastings Street,
Vancouver 1, B. C.

Dear Brodie,

Re: "Dusty Mac" mine

Results of our flotation and cyanidation tests on the composite sample of "Dusty Mac" gold - silver ore, which we received on January 7, 1971 were as follows:

Head assays

		<u>Direct assays</u>	<u>Calculated assays</u> (from test results)
Gold	(Au)	0.28 oz/ton	0.30 oz/ton
Silver	(Ag)	5.65 oz/ton	5.91 oz/ton

Flotation test

A 3000 gram sample of minus 10 mesh ore was ground wet in a ball mill to 82% minus 200 mesh and floated; the rougher concentrate was cleaned once. Test conditions and results are shown in tables 1 and 2; a screen analysis of the flotation feed is given in table 7.

Comments: 92.1% of the gold and 83.1% of the silver were recovered in the cleaned concentrate, which assayed 14.52 oz/ton gold and 255.6 oz/ton silver. An additional 0.5% of the gold and 1.7% of the silver were present

in the cleaner tailing. Only 0.2% of the gold and 0.8% of the silver were recovered in the scavenger concentrate. 7.2% of the gold and 14.4% of the silver were lost in the scavenger tailing.

Allowing for recirculation of cleaner tailings, it is expected that at least 92% of the gold and 84% of the silver would be recovered if similar ore is treated in a full-scale mill. (A coarser grind, say 60-65% minus 200 mesh, may be possible without seriously reducing the gold and silver recoveries.)

Cyanidation tests

Two 1000 gram samples of minus 10 mesh ore were ground for 15 and 20 minutes respectively at 60% solids. After thickening to 40% solids, the pulps were cyanided for 40 hours in an open rolling bottle, followed by filtering and washing of the residue. Test conditions and results are given in tables 3 to 6 inclusive.

Comments: After grinding to 67% -200 mesh, 96.4% of the gold and 94.4% of the silver were extracted by cyanidation. Cyanide and lime consumptions (0.62 lb NaCN/ton and 3.94 lb Ca(OH)₂/ton) were satisfactory; the pulp filtered rapidly. Finer grinding, to 82% minus 200 mesh, improved the gold and silver extractions by only 0.3% and 0.7% respectively.

Yours sincerely,

BRITTON RESEARCH LIMITED

John W. Britton, P. Eng.
Consulting Metallurgist

JWB/lis
Mr. H. Brodie Hicks (3)

Test 300 - F1 conditions

Table 1

	STAGES								Total reagents
	1	2	3	4	5	6	7	8	
Reagents: Lb/ton of ore									
H ₂ SO ₄	-	-	-	-	-	1.5	-	-	1.5
CuSO ₄ · 5H ₂ O	-	-	-	-	-	0.3	-	-	0.3
CX-51 (a)	-	0.10	-	0.10	0.10	-	0.10	0.03	0.43
Pine oil	-	0.024	-	0.012	0.012	-	-	-	0.048
Aerofloat 31	-	0.032	-	-	0.016	-	0.016	-	0.064
Pulp volume - ml (b)	-	9000	9000	9000	9000	9000	9000	2600	-
% solids	60	28	28	-	-	26	26	6	-
Time - minutes	(c)	5	5	5	5	5	5	10	-
pH	-	8.4	8.5	8.6	8.7	6.7	7.6	8.5	-
Temperature - °C	-	22	22	23	23	23	24	20	-

Notes: (a) Potassium amyl xanthate; (b) Per 3000 grams of ore; (c) 3 batches of 1000 grams -10 mesh ore each ground for 20 minutes at 60% solids, combined for flotation.

- Stages:
1. Grinding (82% -200 mesh)
 2. Conditioning
 3. Rougher flotation - 1st stage
 4. " " - 2nd "
 5. " " - 3rd "
 6. Conditioning
 7. Scavenger flotation
 8. Cleaning (of rougher concentrate only)

Test 300 - F1

Table 2

Individual results

#	Product	Weight %	Assays		Distribution %	
			Au oz/ton	Ag oz/ton	Au	Ag
1	Cleaner concentrate	1.91	14.52	255.6	92.1	83.1
2	" tailing	3.23	0.05	3.13	0.5	1.7
3	Scavenger concentrate	1.03	0.06	4.75	0.2	0.8
4	" tailing	93.83	0.023	0.90	7.2	14.4
5	Head (calculated)	100.00	0.30	5.88	100.0	100.0
5	Head (direct assays)		0.28	5.65		

Cumulative results

1	Cleaner concentrate	1.91	14.52	255.6	92.1	83.1
1 + 2	Rougher "	5.14	5.43	96.9	92.6	84.8
1 to 3	Ro. + scav. concentrates	6.17	4.53	81.6	92.8	85.6

Test 300 - C1

Grind: 67% -200 mesh, 49% -325 mesh (1000 grams minus 10 mesh ore ground for 15 minutes at 60% solids)

Table 3

Metallurgical results

#	Product	Cyan. time- Hours	Amount	Assays		Distribution %	
				Au	Ag	Au	Ag
1	Cyan. filtrate*	40	3 litres	3.360 mg/l.	64.130 mg/l.	96.4	94.4
2	Residue	-	100.03%	0.011 oz/ton	0.331 oz/ton	3.6	5.6
3	Head (calculated)	-	100.00%	0.30 oz/ton	5.94 oz/ton	100.0	100.0
3	Head (direct assays) -			0.28 "	5.65 "		

* Including washes.

Table 4

Cyanide and lime consumptions

Stage	Cyan. time- Hours	Sodium Cyanide		Lime			
		Lb. 100% Added	NaCN/ton of ore Consumed	Lb. 100% Ca(OH) ₂ /ton of ore Added		Consumed	
				Ind.	Cum.	Ind.	Cum.
Grind	-	-	-	5.00	5.00)		
Cyanidation	40	7.76	0.62	2.00	7.00)	3.94**	3.94**
Total	-	7.76	0.62	7.00	7.00	3.94	3.94

** Including Ca(OH)₂ added to grind.

Test 300 - C2

Grind: 82% -200 mesh, 62% -325 mesh (1000 grams minus 10 mesh ore ground for 20 minutes at 60% solids)

Table 5

Metallurgical results

#	Product	Cyan. time- Hours	Amount	Assays		Distribution	
				Au	Ag	Au %	Ag
1	Cyan. filtrate*	40	3 litres	3.350 mg/l.	64.35 mg/l.	96.7	95.1
2	Residue	-	100.20%	0.010 oz/ton	0.290 oz/ton	3.3	4.9
3	Head (calculated)	-	100.00%	0.30 oz/ton	5.92 oz/ton	100.0	100.0
3	Head (direct assays) -	-	-	0.28 "	5.65 "	-	-

* Including washes

Table 6

Cyanide and lime consumptions

Stage	Cyan. time- Hours	Sodium Cyanide		Lime			
		Lb. 100% Added	NaCN/ton of ore Consumed	Lb. 100% Ca(OH) ₂ Added		/ton of ore Consumed	
				Ind.	Cum.	Ind.	Cum.
Grind	-	-	-	5.00	5.00)		
)	4.36**	4.36**
Cyanidation	40	7.76	0.68	2.00	7.00)		
Total	-	7.76	0.68	7.00	7.00	4.36	4.36

** Including Ca(OH)₂ added to grind.

Screen analyses

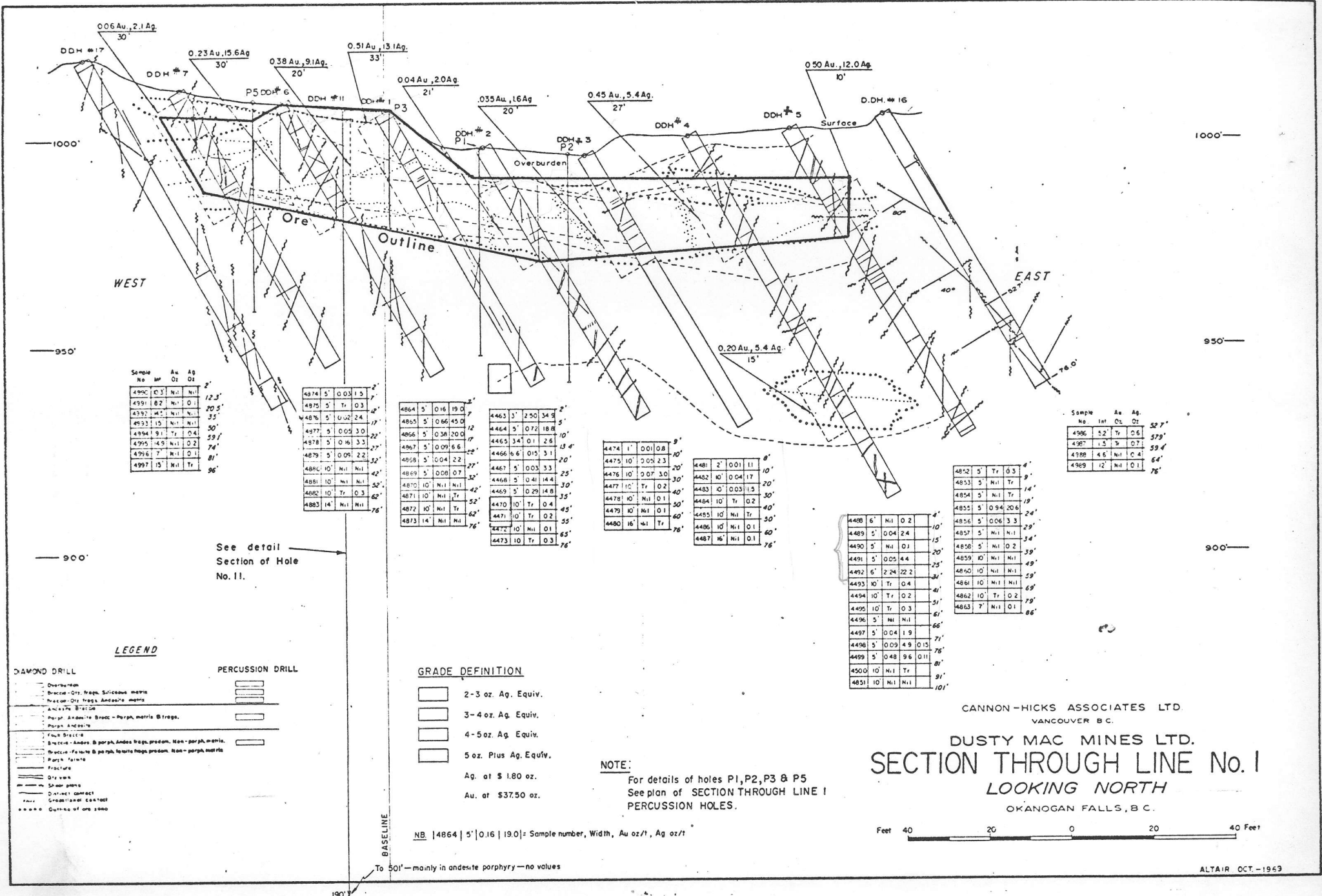
Table 7

Mesh (Tyler)	<u>Feed to ball mill</u>			<u>Feed to test 300-C1</u>			<u>Feed to tests 300-C2 and 300-F1</u>		
	% retained Ind.	% retained Cum.	% passing Cum.	% retained Ind.	% retained Cum.	% passing Cum.	% retained Ind.	% retained Cum.	% passing Cum.
10	-	-	100.0	-	-	100.0	-	-	100.0
14	2.9	2.9	97.1	-	-	100.0	-	-	100.0
20	12.8	15.7	84.3	-	-	100.0	-	-	100.0
28	23.7	39.4	60.6	-	-	100.0	-	-	100.0
35	12.3	51.7	48.3	-	-	100.0	-	-	100.0
48	10.3	62.0	38.0	0.2	0.2	99.8	-	-	100.0
65	7.9	69.9	30.1	1.0	1.2	98.8	0.1	0.1	99.9
100	5.3	75.2	24.8	4.2	5.4	94.6	0.7	0.8	99.2
150	4.1	79.3	20.7	10.7	16.1	83.9	4.2	5.0	95.0
200	4.0	83.3	16.7	17.3	33.4	66.6	13.5	18.5	81.5
+325	3.7	87.0	13.0	17.7	51.1	48.9	19.6	38.1	61.9
-325	13.0	100.0	-	48.9	100.0	-	61.9	100.0	-
Total	100.0	100.0	-	100.0	100.0	-	100.0	100.0	-



DUSTY MAC MINES LTD

CANNON-HICKS ASSOCIATES LTD.	
VANCOUVER	B.C.
DUSTY MAC MINES LTD.	
PROJECT: _____	No. _____
by: B. HICKS	
SCALE: 1" = 136mi. DATE: FEB. '71	



Sample No	Wt	Au	Ag
4990	0.3	Nil	Nil
4991	0.2	Nil	0.1
4992	0.1	Nil	0.1
4993	0.15	Nil	0.1
4994	0.1	Tr	0.4
4995	0.15	Nil	0.2
4996	0.1	Nil	0.1
4997	0.15	Nil	Tr

4874	5'	0.03	1.3
4875	5'	Tr	0.3
4876	5'	U.02	2.4
4877	5'	0.05	3.0
4878	5'	0.16	3.3
4879	5'	0.09	2.2
4880	10'	Nil	Nil
4881	10'	Nil	Nil
4882	10'	Tr	0.3
4883	14'	Nil	Nil

4864	5'	0.16	19.0
4865	5'	0.66	43.0
4866	5'	0.38	20.0
4867	5'	0.09	6.6
4868	5'	0.04	2.2
4869	5'	0.08	0.7
4870	10'	Nil	Nil
4871	10'	Nil	Tr
4872	10'	Nil	Tr
4873	14'	Nil	Nil

4463	5'	2.50	34.9
4464	5'	0.72	18.8
4465	3.4'	0.1	2.6
4466	6.6'	0.15	3.1
4467	5'	0.03	3.3
4468	5'	0.41	14.4
4469	5'	0.29	14.8
4470	10'	Tr	0.4
4471	10'	Tr	0.2
4472	10'	Nil	0.1
4473	10'	Tr	0.3

4474	1'	0.01	0.8
4475	10'	0.02	2.3
4476	10'	0.07	3.0
4477	10'	Tr	0.2
4478	10'	Nil	0.1
4479	10'	Nil	0.1
4480	16'	Nil	Tr

4481	2'	0.01	1.1
4482	10'	0.04	1.7
4483	0'	0.03	1.3
4484	10'	Tr	0.2
4485	10'	Nil	Tr
4486	10'	Nil	0.1
4487	16'	Nil	0.1

4488	6'	Nil	0.2
4489	5'	0.04	2.4
4490	5'	Nil	0.1
4491	5'	0.05	4.4
4492	6'	2.24	22.2
4493	10'	Tr	0.4
4494	10'	Tr	0.2
4495	10'	Tr	0.3
4496	5'	Nil	Nil
4497	5'	0.04	1.9
4498	5'	0.09	4.9
4499	5'	0.48	9.6
4500	10'	Nil	Tr
4501	10'	Nil	Nil

Sample No	Wt	Au	Ag
4987	5.2	Tr	0.6
4988	1.5	Tr	0.7
4989	4.6	Nil	0.4
4989	12	Nil	0.1

4852	5'	Tr	0.3
4853	5'	Nil	Tr
4854	5'	Nil	Tr
4855	5'	0.94	20.6
4856	5'	0.06	3.3
4857	5'	Nil	Nil
4858	5'	Nil	0.2
4859	10'	Nil	Nil
4860	10'	Nil	Nil
4861	10'	Nil	Nil
4862	10'	Tr	0.2
4863	7'	Nil	0.1

See detail Section of Hole No. 11.

LEGEND

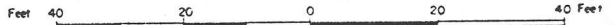
- DIAMOND DRILL**
- Overburden
 - Breccia - Qtz frags, Siliceous matrix
 - Breccia - Qtz frags, Andesite matrix
 - Andesite Breccia
 - Porphy Andesite Breccia - Porph. matrix @ frags.
 - Porphy Andesite
 - Fine Breccia
 - Breccia - Andes. & porph. Andes frags, predom. Non-porph. matrix
 - Breccia - Fine brecc. & porph. to coarse frags, predom. Non-porph. matrix
 - Porphy. Matrix
 - Fracture
 - Discontinuity
 - Spore zone
 - District contact
 - Granite layer contact
 - Outcrop of ore zone
- PERCUSSION DRILL**
- Overburden
 - Andesite Breccia
 - Porphy Andesite Breccia - Porph. matrix @ frags.
 - Porphy Andesite
 - Fine Breccia
 - Breccia - Andes. & porph. Andes frags, predom. Non-porph. matrix
 - Breccia - Fine brecc. & porph. to coarse frags, predom. Non-porph. matrix
 - Porphy. Matrix
 - Fracture
 - Discontinuity
 - Spore zone
 - District contact
 - Granite layer contact
 - Outcrop of ore zone

GRADE DEFINITION

- 2-3 oz. Ag. Equiv.
- 3-4 oz. Ag. Equiv.
- 4-5 oz. Ag. Equiv.
- 5 oz. Plus Ag. Equiv.
- Ag. at \$ 180.00.
- Au. at \$37.50 oz.

NOTE:
For details of holes P1, P2, P3 & P5
See plan of SECTION THROUGH LINE 1
PERCUSSION HOLES.

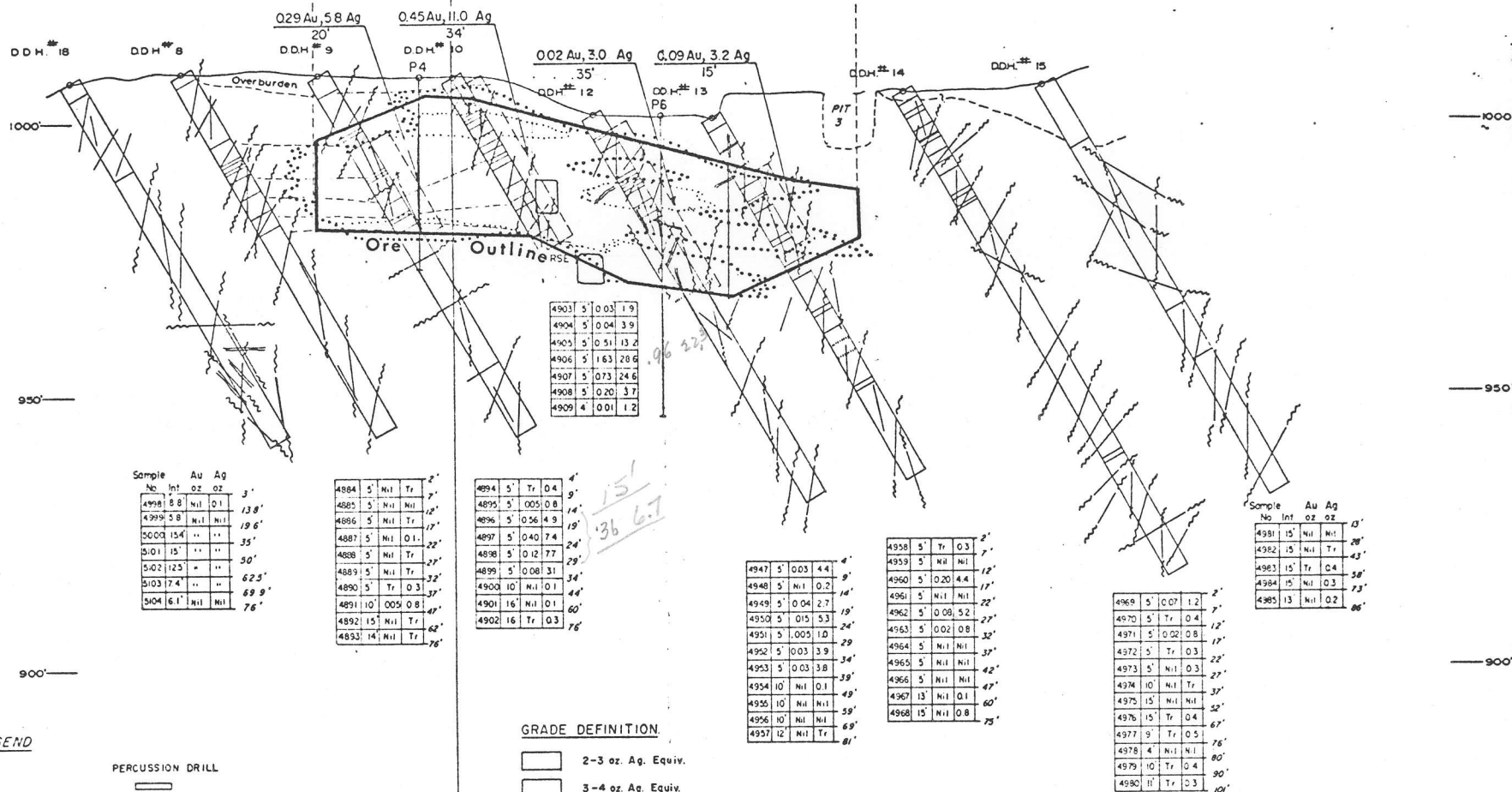
CANNON-HICKS ASSOCIATES LTD
VANCOUVER B.C.
DUSTY MAC MINES LTD.
SECTION THROUGH LINE No. 1
LOOKING NORTH
OKANOGAN FALLS, B.C.



Average DDH'S 9,10,12,13

Au 0.22, Ag 6.2

100' Long X 25' Depth



4901	5'	0.03	1.9
4904	5'	0.04	3.9
4905	5'	0.51	13.2
4906	5'	1.63	28.6
4907	5'	0.73	24.6
4908	5'	0.20	3.7
4909	4'	0.01	1.2

Sample No	Au Int. oz	Ag oz	Tr
4958	8.8	Nil	0.1
4959	5.8	Nil	Nil
5000	15.4	"	"
5001	15	"	"
502	125	"	"
503	7.4	"	"
504	6.1	Nil	Nil

4884	5'	Nil	Tr
4885	5'	Nil	Nil
4886	5'	Nil	Tr
4887	5'	Nil	0.1
4888	5'	Nil	Tr
4889	5'	Nil	Tr
4890	5'	Tr	0.3
4891	10'	0.05	0.8
4892	15'	Nil	Tr
4893	14'	Nil	Tr

4894	5'	Tr	0.4
4895	5'	0.05	0.8
4896	5'	0.56	4.9
4897	5'	0.40	7.4
4898	5'	0.12	7.7
4899	5'	0.08	3.1
4900	10'	Nil	0.1
4901	16'	Nil	0.1
4902	16'	Tr	0.3

4947	5'	0.03	4.4
4948	5'	Nil	0.2
4950	5'	0.15	5.3
4951	5'	0.05	1.0
4952	5'	0.03	3.9
4953	5'	0.03	3.8
4954	10'	Nil	0.1
4955	10'	Nil	Nil
4956	10'	Nil	Nil
4957	12'	Nil	Tr

4958	5'	Tr	0.3
4959	5'	Nil	Nil
4960	5'	0.20	4.4
4961	5'	Nil	Nil
4962	5'	0.06	5.2
4963	5'	0.02	0.8
4964	5'	Nil	Nil
4965	5'	Nil	Nil
4966	5'	Nil	Nil
4967	13'	Nil	0.1
4968	15'	Nil	0.8

4969	5'	0.07	1.2
4970	5'	Tr	0.4
4971	5'	0.02	0.8
4972	5'	Tr	0.3
4973	5'	Nil	0.3
4974	10'	Nil	Tr
4975	15'	Nil	Nil
4976	15'	Tr	0.4
4977	9'	Tr	0.5
4978	4'	Nil	Nil
4979	10'	Tr	0.4
4980	11'	Tr	0.3

Sample No	Au Int. oz	Ag oz	Tr
4981	15	Nil	Nil
4982	15	Nil	Tr
4983	15	Tr	0.4
4984	15	Nil	0.3
4985	13	Nil	0.2

LEGEND

- DIAMOND DRILL
- Overburden
 - Breccia - Qtz frags. Siliceous matrix
 - Breccia - Qtz frags. Andesite matrix
 - Qtz veins
 - Porphy Andesite Breccia - Porph matrix & frags
 - Single Andesite
 - Fault Breccia
 - Breccia - Andes & porph. Andes frags. Breccia. Non-porph. matrix.
 - Breccia - Andes & porph. Andes frags. Breccia. Non-porph. matrix.
 - Porphy Andesite
 - Fracture
 - Qtz vein
 - Shear plane
 - Dip not contact
 - Ground level contact
 - Outline of ore zone
- PERCUSSION DRILL
- Overburden
 - Breccia - Qtz frags. Siliceous matrix
 - Breccia - Qtz frags. Andesite matrix
 - Qtz veins
 - Porphy Andesite Breccia - Porph matrix & frags
 - Single Andesite
 - Fault Breccia
 - Breccia - Andes & porph. Andes frags. Breccia. Non-porph. matrix.
 - Breccia - Andes & porph. Andes frags. Breccia. Non-porph. matrix.
 - Porphy Andesite
 - Fracture
 - Qtz vein
 - Shear plane
 - Dip not contact
 - Ground level contact
 - Outline of ore zone

GRADE DEFINITION

- 2-3 oz. Ag. Equiv.
- 3-4 oz. Ag. Equiv.
- 4-5 oz. Ag. Equiv.
- 5 oz. Plus Ag. Equiv.
- Ag. at \$1.80 oz.
- Au. at \$37.50 oz.

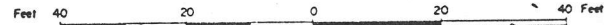
NOTE

For details of holes P4 & P6
See plan of SECTION THROUGH LINE 2
PERCUSSION HOLES.

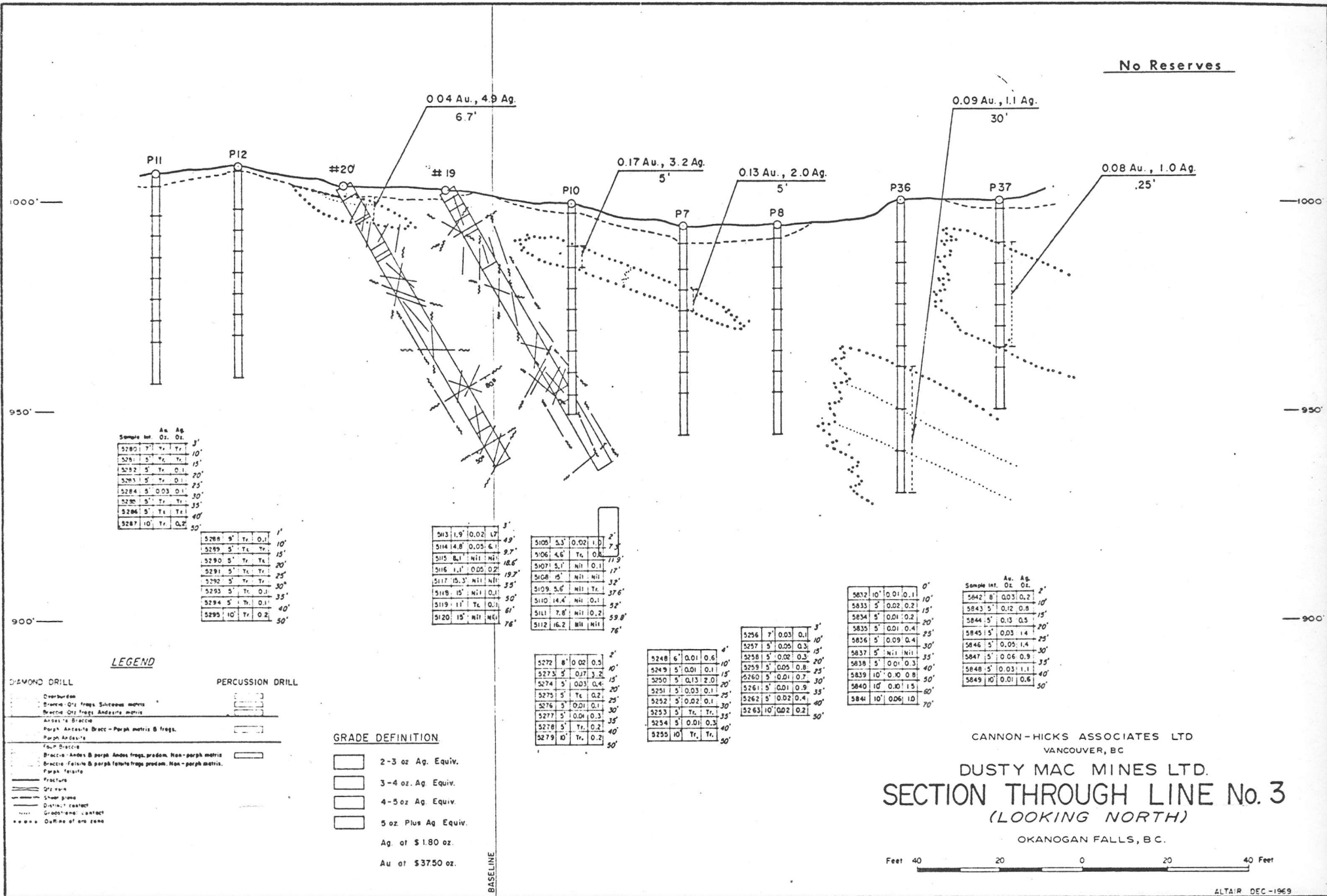
CANNON-HICKS ASSOCIATES LTD
VANCOUVER, B.C.

DUSTY MAC MINES LTD.
SECTION THROUGH LINE No.2
LOOKING NORTH

OKANOGAN FALLS, B.C.



No Reserves



LEGEND

- DIAMOND DRILL
- Overburden
 - Brucite - Qtz frags. Siliceous matrix
 - Brucite - Qtz frags. Andesite matrix
 - Andesite Brucite
 - Porph. Andesite Brucite - Porph. matrix & frags.
 - Porph. Andesite
 - Qtz Brucite
 - Brucite - Andesite & porph. Andesite frags. predom. Non-porph. matrix
 - Brucite - Felsite & porph. felsite frags. predom. Non-porph. matrix.
 - Felsite
 - Fracture
 - Qtz vein
 - Shear zone
 - Dip-slip contact
 - Graben-like contact
 - Outline of ore zone
- PERCUSSION DRILL

GRADE DEFINITION

- 2-3 oz. Ag. Equiv.
 - 3-4 oz. Ag. Equiv.
 - 4-5 oz. Ag. Equiv.
 - 5 oz. Plus Ag. Equiv.
- Ag. at \$1.80 oz.
Au. at \$3750 oz.

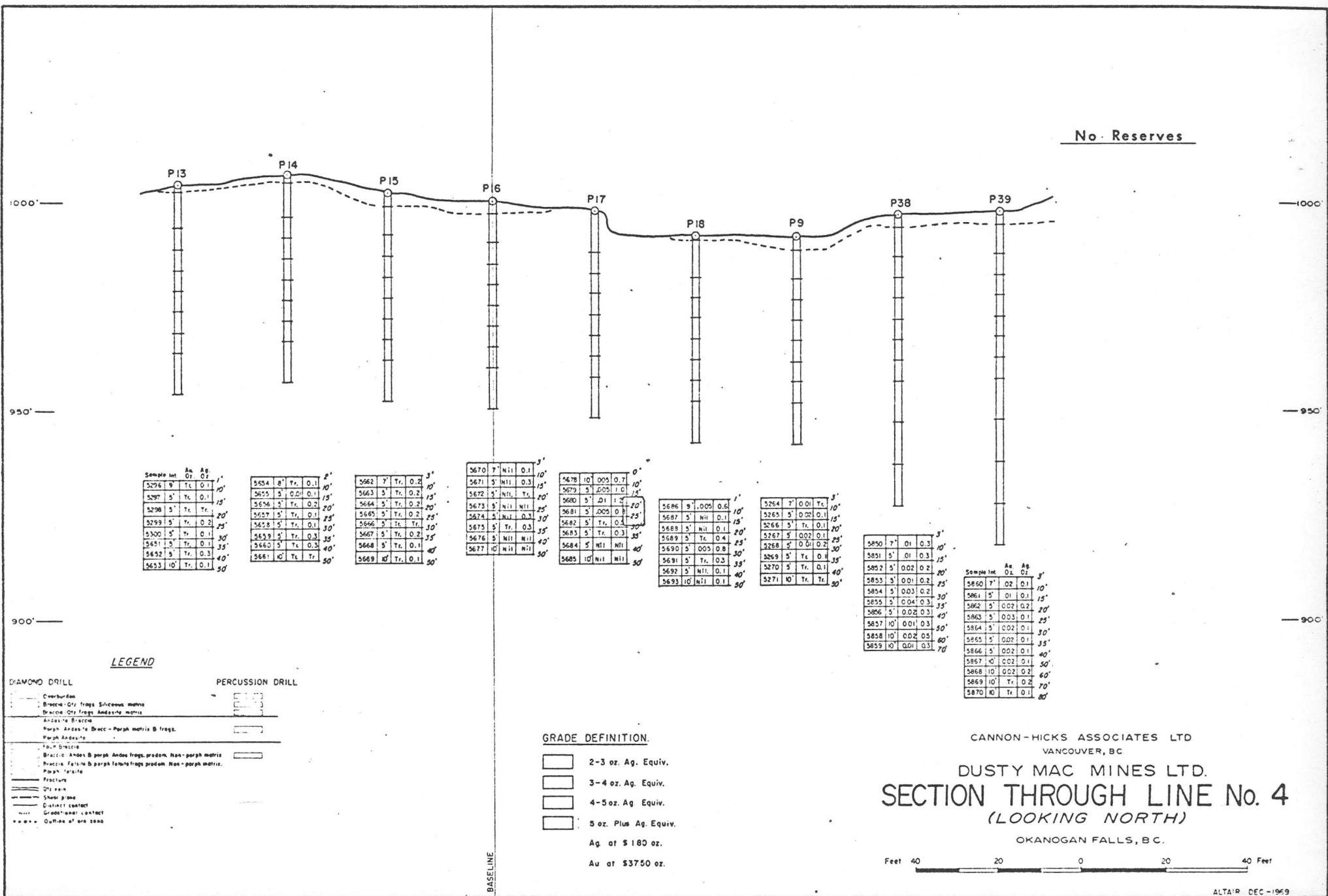
CANNON-HICKS ASSOCIATES LTD
VANCOUVER, B.C.

DUSTY MAC MINES LTD.
SECTION THROUGH LINE No. 3
(LOOKING NORTH)

OKANOGAN FALLS, B.C.

Feet 40 20 0 20 40 Feet

No. Reserves



Sample Int.	Am.	Ag.	Gr.	Eq.
5296	9'	Tr.	0.1	1'
5297	5'	Tr.	0.1	10'
5298	5'	Tr.	0.1	15'
5299	5'	Tr.	0.2	20'
5300	5'	Tr.	0.1	25'
5451	5'	Tr.	0.1	30'
5652	5'	Tr.	0.3	35'
5653	10'	Tr.	0.1	40'

5654	8'	Tr.	0.1	2'
5655	5'	Tr.	0.2	10'
5656	5'	Tr.	0.2	15'
5657	5'	Tr.	0.1	20'
5658	5'	Tr.	0.1	25'
5659	5'	Tr.	0.3	30'
5660	5'	Tr.	0.3	35'
5661	10'	Tr.	Tr.	40'

5662	7'	Tr.	0.2	5'
5663	5'	Tr.	0.2	10'
5664	5'	Tr.	0.2	15'
5665	5'	Tr.	0.2	20'
5666	5'	Tr.	Tr.	25'
5667	5'	Tr.	0.2	30'
5668	5'	Tr.	0.1	35'
5669	10'	Tr.	0.1	40'

5670	7'	Nil	0.1	5'
5671	5'	Nil	0.3	10'
5672	5'	Nil	Tr.	15'
5673	5'	Nil	Nil	20'
5674	5'	Nil	0.3	25'
5675	5'	Tr.	0.3	30'
5676	5'	Nil	Nil	35'
5677	10'	Nil	Nil	40'

5678	10'	0.05	0.7	10'
5679	5'	0.05	1.0	15'
5680	5'	0.1	1.2	20'
5681	5'	0.05	0.8	25'
5682	5'	Tr.	0.3	30'
5683	5'	Tr.	0.3	35'
5684	5'	Nil	Nil	40'
5685	10'	Nil	Nil	50'

5686	9'	0.05	0.6	10'
5687	5'	Nil	0.1	15'
5688	5'	Nil	0.1	20'
5689	5'	Tr.	0.4	25'
5690	5'	0.05	0.8	30'
5691	5'	Tr.	0.2	35'
5692	5'	Nil	0.1	40'
5693	10'	Nil	0.1	50'

5264	7'	0.01	Tr.	5'
5265	5'	0.02	0.1	10'
5266	5'	Tr.	0.1	15'
5267	5'	0.02	0.1	20'
5268	5'	0.01	0.2	25'
5269	5'	Tr.	0.1	30'
5270	5'	Tr.	0.1	35'
5271	10'	Tr.	Tr.	40'

5850	7'	0.1	0.3	5'
5851	5'	0.1	0.3	10'
5852	5'	0.02	0.2	15'
5853	5'	0.01	0.2	20'
5854	5'	0.03	0.2	25'
5855	5'	0.04	0.3	30'
5856	5'	0.02	0.3	35'
5857	10'	0.01	0.3	40'
5858	10'	0.02	0.5	45'
5859	10'	0.01	0.3	50'

Sample Int.	Am.	Ag.	Gr.	Eq.
5860	7'	0.2	0.1	5'
5861	5'	0.1	0.1	10'
5862	5'	0.02	0.2	15'
5863	5'	0.03	0.1	20'
5864	5'	0.02	0.1	25'
5865	5'	0.02	0.1	30'
5866	5'	0.02	0.1	35'
5867	10'	0.02	0.1	40'
5868	10'	0.02	0.2	45'
5869	10'	Tr.	0.2	50'
5870	10'	Tr.	0.1	55'

LEGEND

- DIAMOND DRILL**
- Overburden
 - Breccia - Or. frags. Siliceous matrix
 - Breccia - Or. frags. Andesitic matrix
 - Andesitic Breccia
 - Porph. Andesite Brecc. - Porph. matrix B frags.
 - Porph. Andesite
 - Porph. Breccia
 - Breccia - Andes. B porph. Andes. frags. predom. Non-porph. matrix
 - Breccia - Andes. B porph. Andes. frags. predom. Non-porph. matrix.
 - Porph. Breccia
- PERCUSSION DRILL**
- Fracture
 - Or. vein
 - Shear zone
 - Disconformity contact
 - Grade/level contact
 - Outline of ore mass

GRADE DEFINITION.

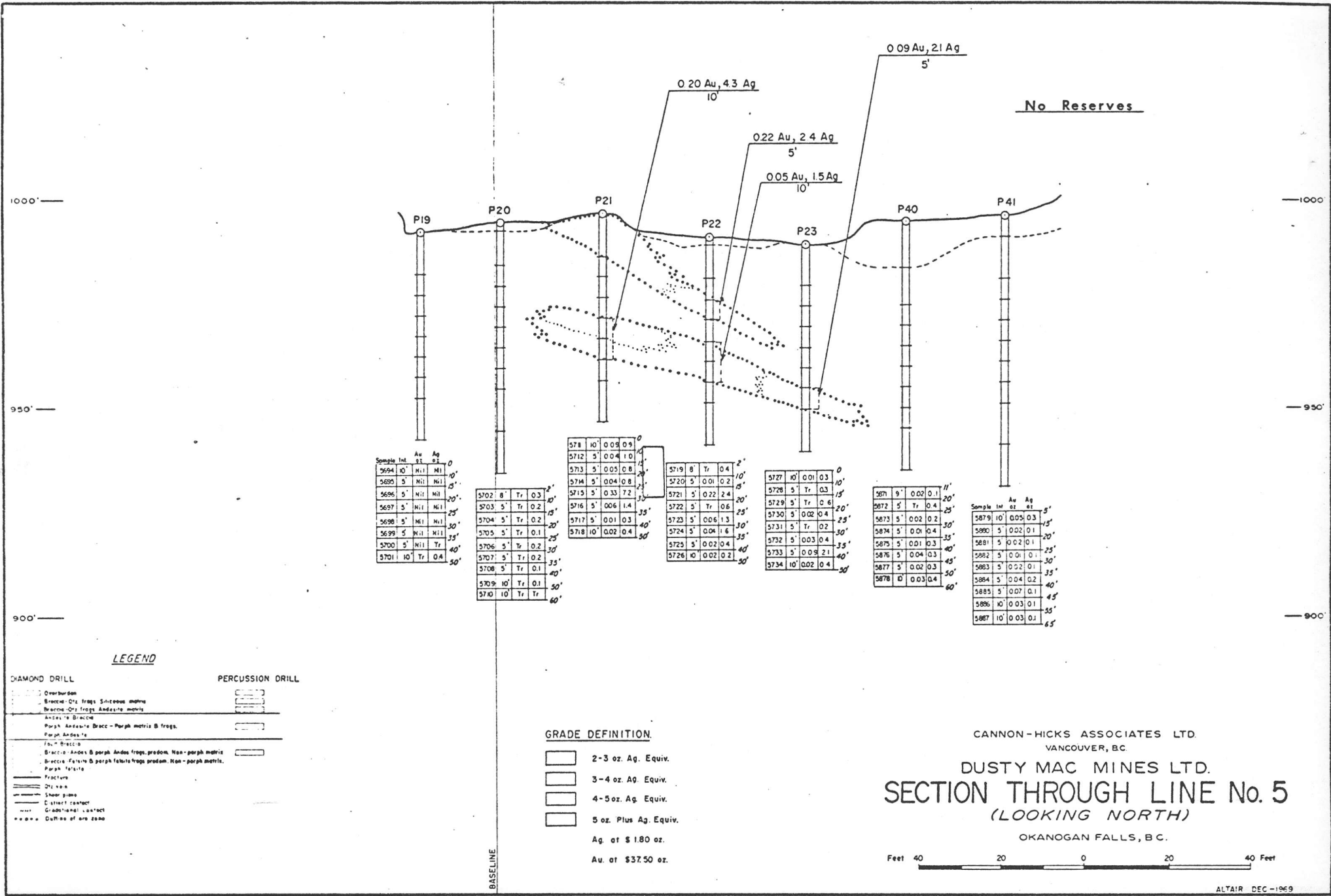
- 2-3 oz. Ag. Equiv.
 - 3-4 oz. Ag. Equiv.
 - 4-5 oz. Ag. Equiv.
 - 5 oz. Plus Ag. Equiv.
- Ag. of \$180 oz.
Au. at \$3750 oz.

CANNON-HICKS ASSOCIATES LTD
VANCOUVER, BC

DUSTY MAC MINES LTD.
SECTION THROUGH LINE No. 4
(LOOKING NORTH)

OKANOGAN FALLS, BC.

Feet 40 20 0 20 40 Feet



No Reserves

0.09 Au, 2.1 Ag
5'

0.20 Au, 4.3 Ag
10'

0.22 Au, 2.4 Ag
5'

0.05 Au, 1.5 Ag
10'

Sample Int.	Au	Ag	0
	oz	oz	
5694	10'	Nil	Nil
5695	5'	Nil	Nil
5696	5'	Nil	Nil
5697	5'	Nil	Nil
5698	5'	Nil	Nil
5699	5'	Nil	Tr
5700	5'	Nil	Tr
5701	10'	Tr	0.4

Sample Int.	Tr	0.3	0.1	0.2	0.1	0.2	0.1	0.2	0.1	0.2	0.1	0.2	0.1	0.2	0.1
5702	8'	Tr	0.3	10'											
5703	5'	Tr	0.2	15'											
5704	5'	Tr	0.2	20'											
5705	5'	Tr	0.1	25'											
5706	5'	Tr	0.2	30'											
5707	5'	Tr	0.2	35'											
5708	5'	Tr	0.1	40'											
5709	10'	Tr	0.1	50'											
5710	10'	Tr	Tr	60'											

Sample Int.	Au	Ag	0
	oz	oz	
5711	10'	0.09	0.9
5712	5'	0.04	1.0
5713	5'	0.05	0.8
5714	5'	0.04	1.0
5715	5'	0.33	7.2
5716	5'	0.06	1.4
5717	5'	0.01	0.3
5718	10'	0.02	0.4

Sample Int.	Tr	0.4	0.2	0.2	0.6	1.3	1.6	0.4	0.2
5719	8'	Tr	0.4	2'					
5720	5'	0.01	0.2	10'					
5721	5'	Tr	0.6	20'					
5722	5'	Tr	0.6	25'					
5723	5'	0.06	1.3	30'					
5724	5'	0.04	1.6	35'					
5725	5'	0.02	0.4	40'					
5726	10'	0.02	0.2	50'					

Sample Int.	Au	Ag	0
	oz	oz	
5727	10'	0.01	0.3
5728	5'	Tr	0.3
5729	5'	Tr	0.6
5730	5'	0.02	0.4
5731	5'	Tr	0.2
5732	5'	0.03	0.4
5733	5'	0.09	2.1
5734	10'	0.02	0.4

Sample Int.	Au	Ag	0
	oz	oz	
5871	9'	0.02	0.1
5872	5'	Tr	0.4
5873	5'	0.02	0.2
5874	5'	0.01	0.4
5875	5'	0.01	0.3
5876	5'	0.04	0.3
5877	5'	0.02	0.3
5878	10'	0.03	0.4

Sample Int.	Au	Ag	0
	oz	oz	
5879	10'	0.03	0.3
5880	5'	0.02	0.1
5881	5'	0.02	0.1
5882	5'	0.01	0.1
5883	5'	0.02	0.1
5884	5'	0.04	0.2
5885	5'	0.07	0.1
5886	10'	0.03	0.1
5887	10'	0.03	0.1

LEGEND

- DIAMOND DRILL**
- Overburden
 - Bracco - Qtz frags Siliceous matrix
 - Bracco - Qtz frags Andesite matrix
 - Andesite Bracco
 - Porph. Andesite Bracc - Porph matrix B frags.
 - Porph. Andesite
 - Foam Bracco
 - Bracco - Andes B porph. Andes frags. predom. Non-porph matrix
 - Bracco - Felsite B porph. felsite frags. predom. Non-porph matrix.
 - Porph. felsite
 - Fracture
 - Qtz vein
 - Shear plane
 - Contact contact
 - Graben contact
 - Duffins of ore zone
- PERCUSSION DRILL**

GRADE DEFINITION.

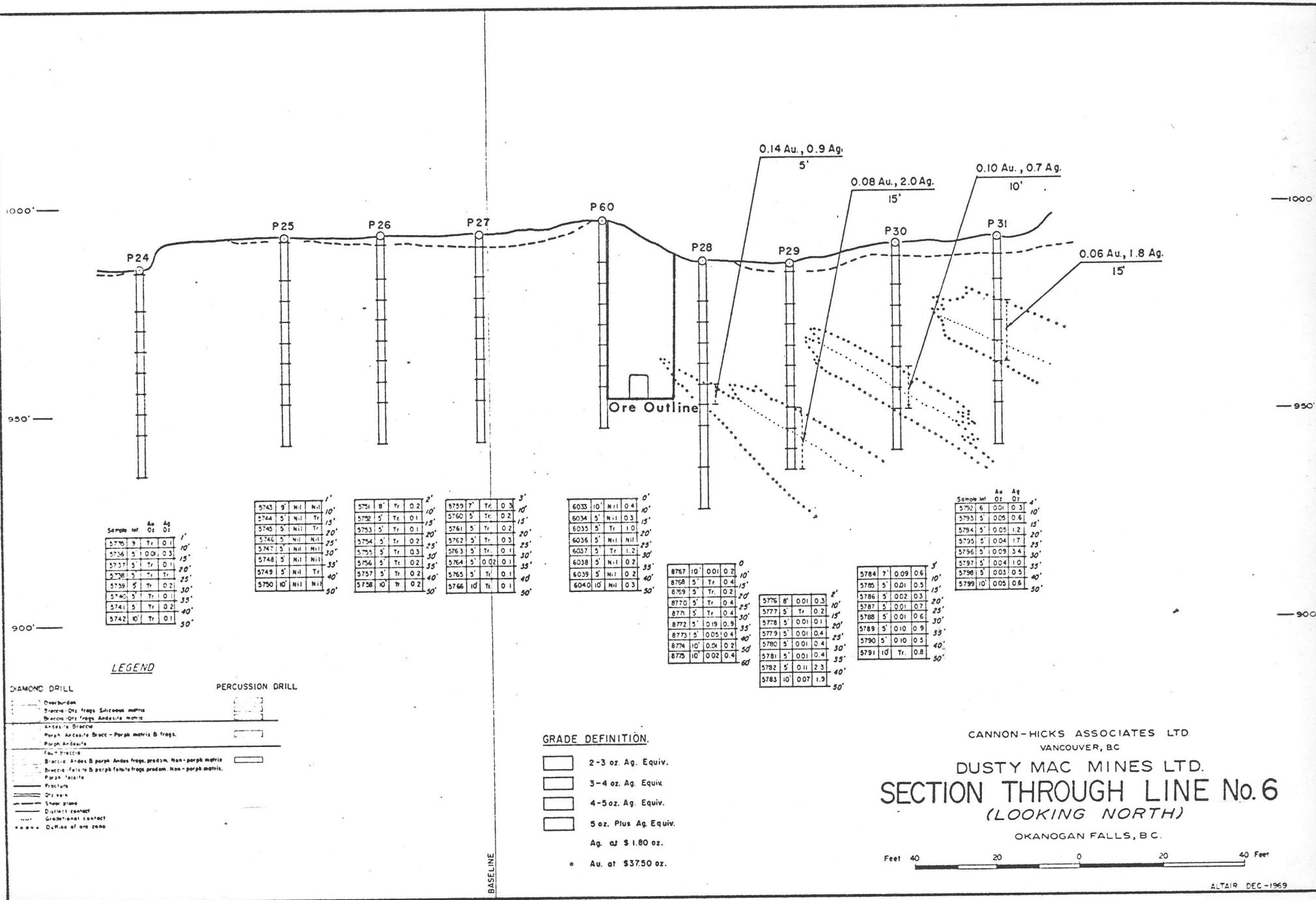
- 2-3 oz. Ag. Equiv.
 - 3-4 oz. Ag. Equiv.
 - 4-5 oz. Ag. Equiv.
 - 5 oz. Plus Ag. Equiv.
- Ag. at \$ 1.80 oz.
Au. at \$37.50 oz.

CANNON-HICKS ASSOCIATES LTD
VANCOUVER, B.C.

DUSTY MAC MINES LTD.
SECTION THROUGH LINE No. 5
(LOOKING NORTH)

OKANOGAN FALLS, B.C.

Feet 40 20 0 20 40



1000'
950'
900'

1000'
950'
900'

BASELINE

Sample No.	Au	Ag	Depth
5770	9	Tr	0.1
5776	5	0.01	0.3
5737	5	Tr	0.1
5738	5	Tr	0.1
5739	5	Tr	0.2
5740	5	Tr	0.1
5741	5	Tr	0.2
5742	10	Tr	0.1

Sample No.	Au	Ag	Depth
5743	5	Nil	Nil
5744	5	Nil	Tr
5745	5	Nil	Tr
5746	5	Nil	Nil
5747	5	Nil	Nil
5748	5	Nil	Nil
5749	5	Nil	Tr
5750	10	Nil	Nil

Sample No.	Au	Ag	Depth
5751	8	Tr	0.2
5752	5	Tr	0.1
5753	5	Tr	0.1
5754	5	Tr	0.2
5755	5	Tr	0.3
5756	5	Tr	0.2
5757	5	Tr	0.2
5758	10	Tr	0.2

Sample No.	Au	Ag	Depth
5759	7	Tr	0.3
5760	5	Tr	0.2
5761	5	Tr	0.2
5762	5	Tr	0.3
5763	5	Tr	0.1
5764	5	0.02	0.1
5765	5	Tr	0.1
5766	10	Tr	0.1

Sample No.	Au	Ag	Depth
6035	10	Nil	0.4
6034	5	Nil	0.3
6035	5	Tr	1.0
6036	5	Nil	Nil
6037	5	Tr	1.2
6038	5	Nil	0.2
6039	5	Nil	0.2
6040	10	Nil	0.3

Sample No.	Au	Ag	Depth
8767	10	0.01	0.2
8768	5	Tr	0.4
8769	5	Tr	0.2
8770	5	Tr	0.4
8771	5	Tr	0.4
8772	5	0.19	0.3
8773	5	0.05	0.4
8774	10	0.06	0.2
8775	10	0.02	0.4

Sample No.	Au	Ag	Depth
5776	8	0.01	0.3
5777	5	Tr	0.2
5778	5	0.01	0.1
5779	5	0.01	0.4
5780	5	0.01	0.4
5781	5	0.01	0.4
5782	5	0.11	2.3
5783	10	0.07	1.9

Sample No.	Au	Ag	Depth
5784	7	0.09	0.6
5785	5	0.01	0.3
5786	5	0.02	0.3
5787	5	0.01	0.7
5788	5	0.01	0.6
5789	5	0.10	0.9
5790	5	0.10	0.3
5791	10	Tr	0.8

Sample No.	Au	Ag	Depth
5792	6	0.01	0.3
5793	5	0.05	0.6
5794	5	0.05	1.2
5795	5	0.04	1.7
5796	5	0.09	3.4
5797	5	0.04	1.0
5798	5	0.03	0.5
5799	10	0.05	0.6

LEGEND

- DIAMOND DRILL**
- Overburden
 - Diabase - Ort frags. Siliceous matrix
 - Diabase - Ort frags. Andesitic matrix
 - Andesite - Diabase
 - Porph. Andesite Brecc - Porph matrix & frags.
 - Porph. Andesite
 - Fels. Breccia
 - Basaltic Andes & porph. Andes frags. predom. Non-porph matrix
 - Basaltic - Felsite & porph. Felsite frags. predom. Non-porph matrix.
 - Porph. Talcite
 - Fracture
 - Ort vein
 - Shear plane
 - Disjunct contact
 - Grabenland contact
 - Outline of ore zone
- PERCUSSION DRILL**
- Overburden
 - Diabase - Ort frags. Siliceous matrix
 - Diabase - Ort frags. Andesitic matrix
 - Andesite - Diabase
 - Porph. Andesite Brecc - Porph matrix & frags.
 - Porph. Andesite
 - Fels. Breccia
 - Basaltic Andes & porph. Andes frags. predom. Non-porph matrix
 - Basaltic - Felsite & porph. Felsite frags. predom. Non-porph matrix.
 - Porph. Talcite
 - Fracture
 - Ort vein
 - Shear plane
 - Disjunct contact
 - Grabenland contact
 - Outline of ore zone

GRADE DEFINITION.

- 2-3 oz. Ag. Equiv.
- 3-4 oz. Ag. Equiv.
- 4-5 oz. Ag. Equiv.
- 5 oz. Plus Ag. Equiv.
- Ag. at \$1.80 oz.
- Au. at \$37.50 oz.

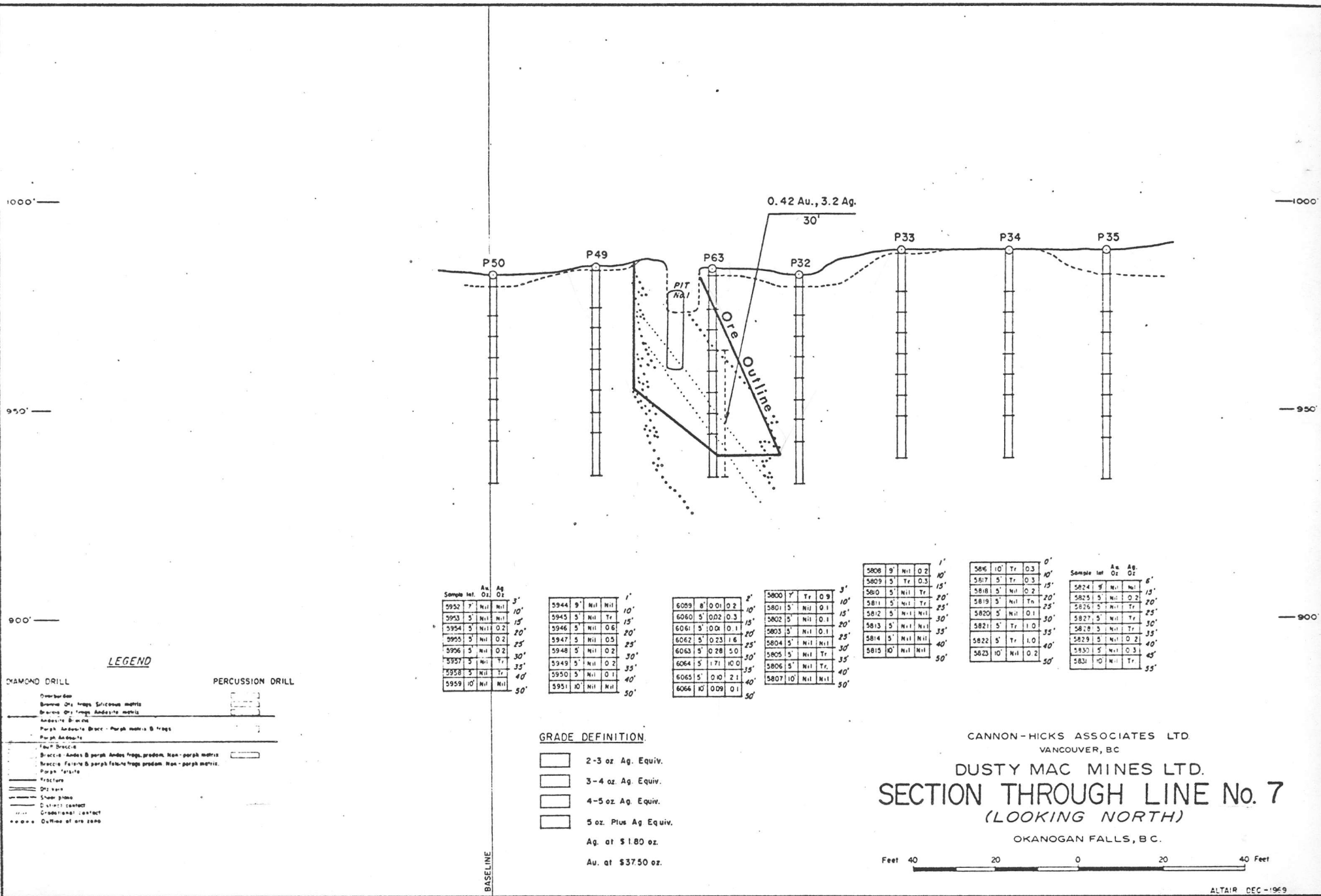
CANNON-HICKS ASSOCIATES LTD
VANCOUVER, BC

DUSTY MAC MINES LTD.
SECTION THROUGH LINE No. 6
(LOOKING NORTH)

OKANOGAN FALLS, B.C.

Feet 40 20 0 20 40 Feet

ALTAR DEC-1969



1000'

1000'

950'

950'

900'

900'

0.42 Au., 3.2 Ag.

30'

P50

P49

P63

P32

P33

P34

P35

PIT No. 1

Ore Outline

Sample Int.	Au Oz	Ag Oz	
5952	7	Nil	5'
5953	5	Nil	10'
5954	5	Nil	15'
5955	5	Nil	20'
5956	5	Nil	25'
5957	5	Nil	30'
5958	5	Nil	35'
5959	10	Nil	40'
			50'

5944	9'	Nil	Nil	10'
5945	5'	Nil	Tr	15'
5946	5'	Nil	0.6	20'
5947	5'	Nil	0.5	25'
5948	5'	Nil	0.2	30'
5949	5'	Nil	0.2	35'
5950	5'	Nil	0.1	40'
5951	10'	Nil	Nil	50'

6059	8'	0.01	0.2	2'
6060	5'	0.02	0.3	10'
6061	5'	0.04	0.1	15'
6062	5'	0.23	1.6	20'
6063	5'	0.28	5.0	25'
6064	5'	1.71	10.0	30'
6065	5'	0.10	2.1	35'
6066	10'	0.09	0.1	50'

5800	7'	Tr	0.9	5'
5801	5'	Nil	0.1	10'
5802	5'	Nil	0.1	15'
5803	5'	Nil	0.1	20'
5804	5'	Nil	Nil	25'
5805	5'	Nil	Tr	30'
5806	5'	Nil	Tr	35'
5807	10'	Nil	Nil	40'
				50'

5808	9'	Nil	0.2	1'
5809	5'	Tr	0.5	10'
5810	5'	Nil	Tr	15'
5811	5'	Nil	Tr	20'
5812	5'	Nil	Nil	25'
5813	5'	Nil	Nil	30'
5814	5'	Nil	Nil	35'
5815	10'	Nil	Nil	40'
				50'

5816	10'	Tr	0.3	0'
5817	5'	Tr	0.3	10'
5818	5'	Nil	0.2	15'
5819	5'	Nil	Tr	20'
5820	5'	Nil	Tr	25'
5821	5'	Tr	1.0	30'
5822	5'	Tr	1.0	35'
5823	10'	Nil	0.2	40'
				50'

Sample Int.	Au Oz	Ag Oz		
5824	9'	Nil	Nil	6'
5825	5'	Nil	0.2	15'
5826	5'	Nil	Tr	20'
5827	5'	Nil	Tr	25'
5828	5'	Nil	Tr	30'
5829	5'	Nil	0.2	35'
5830	5'	Nil	0.3	40'
5831	10'	Nil	Tr	45'
				55'

LEGEND

- DIAMOND DRILL**
- Overburden
 - Granite Qtz frags. Siliceous matrix
 - Granite Qtz frags. Andesite matrix
 - Andesite Breccia
 - Porph. Andesite Brecc. - Porph. matrix & frags
 - Porph. Andesite
 - Tuff Breccia
 - Basaltic Andes. B. porph. Andes. frags. gradom. Non-porph. matrix
 - Basaltic Felsite B. porph. felsite frags. gradom. Non-porph. matrix.
 - Porph. felsite
 - Fracture
 - Drill hole
 - Swamp plain
 - Disjunct contact
 - Gradational contact
 - Duffing of ore zone
- PERCUSSION DRILL**

GRADE DEFINITION:

- 2-3 oz. Ag. Equiv.
 - 3-4 oz. Ag. Equiv.
 - 4-5 oz. Ag. Equiv.
 - 5 oz. Plus Ag. Equiv.
- Ag. at \$1.80 oz.
Au. at \$37.50 oz.

CANNON-HICKS ASSOCIATES LTD
VANCOUVER, BC

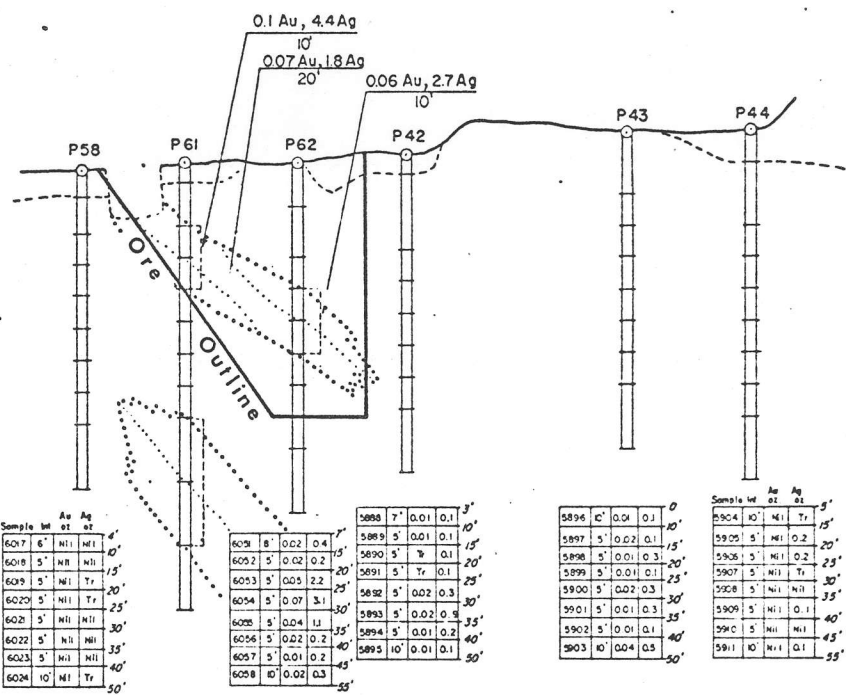
DUSTY MAC MINES LTD.
SECTION THROUGH LINE No. 7
(LOOKING NORTH)

OKANOGAN FALLS, B.C.

Feet 40 20 0 20 40

1000'
950'
900'

1000'
950'
900'



LEGEND

- DIAMOND DRILL**
- Overburden
 - Bracc - Qtz frags Siliceous matrix
 - Bracc - Qtz frags Andesite matrix
 - Andesite Bracc
 - Porph Andesite Bracc - Porph matrix B frags.
 - Porph Andesite
 - Flow Bracc
 - Bracc Andes B porph Andes frags. produm. Non-porph matrix
 - Bracc Facies B porph felsite frags produm. Non-porph matrix.
 - Porph felsite
 - Fracture
 - Qtz vein
 - Shear plane
 - Contact contact
 - Grade/trace contact
 - Outline of ore zone
- PERCUSSION DRILL**

GRADE DEFINITION.

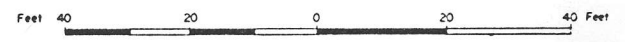
- 2-3 oz Ag Equiv.
 - 3-4 oz Ag. Equiv.
 - 4-5oz Ag. Equiv.
 - 5 oz. Plus Ag. Equiv.
- Ag. at \$1.80 oz.
Au. at \$37.50 oz.

Sample	wt	Au	Ag	oz	oz
6041	7'	Nil	0.5		
6042	5'	0.08	3.4		
6043	5'	0.12	5.4		
6044	5'	Nil	Nil		
6045	5'	Nil	Nil		
6046	5'	Nil	Nil		
6047	5'	Nil	Tr		
6048	10'	0.06	1.4		
6049	10'	0.08	2.2		
6050	10'	Tr	0.2		

CANNON-HICKS ASSOCIATES LTD
VANCOUVER, BC

DUSTY MAC MINES LTD.
SECTION THROUGH LINE No. 8
(LOOKING NORTH)

OKANOGAN FALLS, B.C.



1000'

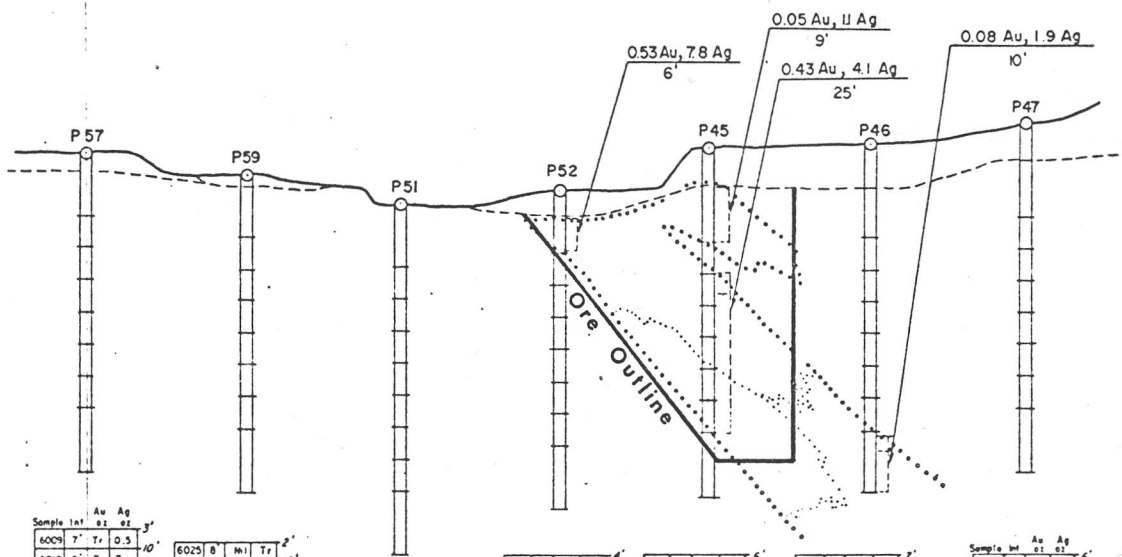
1000'

950'

950'

900'

900'



Sample Int'	Au oz	Ag oz	Interval
6009	7	0.3	10'
6010	5	Tr	15'
6011	5	Tr	20'
6012	5	Tr	25'
6013	5	Tr	30'
6014	5	Tr	35'
6015	5	Tr	40'
6016	10	Tr	50'

Sample Int'	Mt	Tr	Interval
6025	8	Nil	10'
6026	5	Nil	15'
6027	5	Nil	20'
6028	5	Nil	25'
6029	5	Nil	30'
6030	5	Nil	35'
6031	5	Nil	40'
6032	10	Nil	50'

Sample Int'	Au oz	Ag oz	Interval
5960	9	0.02	10'
5961	5	Tr	15'
5962	5	Tr	20'
5963	5	0.05	25'
5964	5	0.02	30'
5965	5	Tr	35'
5966	5	Tr	40'
5967	5	Tr	45'
5968	10	Tr	55'

Sample Int'	Au oz	Ag oz	Interval
5969	8	0.53	10'
5970	5	0.02	15'
5971	5	0.01	20'
5972	5	0.01	25'
5973	5	0.06	30'
5974	5	Tr	35'
5975	5	Tr	40'
5976	10	0.05	55'

Sample Int'	Au oz	Ag oz	Interval
5977	9	0.05	10'
5978	5	0.01	15'
5979	5	1.48	20'
5980	5	0.14	25'
5981	5	0.40	30'
5982	5	0.14	35'
5983	5	0.09	40'
5984	5	0.06	45'
5985	10	0.05	55'

Sample Int'	Au oz	Ag oz	Interval
5986	8	0.03	10'
5987	5	Tr	15'
5988	5	0.05	20'
5989	5	0.07	25'
5990	5	Tr	30'
5991	5	0.01	35'
5992	5	0.01	40'
5993	5	0.03	45'
5994	10	0.08	55'

Sample Int'	Au oz	Ag oz	Interval
5995	9	0.03	10'
5996	5	0.01	15'
5997	5	0.01	20'
5998	5	0.01	25'
5999	5	Tr	30'
6000	5	Tr	35'
6001	5	Tr	40'
6002	10	Tr	55'

LEGEND

- DIAMOND DRILL**
- Overburden
 - Breccia - Qtz frags. Siliceous matrix
 - Breccia - Qtz frags. Andalusite matrix
 - Andalusite Breccia
 - Porph. Andalusite Breccia - Porph matrix B frags.
 - Porph. Andalusite
 - Fault Breccia
 - Breccia - Andes. B porph. Andes. frags. predom. Non-porph matrix
 - Breccia - Felsite B porph. Felsite frags. predom. Non-porph matrix.
 - Fracture
 - Qtz vein
 - Shale zone
 - Dip-slip contact
 - Graben-slip contact
 - Outline of ore zone
- PERCUSSION DRILL**

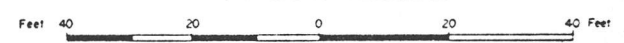
GRADE DEFINITION.

- 2-3 oz. Ag. Equiv.
 - 3-4 oz. Ag. Equiv
 - 4-5oz. Ag. Equiv
 - 5oz. Plus Ag. Equiv.
- Ag. at \$1.80 oz.
Au. at \$37.50 oz.

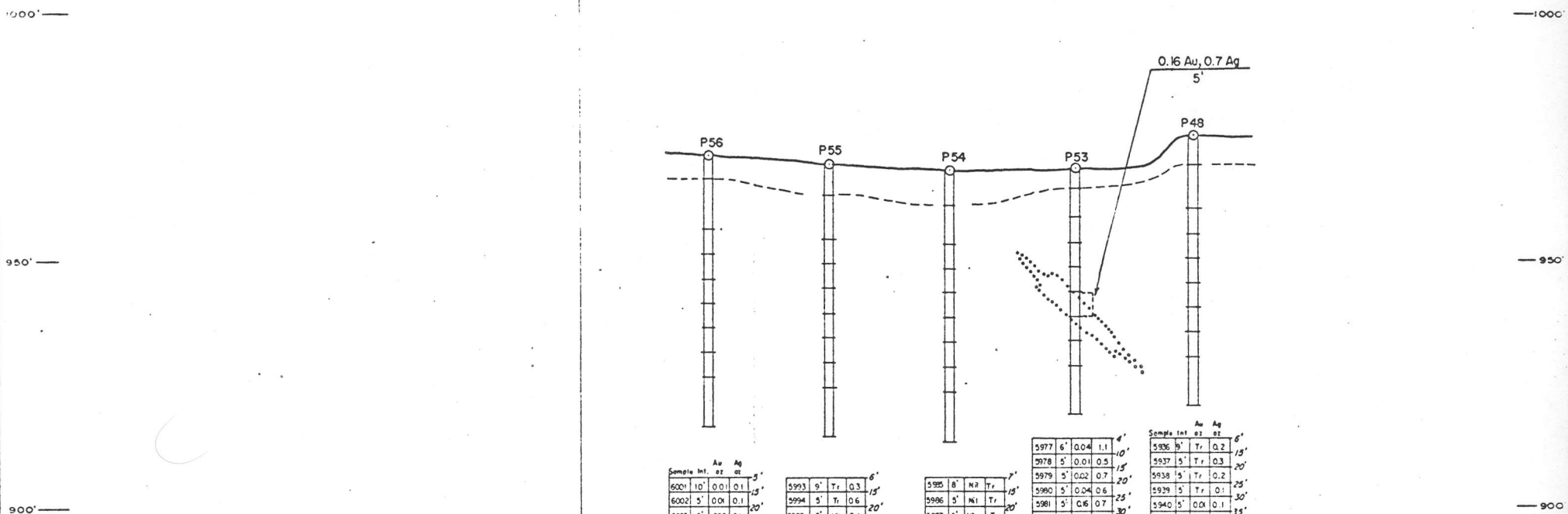
CANNON-HICKS ASSOCIATES LTD VANCOUVER, BC

DUSTY MAC MINES LTD. SECTION THROUGH LINE No. 9 (LOOKING NORTH)

OKANOGAN FALLS, B.C.



No Reserves



LEGEND

DIAMOND DRILL		PERCUSSION DRILL	
Overburden	[Symbol]	[Symbol]	[Symbol]
Braccie - Qtz frags. Siliceous matrix	[Symbol]	[Symbol]	[Symbol]
Braccie - Qtz frags. Andesitic matrix	[Symbol]	[Symbol]	[Symbol]
Accessory Braccie	[Symbol]	[Symbol]	[Symbol]
Porph. Andesite Braccie - Porph matrix & frags.	[Symbol]	[Symbol]	[Symbol]
Porph. Andesite	[Symbol]	[Symbol]	[Symbol]
Flow Braccie	[Symbol]	[Symbol]	[Symbol]
Braccie - Andes & porph. Andes frags. prodom. Non-porph matrix	[Symbol]	[Symbol]	[Symbol]
Braccie - felsite & porph. felsite frags. prodom. Non-porph matrix	[Symbol]	[Symbol]	[Symbol]
Porph. felsite	[Symbol]	[Symbol]	[Symbol]
Fracture	[Symbol]	[Symbol]	[Symbol]
Qtz vein	[Symbol]	[Symbol]	[Symbol]
Shale zone	[Symbol]	[Symbol]	[Symbol]
Distinct contact	[Symbol]	[Symbol]	[Symbol]
Unobscured contact	[Symbol]	[Symbol]	[Symbol]
Colline of ore zone	[Symbol]	[Symbol]	[Symbol]

Sample	Int.	Au	Ag	
		oz	oz	
6001	10'	0.0	0.1	5'
6002	5'	0.0	0.1	15'
6003	5'	0.05	0.1	20'
6004	5'	0.01	0.1	25'
6005	5'	Tr.	0.1	30'
6006	5'	Tr.	0.2	35'
6007	5'	Tr.	0.2	40'
6008	10'	Tr.	0.1	45'

Sample	Int.	Au	Ag	
		oz	oz	
5993	9'	Tr.	0.3	6'
5994	5'	Tr.	0.6	15'
5995	5'	Ni	0.1	20'
5996	5'	Ni	0.3	25'
5997	5'	Ni	Ni	30'
5998	5'	Ni	Tr.	35'
5999	5'	Tr.	0.3	40'
6000	10'	Ni	0.1	45'

Sample	Int.	Au	Ag	
		oz	oz	
5985	8'	Ni	Tr.	7'
5986	5'	Ni	Tr.	15'
5987	5'	Ni	Tr.	20'
5988	5'	Ni	0.1	25'
5989	5'	Ni	0.1	30'
5990	5'	Ni	0.1	35'
5991	5'	Ni	Ni	40'
5992	10'	Ni	Ni	45'

Sample	Int.	Au	Ag	
		oz	oz	
5977	6'	0.04	1.1	4'
5978	5'	0.01	0.5	10'
5979	5'	0.02	0.7	15'
5980	5'	0.04	0.6	20'
5981	5'	0.6	0.7	25'
5982	5'	0.02	0.1	30'
5983	5'	0.02	0.1	35'
5984	10'	0.02	0.2	40'
				50'

Sample	Int.	Au	Ag	
		oz	oz	
5936	5'	Tr.	0.2	6'
5937	5'	Tr.	0.3	15'
5938	5'	Tr.	0.2	20'
5939	5'	Tr.	0.1	25'
5940	5'	0.0	0.1	30'
5941	5'	Tr.	0.2	35'
5942	5'	Tr.	0.6	40'
5943	10'	Tr.	0.5	45'
				55'

GRADE DEFINITION.

- [Symbol] 2-3 oz. Ag. Equiv.
 - [Symbol] 3-4 oz. Ag. Equiv.
 - [Symbol] 4-5 oz. Ag. Equiv.
 - [Symbol] 5 oz. Plus Ag. Equiv.
- Ag. at \$120.00.
Au. at \$375.00.

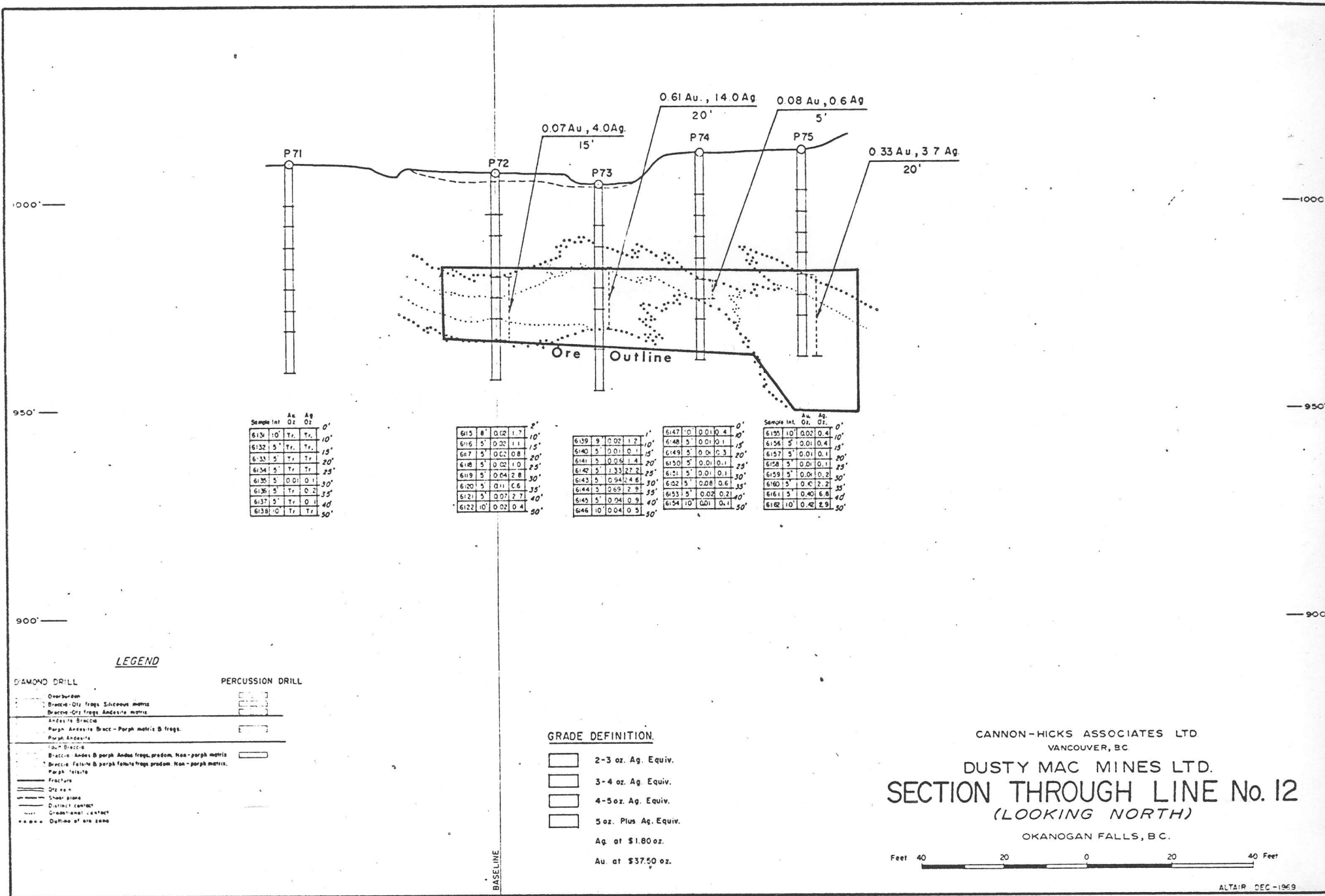
CANNON-HICKS ASSOCIATES LTD
VANCOUVER, BC

DUSTY MAC MINES LTD.

SECTION THROUGH LINE No. 10
(LOOKING NORTH)

OKANOGAN FALLS, B.C.

Feet 40 20 0 20 40



Sample Int.	Au Oz.	Ag Oz.	
613x 10	Tr.	Tr.	0'
6132 5'	Tr.	Tr.	10'
6133 5'	Tr.	Tr.	15'
6134 5'	Tr.	Tr.	25'
6135 5'	0.01	0.1	30'
6136 5'	Tr.	0.2	35'
6137 5'	Tr.	0.1	40'
6138 10'	Tr.	Tr.	50'

615 8'	0.02	1.7	10'
616 5'	0.02	1.1	15'
617 5'	0.02	0.8	20'
618 5'	0.02	1.0	25'
619 5'	0.04	2.8	30'
620 5'	0.11	2.6	35'
621 5'	0.07	2.7	40'
622 10'	0.02	0.4	50'

6139 9'	0.02	1.2	10'
6140 5'	0.01	0.1	15'
6141 5'	0.04	1.4	20'
6142 5'	1.33	27.2	25'
6143 5'	0.94	4.6	30'
6144 5'	2.69	2.9	35'
6145 5'	0.04	0.9	40'
6146 10'	0.04	0.5	50'

6147 10'	0.01	0.4	0'
6148 5'	0.01	0.1	10'
6149 5'	0.06	0.3	15'
6150 5'	0.01	0.1	20'
6151 5'	0.01	0.1	25'
6152 5'	0.08	0.6	30'
6153 5'	0.02	0.2	35'
6154 10'	0.01	0.1	50'

Sample Int.	Au Oz.	Ag Oz.	
6155 10'	0.02	0.4	0'
6156 5'	0.01	0.4	10'
6157 5'	0.01	0.1	15'
6158 5'	0.06	0.1	20'
6159 5'	0.06	0.2	25'
6160 5'	0.02	0.2	30'
6161 5'	0.40	6.8	40'
6162 10'	0.02	2.9	50'

LEGEND

- DIAMOND DRILL**
- Overburden
 - Bracco-Oz frags. Siliceous matrix
 - Bracco-Oz frags. Andesite matrix
 - Andesite Bracco
 - Porph. Andesite Bracc - Porph. matrix B frags.
 - Porph. Andesite
 - Tr. = Bracc B
 - Bracco Andes B porph. Andes. frags. predom. Non-porph. matrix
 - Bracco. Felsite B porph. felsite frags. predom. Non-porph. matrix.
 - Porph. felsite
 - Fracture
 - Qz ss
 - Sharp plane
 - Distinct contact
 - Gradational contact
 - Outline of ore zone
- PERCUSSION DRILL**
- 2-3 oz. Ag. Equiv.
 - 3-4 oz. Ag. Equiv.
 - 4-5 oz. Ag. Equiv.
 - 5 oz. Plus Ag. Equiv.

GRADE DEFINITION

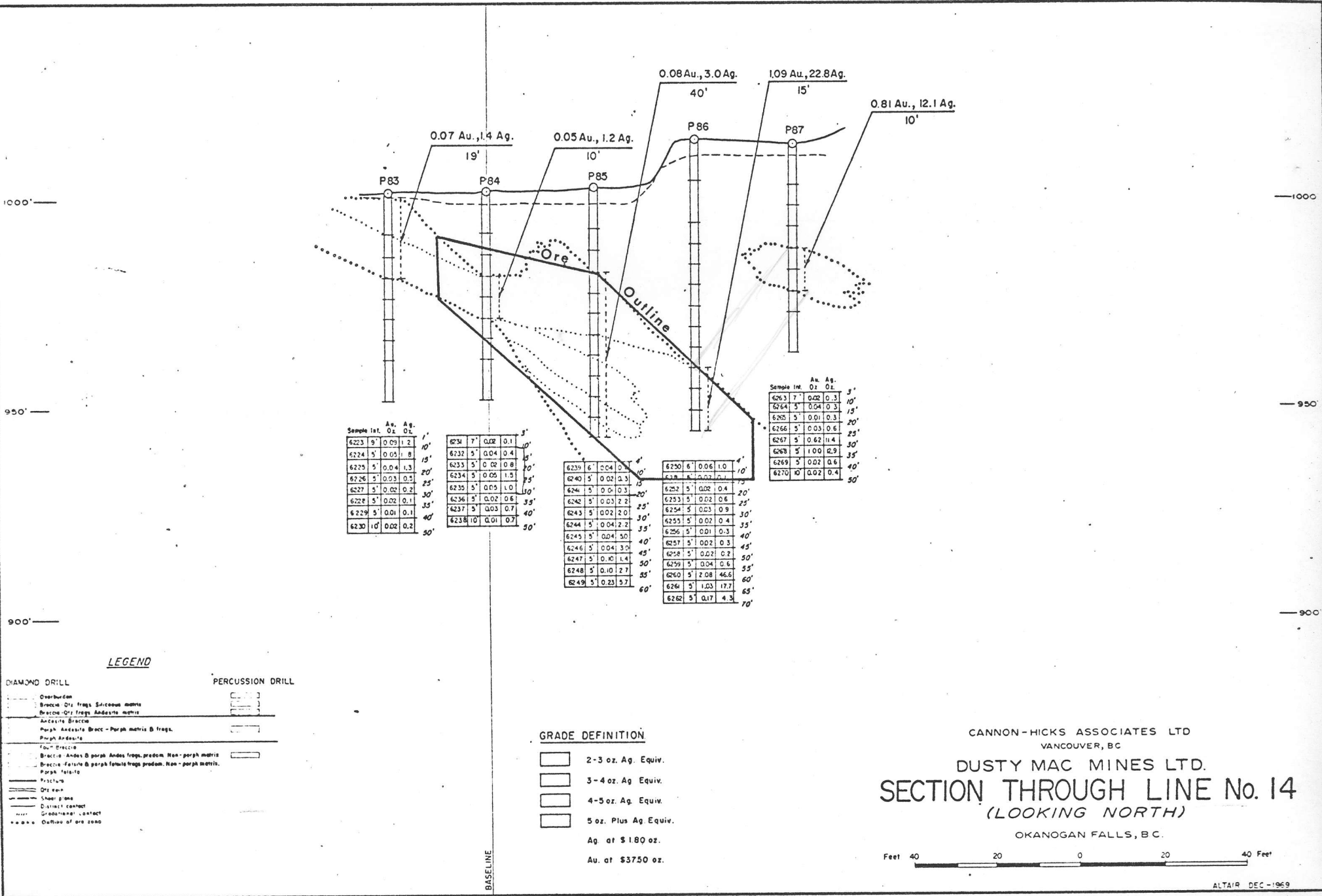
- 2-3 oz. Ag. Equiv.
- 3-4 oz. Ag. Equiv.
- 4-5 oz. Ag. Equiv.
- 5 oz. Plus Ag. Equiv.
- Ag. at \$1.80 oz.
- Au. at \$37.50 oz.

CANNON-HICKS ASSOCIATES LTD
VANCOUVER, BC

DUSTY MAC MINES LTD.
SECTION THROUGH LINE No. 12
(LOOKING NORTH)

OKANOGAN FALLS, B.C.

Feet 40 20 0 20 40 Feet



Sample Int.	Au. Oz.	Ag. Oz.	Depth
6223	9'	0.09	1.2
6224	5'	0.05	1.8
6225	5'	0.04	1.3
6226	5'	0.03	0.5
6227	5'	0.02	0.2
6228	5'	0.02	0.1
6229	5'	0.01	0.1
6230	10'	0.02	0.2

Sample Int.	Au. Oz.	Ag. Oz.	Depth
6231	7'	0.02	0.1
6232	5'	0.04	0.4
6233	5'	0.02	0.8
6234	5'	0.05	1.5
6235	5'	0.05	1.0
6236	5'	0.02	0.6
6237	5'	0.03	0.7
6238	10'	0.01	0.3

Sample Int.	Au. Oz.	Ag. Oz.	Depth
6239	6'	0.04	0.5
6240	5'	0.02	0.3
6241	5'	0.0	0.3
6242	5'	0.03	2.2
6243	5'	0.02	2.0
6244	5'	0.04	2.2
6245	5'	0.04	5.0
6246	5'	0.04	3.0
6247	5'	0.10	1.4
6248	5'	0.10	2.7
6249	5'	0.23	5.7

Sample Int.	Au. Oz.	Ag. Oz.	Depth
6250	6'	0.06	1.0
6251	5'	0.02	0.4
6252	5'	0.02	0.6
6253	5'	0.02	0.6
6254	5'	0.03	0.9
6255	5'	0.02	0.4
6256	5'	0.01	0.3
6257	5'	0.02	0.3
6258	5'	0.02	0.7
6259	5'	0.04	0.6
6260	5'	2.08	46.6
6261	5'	1.03	17.7
6262	5'	0.17	4.3

Sample Int.	Au. Oz.	Ag. Oz.	Depth
6263	7'	0.02	0.3
6264	5'	0.04	0.3
6265	5'	0.01	0.3
6266	5'	0.03	0.6
6267	5'	0.62	11.4
6268	5'	1.00	2.9
6269	5'	0.02	0.6
6270	10'	0.02	0.4

LEGEND

- DIAMOND DRILL**
- Overburden
 - Bracco - Or frags. Siliceous matrix
 - Bracco - Or frags. Andesite matrix
 - Andesite Bracco
 - Porph. Andesite Bracco - Porph matrix B frags.
 - Porph Andesite
 - Porph Bracco
 - Bracco - Andes B porph Andes frags. predom. Non - porph matrix
 - Bracco - Felsite B porph Felsite frags. predom. Non - porph matrix.
 - Porph Felsite
 - Felsite
 - Drill stem
 - Shear plane
 - Distal contact
 - Grade/level contact
 - Outline of ore zone
- PERCUSSION DRILL**
- Overburden
 - Bracco - Or frags. Siliceous matrix
 - Bracco - Or frags. Andesite matrix
 - Andesite Bracco
 - Porph. Andesite Bracco - Porph matrix B frags.
 - Porph Andesite
 - Porph Bracco
 - Bracco - Andes B porph Andes frags. predom. Non - porph matrix
 - Bracco - Felsite B porph Felsite frags. predom. Non - porph matrix.
 - Porph Felsite
 - Felsite
 - Drill stem
 - Shear plane
 - Distal contact
 - Grade/level contact
 - Outline of ore zone

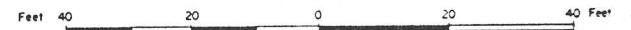
GRADE DEFINITION

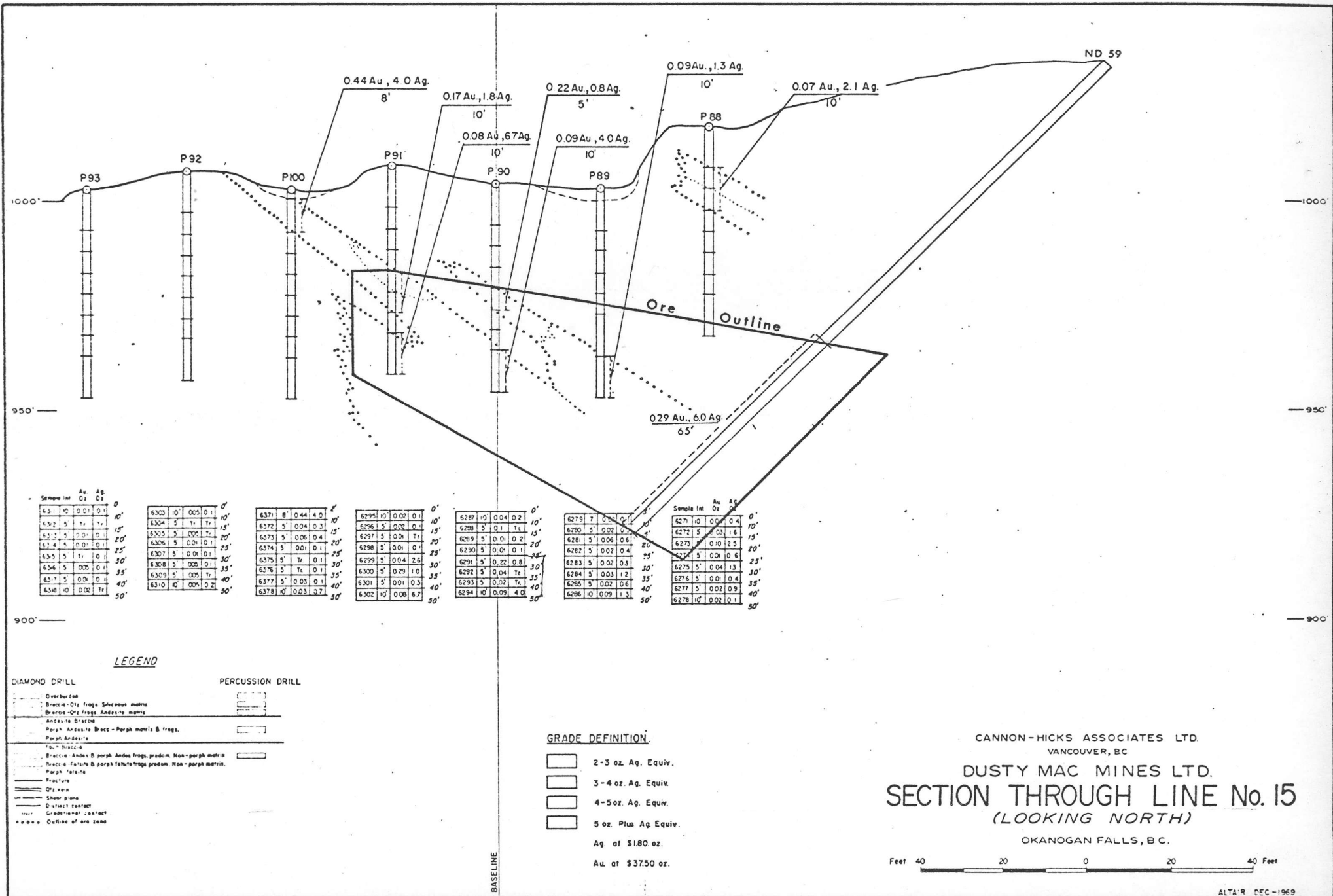
- 2-3 oz. Ag. Equiv.
 - 3-4 oz. Ag. Equiv.
 - 4-5 oz. Ag. Equiv.
 - 5 oz. Plus Ag. Equiv.
- Ag. at \$1.80 oz.
Au. at \$3750 oz.

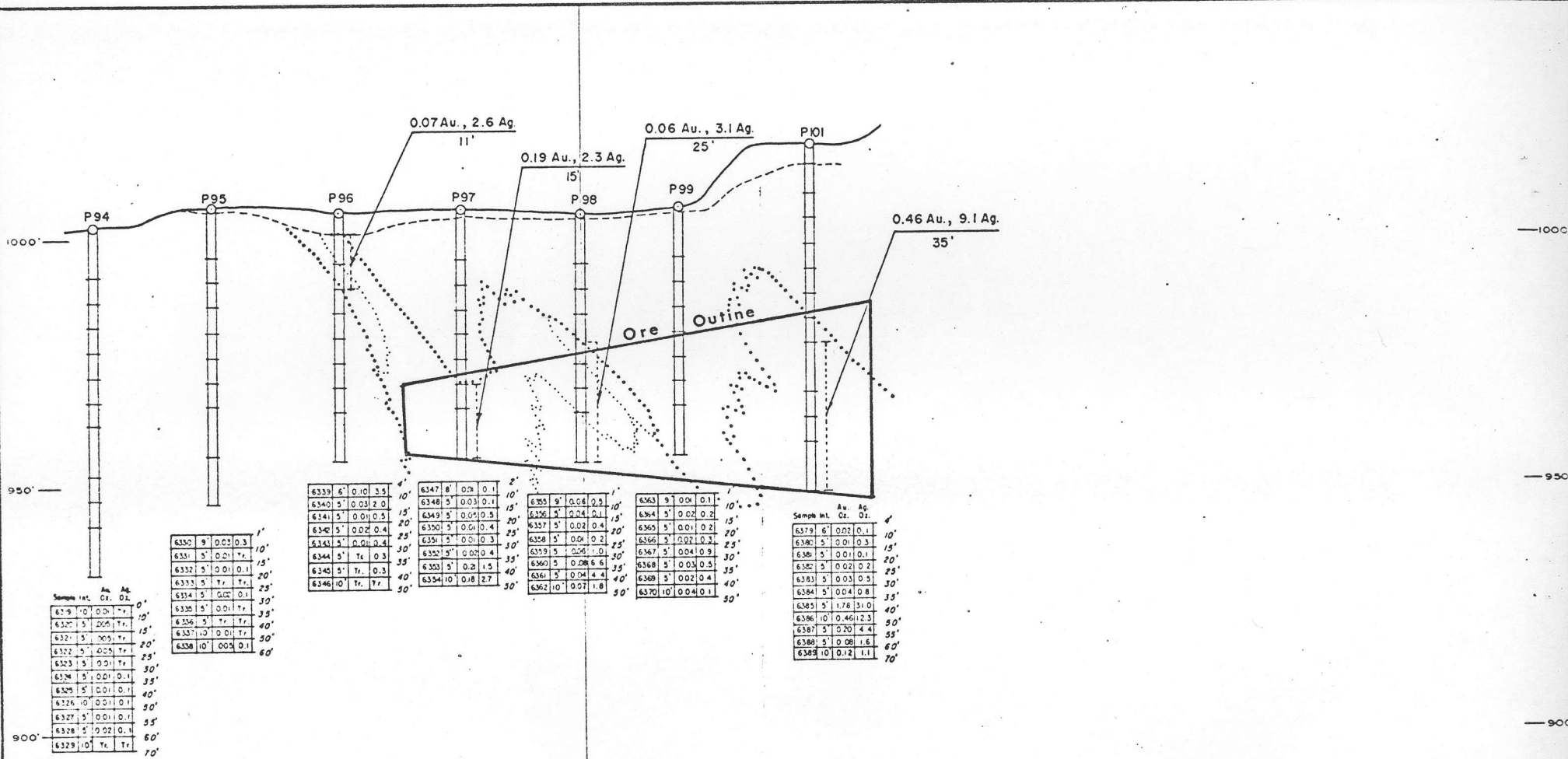
CANNON-HICKS ASSOCIATES LTD
VANCOUVER, B.C.

DUSTY MAC MINES LTD.
SECTION THROUGH LINE No. 14
(LOOKING NORTH)

OKANOGAN FALLS, B.C.







6339	6'	0.10	3.5	10'
6340	5'	0.03	2.0	15'
6341	5'	0.01	0.5	20'
6342	5'	0.02	0.4	25'
6343	5'	0.01	0.4	30'
6344	5'	Tr.	0.3	35'
6345	5'	Tr.	0.3	40'
6346	10'	Tr.	Tr.	50'

6347	8'	0.2	0.1	10'
6348	5'	0.03	0.1	15'
6349	5'	0.05	0.3	20'
6350	5'	0.01	0.4	25'
6351	5'	0.01	0.3	30'
6352	5'	0.02	0.4	35'
6353	5'	0.01	1.5	40'
6354	10'	0.18	2.7	50'

6355	9'	0.06	0.5	10'
6356	5'	0.24	0.1	15'
6357	5'	0.02	0.4	20'
6358	5'	0.06	0.2	25'
6359	5'	0.06	1.0	30'
6360	5'	0.28	6.6	35'
6361	5'	0.04	4.4	40'
6362	10'	0.27	1.8	50'

Sample Int.	Au.	Ag.		
	Oz.	Oz.		
6379	6'	0.02	0.1	10'
6380	5'	0.01	0.3	15'
6381	5'	0.02	0.2	20'
6382	5'	0.02	0.2	25'
6383	5'	0.04	0.9	30'
6384	5'	0.03	0.5	35'
6385	5'	0.02	0.4	40'
6386	10'	0.46	12.3	50'
6387	5'	0.20	4.4	55'
6388	5'	0.08	1.6	60'
6389	10'	0.12	1.1	70'

Sample Int.	Au.	Ag.		
	Oz.	Oz.		
6329	0'	0.0	Tr.	0'
6330	5'	0.01	Tr.	10'
6331	5'	0.01	Tr.	15'
6332	5'	0.01	0.1	20'
6333	5'	Tr.	Tr.	25'
6334	5'	Tr.	Tr.	30'
6335	5'	0.01	Tr.	35'
6336	5'	Tr.	Tr.	40'
6337	5'	0.01	Tr.	45'
6338	10'	0.02	0.1	60'

LEGEND

- DIAMOND DRILL**
- Overburden
 - Brassic Ch. frags. Siliceous matrix
 - Brassic Ch. frags. Andesitic matrix
 - Andesite Breccia
 - Porph. Andesite Brecc. - Porph. matrix & frags.
 - Porph. Andesite
 - Flow Breccia
 - Brassic Andes. B. porph. Andes. frags. predom. Non-porph. matrix
 - Brassic. felsitic B. porph. felsitic frags. predom. Non-porph. matrix
 - Porph. felsite
 - Fracture
 - Qtz vein
 - Shale plane
 - District contact
 - Graben contact
 - Outline of ore zone
- PERCUSSION DRILL**

GRADE DEFINITION

- 2-3 oz. Ag Equiv.
 - 3-4 oz. Ag Equiv.
 - 4-5 oz. Ag Equiv.
 - 5 oz. Plus Ag Equiv.
- Ag. at \$180 oz.
Au. at \$3750 oz.

CANNON-HICKS ASSOCIATES LTD
VANCOUVER, BC
DUSTY MAC MINES LTD.
SECTION THROUGH LINE No. 16
(LOOKING NORTH)
OKANOGAN FALLS, B.C.

