REPORT ON 1989 WORK

on

THE SNOWFIELD GOLD ZONE

and

THE SNOWFIELD GOSSAN AREA

SULPHURETS PROPERTY
SKEENA MINING DIVISION

N.T.S. 104-B/9

March 8, 1990

R.J. JOHNSTON
CORONA CORPORATION

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SUMMARY

*Taking advantage of exceptional snow melt conditions, a short exploration program was conducted around the **Snowfield Gold Zone** located on the north part of **Newhawk-Granduc's Sulphurets Property** north of **Stewart, B.C.** This work was funded and performed by **Corona** on behalf of the joint venture.*

A picketed grid was installed and lithogeochemical sampling, prospecting and cursory mapping were carried out, and core from two 1968 Granduc drill holes was resampled.

*The **Snowfield Gold Zone** was discovered in 1980 and has been estimated to contain 7.7 million tons of 0.08 opt Au in unimpressive looking chloritic andesite tuffs. 1989 results indicate that drilling in the south part of the zone should expand this resource significantly.*

Prospecting discovered a number of new showings, the most significant of which was a 7.3 g/t Au sample from a silicified fault zone on the west end of the grid.

Future work should consist of extending the grid north, east and west for control purposes and to continue the lithogeochemical sampling to discern metal zoning patterns based on a porphyry model. Further geologic work should be detailed and concerted, as obtaining a sound geologic understanding of the area is essential to discovering further mineralization.

INTRODUCTION

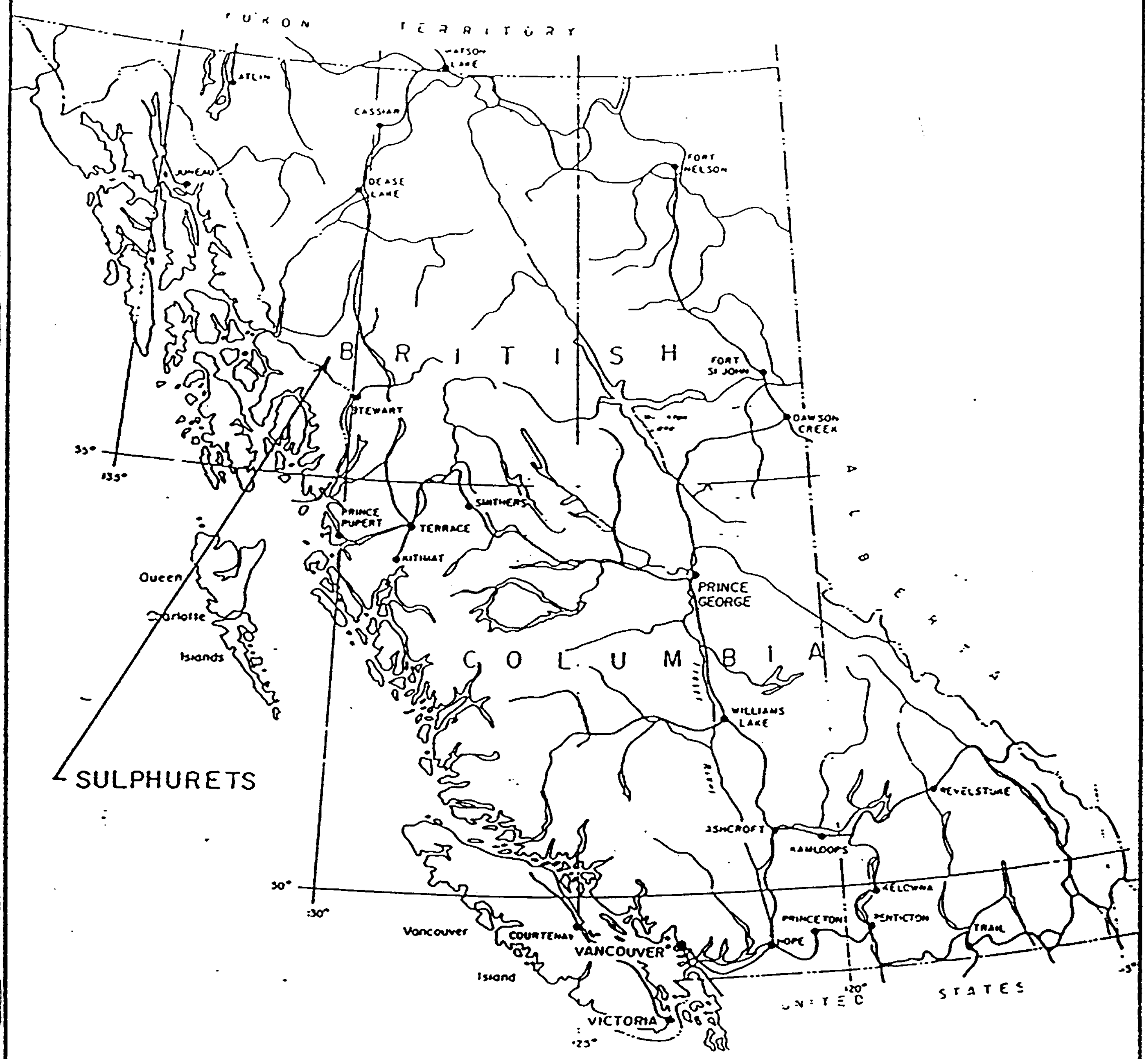
*The **Snowfield Gold Zone** is located 5 km northwest of the Brucejack Au-Ag deposit on **Newhawk Gold Mines-Granduc Mines' Sulphurets Property,** 60 km north of **Stewart, B.C.** in the Coast Mountains of northwest B.C. The zone is situated on the north side of the **Mitchell Sulphurets Ridge** on the east end of the **Snowfield Gossan** at an elevation of 1590 m.*

*Snow conditions in late summer 1989 resulted in the best outcrop exposure in recent history and an excellent opportunity to further explore the Snowfield **Gold Zone** which had previously been extensively snow covered. The work was carried out from a fly camp on the gossan by R. Johnston, B. Laird and D. Gaunt from September 11 - 27, 1989. The project was fully funded by **Corona Corporation** from its 1989 Sulphurets Monitoring Budget.*

HISTORY

*Prospecting and minor placer operations have been carried out in the **Stewart-Unuk River** area throughout this century, and **Mitchell Creek** has long been known to contain placer gold. **Granduc Mines Ltd.** staked the present **Sulphurets Property** in 1960 and subsequent work discovered areas of molybdenite mineralization on the north side of **Mitchell-Sulphurets Ridge**. The **Quartz Stockwork Zone**, located 200 m north of the **Snowfield Gold Zone**, was tested in 1968 by two 1,000 foot diamond drill holes, but only minor molybdenite mineralization was discovered.*

***Esso Minerals Canada** optioned the property in 1980 and the **Snowfield Gold Zone** was discovered in that year as a result of a regional lithogeochemical sampling program. A 200 x 200 m area of chloritic andesite tuffs was found to contain consistent high Au values (>2000 ppb) and trenching carried out in 1981 outlined a large area grading >.04 opt Au.*



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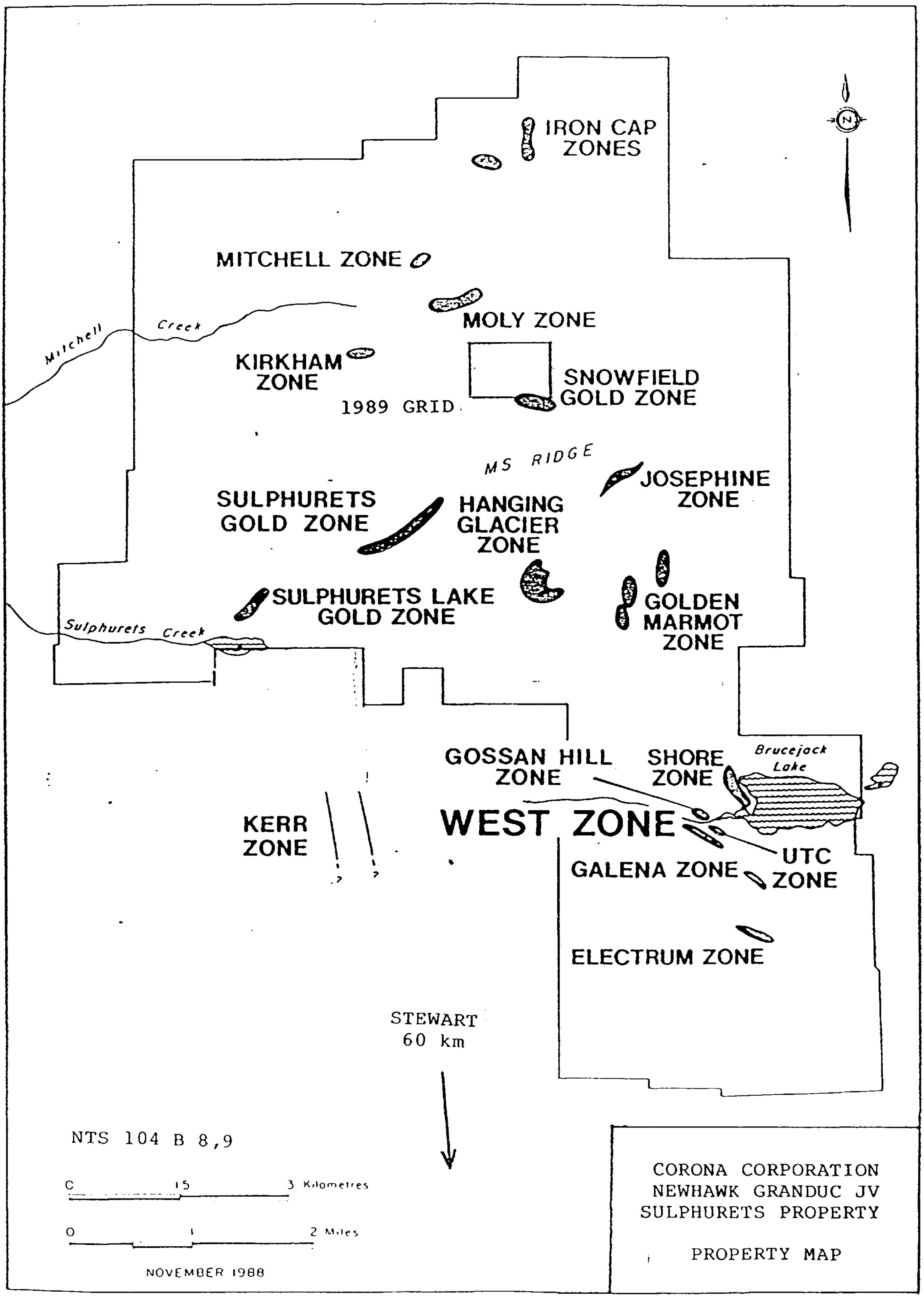
NEWHAWK GRANDUC JV
SULPHURETS PROPERTY

LOCATION MAP


IRON CAP ZONES
MITCHELL ZONE
Mitchell Creek
MOLY ZONE
KIRKHAM ZONE
SNOWFIELD GOLD ZONE
1989 GRID
MS RIDGE
JOSEPHINE ZONE
SULPHURETS GOLD ZONE
HANGING GLACIER ZONE
SULPHURETS LAKE GOLD ZONE
GOLDEN MARMOT ZONE
Sulphurets Creek
GOSSAN HILL ZONE
SHORE ZONE
Brucejack Lake
WEST ZONE
KERR ZONE
GALENA ZONE
UTC ZONE
ELECTRUM ZONE
STEWART 60 km
NTS 104 B 8,9
0 1.5 3 Kilometres
0 1 2 Miles
NOVEMBER 1988
CORONA CORPORATION
NEWHAWK GRANDUC JV
SULPHURETS PROPERTY
PROPERTY MAP

*In 1985 **Newhawk Gold Mines** drilled five diamond drill holes totalling 738.1 m into the auriferous area and outlined a resource of 7.7 million tons averaging 0.08 opt Au. Only cursory visits have been made to the property since 1985.*

REGIONAL GEOLOGY

*The **Mitchell Glacier** area is underlain by Jurassic sedimentary and volcanic rocks of the Hazelton Group which have been locally intruded by intermediate and felsic intrusives and later mafic dykes. Structural deformation has been extensive and large areas have been moderately to intensely sericitized, pyritized and oxidized.*

1989 PROGRAM

*A picketed grid was installed as a control for the mapping and lithogeochemical sampling program and should remain usuable for a number of years. The grid is centred on the **Snowfield Gold Zone**; the collar of 85-112-114 is 0+00N/0+00W and the baseline extends from 1+50E to 10+00W across the **Snowfield Gossan**. A total of 8.025 km of grid lines were put in using 000° as grid north.*

*Rock samples were taken at each of the stations, and the area was prospected and further sampled, and a 1:2,500 geologic map was prepared. Core from the two Granduc drill holes in the **Quartz Stockwork Zone** was logged and resampled. As all of the core from both holes had previously been split, the remaining core was sent out for analysis, with a "skeleton" (3-4 pieces of core from each assay interval) retained at the drill collars.*

LITHOLOGY AND ALTERATION

*The **Snowfield Gossan** is a zone of intense sericite-pyrite ±quartz alteration; an overprint on a reginal chloritization (propylitization?) of the **Mitchell-Sulphurets Ridge**. Most of the original textures have been obscured or obliterated, but the original rock type appears to be andesite lapilli tuff. Bedding measurements near 5+50W/2+00S indicate the tuffs to be overturned.*

A small area of intensely chloritized intermediate intrusive was noted on two small nunataks at the south end of the grid around 3+75W/5+50S. The only other intrusives noted were a number of dark weathering fine grained mafic dykes in the south central part of the grid. Barite veins are spatially related to some of those.

Sericitization is intense throughout much of the gossan with pyrite content ranging from 2-20%. Silicification is locally present both as pervasive alteration and as veins which often contain minor sulphides.

STRUCTURE

*The **Snowfield Gossan** is cut off on the east side by the Brucejack fault and to the west by a northwest fault referred to as the **Ortum Fault**. The gossan itself is cut by numerous regional and local shears which have altered most of the rocks into sericite schists. The more intensely sheared zones contain boudins and rods of quartz and local massive knots of pyrite.*

*Northwest faults which dip 30-55° northeast are the most major in the area The area west of the **Ortum Fault** is made up of chloritized andesites cut by intensely sericitized shears, which is interpreted to be a high level representation of an intense zone of sericitization at depth (the **Snowfield Gossan**). This is similar to the scenario postulated for the **Old Yeller Zone** near **Brucejack Lake** indicating considerable vertical movement on these northwest faults.*

North-south faults cut the northwest ones and have dips ranging from vertical to 65°E, and subvertical east-west faults are also present. Displacement on these faults is unknown.

LITHOGEOCHEMISTRY

*As the **Snowfield Gold Zone** is visually indistinguishable from the surrounding chloritized tuffs, a lithogeochemical sampling program was undertaken as a tool to discover further such zones. Any attempts to contour the geochemical results should take into account two separate populations of samples; more or less systematically collected samples from grid stations; and prospecting samples which tend to be high grade grabs and not necessarily representative of the location.*

*Most of the grid area is extremely high in Au with background values in the >100 ppb range. The **Snowfield Gold Zone** is easily recognized as a 300 x 350 m area in which Au values are consistently >1000 ppb and up to 4060 ppb, surrounded by a 200-300 m wide halo of 300+ ppb Au. No other **Snowfield** type areas were discovered in the sampling program.*

*The **Coffee Pot Zone** shows up as a distinct 200-300 ppb Au anomaly.*

*The eastern half of the grid is strongly anomalous in Mo with values >50 ppm, forming a wide halo around the **Snowfield Gold Zone**, while in the western half of the grid Mo content is less than 20 ppm. This break conincides with an interpreted north-south fault at about 4+50W.*

*Zinc anomalies occur in the propylitically altered areas around the **Snowfield Gold Zone** and on the West side of the **Ortum Fault**, indicating that the intensely sericitized **Snowfield Gossan** is depleted in zinc.*

*Isolated zinc spot anomalies occur around the **Coffee Pot Zone** which contains sphalerite in quartz veins in silicified sericite schists.*

*The **Coffee Pot Zone** is surrounded by a 150 x 100 m area of >3 ppm Ag and a broader area of >1 ppm. The east half of the grid has uniform 1-3 ppm Ag content similar in distribution to Mo values.*

*Cu anomalies are similar to Zn around the **Coffee Pot Zone**, but are absent around the **Snowfield Gold Zone**.*

*Poorly defined anomalous zones of >100 ppm As occurs around both the **Snowfield** and **Coffee Pot Zones**.*

MINERALIZATION

SNOWFIELD GOLD ZONE

*The **Snowfield Gold Zone** is located near the east end of the **Snowfield Gossan** in an area of foliated chloritized andesite tuffs. Sericitization is local and minor and pyrite content is 3-5%. The 1985 **Newhawk** drilling discovered the zone to have sharp assay boundaries, with Au values dropping abruptly from consistently .07 - .09 opt Au to 0.03 opt Au, but with no macroscopic change in lithology, alteration, or sulphide content. All five drill holes went through the gold zone into lower grade material. In situ resource was estimated by **Newhawk** as 7.7 million tons of 0.08 opt Au. Unlike most of the other Au mineralized zones in the **Sulphurets** area the **Snowfield Gold Zone** contains only trace Ag and base metals.*

*Mapping and airphoto interpretation indicated that the NE corner of the **Snowfield Gold Zone** is bounded by a northwest trending fault that dips 30° to the northeast, but the other boundaries of the zone are defined only by decreasing Au values.*

A newly exposed nunatak 100 m south of the edge of the ice was sampled and found to carry >1000 ppb Au, indicating the possibility of greatly increasing reserves with further drilling in that direction.

COFFEE POT ZONE

A zone of silicified sericite schist was located during the lithogeochem sampling in the northernmost part of the grid. This was followed up by prospecting and further sampling. The ***Coffee Pot Zone*** *consists of moderately-intense, pervasively silicified sericite pyrite schist cut by randomly oriented quartz veins. Massive pyrite with local tetrahedrite and chalcopyrite occurs locally in veins and in the silicified schist. The highest precious metal values obtained were .07 opt Au and 3.4 opt Ag from a high grade grab.*

The zone appears to be in the footwall of a northwest trending northeast dipping fault and is cut off to the northeast by a major north-south shear. The zone is open to the southwest and further prospecting could extend the zone in that direction.

QUARTZ STOCKWORK ZONE

A 500 m x 500 m zone containing 30-50% quartz veins extends off the northeast corner of the grid. It contains only minor pyrite but molybdenite was discovered in the northeast part of the zone above the Mitchell Glacier by ***Granduc*** *, and in 1968 two 1000' holes (DDH-7 and 8) were drilled to test the zone. No significant molybdenum mineralization was encountered. As the core had not originally been assayed for Au, it was resampled in 1989 and submitted for gold geochemical analysis. Au results are similar to the rest of the* ***Snowfield Gossan*** *in that almost all samples returned >200 ppb Au. Local zones of higher grade material were encountered, including a single section near the top of DDH-8 which returned .102 opt Au from a narrow oxidized shear. Background levels of Cu and Mo were high throughout the core.*

The southernmost of the two holes, DDH-8, was collared in stockwork but quickly drilled out of it to the south. It appears that the zone is faulted off on the south and west sides.

MOLYBDENITE ZONE

A zone of significant molybdenite mineralization was discovered by Esso in early 1980s 300 m northwest of the ***Granduc*** *drill holes. This area was probably snowcovered in 1968 but was intensely trenched by Esso. The zone extends from 1 N to 4 S between 2+50W and 4W and is comprised of sericite-pyrite schist with abundant molybdenite bearing quartz veins which returned Mo values up to .9%.*

BARITE VEINS

Barite veins, hosted in tension gashes adjacent to fine grained mafic dykes occur in an indistinct zone which extends from 2+50W/4S to 5W/3S. The veins contain local galena and sphalerite and the highest value obtained was .04 opt Au and 0.32 opt Ag from a high grade grab.

One km southeast on the ridgetop is the ***Josephine Zone*** *which contains spotty but spectacular Au and Ag values; up to 1.6 opt Au and 215 opt Ag, in quartz and barite veins. The two zones may be related but the intervening area is ice covered.*

ORTUM FAULT

The best Au result during the 1989 work was .21 opt Au obtained from a 2-3 m wide milled quartz pyrite zone adjacent to the ***Ortum Fault****, which terminates the* ***Snowfield Gossan*** *on the west side. Only minor prospecting was done during the 1989 program and any future work on the* ***Snowfield Gossan*** *area should include detailed prospecting and sampling along the fault.*

CONCLUSIONS

The ***Mitchell-Sulphurets*** *ridge is host to extensive alteration, considerable structural deformation and significant Au and base metal mineralization. Work to date has been sporadic and cursory, and although further work is unlikely to discover large obvious areas of surface mineralization,* *potential does exist for uncovering mineralization of a more subtle nature.*

Most of the ***Snowfield Gossan*** *contains high Au values (>100 ppb), and though no additional* ***Snowfield Gold Zone*** *targets were located, it was shown that the zone does continue to the south under the ice. Mapping around the* ***Snowfield Gold Zone*** *and the* ***Snowfield Gossan*** *were only of a cursory nature and did not reveal any structural, alteration or lithologic controls to the Au mineralization.*

The ***Snowfield Gold Zone*** *differs markedly from other mineralized zone on the property, which are mesothermal, much less consistent in Au content and contain significant Ag.*

Most of the ***Mitchell-Sulphurets*** *ridge west of the grid is propylitically altered and although* ***Esso*** *did lithogeochemical sampling in 1980, some potential exists for the discovery of further mineralization by systematic grid sampling.*

The mineralization on the ***Coffee Pot Zone*** *is later than the above. It is hosted in faulted silicified sericite schists and contains base metal sulphides. The zone looked impressive but precious metal values were disappointing. It appears to be open to the southeast and further prospecting and sampling could extend it considerably.*

The barite veins discovered in the south central part of the grid appear to postdate the fine grained mafic dykes and are probably the latest mineralizing event on the ***Snowfield Gossan*** *area. Auriferous barite veins occur on the* ***Josephine Showing*** *1 km to the southeast.*

RECOMMENDATIONS

The existing grid should be extended to the north across the ***Quartz Stockwork Zone*** *and to the* ***Moly Zone*** *on the* ***Mitchell Glacier,*** *and to the east as the* ***Snowfield Gold Zone*** *is open in that dirction. To the west across the* ***Ortum***

Fault is a large area of propylitic altered volcanics and the potential exists for a discovering further *Snowfield Gold Zone* type mineralization.

Extending the grid and continuing the systematic lithogeochemical sampling will provide the basis for work on metal zonations to locate porphyry mineralization. Detailed mapping is required to understand controls on the known mineralization.

The retreat of snow and ice from the southern part of the **Snowfield Gold Zone** permits an opportunity for further drilling to the south which could significantly increase reserves there.

An obvious target for further sampling and detailed prospecting is the 7.3 g/t Au sample obtained from silicified and pyritic fault gouge on the **Ortum Fault**. This area has the best potential for an easily defined Au zone.

APPENDIX I

ROCK SAMPLE ANALYSES

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: ROCK AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

DATE RECEIVED: SEP 26 1989 DATE REPORT MAILED: Oct 5/89. SIGNED BY. C. Leong .D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

Corona Corporation PROJECT 1014 File # 89-3926 Page 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
2+00N 7+80W	9	62	76	29	5.5	16	22	37	12.59	468	5	ND	1	7	1	2	2	7	.06	.003	2	5	.06	3	.01	8	.29	.02	.17	5	326
1+60N 5+95W	11	164	40	192	3.3	9	9	17	14.04	24	16	ND	2	17	6	2	2	2	.02	.001	2	5	.01	4	.01	4	.12	.01	.05	2	308
1+55N 7+65W	1	60	1569	482	6.0	5	10	27	4.70	173	5	ND	1	19	4	2	2	9	.16	.063	4	2	.04	11	.01	8	.25	.01	.19	1	260
1+50N 8+75W	5	24	80	21	1.8	11	7	18	3.51	123	5	ND	1	9	1	2	2	8	.01	.007	4	5	.04	16	.01	9	.30	.01	.25	2	203
1+35N 8+95W	11	82	125	335	9.6	119	45	17	13.13	471	5	ND	1	6	3	5	2	7	.02	.004	2	7	.03	7	.01	7	.23	.01	.14	2	907
1+35N 7+75W	2	341	653	359	48.1	8	7	17	7.08	121	5	ND	1	16	3	6	2	6	.01	.002	2	3	.02	6	.01	5	.20	.01	.18	1	1787
9+75W 0+60N	9	27	51	11	2.2	10	10	25	4.18	105	5	ND	1	4	1	2	2	7	.01	.010	3	5	.02	14	.01	3	.21	.01	.18	1	302
9+05W 1+55N	2	64	118	30	5.5	26	14	19	5.74	331	5	ND	1	9	1	10	2	8	.03	.010	4	7	.02	9	.01	2	.23	.02	.19	2	186
9+00W 1+50N	4	28	41	15	1.5	17	11	98	4.15	89	5	ND	2	6	1	2	2	21	.04	.046	5	9	.16	20	.01	17	.30	.02	.15	2	65
9+00W 1+00N	9	15	58	42	.9	9	4	153	2.09	49	5	ND	1	24	1	2	2	4	.24	.023	4	5	.02	77	.01	5	.17	.02	.15	2	92
9+00W 0+50N	7	69	280	2579	22.8	14	8	23	4.08	247	5	ND	1	14	29	12	2	14	.06	.018	2	5	.03	16	.04	10	.25	.01	.19	1	927
9+00W OBL	2	17	98	41	1.2	9	10	503	3.48	30	5	ND	3	17	1	2	2	6	.10	.024	5	4	.56	17	.02	2	.63	.01	.21	4	109
8+90W 1+65N	318	36	43	616	2.4	11	4	22	4.63	132	5	ND	1	7	4	9	2	7	.02	.003	3	7	.02	7	.01	5	.22	.01	.15	1	331
8+85W 1+95N	2	140	18	57	4.3	26	9	839	5.28	110	5	ND	2	70	1	7	2	22	1.73	.102	6	10	.76	17	.01	26	.62	.02	.24	2	319
8+60W 0+35S	2	54	239	345	2.4	5	9	1378	4.58	46	5	ND	5	16	2	2	2	34	.22	.184	11	6	1.25	21	.01	15	1.50	.01	.23	1	60
8+00W 2+50N	81	46	102	20	2.0	7	4	209	2.98	19	5	ND	2	20	1	2	2	7	.21	.035	4	6	.06	36	.01	3	.17	.02	.13	2	23
8+00W 2+00N	2	38	16	66	1.3	22	11	778	5.67	110	5	ND	1	47	1	2	2	32	1.33	.060	5	24	.67	15	.03	2	.65	.02	.14	9	175
8+00W 1+50N	4	193	62	54	.7	10	5	754	1.55	60	5	ND	1	119	1	4	2	3	1.23	.027	2	3	.10	22	.01	7	.19	.01	.14	1	74
8+00W 1+00N	2	346	293	273	1.9	15	6	740	4.28	29	5	ND	1	47	2	2	2	9	.74	.044	3	10	.37	18	.01	8	.59	.01	.21	1	134
8+00W 0+50N	1	125	120	118	1.7	8	10	707	3.79	39	5	ND	3	20	1	3	2	23	.22	.100	7	5	.79	35	.06	2	1.05	.01	.23	1	85
8+00W 0+50S	2	68	32	136	1.2	17	11	487	4.75	22	5	ND	1	5	1	2	2	21	.10	.055	4	16	.92	14	.01	16	.93	.01	.18	1	166
8+00W 1+00S	2	334	466	84	5.6	12	16	127	15.95	117	5	ND	3	6	2	22	11	6	.13	.053	3	4	.11	1	.01	2	.40	.01	.16	1	221
8+00W 1+50S	1	55	28	160	.6	8	13	1451	3.53	78	5	ND	1	66	1	4	2	31	1.45	.110	7	6	1.14	19	.07	7	1.36	.01	.18	1	72
8+00W 2+00S	1	22	42	251	.4	4	13	3192	4.10	45	5	ND	1	79	1	2	2	38	2.47	.134	7	3	1.71	13	.07	2	1.82	.01	.15	1	77
8+00W 2+50S	1	23	41	287	1.1	5	10	3500	3.56	106	5	ND	1	61	2	3	2	17	3.50	.122	8	2	.59	12	.07	5	.81	.01	.23	9	141
7+75W 1+15N	13	461	67	69	3.4	26	20	931	4.02	99	5	ND	2	38	1	4	2	6	.42	.052	7	3	.06	15	.01	5	.39	.01	.27	1	264
7+60W 1+60N	1	779	44	408	2.1	3	7	1807	4.35	20	5	ND	2	58	6	2	2	14	1.13	.151	7	1	.31	12	.01	2	.42	.01	.27	1	78
7+00W 3+50N	64	63	99	33	3.7	4	3	68	4.48	156	5	ND	2	11	1	4	2	13	.02	.057	7	8	.02	116	.01	16	.18	.03	.23	3	574
7+00W 3+00N	8	276	112	147	3.3	30	6	839	6.52	118	5	ND	1	36	3	6	2	5	1.19	.046	2	5	.05	3	.01	2	.30	.01	.19	10	388
7+00W 2+50N	3	1615	98	187	46.7	6	4	32	4.91	597	5	ND	1	7	2	572	22	7	.01	.012	5	4	.01	6	.01	4	.16	.01	.14	1	639
7+00W 2+00N	2	35	146	31	3.3	6	8	20	5.68	84	5	ND	2	41	1	7	2	7	.01	.037	4	4	.02	7	.01	14	.19	.01	.22	1	186
7+00W 1+50N	2	424	79	63	4.7	6	9	543	3.71	46	5	ND	3	42	1	5	2	11	.55	.118	4	2	.22	22	.01	2	.37	.01	.26	2	131
7+00W 1+00N	5	230	105	102	2.7	5	8	338	3.09	35	5	ND	3	36	1	12	2	16	.33	.130	3	2	.34	12	.01	5	.58	.01	.26	1	121
7+00W 0+50N	11	32	90	48	.9	13	6	46	2.70	39	5	ND	1	57	1	4	2	8	.01	.026	2	7	.03	21	.01	2	.24	.02	.21	1	166
7+00W 0+40N	4	120	111	42	5.9	28	22	13	13.16	159	5	ND	1	36	1	6	2	9	.04	.018	2	5	.01	1	.01	23	.20	.01	.09	1	499
STD C/AU-R	18	61	40	132	6.5	68	30	946	4.08	40	18	7	37	48	18	15	19	57	.50	.088	38	56	.90	174	.05	36	1.91	.06	.14	13	505

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
7+00W 0+50S	2	89	88	133	1.8	41	28	67	7.59	81	5	ND	1	11	1	15	2	9	.24	.116	2	7	.31	5	.01	5	.65	.01	.14	1	66
7+00W 1+00S	2	52	66	21	1.0	28	15	12	6.64	30	5	ND	1	29	1	8	2	4	.08	.035	2	2	.06	4	.01	9	.33	.01	.10	1	75
7+00W 1+50S	2	19	50	10	.1	25	10	7	4.04	38	5	ND	1	5	1	2	2	1	.02	.008	2	1	.01	4	.01	2	.02	.01	.01	1	72
7+00W 2+00S	3	33	31	91	.6	15	6	35	1.98	21	5	ND	1	22	1	2	2	4	.10	.043	2	4	.09	12	.01	2	.28	.01	.03	1	46
6+90W 3+00N	9	129	7	18	2.1	27	17	25	9.15	248	5	ND	1	5	1	7	2	6	.02	.002	3	5	.02	3	.01	5	.20	.01	.13	3	930
6+90W 1+40N	3	1236	13584	1177	57.1	7	4	22	1.68	107	5	ND	2	30	22	39	45	6	.14	.088	3	4	.03	78	.01	2	.28	.01	.19	1	1160
6+75W 0+60S	3	69	133	41	2.6	19	9	40	14.54	164	5	ND	1	26	1	10	2	4	.04	.017	2	9	.08	3	.01	2	.23	.01	.06	1	210
6+10W 0+10N	4	17	51	10	.5	14	7	13	3.44	16	5	ND	1	4	1	2	2	3	.01	.010	2	1	.03	15	.01	3	.32	.01	.14	1	62
6+05W 2+40N	1	12	27	5	.5	4	1	2	.45	8	5	ND	1	439	1	2	2	1	.02	.008	2	1	.01	66	.01	2	.05	.01	.03	2	17
6+05W 1+85N	4	21	68	3	1.8	11	2	25	.93	5	5	ND	1	29	1	2	2	3	.01	.007	2	8	.01	45	.01	2	.11	.01	.07	1	143
5+00W 3+50N	4	54	14	7	1.3	5	1	21	2.65	24	5	ND	2	28	1	2	2	9	.01	.069	3	3	.03	106	.01	2	.18	.02	.14	1	240
5+00W 3+00N	1	182	33	67	2.5	6	8	538	3.05	28	5	ND	3	18	1	2	2	38	.20	.117	7	9	.77	19	.01	2	.88	.02	.20	1	173
5+00W 2+50N	3	122	47	18	4.0	8	4	85	2.88	23	5	ND	3	27	1	2	2	15	.10	.073	4	3	.15	14	.01	4	.41	.01	.27	1	440
5+00W 2+00N	2	1102	25	49	2.1	8	8	228	2.77	29	5	ND	2	101	1	11	2	7	.45	.119	4	3	.13	13	.01	9	.40	.01	.24	1	102
6+00W 1+50N	9	496	40	56	3.4	6	25	9	3.88	101	5	ND	2	5	1	27	2	6	.02	.014	3	1	.03	10	.01	2	.34	.01	.21	1	220
6+00W 1+00N	13	25	45	11	.6	22	18	8	4.62	40	5	ND	1	4	1	2	2	3	.01	.009	2	1	.01	11	.01	2	.34	.01	.17	1	60
5+00W 0+50N	2	108	171	190	1.6	22	22	20	6.30	34	5	ND	1	11	3	2	2	7	.06	.060	2	5	.18	4	.01	2	.63	.01	.11	1	48
5+00W 0+00N	3	70	32	23	.7	17	9	18	3.35	23	5	ND	1	5	1	2	2	4	.01	.012	2	3	.12	11	.01	4	.49	.01	.12	1	50
5+00W 0+50S	70	120	33	93	.5	20	11	240	3.16	20	5	ND	2	15	1	6	2	7	.50	.058	2	9	.62	16	.01	2	.77	.01	.14	1	75
5+00W 1+00S	1	16	20	27	.3	14	8	7	3.54	6	5	ND	1	5	1	2	2	3	.01	.013	2	2	.07	9	.01	2	.40	.01	.11	1	66
5+00W 1+50S	2	28	50	19	.4	26	9	16	4.39	6	5	ND	1	16	1	2	2	5	.19	.085	2	3	.05	6	.01	3	.45	.01	.16	1	71
5+00W 2+00S	1	12	48	52	.3	32	17	30	5.24	5	5	ND	1	12	1	2	2	10	.03	.023	2	5	.27	5	.01	2	.79	.01	.12	1	31
5+00W 2+50S	3	12	172	5	.2	9	2	14	1.21	7	5	ND	1	52	1	2	2	2	.05	.026	2	3	.02	27	.01	2	.28	.01	.12	1	30
5+00W 2+95S	2	78	108	40	1.4	14	8	9	2.54	32	5	ND	1	13	1	2	2	2	.02	.012	2	2	.02	11	.01	2	.30	.01	.13	1	42
5+75W 0+40S	427	105	112	232	1.9	11	6	34	4.98	44	5	ND	1	78	4	2	2	3	.01	.006	2	7	.09	5	.01	3	.24	.01	.06	1	210
5+50W OBL	43	431	187	105	6.2	5	7	51	6.06	88	5	ND	2	24	3	23	2	4	.02	.046	2	4	.28	4	.01	2	.58	.01	.14	1	158
5+25W 1+00N	61	248	61	198	1.2	17	18	262	4.23	3	5	ND	1	4	1	2	2	9	.15	.046	2	10	.64	12	.01	2	.92	.01	.12	1	105
5+10W 0+50N	22	58	74	87	.6	7	3	111	2.84	5	5	ND	2	7	1	2	2	9	.03	.057	5	7	.46	64	.01	2	.73	.01	.15	1	136
5+00W 3+50N	7	23	42	31	.9	8	6	35	5.54	11	5	ND	1	36	1	2	2	6	.01	.030	2	4	.07	5	.01	2	.24	.01	.11	1	100
5+00W 3+00N	2	40	45	62	.8	5	9	57	4.36	18	5	ND	1	6	1	3	2	13	.09	.063	2	5	.47	8	.01	2	.78	.01	.12	1	95
5+00W 2+50N	16	16	28	11	.2	26	11	9	5.01	4	5	ND	2	5	1	2	2	4	.03	.024	2	3	.04	6	.01	4	.32	.01	.14	1	47
5+00W 2+00N	4	7	9	5	.2	12	6	9	2.72	21	5	ND	1	5	1	2	2	2	.01	.010	2	1	.01	14	.01	4	.23	.01	.12	1	56
5+00W 1+50N	307	264	49	106	1.7	5	8	1104	2.97	3	5	ND	1	50	1	2	2	4	.31	.014	2	4	.17	10	.01	2	.35	.01	.16	1	112
5+00W 0+50S	19	84	32	74	.7	15	10	76	3.49	5	5	ND	2	6	1	2	2	6	.06	.032	3	8	.33	9	.01	6	.56	.01	.14	1	69
5+00W 1+00S	29	87	65	163	1.2	26	12	256	3.34	21	5	ND	2	56	1	6	2	19	.02	.041	4	15	1.40	18	.01	2	1.51	.01	.16	1	196
5+00W 1+50S	4	80	53	114	.6	17	9	254	3.13	12	5	ND	2	44	1	2	2	14	.06	.035	3	17	.93	9	.01	5	1.01	.02	.13	1	151
STD C/AU-R	18	57	42	132	6.6	67	30	1031	4.03	41	19	7	37	47	18	15	21	57	.48	.091	38	55	.91	174	.05	34	1.94	.06	.14	12	495

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
5+00W 2+00S	26	60	41	9	4.8	3	1	23	3.57	281	5	ND	2	14	1	27	2	4	.19	.061	2	1	.01	201	.01	2	.26	.01	.13	1	123
5+00W 2+50S	4	23	46	47	.5	11	7	27	3.18	7	5	ND	1	15	1	2	2	5	.20	.023	2	3	.25	11	.01	2	.54	.01	.13	1	144
5+00W 3+00S	9	46	30	7	.7	57	13	7	3.82	3	5	ND	1	9	1	2	2	3	.11	.040	2	3	.01	8	.01	2	.30	.01	.13	1	280
5+00W 3+50S	6	60	36	83	.5	15	9	127	3.72	14	5	ND	1	6	2	4	2	7	.07	.031	2	8	.71	15	.01	2	.98	.02	.14	1	104
4+95W 2+10S	6	32	73	209	.5	11	1	68	.66	17	5	ND	1	109	4	3	2	4	.07	.020	2	11	.26	415	.01	5	.48	.01	.02	1	23
4+80W 3+30S	11	25	21	4	.8	14	8	7	3.11	7	5	ND	1	21	1	2	2	3	.03	.027	2	1	.01	9	.01	2	.27	.01	.14	1	135
4+10W 1+00S	393	113	35	23	.6	7	3	8	2.09	97	5	ND	1	6	1	6	2	2	.01	.005	2	2	.01	26	.01	2	.23	.01	.11	1	143
4+07W 1+90N	189	163	26	24	1.3	9	8	14	6.65	37	5	ND	1	32	1	4	2	2	.03	.012	2	2	.01	4	.01	2	.17	.01	.09	1	165
4+00W 3+50N	61	263	15	72	1.0	3	7	144	3.95	2	5	ND	3	19	1	2	2	38	.29	.164	8	6	.87	36	.01	4	1.23	.01	.21	1	430
4+00W 3+20N	47	454	17	93	2.4	8	64	103	24.68	8	5	ND	1	7	1	4	2	18	.12	.062	2	7	.18	2	.01	13	.39	.01	.04	1	920
4+00W 3+00N	43	80	36	40	.9	3	7	83	2.63	4	5	ND	1	66	1	2	2	24	.11	.056	6	4	.41	21	.01	2	.69	.01	.21	1	480
4+00W 2+50N	293	266	34	77	1.6	7	9	164	8.84	50	5	ND	1	9	1	2	2	41	.03	.081	6	12	.83	50	.01	2	1.19	.01	.15	1	450
4+00W 2+00N	114	570	20	34	.9	10	5	577	2.27	14	5	ND	1	10	1	2	2	2	.42	.029	2	5	.29	25	.01	2	.34	.01	.13	2	102
4+00W 1+50N	149	201	37	67	1.2	22	9	63	6.13	22	5	ND	1	8	2	2	2	6	.08	.060	2	6	.08	11	.01	2	.44	.01	.14	1	460
4+00W 1+20N	9305	113	86	77	2.3	20	5	45	1.93	4	7	ND	1	6	3	2	3	6	.01	.013	2	8	.03	19	.01	6	.17	.01	.05	1	230
4+00W 1+13N	396	49	24	22	.8	11	4	6	1.60	2	5	ND	1	7	1	2	2	3	.01	.007	2	2	.01	52	.01	3	.27	.01	.13	1	150
4+00W OBL	77	231	55	29	.9	11	7	12	3.14	75	5	ND	1	27	1	7	2	2	.01	.012	2	2	.01	17	.01	2	.21	.01	.11	1	111
4+00W 0+50S	64	402	12	32	.6	49	13	51	4.14	15	5	ND	2	8	1	2	2	8	.19	.113	2	4	.14	30	.01	2	.64	.01	.22	1	660
4+00W 1+35S	59	480	19	54	.1	1	3	24	38.74	49	5	ND	1	31	1	2	2	26	.01	.392	2	5	.01	118	.01	2	.19	.01	.05	1	63
4+00W 1+50S	89	242	28	115	.4	29	12	360	4.63	5	5	ND	3	110	1	2	2	22	.05	.074	2	20	1.46	48	.01	3	2.09	.01	.12	1	350
4+00W 2+00S	39	112	30	63	.7	6	9	98	4.13	20	5	ND	2	19	1	2	2	5	.08	.063	2	5	.22	22	.01	2	.60	.01	.14	1	960
4+00W 2+50S	350	121	528	87	.7	19	6	71	2.04	34	5	ND	1	21	1	14	2	5	.05	.025	2	8	.22	22	.01	2	.53	.01	.10	1	107
4+00W 2+85S	225	53	433	202	.4	12	3	23	.73	2	5	ND	1	114	2	2	2	2	.01	.003	2	8	.04	95	.01	2	.18	.01	.04	1	117
4+00W 3+00S	1974	91	30	10	1.7	12	2	22	1.12	6	5	ND	1	44	1	6	2	2	.01	.004	3	9	.01	31	.01	2	.17	.01	.09	1	118
4+00W 3+50S	42	43	84	6	1.2	20	11	11	7.41	6	5	ND	1	13	1	2	2	3	.01	.013	2	4	.02	4	.01	2	.25	.01	.13	1	134
3+95W 3+52N	87	200	7	12	1.5	10	23	24	3.55	4	5	ND	1	2	1	2	2	1	.01	.001	2	6	.01	16	.01	2	.02	.01	.01	1	80
3+95W 1+65N	8	77	35	6	10.9	10	44	18	5.90	525	7	2	1	6	1	2	2	4	.01	.009	3	4	.01	9	.01	2	.15	.02	.12	2	1940
3+95W 1+50S	48	16	90	58	.1	13	1	61	.72	2	5	ND	1	77	1	2	2	2	.01	.008	2	11	.13	148	.01	2	.22	.01	.01	1	117
3+85W 0+60N	37	84	47	11	.5	12	5	18	2.94	47	5	ND	1	25	1	6	2	4	.01	.016	2	3	.01	41	.01	3	.25	.01	.13	1	104
3+50W 3+50S	25	110	106	29	3.1	22	14	17	13.79	115	5	ND	1	9	1	16	2	3	.04	.029	4	6	.02	4	.01	8	.25	.01	.13	1	210
3+00W 3+50N	98	552	57	181	1.3	16	10	1185	4.68	2	5	ND	2	13	1	2	2	12	.47	.069	2	12	1.00	28	.01	2	1.19	.01	.12	1	490
3+00W 3+00N	74	378	26	64	1.3	11	7	58	4.06	5	5	ND	4	12	1	2	2	12	.05	.086	2	9	.32	57	.01	3	.75	.01	.12	1	720
3+00W 2+50N	307	255	140	139	1.4	18	4	167	3.44	4	5	ND	1	8	1	2	2	7	.14	.073	2	9	.24	44	.01	2	.69	.01	.08	1	540
3+00W 2+00N	177	40	31	7	.6	16	3	13	1.49	5	5	ND	1	19	1	2	2	3	.01	.007	2	6	.01	69	.01	2	.23	.01	.10	1	280
3+00W 1+50N	79	48	176	20	.6	6	1	13	1.53	15	5	ND	1	10	1	2	2	4	.01	.020	2	4	.01	166	.01	2	.22	.01	.11	1	134
3+00W 1+00N	101	172	50	89	.8	25	13	219	5.82	4	5	ND	1	7	1	2	2	8	.08	.049	2	7	.22	17	.01	2	.77	.01	.09	1	300
STD C/AU-R	18	58	39	132	6.6	67	30	1037	4.16	40	18	7	37	47	18	15	20	57	.48	.093	38	55	.91	175	.05	35	1.95	.06	.14	13	515

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
3+00W 0+50N	77	338	40	20	1.0	17	8	9	2.90	7	5	ND	1	12	1	2	2	2	.03	.008	2	1	.01	8	.01	3	.24	.01	.10	2	134
3+00W OBL	192	559	74	301	1.2	57	22	276	4.11	14	5	ND	3	128	1	2	2	22	.08	.096	2	20	.56	23	.01	2	1.40	.01	.10	1	1040
3+00W 0+50S	97	291	107	481	1.2	35	10	359	4.09	6	5	ND	1	21	5	2	2	18	.10	.076	2	12	.56	9	.01	6	1.43	.01	.07	1	400
3+00W 1+00S	81	139	51	76	1.1	22	17	61	4.90	20	5	ND	2	8	1	2	2	5	.15	.068	2	2	.10	4	.01	2	.43	.01	.13	1	430
3+00W 1+50S	74	429	75	145	1.5	13	9	362	4.09	165	5	ND	1	8	2	4	2	7	.28	.064	2	3	.26	6	.01	2	.67	.01	.11	1	430
3+00W 3+50S	44	218	43	47	.6	30	12	90	3.76	19	5	ND	1	14	2	2	3	7	.16	.062	4	13	.28	6	.01	14	.54	.01	.17	2	101
2+90W 2+00N	237	144	27	124	.8	20	10	114	4.38	11	5	ND	1	4	1	2	2	10	.04	.030	2	5	.21	8	.01	2	.67	.01	.06	1	420
2+60W 3+50S	26	719	30	107	.4	22	9	332	3.54	2	5	ND	3	15	1	2	2	29	.23	.093	6	19	2.21	10	.01	3	2.09	.01	.14	1	144
2+00W 1+50N	225	316	97	109	1.0	5	2	53	8.00	18	5	ND	1	14	1	2	2	6	.01	.056	2	3	.01	101	.01	5	.31	.01	.10	1	320
2+00W 1+00N	177	105	171	97	1.6	5	2	61	2.47	16	5	ND	1	18	1	2	2	4	.01	.036	2	2	.10	113	.01	2	.42	.01	.11	1	320
2+00W 0+50N	228	168	92	370	1.4	6	5	1896	3.81	24	5	ND	2	36	2	2	2	27	.06	.064	2	10	.66	30	.01	12	1.11	.01	.10	1	1460
2+00W OBL	202	233	53	1099	1.5	4	13	2406	7.45	32	5	.3	3	10	2	2	2	93	.39	.164	6	11	2.49	15	.01	3	3.59	.01	.09	1	1960
2+00W 0+50S	35	222	23	1778	.4	3	6	1502	4.28	13	5	ND	2	29	12	2	2	25	1.64	.082	2	8	1.43	26	.01	2	2.27	.01	.10	1	1380
2+00W 1+00S	42	281	45	662	.7	3	10	2661	4.40	17	5	ND	2	52	2	2	2	26	2.85	.126	4	8	1.00	15	.01	8	1.73	.01	.11	1	930
0+00 9+15W	3	26	550	34	54.9	13	87	309	15.72	615	7	ND	1	15	1	2	3	3	.22	.005	2	9	.03	1	.01	10	.15	.01	.10	8	7340
0+00 9+00W	1	10	38	57	1.8	12	7	702	2.68	46	5	ND	1	16	1	2	2	12	.32	.061	8	12	.46	16	.03	2	.57	.02	.13	3	156
0+00 8+50W	1	17	98	159	1.2	4	11	1424	3.93	29	6	ND	3	11	1	2	2	27	.28	.114	7	9	.94	9	.07	2	1.15	.01	.23	6	91
0+00 8+00W	1	45	165	289	2.5	4	9	1077	5.19	69	5	ND	1	50	1	2	2	28	.20	.125	5	10	1.33	7	.01	2	1.46	.01	.19	1	106
0+00 7+50W	10	349	54	147	1.2	18	14	375	3.94	41	5	ND	1	14	1	2	2	16	.06	.046	4	15	1.47	6	.01	5	1.37	.01	.15	1	129
0+00 7+00W	8	163	243	246	2.5	13	6	200	3.76	32	5	ND	1	12	3	3	2	11	.06	.055	2	10	.78	12	.01	12	.84	.01	.14	1	66
0+00 6+50W	2	48	89	9	.8	23	15	15	4.94	15	5	ND	1	6	1	2	2	4	.09	.049	2	1	.02	5	.01	12	.27	.01	.12	1	96
0+00 5+00W	150	188	37	87	.5	15	9	251	3.80	2	5	ND	1	11	1	2	2	13	.09	.054	3	14	1.03	12	.01	2	1.12	.01	.12	1	200
0+00 2+50W	191	96	74	98	.8	9	4	111	1.89	54	5	ND	1	24	1	4	2	4	.01	.009	2	4	.08	15	.01	3	.32	.01	.09	1	141
1+05S 8+08W	5	508	425	57	10.6	7	5	23	16.34	72	7	ND	1	5	1	54	12	2	.04	.021	2	5	.01	1	.01	3	.16	.01	.09	1	320
1+40S 5+20W	6	33	40	116	.5	9	1	314	1.44	2	5	ND	1	74	1	2	3	7	.01	.005	2	14	1.23	25	.01	5	.98	.01	.02	1	43
3+10S 4+70W	10	24	41	16	.5	18	4	29	2.32	6	5	ND	1	20	1	2	2	3	.03	.017	2	4	.07	9	.01	2	.29	.01	.08	1	110
STD C/AU-R	18	58	43	132	6.6	67	30	946	4.11	39	22	7	37	48	19	15	22	58	.48	.094	38	54	.88	175	.06	34	1.94	.06	.14	12	480

MPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
50W 3+00N	56	48	38	14	1.5	6	3	26	2.40	50	5	ND	1	8	1	2	9	5	.05	.039	4	14	.03	61	.01	4	.19	.01	.14	2	34
50W 2+50N	17	45	59	35	1.4	12	4	733	1.86	19	5	ND	1	85	1	2	2	6	1.86	.029	3	6	.09	26	.01	2	.18	.02	.11	1	57
50W 2+00N	2	117	225	208	6.7	3	8	119	7.24	154	5	ND	1	35	2	16	7	9	.17	.047	3	15	.01	6	.01	10	.17	.01	.20	1	440
50W 1+65N	3	1588	5940	5117	41.1	3	6	7665	15.80	185	5	ND	1	102	50	10	11	9	2.88	.043	3	15	.39	1	.01	5	.40	.01	.11	1	1830
50W 1+50N	2	562	199	123	4.5	2	15	492	6.14	56	5	ND	2	35	1	2	5	18	.59	.153	6	11	.15	14	.01	4	.37	.01	.26	1	410
50W 1+00N	2	228	106	159	2.1	5	13	2873	3.67	31	5	ND	2	177	1	2	2	24	2.66	.094	5	10	.74	10	.02	2	.84	.01	.21	1	53
50W 0+50N	1	84	60	96	3.2	3	10	757	3.91	35	5	ND	3	15	1	2	5	26	.25	.107	4	13	.87	10	.01	6	.95	.01	.22	4	116
48W 1+65N	1	10021	5668	3992	82.2	1	11	12290	16.90	409	9	ND	1	291	43	102	15	6	8.06	.048	7	25	.05	1	.01	2	.20	.01	.10	16	1970
55W 2+10N	5	70	180	35	1.1	6	1	51	1.62	58	5	ND	2	96	1	5	2	3	.03	.144	2	4	.01	212	.01	2	.12	.02	.07	1	75
50W 3+00N	2	181	32	18	2.9	6	4	55	2.03	34	5	ND	2	88	1	4	2	9	.05	.063	2	2	.03	27	.01	2	.23	.02	.14	1	260
50W 2+50N	2	795	126	72	5.1	3	14	670	3.48	40	5	ND	2	16	1	2	2	32	.20	.114	5	15	.82	10	.01	2	.83	.01	.20	1	360
50W 2+00N	5	103	253	23	9.7	7	7	26	3.15	64	5	ND	1	25	1	7	5	4	.01	.044	4	3	.01	11	.01	2	.13	.01	.08	1	790
50W 1+50N	2	3244	38	102	4.0	3	13	415	2.29	29	5	ND	2	69	2	2	3	11	.42	.130	3	10	.30	18	.01	4	.40	.01	.24	1	210
50W 1+13N	3	655	46	30	3.0	12	3	22	1.54	16	5	ND	1	57	1	2	5	3	.07	.033	2	6	.02	24	.01	2	.19	.02	.09	1	169
50W 1+00N	3	623	17	83	.9	4	11	430	3.38	38	5	ND	2	22	1	2	2	22	.32	.126	7	12	.59	20	.01	4	.61	.01	.23	1	210
50W 0+50N	3	63	65	105	1.1	28	15	109	4.40	10	5	ND	1	11	2	2	2	2	.03	.021	2	4	.01	7	.01	33	.13	.01	.06	1	53
0W 1+90N	2	218	142	64	6.3	6	8	104	2.85	19	5	ND	2	44	1	2	2	3	.19	.065	4	35	.01	13	.01	2	.12	.04	.04	1	400
0W 1+50N	3	28	32	26	1.4	8	2	27	2.11	10	5	ND	1	160	1	2	2	2	.01	.025	2	3	.01	14	.01	2	.10	.01	.07	1	97
15W 0+40N	1	63	298	325	2.2	29	20	27	12.66	53	5	ND	1	23	4	5	2	5	.03	.017	2	30	.09	2	.01	5	.36	.01	.08	1	79
75W 0+25N	101	200	204	3693	5.7	9	6	28	3.26	25	5	ND	1	81	75	8	2	2	.01	.034	2	4	.01	9	.01	4	.10	.01	.03	1	320
0W 2+60AS	3	45	71	36	.9	13	16	26	4.39	48	5	ND	1	30	1	2	2	6	.02	.038	3	23	.02	7	.01	3	.26	.01	.12	1	73
5W 3+10S	87	39	71	244	1.3	23	14	15	5.72	7	5	ND	1	16	6	2	2	4	.06	.046	2	4	.03	4	.01	2	.28	.01	.11	1	66
0W 3+60S	91	92	147	39	1.0	27	19	14	5.08	26	5	ND	2	22	2	2	2	3	.01	.023	3	20	.03	7	.01	4	.26	.01	.14	1	144
0W 3+80S	11	155	37	45	.8	32	10	96	5.39	61	5	ND	2	34	1	2	2	8	.11	.239	3	11	.51	10	.01	2	.71	.01	.17	1	75
0W 3+60S	14	39	43	19	1.0	9	6	11	2.94	9	5	ND	1	10	1	2	2	2	.01	.004	3	24	.02	11	.01	2	.23	.01	.13	1	31
0W 1+45S	159	145	60	34	1.6	24	19	31	8.62	65	5	ND	1	14	1	7	2	2	.02	.012	2	5	.05	3	.01	3	.22	.01	.10	1	330
5W 4+30S	3	19	16	31	.2	11	6	75	3.39	4	5	ND	1	13	1	2	2	7	.04	.032	2	22	.49	8	.01	2	.59	.02	.11	1	30
5W 3+00N	6	19	27	9	.7	11	11	28	8.17	24	5	ND	1	1	1	2	2	1	.01	.001	2	3	.01	6	.01	21	.09	.01	.04	1	250
5W 4+50S	5	46	31	40	.2	24	18	84	4.40	15	5	ND	5	8	1	2	2	7	.15	.081	2	10	.47	10	.01	4	.74	.02	.16	1	220
5W 4+75S	86	40	37	20	.2	14	9	33	3.36	8	5	ND	1	12	1	2	2	3	.06	.027	2	3	.13	9	.01	2	.35	.01	.11	1	290
5W 5+00S	3	43	3	11	.6	17	11	6	3.62	12	5	ND	3	8	1	7	2	3	.02	.021	2	13	.01	14	.01	2	.25	.01	.12	1	57
0W 3+25S	82	96	61	35	4.3	17	15	101	7.71	272	5	ND	1	38	1	20	2	7	.04	.028	2	7	.34	4	.01	3	.46	.01	.11	1	610
0W 5+00S	79	272	33	63	.7	11	9	98	5.50	40	5	ND	2	21	1	2	2	9	.08	.119	3	26	.38	18	.01	2	.65	.01	.15	1	210
0W 1+80S	83	64	41	21	.7	11	7	20	3.56	11	5	ND	1	7	1	2	2	3	.04	.024	2	2	.04	10	.01	5	.25	.01	.11	1	155
5W 1+10S	316	497	40	11	.9	11	10	13	3.93	6	5	ND	2	16	1	2	5	4	.05	.048	2	18	.01	15	.01	2	.32	.01	.13	1	220
5W 0+75S	8525	352	167	584	2.3	24	12	39	5.41	87	14	ND	1	21	5	2	27	13	.01	.017	2	9	.11	5	.01	4	.45	.01	.11	1	690
C/AU-R	18	58	42	132	7.2	67	30	945	4.07	39	17	7	37	47	18	16	21	57	.48	.092	38	55	.91	175	.05	34	1.94	.06	.14	12	520

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
3+80W 1+90S	3114	108	159	33	.5	17	8	30	4.42	2	5	ND	2	13	1	6	2	2	.01	.008	2	12	.02	9	.01	2	.13	.01	.05	1	280
3+75W 5+00S	96	79	30	21	.2	15	8	21	3.17	21	5	ND	2	12	1	6	2	5	.02	.029	5	4	.09	11	.01	2	.37	.01	.23	2	110
3+75W 5+25S	183	129	49	71	.1	18	7	94	3.30	18	5	ND	2	14	1	4	2	9	.06	.035	4	9	.44	12	.01	2	.63	.01	.20	2	190
3+75W 5+50S	29	114	90	28	.1	27	7	27	3.24	40	6	ND	2	12	1	7	2	5	.06	.037	4	8	.08	10	.01	2	.36	.01	.20	3	88
3+65W 2+75S	16	19	924	15	.5	12	1	30	.45	6	5	ND	1	97	1	17	2	2	.01	.003	2	11	.01	371	.01	3	.18	.01	.10	2	54
3+55W 2+75S	14	36	80	1010	.4	11	5	14	2.93	14	5	ND	1	253	19	6	2	2	.03	.018	2	4	.03	9	.01	2	.19	.01	.13	1	51
3+50W OBL	1062	640	79	31	1.6	6	7	18	3.40	2	5	ND	2	24	1	2	3	5	.14	.068	2	3	.07	8	.01	2	.44	.01	.16	1	490
3+50W 2+75S	2008	154	101	58	.2	25	11	19	4.11	10	5	ND	1	11	1	18	2	3	.01	.028	2	6	.02	6	.01	2	.28	.01	.16	1	340
3+50W 3+00S	233	153	88	141	.3	16	10	25	4.72	30	5	ND	1	7	1	38	2	5	.09	.043	2	6	.04	7	.01	2	.39	.01	.20	1	340
3+50W 3+25S	207	67	146	115	.4	26	11	14	7.50	16	5	ND	3	5	1	7	2	4	.04	.043	2	5	.04	5	.01	2	.35	.01	.18	1	178
3+50W 3+65S	12	80	204	30	5.8	18	4	38	18.18	778	5	ND	3	31	1	48	2	4	.01	.015	3	6	.09	2	.01	2	.22	.01	.11	2	860
3+50W 3+75S	44	118	64	209	.3	22	13	155	4.41	18	6	ND	3	18	5	4	2	10	.20	.081	5	8	.58	7	.01	6	.77	.01	.28	1	360
3+45W-5+60S	11	195	18	141	.1	30	11	521	5.35	17	5	ND	3	29	1	2	2	41	.38	.093	5	18	2.30	8	.01	2	2.21	.02	.19	1	430
3+35W 5+53S	106	92	37	25	.3	19	11	34	5.76	20	5	ND	2	79	1	4	2	4	.07	.044	2	4	.13	4	.01	2	.42	.01	.23	1	155
3+35W 5+60S	370	248	34	30	.2	20	10	314	3.92	3	5	ND	1	14	1	2	2	5	.50	.028	3	8	.19	11	.01	2	.43	.01	.22	1	195
3+25W 1+50N	85	275	34	212	.3	68	17	107	5.94	155	5	ND	2	10	1	2	2	7	.49	.199	3	6	.07	7	.01	3	.49	.01	.18	1	820
3+20W 3+70S	14	119	186	272	1.8	8	2	21	2.19	65	5	ND	1	279	4	11	3	2	.02	.024	2	5	.03	11	.01	2	.16	.01	.11	1	93
3+18W 3+50S	17	25	440	781	.3	5	2	14	1.11	10	5	ND	1	508	13	4	2	1	.01	.017	2	3	.02	27	.01	2	.09	.01	.06	1	27
3+17W 3+50S	11	67	96	76	.2	18	9	26	4.86	18	5	ND	1	24	1	6	2	4	.04	.020	2	7	.05	5	.01	4	.32	.01	.19	1	110
3+17W 3+75S	11	552	20766	72066	11.1	5	4	21	2.66	76	5	ND	1	126	1540	34	2	2	.02	.018	2	26	.05	5	.01	3	.14	.01	.06	1	1610
2+65W 2+75S	42	56	66	45	.1	12	5	16	2.98	55	5	ND	1	8	1	5	2	4	.01	.009	3	5	.04	9	.01	2	.31	.01	.18	1	99
2+60W 3+00S	68	228	168	315	.3	15	5	74	2.67	34	5	ND	1	74	7	7	2	4	.07	.036	3	8	.07	9	.01	2	.27	.01	.13	1	124
2+60W 3+35S	381	42	13	14	.1	13	4	15	1.68	3	5	ND	1	53	1	2	3	3	.01	.007	7	5	.02	14	.01	2	.25	.01	.15	1	113
2+60W 3+75S	48	410	39	70	.5	21	11	244	5.13	27	5	ND	2	24	1	2	2	10	.33	.058	8	8	.53	5	.01	2	.74	.01	.23	1	240
1+70W 1+65S	70	103	53	95	.5	3	3	85	4.51	81	5	ND	2	12	1	10	2	7	.03	.061	7	3	.19	38	.01	2	.47	.02	.15	1	740
1+70W 1+75S	91	90	40	132	.2	4	3	161	4.60	41	5	ND	2	22	1	6	2	6	.05	.073	7	4	.13	41	.01	2	.43	.02	.12	1	520
1+50W OBL	25	122	69	219	3.4	4	6	209	5.17	84	5	ND	2	34	1	7	2	9	.19	.076	2	3	.40	5	.01	2	.76	.01	.18	1	930
1+20W 2+00S	70	271	29	542	.3	5	12	1326	3.78	75	5	ND	1	22	7	38	2	7	1.63	.090	4	3	.21	8	.01	2	.53	.01	.21	1	1780
1+00W 4+50N	143	62	20	20	.5	8	1	35	1.90	5	5	ND	1	45	1	2	3	4	.01	.004	2	8	.02	597	.01	2	.24	.01	.10	1	350
1+00W 4+00N	142	73	38	10	1.8	4	1	23	2.01	9	5	ND	1	9	1	2	2	4	.01	.016	2	5	.01	340	.01	3	.24	.01	.12	1	250
1+00W 3+50N	126	87	63	7	2.1	6	1	16	2.54	9	5	ND	1	9	1	2	2	5	.01	.019	2	6	.01	247	.01	4	.23	.01	.11	1	390
1+00W 3+00N	151	355	99	124	3.0	29	9	33	4.27	7	5	ND	1	7	1	2	3	8	.07	.037	2	6	.10	10	.01	2	.43	.01	.11	1	940
1+00W 2+50N	160	64	29	24	1.7	6	1	24	1.82	2	5	ND	1	12	1	2	2	6	.01	.044	2	5	.03	64	.01	2	.24	.01	.11	1	450
1+00W 2+00N	129	318	267	357	2.1	14	12	102	3.29	2	5	ND	1	9	2	2	2	7	.10	.074	2	7	.14	21	.01	2	.52	.01	.13	1	1290
1+00W 2+00S	141	239	30	860	.1	3	9	2799	5.35	69	5	ND	1	21	7	12	2	27	.82	.097	6	2	1.15	13	.01	2	1.89	.02	.13	1	2430
1+00W 2+20S	47	33	54	75	1.8	2	2	200	1.60	52	5	2	2	15	1	20	2	6	.10	.064	11	2	.06	151	.01	3	.39	.01	.18	1	4060
STD C/AU-R	18	59	40	134	6.8	67	30	988	4.26	39	22	6	35	48	19	15	21	60	.47	.095	38	56	.93	170	.05	35	1.93	.06	.13	13	530

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
1+00W 1+50N	140	210	138	82	1.6	9	3	28	4.28	19	5	ND	1	50	1	2	7	4	.04	.105	2	7	.01	18	.01	2	.25	.01	.14	2	350
1+00W 1+50S	157	101	82	162	1.9	2	1	265	6.58	117	5	3	3	66	1	39	4	17	.03	.141	20	3	.50	62	.01	2	.74	.02	.22	1	2090
1+00W 1+00N	87	90	53	90	2.6	7	3	65	2.86	18	5	ND	2	8	1	2	2	6	.01	.022	2	5	.07	38	.01	4	.42	.01	.13	2	420
1+00W 1+00S	200	292	95	2690	2.7	5	9	2077	4.44	110	5	ND	2	67	31	29	5	12	1.82	.085	4	4	.48	5	.01	8	.85	.02	.21	1	1450
1+00W 0+50N	305	340	65	411	2.3	7	8	1029	4.38	46	5	ND	3	29	2	3	2	36	.16	.096	3	8	1.07	11	.01	3	1.58	.01	.18	1	1330
1+00W 0+50S	225	305	50	900	2.0	4	9	1692	4.45	127	5	2	2	20	9	28	4	9	1.04	.097	4	3	.41	7	.01	2	.75	.02	.21	1	1860
1+00W OBL	312	100	60	72	2.3	4	1	32	3.74	170	5	2	3	35	1	13	5	12	.01	.045	10	3	.05	81	.01	6	.45	.01	.19	2	2050
0+85W 2+30S	67	269	28	323	1.7	6	14	843	4.89	122	5	2	3	15	1	40	2	25	.26	.113	4	5	1.11	6	.01	2	1.45	.01	.24	1	1460
0+65W 3+20S	133	218	27	126	.8	6	5	427	3.04	19	5	2	4	41	1	2	2	37	.21	.102	4	9	1.38	15	.01	3	1.51	.02	.20	1	1200
0+65W 3+25S	176	108	40	211	2.0	6	10	788	3.75	22	5	ND	4	44	1	2	2	50	.17	.093	5	10	2.41	18	.01	3	2.52	.01	.25	1	1130
0+60W 3+20S	82	215	41	267	.4	6	9	805	3.95	23	5	ND	4	17	1	2	2	68	.21	.102	4	12	2.39	20	.01	2	2.36	.02	.17	1	1100
0+60W 3+25S	121	276	38	310	.6	7	14	991	5.74	20	5	2	4	48	1	3	2	46	.34	.111	5	10	3.04	8	.01	2	3.10	.01	.18	1	1210
0+50W OBL	97	400	50	681	2.1	4	6	443	4.21	128	5	3	2	43	5	8	2	23	.12	.076	3	3	.92	9	.01	4	1.65	.01	.15	1	2150
0+50W 2+00S	29	88	64	1737	.7	22	11	1813	6.66	587	5	4	2	45	17	13	4	45	1.50	.116	5	40	1.51	10	.07	7	1.90	.04	.19	1	3740
0+50W 3+20S	58	151	26	306	.4	7	4	1001	5.06	12	5	ND	4	42	1	2	2	70	.14	.136	9	16	2.73	923	.01	2	3.36	.01	.13	1	1030
0+45W 3+20S	83	131	61	95	.2	7	10	328	4.02	27	5	ND	3	78	2	2	2	8	.21	.094	6	4	.23	8	.01	2	.57	.01	.22	1	490
0+45W 3+30S	81	127	22	341	.5	7	4	923	4.14	17	5	2	3	27	1	3	2	55	.12	.094	13	10	3.26	322	.01	3	3.38	.01	.15	1	1600
0+00 4+50N	41	85	45	13	2.1	7	1	29	1.89	9	5	ND	1	14	1	2	4	6	.01	.022	2	6	.02	288	.01	2	.25	.01	.12	1	600
0+00 4+00N	67	80	66	58	3.4	9	1	30	1.49	10	5	ND	1	32	1	7	3	5	.01	.005	2	9	.03	639	.01	2	.26	.01	.15	2	370
0+00 3+50N	102	70	117	124	2.0	8	1	27	.92	22	5	ND	1	30	1	2	2	6	.01	.021	2	8	.01	374	.01	11	.17	.01	.10	1	350
0+00 3+00N	86	228	70	87	1.8	10	5	32	3.18	14	5	ND	1	16	1	2	2	3	.01	.012	2	7	.01	10	.01	7	.16	.01	.11	1	350
0+00 2+50N	182	96	37	15	3.1	8	2	18	2.15	27	5	ND	1	19	1	22	2	4	.01	.006	2	7	.01	37	.01	2	.25	.01	.14	2	310
0+00 2+00N	116	135	32	16	1.8	8	1	21	3.38	9	5	ND	1	48	1	2	3	6	.01	.015	2	9	.01	621	.01	2	.31	.01	.17	2	490
0+00 1+50N	44	12	88	53	2.1	4	1	13	.46	2	5	ND	1	32	1	2	2	7	.01	.007	2	4	.02	710	.01	2	.28	.01	.13	1	530
0+00 1+00N	62	53	32	158	1.3	6	3	156	4.00*	13	5	ND	2	82	1	2	3	18	.01	.062	2	5	.24	17	.01	2	.59	.01	.10	1	580
0+00 0+50N	92	196	40	509	1.9	5	3	599	4.77	21	5	2	3	38	1	2	2	50	.09	.109	5	11	1.66	54	.01	2	2.45	.01	.14	1	1230
0+00 0+00S	170	162	50	175	2.6	5	7	134	4.51	75	5	2	2	14	1	10	2	9	.08	.074	2	4	.18	9	.01	2	.56	.01	.17	1	1760
0+00 0+50S	801	96	102	365	2.5	4	2	96	3.15	76	5	ND	1	33	4	26	6	5	.09	.084	10	3	.10	24	.01	2	.41	.01	.18	1	980
0+00 1+00S	128	88	34	742	.4	3	5	3424	4.41	60	5	ND	2	23	6	20	2	20	1.05	.112	6	3	1.36	17	.01	2	1.64	.01	.19	1	1420
0+00 1+50S	156	51	71	84	1.8	5	2	388	2.45	31	5	ND	1	14	1	27	2	14	.11	.094	7	5	.40	36	.01	3	.69	.01	.23	1	1300
0+00 1+80S	51	63	63	194	.2	4	9	859	5.32	23	5	ND	1	15	3	13	2	13	.65	.101	6	3	.55	7	.01	2	.83	.01	.22	1	690
1+00E 4+50N	66	53	16	15	1.3	5	1	16	1.86	8	5	ND	1	48	1	2	4	3	.01	.003	2	5	.01	668	.01	7	.21	.01	.11	1	270
1+00E 4+00N	78	50	44	20	3.3	5	3	14	1.85	8	5	ND	1	18	1	30	4	5	.01	.003	2	4	.01	19	.01	2	.29	.01	.14	2	350
1+00E 3+50N	66	63	15	11	.7	6	2	23	1.74	13	5	ND	1	37	1	18	2	7	.01	.004	2	6	.01	1016	.01	2	.22	.01	.11	1	370
1+00E 3+00N	78	53	25	18	1.4	7	1	22	1.24	30	5	ND	1	61	1	32	2	4	.01	.010	2	7	.01	800	.01	2	.17	.01	.09	1	360
1+00E 2+50N	148	55	20	22	1.9	5	1	19	1.33	2	5	ND	1	31	1	2	2	3	.01	.005	2	5	.01	70	.01	8	.20	.01	.11	1	570
STD C/AU-R	18	60	39	132	7.1	68	30	939	3.88	43	21	7	37	47	18	15	19	59	.45	.094	37	55	.91	175	.05	34	1.86	.06	.14	12	480

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
1+00E 2+00N	149	94	8	80	1.2	7	2	18	1.78	10	5	ND	1	25	1	7	2	4	.01	.005	2	8	.01	283	.01	4	.17	.01	.08	1	400
1+00E 1+50N	103	35	149	60	2.1	6	2	17	1.57	8	5	ND	1	39	1	2	4	6	.01	.041	2	7	.01	702	.01	2	.30	.01	.15	1	390
1+00E 0+50S	209	86	33	594	1.2	4	3	1269	3.87	83	5	2	4	7	3	17	2	50	.12	.093	6	12	1.44	234	.01	3	1.72	.01	.13	1	2070
1+00E 1+00S	42	249	36	769	2.2	7	15	2618	5.08	97	8	3	7	12	4	49	10	57	.43	.115	6	12	2.01	52	.01	4	2.62	.01	.13	1	2100
1+00E 1+50S	103	67	53	634	1.2	4	6	1906	4.30	205	5	3	3	12	5	21	8	39	.33	.121	9	6	1.00	29	.01	11	1.36	.01	.12	1	2200
1+00E 1+55S	84	58	29	817	.6	4	7	4506	3.76	34	5	ND	3	37	7	11	2	58	2.34	.111	7	8	1.70	71	.01	2	2.27	.01	.14	1	670
STD C/AU-R	18	61	42	131	7.0	68	31	1022	3.97	41	22	8	40	49	19	16	21	60	.50	.091	40	55	.89	174	.06	35	2.04	.06	.14	13	510

Assay Recommened for Cu, Pb, Zn > 1%
Ag > 30 ppm

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: ROCK AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

DATE RECEIVED: OCT 3 1989 DATE REPORT MAILED: Oct 11/89 SIGNED BY. C. Leong .D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

Corona Corporation PROJECT 1014 File # 89-4062

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
8+20W 2+00N	12	32	63	51	2.8	21	9	187	8.73	140	5	ND	2	17	1	2	6	8	.38	.017	2	16	.03	2	.01	4	.23	.02	.16	3	370
8+15W 1+45N	138	220	97	243	2.4	9	24	259	7.64	123	6	ND	1	30	2	2	2	4	.43	.018	2	4	.02	1	.01	2	.20	.01	.14	1	310
8+00W 1+75N	4	130	416	706	2.1	36	32	1025	6.15	107	5	ND	3	37	5	8	2	27	.96	.077	4	20	.59	7	.01	2	.69	.02	.24	3	360
7+85W 1+50N	11	3773	617	2521	36.5 ✓	10	16	585	11.31	925	5	2	3	75	28	138	5	7	.64	.031	3	3	.04	3	.01	3	.19	.01	.14	1	1710
7+75W 2+05N	2	41	172	390	1.9	25	13	361	4.11	92	5	ND	2	28	3	2	2	8	.45	.044	2	13	.11	8	.01	10	.29	.01	.18	2	185
7+70W 1+35N	2	178	93	20	14.5	15	11	16	6.58	58	5	ND	2	14	1	13	2	14	.04	.018	4	5	.01	4	.01	2	.21	.01	.20	1	470
7+50W 1+25N	3	602	78	45	3.0	6	4	416	1.73	17	5	ND	1	31	1	2	2	7	.29	.024	3	19	.04	57	.01	4	.27	.01	.22	1	97
7+35W 1+75N	2	166	1552	1541	118.7 ✓	4	12	18	9.45	150	5	3	3	20	13	14	22	8	.02	.019	3	5	.01	2	.01	4	.18	.01	.18	1	2110
7+35W 1+78N	1	2117	2886	1658	62.4 ✓	5	8	196	7.84	918	5	3	3	58	19	66	18	10	.37	.101	4	14	.03	6	.01	3	.23	.01	.18	1	2430
7+35W 2+40N	2	877	1357	5796	16.5	3	7	18	7.15	387	5	ND	3	22	53	117	2	9	.01	.011	6	4	.01	2	.01	2	.19	.01	.15	3	133
7+25W 2+25N	1	139	64	87	1.9	2	6	4269	2.87	71	5	ND	1	263	1	15	5	6	2.57	.075	3	40	.05	18	.01	16	.20	.01	.14	1	58
7+10W 1+40N	2	555	301	70	3.8	11	3	1012	1.57	8	5	ND	2	131	1	2	2	8	.57	.054	4	6	.24	59	.01	9	.30	.01	.21	1	132
7+05W 1+25N	3	617	372	92	5.8	20	12	731	4.55	50	5	ND	1	81	1	2	2	18	.50	.071	2	21	.16	9	.01	6	.35	.01	.24	1	400
7+05W 1+55N	1	762	375	426	6.9	3	4	9185	3.08	170	5	ND	2	534	5	40	2	10	4.78	.048	3	5	1.80	12	.01	6	.21	.01	.14	1	124
7+00W 2+10N	3	168	82	20	7.2	2	13	100	10.57	152	5	ND	3	15	1	2	9	9	.14	.062	3	14	.03	3	.01	2	.23	.01	.18	1	570
6+30W 1+15N	5	516	60	50	1.8	3	14	294	3.68	46	5	ND	2	73	1	16	2	17	.36	.117	3	3	.38	4	.01	6	.46	.01	.22	1	74
6+30W 1+16N	4	19	34	8	.3	7	1	74	1.22	29	5	ND	1	167	1	2	2	3	.01	.020	2	8	.01	103	.01	2	.07	.01	.04	1	19
6+30W 1+25N	3	244	22	27	.9	12	5	32	1.86	26	5	ND	1	43	1	2	2	7	.08	.048	3	10	.03	16	.01	3	.22	.02	.16	1	97
6+45W 1+30N	5	1080	51	89	7.6	12	9	141	3.98	160	5	ND	1	31	1	93	2	9	.15	.045	2	5	.10	3	.01	7	.27	.01	.18	1	660
6+10W 0+80N	1	1204	98	206	7.2	22	107	89	14.47	278	5	ND	2	4	2	11	2	24	.11	.045	2	9	1.64	1	.01	4	2.02	.01	.06	1	380
6+00W 1+75N	1	248	29	104	1.0	2	5	157	4.22	43	5	ND	4	34	1	2	2	21	.15	.130	5	2	.29	29	.01	6	.63	.01	.23	1	81
5+25W 0+50N	787	129	127	153	3.3	8	23	21	10.27	82	5	ND	2	55	2	4	2	6	.02	.015	2	4	.08	3	.01	2	.25	.01	.07	1	410
5+70W 3+05S	1	16	63	5	.4	8	5	12	1.88	9	5	ND	1	25	1	2	2	2	.03	.025	2	2	.01	14	.01	4	.25	.01	.14	1	27
5+55W 2+75S	5	4	19	2	.1	2	1	8	.59	6	5	ND	1	13	1	2	2	3	.01	.016	2	5	.01	264	.01	4	.26	.01	.16	1	92
5+12W 2+70S	1	1016	13	256	1.9	27	22	782	10.72	12	5	ND	3	5	1	2	2	57	.46	.187	3	14	2.33	7	.01	6	2.70	.01	.10	1	390
5+00W 3+20S	5	4	13	8	.1	7	1	2	.76	3	5	ND	1	318	1	2	2	1	.01	.030	2	8	.01	36	.01	3	.05	.01	.03	1	25
3+50W 2+45S	44	84	45	24	.4	9	6	13	2.65	13	5	ND	1	17	1	19	2	2	.05	.023	2	4	.04	8	.01	5	.27	.01	.10	1	116
3+50W 2+25S	119	60	40	30	.8	9	5	7	2.24	9	5	ND	1	24	1	18	2	4	.01	.012	2	4	.01	8	.01	5	.23	.01	.12	1	870
3+50W 2+18S	1	68	9	209	.1	66	25	698	4.10	34	5	ND	1	252	1	2	2	84	2.78	.123	6	152	2.74	276	.18	8	2.66	.11	.09	1	12
3+50W 2+00S	134	133	146	126	.6	21	14	59	4.51	40	5	ND	1	7	1	22	2	9	.13	.048	2	8	.11	8	.01	5	.48	.01	.13	1	420
3+50W 1+75S	117	265	219	154	.5	12	11	22	3.67	34	5	ND	1	45	2	2	2	5	.03	.022	2	4	.10	6	.01	3	.36	.01	.10	1	360
3+50W 1+50S	88	166	44	47	.8	17	8	11	3.46	37	5	ND	1	12	1	2	2	4	.02	.030	2	4	.06	9	.01	3	.39	.01	.14	1	700
3+50W 1+25S	216	152	67	59	1.1	59	17	27	6.52	114	5	2	2	5	1	2	2	5	.10	.044	2	3	.05	6	.01	3	.34	.01	.12	1	1030
STD C/AU-R	18	63	36	132	6.7	68	31	1008	4.00	41	24	7	38	48	18	16	22	59	.49	.089	38	56	.89	174	.06	34	1.92	.06	.13	13	520

✓ **ASSAY RECOMMENDED**

ACME ANALYTICAL LABORATORIES LTD.
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE(604)253-3158 FAX(604)253-1716 DATE RECEIVED: OCT 10 1989
DATE REPORT MAILED: Oct. 16/89.

ASSAY CERTIFICATE

AU** BY FIRE ASSAY FROM 1/2 A.T.
- SAMPLE TYPE: ROCK PULP

SIGNED BY C. Leong ... D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

Corona Corporation PROJECT 1014 FILE # 89-4062R

SAMPLE#	Au** OZ/T
7+85W 1+50N	.053
7+35W 1+75N	.075
7+35W 1+78N	.078
3+50W 1+25S	.032

APPENDIX II

DRILL LOGS - DDH 7, 8

DDH-7

Drilled 1968 Granduc Mines Ltd. Depth: 306.32m Collar Elevation: 1590m
Grid: 0+20E/4+00N AZ: 180° Dip: -45°(?)

Interval	Description	Interval	Sample	Au(ppb)	Mo(ppm)
6.10-306.32	qtz stockwork, 20-50% 1-2 cm white qtz veins with minor py, trace mo, cp, in qtz-ser schist	6.10- 9.02m	20501	300	46
		- 12.19	02	320	51
		- 15.54	03	280	81
		- 18.25	04	300	66
		- 21.34	05	300	72
6.10-25.0	20-50% qtz veins	- 24.08	06	200	49
		- 28.04	07	410	58
7.62	ox shear	- 30.18	08	230	71
		- 32.00	09	430	103
23.7-24.08	fault gouge	- 35.05	10	370	103
		- 38.10	11	200	84
25.0-306.32	20-30% qzt veins	- 39.47	12	190	77
		- 42.67	13	320	101
141.73-142.23	fault gouge	- 45.87	14	310	71
		- 49.09	15	390	97
157.58-158.19	fault gouge	- 52.27	16	290	121
		- 55.47	17	370	95
171.0		- 58.52	18	430	66
		99.06-101.19	19	200	122
		95.40- 99.06	20	390	92
306.32	E.O.H.	92.35- 95.40	21	530	95
		89.64- 92.35	22	118	20
		87.19- 89.64	23	640	82
		84.12- 87.19	24	650	61
		80.92- 84.12	25	620	55
		77.60- 80.92	26	290	79
		74.37- 77.60	27	830	73
		71.17- 74.37	28	780	76
		67.97- 71.17	29	640	89
		64.92- 67.97	30	390	96
		61.57- 64.92	31	450	77
		58.52- 61.57	32	500	72
		101.19-109.73	33	430	82
		170.99-174.04	34	530	120
		167.94-170.99	35	1020	101
		164.59-167.94	36	340	113
		161.57-164.59	37	470	107
		158.50-161.57	38	270	107
		155.45-158.50	39	520	108
		152.86-155.45	40	710	75
		148.71-152.86	41	370	71
		145.54-148.71	42	300	65
		141.73-145.54	43	123	68
		138.68-141.73	44	240	85

DDH-7 (Continued)

Interval	Description	Interval	Sample	Au(ppb)	Mo(ppm)
		135.64-138.68m	20545	200	77
		131.98-135.64	46	128	90
		128.93-131.98	47	178	78
		125.88-128.93	48	124	76
		122.22-125.88	49	149	95
		117.65-122.22	50	135	100
		239.57-242.64	51	490	76
		236.52-239.57	52	380	93
		233.48-236.52	53	600	97
		230.43-233.48	54	450	85
		227.38-230.43	55	380	98
		224.33-227.38	56	178	90
		221.28-224.33	57	177	98
		218.24-221.28	58	230	81
		215.18-218.24	59	540	118
		212.14-215.18	60	380	157
		209.09-212.14	61	164	68
		206.04-209.09	62	290	70
		109.73-113.39	63	320	87
		113.39-117.65	64	350	98
		203.00-206.04	65	430	104
		199.95-203.00	66	520	98
		196.90-199.95	67	750	94
		193.85-196.90	68	920	97
		190.80-193.85	69	650	160
		187.76-190.80	70	610	97
		184.71-187.76	71	650	106
		181.66-184.71	72	800	119
		178.61-181.66	73	820	171
		174.04-178.61	74	650	108
		303.28-306.32	75	220	61
		300.23-303.28	76	260	67
		297.48-300.23	77	151	65
		294.44-297.48	78	153	72
		291.39-294.44	79	380	66
		288.34-291.39	80	99	60
		285.29-288.34	81	120	49
		282.24-285.29	82	124	45
		279.20-282.24	83	128	68
		276.15-279.20	84	138	62
		272.80-276.15	85	190	58
		270.05-272.80	86	146	74
		267.00-270.05	87	145	75
		263.96-267.00	88	164	96
		260.91-263.96	89	185	90
		257.86-260.91	90	200	108
		254.81-257.86	91	240	71
		251.76-254.81	92	120	74

DDH-7 (Continued)

Interval	Description	Interval	Sample	Au(ppb)	Mo(ppm)
		248.72-251.76m	20593	380	83
		245.67-248.72	94	850	64
		242.62-245.67	95	760	61

DDH-8

Drilled 1968 Granduc Mines Ltd. Depth: 304.80m Collar Elevation: 1650m
Grid: 0+00W/1+95N AZ: 180° Dip: -45°(?)

Interval	Description
1.21-182.0	light gy ser sch, local massive sections. 1-3% diss, stringer py, local minor mo on fractures & qtz veins. Foliation 70-90° CA
14.6	ox shear
13.59- 26.21	50% recovery, ox shear
30.78	ox shear
27.0-57.0	qtz stockwork; 10-15 veins/m
52.12-62.18	ox shear
171.0	slickensides 45° CA
182.0-304.80	chloritized fragmental andesite - lapilli tuff?; up to 1% diss py, local chl-py veins, 70-80° CA foliation
304.80	E.O.H.

Interval	Sample	Au(ppb)	Mo(ppm)
1.21- 6.06m	20401	1240	72
- 7.92	02	1300	53
- 10.97	03	990	43
- 14.02	04	3490	101
- 15.54	05	660	78
- 18.59	06	870	116
- 22.55	07	450	149
- 26.21	08	610	69
- 29.26	09	150	75
- 32.31	10	200	109
- 35.36	11	450	77
- 38.40	12	500	99
- 41.18	13	750	121
- 44.50	14	350	113
- 47.24	15	380	82
- 49.37	16	280	80
- 52.12	17	320	103
- 57.00	18	300	126
- 62.18	19	380	126
- 65.23	20	370	60
- 67.36	21	690	98
- 70.41	22	370	50
- 73.76	23	510	73
- 76.81	24	480	71
- 79.86	25	420	74
- 82.91	26	380	67
- 85.95	27	430	91
- 89.00	28	780	85
- 92.04	29	620	82
- 95.10	30	510	69
- 98.14	31	590	108
-101.19	32	390	104
-103.63	33	270	115
-106.83	34	520	92
-109.42	35	360	90
-112.57	36	500	80
112.57-115.52	37	350	60
-118.57	38	440	95
-121.77	39	380	110
-124.97	40	400	165
-128.17	41	320	80
-129.23	42	330	86
-132.44	43	124	65
-135.64	44	181	98

DDH-8 (Continued)

Interval	Description	Interval	Sample	Au(ppb)	Mo(ppm)
		135.64-138.84m	20445	210	76
		-140.21	46	157	114
		-143.25	47	132	126
		-146.30	48	270	70
		-149.35	49	290	94
		-152.40	50	310	130
		-155.45	51	480	73
		-158.50	52	163	82
		-161.54	53	153	73
		-164.90	54	430	84
		-167.94	55	380	85
		-171.14	56	410	85
		-174.19	57	340	127
		-177.39	58	340	83
		-180.59	59	230	90
		-183.79	60	470	89
		-186.84	61	700	81
		-189.89	62	720	86
		-192.24	63	710	77
		-197.05	64	710	89
		-200.10	65	270	148
		-203.15	66	220	88
		-206.20	67	720	94
		-209.09	68	1070	92
		-212.14	69	1120	92
		-215.19	70	470	98
		-218.24	71	520	98
		-221.28	72	310	94
		-224.33	73	227	95
		-227.08	74	440	78
		-230.43	75	330	73
		-233.48	76	700	92
		-238.35	77	980	103
		-241.40	78	900	135
		-244.45	79	850	109
		-247.50	80	990	95
		-250.54	81	760	102
		-253.59	82	630	98
		-256.79	83	580	75
		-260.91	84	880	69
		-263.96	85	390	68
		-266.70	86	540	59
		-270.05	87	450	80
		-273.40	88	570	56
		-276.15	89	320	129
		-279.20	90	91	70
		-282.24	91	970	103
		-285.29	92	1090	82

DDH-8 (Continued)

Interval	Description	Interval	Sample	Au(ppb)	Mo(ppm)
		135.64-288.34m	20493	880	129
		-291.38	94	560	127
		-294.43	95	940	129
		-297.48	96	770	136
		-300.53	97	670	134
		-303.58	98	700	75
		-304.80	99	390	67

APPENDIX III

DRILL CORE ANALYSES

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: Core AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

DATE RECEIVED: OCT 3 1989 DATE REPORT MAILED: Oct 11/89 SIGNED BY......D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

Corona Corporation PROJECT 1014 File # 89-4061 Page 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
E 20401	72	658	75	970	2.1	7	13	125	4.76	8	5	ND	1	24	8	2	2	14	.23	.095	2	5	.12	7	.01	5	.47	.01	.07	1	1240
E 20402	53	468	71	1774	2.3	8	11	447	5.09	12	5	ND	1	25	15	2	2	31	.36	.132	2	6	.46	8	.01	6	1.20	.01	.06	1	1300
E 20403	43	488	96	1295	2.2	5	10	175	4.72	8	5	ND	1	35	11	2	2	17	.18	.102	2	3	.17	8	.01	2	.55	.01	.04	1	990
E 20404	101	671	95	1307	3.2	4	14	651	5.92	13	5	3	1	20	9	2	2	39	.16	.086	2	6	.65	8	.01	3	1.73	.01	.04	1	3490
E 20405	78	388	55	1282	1.6	5	10	535	5.90	7	5	ND	1	54	12	2	2	36	.18	.143	2	6	.49	14	.01	4	1.37	.01	.04	1	660
E 20406	116	588	55	667	1.9	7	13	216	4.23	2	5	ND	1	17	6	2	2	17	.11	.081	2	5	.19	10	.01	2	.64	.01	.06	1	870
E 20407	149	130	78	21	1.9	3	4	4	4.39	11	5	ND	1	54	1	2	2	21	.01	.083	2	3	.01	22	.01	2	.14	.01	.12	1	450
E 20408	69	173	20	83	1.6	7	6	13	3.26	6	5	ND	1	17	1	2	2	6	.01	.009	2	4	.01	9	.01	2	.18	.01	.08	1	610
E 20409	75	219	61	66	1.3	8	4	10	1.92	2	5	ND	1	16	1	2	2	2	.01	.008	2	5	.01	18	.01	4	.12	.01	.06	1	150
E 20410	109	93	45	48	1.3	3	3	7	1.01	3	5	ND	1	17	1	2	2	2	.01	.008	2	4	.01	112	.01	3	.08	.01	.05	1	200
E 20411	77	252	50	144	1.1	15	9	5	3.66	11	5	ND	1	10	1	2	2	2	.01	.022	2	3	.01	13	.01	2	.12	.01	.06	1	450
E 20412	99	597	26	290	1.6	17	10	8	4.29	33	5	ND	1	4	2	7	2	2	.03	.019	2	5	.01	7	.01	4	.16	.01	.07	1	500
E 20413	121	857	27	656	1.5	13	9	8	4.03	6	5	ND	1	4	5	2	2	3	.01	.014	2	4	.02	11	.01	2	.16	.01	.05	1	750
E 20414	113	359	22	92	1.1	12	6	4	2.66	3	5	ND	1	8	1	2	2	2	.01	.005	2	4	.01	17	.01	3	.10	.01	.05	1	350
E 20415	82	247	16	23	1.5	12	10	2	3.38	12	5	ND	1	8	1	2	2	1	.01	.007	2	3	.01	13	.01	3	.12	.01	.07	1	380
E 20416	80	75	49	13	1.3	8	3	7	1.30	2	5	ND	1	20	1	2	2	1	.01	.005	2	5	.01	45	.01	2	.11	.01	.06	1	280
E 20417	103	171	8	20	1.5	8	6	6	2.37	11	5	ND	1	8	1	2	2	1	.01	.001	2	4	.01	16	.01	2	.10	.01	.05	1	320
E 20418	126	85	47	22	1.1	1	3	8	6.07	95	5	ND	2	120	1	2	2	14	.01	.166	2	4	.01	103	.01	5	.11	.01	.10	1	300
E 20419	126	218	56	20	.9	3	6	3	5.77	102	5	ND	1	22	1	6	2	4	.01	.039	2	3	.01	11	.01	6	.06	.01	.02	1	380
E 20420	60	593	55	56	1.1	8	12	6	5.87	111	5	ND	1	18	1	6	2	3	.01	.005	2	3	.01	1	.01	3	.07	.01	.02	1	370
E 20421	98	844	116	92	2.0	8	13	13	6.20	158	5	ND	1	194	1	2	2	5	.23	.085	2	2	.01	1	.01	2	.10	.01	.03	1	690
E 20422	50	554	208	62	1.4	9	13	7	5.47	118	5	ND	1	256	1	2	2	3	.24	.090	2	5	.01	5	.01	7	.09	.01	.02	1	370
E 20423	73	460	166	559	1.1	9	12	8	4.41	54	5	ND	1	172	4	2	2	4	.16	.063	2	2	.01	4	.01	3	.06	.01	.01	1	510
E 20424	71	511	151	126	1.6	8	16	11	5.27	13	5	ND	1	149	1	2	2	5	.30	.113	2	3	.01	5	.01	2	.09	.01	.02	1	480
E 20425	74	562	76	92	.8	9	15	10	5.03	53	5	ND	1	81	1	2	2	5	.38	.130	2	3	.01	4	.01	2	.11	.01	.03	1	420
E 20426	67	418	16	235	.9	8	10	10	4.36	61	5	ND	1	75	1	14	2	5	.29	.098	2	2	.01	1	.01	2	.10	.01	.03	1	380
E 20427	91	559	25	436	1.6	7	12	15	4.55	7	5	ND	1	86	3	2	2	7	.33	.103	2	3	.01	7	.01	13	.26	.01	.09	1	430
E 20428	85	520	47	1151	1.7	8	14	372	5.63	11	5	ND	2	26	11	2	2	25	.33	.102	2	5	.50	9	.01	4	1.13	.01	.08	1	780
E 20429	82	484	52	749	2.0	11	11	287	4.94	11	5	ND	2	20	5	2	2	16	.33	.106	2	4	.34	5	.01	8	.76	.01	.08	1	620
E 20430	69	589	49	478	1.2	8	12	328	4.96	10	5	ND	2	18	3	2	2	17	.35	.111	2	4	.40	5	.01	2	.85	.01	.08	1	510
E 20431	108	627	24	485	1.7	9	12	586	4.47	18	5	ND	2	13	2	2	2	22	.26	.083	2	6	.70	12	.01	8	1.28	.01	.07	1	590
E 20432	104	734	105	401	2.1	8	10	157	4.04	15	5	ND	3	13	4	2	2	7	.19	.055	2	4	.19	7	.01	3	.47	.01	.08	1	390
E 20433	115	578	31	202	1.1	7	9	43	3.46	11	5	ND	3	10	1	2	2	3	.14	.045	2	2	.06	11	.01	2	.23	.01	.08	1	270
E 20434	92	1051	69	462	1.3	21	12	97	4.20	18	5	ND	2	10	4	2	2	4	.10	.021	2	6	.03	6	.01	2	.30	.01	.12	1	520
E 20435	90	633	45	629	1.2	12	13	27	3.90	20	5	ND	2	8	4	2	2	3	.06	.011	2	5	.03	7	.01	2	.28	.01	.11	1	360
E 20436	80	547	19	207	1.4	11	12	58	4.99	11	5	ND	2	6	1	2	2	4	.05	.010	2	5	.12	3	.01	2	.41	.01	.11	1	500
STD C/AU-R	17	58	38	132	7.1	68	31	1017	4.00	37	17	6	37	47	17	15	21	56	.49	.081	36	55	.87	174	.06	31	1.90	.06	.14	13	510

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
E 20437	60	574	31	157	1.0	11	13	99	4.34	5	5	ND	1	9	1	2	2	10	.08	.011	2	5	.12	18	.01	7	.46	.01	.12	1	350
E 20438	95	1177	56	195	2.6	8	11	63	3.90	10	5	ND	2	10	2	2	2	6	.07	.011	2	8	.07	16	.01	4	.36	.01	.10	1	440
E 20439	110	954	48	149	1.8	16	10	57	4.64	30	5	ND	1	10	1	4	2	4	.16	.049	2	3	.05	21	.01	12	.31	.01	.12	1	380
E 20440	165	738	38	276	1.8	17	10	124	4.67	32	5	ND	2	13	2	3	2	4	.23	.067	2	19	.07	20	.01	5	.38	.01	.13	1	400
E 20441	80	496	35	155	1.0	15	10	41	3.86	25	5	ND	1	7	1	2	2	3	.14	.046	2	2	.05	30	.01	5	.27	.01	.10	1	320
E 20442	86	729	39	194	1.0	11	8	81	5.67	35	5	ND	1	6	2	2	2	5	.16	.058	2	29	.15	11	.01	2	.42	.01	.10	1	330
E 20443	65	570	52	187	1.3	9	6	92	2.57	129	5	ND	1	8	2	15	2	2	.14	.030	2	36	.06	22	.01	3	.29	.01	.11	1	124
E 20444	98	615	44	126	1.1	16	10	87	3.84	182	5	ND	2	9	1	17	2	2	.17	.053	2	2	.07	18	.01	2	.31	.01	.11	1	181
E 20445	76	582	36	73	1.0	15	8	83	3.75	132	5	ND	2	8	1	10	2	3	.22	.071	2	3	.07	20	.01	2	.34	.01	.13	1	210
E 20446	114	632	28	84	.9	9	5	118	2.92	168	5	ND	1	11	1	8	2	2	.24	.052	2	20	.06	18	.01	2	.27	.01	.11	1	157
E 20447	126	640	30	86	1.1	13	7	126	3.41	176	5	ND	1	11	1	11	2	2	.26	.051	2	3	.06	17	.01	2	.26	.01	.11	1	182
E 20448	70	758	64	492	2.1	9	7	144	4.28	346	5	ND	1	12	4	19	2	2	.32	.054	2	23	.05	16	.01	8	.27	.01	.12	1	270
E 20449	94	467	39	157	1.0	16	9	135	3.93	117	5	ND	2	12	1	3	2	3	.32	.064	2	2	.09	17	.01	2	.32	.01	.12	1	290
E 20450	130	539	45	155	1.1	17	10	97	4.30	75	5	ND	2	12	1	4	2	4	.31	.089	2	22	.08	17	.01	10	.42	.01	.17	1	310
E 20451	73	620	21	97	.7	20	11	76	5.09	18	5	ND	2	9	1	2	2	3	.14	.046	2	3	.12	8	.01	9	.38	.01	.12	1	480
E 20452	82	226	37	60	.6	11	8	67	4.74	93	5	ND	1	10	1	11	2	3	.18	.045	2	18	.03	12	.01	2	.24	.01	.11	2	163
E 20453	73	480	36	67	1.0	10	8	63	3.24	151	5	ND	1	16	1	10	2	2	.16	.037	2	2	.03	17	.01	13	.21	.01	.10	1	153
E 20454	84	525	43	110	.9	12	11	176	4.59	53	5	ND	1	21	1	2	2	4	.30	.050	2	32	.13	8	.01	7	.45	.01	.15	1	430
E 20455	85	318	16	37	.7	14	8	79	4.10	46	5	ND	1	27	1	2	2	7	.26	.058	2	5	.10	9	.01	10	.43	.01	.17	1	380
E 20456	85	444	18	51	.6	15	9	43	3.99	103	5	ND	1	20	1	8	2	6	.19	.051	2	7	.08	9	.01	2	.35	.01	.13	1	410
E 20457	127	449	17	72	.8	14	11	41	4.49	155	5	ND	1	16	1	10	2	4	.22	.078	2	2	.05	8	.01	12	.30	.01	.12	1	
E 20458	83	281	45	54	.7	14	10	65	3.60	97	5	ND	1	44	1	6	2	3	.16	.043	2	6	.06	7	.01	7	.29	.01	.12	1	340
E 20459	90	399	41	90	.9	14	9	82	4.48	148	5	ND	1	17	1	9	2	2	.15	.037	2	1	.08	7	.01	12	.29	.01	.10	1	230
E 20460	89	712	17	225	1.3	21	11	356	4.44	82	5	ND	1	17	3	2	2	5	.46	.051	2	8	.27	11	.01	2	.56	.01	.12	1	470
E 20461	81	474	17	880	.9	16	12	1174	4.01	12	5	ND	2	17	12	2	2	12	.97	.060	3	16	1.31	38	.01	3	1.63	.01	.10	1	700
E 20462	86	438	20	669	1.6	19	13	2008	4.55	19	5	ND	3	31	8	2	2	12	2.43	.087	7	15	1.05	34	.01	5	1.49	.01	.12	1	720
E 20463	77	484	28	525	1.3	20	14	2036	4.65	18	5	ND	2	32	2	2	2	14	2.34	.097	7	17	1.30	38	.01	7	1.76	.01	.11	1	710
E 20464	89	542	42	270	1.5	19	10	1050	5.38	16	5	ND	2	19	1	2	2	9	1.15	.059	5	14	.71	21	.01	5	1.07	.01	.12	1	710
E 20465	148	324	45	80	.8	12	9	295	4.22	59	5	ND	1	11	1	2	2	3	.46	.027	2	2	.04	20	.01	2	.26	.01	.11	1	270
E 20466	88	296	42	81	.8	15	9	133	4.15	92	5	ND	1	11	1	9	2	3	.24	.037	2	2	.01	12	.01	3	.25	.01	.12	1	220
E 20467	94	333	31	262	2.1	22	13	205	5.20	83	5	ND	1	10	2	2	2	4	.30	.071	3	5	.18	27	.01	2	.46	.01	.11	1	720
E 20468	92	603	16	431	1.1	22	13	2459	4.81	22	5	ND	2	38	2	2	2	16	2.78	.074	5	17	1.21	23	.01	2	1.60	.01	.11	1	1070
E 20469	92	617	15	286	1.5	23	14	2617	5.54	13	5	ND	2	44	1	2	2	17	3.47	.083	6	19	1.31	23	.01	2	1.69	.01	.11	1	1120
E 20470	98	548	68	99	2.1	15	11	340	4.90	134	5	ND	1	22	2	2	2	3	.53	.034	2	3	.11	10	.01	2	.35	.01	.13	1	470
E 20471	98	693	46	171	2.3	12	9	559	3.15	255	5	ND	1	30	3	12	2	3	.69	.034	2	5	.32	23	.01	2	.54	.01	.12	1	520
E 20472	94	460	29	107	.7	12	9	416	3.38	169	5	ND	1	25	1	3	2	3	.50	.031	2	7	.29	16	.01	2	.50	.01	.12	1	310
STD C/AU-R	17	59	44	132	6.7	68	30	998	4.19	43	23	7	38	49	18	15	17	58	.48	.095	38	55	.88	172	.06	34	1.92	.06	.13	12	470

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
E 20473	95	593	34	118	.8	12	7	80	3.05	211	5	ND	1	11	1	19	2	2	.18	.031	2	5	.05	16	.01	4	.23	.01	.11	1	227
E 20474	78	546	18	168	.7	17	11	331	3.65	129	5	ND	2	14	1	10	2	5	.34	.061	2	6	.41	12	.01	8	.61	.01	.12	2	440
E 20475	73	504	38	490	.6	19	12	701	3.32	105	5	ND	2	20	8	10	2	8	.79	.061	2	9	.63	17	.01	3	.81	.01	.12	1	330
E 20476	92	386	36	197	.7	11	13	282	3.73	76	5	ND	1	21	1	7	3	7	.52	.082	2	5	.11	8	.01	2	.36	.01	.12	1	700
E 20477	103	335	29	437	.9	7	12	1768	4.12	15	5	ND	3	43	3	2	2	21	2.37	.088	4	6	.81	15	.01	2	1.12	.01	.10	1	980
E 20478	135	399	44	430	1.6	5	12	1948	4.63	24	5	ND	3	39	3	2	2	22	2.59	.088	4	6	1.14	18	.01	11	1.48	.01	.12	1	900
E 20479	109	347	31	404	1.3	7	12	2383	4.07	23	5	ND	4	81	1	2	2	24	3.22	.098	7	9	1.12	19	.01	3	1.39	.01	.11	2	850
E 20480	95	372	39	465	2.1	7	10	1874	3.53	21	5	ND	3	83	4	2	2	34	2.42	.097	6	8	1.28	16	.01	12	1.50	.01	.12	1	990
E 20481	102	335	26	291	1.2	8	10	1453	3.62	14	5	ND	3	156	1	2	2	22	2.37	.101	4	8	1.12	12	.01	5	1.36	.01	.12	1	760
E 20482	98	318	20	669	.9	9	10	1940	3.75	8	5	ND	3	221	7	2	2	32	2.66	.111	7	10	1.54	23	.01	10	2.04	.01	.11	1	630
E 20483	75	296	26	282	1.1	8	9	2286	3.33	12	5	ND	3	106	1	2	2	18	3.97	.094	5	7	.98	13	.01	2	1.08	.01	.11	2	580
E 20484	69	309	36	691	1.3	9	12	1753	3.77	24	5	ND	3	155	8	2	2	30	2.80	.094	8	14	1.27	14	.01	2	1.49	.01	.11	1	880
E 20485	68	212	41	816	1.7	7	13	1641	3.72	19	5	ND	3	182	7	2	2	37	3.12	.099	7	17	1.42	16	.01	2	1.64	.01	.09	1	390
E 20486	59	225	12	478	.7	7	10	1562	3.96	4	5	ND	3	271	4	2	2	37	3.14	.097	6	14	1.53	18	.01	3	2.00	.01	.08	1	540
E 20487	80	229	20	247	.6	10	11	1097	3.79	10	5	ND	4	176	1	2	2	26	2.07	.108	7	9	1.35	16	.01	2	1.64	.01	.13	1	450
E 20488	56	4942	65	130	4.9	12	14	287.	7.91	162	5	ND	3	38	3	37	2	8	.89	.094	9	6	.17	8	.01	9	.44	.01	.14	1	570
E 20489	129	1943	42	112	2.0	12	11	128	5.81	250	5	ND	3	29	2	46	2	6	.56	.086	7	4	.04	4	.01	6	.30	.01	.15	1	320
E 20490	70	146	84	45	.4	15	8	30	4.06	24	5	ND	1	24	1	8	2	5	.25	.046	6	6	.02	3	.01	2	.36	.01	.16	2	91
E 20491	103	241	14	107	.4	9	12	877	4.78	28	5	2	3	41	1	2	2	17	2.04	.098	7	5	.70	11	.01	12	.95	.01	.16	2	970
E 20492	82	336	13	124	.7	7	10	989	3.65	19	5	ND	3	115	1	2	2	35	1.96	.081	6	9	1.23	15	.01	5	1.48	.02	.13	1	1090
E 20493	129	306	18	120	.5	7	11	912	3.72	15	5	ND	3	60	1	2	2	33	1.65	.079	5	9	1.34	23	.01	6	1.59	.01	.12	2	880
E 20494	127	206	21	114	.4	7	11	973	3.90	13	5	ND	3	98	1	2	2	25	2.25	.086	6	7	1.06	10	.01	11	1.30	.01	.12	1	560
E 20495	129	252	10	120	.5	6	11	971*	4.01	10	5	ND	4	51	1	2	3	34	2.09	.082	5	9	1.44	20	.01	5	1.77	.01	.12	1	940
E 20496	136	317	25	172	.7	13	10	775	3.33	31	5	ND	3	29	1	2	2	14	1.80	.065	4	8	1.03	27	.01	2	1.22	.01	.15	1	770
E 20497	134	589	25	181	1.0	10	10	860	3.36	44	5	ND	4	34	1	3	2	16	1.74	.067	5	7	.98	14	.01	10	1.09	.01	.12	1	630
E 20498	75	455	17	218	.7	9	11	1079	3.98	13	5	ND	4	29	1	2	2	29	1.91	.087	8	6	1.38	23	.01	10	1.65	.01	.14	1	700
E 20499	67	319	46	294	.9	15	9	1034	3.50	25	5	ND	3	26	4	2	2	14	1.60	.053	6	10	.91	16	.01	4	1.11	.01	.11	1	390
E 20501	46	1596	54	124	2.0	16	4	29	3.11	2	5	ND	1	29	1	2	2	2	.04	.028	2	7	.01	7	.01	2	.19	.01	.08	1	300
E 20502	51	1422	57	114	2.3	15	12	24	3.50	3	5	ND	1	21	1	2	3	2	.02	.013	2	7	.01	10	.01	2	.18	.01	.08	1	320
E 20503	81	1556	76	125	2.0	20	13	26	4.93	7	5	ND	1	28	1	2	2	3	.04	.030	2	7	.02	5	.01	3	.20	.01	.07	1	280
E 20504	66	1409	53	180	2.6	19	10	20	4.75	2	5	ND	1	24	1	2	2	3	.05	.026	2	7	.01	7	.01	2	.18	.01	.08	1	300
E 20505	72	981	45	117	2.6	20	7	25	2.73	2	5	ND	1	20	1	2	2	2	.01	.018	2	7	.01	14	.01	5	.16	.01	.08	1	300
E 20506	49	350	40	75	2.1	13	3	26	1.81	3	5	ND	1	18	1	2	2	2	.01	.006	2	10	.01	24	.01	2	.14	.01	.08	1	200
E 20507	58	2194	98	774	4.8	12	9	27	4.58	60	5	ND	1	58	7	21	2	4	.14	.063	2	6	.01	7	.01	13	.17	.01	.07	1	410
E 20508	71	1094	34	117	1.6	14	7	25	3.97	11	5	ND	1	22	1	6	2	3	.01	.005	2	10	.01	8	.01	3	.13	.01	.07	1	230
E 20509	103	1364	86	600	4.3	13	8	23	3.86	99	5	ND	1	47	6	46	2	4	.06	.023	2	8	.01	9	.01	2	.17	.01	.07	1	430
STD C/AU-R	17	57	37	132	7.0	67	30	999	3.93	40	18	6	36	44	17	15	16	55	.49	.082	36	55	.87	173	.06	35	1.87	.06	.14	12	480

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
E 20510	103	1863	148	211	2.2	9	9	36	3.87	43	5	ND	1	218	3	17	2	4	.09	.041	2	2	.01	5	.01	3	.17	.01	.06	1	370
E 20511	84	1203	75	247	1.9	10	7	30	3.87	50	5	ND	1	64	4	23	2	4	.07	.039	2	5	.01	4	.01	3	.17	.01	.08	1	200
E 20512	77	1365	46	195	1.9	9	5	30	3.32	54	5	ND	1	55	3	31	2	3	.05	.027	2	4	.01	5	.01	2	.14	.01	.07	1	190
E 20513	101	1764	72	172	3.1	8	10	30	5.31	103	5	ND	1	33	3	54	2	3	.06	.029	2	5	.01	3	.01	2	.15	.01	.07	1	320
E 20514	71	1081	54	260	1.6	7	10	22	4.30	34	5	ND	1	51	3	18	2	2	.04	.021	2	2	.01	4	.01	2	.16	.01	.08	1	310
E 20515	97	1217	64	307	2.1	8	9	24	4.36	71	5	ND	1	53	3	35	3	3	.03	.016	2	4	.01	4	.01	6	.16	.01	.07	1	390
E 20516	121	1064	87	350	1.8	6	9	21	4.13	39	5	ND	1	57	4	21	2	3	.04	.019	2	1	.01	4	.01	3	.17	.01	.07	1	290
E 20517	95	1295	92	310	2.4	6	9	27	4.31	59	5	ND	1	82	3	29	3	3	.05	.023	2	1	.01	4	.01	4	.17	.01	.07	1	370
E 20518	66	1098	132	263	1.9	6	8	21	4.94	18	5	ND	1	87	3	11	2	3	.05	.018	2	2	.01	4	.01	3	.18	.01	.08	1	430
E 20519	122	1126	94	455	2.0	8	8	26	3.82	85	5	ND	1	107	5	32	2	3	.01	.013	2	3	.01	5	.01	2	.15	.01	.07	1	200
E 20520	92	224	49	62	1.8	8	5	16	2.71	13	5	ND	1	42	1	2	3	3	.01	.041	2	5	.01	8	.01	3	.16	.01	.10	1	390
E 20521	95	952	62	115	1.8	10	8	21	3.38	7	5	ND	1	36	2	2	2	3	.01	.016	2	5	.01	6	.01	2	.16	.01	.08	2	530
E 20522	20	246	24	282	.9	64	21	1130	7.30	14	5	ND	1	75	2	2	2	100	.05	.067	2	83	2.56	35	.01	6	5.11	.01	.05	1	118
E 20523	82	983	49	138	1.5	11	10	95	4.27	13	5	ND	1	51	3	2	3	7	.08	.049	2	5	.13	5	.01	2	.46	.01	.11	1	640
E 20524	61	888	61	381	1.4	7	10	45	4.47	16	5	ND	1	117	3	8	4	4	.11	.050	2	3	.04	5	.01	4	.20	.01	.06	1	650
E 20525	55	401	82	139	1.9	6	7	15	3.46	47	5	ND	1	94	2	21	2	4	.01	.034	2	2	.01	6	.01	2	.12	.01	.06	1	620
E 20526	79	864	87	284	2.3	6	9	20	4.28	61	5	ND	1	132	3	17	3	4	.04	.026	2	2	.01	5	.01	2	.23	.01	.10	1	290
E 20527	73	1145	98	361	2.2	5	11	16	4.40	10	5	ND	1	55	3	2	2	2	.03	.030	2	1	.01	4	.01	2	.13	.01	.04	1	830
E 20528	76	1111	78	378	2.1	7	11	39	4.81	14	5	ND	1	66	3	2	3	3	.03	.015	2	1	.01	4	.01	2	.13	.01	.05	1	780
E 20529	89	1072	123	560	2.4	5	11	28	5.10	25	5	ND	1	117	6	5	2	3	.06	.035	2	1	.01	4	.01	2	.15	.01	.06	1	640
E 20530	96	1321	132	422	2.6	7	9	20	4.51	42	5	ND	1	152	5	15	2	4	.04	.024	2	1	.01	4	.01	2	.23	.01	.09	1	390
E 20531	77	1011	97	678	1.9	5	10	20	4.56	6	5	ND	1	80	7	2	2	4	.03	.021	2	1	.02	4	.01	2	.20	.01	.08	1	450
E 20532	72	897	112	638	2.1	6	9	17	4.76	11	5	ND	1	75	6	2	2	4	.02	.013	2	2	.01	4	.01	2	.24	.01	.10	1	500
E 20533	82	806	48	213	1.4	10	11	25	4.55	53	5	ND	1	252	2	13	2	4	.03	.028	2	3	.01	5	.01	2	.14	.01	.07	1	430
E 20534	120	1198	78	316	2.8	23	12	25	4.13	27	5	ND	1	8	3	13	2	3	.08	.034	2	3	.02	14	.01	3	.22	.01	.08	1	530
E 20535	101	1122	45	1169	3.5	35	13	54	4.61	39	5	ND	1	26	10	14	2	2	.07	.024	2	2	.01	7	.01	2	.08	.01	.03	1	1020
E 20536	113	1069	61	185	1.9	29	9	20	4.11	38	5	ND	1	12	2	10	2	3	.05	.017	2	3	.01	7	.01	2	.17	.01	.07	1	340
E 20537	107	1162	89	182	2.4	37	10	18	4.06	33	5	ND	1	96	3	21	2	3	.09	.036	2	2	.01	6	.01	2	.18	.01	.07	1	470
E 20538	107	1086	56	65	1.5	26	9	19	4.01	15	5	ND	1	452	1	8	2	3	.09	.034	2	4	.01	7	.01	2	.22	.01	.10	1	270
E 20539	108	1370	39	90	1.4	21	10	27	3.71	48	5	ND	1	382	1	11	3	3	.07	.026	2	3	.01	7	.01	2	.15	.01	.05	1	520
E 20540	75	960	48	291	2.2	30	11	24	4.12	155	5	ND	1	23	3	22	2	2	.06	.024	2	1	.01	5	.01	7	.09	.01	.03	1	710
E 20541	71	718	38	533	1.6	25	11	13	2.96	146	5	ND	1	10	4	13	2	2	.13	.047	2	1	.01	13	.01	2	.07	.01	.02	1	370
E 20542	65	578	88	100	1.6	19	8	18	3.11	127	5	ND	1	410	1	39	3	2	.20	.079	2	2	.01	7	.01	2	.12	.01	.05	1	300
E 20543	68	447	25	61	1.0	10	8	18	4.07	65	5	ND	1	310	1	66	3	3	.06	.020	2	1	.01	6	.01	2	.13	.01	.06	1	123
E 20544	85	1077	20	105	1.7	15	7	16	3.53	112	5	ND	1	262	2	126	2	4	.05	.016	2	2	.01	6	.01	2	.17	.01	.08	1	240
E 20545	77	1141	52	79	1.5	15	10	15	5.17	94	5	ND	1	251	1	89	2	5	.07	.021	2	4	.01	4	.01	2	.15	.01	.06	1	200
STD C/AU-R	18	60	38	132	6.7	68	30	1022	4.22	36	20	8	38	49	20	15	18	60	.48	.099	39	57	.89	172	.06	35	2.02	.06	.13	13	470

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
E 20546	90	632	39	29	.9	10	9	12	3.96	41	5	ND	1	37	1	17	2	2	.01	.003	2	2	.01	14	.01	2	.09	.01	.02	1	128
E 20547	78	839	25	20	1.6	14	7	26	3.61	11	5	ND	1	28	1	10	2	3	.01	.006	2	4	.01	18	.01	2	.18	.01	.09	1	178
E 20548	76	772	39	17	1.1	13	8	17	3.89	12	5	ND	1	56	1	5	2	2	.04	.013	2	4	.01	11	.01	2	.19	.01	.09	1	124
E 20549	95	650	29	25	.8	12	9	20	3.51	29	5	ND	1	32	1	15	2	4	.01	.004	2	3	.01	13	.01	2	.18	.01	.08	1	149
E 20550	100	81	19	9	.2	6	5	13	2.15	7	5	ND	1	681	1	2	2	2	.09	.042	2	3	.01	30	.01	2	.08	.01	.01	2	135
E 20651	76	793	76	539	1.6	25	8	72	4.07	3	5	ND	1	9	3	3	2	4	.14	.049	2	5	.08	19	.01	3	.37	.01	.13	1	490
E 20652	93	961	64	271	1.4	22	9	76	3.68	4	5	ND	1	7	2	2	2	3	.05	.014	2	4	.09	23	.01	3	.31	.01	.10	1	380
E 20653	97	660	44	1436	2.6	23	14	66	4.30	14	5	ND	1	3	10	2	2	3	.05	.018	2	3	.05	25	.01	2	.29	.01	.10	1	600
E 20654	85	551	68	865	2.4	21	9	40	3.03	14	5	ND	1	4	6	5	2	3	.07	.025	2	3	.01	22	.01	2	.22	.01	.09	1	450
E 20655	98	840	27	189	1.3	15	8	22	2.61	3	5	ND	1	5	2	2	2	2	.08	.028	2	4	.01	31	.01	2	.27	.01	.12	1	380
E 20656	90	799	45	72	1.2	14	8	25	2.42	7	5	ND	1	6	1	5	2	2	.05	.016	2	4	.03	33	.01	2	.27	.01	.11	1	178
E 20657	98	1010	62	139	1.3	14	8	25	2.97	4	5	ND	1	8	1	2	2	2	.11	.035	2	2	.02	26	.01	2	.29	.01	.11	1	177
E 20658	81	832	95	378	1.7	28	12	21	3.96	8	5	ND	1	8	4	2	2	3	.06	.021	2	2	.02	14	.01	2	.26	.01	.12	1	230
E 20659	118	901	64	432	1.7	33	13	34	3.87	5	5	ND	1	9	3	3	2	5	.08	.027	2	2	.04	17	.01	2	.39	.01	.16	1	540
E 20660	157	1073	64	79	2.0	30	13	21	4.57	5	5	ND	1	6	1	2	2	4	.07	.023	2	2	.03	15	.01	2	.29	.01	.12	1	380
E 20661	68	866	50	71	1.7	16	10	21	4.65	30	5	ND	1	10	1	18	2	4	.08	.027	2	2	.03	10	.01	2	.31	.01	.13	1	164
E 20662	70	1218	60	47	1.8	16	12	23	5.67	16	5	ND	1	19	1	8	2	5	.07	.023	2	3	.03	9	.01	2	.30	.01	.13	1	290
E 20663	87	948	30	132	1.7	9	10	26	4.35	19	5	ND	1	132	2	9	2	3	.01	.041	2	4	.01	11	.01	3	.14	.01	.06	1	320
E 20664	98	455	37	143	1.9	11	8	26	3.41	32	5	ND	1	116	2	10	2	4	.01	.036	2	6	.01	11	.01	2	.18	.01	.09	1	350
E 20665	104	1178	53	41	2.2	14	10	28	5.26	25	5	ND	1	8	1	16	2	4	.04	.015	2	3	.02	9	.01	2	.25	.01	.11	1	430
E 20666	98	857	122	360	2.3	19	13	35	5.78	11	5	ND	1	5	3	3	2	4	.05	.016	2	3	.03	12	.01	2	.28	.01	.11	1	520
E 20667	94	953	34	558	2.8	20	12	37	3.78	50	5	ND	1	4	4	44	2	2	.05	.017	2	1	.01	26	.01	4	.22	.01	.10	1	750
E 20668	97	946	61	422	2.3	22	14	42	4.51	16	5	ND	1	5	3	9	2	3	.03	.008	2	3	.01	21	.01	2	.22	.01	.09	1	920
E 20669	160	1056	80	1073	2.5	34	15	33	4.08	12	5	ND	1	4	7	2	2	2	.05	.012	2	3	.01	23	.01	2	.17	.01	.07	1	650
E 20670	97	871	43	1001	2.8	24	12	56	4.04	13	5	ND	1	5	8	2	2	3	.10	.010	2	3	.01	24	.01	3	.19	.01	.08	1	610
E 20671	106	1049	42	599	2.9	29	14	28	3.65	12	5	ND	1	5	4	6	2	4	.04	.016	2	3	.02	30	.01	2	.27	.01	.10	1	650
E 20672	119	1055	64	1132	3.2	35	13	44	3.83	35	5	ND	1	4	9	21	3	3	.05	.012	2	3	.01	23	.01	2	.16	.01	.06	1	800
E 20673	171	1494	63	358	4.3	29	14	24	3.85	50	5	ND	1	4	4	36	2	2	.05	.015	2	3	.01	25	.01	2	.17	.01	.06	1	820
E 20674	108	1213	70	534	3.3	22	14	29	4.33	45	5	ND	1	4	5	30	3	2	.06	.020	2	3	.01	20	.01	2	.15	.01	.06	1	650
E 20675	61	765	166	416	1.6	13	7	200	3.45	7	5	ND	1	7	2	2	2	5	.29	.114	2	9	.24	28	.01	7	.57	.01	.12	1	220
E 20676	67	853	243	424	2.1	11	7	127	3.32	5	5	ND	1	6	2	2	2	3	.23	.087	2	6	.16	27	.01	2	.43	.01	.12	1	260
E 20677	65	932	187	322	1.4	14	7	43	3.23	36	5	ND	1	7	2	9	2	2	.13	.046	2	4	.02	23	.01	4	.23	.01	.11	1	151
E 20678	72	788	45	188	.9	15	7	71	3.39	4	5	ND	1	9	2	2	2	3	.26	.099	2	8	.08	21	.01	2	.38	.01	.15	1	153
E 20679	66	780	25	273	1.0	14	9	280	4.11	7	5	ND	1	7	1	2	2	7	.33	.128	2	10	.43	30	.01	2	.78	.01	.12	1	380
E 20680	60	993	94	251	1.5	15	6	221	3.93	2	5	ND	1	10	1	2	2	5	.29	.111	2	9	.34	22	.01	2	.69	.01	.13	1	99
E 20681	49	956	52	204	1.2	17	8	389	4.92	2	5	ND	1	6	1	2	2	7	.16	.062	2	11	.49	25	.01	2	.95	.01	.12	1	120
STD C/AU-R	17	59	40	132	6.7	64	30	1037	4.11	41	20	7	38	48	18	15	19	58	.48	.095	38	55	.88	176	.06	35	1.92	.06	.13	13	480

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
E 20682	45	875	57	277	1.1	13	8	198	3.97	2	5	ND	1	6	2	2	2	4	.17	.060	2	8	.27	22	.01	3	.54	.01	.09	1	124
E 20683	68	1144	73	294	1.2	16	8	61	4.00	9	5	ND	1	11	2	2	2	3	.25	.087	2	6	.09	17	.01	4	.30	.01	.10	1	128
E 20684	62	1035	48	277	1.1	15	8	61	3.92	12	5	ND	1	9	2	2	2	2	.09	.029	2	5	.06	17	.01	5	.25	.01	.10	1	138
E 20685	58	908	49	486	1.5	15	7	47	3.50	35	5	ND	1	8	2	9	3	2	.06	.017	2	3	.06	18	.01	3	.24	.01	.10	1	190
E 20686	74	1163	62	659	1.3	16	7	49	3.83	14	5	ND	1	7	3	2	3	2	.11	.031	2	6	.04	18	.01	7	.25	.01	.11	1	146
E 20687	75	1021	53	342	1.4	13	6	42	3.16	14	5	ND	1	9	2	3	2	2	.07	.011	2	6	.04	21	.01	4	.22	.01	.10	1	145
E 20688	96	930	51	396	.9	16	7	44	3.58	24	5	ND	1	9	2	8	3	2	.12	.038	2	6	.05	16	.01	5	.25	.01	.10	1	164
E 20689	90	845	66	259	1.2	15	7	73	2.96	7	5	ND	1	7	2	2	2	2	.08	.018	2	4	.06	21	.01	3	.22	.01	.09	1	185
E 20690	108	891	49	454	1.0	18	9	48	3.27	4	5	ND	1	15	3	2	2	3	.09	.020	2	6	.06	18	.01	2	.23	.01	.09	1	200
E 20691	71	836	74	256	1.1	17	6	46	3.23	12	5	ND	1	15	2	2	2	3	.07	.018	2	5	.06	19	.01	4	.26	.01	.10	1	240
E 20692	74	700	105	219	1.4	17	7	38	2.98	10	5	ND	1	21	2	2	2	2	.10	.024	2	6	.04	17	.01	5	.23	.01	.10	1	120
E 20693	83	1216	67	387	2.2	24	10	55	4.32	2	5	ND	1	7	2	2	3	3	.13	.042	2	7	.06	15	.01	3	.28	.01	.11	1	380
E 20694	64	854	35	435	1.6	25	9	155	4.32	7	5	ND	1	6	3	2	2	5	.10	.031	2	8	.15	16	.01	5	.38	.01	.10	1	850
E 20695	61	763	8	412	1.4	34	12	741	5.53	4	5	ND	2	5	1	2	2	17	.20	.079	2	21	.86	27	.01	5	1.51	.01	.11	1	760
STD C/AU-R	17	58	42	134	6.6	67	30	1034	4.13	37	20	7	38	48	18	15	23	58	.48	.093	38	58	.88	174	.06	37	1.92	.06	.13	11	520

ACME ANALYTICAL LABORATORIES LTD.
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE(604)253-3158 FAX(604)253-1716 DATE RECEIVED: OCT 12 1989
DATE REPORT MAILED: Oct. 16/89

ASSAY CERTIFICATE

AU** BY FIRE ASSAY FROM 1/2 A.T.
- SAMPLE TYPE: ROCK PULP

SIGNED BY C. Leong D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

Corona Corporation PROJECT 1014 FILE # 89-4061R

SAMPLE#	Au** OZ/T
E 20401	.039
E 20402	.037
E 20404	.105
E 20468	.030
E 20469	.032
E 20492	.033
E 20535	.036