

Sample No.	Hole	Interval	Williams	Loring	Bondar-Clegg	Skyline	sludge
452	16	42-52	<u>.098</u>	<u>.054</u>		<u>.0375</u>	673999 Mt. Haskins 104P/6
485	16	402-412	tr	.023		.0036	
540	18	834-844	<u>.052</u>	<u>.018</u>		<u>.0026</u>	
543	12	165-174	<u>.126</u>	<u>.065</u>		<u>.0575</u>	
544	162	194-204	<u>.071</u>	.042		.026	
552	13	203-209	<u>.080</u>	.065		.047	
553	19	54-64	<u>.113</u>		<u>.264</u>	} 100'	
554	19	64-74	<u>.150</u>		<u>.140</u>		
555	19	74-84	<u>.495</u>		<u>.620</u>		
556	19	84-94	<u>.176</u>		<u>.224</u>		
557	19	94-104	<u>.098</u>		<u>.152</u>		
558	19	104-114	<u>.153</u>		<u>.142</u>		
559	19	114-124	<u>.076</u>		<u>.141</u>		
560	19	124-134	.081		.102		
561	19	134-144	.091		.095		
562	19	144-154	<u>.165</u>		<u>.248</u>		
572	19	239-244	<u>.012</u>		<u>.078</u>		
573	19	244-254	<u>.Tr.</u>		.007		
574	19	254-261	<u>.054</u>		<u>.023</u>		
575	19	261-271	.087		.095		
576	19	271-281	<u>.023</u>		<u>.021</u>		
577	19	281-291	<u>.035</u>		<u>.020</u>		
578	19	291-301	<u>.037</u>		<u>.019</u>		
579	19	301-311	<u>.015</u>		<u>.002</u>		
580	19	311-321	<u>.011</u>		<u>.002</u>		
581	19	321-331	.008		.008		
582	19	331-341	<u>Tr.</u>		<u>.002</u>		
583	19	341-351	<u>Tr.</u>		<u>.009</u>		
584	19	351-361	<u>Tr.</u>		<u>.002</u>		

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Sample No.	Hole	Interval	Williams	Loring	Bondar-Clegg	Skyline	Warnock Hersey
585	19	361-367	Tr.		.003		
586	20	18-28	<u>.098</u>	<u>.062</u>		<u>.052</u>	
587	20	28-38	<u>.078</u>	<u>.054</u>		<u>.047</u>	
588	20	38-48	<u>.109</u>	<u>.010</u>			
589	20	48-58	.067	.042			
590	20	58-68	<u>.087</u>	<u>.054</u>			
591	20	68-78	.170	.179		.165	
592	20	78- 88	<u>.104</u>	<u>.010</u>			
593	20	88-98	<u>.069</u>	.062			
594	20	98-108	<u>.072</u>	<u>.046</u>			
595	20	108-118	<u>.065</u>	<u>.038</u>			
596	20	118-128	<u>.076</u>	.112		.080	
597	20	128-138	.052	.058			
598	20	138-148	.072	.042			
599	20	148-158	.087	.084			
600	20	158-168	<u>.069</u>	.077	.064		
601	20	168-178	.083	.077	.075		
602	20	178-188	.078	.058	.044		
603	20	188-198	<u>.122</u>	<u>.101</u>	<u>.096</u>		
604	20	198-208	<u>.096</u>	<u>.069</u>	<u>.061</u>		
605	20	208-218	<u>.050</u>	<u>.018</u>	<u>.021</u>		<u>.013</u>
606	20	218-228	<u>.063</u>	<u>.018</u>	<u>.019</u>		<u>.010</u>
607	20	228-238	<u>.043</u>	<u>.018</u>	<u>.019</u>		<u>.009</u>
608	20	238-248	.028	.018	.019		
609	20	248-258	.034	.023	.024		
610	20	258-268	.069	.042			
611	20	268-278	.048	.031			
612	20	278-288	<u>.046</u>	<u>.018</u>			
613	20	288-298	<u>.054</u>	<u>.018</u>			

ASSAY RESULTS

No.	H	Interval	Williams	Loring	Bondar-Clegg	No.	H	Interval	Williams	Loring	Bondar-Clegg
452	16	42-52'	.098	.054		608	20	238-248	.028	.018	.019
485	16	402-412'	TR	.023		609	20	248-258	.034	.023	.024
540	18	834-844	.052	.018		610	20	258-268	.069	.042	
543	12	165-174	.126	.065		611	20	268-278	.048	.031	
544	12	194-204	.071	.042		612	20	278-288	.046	.018	
552	13	203'-209'	.080	.065		613	20	288-298	.054	.018	
586	20	18-28	.098	.062		614	20	298-308	.067	.023	
587	20	28-38	.078	.054		615	20	308-318	.089	.027	
588	20	38-48	.109	.010		616	20	318-328	.043	.018	
589	20	48-58	.067	.042		617	20	328-338	.028	.015	
590	20	58-68	.087	.054		618	20	338-348	.045	.015	
591	20	68-78	.170	.179		619	20	348-358	.064	.015	
592	20	78-88	.104	.010		620	20	358-368	.050	.011	
593	20	88-98	.069	.062		621	20	368-378	.045	.015	
594	20	98-108	.072	.046		622	20	378-388	.085	.046	
595	20	108-118	.065	.038		623	20	388-398	.076	.027	
596	20	118-128	.076	.112		624	20	398-408	.069	.133	
597	20	128-138	.052	.058		625	20	408-418	.063	.069	
598	20	138-148	.072	.042		718	11	24-34	.113	.054	
599	20	148-158	.087	.084		719	11	34-44	.039	.056	
600	20	158-168	.069	.077	.064	723	22	57- 67	.150	.163	
601	20	168-178	.083	.077	.075	725	22	77- 87	.069	.084	
602	20	178-188	.078	.058	.044	728	22	107-117	.037	.073	
603	20	188-198	.122	.101	.096	729	22	117-127	.050	.065	
604	20	198-208	.096	.069	.061	730	22	127-137	.141	.112	
605	20	208-218	.050	.018	.021	732	22	147-157	.078	.084	
606	20	218-228	.063	.018	.019	733	22	157-167	.143	.163	
607	20	228-238	.043	.018	.019						

7 samples Williams .074%
 Loring .055%

Sample No.	Hole	Interval	Williams	Loring	Bondar-Clegg	Skyline
730	22	127-137	.141	.112		
731	22	137-147	.091		.080	
732	22	147-157	.078	.084		
733	22	157-167	.143	.163		
734	22	167-177	.050		.033	
735	22	177-187	.069		.040	
736	22	187-197	.048		.043	
737	22	197-207	.050		.034	
738	22	207-217	.080		.023	
740	22	227-237	.068		.018	
741	22	237-247	.052		.017	
742	22	247-257	.043		.018	
743	22	257-267	.039		.011	
744	22	267-277	.082		.079	
745	22	277-287	.052		.040	

20.11022

Sample No.	Hole	Interval	Williams	Loring	Bondar-Clegg	Skyline*
614	20	298-308	<u>.067</u>	<u>.023</u>		EO Post CARB. THOMPSON.
615	20	308-318	<u>.089</u>	<u>.027</u>		
616	20	318-328	<u>.043</u>	<u>.018</u>		
617	20	328-338	<u>.028</u>	<u>.015</u>		
618	20	338-348	<u>.045</u>	<u>.015</u>		
619	20	348-358	<u>.064</u>	<u>.015</u>		
620	20	358-368	<u>.050</u>	<u>.011</u>		
621	20	368-378	<u>.045</u>	<u>.015</u>		
622	20	378-388	<u>.085</u>	<u>.046</u>		
623	20	388-398	<u>.076</u>	<u>.027</u>		
624	20	398-408	<u>.069</u>	<u>.133</u>		
625	20	408-418	<u>.063</u>	<u>.069</u>		
702	21	15-25	<u>.043</u>		<u>.028</u>	
704	21	35-45	<u>.028</u>		<u>.020</u>	
706	21	55-65	<u>.034</u>		<u>.026</u>	
708	21	75-85	<u>.028</u>		<u>.017</u>	
710	21	95-105	<u>.030</u>		<u>.016</u>	
718	//	24-34	<u>.113</u>	<u>.054</u>		
719	//	34-44	<u>.039</u>	<u>.056</u>		
720	22	27-37	<u>.067</u>		<u>.133</u>	
721	22	37-47	<u>.244</u>		<u>.225</u>	
722	22	47-57	<u>.090</u>		<u>.133</u>	
723	22	57-67	<u>.150</u>	<u>.163</u>		
724	22	67-77	<u>.191</u>		<u>.078</u>	
725	22	77-87	<u>.069</u>	<u>.084</u>		
726	22	87-97	<u>.061</u>		<u>.045</u>	
727	22	97-107	<u>.072</u>		<u>.120</u>	
728	22	107-117	<u>.037</u>	<u>.073</u>		
729	22	117-127	<u>.050</u>	<u>.065</u>		

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Sample No.	Hole	Interval	Williams	Loring	Bondar-Clegg	Skyline
6-29-1	25	34-44	.20	.12		
6-29-2	25	44-54	.12	.06		
6-29-3		Outcrop		.12		} LORING } CONST ELDRIDGE }
6-29-4	15			.15		
6-29-5	17	435-445	1.20	.12		
6-29-6	17	445-455	.80	.12		
909	25	224-234	.34		.02	
910	25	234-244	.35		.02	
911	25	244-254	.30		.03	
912	25	254-264	.53		.03	