## 015411

- 934/2E Owen Lake, 3.C. June 17, 1929.

Owen Lake Mining and Development Co., Ltd., Vancouver, B.C.

<sup>µ</sup>ear sirs,

932-2-07 PROPERTY FILE

Following is our progress Report on the operations at your property at Owen Lake, B.C.

Since our last report development work has been confined to driving the main crosscut and further work opening up the veins exposed. The results of this work have been eminently satisfactory.

Main Crosscut has been advanced to a distance of 1115 feet from the portal. Advance has been rapid, averaging approximately 10 feet per day of two shifts. This crosscut has exposed seven mineralized shears on which some work has been done and several others that have possibilities but on which no work has been done.

The country in the crosscut is much altered and there is a great deal of fracturing. About 50 feet back from the face is a zone over 30 feet in width where the replacement of the country is so pronounced that the original rock is inderterminable. The greater part of the country rock is probably a much altered andesite porphyry and gabbro and there are several fine grained acidic dykes crossing the owrking.

The country rock is ordinarily fairly soft but the mineralization is a accompanied by silicification and the ore is hard.

No. 1 Drift East follows a well defined fracture for about 40 feet and then swings off the vein to the hanging, following a mineralized cross fracture that has a well defined footwall. The working follows the cross fracture on strike for about 30 feet and then swings to the north on the dip of the fracture, holing back into the main crosscut. The face of the drift on the main shear shows nice ore, a sample across 4 feet, in the face, assaying Gold 0.16 ozs., Silver 46.6 ozs., Copper 3.4%, Lead Nil, Zinc 1.4%. It is proposed to drive the drift ahead on the main fracture.

<u>No. 2 Drift East</u> also shows the tendency for the main fractures to be left and the cross fractures foll wed. This drift is on strike for about 30 feet where a fault occurs and the drift swings to the north east. This crosscut section is in mineralized country and may be on cross fracturing. About 20 feet back from the face the drift is on one of the main fractures but this is probably not the same shear as the drift started on. Near the face there is another cross fracture which carries nice copper ore. The main fracture continues through this cross fracture and the face of the drift is well mineralized.

No. 3 Drift Eaststarts on a well defined fissure but is off strike, In about 40 feet it picks up a good vein with normal strike. About 70 feet from the main crosscut a crosscut has been driven North east and south west exposing a section 40 feet in width. In the north east crosscut a good vein about 10 feet in width is exposed and in the south west cross -cut is what is probably the vein showing in the face of No. 2 drift. This crosscut exposes an important ore showing, the average off the samples from the north west side showing a width of slightly over 11<sup>1</sup>/<sub>2</sub> feet with an ayeragesyalue of Gold 0.20 ozs., Silver 33.6 ozs., Copper 4.0%. Sample 3 gave also 2.3% Lead and 2.0% zinc. Zinc occurs consistently with the **wwyp** copper and in sufficient quantities to be a connercial consideration.

No. 4. Drift East starts on a main fracture but swings diagonally on to another fracture. In the face is a fissure about 6 feet in width which is sparely mineralized, chalcop rite occuring in stringers on both the foot and hanging sides. The footside carries most copper.

<u>No. 5 Drift East</u> has been driven only about 16 feet on a narrow zinc vein.

No.6 drift East at 865' from the portal has been driven about 30 feet on a soft shear that does not show much ore in the drift, other than a narrow copper vein which assayed, across 4" Gold 0.15 ozs., Silver 14.6 ozs., Copper 4.5%, Lead 0.1%, Zinc 2.0%. It is proposed to drive this drift ahead as, on the surface, about 420 feet south east, there is a very promising surface exposure that is probably on this vein. Also, as there is about 250 feet of backs at this section this drift will be used as one of the main preliminary workings. If the surface exposure is on this vein, as appears probable, an ore shoot should be encountered south west and a raise can be put up to the surface.

<u>No. 7 Drift East</u> has been started to prospect a pyritic zinc vein about five feet in width. This is a very strong vein but values are low, the vein running between 4 and 4.5% zinc with inappreciable values in other metals. This vein is closely associated with a wide dyke that probably cuts through the vein going south east. This vein is intersected at 960 feet from the portal.

It is recommended that future work should be designed to prospect this section as a zone rather than to attempt to open up each shear individually. Driving the crosscut off No. 3 drift will prospect the zone between No. 3 vein and the portal and off No. 6 Drift drilling or crosscutting can be laid out to prospect the whole zone south east of the main cross cut. In the mean while the most important work of all, driving the **MXX** • main crosscut, is going ahead rapidly.

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No.1. DRING. Rast and West.

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$ \begin{cases} 377 & & Tr. & 1.4 & 0.2 & 311 & 2.3 & 4^{\circ} & 3^{\circ} C^{\circ} \\ 399 & & 0.16 & 27.5 & 1.9 & 0.1 & 3.1 & 0^{\circ} C^{\circ} & 3^{\circ} C^{\circ} \\ 360 & & 0.05 & 4.5 & 0.6 & 11 & 4.6 & 0^{\circ} C^{\circ} & 5^{\circ} C^{\circ} \\ 362 & & 0.18 & 26.0 & 2.4 & 111 & 3.6 & 0^{\circ} C^{\circ} & 5^{\circ} C^{\circ} \\ 363 & & 0.05 & 3.4 & 0.4 & 11. & 3.6 & 0^{\circ} C^{\circ} & 5^{\circ} C^{\circ} \\ 364 & & 0.06 & 3.4 & 0.4 & 11 & 3.6 & 0^{\circ} C^{\circ} & 5^{\circ} C^{\circ} \\ 365 & & 0.06 & 6.3 & 1.9 & 7.6 & 0.7 & 3^{\circ} C^{\circ} & 3^{\circ} C^{\circ} \\ 365 & & 0.01 & 3.4 & 0.4 & 11 & .7 & 76^{\circ} \\ 366 & & 0.02 & 3.0 & 0.5 & 0.1 & Tr. & 5^{\circ} C^{\circ} & 3^{\circ} C^{\circ} & 3^{\circ} C^{\circ} \\ 366 & & 0.01 & 5.0 & 1.7 & 77. & 5.6 & 11^{\circ} 110^{\circ} \\ 366 & & 0.02 & 3.0 & 0.5 & 0.1 & Tr. & 5^{\circ} C^{\circ} & 3^{\circ} C^{\circ} & 3^{\circ} C^{\circ} \\ 367 & & 0.32 & 60.1 & 5.7 & 1.0 & 6.2 & 6^{\circ} C^{\circ} & 100^{\circ} \\ 366 & & 0.19 & 60.1 & 5.7 & 1.0 & 6.2 & 0^{\circ} C^{\circ} & 3^{\circ} C^{\circ} \\ 363 & & 0.65 & 3.4 & 0.4 & 1.2 & 4.7 & 5^{\circ} C^{\circ} & 3^{\circ} C^{\circ} \\ 363 & & 0.65 & 3.4 & 0.1 & 0.6 & 0^{\circ} C^{\circ} & 3^{\circ} C^{\circ} \\ 363 & & 0.65 & 3.4 & 0.1 & 0.4 & 1.2 & 4.7 & 5^{\circ} C^{\circ} & 3^{\circ} C^{\circ} \\ 363 & & 0.65 & 3.4 & 1.1 & 0.1 & 0.6 & 0^{\circ} C^{\circ} & 3^{\circ} C^{\circ} \\ 363 & & 0.65 & 3.4 & 1.1 & 0.1 & 0.4 & 0^{\circ} C^{\circ} & 3^{\circ} C^{\circ} \\ 363 & & 0.65 & 3.4 & 1.1 & 0.1 & 7.9 & 3^{\circ} C^{\circ} & 3^{\circ} C^{\circ} \\ 363 & & 0.65 & 3.4 & 1.1 & 0.1 & 7.9 & 3^{\circ} C^{\circ} & 3^{\circ} C^{\circ} \\ 316 & 3 & 3^{\circ} T^{\circ} & T^{\circ} & T^{\circ} & T^{\circ} & 3^{\circ} & 3^{\circ} C^{\circ} \\ 316 & 3 & 3^{\circ} T^{\circ} & T^{\circ} & T^{\circ} & T^{\circ} & 3^{\circ} & 3^{\circ} C^{\circ} \\ 316 & 3 & 3^{\circ} T^{\circ} & T^{\circ} & T^{\circ} & T^{\circ} & T^{\circ} & 3^{\circ} & 3^{\circ} C^{\circ} \\ 316 & 3 & 3^{\circ} T^{\circ} & T^{\circ} & T^{\circ} & T^{\circ} & 3^{\circ} & 3^{\circ} C^{\circ} \\ 316 & 3^{\circ} T^{\circ} & T^{\circ} & T^{\circ} & T^{\circ} & T^{\circ} & 3^{\circ} & 5^{\circ} & 5^{\circ} & 5^{\circ} \\ 316 & 0.5 & 1.5 & 0^{\circ} & T^{\circ} & T^{\circ} & T^{\circ} & 3^{\circ} & 5^{\circ} & 5^{\circ$								5*8"	
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310 0.01 1.5 TR. 0.4 4.2 4'6" #7YEIN AS CUT 311 0.01 1.4 " TR. 4.0 4'6" #7YEIN AS CUT by MRIN XENT DR.	319 320 321 352 353 353 353 353 353 354 305 298 280 272 303	Ao. Grab Grab Grab O.08 0.08 0.08 0.08 0.08 0.08 0.08 0.08	A. 14.6 19.0 25.9 53.4 69.1 11.6	4' co 4' co horizo wall co ite wa Cu. 2.3 2.8 1.9 4.8 9.7 1.4	Cootwal continuit intinuit intal so intal so if righ ill of TR. TR. TR. 0.2 2.3 0.2 1.2	1 4: 1 ng fr ng fr ample t ere pyrit Zn, 0: 1:9 2. 2. 0 2.	$ \begin{array}{c} \text{I.S. of } \\ \text{om } & \text{S1} \\ \text{om } & \text{S1} \\ \text{over } & S$	$e \neq T X$ $2^{n/2}$ $2^{n/2}$ $2^{n/2}$	оррег bearing rock. rift. Cut of #3 DR. E # 315- 320. /'2' } Rightix Cut #3DR.
· 311 0.01 114 " TR. 4.0 416" (#7YEIN AS COT	319 320 321 352 353 353 353 353 353 354 305 298 280 272 303	Ao. Grab Grab Grab O.08 O.08 O.08 O.08 O.08 O.08 O.08 O.08	A. 14.6 19.0 25.9 53.4 69.1 11.6	4' co 4' co horizo wall co ite wa Co. 2.3 2.8 1.9 4.8 9.7 1.4 3.3	Cootwal continuit intinuit intal sub- of right all of TR. TR. TR. TR. 0.2 2.3 0.2 1.2 0.1	1 4: 1 ng fr ng fr ample t ere pyrit Zn, 0: 1:9 2: 2. 0 2. 1	$ \begin{bmatrix} \mathbf{n} & \mathbf{n} \\ \mathbf{n}$	$e \neq T X$ $2^{n/2}$	оррег bearing rock. rift. Cut of #3 DR. E # 315- 320. /'2' } Rightix Cut #3DR.
· 311 0.01 114 " TR. 4.0 416" (#7YEIN AS COT	272 321 321 321 352 353 353 354 305 297 280 272 303 	Ao. Grab Grab Grab O.08 O.08 O.08 O.08 O.08 O.08 O.08 O.08	Aq. 14.6 19.0 25.9 53.4 69.1 11.6 6.8	4' co 4' co horizo wall co ite wa Co. 2.3 2.8 1.9 4.8 9.7 1.4 3.3	Cootwal continuit intinuit intal sub- of right all of TR. TR. TR. TR. 0.2 2.3 0.2 1.2 0.1	1 4: 1 ng fr ng fr ample t ere pyrit Zn, 0: 1:9 2: 2. 0 2. 1	$ \begin{bmatrix} \mathbf{n} & \mathbf{n} \\ \mathbf{n}$	$e \neq T X$ $2^{n/2}$	оррег bearing rock. rift. Cut of #3 DR. E # 315- 320. /'2' } Rightix Cut #3DR.
21)	319 320 321 352 353 353 353 353 353 304 305 298 298 298 272 303 299 300	Ao. Grab Grab Orab Orab Orab Orab Orab Orab Orab O	on right of $351.$ on oppose Aq. 14.6 19.0 25.9 53.4 69.1 11.6 6.8 3.4	4° co 4° co horizo wall co ite wa Cu. 2.3 2.8 1.9 4.8 9.7 1.4 3.3 1.5	Cootwal continuit intinuit intal so intal so if righ ill of TR. TR. TR. TR. 0.2 2.3 0.2 1.2 0.1 ML	1 4: 1 ng fr ng fr ample t ere pyrit Zn, 0: 1:9 2: 2. 0 2 1	$\begin{bmatrix} \mathbf{N} & \mathbf{O} \\ \mathbf{O} $	E = T X $A_{LSO} S = 0$ $2\frac{1}{2}$ $1^{'} A^{''}$ $1^{'} 5^{''}$	$\begin{cases} \text{opper bearing rock.} \\ \text{rift.} \\ \\ \begin{array}{c} & & & & & & & & & & & & & & & & & & &$
21)	319 320 321 352 353 353 353 353 353 353 353 353 353	Ao. Grab Grab Grab O.08 O.08 O.08 O.08 O.08 O.08 O.08 O.08	on right of $351.$ on oppose Aq. 14.6 19.0 25.9 53.4 69.1 11.6 6.8 3.4	4 $c_{4}$ $4 c_{4}$ $c_{4}$ $c_{4}$ $c_{4}$ $c_{4}$ $c_{1}$ $c_{1}$ $c_{2}$ $c_{3}$ $c_{2}$ $c_{3}$ $c_{2}$ $c_{3}$ $c_{4}$ $r_{3}$ $c_{4}$ $r_{3}$ $r_{4}$ $r_{5}$ $r_{7}$	Sootwal restinution $restinution restinution resti$	1 4: 1 ng fr ng fr ample t ere pyrit 2. 2. 0 2 1 1 4	$ \begin{bmatrix} \mathbf{n} & \mathbf{n} \\ \mathbf{n}$	$E \neq T X$ A' 6''	$\begin{cases} \text{opper bearing rock.} \\ \text{rift.} \\ \\ \begin{array}{c} & & & & & & & & & & & & & & & & & & &$
	319 320 321 352 353 353 353 353 353 353 353 353 353	Ao. Grab Grab Grab O.08 O.08 O.08 O.08 O.08 O.08 O.08 O.08	on right on right on oppose Aq. 14.6 19.0 25.9 53.4 69.1 11.6 6.8 3.4 1.5	4 $c_{4}$ $4 c_{4}$ $c_{4}$ $c_{4}$ $c_{4}$ $c_{4}$ $c_{1}$ $c_{1}$ $c_{2}$ $c_{3}$ $c_{2}$ $c_{3}$ $c_{2}$ $c_{3}$ $c_{4}$ $r_{3}$ $c_{4}$ $r_{3}$ $r_{4}$ $r_{5}$ $r_{7}$	Sootwal restinution $restinution restinution resti$	1 4: 1 ng fr ng fr ample t ere pyrit 2. 2. 0 2 1 1 4	$ \begin{bmatrix} \mathbf{n} & \mathbf{n} \\ \mathbf{n}$	$E \neq T X$ $A_{LSO} S = 1$ $2 / 2 ^{1}$ $1 ^{1} A^{11}$ $1 ^{1} 5 ^{11}$ $4 ^{1} 6 ^{11}$ $4 ^{1} 6 ^{11}$	$\begin{cases} \text{opper bearing rock.} \\ \text{rift.} \\ \\ \begin{array}{c} & & & & & & & & & & & & & & & & & & &$