

$$\begin{array}{r} 180 \\ 46 \\ \hline 1080 \\ 720 \\ \hline 8280 \\ 90 \\ 45 \\ \hline 135 \\ \hline 675 \end{array}$$

Calcs - July 171

801309

Silver Star

$67.5 \times 126' = \frac{8500^D \times 2.4}{10} = 2040$

$2420 @ 0.322 = 780.0 @ 6.90 = 16,700 @ 9.6 = 23,200 @ 9.1 = 22,000$
 $2040 @ 0.344 = 700.0 @ 5.50 = 11,200 @ 5.3 = 10,800 @ 5.6 = 11,420$
 $\frac{4460}{1480} \quad \quad \quad \frac{27,900}{34,000} \quad \quad \quad \frac{33,420}{33,420}$
 $4460 \text{ lbs} @ 0.332 \text{ Au.} \quad 6.3 \text{ Ag.} \quad 7.6 \text{ Pb.} \quad 7.5 \text{ Zn}$

$A-1, 29,120^D \times 2.82 = 82,000$ Consider 30% Wettable = 20% wt. dil.
 $A-2, 12,600^D \times 2.04 = 25,700$
 $A-3, 11,800^D \times 2.86 = 33,800$ 20% wt. dil.
 $B-1, 7,200^D \times 2.5 = 18,000 \rightarrow \frac{12}{9.5} \times 20 = 25\% \text{ vol-dil.}$
 $B-2, 3,400^D \times 2.5 = 8,500$
 $Q, 6,330^D \times 2.52 = 16,000$ or $\frac{12}{9.5} \times 25 = 31.5\% \text{ vol-dil.}$
 $\frac{70,450}{184,000}$

\rightarrow w/d avg. width of a 2.5'
 @ 20% wt. dil'n & 25% vol-dil'n practicable mining width = $2.5' \times 1.25 = 3.12'$

* This mining performance is feasible even if mining to 3.5 - 4.0' widths, if large waste is sorted out at portal.

Dil grade $\approx 0.835 \times$ non dil. grade w. consid. for Au + Ag assoc. w. pyritized walls.

@ 25% wt. dil = 31.5% vol-dil
 \therefore mined width = $2.5' \times 1.315 = 3.3'$

@ 30% vol. dil

Basic premise - expand

A-1 Block, West Sunset, Calc Sheet, July 71

1) Component Sample Areas (draft, raises)

$160 \times 2.28' = 429 \square'$
 $75 \times 3' = 225 \square'$
 ~~$60 \times 2.5' = 138 \square'$~~
 $\frac{130 \times 3.0'}{420} = \frac{390 \square'}{1182}$

→ Avg. width = 2.82' (horiz.) safe

2) Average Grades:

$429 \times 0.524 = 225.0$	$\times 10.77 = 4620$	$\times 13.5 = 5800$	$\times 16.6 = 7130$
$225 \times 0.18 = 40.5$	$\times 6.6 = 1485$	$\times 9.4 = 2115$	$\times 7.9 = 1775$
$138 \times 0.18 = 24.8$	$\times 4.5 = 620$	$\times 5.8 = 800$	$\times 5.7 = 785$
$390 \times 0.10 = 39.0$	$\times 7.8 = 3040$	$\times 8.3 = 3240$	$\times 6.3 = 2460$
<u>1182</u>	<u>329.3</u>	<u>9765</u>	<u>11955</u>
$2.82' @$	0.279	8.25	10.1
	<i>Av</i>	<i>Ag</i>	<i>Pb</i>

Gross Area, A-1 = $\frac{160+188}{2} \times 206 = 32600 \square'$
 Less cut-out = $- 60 \times 58 = - 3480 \square'$
 Net Vert. Area, A-1 = $29120 \square'$

A-1 Tons = $\frac{29,120 \times 2.82'}{9.0} = 9120 \text{ Tons}$

A-2 Block, West Sunset:

1) Component Sample Areas (raises):

$60 \times 2.0' = 120.0$
 $28 \times 2.1' = 58.8$
 $28 \times 2.0' = 56.0$
 $10 \times 2.2' = 22.0$
126

→ Avg width = 2.04' (horiz.) safe

2) Average Grades:

$120.0 \times 0.39 = 46.80$	$\times 6.90 = 826.0$	$\times 11.00 = 1320.0$	$\times 10.80 = 1296.0$
$58.8 \times 0.19 = 11.20$	$\times 6.84 = 402.0$	$\times 6.54 = 384.0$	$\times 5.96 = 351.0$
$56.0 \times 0.37 = 20.70$	$\times 8.50 = 476.0$	$\times 13.20 = 740.0$	$\times 11.70 = 655.0$
$22.0 \times 0.13 = 3.96$	$\times 3.10 = 68.2$	$\times 1.20 = 26.4$	$\times 2.00 = 44.0$
<u>256.8</u>	<u>826.6</u>	<u>1772.2</u>	<u>2470.4</u>
$2.04' @$	0.322	6.9%	9.6%
	<i>Av</i>	<i>Ag</i>	<i>Pb</i>

Net Vert. Area A-2 = $\frac{120+180}{2} \times 84' = 12600 \square'$

A-2 Tons = $\frac{12,600 \times 2.04'}{9.0} = 2850 \text{ Tons}$

A-3 BLOCK, West Sunset

Vert. Area = $\frac{1}{2} (227 \times 104) = 11,800 \square'$

A-3 Tons = $\frac{11,800 \times 2.86}{9.5} = 3550 \text{ Tons}$

B-1 BLOCK - WEST SUNSET

Calc. Sheet July 71

Vert. Area = $90' \times 80' = 7200 \text{ sq}'$ @ avg. width 2.5' (hor.)

$B-1 \text{ Tons} = \frac{7200 \times 2.5}{10} = 1800 \text{ TONS}$

B-2 BLOCK - WEST SUNSET

Vert. Area = $85' \times 40' = 3400 \text{ sq}'$ @ avg. width 2.5' (hor.)

$B-2 \text{ Tons} = \frac{3400 \times 2.5}{10} = 850 \text{ TONS}$

Q - BLOCK, WEST SUNSET:

Vert Area = $96 \times 66' = 6336 \text{ sq}'$ @ avg. hor. width = 2.52' (horiz)

$Q - \text{Tons} = \frac{6336 \times 2.52}{10} = 1600 \text{ TONS}$

Avg grade:

$2.26 \times 0.032 = 0.072 \times 11.60 = 26.20 \times 6.8 = 15.40 \times 5.0 = 11.30$

$2.25 \times 0.260 = 0.585 \times 4.55 = 10.25 \times 5.3 = 11.92 \times 4.7 = 10.60$

$2.17 \times 0.080 = 0.174 \times 0.25 = 0.54 \times 0.3 = 0.65 \times 0.1 = 0.22$

$2.33 \times 0.320 = 0.745 \times 1.80 = 4.19 \times 2.3 = 5.36 \times 6.5 = 15.15$

$\frac{4}{9.01} \quad \frac{1.576}{41.18} \quad \frac{33.33}{37.27}$

2.25' true

Av.

A7

P6

Zm

2.52' horiz @ 0.175

4.57

3.7

4.15

INFERRED - CLASS A - July 171.

$10,000 \times 0.03 = 300$	$\times 6.5 = 60,500$
$2,420 \times 0.322 = 774$	$\times 6.9 = 16,700$
$2,040 \times 0.344 = 700$	$\times 5.5 = 11,220$
$1,800 \times 0.25 = 450$	$\times 10.0 = 18,000$
<hr/> 16,260	<hr/> 106,420
2224	

16,260 Tons @ 0.14

6.55%

John Star - Scranton
Pb.

$\times 4.5 = 40,500$	$\times 1.0 = 10,000$
$\times 9.6 = 23,200$	$\times 9.1 = 22,000$
$\times 5.3 = 10,800$	$\times 5.6 = 11,420$
$\times 10.0 = 18,000$	$\times 8.0 = 14,400$
<hr/> 92,500	<hr/> 57,820

5.7%

3.6%

INFERRED - CLASS B.

$11,500 @ 0.03 = 345$	$@ 6.4 = 73,500$
$7,000 @ 0.06 = 420$	$@ 2.32 = 16,250$
$2,550 @ 0.20 = 510$	$@ 10.0 = 25,500$
<hr/> 21,050	<hr/> 115,250
1275	

21,050 Tons @ 0.065

5.47

$@ 4.6 = 52,800$	$@ 2.8 = 32,200$
$@ 9.1 = 63,700$	$@ 5.1 = 35,750$
$@ 8.0 = 20,400$	$@ 6.0 = 15,300$
<hr/> 136,900	<hr/> 83,250

6.5%

4.0

INDICATED ON Au

16,000 x 0.03 = 480

12,400 x 0.092 = 1142

2,550 x 0.20 = 510

30,950 @ 2132

7.0.069

Au

Order W. Serv. 9,770 x 0.27 = 5,350

Order S. V. Port. 30,950 x 0.069 = 2,132

Total Indic 50,720 @ 7,1482

0.147

Ag

x 6.9 = 110,500

x 3.27 = 40,600

x 10.0 = 25,500

176,600

5.71

Ag

x 7.0 = 138,390

x 5.71 = 176,600

314,990

6.21

Pb

x 5.5 = 88,000

x 9.1 = 112,800

x 8.0 = 20,400

221,200

7.15

Pb

x 8.2 = 162,000

x 7.15 = 221,200

383,200

7.55

Zn July/71

x 1.9 = 30,400

x 5.1 = 63,150

x 6.0 = 15,300

108,850

3.52

Zn

x 8.0 = 158,160

x 3.52 = 108,850

267,010

5.26

57-WEST TRANSFER RAISE :- ASSAY CALCS March 21/70

LOWER SECTION:

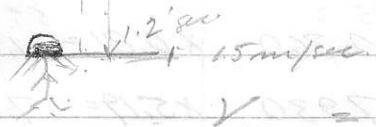
$1.5 \times 0.07 = 0.103$	$\times 0.7 = 1.025$	$\times 0.24 = 0.360$	$\times 0.81 = 1.218$
$1.5 \times 0.16 = 0.240$	$\times 3.1 = 4.650$	$\times 5.32 = 7.930$	$\times 5.19 = 7.700$
$1.5 \times d_0 = 0.240$	$d_0 = 4.650$	$\times d_0 = 7.930$	$\times d_0 = 7.700$
$2.5 \times 0.05 = 0.125$	$\times 6.6 = 15.700$	$\times 6.81 = 17.000$	$\times 3.69 = 9.200$
$2.5 \times d_0 = 0.125$	$\times d_0 = 15.700$	$\times d_0 = 17.000$	$\times d_0 = 9.200$
$2.5 \times 0.13 = 0.325$	$\times 4.5 = 11.250$	$\times 1.62 = 4.050$	$\times 10.98 = 27.500$
$2.0 \times 0.63 = 1.260$	$\times 9.2 = 18.400$	$\times 11.96 = 23.920$	$\times 12.45 = 24.900$
$2.0 \times d_0 = 1.260$	$\times d_0 = 18.400$	$\times d_0 = 23.920$	$\times d_0 = 24.900$
$2.7 \times 0.15 = 0.420$	$\times 3.0 = 8.100$	$\times 5.24 = 14.200$	$\times 4.50 = 12.180$
$2.7 \times d_0 = 0.420$	$\times d_0 = 8.100$	$\times d_0 = 14.200$	$\times d_0 = 12.180$
$3.1 \times 0.05 = 0.153$	$\times 2.9 = 9.000$	$\times 4.70 = 14.600$	$\times 3.54 = 10.500$
$3.1 \times d_0 = 0.153$	$\times d_0 = 9.000$	$\times d_0 = 14.600$	$\times d_0 = 10.500$
$27.6 \times 2.3 = 4.824$	123.975	159.710	157.678
$55' \times 2.3' @ 0.18$ (2.5' / ton)	4.5 g Ag.	5.8	5.7

2.9 m
 0.77 sec
 7.54 m/sec
d = 11.5 metres

$v^2 = 2ab$
 $v = \sqrt{2ab}$

$v^2 = 2ad$

$d = \frac{v^2}{2a} = \frac{225}{19.6} = 1.53$



$V_f = v_i + at$
 $1.2 \text{ sec} = 15 + 9.8(1.2)$

150
 11.80
 3.2

98 | 150
 98
 520
 490
 300

$V_f = at = t = \frac{V_f}{a} = \frac{15}{9.8} = 1.53 \text{ sec}$

2.30
 1.53
 .77

$V_{2.3} = V_0 + at$, $t = 2.3 - 1.53 = 0.77 \text{ sec}$

$v_f = at = 9.8(0.77) = 7.54 \text{ m/sec}$

$d = \frac{1}{2} at^2 = \frac{1}{2}(9.8)(.77)^2$
 $= (4.9)(.593) = 2.9 \text{ metres}$

.77
 .77
 539
 579
 5929

$d_g = 15.5 - 2.9 = 12.6 \text{ metres}$

15.5
 2.9
 12.6

$d = \frac{1}{2} at^2 = \frac{at^2}{2}$

$d = v_i t + \frac{at^2}{2}$

$d = vt$

Let $V_i = 15$, $t =$

$V_{0.77} = 7.54$ for $t = 0.77 \text{ sec}$

1.593
 4.9

$d = \frac{at^2}{2} = \frac{9.8(.593)}{2} = 2.9 \text{ metres}$

5337
 2372
 29057

$d_g = 15.5 - 2.9 = 12.6 \text{ metres}$

15.5
 2.9
 12.6

57-WEST TRANSFER RAISE - ASSAY CALC. MARCH 21/70

UPPER SECTION

$3.1 \times 0.13 = 0.403$	$\times 5.7 = 2.317$	$\times 6.06 = 14.04$	$\times 10.47 = 147.2$
$3.1 \times 0.10 = 0.310$	$\times 5.0 = 1.550$	$\times 10.65 = 16.01$	$\times 6.20 = 99.2$
$3.0 \times 0.10 = 0.300$	$\times 12.7 = 3.810$	$\times 25.13 = 96.39$	$\times 12.50 = 1205.0$
$2.4 \times 0.09 = 0.216$	$\times 22.0 = 4.752$	$\times 14.01 = 66.12$	$\times 28.20 = 1863.6$
$2.7 \times 0.08 = 0.216$	$\times 9.1 = 1.9656$	$\times 9.08 = 19.65$	$\times 16.07 = 315.7$
$2.7 \times 0.17 = 0.460$	$\times 5.9 = 2.713$	$\times 8.59 = 23.30$	$\times 4.73 = 110.3$
$2.4 \times 0.005 = 0.010$	$\times 10.3 = 0.103$	$\times 17.92 = 1.8458$	$\times 6.45 = 11.90$
$2.7 \times 0.10 = 0.270$	$\times 5.7 = 1.539$	$\times 6.79 = 10.39$	$\times 17.81 = 185.0$
$2.6 \times 0.11 = 0.285$	$\times 3.5 = 1.00$	$\times 8.62 = 8.62$	$\times 2.71 = 23.36$
$2.7 \times 0.07 = 0.189$	$\times 2.7 = 0.5103$	$\times 8.69 = 4.46$	$\times 1.16 = 5.17$
$3.0 \times 0.12 = 0.360$	$\times 3.8 = 1.368$	$\times 4.63 = 6.31$	$\times 4.01 = 25.40$
$2.8 \times 0.25 = 0.700$	$\times 1.8 = 1.26$	$\times 5.25 = 6.51$	$\times 0.30 = 1.95$
$2.8 \times 0.09 = 0.252$	$\times 1.4 = 0.3528$	$\times 2.40 = 0.6067$	$\times 0.40 = 0.2421$
$3.1 \times 0.98 = 3.038$	$\times 4.0 = 12.152$	$\times 5.45 = 66.20$	$\times 2.33 = 154.25$
$39.1 = 2.8'$	7.011	255.91	369.83
$75' \times 2.8' @$ (3.0' hor)	0.18	6.6	9.4
			308.04
			7.9

DEVELOP/INDICATED ORE

(A) 5700-5900 BLOCK:

$$\left(\frac{160 + 110}{2} \right) \frac{135^2 \times 250^2 \times 2.61^3}{9.5 \text{ cft}} = 9,200 \text{ tons}$$

as prev. 5900 BLOCK: $145^2 \times 60^2 \times 2.0^3 = 1,830 \text{ tons}$

5700 SILL BLOCK $\frac{16}{2} \left(\frac{105 \times 100 \times 3.03}{10} \right) = 1,590 \text{ tons}$

GROSS 5900-5700 ORE SHOOT = 12,620 tons @ re-eval. grade pending completion 57-1 rec.

(B) 5900 N.E. BLOCK

as prev. - $\frac{100 \times 155 \times 2.5}{10.0} = 3,875 \text{ " as prev. section.}$

(D) S.W. SUNRISE BLOCK

as prev. $\frac{175^2 \times 275^2 \times 2.5^3}{10.0} = 12,000 \text{ " " " "}$

Sub Total, Tunnel-Indicated 28,495 tons* at re-eval. org. grade.

DRILL-INDICATED ORE

(C) ~~SUNRISE~~ BASIN BLOCK

as prev. $\frac{180 \times 170 \times 5.4}{11.0} = 15,000 \text{ tons}$ 26,905
18,750

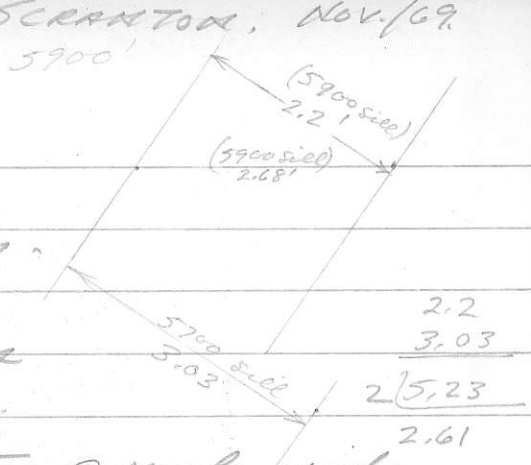
(F) SUNSET DEPTH EXTENSION - sill + drill-indic. 45,165

as prev. $150 \times 100^2 \times 2.5^3 = 3,750 \text{ tons}$ 47,125
1,530

Sub-Total Drill-Indicated - 18,750 tons*

Total, Develop + Drill

Indicated ore - 47,245 tons* ← 44,125 tons
= incr. of 1530 tons
@ normal dilution.



5700 ASSAY CALCULATIONS Oct. 29/69

Main Ore Shoot 57-12.13 ore shoot

July/75

WIDTH	x Au =	x Ag =	x Pb =	x Zn =
1.4	x0.005 = ⁹⁷ 0.007	x0.91 = ¹¹⁸³¹ 1.275	x0.42 = ¹¹⁰⁶ 0.598	x3.29 = 4.61
2.5	x0.04 = 0.100	x0.45 = 1.125	x1.77 = 4.430	x0.64 = ⁸⁸⁵ 1.60
4.3	x0.03 = 0.129	x1.90 = 8.170	x2.05 = 8.800	x5.95 = 25.60
4.0	x0.21 = 0.840	x9.00 = 36.000	x8.59 = 34.360	x7.69 = 30.76
3.0	x0.06 = 0.180	x3.00 = 9.000	x7.42 = 22.260	x4.10 = 12.30
1.7	x0.04 = 0.068	x11.90 = 20.220	x11.03 = 18.780	x3.49 = 5.93
2.0	x0.13 = 0.260	x2.30 = 4.600	x2.82 = 5.640	x1.54 = 3.08
4.7	x0.05 = 0.235	x5.60 = 26.300	x6.59 = 30.950	x2.43 = 11.42
3.4	x0.06 = 0.210	x14.50 = 49.300	x10.59 = 36.000	x3.82 = 13.00
3.4	x0.06 = 0.210	x14.50 = 49.300	x10.59 = 36.000	x3.82 = 13.00
3.0	x0.03 = 0.090	x0.60 = 1.800	x2.11 = 6.330	x0.52 = 1.56
3.8	x0.02 = 0.076	x2.30 = 8.730	x2.67 = 10.150	x0.96 = 3.65
3.6	x0.01 = 0.036	x1.90 = 6.830	x3.74 = 13.470	x0.46 = 1.65
2.2	x0.02 = 0.044	x1.70 = 3.740	x4.19 = 9.220	x1.42 = 9.21
2.0	x0.02 = 0.040	x2.30 = 4.600	x3.85 = 6.700	x2.73 = 5.46
2.3	x0.02 = 0.046	x1.70 = 3.910	x3.38 = 7.770	x1.48 = 3.41
2.3	x0.31 = 0.713	x15.80 = 36.400	x17.24 = 39.700	x16.47 = 37.90
3.0	x0.22 = 0.660	x16.10 = 48.300	x16.59 = 49.700	x18.04 = 54.12
3.2	x0.18 = 0.575	x21.80 = 69.700	x18.81 = 60.400	x21.66 = 69.40
3.2	x0.18 = 0.575	x14.40 = 46.000	x11.98 = 38.400	x15.53 = 49.70
3.0 (20)	x0.13 0.390	x14.40 = 43.200	x21.78 = 65.340	x10.02 = 30.06
60.6	5.483	477.225	504.500	382.81
wt. Avg. 3.03' x 110'	0.09	7.88	8.32	6.32

Nov. 10/69.

5700 WEST.

$3.2' \times 0.04 = 0.128$; $\times 3.4 = 10.87$; $\times 4.83 = 15.60$; $\times 0.71 = 2.27$

$2.3' \times 0.005 = 0.011$; $\times 6.0 = 13.80$; $\times 10.86 = 25.00$; $\times 2.30 = 5.28$

$2.5' \times 0.01 = 0.025$; $\times 2.1 = 5.25$; $\times 2.23 = 5.58$; $\times 0.61 = 1.52$

$2.7' \times 0.02 = 0.054$; $\times 1.9 = 5.13$; $\times 3.82 = 10.30$; $\times 1.11 = 3.00$

10.7	0.218	35.05	56.48	12.07
<u>50' x 2.7' @</u>	0.204			
	Am.	3.3	5.3	1.13
		17.	16.	2m.

$2.0' \times 0.67 = 1.340$; $\times 3.4 = 6.80$; $\times 2.62 = 5.24$; $\times 5.11 = 10.22$

$1.5' \times 0.09 = 0.135$; $\times 2.1 = 3.15$; $\times 1.10 = 1.65$; $\times 0.51 = 0.77$

$2.2' \times 0.44 = 0.968$; $\times 3.0 = 6.60$; $\times 2.06 = 4.53$; $\times 1.82 = 4.00$

$2.1' \times 0.15 = 0.315$; $\times 5.2 = 10.90$; $\times 1.76 = 3.70$; $\times 1.16 = 2.44$

$2.6' \times 0.26 = 0.675$; $\times 11.4 = 29.60$; $\times 13.13 = 34.20$; $\times 15.61 = 40.60$

110.4	3.433	57.05	49.32	58.03
<u>37' x 2.1' @</u>	0.33	5.5	4.73	5.80

Oct. 29/69.

5700 ASSAY CALCULATIONS

57-11 Section

WIDTH'	x Au =	x Ag =	x Pb =	x Zn =
0.9	x 0.22 = 0.198 ³²	x 2.15 = 1.938 ²⁴¹	x 2.15 = 1.938 ²⁵²¹	x 1.70 = 1.53 ³³²
1.0	x 0.38 = 0.380	x 4.35 = 4.350	x 4.35 = 4.350	x 3.95 = 3.95
1.5	x 0.28 = 0.420	x 4.90 = 7.350	x 5.80 = 8.700	x 5.30 = 7.95
1.7	x 0.42 = 0.713	x 14.45 = 24.600	x 14.40 = 24.450	x 21.20 = 36.00
1.6	x 0.41 = 0.656	x 13.50 = 21.600	x 6.75 = 10.800	x 14.70 = 23.50
0.9	x 0.14 = 0.126	x 4.70 = 4.230	x 4.10 = 3.695	x 9.60 = 8.63
1.0	x 0.14 = 0.140	x 4.80 = 4.800	x 10.80 = 10.800	x 7.05 = 7.05
0.8 ⁽⁸⁾	x 0.08 = 0.064	x 1.00 = 0.800	x 3.50 = 2.800	x 1.25 = 1.00
* 9.4	2.697	69.668	67.533	89.61
wt & Avg.	(0.278)	(7.43)	(7.18)	(9.53)
1.2' x 35'	Void .28	7.43	7.2	9.5
Expanded	(0.214)	(5.95)	(5.76)	(7.59)
a) 1.5' x 35'	Void .22	6.0	5.6	7.6
b) <u>or</u>				
2.0' x 35'	Void .107	4.46	(4.31)	(5.72)
	0.17	4.5	4.3	5.7
* Extended Calc. of Section, supplementary to above:				
or down,				
* 9.4 ⁽⁸⁾	2.697	69.668	67.533	89.61
2.0	x 0.730 = 1.460	x 2.10 = 4.200	x 1.980 = 3.960	x 1.06 = 2.12
2.2	x 0.54 = 1.190	x 5.40 = 11.900	x 5.98 = 13.180	x 5.79 = 12.75
2.3	x 0.35 = 0.805	x 8.20 = 18.860	x 7.79 = 17.900	x 12.45 = 28.60
2.3	x 0.04 = 0.092	x 0.60 = 1.380	x 2.25 = 5.170	x 0.68 = 1.56
18.2 ⁽¹²⁾	6.244	106.008	107.743	134.64
Wtd Avg:				
1.515% Au, 0.342% Ag, 5.83% Pb, 5.92% Zn, 7.40%				
Expanded to 2.3' (indicated round width per R. Dealy samples)				
2.3' Au, 0.225% Ag, 3.84% Pb, 3.9% Zn, 4.87%				

Oct. 29/69
SCRANTON 5900 RAISE ASSAY CALC'S.

WIDTH'	X Au =	X Ag =	X Pb =	X Zn =
<u>59-1 RAISE TO CUT-OFF ABOVE CROTCH OF N.E. & S.W. BRANCHES.</u>				
	<u>Au</u>	<u>Ag</u>	<u>Pb</u>	<u>Zn</u>
	<u>6 53</u>	<u>6 3 1</u>	<u>5 5 2</u>	<u>6 4 2</u>
1.7'	x 0.09 = 0.153	x 5.25 = 8.93	x 5.90 = 10.10	x 4.80 = 8.15
2.0	x 0.28 = 0.560	x 9.10 = 18.20	x 8.20 = 16.40	x 4.50 = 9.00
1.9	x 0.73 = 1.388	x 6.0 = 11.40	x 5.50 = 10.45	x 6.80 = 12.92
1.3	x 1.14 = 1.481	x 5.85 = 7.60	x 13.40 = 17.40	x 8.30 = 10.80
0.9	x 0.40 = 0.360	x 10.00 = 9.00	x 14.60 = 13.13	x 8.20 = 7.38
1.8	x 1.06 = 1.910	x 4.65 = 8.37	x 8.10 = 14.60	x 3.80 = 6.85
1.3	x 0.35 = 0.455	x 10.05 = 13.07	x 11.50 = 14.95	x 9.70 = 12.60
2.0	x 0.45 = 0.900	x 8.10 = 16.20	x 11.80 = 23.60	x 13.10 = 26.20
0.8	x 0.22 = 0.176	x 6.65 = 5.32	x 10.05 = 8.05	x 15.20 = 12.18
2.3	x 0.23 = 0.529	x 9.15 = 21.00	x 14.60 = 33.60	x 29.10 = 67.00
1.3	x 0.25 = 0.325	x 12.00 = 15.60	x 42.20 = 54.80	x 12.15 = 15.80
* 3.0 (12)	x 0.31 = 0.930	x 10.00 = 30.00	x 14.35 = 43.05	x 23.80 = 69.00
20.3	9.167	164.69	260.13	257.88
1.7' x 60' @	0.452	8.11	12.9	12.7
2.0 x 60' @	0.39	6.9	11.0	10.8
(* Avg. of 2 drift samples (blank collar of 59-1 raise to complete raise assay section)				
(2.5 x 60' @	0.34	6.10	5.7	9.5

N.E. BRANCH, UPPER SECTION: 59-1 RAISE:

1.0	x 0.48 = 0.480	x 4.75 = 4.75	x 4.80 = 4.80	x 6.15 = 6.15
4.0	x 0.20 = 0.800	x 6.60 = 26.40	x 7.05 = 28.20	(x 6.0 = 24.00)
1.6	x 0.22 = 0.352	x 13.55 = 21.70	x 24.20 = 38.80	x 17.60 = 28.20
1.7	x 0.16 = 0.272	x 6.45 = 10.80	x 6.70 = 11.38	x 5.40 = 9.17
2.2	x 0.14 = 0.308	x 1.45 = 3.19	x 0.88 = 1.94	x 0.75 = 1.65
2.0	x 0.08 = 0.160	x 3.10 = 6.20	x 3.34 = 6.68	x 2.70 = 5.40
12.5 add any.	2.372	73.04	81.80	74.57
2.1 x 28' @	0.19	6.84	6.54	5.96
2.5 x 28' @	0.161	5.8	5.6	5.1

SCRANTON 5900 RAISE ASSAY CALC'S.

59-2 RAISE

WIDTH'	x Au =	x Ag =	x Pb =	x Zn =
² 1.3	x 0.52 = $\frac{5.52}{0.676}$	x 9.10 = $\frac{25.1}{10.83}$	x 11.60 = $\frac{32}{15.10}$	x 10.20 = $\frac{43.1}{13.28}$
1.1	x 0.44 = 0.484	x 7.00 = 7.70	x 13.50 = 14.85	x 11.80 = 12.98
0.5	x 0.40 = 0.200	x 5.75 = 2.38	x 16.60 = 8.30	x 13.80 = 6.90
1.1	x 0.35 = 0.385	x 5.40 = 5.93	x 11.90 = 13.10	x 7.30 = 8.00
1.8	x 0.38 = 0.685	x 19.95 = 35.90	x 17.50 = 31.50	x 18.50 = 33.30
2.3	x 0.37 = 0.850	x 14.60 = 33.60	x 26.26 = 60.50	x 21.40 = 49.20
2.1	x 0.57 = 1.197	x 8.70 = 18.30	x 12.69 = 26.60	x 18.60 = 39.00
2.2(8)	x 0.65 = 1.430	x 9.50 = 20.90	x 18.62 = 41.00	x 10.82 = 23.80
12.4	5.907	135.54	210.95	186.46
1.55' x 45' @	0.477	10.95	17.02	15.04
² 2.0' x 45' @	<u>0.37</u>	<u>8.5</u>	<u>13.2</u>	<u>11.7</u>
² 2.5' x 45' @	0.317	7.3	11.3	10.0