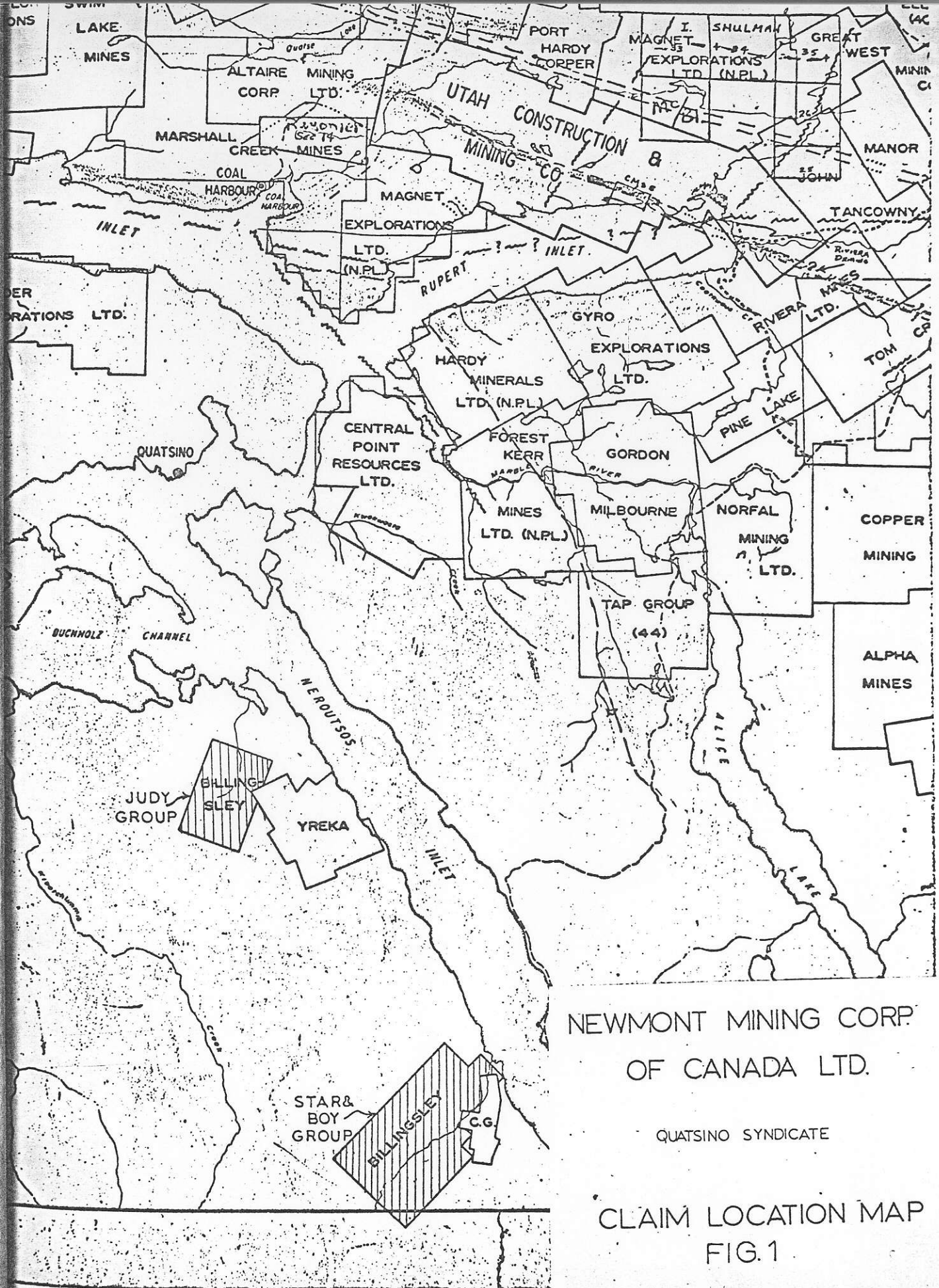


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TEETA CREEK GEOLOGICAL REVIEW
AND
ANALYSIS OF DIAMOND DRILL RESULTS 1968

Report by: J. H. Tremblay

Geological Consultant : H. C. B. Leitch
Geophysical Consultant : W. M. Dolan
Geochemical Consultant : J. A. Coope
Supervised by : R. F. Sheldon



NEWMONT MINING CORP.
OF CANADA LTD.

QUATSINO SYNDICATE

CLAIM LOCATION MAP
FIG. 1



In addition, 24 mineral claims were staked 2 1/2 miles to the north of Teeta Creek, immediately to the northwest of Yreka Mine Crown-grants. These mineral claims were recorded as listed below:

<u>Claim</u>	<u>Record Numbers</u>
Judy 1 - 4	888811 - 814 inclusive
Judy 5	888810
Judy 6 - 8	888815 - 817 inclusive
Judy 9 - 10	888820 - 821
Judy 11 - 12	888823 - 822
Judy 13 - 14	888825 - 824
Judy 15 - 16	888827 - 826
Judy 17 - 24	888828 - 835 inclusive

These claims were staked in February, 1968, and recorded on March 4th, 1968.

HISTORY

The Teeta Creek copper-molybdenum prospect was discovered in the winter of 1967 - 1968 as the result of a syndicate agreement involving Newmont Mining Corporation of Canada Limited, Can-Fer Mines Ltd., and Mr. J. Billingsley.

Interest in an area of some 100 square miles, as outlined in A. G. Spat's 1968 Quatsino Syndicate area report, considered favorable for the occurrence of disseminated copper deposits and/or contact metamorphic deposits, was stimulated by Mr. J. Billingsley of Vancouver. Subsequently, the Quatsino Syndicate was formed by the principals mentioned above with the objective of carrying out an exploration program.

copper values are given below.

<u>Percentage of Total Footage</u>	<u>Range of Cu Values</u>	<u>Estimated Av. %Cu</u>	<u>Estimated Av. %MoS₂</u>
6.5	0.30 - 0.40	0.34	0.025
37.5	0.15 - 0.30	0.20	0.015+
56	- 0.15	-0.15	0.01

Detailed Drill Hole Analysis

The drill hole assay results have been categorized according to the degree of sample information. The better mineralized sections were sampled throughout while in certain other sections of uniform weak mineralization only representative sections were cut for assay. The visual estimates and representative sections are used to assign estimated values of mineralization for all the drill holes.

DH S-1

<u>Footage</u>	<u>Feet</u>	<u>%Cu</u>	<u>%MoS₂</u>	<u>Est. %Cu</u>	<u>Est. %MoS₂</u>
0 - 8	8		Overburden		
8 - 31	23	0.10	0.028		
31 - 101	70	0.21	0.027		
101 - 130	29	0.08	0.018		
8 - 130	122	0.16	0.024		
130 - 502	372			0.10	0.015

DH S-2

0 - 29	29		Overburden		
29 - 78	49	0.08	0.005		

4.2
5.5
9.6
124.9
122.3
2.6
710
32

<u>Footage</u>	<u>Feet</u>	<u>%Cu</u>	<u>%MoS₂</u>	<u>Est. %Cu</u>	<u>Est. %MoS₂</u>
78 - 98	20	0.21	0.023		
98 - 153	55	0.09	0.005		
153 - 174	21			0.10	0.010
174 - 195	21		Dyke		
195 - 255	60	0.15	0.005		
255 - 325.5	70.5			0.15	0.005 - 0.010
325.5 - 335	9.5		Dyke		
335 - 408	73			0.10 - 0.15	0.005 - 0.010
408 - 424	16		Dyke		
424 - 499	75			0.15	0.005
499 - 506	7		Dyke		
506 - 567	61			0.10 - 0.15	0.005
567 - 582	15		Dyke		
582 - 612	30	0.10	0.005		
612 - 632	20	0.21	0.015		
632 - 674	42	0.13	0.005	.16	
674 - 734	<u>60</u>	0.16	0.014		
734 - 744	10	0.12	0.005		
744 - 757	13		Dyke		
757 - 787	30	0.12	0.005		
787 - 798	11	0.23	0.015		
29 - 174	145	0.10	0.008		
174 - 195	21		Dyke		
195 - 582	387			0.11+	0.005

<u>Footage</u>	<u>Feet</u>	<u>%Cu</u>	<u>%MoS₂</u>	<u>Est. %Cu</u>	<u>Est. %MoS₂</u>
582 - 744	162	0.14	0.010		
744 - 757	13		Dyke		
757 - 798	41	0.15	0.009		
29 - 798	769			0.11	0.007

DH S-3

0 - 14	14		Overburden		
14 - 71.5	57.5	0.14	0.005		
71.5 - 100	29.5		Dyke		
100 - 140	40	0.15	0.010	.26	.02
140 - 260	120	0.36	0.025		
260 - 315	55	0.12	0.015		
315 - 350.5	35.5			0.20	0.015
350.5 - 372	22.5		Dyke		
372 - 381.5	9.5	0.23	0.015	.25	.02
381.5 - 386	5.5		Dyke		
386 - 406	20	0.32	0.018	.24	
406 - 449.5	43.5	0.16	0.013		
449.5 - 468	18.5		Dyke		
468 - 478.5	10.5	0.20	0.015		
478.5 - 484.5	6		Dyke		
484.5 - 544.5	60	0.21	0.015		
544.5 - 559.5	15		Dyke		
559.5 - 585	25.5	0.15	0.012		
585 - 605	20		Dyke		

<u>Footage</u>	<u>Feet</u>	<u>%Cu</u>	<u>Est. %Cu</u>	<u>%MoS₂</u>	<u>Est. %MoS₂</u>
14 - 140	126	0.12	0.005	0.630	
140 - 260	120	0.36	0.025	3.000	
260 - 350.5	90.5	0.15	0.015	1.3575	
14 - 350.5	336.5	0.214	0.0148	4.9875	
350.5 - 605	254.5				
	87.5				
				Dykes	
	167	0.17	0.014		
14 - 605	591			0.17	0.012

DH S-4

0 - 17	17			Overburden	
17 - 77	60	0.19	0.018		
77 - 167	90	0.14	0.014		0.015
167 - 187	20	0.36	0.028		
187 - 199.5	12.5			0.30	0.020
199.5 - 226.5	27			Dyke	
226.5 - 307	79.5			0.20 - 0.25	0.015
307 - 347	40	0.15	0.012		
347 - 382	35	0.34	0.015		
382 - 437	55	0.17	0.015		
437 - 524	87			0.15	0.010
524 - 550	26	0.14	0.005		
17 - 199.5	182.5			0.19	0.018
199.5 - 226.5	27			Dyke	
226.5 - 437	211.5			0.20	0.014
437 - 550	113			0.15	0.010

<u>Footage</u>	<u>Feet</u>	<u>%Cu</u>	<u>%MoS₂</u>	<u>Est. %Cu</u>	<u>Est. %MoS₂</u>
17 - 550	533			<u>0.18</u>	0.014
<u>DH S-5</u>					
0 - 15	15		Overburden		
15 - 90	75	0.08	0.015		
90 - 136	46	0.09	0.024		
136 - 145	9		Dyke		
145 - 185	<u>40</u>	0.20	0.015	} .15	0.015
185 - 234	49				
234 - 339	105	0.14	0.012		
339 - 359	20			0.10	0.010
359 - 389	30	0.09	0.012		
389 - 455				0.05 - 0.10	0.01 - 0.015
15 - 145	130	0.08	0.018		
145 - 339	194			0.15	0.013
339 - 455	116			0.10	0.010
15 - 455	440			0.12	0.014

EXPLORATION PROGRAM: JUDY CLAIM GROUP

The Judy claims Nos. 1 - 24 located on Mahwhieclas Creek were staked as a result of copper-mineralized float found by A. G. Spat as mentioned on page 12 of his preliminary report.

In August, 1968, prospector S. W. Barclay and a helper searched the headwaters of the creek over a period of 4 days but were unable to relate the float to any outcrops or to find added mineralized float of any consequence. It can only be surmised that the float is derived from one of the relatively small lenses of copper mineralization common to the Quatsino limestone contact area.