REPORT ON THE IRON COP PROPERTY
ALBERNI AND NANAIMO MINING DIVISIONS
ALICE LAKE AREA, VANCOUVER ISLAND, B.C.

LOCATION

N.T.S.: 92L/5E
LATITUDE: 50° 17'N.
LONGITUDE: 127° 36'W.

CLAIMS

LONDON 1 (1850); LONDON 2 (1852); BEV (1758);
BOZO 1 (1595); BOZO 2 (1596); RANDY 1 (4249) & RANDY 2 (4250)

FOR

OMAX RESOURCES LTD.

PREPARED BY

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PROFESSIONAL ENGINEER
PROVINCE OF BRITISH COLUMBIA
P. A. Christopher

APRIL 30, 1991

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SUMMARY

The Iron Cop Property, consisting of seven metric claims totalling 95 units, covers about 1650 hectares (4077 acres) in the Alberni and Nanaimo Mining Divisions on Vancouver Island, B.C. The claim area is presently accessed by helicopter from Port Hardy about 50 kilometers to the north. Roads along Colonial Creek are driveable to within about 4 kilometers of the property and heavier equipment could be ferried from the end of the Colonial Creek Road.

The Iron Cop Property has been actively explored since prospectors located the initial copper showings in 1960. The claims contain several copper vein and porphyry style showings in Vancouver Group rocks. Limestone horizons in the area give the potential for copper-gold skarn deposits. Exploration programs have concentrated on the Wilf, Iron Cop, Ridge and Lois showings with geologic mapping, geochemical sampling, geophysical surveys, and diamond drilling.

The property was explored in 1962-64 by Riocanex Ltd. and from 1984 to 1986 by Brinco Mining Ltd., who drilled 7 diamond drill holes in the Iron Cop zone. The writer evaluated and sampled sections of Brinco's drill core which is stored at the Iron Cop camp. The writer collected 19 core samples from thè old core with values up to 38783 ppm copper and 1520 ppb gold obtained over a 0.5 meter interval in hole 84-2. The writer's samples (Table 4) provide values for a number of intersection reported as >10,000 ppm copper and provide copper and gold values for additional intervals. The writer's sampling allow recalculation of the following drill intercepts.

Hole #	Interval	Length	% Cu	PPB Au	Reason For Hole
IC-84-1	9.42-20.69m	11.27m	0.558	185	Test below Tr1
IC-84-2	16.04-41.45m	25.41m	0.341	150	Test below Tr1
IC-84-3	31.09-32.31m	1.22m	0.360	77	Test below Tr1
IC-84-4	60.04-89.90m	29.86m	0.305	192	Test below Tr3
IC-84-5	15.64-17.48m	1.84m	1.63	580	Test below Tr5
	51.00-62.78m	11.34m	0.349	153	" " "
IC-84-7	41.15-43.28m	2.13m	0.13	15	" " "

The Iron Cop zone (Figure 6) has a gold anomaly which extends to the northwest boundary of the Iron Cop grid. The anomaly extends for about 700 meters from about 4400E to 5100E with drill testing restricted to 4825E to 5250E. The anomaly is open to the west and should be defined and evaluated by extending grid geochemical, geophysical and geological coverage and trenching before selecting further drill sites.

The writer recommends further, success contingent, staged exploration of the Iron Cop Property. A Stage I program, of grid extension, geochemical sampling, geological mapping, induced polarization and trenching for the Iron Cop zone and further prospecting of the Ridge, Wilf and Grid 2 showing, is estimated to cost $90,000. Contingent on the success of the Stage I program, a Stage II, 600 meter drill test is estimated to cost $140,000.

northern Vancouver Island, British Columbia. The total area of the property is estimated from government claim plans to be about 1650 ha. (4077 acres). The Bev, Randy 1, London 1 and Bev claim were optioned by Omax Resources Ltd. in May 1990 and acquired the London 2, Bozo 1 and Bozo 2 in April 1991.

Pertinent claim data for the Iron Cop Property is summarized in Table 1 with claim locations shown on Figures 1 and 2.

Table 1. Pertinent claim data for Iron Cop Property.

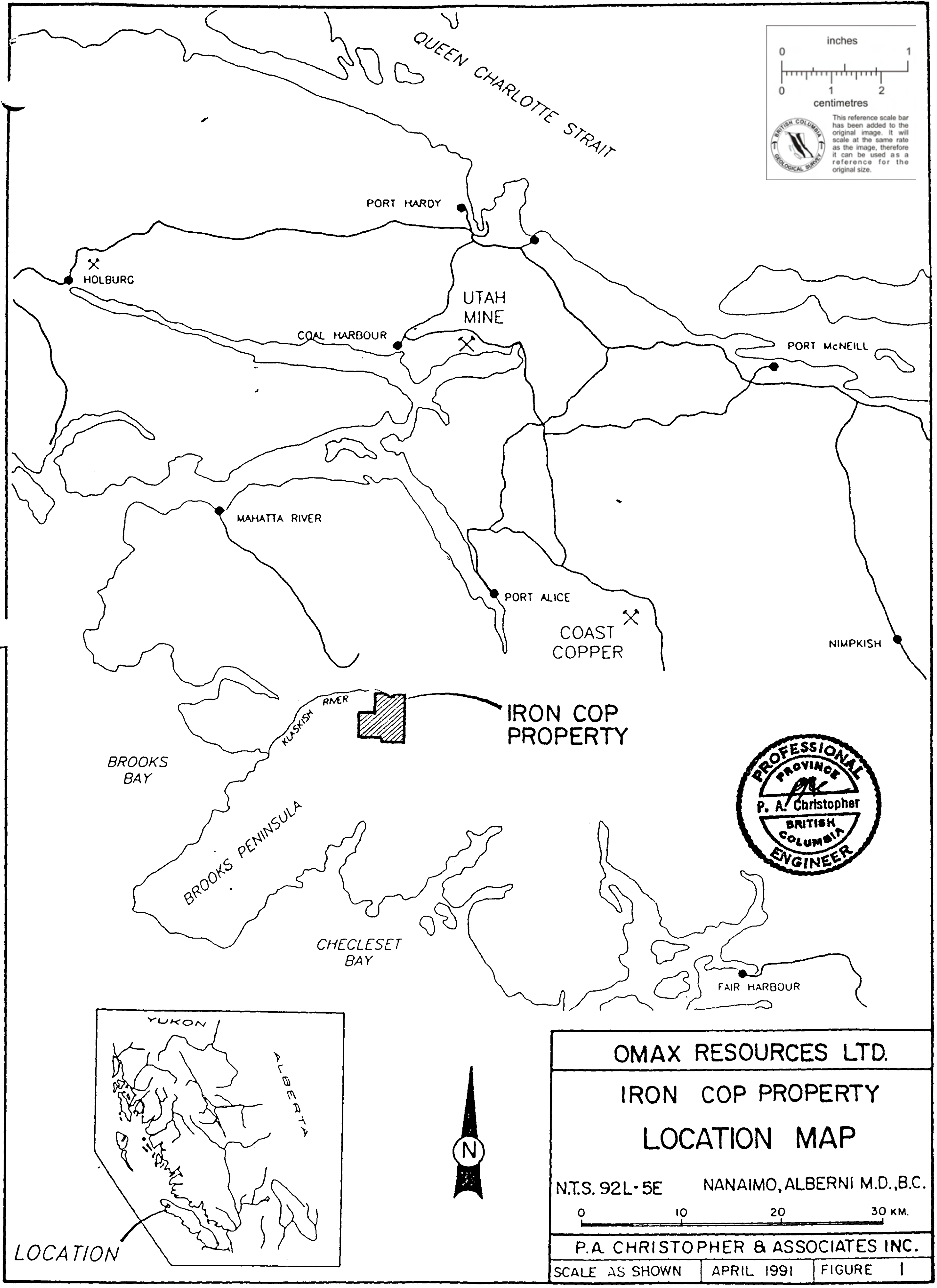
CLAIM	RECORD #	UNITS/SHAPE	EXPIRY DATE	MINING DIVISION
London 1	1850	20/5Wx4S	Sept 26, 1991	ALBERNI
London 2	1852	20/4Wx5N	Sept 26, 1991	ALBERNI
Bozo 1	1595	8/4Wx2S	Oct. 19, 1991	NANAIMO
Bozo 2	1596	12/4Wx3N	Oct. 19, 1991	NANAIMO
Bev	1758	4/2Wx2N	Sept 26, 1991	NANAIMO
Randy 1	4249	12/3Wx4N	Nov. 5, 1991	ALBERNI
Randy 2	4250	9/3Wx3S	Nov. 5, 1991	ALBERNI
	Total Units 85			

HISTORY

The initial copper-magnetite discovery and claim staking was by Wilf Trembaly in 1960. The property was optioned to Rio Tinto Canadian Explorations Ltd. (Riocanex) in 1962 with initial mapping, trenching and surface sampling conducted in 1963. Two shallow drill holes (W-1 & W-2) were drilled from the same collar in 1964 to test below a well mineralized trench at the Wilf Showing. The holes were drilled from the same collar at 180 feet east on section 745 feet south. Hole W1 was drilled at -60° in a direction 225° for 290.4 feet, and hole W2 was drilled at -60° in a direction 025°. The initial 100.8 feet of hole W1 averaged 0.19% copper and the final 41.8 feet averaged 0.15% copper. Hole W2 contained 35.8 feet, from about 105 feet to 140.8 feet, grading 0.371 (feet.)

Riocanex completed geological mapping, geochemical sampling, self potential, trenching and drilled the IC-1 through IC-3 holes totalling 527.7 feet. in the Iron Cop grid area. Trench 1 at 5000N/4950E (1984 Iron Cop Grid) contained 2.5 meters (8.2 feet) grading 12.2% copper, 0.128 oz/ton gold and 1.27 oz/ton silver. Hole IC-1 tested below trench 1 contained 26.5 feet from 57.0 feet to 83.5 feet grading 0.65% copper. Trench 2 samples by Riocanex assayed 10.90% copper, 0.02 oz/ton gold and 0.60 oz/ton silver over 0.5 meters (1.64 feet). Hole IC-3 drilled below trench 2 intersected only 0.35 meters (1.1 feet) grading (0.07% copper). Hole IC-2, drilled at 5200E/5060N, had very poor recovery and limited assaying with a 1.1 foot section reported to contain 0.30% copper.

Four holes were reportedly drilled at the Lois showing on the adjacent property. Results of drilling on the Lois claim are not available to the writer.



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BRITISH COLUMBIA GEOLOGICAL SURVEY
QUEEN CHARLOTTE STRAIT
PORT HARDY
HOLBURG
UTAH MINE
COAL HARBOUR
PORT McNEILL
MAHATTA RIVER
PORT ALICE
COAST COPPER
NIMPKISH
KLASKISH RIVER
IRON COP PROPERTY
BROOKS BAY
BROOKS PENINSULA
CHECLESET BAY
FAIR HARBOUR
PROFESSIONAL ENGINEER
PROVINCE
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BRITISH COLUMBIA
YUKON
ALBERTA
LOCATION
N
OMAX RESOURCES LTD.
IRON COP PROPERTY
LOCATION MAP
N.T.S. 92L-5E
NANAIMO, ALBERNI M.D., B.C.
0
10
20
30 KM.
P.A CHRISTOPHER & ASSOCIATES INC.
SCALE AS SHOWN
APRIL 1991
FIGURE 1

CHONG

INTRODUCTION:

Omax Resources Ltd. presently holds an option on the Iron Cop property, situated between Brooks Peninsula and Alice Lake, in the northwestern part of Vancouver Island. Peter Christopher & Associates Inc. was retained by the management of Omax Resources Ltd. to review the companies and previous exploration programs on the Iron Cop property. The review was conducted to formulate a program for further exploration of the Iron Cop property, if warranted. The writer examined the Iron Cop property from September 10th to 13th, 1990 and located and resampled a total of 19 intercepts from seven 1984 holes drilled by Brinco Mining Limited.

Previous exploration results and check samples collected by the writer suggest that the property has potential for small to moderate size copper-gold deposits which could occur as sulfide bearing quartz veins, copper-gold-magnetite skarns, mineralized shear zones or contact breccia zones. Further work is recommended for the Iron Cop property and a success contingent, staged exploration program is outlined.

LOCATION AND ACCESS: (FIGURES 1 & 2)

The property straddles the height of land between the Little Klaskish River drainage on the northwest, and the Nesparti River drainage on the south. The Colonial Creek and Power River drainages are situated east of the property. The property is also situated between the Brooks Peninsula and Alice Lake in the Kyuquot Provincial Forest in the northwest part of Vancouver Island, British Columbia.

The claims straddle the boundary between the Alberni and Nanaimo Mining Divisions and lie within N.T.S. map sheet 92L/5E at geographic coordinates 50° 17'N. latitude and 127° 36'W. longitude.

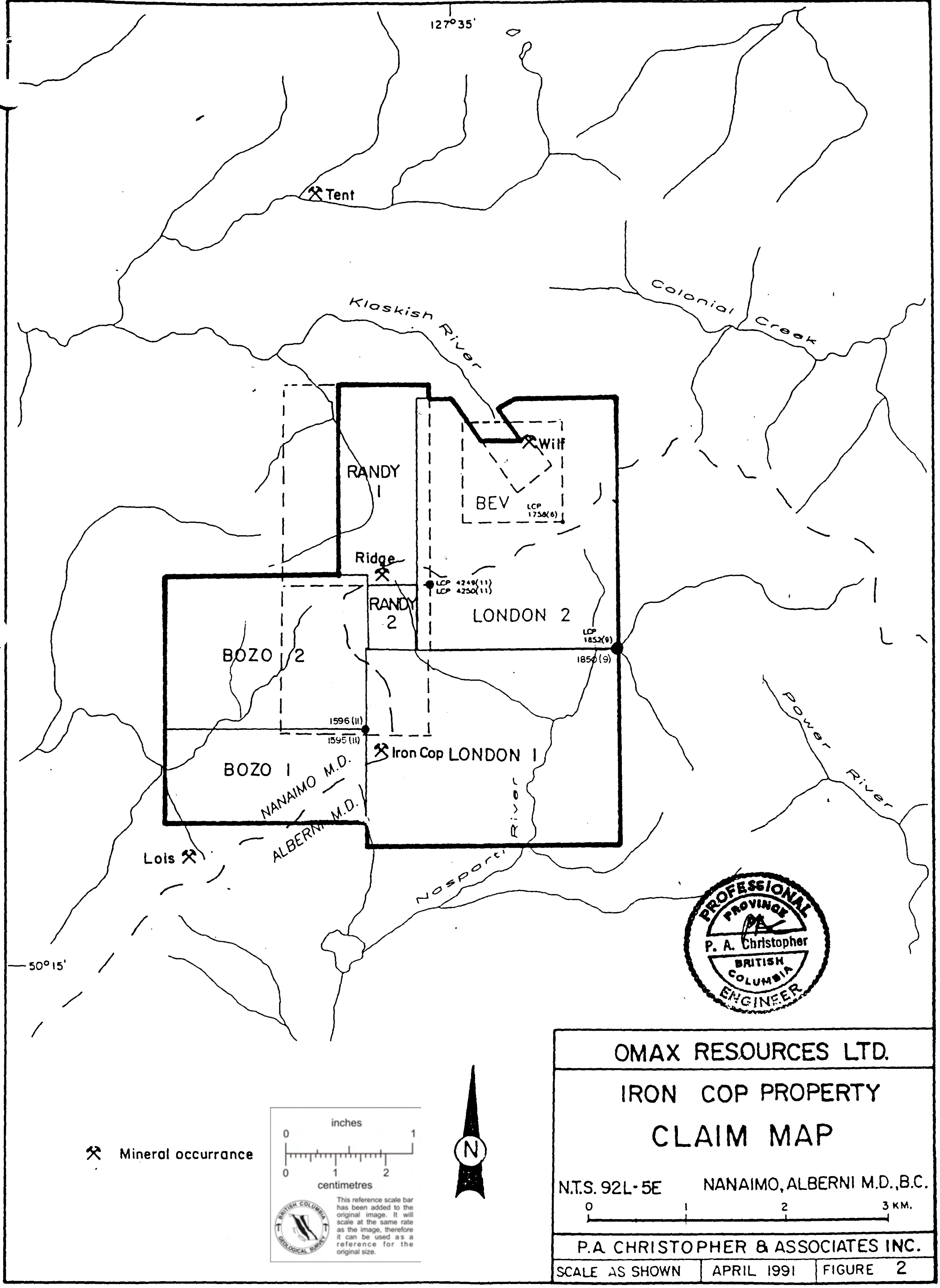
The Iron Cop property is located about 13 kilometers southeast of the village of Port Alice with Port Hardy, a major supply and service center, about 50 kilometers north of the claims. Logging roads extend to within 3 km of the claims and eventually will cross the claims. At present, access is by helicopter from Port Hardy with shorter ferrying possible from the Colonial Creek logging road system.

The property is mainly covered with dense coastal forest of spruce, fir, hemlock and cedar. Muskeg occurs on some slopes and around small lakes which occur on flatter upper slopes. Moderate to thick underbrush makes traversing slow and grid construction relatively expensive.

Topography varies from moderate to steep slopes with some rounded and swampy ridges. Parts of the property are too steep to easily traverse.

CLAIMS: (FIGURE 2)

The Iron Cop property, consisting of seven metric claims totalling 85 units, straddles the Alberni and Nanaimo Mining Divisions in



127°35'
Tent
Kloskish River
Colonial Creek
RANDY 1
Wilf
BEV
LCP 1758(6)
Ridge
LCP 4249(11)
LCP 4250(11)
RANDY 2
LONDON 2
LCP 1852(9)
1850(9)
BOZO 2
1596(II)
1595(II)
Iron Cop
LONDON 1
BOZO 1
NANAIMO M.D.
ALBERNI M.D.
River
Nasparti
Power River
Lois
50°15'
PROFESSIONAL ENGINEER
PROVINCE
P. A. Christopher
BRITISH COLUMBIA
Mineral occurrance
inches
0 1
0 1 2
centimetres
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BRITISH COLUMBIA GEOLOGICAL SURVEY
N
OMAX RESOURCES LTD.
IRON COP PROPERTY
CLAIM MAP
N.T.S. 92L-5E
NANAIMO, ALBERNI M.D., B.C.
0 1 2 3 KM.
P.A CHRISTOPHER & ASSOCIATES INC.
SCALE AS SHOWN
APRIL 1991
FIGURE 2

CHONG

REGIONAL GEOLOGY: (Figures 3, 4, & 5)

The Iron Cop Property is situated in the Insular Tectonic Belt of the Canadian Cordillera. The northern part of Vancouver Island is mainly underlain by sedimentary and volcanic rock of the Mesozoic Vancouver Group with a basement of gneissic or granitoid rocks called the Westcoast Crystalline Complex. The Vancouver Group consists of the mainly volcanic Karmutsen and Bonanza Formations, and the mainly sedimentary Parsons Bay, Harbledown and Quatsino Formations. The Vancouver Group has been intruded by Jurassic "Island" intrusions and Tertiary epizonal intrusions. The geology of the area has been mapped by Muller et. al. (1974) with the regional geological setting shown on Figure 3 and geological sections and correlations summarized in figures 4 and 5.

The area has a regional northwesterly structural trend and mainly southwesterly dips. In the area of the Iron Cop Property, the northwest trending Mahatta fault zone is interrupted by transverse faults which are part of the northeast trending Brooks Peninsula Fault block. On Brooks Peninsula, gneissic rocks of the Westcoast Crystalline Complex have been exposed by uplift along along major northeasterly trending faults. The gneissic complex is generally quartz diorite with mafic to ultràmafic components. A northwest trending zone of small, leucocratic, Tertiary intrusive bodies transect the northeast trending structural high. The Mahatta, Amai and Kashutl Intrusions are accompanied by swarms of dykes and sills, and characterized by chlorite, sericite, clay, silica and saussurite alteration.

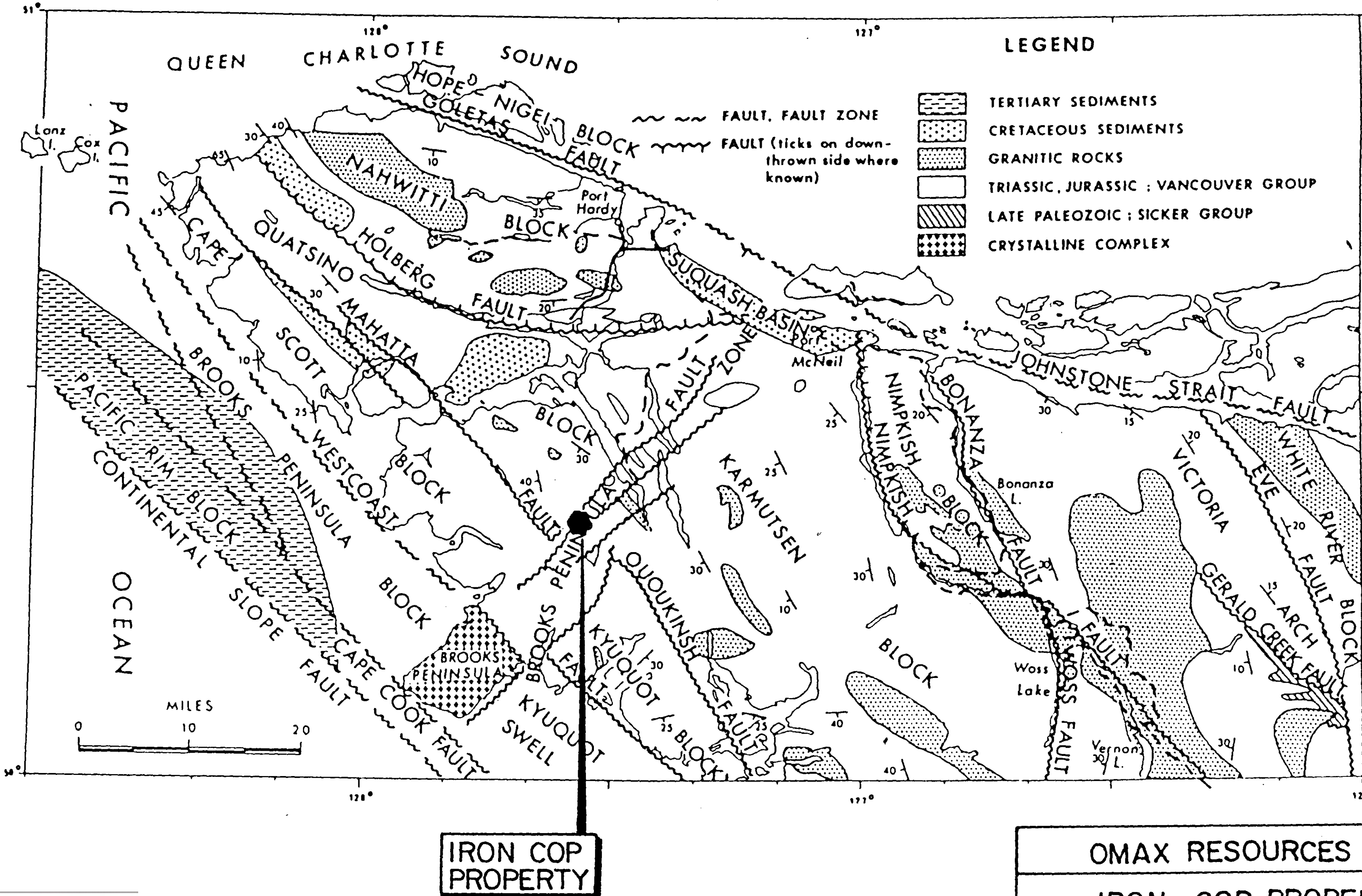
PROPERTY GEOLOGY (Figure 6)

The Property geology shown on Figure 6 has been compiled from a number of mapping programs conducted by Rio Tinto, Esso, Vanco, Brinco and Omax Resources (Gatenby, 1964; Somerville, 1977; Epp, 1984; and Greene, 1990). Property mapping shows that outcrops consist mainly of basaltic rocks of the Triassic Karmutsen Formation and granitic rocks of the Island Intrusions. The Iron Cop Zone (Figure 6) has been described by Gonzalez (1984) as 62 meters of alternating bedded limestone and thin inter-bedded highly altered basic volcanics.

The Wilf Showing area has been shown by Greene (1990) to be a contact area between limy Bonanza or Karmutsen volcanic rocks and granodiorite bodies of the island intrusions. Fracture controlled, quartz-chalcopyrite-pyrite-magnetite mineralization is skarn related, but mineralization is often a considerable distance from a known intrusive body.

The Ridge showing occurs along the ridge near the boundary of the Bozo and Randy claims. The showing contains up to 10% pyrite in a silicified, argillic phyllic alteration zone with weakly anomalous gold (to 30 ppb) and arsenic (to 71 ppm) rock geochemical samples (Sketchley, 1989).

A silicified, east-west, shear zone, which cuts Karmutsen volcanics near the eastern boundary of the London 2 claim contains sphalerite mineralization (Grid 2 area Figure 6).



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N

AFTER MULLER ET AL, 1974

OMAX RESOURCES LTD.		
IRON COP PROPERTY		
REGIONAL GEOLOGY		
N.T.S. 92L-5E NANAIMO, ALBERNI M.D., B.C.		
0 10 20 40 KM.		
P.A CHRISTOPHER & ASSOCIATES INC.		
SCALE AS SHOWN	APRIL 1991	FIGURE 3

inches 0 1
0 1 2 centimetres

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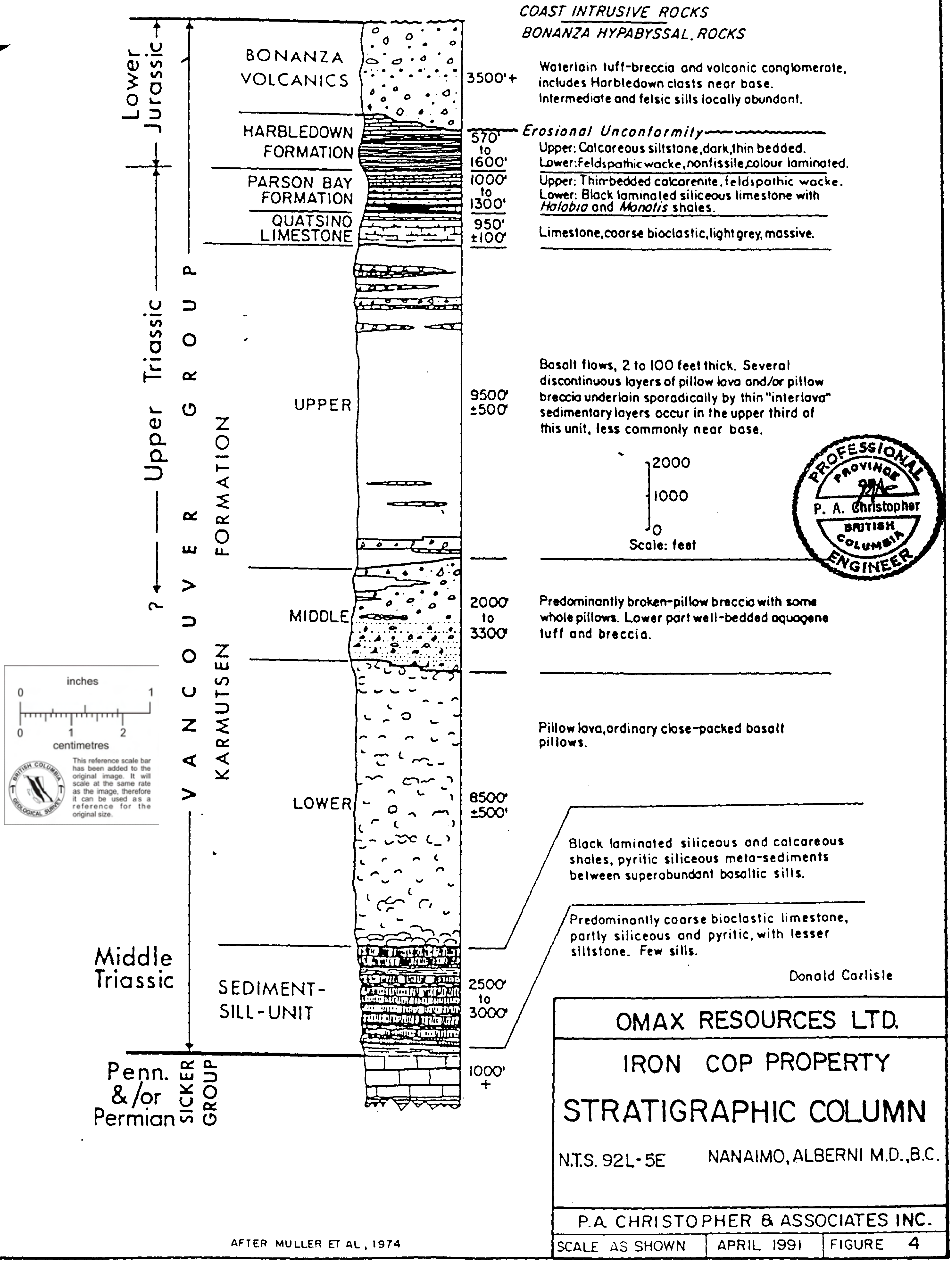

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IRON COP PROPERTY

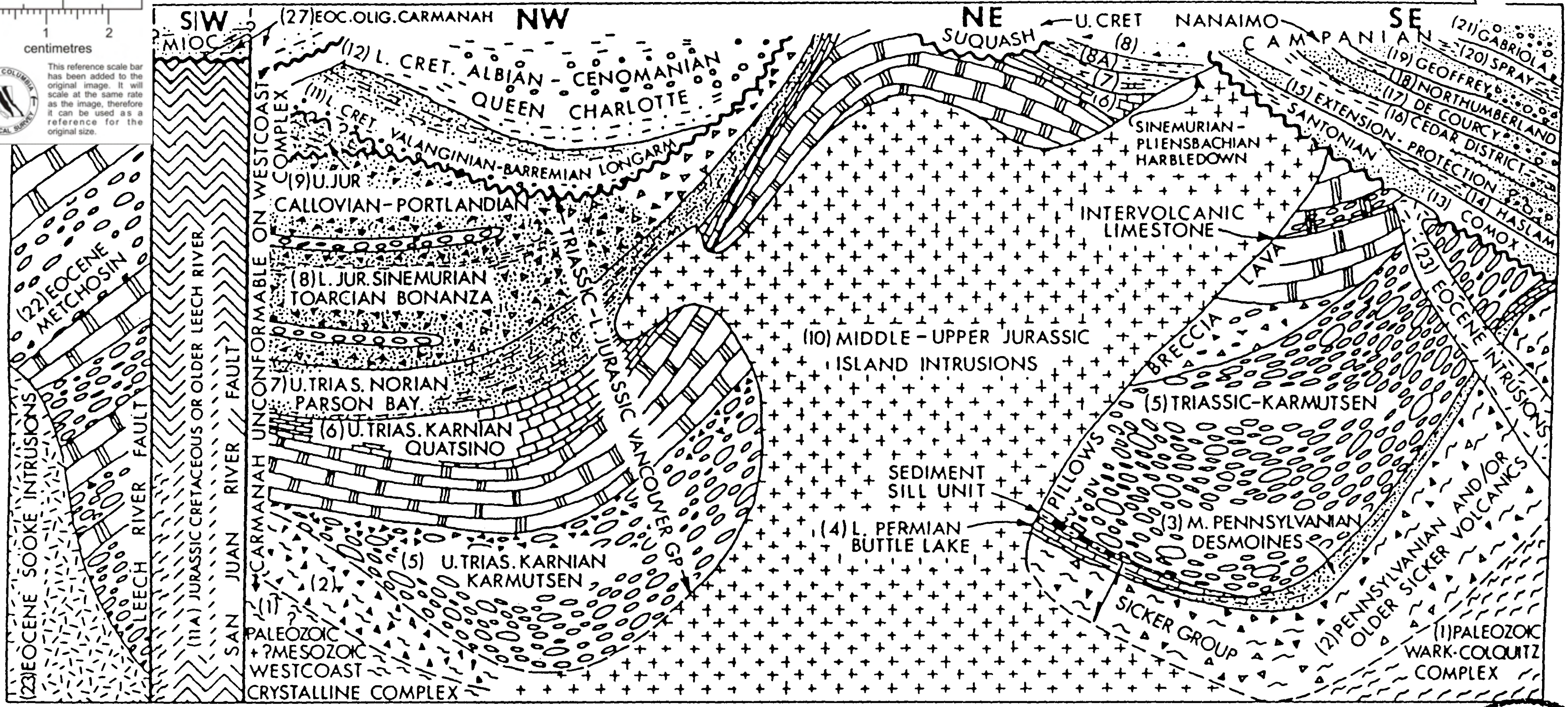
STRATIGRAPHIC COLUMN

N.T.S. 92L-5E NANAIMO, ALBERNI M.D., B.C.

P.A. CHRISTOPHER & ASSOCIATES INC.

SCALE AS SHOWN	APRIL 1991	FIGURE 4

CHONG



- SANDSTONE, GREYWACKE
- SHALE, SILTSTONE
- CONGLOMERATE
- CALCAREOUS SANDSTONE, SILTSTONE
- LIMESTONE
- MAINLY INTERMEDIATE TO SILICIC TUFF AND VOLCANIC BRECCIA
- INTERMEDIATE TO SILICIC PYROCLASTICS AND GREENSTONE
- MAINLY BASALTIC FLOWS
- PILLOW-BRECCIA
- PILLOW-LAVA
- MAINLY QUARTZ MONZONITE, GRANODIORITE
- MAINLY QUARTZ DIORITE, GABBRO
- SHEARFOLDED GREYWACKE, ARGILLITE, PHYLLITE
- GNEISS, SCHIST
- ARGILLITE, DIABASE
- ANGULAR UNCONFORMITY

AFTER MULLER ET AL, 1974

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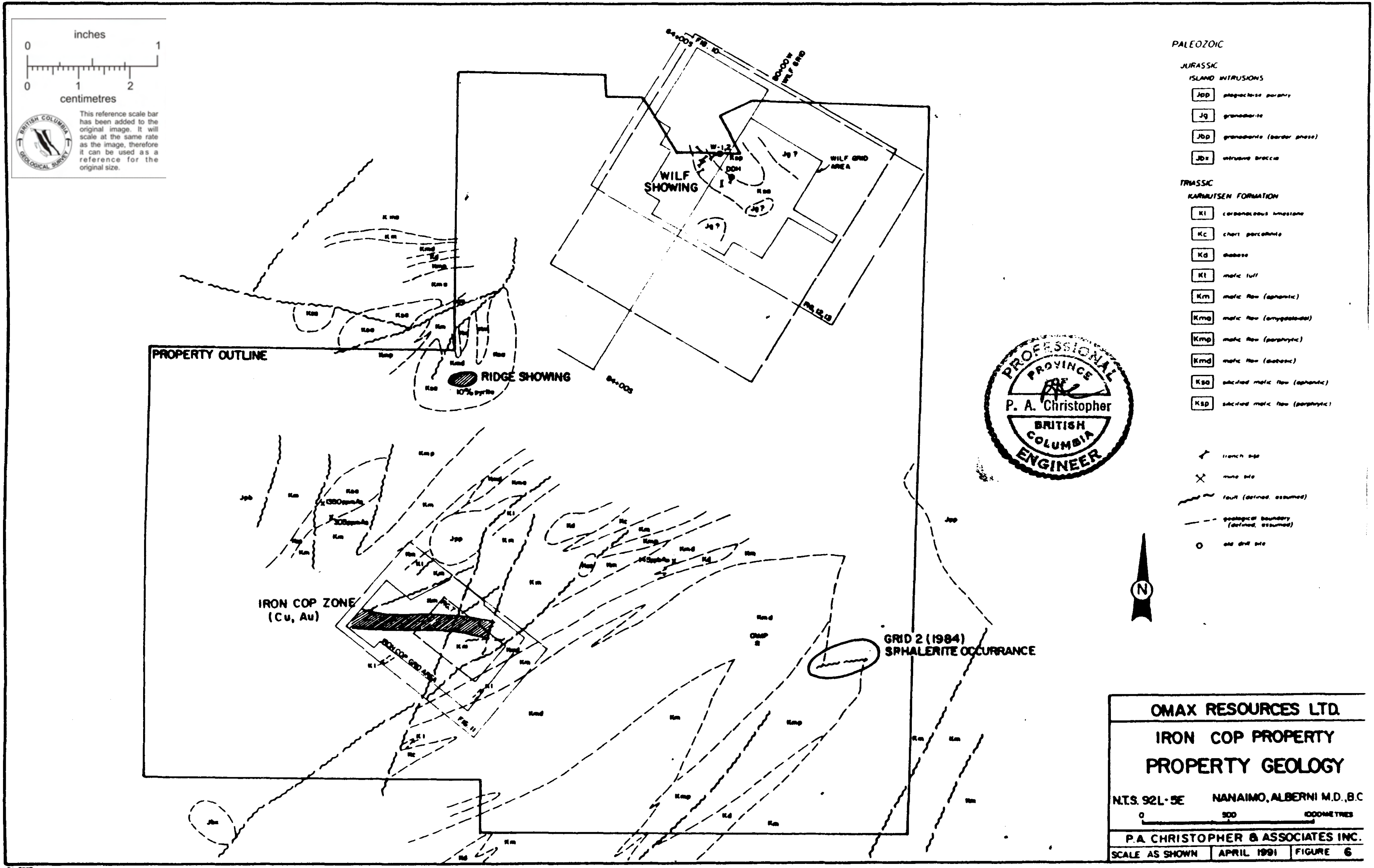
P. A. Christopher

OMAX RESOURCES		
IRON COP PROPERTY SCHEMATIC SECTION		
N.T.S. 92L-5E	NANAIMO, ALBERNI M.D., B.C.	
P.A CHRISTOPHER & ASSOCIATES INC.		
SCALE AS SHOWN	APRIL 1991	FIGURE 5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BRITISH COLUMBIA GEOLOGICAL SURVEY
PROPERTY OUTLINE
WILF SHOWING
WILF GRID AREA
RIDGE SHOWING
10% pyrite
IRON COP ZONE (Cu, Au)
GRID 2 (1984) SPHALERITE OCCURRANCE
FIG. 10
FIG. 11
FIG. 12, 13
PROFESSIONAL ENGINEER
PROVINCE OF BRITISH COLUMBIA
P. A. Christopher
PALEOZOIC
JURASSIC
ISLAND INTRUSIONS
Jpp plagioclase porphyry
Jg granodiorite
Jbp granodiorite (border phase)
Jbx intrusive breccia
TRIASSIC
KARMUTSEN FORMATION
Kl carbonaceous limestone
Kc chert porcellanite
Kd diabase
Kt mafic tuff
Km mafic flow (aphanitic)
Kma mafic flow (amygdaloidal)
Kmp mafic flow (porphyritic)
Kmd mafic flow (diabasic)
Ksa silicified mafic flow (aphanitic)
Ksp silicified mafic flow (porphyritic)
trench site
mine site
fault (defined, assumed)
geological boundary (defined, assumed)
old drill site
N
OMAX RESOURCES LTD.
IRON COP PROPERTY
PROPERTY GEOLOGY
N.T.S. 92L-5E
NANAIMO, ALBERNI M.D., B.C.
0 500 1000METRES
P.A. CHRISTOPHER & ASSOCIATES INC.
SCALE AS SHOWN
APRIL 1991
FIGURE 6

MINERALIZATION

The Iron Cop property contains the Iron Cop, Ridge, Wilf and Grid #2 showings. It has been demonstrated by previous exploration programs to contain several types of mineralized environments. Sulfide rich quartz veins occur in a skarn environment at the Iron Cop showing. A silicified zone at the Ridge showing may reflect epithermal alteration or pipe like breccia zones related to Tertiary intrusives. The Wilf showing is described as fissure filling of quartz-epidote-magnetite-chalcopyrite and pyrite and sphalerite has been identified in a shear zone in Grid #2 (Figure 6).

The Iron Cop zone has yielded the best previous results with a number of high grade grab and chip samples obtained from float, outcrops and trenches (Figure 7). Table 2 summarizes previous trench sample results from the Iron Cop zone.

Table 2. Summary of Iron Cop Zone Trench Sampling.

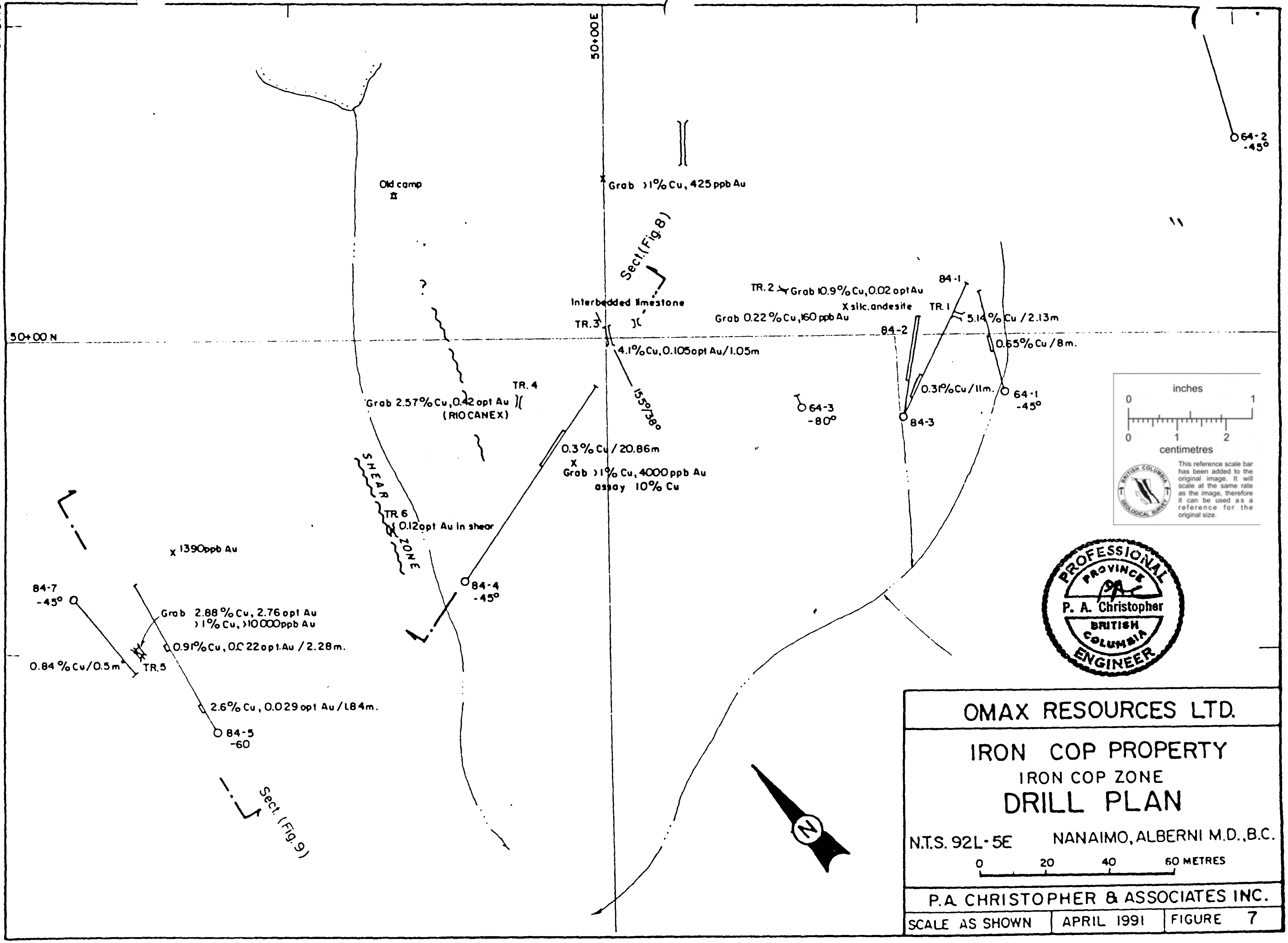
Trench	Width	Copper	Gold	Silver	Sampler
Tr1	2.5 m.	12.2%	0.128 opt	1.27 opt	Brinco, 1984
Tr1	2.1 m.	5.74%	0.09 opt	0.53 opt	Riocanex, 1964
Tr2	0.5 m.	10.90%	0.02 opt	0.60 opt	Riocanex, 1964
Tr3	1.05m.	4.15%	0.105 opt	0.51 opt	Brinco, 1984
Tr4	1.68m.	5.06%	0.127 opt	1.26 opt	Riocanex, 1964
Tr4	grab	2.57%	0.42 opt	1.00 opt	Riocanex, 1964
Tr5	0.3 m.		0.118 opt	0.16 opt	Brinco, 1984
Tr5	grab		2.758 opt		Brinco, 1984
Tr5	grab		1.14 opt	1.25 opt	Riocanex, 1964
Tr6	1.3 m.	0.26%	0.118 opt	0.15 opt	Brinco, 1984

The Iron Cop zone has been partially tested by Riocanex in 1964 with three EX diamond drill holes and by Brinco in 1984 with 7 BQ diamond drill holes. Significant intersections are summarized in Table 3.

Table 3 Summary of Iron Cop Drill Results.

Hole #	Interval	Length	% Cu	PPB Au	Reason For Hole
IC-64-1	17.4-25.5m	8.1m	0.65		Test below Tr1
IC-84-1	9.42-20.69m	11.27m	0.558	185	Test below Tr1
IC-84-2	16.04-41.45m	25.41m	0.341	150	Test below Tr1
IC-84-3	31.09-32.31m	1.22m	0.360	77	Test below Tr1
IC-84-4	60.04-89.90m	29.86m	0.305	192	Test below Tr3
IC-84-5	15.64-17.48m	1.84m	1.63	580	Test below Tr5
	51.00-62.78m	11.34m	0.349	153	" " "
IC-84-7	41.15-43.28m	2.13m	0.13	15	" " "

Drill hole IC-64-1, drilled at 45° below trench 1, contained 26.5 feet (57 to 83.5 feet) grading 0.65% copper. Hole 84-1, drilled below trench 1, was reported by Brinco to contain 11 meters grading > 0.31% copper but geochemical methods reported copper values only up to



OMAX RESOURCES LTD.

IRON COP PROPERTY

IRON COP ZONE

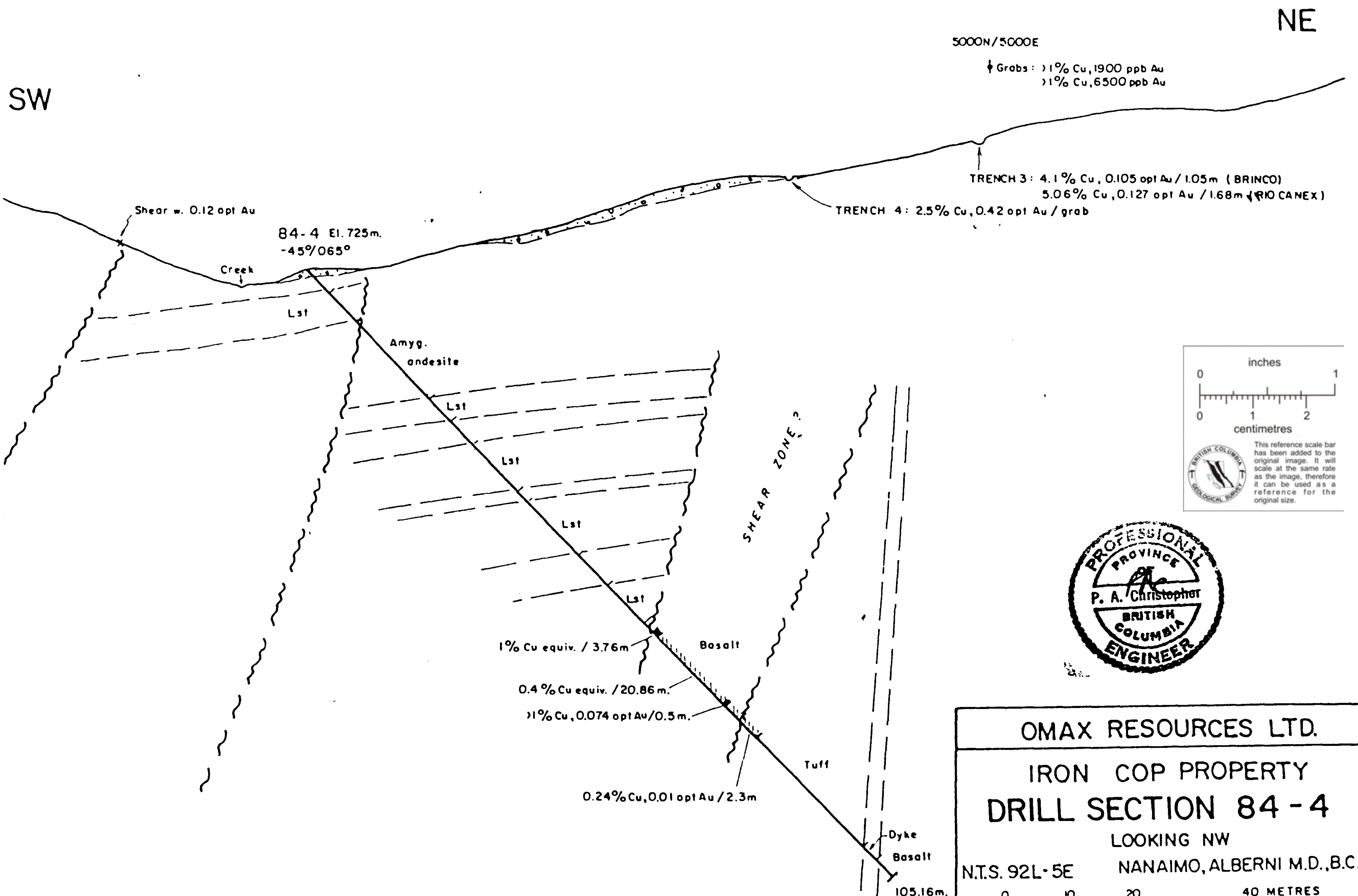
DRILL PLAN

N.T.S. 92L-5E | NANAIMO, ALBERNI M.D., B.C.

0 20 40 60 METRES

P.A. CHRISTOPHER & ASSOCIATES INC.

SCALE AS SHOWN | APRIL 1991 | FIGURE 7



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IRON COP PROPERTY

DRILL SECTION 84-4

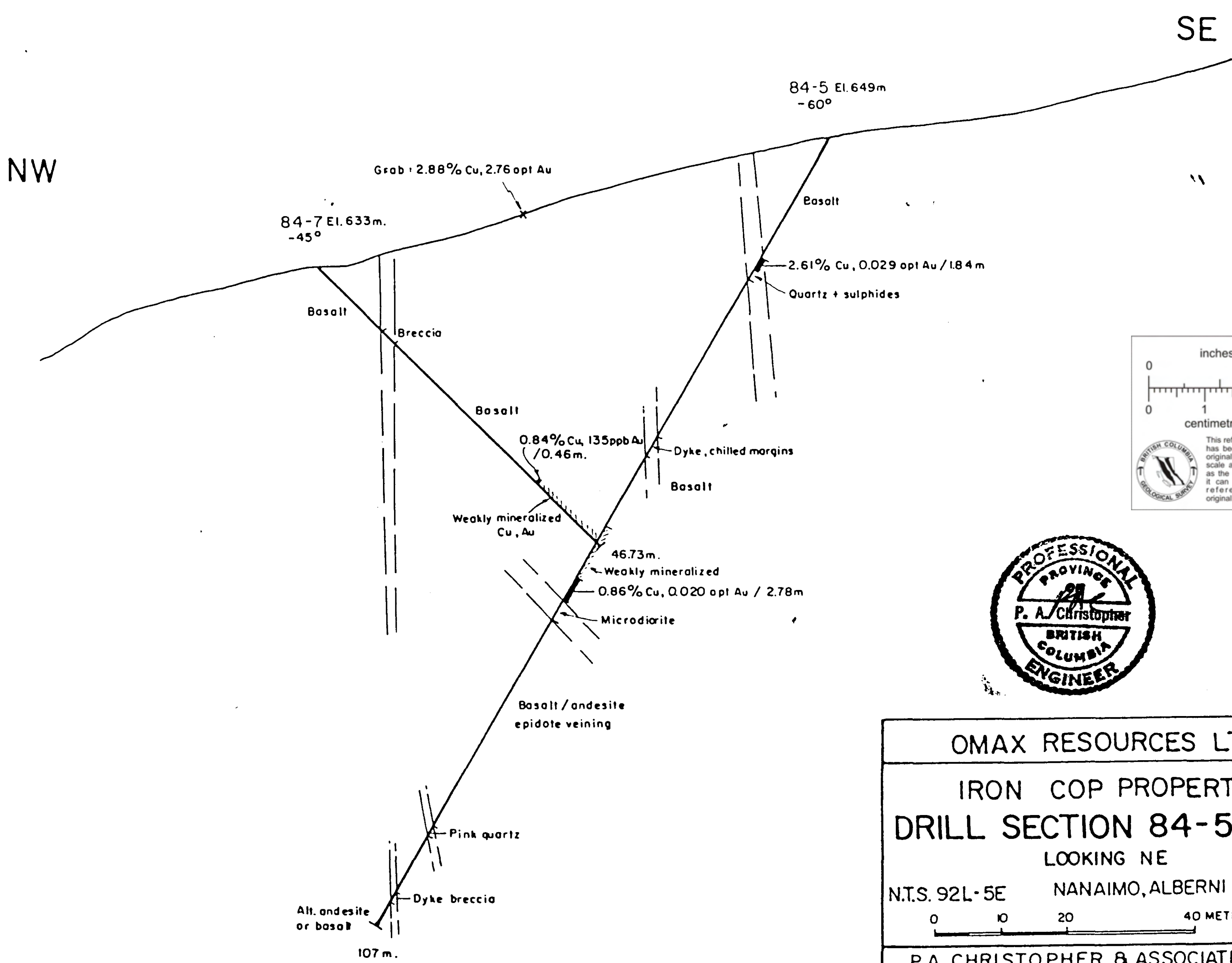
LOOKING NW

N.T.S. 92L-5E — NANAIMO, ALBERNI M.D., B.C.

0 10 20 40 METRES

P.A. CHRISTOPHER & ASSOCIATES INC.

SCALE AS SHOWN	APRIL 1991	FIGURE 8



OMAX RESOURCES LTD.

IRON COP PROPERTY

DRILL SECTION 84-5 & 7

LOOKING NE

N.T.S. 92L-5E — NANAIMO, ALBERNI M.D., B.C.

0 10 20 40 METRES

P.A. CHRISTOPHER & ASSOCIATES INC.

SCALE AS SHOWN	APRIL 1991	FIGURE 9

>10,000ppm. Since a number of the 1984 holes had intervals reported to contain >10,000 ppm copper and/or unassayed intervals, the writer was retained to resample the drill core. Table 4 summarizes the writers sample results which were used in calculating intervals presented in Table 3. The core has suffered minor spillage, but also has had a number of selected specimens removed. The specimens are generally from better mineralized sections and previous high grading probably resulted in lower interval grades.

Table 4. Summary of the writer's samples from 1984 core.

Number	Hole	Interval (m.)	Length	Cu PPM	Au PPB	Cu%
59451	IC84-6	85.37-90.00	4.63	149	6	
59452	IC84-6	73.17-75.50	2.33	107	3	
59453	IC84-7	41.15-43.28	2.13	1322	15	
59454	IC84-5	15.64-17.48	1.84	14024	540	0.82
59455	IC84-5	51.00-53.40	2.40	2653	60	
59456	IC84-4	61.04-61.76	0.72	16527	510	1.11
59457	IC84-4	62.48-63.14	0.66	9950	340	
59458	IC84-4	67.53-68.58	1.05	7570	166	
59459	IC84-4	75.10-75.67	0.55	11585	1250	0.91
59460	IC84-2	16.04-17.04	1.00	14599	340	0.97
59461	IC84-2	17.04-18.04	1.00	4347	109	
59462	IC84-2	18.04-18.54	0.50	38783	1520	2.75
59463	IC84-2	23.01-26.21	3.20	562	20	
59464	IC84-2	26.21-29.26	3.04	166	10	
59465	IC84-2	29.26-32.50	3.24	146	2	
59466	IC84-2	32.50-35.35	2.85	261	5	
59467	IC84-1	9.42-10.42	1.00	36558	410	3.22
59468	IC84-1	18.00-18.36	0.36	22057	1090	1.94
59469	IC84-3	31.09-32.31	1.22	3635	77	

Iron Cop drill hole locations and previous trench assay results are summarized on in plan form on Figure 7 with sections for drill holes 84-4, 84-5 and 84-7 presented as Figures 8 and 9. The sections show the interlayering of altered volcanics and limestone at the Iron Cop showing.

The Wilf showing was tested in 1964 by Riocanex with two holes drilled from the same site. Hole W-1 was drilled for 294.4 feet with the initial 100.8 feet averaging 0.19% copper and the final 41.8 feet averaging 0.~~19%~~ copper. A second hole, apparently drilled in 1974, was located during the 1990 field program in the Wilf Grid area (Figure 6) but no data is available for the hole.

Sphalerite was reported by Epp (1984) to occur in a shear zone within the Grid 2 area (Figure 6) but little additional data remains for this area. Prospecting should be conducted to relocate and sample the showing.

The Ridge showing represents a large altered, pyritic area which requires additional prospecting. Limited sampling by Sketchley (1989) revealed only weakly anomalous rock values for arsenic (to 71 ppm) and gold (to 30 ppb).

GEOCHEMICAL SURVEYS (Figures 10 & 11)

Wilf Grid

In 1990, Omax Resources Ltd. collected 436 soil samples from the Wilf Grid area. Samples were obtained at 25 meter intervals on lines spaced at 50 meter intervals. Holes 20-30 cm. were dug to sample B-horizon soil. Soils were often poorly developed below a thick humus layer. Samples were dried and shipped to Acme Analytical Laboratories Ltd. in Vancouver, B.C. for 32 element ICP and assay/AA gold analyses. Sample locations are plotted on Figure 10 with gold values $\geq$ 10 ppb plotted and areas with $\geq$ 75 ppm copper, $\geq$ 10 ppm molybdenum, and $\geq$ 30 ppm arsenic outline. Certificates of analyses are included in appendix A.

Gold

Gold values in soils varied from the detection limit of 1 ppb to 450 ppb with four the values above ten plotted on Figure 10. The strongest gold response occurs with anomalous arsenic at the northeast margin of the grid. The strongest gold response is north of the property boundary.

Copper

Copper values in soils varied from 1 ppm to 478 ppm at 72+00S/ 77+50W with 18 values of $\geq$ 75 ppm outline on Figure 10. The largest anomalous zone contains ten samples and is situated west of the previously trenched copper showings. The poor copper response from area of known copper mineralization (ie. holes W-1 & W-2) suggests that soil geochemical method has not worked well.

Arsenic

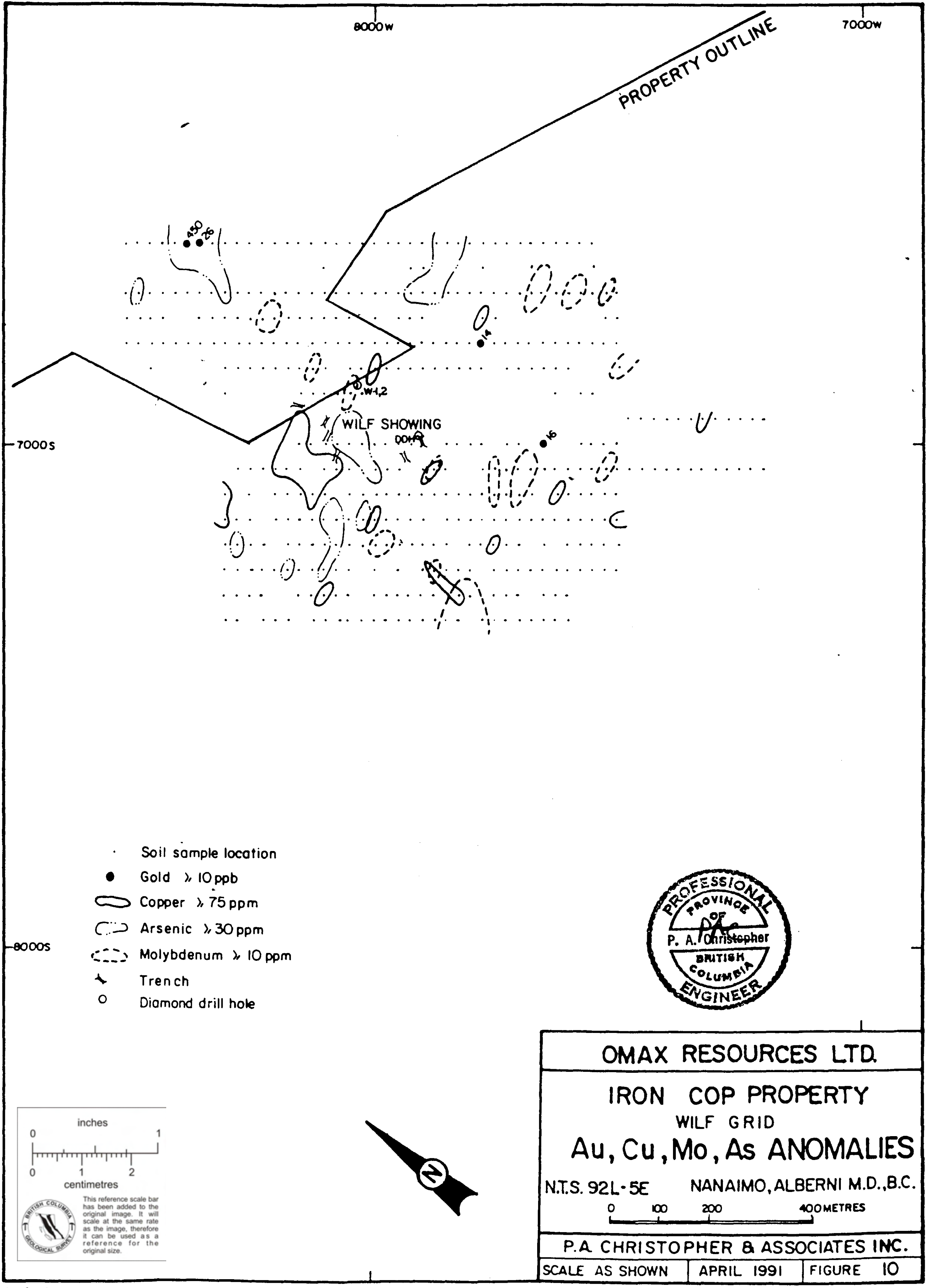
Arsenic values in soils varied from 2 ppm to 203 ppm at 67+00S/ 85+00W with 17 values of $\geq$ 30 ppm outlined on Figure 10. The strongest arsenic response occurs in the northeast part of the grid area with a northerly trend of anomalous arsenic values passing through the Wilf Showing area.

Molybdenum

Molybdenum values in soils varied from 1 ppm to 120 ppm at 72+50S/ 78+75W with 27 values $\geq$ 10 ppm outlined on Figure 10. Anomalous molybdenum values mainly occur south and east of the Wilf Showing and are generally separated from other anomalous elements.

Iron Cop Grid

Soil geochemistry in the Iron Cop Grid area was completed by Riocanex in 1964 with an additional 623 samples collected by Brinco in 1964 (Gonzalez, 1984). Brinco's samples were collected from poorly developed B horizon soils and sent to Chemex Labs Ltd in North Vancouver for Ag, Co, and Cu analyses by atomic absorption, Au by fire assay start and atomic absorption finish, and As by hydride generation method with values over 100 ppm finished with electrodless discharge lamp techniques.



8000W
7000W
PROPERTY OUTLINE
450
26
14
16
W-1,2
WILF SHOWING
DDH-1
7000S
8000S
Soil sample location
Gold ≥ 10 ppb
Copper ≥ 75 ppm
Arsenic ≥ 30 ppm
Molybdenum ≥ 10 ppm
Trench
Diamond drill hole
N
PROFESSIONAL
PROVINCE OF
P. A. Christopher
BRITISH COLUMBIA
ENGINEER
OMAX RESOURCES LTD.
IRON COP PROPERTY
WILF GRID
Au, Cu, Mo, As ANOMALIES
N.T.S. 92L-5E
NANAIMO, ALBERNI M.D., B.C.
0 100 200 400 METRES
P.A. CHRISTOPHER & ASSOCIATES INC.
SCALE AS SHOWN
APRIL 1991
FIGURE 10
inches
0 1
0 1 2
centimetres
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BRITISH COLUMBIA GEOLOGICAL SURVEY

CHONG

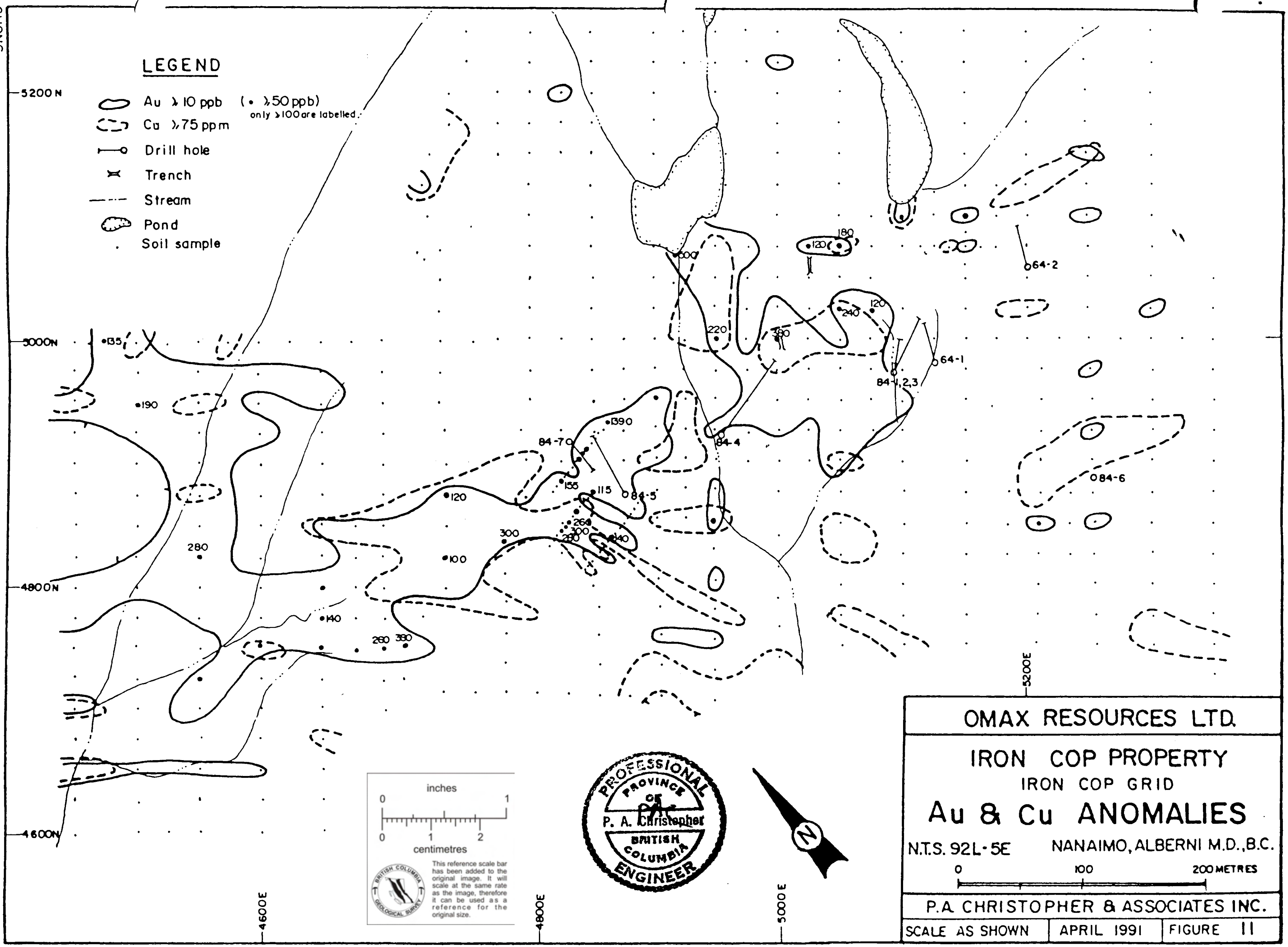

LEGEND
Au ≥ 10 ppb (• ≥ 50 ppb)
only ≥ 100 are labelled.
Cu ≥ 75 ppm
Drill hole
Trench
Stream
Pond
Soil sample
5200N
5000N
4800N
4600N
4600E
4800E
5000E
5200E
135
190
280
140
260
380
120
100
300
260
300
280
155
115
140
1390
84-7
84-5
84-4
500
220
380
240
120
180
120
64-2
64-1
84-1,2,3
84-6
inches
0
1
centimetres
0
1
2
This reference scale bar has been added to the original image. It will scale at the same rate as the image, therefore it can be used as a reference for the original size.
BRITISH COLUMBIA GEOLOGICAL SURVEY
PROFESSIONAL
PROVINCE OF
P. A. Christopher
BRITISH COLUMBIA
ENGINEER
N
OMAX RESOURCES LTD.
IRON COP PROPERTY
IRON COP GRID
Au & Cu ANOMALIES
N.T.S. 92L-5E
NANAIMO, ALBERNI M.D., B.C.
0
100
200 METRES
P.A. CHRISTOPHER & ASSOCIATES INC.
SCALE AS SHOWN
APRIL 1991
FIGURE 11

Figure 11 presents a summary of Gonzalez's (1984) geochemical compilations for gold and copper for the Iron Cop grid area. The original geochemical sheets for the Riocanex and Brinco surveys were not available to the writer.

Gold

Gold values varied from a detection limit of 1 ppb to a maximum of 500 ppb with 22 values over 100 ppb plotted on Figure 11. Gold values $\geq$ 10 ppb are outline on Figure 11 with a 800 meter northwest-southeast trending zone which remains open to the northwest. About 450 meters, from 5100E to 4650E, contains coincident gold and copper values of interest.

Copper

Copper values vary from 2 ppm to 4200 ppm with the strongest copper response in an area of detailed (10m. interval) sampling near drill hole 84-5. A total of 76 values $\geq$ 75 ppm copper are outlined on Figure 11. The anomalous copper zone extends about 200 meters westerly from diamond drill hole IC-84-7, the nearest drill hole.

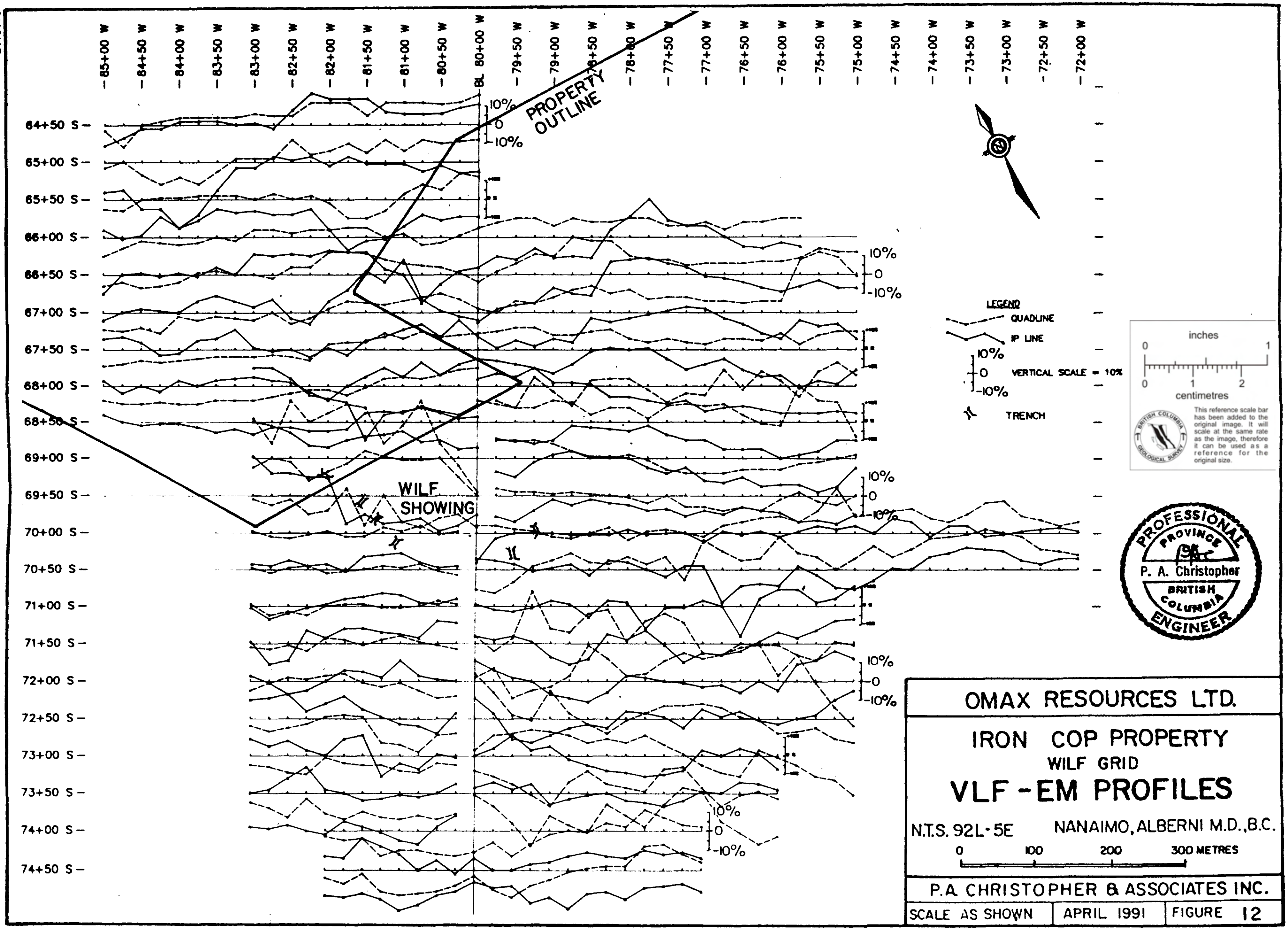
Arsenic

Arsenic values vary from 2 to 800 ppm with 87 values of $\geq$ 50 ppm considered anomalous. The anomalous Arsenic values occur mainly along the southern boundary of the grid area and in the northwest corner of the grid. Arsenic values mainly halo the gold-copper soil anomaly associated with the Iron Cop zone.

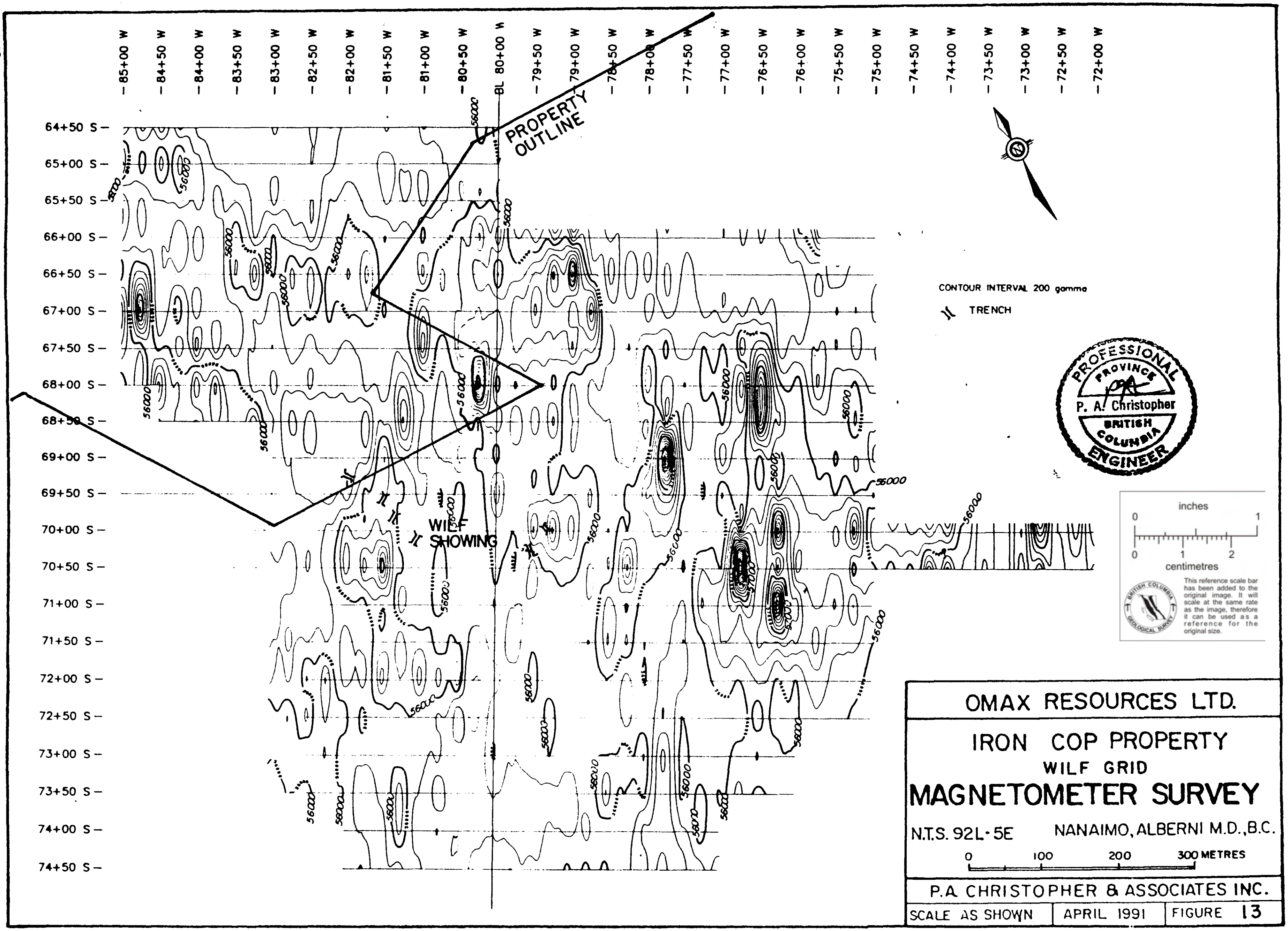
GEOPHYSICAL SURVEYS (Figures 12 & 13)

In 1990, Omax Resources Ltd. conducted magnetic and VLF-Em surveys over the Wilf grid area with about 100 hectares, in the area of the Wilf showing, surveyed. Readings were collected at 25 meter spacing along lines spaced at 50 meter intervals with about 17.2 line kilometers surveyed. A Scintrex MP-2 total field proton magnetometer and a Geonics EM-16 were used for survey readings. The Seattle transmission station was used for VLF-Em readings. Geophysical data was drafted and plotted by New Horizons Software, J.P. Stevenson and Associates and Spectrum Geological Services.

Magnetic values vary from lows of about 55,400 gammas to over 59,400 gammas at 76+75W/75+00S. The magnetic survey readings were corrected for diurnal variations by looping to a base station. Greene (1990) suggested that, "dramatic variations in base station readings were noted and it is possible that without continuous base station readings, errors arising from the interpolation of one base station reading to another, particularly during dramatic magnetic shifts, may have occurred." If the possible effect of diurnal variations is not considered, the magnetic data indicates at least two sets of northeasterly trending, alternating high and low trends which are situated east of the Wilf baseline. A strongly magnetic body which has been cut by a northeast trending fault or shear zone would explain the pattern.



PROPERTY OUTLINE
WILF SHOWING
10%
0
-10%
BL 80+00 W
64+50 S
65+00 S
65+50 S
66+00 S
66+50 S
67+00 S
67+50 S
68+00 S
68+50 S
69+00 S
69+50 S
70+00 S
70+50 S
71+00 S
71+50 S
72+00 S
72+50 S
73+00 S
73+50 S
74+00 S
74+50 S
LEGEND
QUADLINE
IP LINE
VERTICAL SCALE = 10%
TRENCH
inches
centimetres
This reference scale bar has been added to the original image. It will scale at the same rate as the image, therefore it can be used as a reference for the original size.
PROFESSIONAL ENGINEER
PROVINCE OF BRITISH COLUMBIA
P. A. Christopher
OMAX RESOURCES LTD.
IRON COP PROPERTY
WILF GRID
VLF - EM PROFILES
N.T.S. 92L-5E
NANAIMO, ALBERNI M.D., B.C.
0 100 200 300 METRES
P.A. CHRISTOPHER & ASSOCIATES INC.
SCALE AS SHOWN
APRIL 1991
FIGURE 12



OMAX RESOURCES LTD.
IRON COP PROPERTY
WILF GRID
MAGNETOMETER SURVEY
N.T.S. 92L-5E
NANAIMO, ALBERNI M.D., B.C.
0 100 200 300 METRES
P.A. CHRISTOPHER & ASSOCIATES INC.
SCALE AS SHOWN
APRIL 1991
FIGURE 13
CONTOUR INTERVAL 200 gamma
TRENCH
PROPERTY OUTLINE
WILF SHOWING
BL 80+00 W
56000
PROFESSIONAL ENGINEER
PROVINCE OF BRITISH COLUMBIA
P. A. Christopher
inches
centimetres
This reference scale bar has been added to the original image. It will scale at the same rate as the image, therefore it can be used as a reference for the original size.
64+50 S
65+00 S
65+50 S
66+00 S
66+50 S
67+00 S
67+50 S
68+00 S
68+50 S
69+00 S
69+50 S
70+00 S
70+50 S
71+00 S
71+50 S
72+00 S
72+50 S
73+00 S
73+50 S
74+00 S
74+50 S
85+00 W
84+50 W
84+00 W
83+50 W
83+00 W
82+50 W
82+00 W
81+50 W
81+00 W
80+50 W
79+50 W
79+00 W
78+50 W
78+00 W
77+50 W
77+00 W
76+50 W
76+00 W
75+50 W
75+00 W
74+50 W
74+00 W
73+50 W
73+00 W
72+50 W
72+00 W

The VLF-Em data shows a conductive zone which extends from about 81+00W/74+50S to 78+25W/66+00S. The VLF-Em trend corresponds with an area of strong magnetic contrasts which the writer considers to be a fault zone. A weaker VLF-Em anomaly coincides with a magnetic low feature which extends from 78+50W/74+50S to 76+75W/66+00S. Geological mapping and prospecting is required to evaluate the significance of the trends.

Iron Cop

Geophysical exploration of the Iron Cop property was initiated in 1964 by Riocanex with magnetic and self potential surveys conducted over the Iron Cop zone. The self potential survey covered about 6 line miles with a strong anomalous zone (values >250mv) between holes IC-64-1 and IC-84-7. Riocanex magnetic data was not made available to the writer.

A magnetic survey was conducted by Brinco using a Geometrics Portable Proton Magnetometer (Model G-816). The data was compiled by Gonzalez (1984). The survey had magnetic relief of over 11,000 gammas with values ranging from about 53,000 gammas to over 64,000 gammas with 56,000 gammas considered typical background for this area. A 50 meter area with magnetic relief of over 10,000 gammas occurs west of trench 3 at the northwest end of 200 meter (NW-SE) by 100 meter (NE-SW) zone of magnetic values over 57,000 gammas. The zone of elevated magnetic values is probably caused by pyrrhotite and magnetite skarn exposed in trench 1 and trench 3. Two northeast trending faults which cross the Iron Cop grid are represented by distinct magnetic lows. Magnetic lows correspond with mappable surface traces on the faults which extend from 4650N/4450E to 5000N/4500E and from 4650N/4550E to 5250N/ 4950E.

DISCUSSION

Previous exploration on the Iron Cop property has located the Iron Cop, Wilf, Ridge and Grid 2 showings with the Wilf and Iron Cop grid areas receiving the most attention. Their have been repeated attempts by major mining companies, since Riocanex acquired the property in 1962, to locate bulk tonnage deposits. However, reports of grab samples containing up to 2.88% copper and 2.76 opt gold suggest to the writer that potential exists for high grade, copper-gold vein, shear or skarn targets of interest to junior mining companies.

The Iron Cop zone (Figure 6) has a gold anomaly which extends to the northwest boundary of the Iron Cop grid. The anomaly extends for about 700 meters from about 4400E to 5100E with drill testing restricted to 4825E to 5250E. The anomaly is open to the west and should be defined and evaluated by extending grid geochemical, geophysical and geological coverage and trenching before selecting further drill sites.

Data obtained in 1990 from the Wilf showing requires additional prospecting to determine if further ground acquisition is warranted.

Data obtained in 1990 from the Wilf showing requires additional prospecting to determine if further ground acquisition is warranted.

CONCLUSIONS & RECOMMENDATIONS

The Iron Cop zone has potential for producing concentrations of high grade copper-gold mineralization as vein, shear or skarn type deposits. The zone, of anomalous gold and copper in soils extending west-northwest from the previous Iron Cop drill holes, is a priority target. The anomalous zone extends to the Iron Cop grid boundary and the trend is open to the west.

The Iron Cop grid should be extended to the north and west with geological, geochemical and geophysical coverage. An inducted polarization survey is recommended to define sulphide rich areas and assist with drill site selection. Trenching should be conducted to further evaluate targets before undertaking a helicopter supported drill program.

The 1984 drill core, presently stored at the old Iron Cop camp, should be logged with further samples selected. A prospecting budget should be available for further evaluation of the Wilf, Ridge and Grid 2 showings.

The writer recommends further, success contingent, staged exploration of the Iron Cop Property. A Stage I program, of grid extension, geochemical sampling, geological mapping, induced polarization and trenching for the Iron Cop zone and further prospecting of the Ridge, Wilf and Grid 2 showing, is estimated to cost $90,000. Contingent on the success of the Stage I program, a Stage II, 600 meter drill test is estimated to cost $140,000.

COST STATEMENT

Stage I. Geological, Geochemical, Geophysical, Trenching

Project Preparation	$ 2000
Grid	3000
Personnel	
Geologist	6000
Field Assistants	6000
Consulting	1500
Room & Board	3000
Transportation	
Truck Rental	1500
Airfares	1500
Helicopter Support	8000
I.P Survey and Report	20000
Geochemical Analyses	8000
Consumables & Rentals	2000
Trenching & Blasting	3000
Reporting & Drafting	4500
Recording	3000
G.S.T	5000
Contingency	12000
Stage 1 Total	$ 90000

Stage II. Diamond Drilling (Contingent on Stage I Results)

Project Preparation	$ 2000
Camp & Drill Site Preparation	$ 5000
Reclamation	$ 2000
Personnel	
Geologist	$ 9000
Assistant	$ 5000
Consulting	$ 2000
Room & Board	$ 3000
Transportation	$ 15000
Consumables	$ 2000
Diamond Drilling.. 600 meters @ $ 100/meter	$ 60000
Geochemical Analyses	$ 5000
Reporting & Drafting	$ 5000
G.S.T	$ 9000
Recording	$ 3000
Contingency	$ 13000
Stage II Total	$ 140000

PROFESSIONAL ENGINEER — PROVINCE OF BRITISH COLUMBIA — P. A. Christopher

Peter A. Christopher, Ph.D., P.Eng.
April 30, 1991

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CERTIFICATE

I, Peter A. Christopher, with business address at 3707 West 34th Avenue, Vancouver, British Columbia, do hereby certify that:

1) I am a consulting geological engineer registered with the Association of Professional Engineers of British Columbia since 1976.

2) I am a Fellow of the Geological Association of Canada and a member of the Society of Economic Geologists.

3) I hold a B.Sc. (1966) from the State University of New York at Fredonia, a M.A. (1968) from Dartmouth College and a Ph.D. (1973) from the University of British Columbia.

4) I have been practising my profession as a Geologist for over 25 years.

5) I have no direct or indirect interest, nor do I expect to receive any interest directly or indirectly in the property or securities of Omax Resources Ltd.

6) I have based this report on all available geological data on the property and adjacent mineral prospects. I conducted a personal field examination of the Iron Cop Property between September 10, 1990 and September 13, 1990.

7) I consent to the use of this report by Omax Resources Ltd. in any Prospectus, Filing Statement, or Statement of Material Facts.

PROFESSIONAL ENGINEER PROVINCE OF BRITISH COLUMBIA P. A. Christopher

Peter A. Christopher, Ph.D., P.Eng.
April 30, 1991

APPENDIX I

GEOCHEMICAL ANALYSES

Writer's Samples

1990 Wilf Grid Sampling

IRON COP

GEOCHEMICAL ANALYSIS CERTIFICATE

Peter A. Christopher PROJECT IRON COP File # 90-4597
3707 W. 34th Ave, Vancouver BC V6N 2C9

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Au*
	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	ppm	%	%	%	ppm	ppb
E 59451	1	149	2	42	.2	62	24	949	5.45	146	5	ND	1	74	.2	25	5	52	9.39	.067	2	45	1.76	29	.01	7	.49	.01	.16	2	6
E 59452	1	107	2	39	.3	51	32	1096	7.75	76	5	ND	1	94	.2	14	3	89	5.61	.025	2	49	2.51	53	.02	8	1.04	.04	.09	2	3
E 59453	6	1322	2	31	.3	40	13	1295	6.14	4	5	ND	1	39	.3	6	2	71	6.35	.096	3	53	2.32	37	.02	4	3.01	.01	.15	1	15
E 59454	34	14024	8	13	2.8	47	92	1108	8.31	2	5	ND	1	36	.6	7	4	78	13.81	.023	2	68	1.82	2	.02	3	2.42	.01	.03	1	540
E 59455	48	2653	4	38	.5	32	25	1077	6.34	2	5	ND	1	63	.2	6	4	82	6.93	.110	2	46	1.92	31	.01	6	2.58	.01	.15	1	60
E 59456	9	16527	9	16	2.1	107	118	650	11.24	4	5	ND	1	77	1.6	13	4	88	4.50	.109	2	95	2.52	41	.04	8	3.02	.02	.12	1	510
E 59457	11	9950	15	41	3.3	98	59	687	11.29	48	5	ND	1	109	.8	61	2	104	3.13	.228	3	143	2.66	17	.01	6	3.38	.01	.08	1	340
E 59458	9	7570	7	33	1.4	89	46	542	9.27	3	5	ND	1	13	1.4	8	2	82	1.40	.056	2	128	2.51	38	.18	9	2.88	.08	.15	1	166
E 59459	9	11585	22	147	5.2	32	39	405	2.84	177	5	ND	1	28	2.8	2	2	13	3.28	.022	2	16	.28	9	.01	3	.41	.01	.05	1	1250
E 59460	40	14599	11	41	2.4	64	78	720	14.33	2	5	ND	1	25	1.7	8	3	87	3.76	.322	2	25	2.17	32	.12	5	2.72	.01	.06	1	340
E 59461	4	4347	12	52	.9	58	34	1059	10.66	2	5	ND	1	32	1.0	7	2	174	5.23	.049	2	72	2.64	6	.15	6	2.95	.02	.05	1	109
E 59462	4	38783	2	47	3.5	99	108	950	15.06	2	5	ND	1	31	2.5	8	12	116	4.54	.135	2	65	2.31	15	.10	6	2.73	.01	.04	1	1520
E 59463	2	562	2	12	.2	31	27	427	4.88	2	5	ND	1	24	.6	2	5	123	2.79	.090	2	49	1.56	10	.28	5	2.07	.07	.04	1	20
E 59464	1	166	2	20	.2	8	22	467	5.35	2	5	ND	1	18	.7	2	2	60	2.69	.315	2	14	1.17	8	.18	4	1.86	.05	.05	1	10
E 59465	1	146	2	20	.3	11	17	430	5.68	2	5	ND	1	16	.4	3	2	79	2.15	.261	2	15	1.10	8	.19	5	1.41	.08	.04	1	2
E 59466	1	261	2	21	.3	17	15	404	6.04	2	5	ND	1	14	.6	2	2	121	1.94	.067	2	20	1.15	7	.21	3	1.53	.06	.04	1	5
E 59467	1	36558	3	13	2.5	57	54	610	9.08	2	5	ND	1	15	2.8	5	10	122	2.68	.042	2	38	1.39	7	.15	4	1.64	.07	.05	1	410
E 59468	13	22057	9	44	2.8	96	91	995	11.88	2	5	ND	1	47	2.1	5	8	54	5.89	.361	2	19	1.99	11	.09	5	2.66	.01	.05	1	1090
E 59469	1	3635	12	32	.8	38	27	748	8.12	2	5	ND	1	13	.4	6	2	105	3.00	.151	2	61	2.52	21	.12	5	3.15	.03	.07	1	77
STANDARD C/AU-R	18	61	44	135	7.3	72	31	1059	3.99	40	21	7	38	52	18.6	15	21	55	.53	.098	37	60	.90	181	.07	38	1.90	.06	.14	12	520

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: CORE AU* ANALYSIS BY ACID LEACH/AA FROM 20 GM SAMPLE.

DATE RECEIVED: SEP 19 1990 DATE REPORT MAILED: Sept 25/90 SIGNED BY [signature] D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

ASSAY RECOMMENDED for Cu >1%
(In Progress).

ACME ANALYTICAL LABORATORIES LTD.
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE(604)253-3158 FAX(604)253-1716

DATE RECEIVED: SEP 25 1990

DATE REPORT MAILED: Oct. 1/90.

ASSAY CERTIFICATE

Peter A. Christopher PROJECT IRON COP FILE # 90-4597R

SAMPLE#	Cu %
E 59454	.82
E 59456	1.11
E 59459	.91
E 59460	.97
E 59462	2.75
E 59467	3.22
E 59468	1.94

- 1 GM SAMPLE LEACHED IN 50 ML AQUA - REGIA, ANALYSIS BY ICP.
- SAMPLE TYPE: CORE PULP

SIGNED BY.......... D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

Stevenson & Assoc. PROJECT WILF File # 90-3341 Page 1

303 - 475 Howe St., Vancouver BC V6B 2C3 Submitted by: HUGH GREMFAL

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
WF 67+00S 85+00W	1	4	10	38	.2	18	6	144	7.19	203	5	ND	1	9	.2	2	2	178	.10	.029	2	51	.44	3	.06	2	1.48	.01	.02	1	4
WF 67+00S 84+75W	1	23	2	21	.1	5	10	118	10.49	29	5	ND	1	10	.2	2	2	293	.10	.026	2	46	.13	1	.40	2	1.27	.01	.01	1	3
WF 67+00S 84+50W	1	12	4	30	.1	7	12	134	8.74	7	5	ND	1	10	.2	2	2	198	.10	.028	5	49	.20	2	.22	2	1.74	.01	.01	1	3
WF 67+00S 84+25W	1	24	2	35	.3	10	13	149	17.03	12	5	ND	1	9	.2	5	2	239	.08	.044	2	109	.33	3	.21	2	3.50	.01	.02	1	4
WF 67+00S 84+00W	1	22	8	42	.3	10	11	163	16.91	14	5	ND	1	9	.2	7	2	239	.09	.052	4	102	.31	4	.23	4	3.71	.01	.02	1	1
WF 67+00S 83+75W P	1	11	8	36	.2	8	15	128	6.69	8	5	ND	1	18	.2	3	2	136	.20	.048	4	32	.22	5	.20	3	1.24	.03	.03	1	3
WF 67+00S 83+50W P	1	38	2	66	.3	26	32	423	10.73	14	5	ND	1	16	.5	8	2	113	.19	.042	2	74	1.60	7	.15	2	3.66	.01	.02	1	4
WF 67+00S 83+25W P	1	11	5	44	.2	6	13	202	6.23	7	5	ND	1	16	.2	2	2	136	.17	.036	4	20	.17	6	.28	2	1.48	.02	.02	1	1
WF 67+00S 83+00W	5	41	19	78	.1	19	43	269	8.82	45	5	ND	1	12	.3	2	2	134	.18	.026	3	72	.47	16	.19	2	8.79	.01	.02	1	1
WF 67+00S 82+75W	4	9	8	35	.1	4	9	128	5.28	14	5	ND	1	13	.2	2	4	124	.13	.015	4	24	.13	4	.21	2	1.72	.01	.02	1	1
WF 67+00S 82+50W P	2	42	6	92	.1	41	70	543	5.56	21	5	ND	1	31	.2	3	5	90	.62	.045	4	54	1.48	33	.08	3	4.06	.02	.04	1	3
WF 67+00S 82+25W	1	18	10	35	.1	7	7	230	8.11	12	5	ND	1	16	.2	2	2	160	.18	.015	3	40	.39	12	.26	3	1.98	.01	.02	1	1
WF 67+00S 82+00W	1	3	7	32	.1	11	5	184	5.59	7	5	ND	1	10	.2	2	3	146	.10	.012	3	52	.48	5	.15	2	1.94	.01	.02	1	2
WF 67+00S 81+75W	1	1	4	20	.1	6	4	71	1.74	2	5	ND	1	18	.2	2	4	122	.19	.011	2	204	.13	1	.24	2	.64	.01	.01	2	2
WF 67+00S 81+50W	1	1	6	21	.1	16	7	177	5.57	6	5	ND	1	7	.2	2	5	266	.06	.013	2	142	.43	2	.15	2	1.27	.01	.01	1	1
WF 67+00S 81+25W	1	1	6	39	.2	11	9	166	5.49	7	5	ND	1	7	.2	2	4	271	.07	.011	2	152	.11	2	.18	4	.98	.01	.01	2	1
WF 67+00S 81+00W	1	18	11	22	.1	1	2	72	3.67	6	5	ND	1	11	.2	2	2	173	.12	.007	6	23	.07	2	.13	2	1.82	.01	.01	1	1
WF 67+00S 80+75W	1	26	7	43	.2	15	10	347	4.69	10	5	ND	1	22	.2	2	2	101	.24	.015	5	37	.87	20	.16	2	2.25	.01	.03	1	2
WF 67+00S 80+50W	1	32	10	23	.1	7	5	194	2.31	4	5	ND	1	16	.2	2	4	152	.17	.010	5	36	.52	7	.23	2	2.53	.01	.02	1	1
WF 67+00S 80+25W	1	9	3	21	.1	3	3	118	3.58	8	5	ND	1	15	.2	2	2	101	.14	.007	6	21	.24	3	.12	3	1.73	.01	.01	1	4
WF 67+00S 80+00W	1	19	5	41	.1	10	7	255	5.77	11	5	ND	1	15	.2	3	4	94	.15	.021	7	40	.57	11	.11	2	2.93	.01	.02	1	1
WF 67+00S 79+75W	1	20	4	49	.2	16	10	357	4.32	9	5	ND	1	19	.2	2	2	93	.18	.017	7	33	1.00	13	.12	2	2.80	.01	.03	1	3
WF 67+00S 79+50W	1	8	6	20	.1	2	3	81	4.52	24	5	ND	1	8	.2	2	2	103	.07	.015	9	15	.17	4	.05	2	2.19	.01	.01	1	1
WF 67+00S 79+25W	5	10	10	23	.2	2	3	72	4.67	31	5	ND	2	7	.2	2	3	106	.07	.021	11	19	.15	4	.03	2	3.14	.01	.01	1	3
WF 67+00S 79+00W	2	10	5	22	.1	2	4	85	5.54	44	5	ND	2	6	.2	2	4	93	.05	.016	14	13	.06	3	.06	2	1.19	.01	.02	1	1
WF 67+00S 78+75W	1	17	8	43	.1	2	7	166	5.07	33	5	ND	1	5	.2	2	2	122	.03	.017	14	5	.04	3	.03	2	1.10	.01	.01	1	2
WF 67+00S 78+50W	3	1	11	17	.1	1	2	31	3.40	16	5	ND	2	5	.3	2	2	54	.03	.013	11	3	.06	4	.01	2	1.63	.01	.02	1	1
WF 67+00S 78+25W	1	4	8	17	.1	3	3	108	5.64	13	5	ND	1	13	.2	2	2	130	.14	.015	10	10	.28	4	.06	2	1.50	.01	.01	1	2
WF 67+00S 78+00W	2	14	10	39	.1	7	8	388	3.50	8	5	ND	1	8	.2	2	2	43	.08	.029	11	12	.32	13	.01	3	1.13	.01	.02	1	1
WF 67+00S 77+75W	8	7	7	26	.1	1	6	129	6.66	10	5	ND	1	6	.2	2	2	121	.04	.021	10	17	.03	2	.05	2	1.29	.01	.01	1	1
WF 67+00S 77+50W	1	5	4	23	.1	1	1	92	8.00	7	6	ND	1	17	.2	2	3	209	.13	.027	4	17	.16	1	.44	2	1.32	.01	.01	1	1
WF 67+00S 77+25W	1	3	5	30	.1	1	2	97	1.50	3	5	ND	1	10	.6	2	2	62	.10	.017	9	10	.28	5	.03	2	1.26	.01	.02	1	1
WF 67+00S 77+00W	1	7	7	22	.1	5	5	123	7.60	12	5	ND	1	9	.2	3	2	156	.09	.020	6	34	.38	4	.07	2	2.48	.01	.01	1	1
WF 67+00S 76+75W	20	3	11	29	.2	1	105	1501	12.13	5	5	ND	2	10	.2	2	2	135	.09	.046	4	41	.08	4	.14	2	2.72	.01	.02	1	1
WF 67+00S 76+50W	14	3	6	20	.1	1	6	105	3.11	6	5	ND	1	10	.2	2	5	114	.10	.011	5	16	.04	2	.13	3	.77	.01	.01	1	1
WF 67+00S 76+25W	5	4	11	17	.1	1	1	66	2.61	3	5	ND	1	15	.2	2	2	100	.24	.015	4	7	.07	2	.17	2	.87	.01	.01	1	5
STANDARD C/AU-S	18	58	36	131	6.9	68	31	1051	3.97	40	18	7	37	51	18.3	15	19	55	.50	.096	36	56	.87	183	.08	33	1.90	.06	.14	13	47

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: Soil -80 Mesh AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

P = PULVERIZING

DATE RECEIVED: AUG 9 1990 DATE REPORT MAILED: Aug 16/90. SIGNED BY: C. Leong ...D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
WF 67+00S 76+00W	24	2	9	26	.2	7	49	235	6.55	12	5	ND	1	13	.2	2	2	162	.14	.024	4	32	.23	3	.19	3	1.83	.01	.03	1	2
WF 67+00S 75+75W	20	2	13	36	.2	7	66	361	6.03	10	5	ND	1	15	.2	2	2	123	.17	.032	3	33	.21	3	.18	2	1.92	.01	.03	1	3
WF 67+00S 75+50W	7	1	8	27	.2	15	40	1295	3.38	8	5	ND	1	20	.2	2	2	148	.28	.018	2	47	.62	2	.40	4	1.13	.02	.02	1	5
WF 67+00S 75+25W	19	4	10	69	.5	10	247	4136	13.32	14	5	ND	1	16	.2	3	2	152	.14	.042	2	63	.16	29	.09	4	2.96	.01	.02	1	4
WF 67+00S 75+00W	4	4	10	41	.2	9	22	651	8.26	9	5	ND	1	17	.3	3	2	156	.18	.020	2	58	.30	7	.13	2	1.30	.01	.01	1	1
WF 67+50S 85+00W	1	11	5	14	.3	3	5	56	5.00	10	6	ND	1	16	.2	2	2	349	.16	.024	2	1	.03	1	.55	5	.49	.01	.01	1	2
WF 67+50S 84+75W	1	5	2	9	.1	5	8	56	3.53	19	5	ND	1	10	.2	2	2	139	.08	.019	3	13	.05	1	.18	2	.62	.01	.01	1	2
WF 67+50S 84+50W	1	3	2	12	.1	6	4	50	5.34	6	5	ND	1	8	.2	2	2	206	.08	.024	2	46	.16	1	.14	2	.66	.01	.01	1	4
WF 67+50S 84+25W	1	15	5	54	.1	8	8	90	6.92	7	5	ND	1	12	.2	2	2	126	.13	.064	2	27	.24	6	.16	4	1.52	.02	.03	1	1
WF 67+50S 83+50W	1	2	6	25	.1	6	5	95	3.14	4	6	ND	1	11	.2	2	2	93	.11	.033	3	15	.31	2	.19	8	1.03	.02	.02	1	3
WF 67+50S 83+25W	1	13	5	41	.2	12	16	125	4.68	7	5	ND	1	12	.2	2	3	104	.15	.048	2	20	.34	3	.18	4	1.27	.01	.03	1	2
WF 67+50S 83+00W	2	6	4	29	.1	4	5	66	2.67	5	5	ND	1	6	.2	2	2	59	.07	.024	3	4	.20	3	.12	3	.90	.02	.02	1	6
WF 67+50S 82+75W	2	8	2	88	.1	1	1	2	.07	2	5	ND	1	40	.2	2	2	4	.47	.022	2	2	.18	17	.01	5	.07	.04	.02	3	6
WF 67+50S 82+50W	1	7	2	17	.1	5	7	132	4.44	7	5	ND	1	9	.2	2	5	165	.10	.011	3	21	.14	3	.22	2	.96	.01	.01	1	3
WF 67+50S 82+25W	19	4	9	40	.1	3	4	70	.80	2	9	ND	1	15	.2	2	2	56	.27	.027	2	4	.10	4	.11	4	.35	.02	.03	1	4
WF 67+50S 82+00W	18	31	9	67	.1	19	31	445	7.57	4	5	ND	1	13	.2	3	2	125	.15	.023	2	45	.89	9	.15	3	2.74	.02	.02	2	1
WF 67+50S 81+75W	1	2	3	61	.1	11	4	87	2.32	3	6	ND	1	22	.2	2	2	83	.22	.022	2	111	.20	8	.20	2	.89	.02	.02	1	1
WF 67+50S 81+50W	1	1	2	15	.1	13	14	135	2.76	5	5	ND	1	16	.2	2	2	172	.15	.009	2	204	.22	1	.30	2	.77	.02	.01	2	2
WF 67+50S 81+25W	1	1	9	42	.1	7	2	101	.79	2	5	ND	1	17	.2	2	2	24	.13	.019	2	19	.38	4	.11	3	.53	.02	.02	3	4
WF 67+50S 81+00W	1	1	2	91	.1	3	1	73	.81	2	8	ND	1	27	.2	2	2	36	.25	.033	2	5	.33	2	.11	6	.37	.03	.06	1	2
WF 67+50S 80+75W	1	6	3	18	.1	7	4	147	6.18	6	5	ND	1	17	.2	2	2	193	.15	.014	3	29	.28	6	.31	2	1.61	.01	.02	1	1
WF 67+50S 80+50W	1	2	6	21	.1	2	1	16	.09	2	5	ND	1	11	.2	2	2	44	.04	.007	4	5	.03	2	.12	2	.44	.02	.01	1	1
WF 67+50S 80+00W	1	3	2	129	.1	3	1	20	.12	2	5	ND	1	13	.2	2	2	7	.09	.079	2	3	.06	6	.02	7	.30	.04	.04	1	2
WF 67+50S 79+50W	1	1	8	34	.1	14	1	55	.43	2	6	ND	1	13	.2	2	2	37	.17	.024	3	62	.23	5	.15	5	.64	.02	.03	1	2
WF 67+50S 79+25W	1	5	3	10	.1	3	2	71	5.15	14	5	ND	1	8	.2	2	2	87	.08	.011	11	9	.10	3	.03	2	1.86	.01	.01	1	1
WF 67+50S 79+00W	1	1	2	11	.1	2	1	30	.62	5	5	ND	1	3	.2	2	2	34	.02	.007	20	1	.05	1	.03	3	.53	.01	.01	1	1
WF 67+50S 78+25W	4	32	7	56	.1	14	16	558	5.60	7	5	ND	1	13	.2	2	2	78	.13	.031	10	29	.64	27	.02	2	2.02	.01	.03	1	2
WF 67+50S 77+75W	4	80	9	68	.1	18	9	282	10.27	5	5	ND	1	13	.2	3	2	150	.12	.028	2	61	.71	11	.07	2	2.76	.02	.02	1	1
WF 67+50S 77+50W	2	3	3	37	.1	12	2	77	1.80	2	8	ND	1	18	.2	2	2	52	.15	.055	3	46	.35	6	.12	3	.96	.02	.03	1	3
WF 67+50S 75+25W	4	2	2	33	.1	25	12	294	2.88	3	5	ND	1	16	.2	2	2	106	.19	.017	2	80	1.07	7	.11	3	1.92	.02	.02	1	3
WF 67+50S 75+00W	2	1	6	13	.1	2	1	28	.93	2	5	ND	1	12	.2	2	2	58	.12	.013	3	9	.06	5	.09	2	.50	.01	.01	1	1
WF 68+50S 83+00W	1	12	4	42	.1	15	7	151	5.13	16	5	ND	1	23	.2	2	2	122	.28	.059	2	43	.50	4	.29	4	1.19	.03	.02	1	1
WF 68+50S 82+75W	1	26	7	31	.2	19	10	266	10.38	9	5	ND	1	11	.2	4	2	197	.10	.032	2	48	.83	7	.21	2	2.41	.01	.02	1	3
WF 68+50S 82+50W	1	24	3	52	.1	7	4	99	4.16	2	7	ND	1	11	.2	2	3	67	.08	.095	3	12	.12	10	.10	3	1.26	.02	.05	1	2
WF 68+50S 82+25W	1	6	8	12	.1	2	3	53	3.28	3	5	ND	1	11	.2	2	2	174	.09	.014	3	7	.08	4	.29	2	.90	.01	.02	1	1
WF 68+50S 82+00W	1	13	2	30	.1	11	13	230	4.70	10	5	ND	1	12	.2	2	2	128	.12	.026	3	31	.61	8	.14	2	1.80	.01	.02	1	1
STANDARD C/AU-S	18	60	39	129	7.1	73	31	1053	3.97	42	17	7	37	53	18.5	15	21	55	.51	.098	37	59	.89	180	.07	36	1.91	.06	.14	11	51

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
WF 68+50S 81+75W	1	50	7	39	.1	9	15	309	8.82	6	5	ND	2	12	.2	2	2	177	.12	.052	4	38	.27	12	.19	3	2.43	.02	.07	1	2
WF 68+50S 81+50W	1	9	2	15	.2	6	3	159	6.10	4	5	ND	2	14	.2	2	2	209	.13	.008	5	28	.19	6	.39	3	1.30	.01	.04	1	9
WF 68+50S 81+25W	27	38	18	60	.1	7	367	10976	8.49	4	7	ND	1	14	.2	5	3	151	.19	.057	6	46	.17	25	.14	6	4.17	.02	.07	1	1
WF 68+50S 81+00W	8	17	3	27	.2	7	5	324	6.67	2	5	ND	2	20	.2	3	2	179	.22	.013	5	33	.25	9	.31	3	1.50	.01	.03	1	1
WF 68+50S 80+50W	1	9	3	37	.1	6	2	80	3.79	2	5	ND	1	6	.2	2	2	75	.19	.071	5	19	.15	6	.20	5	1.69	.04	.04	1	2
WF 68+50S 80+25W	1	5	7	12	.1	3	1	23	.54	2	5	ND	1	13	.2	2	2	44	.16	.025	4	6	.10	6	.18	3	.63	.04	.04	1	1
WF 68+50S 80+00W	1	76	4	32	.2	13	2	93	7.19	2	5	ND	2	20	.2	2	2	452	.29	.023	3	25	.89	7	.54	2	1.69	.07	.04	1	9
WF 68+50S 79+75W	1	6	2	94	.1	1	1	17	.30	2	5	ND	1	71	.2	2	2	12	.30	.026	2	1	.30	11	.01	6	.16	.03	.02	1	1
WF 68+50S 79+50W	1	16	4	35	.1	16	5	198	3.90	2	5	ND	1	13	.2	2	2	136	.15	.017	4	78	.87	6	.26	3	1.59	.02	.02	1	1
WF 68+50S 79+25W	1	11	6	22	.2	5	2	91	6.06	8	5	ND	2	12	.2	2	3	232	.12	.011	6	32	.17	4	.26	2	1.31	.01	.03	1	3
WF 68+50S 79+00W	1	6	2	39	.3	12	3	151	4.06	6	5	ND	2	16	.2	2	2	135	.17	.049	5	67	.43	8	.13	3	1.81	.02	.04	1	1
WF 68+50S 78+75W	1	4	5	18	.1	2	1	57	1.97	6	5	ND	3	11	.2	2	2	100	.13	.007	8	14	.15	5	.30	2	.78	.02	.02	1	2
WF 68+50S 78+50W	1	19	4	61	.1	3	5	264	2.43	2	5	ND	1	15	.2	2	2	29	.20	.054	5	6	.64	12	.03	3	1.41	.03	.05	1	2
WF 68+50S 78+25W	1	5	6	65	.1	6	4	247	2.44	2	5	ND	1	13	.2	2	2	50	.11	.044	3	13	1.16	5	.05	4	1.32	.05	.04	1	1
WF 68+50S 78+00W	1	5	6	139	.1	3	1	49	.17	2	5	ND	1	45	.2	2	2	3	.58	.066	2	1	.18	8	.01	11	.18	.06	.09	1	1
WF 68+50S 77+75W	1	7	8	28	.3	10	25	156	8.94	5	8	ND	2	13	.3	3	2	298	.15	.015	4	40	.26	5	.51	4	1.12	.01	.04	1	1
WF 68+50S 77+25W	1	26	3	57	.1	4	2	24	2.02	2	5	ND	1	9	.2	2	2	69	.11	.114	5	15	.06	7	.03	3	1.26	.02	.04	1	1
WF 68+50S 77+00W	1	6	6	70	.1	3	1	12	.54	2	5	ND	1	5	.2	2	2	9	.07	.072	2	3	.02	5	.01	4	.95	.03	.02	2	1
WF 68+50S 76+75W	1	10	8	93	.1	4	1	51	.86	2	5	ND	1	33	.3	2	2	19	.27	.074	2	3	.14	34	.04	8	.37	.04	.08	1	2
WF 68+50S 76+50W	1	51	7	73	.1	5	1	42	1.10	2	5	ND	1	8	.2	2	2	62	.07	.082	7	17	.11	8	.04	3	2.04	.03	.03	1	1
WF 68+50S 76+25W	1	20	4	37	.1	6	5	192	3.93	2	5	ND	2	11	.2	2	2	226	.10	.022	10	16	.85	12	.02	2	2.60	.01	.05	1	1
WF 68+50S 76+00W	1	18	8	40	.2	7	6	230	3.55	2	5	ND	1	16	.2	2	2	94	.17	.035	4	16	.88	9	.08	3	2.01	.03	.03	1	1
WF 68+50S 75+00W	18	15	8	31	.2	11	5	168	1.79	2	5	ND	1	38	.2	2	2	68	.30	.027	8	24	.64	67	.06	3	1.72	.02	.04	2	1
WF 69+50S 74+75W	5	10	8	37	.1	10	4	85	9.44	4	5	ND	1	11	.2	2	2	107	.08	.017	2	28	.24	7	.06	3	1.64	.02	.03	1	2
WF 69+50S 74+50W	4	8	7	30	.1	7	3	66	8.48	2	5	ND	1	7	.2	2	2	86	.06	.016	2	19	.15	5	.04	2	1.45	.02	.02	1	1
WF 69+50S 74+25W	1	1	4	86	.2	5	1	115	1.69	2	5	ND	1	6	.2	2	3	23	.05	.080	2	59	.08	6	.07	4	.75	.02	.07	1	1
WF 69+50S 74+00W	4	3	4	34	.2	11	6	186	5.23	4	5	ND	1	15	.2	2	2	171	.15	.013	7	30	.70	11	.17	3	2.07	.01	.03	1	2
WF 69+50S 73+75W	1	33	6	51	.2	17	8	264	8.56	11	5	ND	2	17	.2	2	2	197	.13	.015	4	62	.79	9	.23	2	2.88	.01	.03	1	1
WF 69+50S 73+50W	1	21	8	37	.2	13	6	211	9.15	5	5	ND	1	18	.4	2	2	204	.13	.014	4	53	.54	8	.23	2	2.48	.01	.01	1	5
WF 69+50S 73+25W	1	303	5	67	.1	40	18	388	12.31	3	5	ND	2	7	.4	4	2	174	.06	.051	6	59	.31	9	.01	3	1.34	.01	.04	1	1
WF 69+50S 73+00W	1	45	8	48	.3	42	12	352	6.46	6	5	ND	1	22	.2	2	2	129	.25	.038	3	55	1.10	14	.10	3	1.70	.01	.04	1	1
WF 69+50S 72+75W	1	9	6	31	.3	8	3	132	4.02	5	5	ND	1	23	.2	2	2	151	.19	.023	4	29	.32	9	.14	3	1.74	.02	.03	1	1
WF 69+50S 72+50W	1	5	4	26	.3	11	4	173	4.48	7	5	ND	1	19	.2	2	2	182	.16	.015	3	36	.41	8	.19	2	1.90	.01	.02	1	1
WF 69+50S 72+25W	1	19	9	62	.2	30	13	387	8.74	2	5	ND	1	19	.3	2	2	205	.13	.025	3	68	1.31	10	.14	4	3.02	.01	.03	1	2
WF 69+50S 72+00W	1	13	6	94	.5	40	17	521	7.40	2	5	ND	2	27	.2	2	2	173	.30	.033	2	65	1.93	9	.27	3	2.56	.03	.05	1	2
WF 70+00S 82+50W	1	57	7	74	.2	26	38	5223	6.84	2	5	ND	1	37	.2	2	2	101	.53	.140	9	51	1.63	52	.04	2	3.54	.02	.04	1	2
WF 70+00S 81+50W	1	146	8	59	.4	7	55	1303	5.90	8	5	ND	1	8	.2	2	2	52	.10	.182	6	19	.20	13	.04	8	3.37	.03	.06	1	2
STANDARD C/AU-S	18	59	39	129	6.9	72	32	1045	3.96	41	17	7	39	52	18.5	15	19	57	.51	.094	39	59	.89	182	.09	35	1.90	.06	.13	12	49

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
WF 70+00S 81+25W	2	21	2	31	.2	11	15	254	9.19	7	5	ND	1	9	.4	2	7	185	.12	.022	6	45	.40	8	.10	3	1.81	.02	.02	1	1
WF 70+00S 81+00W	3	22	15	82	.2	38	203	9505	8.31	14	5	ND	1	12	.5	2	2	117	.22	.113	4	54	2.00	34	.01	2	3.61	.03	.05	1	1
WF 70+00S 80+75W	1	39	8	85	.2	25	31	1550	9.21	44	5	ND	1	7	.3	2	2	129	.06	.093	9	52	.71	38	.01	2	2.96	.02	.04	1	1
WF 70+00S 80+50W	1	33	7	81	.2	19	22	995	8.65	40	5	ND	1	6	.2	2	2	124	.04	.091	10	44	.49	36	.01	3	2.71	.01	.03	1	1
WF 70+00S 80+25W	1	30	8	79	.3	20	22	1091	8.75	43	5	ND	1	5	.2	2	2	126	.04	.074	9	45	.44	26	.01	2	2.50	.01	.03	1	3
WF 70+00S 79+75W	2	26	2	45	.1	13	11	394	3.64	7	5	ND	1	30	.6	2	2	99	.36	.025	6	30	.85	21	.17	4	2.03	.01	.02	1	1
WF 70+00S 79+50W	1	28	2	43	.1	17	11	413	3.62	5	5	ND	1	30	.3	2	2	95	.36	.024	6	32	.90	18	.17	2	2.07	.01	.02	1	1
WF 70+00S 79+25W	2	16	2	20	.1	5	6	117	6.18	3	5	ND	1	19	.3	2	2	191	.20	.018	6	27	.12	7	.20	2	1.54	.01	.02	1	1
WF 70+00S 79+00W	2	16	5	21	.1	3	6	118	6.92	5	5	ND	1	19	.4	3	2	203	.27	.021	6	29	.15	7	.21	2	1.70	.01	.02	1	1
WF 70+00S 78+50W	4	42	2	40	.1	8	8	207	7.78	8	5	ND	1	12	.2	2	2	125	.14	.020	7	19	.56	6	.11	4	1.93	.01	.02	1	1
WF 70+00S 78+25W	4	44	8	36	.1	7	9	207	10.17	14	5	ND	2	12	.2	2	2	135	.16	.018	6	21	.58	11	.16	4	1.96	.01	.03	1	1
WF 70+00S 78+00W	5	19	2	25	.2	7	7	116	6.87	11	5	ND	1	15	.8	2	4	370	.16	.019	3	36	.46	5	.34	2	1.34	.01	.02	1	1
WF 70+00S 77+75W	5	15	2	19	.2	6	6	90	6.00	7	5	ND	1	14	1.0	2	2	348	.16	.017	3	29	.23	4	.33	2	1.07	.01	.01	1	1
WF 70+00S 77+25W	7	16	3	65	.1	4	5	153	3.34	4	5	ND	1	11	.2	2	2	99	.13	.091	3	11	.40	8	.03	4	1.02	.03	.03	1	1
WF 70+00S 77+00W	7	10	3	36	.1	2	4	103	2.82	2	5	ND	1	10	.2	2	2	85	.12	.073	2	9	.34	4	.04	5	.85	.02	.02	1	1
WF 70+00S 76+75W	1	1	3	18	.1	3	2	69	1.46	2	5	ND	1	8	.2	2	2	130	.10	.011	6	13	.14	3	.34	4	.54	.02	.02	1	7
WF 70+00S 76+50W	2	1	2	14	.1	1	1	33	1.14	2	5	ND	1	6	1.1	2	6	159	.07	.010	7	12	.06	6	.43	3	.54	.01	.01	1	16
WF 70+00S 75+75W	2	1	6	50	.1	35	13	372	11.71	7	5	ND	3	2	.4	2	2	73	.03	.014	4	14	2.65	9	.01	2	4.14	.01	.01	1	1
WF 70+00S 75+50W	2	1	2	51	.1	31	13	334	10.71	9	5	ND	3	5	.8	2	2	75	.06	.015	4	16	2.34	13	.01	2	3.88	.01	.01	1	1
WF 70+00S 75+25W	3	12	10	40	.3	17	11	301	5.26	7	5	ND	4	22	1.2	3	2	170	.26	.014	9	42	.83	19	.30	4	3.33	.02	.03	2	1
WF 70+00S 75+00W	1	8	5	38	.1	12	9	241	4.67	5	5	ND	1	18	.8	2	5	169	.23	.012	8	36	.74	14	.28	3	2.95	.01	.02	1	4
WF 70+50S 82+75W	1	2	2	7	.1	1	2	98	1.40	2	5	ND	1	9	.9	2	2	179	.09	.009	2	11	.06	4	.54	2	.37	.01	.01	1	1
WF 70+50S 82+50W	1	35	2	46	.1	43	23	710	7.34	6	5	ND	1	11	.6	2	2	178	.29	.088	3	73	2.14	8	.19	2	2.55	.04	.04	1	1
WF 70+50S 82+25W	1	10	7	15	.2	13	8	183	7.17	3	5	ND	1	16	.3	2	2	212	.14	.029	2	46	.68	9	.24	2	1.45	.01	.02	1	2
WF 70+50S 82+00W	2	112	6	30	.1	10	16	354	11.68	7	5	ND	1	14	.5	2	2	167	.13	.067	4	46	.71	7	.12	2	2.69	.01	.04	1	1
WF 70+50S 81+75W	1	91	8	45	.3	15	88	2758	7.43	6	5	ND	1	19	.8	2	2	110	.24	.075	3	36	1.29	11	.13	6	2.67	.02	.03	1	1
WF 70+50S 81+50W	1	177	12	48	.1	9	44	766	2.29	2	5	ND	1	12	.2	2	2	39	.13	.148	5	10	.16	16	.03	8	2.08	.02	.07	1	1
WF 70+50S 81+00W	1	139	6	82	.2	37	28	2860	4.30	4	5	ND	1	48	.5	3	4	62	1.70	.123	15	80	1.53	102	.02	4	3.29	.02	.02	2	3
WF 70+50S 80+75W	5	70	5	63	.1	15	15	475	4.93	3	5	ND	1	23	.2	2	2	82	.46	.139	6	46	.81	23	.03	2	2.58	.02	.03	3	1
WF 70+50S 80+50W	2	44	12	77	.2	24	18	660	6.83	30	5	ND	1	10	.2	2	2	104	.13	.064	6	47	.80	20	.01	2	1.69	.01	.05	1	4
WF 70+50S 80+00W	2	60	7	107	.3	30	38	3633	9.04	47	9	ND	1	8	.2	2	2	111	.08	.122	11	51	1.06	41	.01	4	2.49	.01	.06	1	1
WF 70+50S 79+75W	3	46	13	105	.4	21	28	3314	6.26	16	6	ND	1	19	.2	2	4	92	.24	.099	8	41	.76	54	.03	3	2.75	.02	.05	3	1
WF 70+50S 79+50W	2	38	9	107	.2	20	18	841	7.89	11	5	ND	1	14	.2	2	2	107	.13	.058	5	54	.62	12	.04	4	2.29	.01	.02	1	1
WF 70+50S 79+00W	2	19	8	67	.2	23	17	596	5.25	7	5	ND	1	36	.2	2	2	97	.45	.048	5	39	1.67	15	.14	5	2.24	.02	.04	1	1
WF 70+50S 78+75W	38	267	6	91	.1	17	61	1303	9.63	13	5	ND	1	29	.8	2	2	126	.39	.097	7	55	.58	64	.09	5	5.71	.02	.03	3	1
WF 70+50S 78+50W	1	13	2	79	.2	3	3	68	2.52	2	5	ND	1	7	.2	2	4	26	.11	.090	3	7	.04	22	.02	3	1.19	.02	.01	1	1
STANDARD C/AU-S	19	57	42	131	7.0	67	32	1050	3.95	40	20	7	37	52	18.7	15	22	55	.51	.090	37	56	.92	180	.07	36	1.87	.06	.14	11	54

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
WF 70+50S 77+75W	7	54	4	79	.3	12	13	336	7.65	3	5	ND	1	16	1.0	2	2	110	.20	.095	3	33	.56	7	.13	2	2.10	.02	.05	1	2
WF 70+50S 77+50W	15	41	24	90	.6	5	233	11453	6.70	5	5	ND	1	17	1.1	3	9	135	.24	.101	5	26	.11	38	.13	6	1.62	.02	.08	2	1
WF 70+50S 77+25W	10	9	4	17	.2	2	8	423	4.04	2	5	ND	1	12	.8	2	4	168	.11	.014	5	25	.08	4	.22	4	.88	.01	.02	1	1
WF 70+50S 77+00W	19	20	2	43	.2	16	18	684	8.62	5	5	ND	1	14	.3	2	2	219	.17	.027	4	58	.57	7	.20	3	1.84	.01	.03	1	1
WF 70+50S 76+75W	12	17	3	47	.1	22	12	356	8.17	7	5	ND	1	14	1.4	2	2	227	.18	.015	3	56	1.03	7	.27	2	2.93	.01	.02	2	1
WF 70+50S 76+50W	4	3	6	20	.1	5	4	104	1.76	2	5	ND	1	4	.2	2	2	42	.04	.025	7	9	.40	1	.02	4	.96	.02	.02	1	1
WF 70+50S 76+25W	1	6	2	44	.1	2	1	55	.41	2	5	ND	1	8	.3	2	2	19	.03	.041	2	2	.07	2	.03	7	.41	.03	.02	1	2
WF 70+50S 76+00W	1	6	6	52	.2	34	14	399	8.18	3	5	ND	1	26	1.3	2	2	205	.21	.022	2	61	1.51	3	.46	3	1.94	.02	.01	1	1
WF 70+50S 75+75W	1	3	6	59	.3	43	17	475	9.83	7	6	ND	1	15	1.7	2	2	230	.15	.025	2	76	1.85	5	.47	2	2.22	.02	.02	1	5
WF 70+50S 75+50W	2	9	3	22	.2	17	7	154	7.06	5	5	ND	1	12	.6	2	4	198	.14	.011	2	64	.65	2	.24	2	1.60	.01	.02	1	1
WF 70+50S 75+25W	16	73	6	65	.2	27	15	492	7.37	12	5	ND	1	17	.6	2	2	201	.20	.017	5	67	1.61	6	.16	6	3.67	.01	.02	1	1
WF 70+50S 75+00W	3	10	8	34	.1	21	9	376	3.85	2	5	ND	1	7	.5	2	4	79	.12	.011	5	42	.90	6	.11	2	1.49	.01	.02	1	1
WF 70+50S 74+75W	4	7	7	29	.1	3	2	55	1.64	2	5	ND	1	2	.4	2	2	52	.01	.015	10	3	.11	1	.01	4	.45	.03	.01	1	1
WF 70+50S 74+50W	7	18	2	47	.1	1	3	75	2.72	5	5	ND	1	3	.4	2	2	42	.02	.037	12	2	.14	5	.01	5	.69	.03	.02	1	1
WF 70+50S 74+25W	2	31	8	43	.1	7	10	175	9.03	7	5	ND	2	14	1.1	2	2	156	.13	.035	5	47	.33	6	.27	2	3.16	.01	.02	2	1
WF 70+50S 74+00W	2	28	3	33	.1	7	10	149	9.13	9	5	ND	1	14	.9	2	2	166	.13	.033	5	42	.28	5	.26	3	2.93	.02	.03	1	3
WF 70+50S 73+75W	1	46	4	33	.1	12	6	224	2.17	4	5	ND	1	26	.5	2	2	76	.26	.015	4	34	.74	11	.16	2	1.93	.01	.02	1	1
WF 70+50S 73+50W	1	21	2	59	.1	19	14	496	6.84	4	5	ND	1	26	.7	2	3	181	.27	.030	3	43	1.30	6	.23	4	1.82	.03	.03	1	4
WF 70+50S 73+25W	1	38	2	22	.1	7	4	164	2.64	4	5	ND	1	21	.4	2	2	104	.23	.011	4	21	.34	4	.19	5	1.68	.01	.02	1	1
WF 70+50S 73+00W	1	41	5	63	.1	3	1	16	.32	2	5	ND	1	12	.2	2	2	11	.08	.064	2	3	.05	2	.04	10	.40	.02	.04	1	2
WF 70+50S 72+75W	1	17	7	38	.1	17	9	291	3.65	3	5	ND	1	12	.2	2	3	109	.13	.023	6	37	.79	8	.10	4	2.86	.01	.03	1	1
WF 70+50S 72+50W	1	11	11	49	.2	15	10	305	6.47	2	5	ND	1	22	1.2	2	2	168	.20	.013	3	29	.81	9	.38	3	1.89	.02	.03	1	1
WF 70+50S 72+25W	1	6	6	84	.2	29	21	702	8.88	5	5	ND	1	23	1.5	2	4	164	.41	.066	3	34	1.96	8	.35	2	2.34	.03	.03	1	2
WF 70+50S 72+00W	1	72	10	94	.2	42	27	1330	6.09	6	5	ND	1	52	.7	2	2	107	1.05	.064	11	51	2.15	60	.19	11	3.21	.04	.08	1	1
WF 71+00S 83+00W	2	84	3	31	.1	12	15	453	13.16	6	5	ND	1	4	.4	3	2	214	.03	.062	4	56	.49	8	.02	5	2.40	.01	.02	2	1
WF 71+00S 82+50W	1	7	10	18	.1	5	5	94	3.77	2	5	ND	1	5	.2	2	2	147	.03	.027	7	20	.14	2	.02	5	1.04	.01	.01	1	3
WF 71+00S 82+00W	1	38	2	31	.2	13	11	327	10.59	12	5	ND	1	7	.9	2	2	235	.04	.042	4	80	.28	7	.01	2	1.86	.01	.01	1	1
WF 71+00S 81+75W	1	64	3	59	.1	25	17	452	11.27	9	5	ND	1	5	.2	2	2	200	.04	.043	5	88	1.05	9	.01	6	3.38	.01	.02	1	4
WF 71+00S 81+50W	1	9	3	81	.1	89	32	1218	8.20	4	5	ND	1	7	.9	2	2	194	.20	.098	3	178	3.79	29	.01	7	4.07	.02	.04	1	2
WF 71+00S 81+25W	1	88	2	162	.1	77	40	4786	10.79	10	5	ND	1	12	.8	2	2	127	.33	.101	9	113	3.26	218	.01	3	5.17	.01	.06	1	2
WF 71+00S 81+00W	1	9	3	99	.1	6	2	164	.33	3	5	ND	1	25	.2	2	2	6	.56	.054	2	6	.20	11	.01	9	.21	.03	.05	1	3
WF 71+00S 80+50W	3	22	10	94	.4	14	31	1901	8.26	18	5	ND	1	24	.4	2	2	152	.31	.039	5	51	.64	48	.08	2	2.70	.01	.02	2	1
WF 71+00S 80+25W	1	5	7	32	.2	9	9	471	5.80	6	5	ND	1	14	.2	2	2	169	.14	.017	5	26	.44	11	.15	3	1.83	.01	.02	1	1
WF 71+00S 80+00W	1	15	6	37	.2	11	8	257	6.22	7	5	ND	1	8	.2	2	2	123	.08	.037	6	28	.35	6	.03	5	1.72	.01	.03	1	1
WF 71+00S 79+75W	1	40	5	57	.1	11	16	741	9.65	16	5	ND	1	64	.8	2	3	149	.41	.083	5	30	.82	21	.05	5	3.04	.01	.04	2	1
WF 71+00S 79+50W	1	45	14	80	.3	14	19	2303	4.91	14	5	ND	1	7	.2	2	2	62	.11	.067	8	22	.42	56	.01	5	1.77	.01	.08	1	4
STANDARD C/AU-S	18	58	43	131	6.9	70	31	1048	3.95	41	21	7	37	53	18.5	15	22	55	.51	.092	37	56	.90	182	.07	37	1.88	.06	.14	12	52

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
WF 71+00S 79+25W	1	43	9	75	.2	14	17	2078	4.47	22	5	ND	1	5	.3	2	2	55	.10	.068	7	17	.37	55	.01	2	1.63	.01	.06	1	6
WF 71+00S 79+00W	5	9	8	36	.1	13	8	325	3.09	2	5	ND	1	22	.3	2	2	110	.25	.027	4	33	.73	19	.17	3	2.34	.01	.02	1	4
WF 71+00S 78+75W	1	43	14	130	.3	29	26	1963	5.72	9	5	ND	1	22	.8	2	2	86	.46	.069	5	46	1.01	40	.04	4	2.04	.02	.03	1	8
WF 71+00S 78+50W	1	6	10	14	.1	5	3	127	3.79	2	5	ND	1	8	.2	2	2	134	.07	.017	9	15	.25	6	.08	3	1.20	.01	.01	1	3
WF 71+00S 78+25W	1	7	7	13	.2	6	3	214	5.51	2	5	ND	1	12	.3	2	3	183	.13	.011	4	28	.42	5	.22	2	1.55	.01	.01	1	3
WF 71+00S 78+00W	1	7	7	17	.1	4	1	106	1.05	2	7	ND	1	9	.2	2	2	110	.12	.015	5	21	.22	8	.07	2	1.54	.01	.01	1	1
WF 71+00S 77+75W	1	32	5	40	.1	8	8	217	8.51	2	5	ND	1	7	.4	2	2	180	.05	.032	2	30	.30	9	.14	3	1.33	.01	.02	1	5
WF 71+00S 77+50W	11	55	12	38	.1	14	8	260	3.05	3	5	ND	1	13	.3	2	2	99	.13	.022	7	35	.76	17	.08	2	2.20	.01	.03	1	7
WF 71+00S 77+25W	8	42	2	29	.1	25	11	325	7.48	2	5	ND	1	8	.2	2	2	172	.08	.021	3	74	1.41	7	.16	2	2.34	.01	.01	1	3
WF 71+00S 77+00W	11	21	6	31	.1	8	6	235	6.51	2	5	ND	1	12	.3	2	2	121	.17	.029	3	25	.48	8	.13	2	1.44	.01	.03	1	3
WF 71+00S 76+75W	8	10	8	14	.1	2	2	143	3.90	2	5	ND	1	7	.2	2	2	142	.08	.023	6	13	.17	7	.13	2	1.03	.01	.02	1	6
WF 71+00S 76+25W	2	88	16	40	.2	9	38	810	3.90	2	5	ND	1	13	.2	2	2	94	.15	.027	6	27	.40	26	.08	2	2.36	.01	.02	1	1
WF 71+00S 76+00W	1	2	2	13	.1	3	4	36	.66	3	5	ND	1	3	.2	2	2	22	.01	.009	6	1	.08	1	.01	3	.29	.02	.01	1	3
WF 71+00S 76+00W A	1	38	8	23	.2	15	7	294	5.98	2	5	ND	1	7	.2	2	2	165	.07	.025	4	37	.84	8	.09	3	2.25	.01	.02	1	3
WF 71+00S 75+75W	1	19	4	22	.1	6	4	241	5.77	2	5	ND	1	12	.4	2	2	209	.16	.056	2	11	.34	10	.24	4	.69	.02	.03	1	4
WF 71+00S 75+50W P	1	6	3	59	.1	1	1	42	1.09	2	5	ND	1	15	.4	2	2	62	.10	.029	3	4	.06	15	.02	2	.40	.02	.03	1	1
WF 71+00S 75+25W	1	19	7	56	.2	11	7	225	5.74	2	5	ND	1	8	.2	2	2	129	.14	.040	3	18	.53	8	.10	5	1.25	.02	.02	1	1
WF 71+00S 75+00W	1	24	5	88	.2	21	12	397	4.96	2	5	ND	1	7	.2	2	2	100	.11	.054	4	33	.82	11	.01	5	1.92	.01	.03	1	1
WF 71+50S 83+00W	3	131	11	83	.2	25	22	719	7.38	4	5	ND	1	4	.3	2	2	153	.04	.050	2	45	1.46	12	.01	2	3.03	.01	.03	1	3
WF 71+50S 82+75W P	1	47	7	122	.2	28	32	2539	10.16	17	5	ND	1	18	.5	3	2	96	.44	.139	11	42	1.38	65	.01	3	2.42	.01	.05	1	7
WF 71+50S 82+50W P	1	37	8	130	.3	40	30	8322	7.08	23	5	ND	1	30	.4	3	2	87	.73	.168	11	59	1.62	197	.01	4	3.12	.02	.04	1	2
WF 71+50S 82+00W	1	18	8	47	.1	6	6	439	4.35	11	5	ND	1	8	.2	2	2	73	.06	.049	10	12	.33	14	.01	3	1.25	.01	.02	1	1
WF 71+50S 81+75W	1	60	2	65	.1	15	10	517	11.60	11	5	ND	1	5	.6	2	2	147	.04	.036	9	53	.78	15	.01	2	3.47	.01	.02	1	1
WF 71+50S 81+50W	2	19	4	131	.4	27	19	1720	5.92	12	5	ND	1	28	.2	5	2	94	.50	.066	6	52	1.36	82	.04	5	2.63	.01	.02	1	6
WF 71+50S 81+25W	1	15	12	136	.2	13	70	9744	6.31	9	5	ND	1	21	.2	2	4	105	.36	.078	4	38	.51	89	.04	5	2.08	.02	.03	2	1
WF 71+50S 81+00W	1	11	10	44	.2	11	13	820	5.57	33	5	ND	1	10	.2	2	2	123	.11	.039	6	31	.69	14	.03	2	2.00	.01	.02	1	1
WF 71+50S 80+75W	1	19	8	57	.2	17	18	792	6.49	34	5	ND	1	9	.2	2	2	125	.09	.045	5	38	1.02	13	.04	3	2.46	.01	.02	1	1
WF 71+50S 80+50W	1	31	13	83	.2	19	15	632	8.08	8	5	ND	1	27	.2	3	2	179	.24	.058	5	61	1.02	36	.07	3	3.47	.01	.02	1	1
WF 71+50S 80+25W	1	14	10	44	.1	11	12	565	6.78	37	5	ND	1	9	.2	2	3	125	.08	.039	6	34	.61	13	.03	4	2.06	.01	.02	2	1
WF 71+50S 80+00W	1	81	2	95	.2	24	20	1092	9.16	24	5	ND	1	6	.2	4	2	121	.07	.084	9	50	.92	58	.01	2	3.89	.01	.03	1	3
WF 71+50S 79+75W	1	35	16	57	.1	9	14	1000	4.23	11	5	ND	1	3	.2	2	2	52	.04	.059	5	15	.27	26	.01	3	1.70	.01	.05	1	1
WF 71+50S 79+50W P	3	7	14	57	.1	19	11	462	4.17	2	5	ND	1	18	.2	2	2	106	.26	.032	3	39	1.06	11	.17	3	2.10	.02	.02	1	1
WF 71+50S 79+25W	1	5	6	24	.2	18	6	310	4.43	3	5	ND	1	14	.2	2	2	186	.17	.013	3	23	.56	6	.30	5	1.47	.01	.02	1	1
WF 71+50S 79+00W	1	12	14	27	.1	16	7	319	4.19	6	5	ND	1	18	.2	2	2	120	.19	.017	5	35	.75	12	.23	5	2.31	.01	.03	1	2
WF 71+50S 78+50W	1	9	5	37	.1	11	6	333	2.38	3	5	ND	1	17	.2	2	2	66	.24	.022	2	32	.59	6	.08	5	1.12	.02	.02	1	1
WF 71+50S 78+25W	1	28	15	22	.1	6	4	224	2.07	2	5	ND	1	16	.2	2	2	91	.16	.022	3	31	.38	5	.14	3	1.11	.01	.02	1	1
WF 71+50S 78+00W	1	8	10	18	.1	9	3	131	3.92	3	5	ND	1	11	.2	2	2	134	.10	.011	5	28	.28	6	.17	3	1.72	.01	.01	1	2
STANDARD C/AU-S	17	59	41	131	6.9	70	32	1053	3.97	40	16	7	36	51	18.4	15	21	56	.51	.097	36	59	.88	179	.07	37	1.89	.06	.14	12	51

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
WF 71+50S 77+75W	1	32	8	86	.2	17	29	3545	5.78	2	5	ND	1	20	.2	2	2	99	.33	.058	5	32	.72	61	.05	4	2.02	.02	.03	1	1
WF 71+50S 77+50W	1	14	2	22	.1	2	3	154	5.42	2	5	ND	1	12	.2	2	2	174	.11	.017	7	11	.12	8	.19	3	.57	.01	.01	1	2
WF 71+50S 77+25W	1	38	7	58	.1	11	9	254	7.54	2	5	ND	1	11	.2	2	2	167	.09	.032	4	40	.42	9	.13	3	1.88	.01	.02	1	1
WF 71+50S 77+00W	4	24	11	49	.1	2	13	542	5.82	3	5	ND	1	6	.4	2	2	129	.06	.055	4	16	.21	8	.05	2	1.44	.01	.01	2	4
WF 71+50S 76+75W	3	15	6	22	.1	4	5	188	3.66	2	5	ND	1	10	.2	2	2	143	.09	.018	6	21	.23	13	.10	2	1.44	.01	.02	1	4
WF 71+50S 76+50W	2	26	7	25	.1	3	3	152	7.87	5	5	ND	1	7	.2	2	2	229	.06	.022	3	23	.24	8	.15	3	1.40	.01	.01	1	7
WF 71+50S 76+25W	1	33	2	34	.1	4	6	189	10.27	3	5	ND	1	7	.5	3	2	200	.06	.028	3	36	.15	6	.19	2	1.55	.01	.02	1	4
WF 71+50S 76+00W	1	37	3	31	.1	4	30	929	5.58	2	5	ND	1	8	.2	2	2	159	.08	.042	5	21	.23	19	.10	3	1.54	.01	.03	1	1
WF 71+50S 75+75W	2	50	2	50	.1	7	11	498	10.21	3	5	ND	1	9	.2	2	2	208	.11	.033	4	35	.26	39	.12	4	1.98	.01	.02	1	1
WF 71+50S 75+50W	1	12	6	22	.1	1	2	105	4.36	2	5	ND	1	8	.2	2	3	143	.07	.017	3	15	.18	7	.08	2	1.55	.01	.01	1	2
WF 71+50S 75+25W	1	7	6	9	.1	1	3	164	2.98	2	6	ND	1	6	.2	2	2	204	.05	.009	3	7	.11	5	.24	2	.79	.01	.01	1	1
WF 71+50S 75+00W	1	76	11	75	.1	19	17	603	8.03	2	5	ND	1	13	.2	2	2	120	.13	.061	7	47	1.15	22	.02	3	3.20	.01	.03	1	1
WF 72+00S 83+00W	1	66	10	82	.1	8	31	3553	6.29	25	5	ND	1	17	.5	2	2	85	.31	.144	9	10	.32	97	.01	4	1.50	.01	.04	1	1
WF 72+00S 82+75W	1	53	8	110	.3	24	47	4051	7.95	61	5	ND	1	9	.4	6	2	97	.11	.116	9	51	.67	58	.01	2	2.51	.01	.05	1	2
WF 72+00S 82+50W	1	20	3	42	.2	2	28	2461	5.97	3	5	ND	1	6	.3	2	2	101	.09	.054	13	12	.20	28	.01	2	1.35	.01	.02	1	1
WF 72+00S 82+25W	1	2	4	8	.1	1	1	117	1.58	3	5	ND	1	35	.2	2	2	83	.23	.015	3	10	.06	5	.20	2	.64	.01	.02	2	2
WF 72+00S 81+75W	1	17	9	40	.1	2	14	581	12.81	5	5	ND	1	8	.2	2	2	164	.06	.037	4	39	.14	9	.07	3	2.01	.01	.03	1	1
WF 72+00S 81+50W	1	9	5	49	.1	5	7	427	4.58	12	5	ND	1	11	.2	2	2	138	.08	.029	6	30	.58	8	.06	2	1.97	.01	.02	1	1
WF 72+00S 81+25W	3	27	5	97	.4	19	140	17476	12.28	2	5	ND	1	9	.4	5	2	89	.08	.055	3	66	1.00	73	.03	2	3.84	.01	.02	1	2
WF 72+00S 81+00W	1	13	2	15	.1	1	5	402	6.08	11	5	ND	1	3	.6	2	2	130	.02	.022	9	13	.05	9	.01	2	1.16	.01	.01	1	1
WF 72+00S 80+75W	2	39	2	44	.1	31	13	753	10.86	39	5	ND	1	5	.2	2	3	156	.05	.073	6	56	.46	14	.01	2	1.82	.01	.03	1	1
WF 72+00S 80+50W	1	39	2	59	.1	3	8	703	8.06	19	5	ND	1	4	.2	2	2	179	.02	.053	10	1	.06	4	.09	2	.37	.01	.01	1	1
WF 72+00S 80+25W	1	14	5	25	.1	1	3	157	4.57	6	5	ND	1	4	.2	2	2	131	.03	.021	6	11	.04	8	.06	2	.83	.01	.01	1	1
WF 72+00S 80+00W	19	7	6	22	.1	1	3	145	3.05	4	5	ND	1	4	.5	2	2	71	.05	.024	6	10	.06	9	.01	2	1.26	.01	.03	2	1
WF 72+00S 79+75W	18	7	7	21	.1	1	3	175	2.48	5	5	ND	1	4	.2	2	2	48	.03	.021	7	6	.05	10	.01	2	1.18	.01	.04	2	2
WF 72+00S 79+50W	1	6	8	19	.1	4	3	146	4.52	2	5	ND	1	13	.2	2	2	169	.13	.010	4	21	.26	5	.22	2	1.70	.01	.01	1	2
WF 72+00S 79+25W	1	5	6	11	.1	2	2	118	3.72	2	5	ND	1	14	.2	2	2	151	.14	.009	4	18	.20	5	.17	2	1.44	.01	.01	1	1
WF 72+00S 79+00W	2	7	6	28	.1	6	4	216	2.37	2	5	ND	1	23	.2	2	2	74	.22	.012	4	22	.44	8	.18	2	1.84	.01	.02	2	1
WF 72+00S 78+75W	2	7	6	22	.1	5	3	217	1.98	2	5	ND	1	22	.2	2	4	70	.22	.012	4	23	.39	8	.18	2	1.81	.01	.02	2	2
WF 72+00S 78+50W	8	18	5	62	.1	15	10	513	8.52	3	5	ND	1	12	.2	3	2	107	.11	.018	5	47	.87	10	.13	3	2.78	.01	.02	1	2
WF 72+00S 78+00W	1	17	7	19	.1	3	6	217	7.70	4	5	ND	1	6	.2	2	3	246	.06	.013	4	30	.21	3	.30	2	.90	.01	.02	1	1
WF 72+00S 77+75W	1	17	2	32	.1	4	5	184	8.11	9	8	ND	1	6	.2	2	2	249	.05	.014	4	32	.08	3	.28	2	.78	.02	.01	1	1
WF 72+00S 77+50W	1	478	13	69	.1	18	17	762	3.52	2	5	ND	1	21	.4	2	2	72	.31	.079	7	38	.83	32	.05	2	2.21	.03	.03	1	1
WF 72+00S 77+25W	1	20	2	29	.1	2	6	131	4.87	2	5	ND	1	8	.2	2	2	186	.06	.015	5	22	.03	5	.14	3	.32	.02	.01	1	1
WF 72+00S 77+00W	1	17	12	27	.1	5	6	138	4.44	5	5	ND	1	10	.2	2	2	166	.07	.018	4	26	.10	5	.12	3	.36	.02	.02	1	1
WF 72+00S 76+50W	1	37	10	33	.1	9	7	297	4.39	3	5	ND	1	14	.2	2	2	96	.13	.029	4	29	.57	8	.14	2	1.42	.01	.02	2	2
STANDARD C/AU-S	18	59	42	131	7.1	70	32	1052	3.97	39	18	6	36	52	18.9	16	19	56	.51	.097	36	57	.88	179	.08	34	1.89	.06	.14	11	52

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
WF 72+00S 76+00W	6	24	22	69	.1	10	492	20124	11.46	12	6	ND	2	13	.6	2	3	155	.12	.078	5	44	.42	53	.16	8	2.80	.02	.06	1	1
WF 72+00S 75+75W	1	7	13	35	.3	5	6	476	7.65	2	5	ND	1	4	.2	3	2	231	.04	.064	4	35	.20	9	.02	5	2.07	.01	.05	1	1
WF 72+00S 75+50W	1	7	11	35	.3	3	2	170	8.84	2	6	ND	1	4	.2	2	2	238	.04	.059	3	35	.18	8	.03	4	2.08	.01	.04	1	1
WF 72+00S 75+25W	1	25	18	80	.1	16	11	807	10.32	2	5	ND	2	9	.5	2	2	192	.07	.048	5	73	.89	38	.08	4	4.09	.02	.06	1	1
WF 72+00S 75+00W	1	27	15	94	.2	16	14	975	10.95	2	5	ND	2	8	.3	4	2	198	.06	.053	5	76	.84	36	.08	4	4.32	.01	.06	1	1
WF 72+50S 83+00W	1	5	9	26	.3	4	2	118	2.62	10	5	ND	1	14	.2	2	2	127	.13	.042	5	25	.22	9	.11	5	1.74	.01	.03	1	4
WF 72+50S 82+75W	1	9	14	70	.3	13	8	593	5.70	2	5	ND	1	16	.2	2	2	156	.13	.056	4	35	.71	15	.18	5	2.11	.01	.05	1	2
WF 72+50S 82+50W	1	18	12	35	.2	4	5	222	8.80	2	5	ND	1	9	.2	2	2	211	.06	.045	5	28	.25	11	.04	3	2.25	.01	.04	1	1
WF 72+50S 82+25W	1	11	8	25	.2	2	1	58	1.25	2	5	ND	1	20	.2	2	2	88	.15	.061	4	24	.06	9	.11	3	1.70	.01	.03	2	3
WF 72+50S 82+00W	1	29	17	98	.1	10	333	13461	9.01	3	5	ND	1	10	.3	2	2	118	.08	.129	7	40	.46	34	.04	6	3.99	.01	.07	1	2
WF 72+50S 81+75W	1	44	12	74	.2	15	18	1273	9.13	38	5	ND	2	15	.2	4	2	155	.14	.046	6	66	.60	30	.03	3	3.31	.01	.05	1	1
WF 72+50S 81+50W	1	31	10	30	.3	5	8	251	5.95	2	5	ND	1	16	.2	2	2	154	.17	.038	13	31	.20	17	.01	2	1.58	.01	.04	1	1
WF 72+50S 81+25W	1	29	12	85	.3	85	28	601	7.56	6	5	ND	1	11	.2	2	2	126	.10	.043	4	130	2.43	23	.01	2	4.15	.01	.07	1	2
WF 72+50S 81+00W	1	75	12	39	.1	12	9	400	10.70	99	5	ND	1	4	.7	5	2	150	.03	.060	7	39	.63	9	.01	7	3.17	.01	.01	1	2
WF 72+50S 80+75W	1	49	9	113	.1	15	16	2141	5.71	12	5	ND	1	8	.2	2	2	75	.23	.080	8	19	.33	82	.01	4	1.43	.01	.10	1	2
WF 72+50S 80+50W	1	4	7	84	.1	3	3	108	.39	2	5	ND	1	41	.4	2	2	26	.46	.055	2	12	.13	12	.09	9	.25	.05	.04	1	1
WF 72+50S 80+00W	1	26	16	85	.2	13	8	445	10.19	12	5	ND	1	20	1.0	2	2	172	.17	.042	6	53	.79	10	.39	7	3.28	.01	.03	1	1
WF 72+50S 79+50W	2	46	13	50	.3	18	9	435	6.36	5	5	ND	1	27	.3	2	2	158	.26	.023	5	48	.96	10	.45	7	3.13	.01	.02	1	1
WF 72+50S 79+00W	8	13	8	60	.3	22	10	528	4.27	7	5	ND	1	43	.2	3	2	137	.35	.016	6	49	1.29	12	.36	7	2.86	.02	.04	1	1
WF 72+50S 78+75W	120	81	20	49	.1	12	90	393	5.10	9	6	ND	1	16	.2	3	2	134	.15	.069	12	66	.27	17	.23	10	7.27	.01	.03	1	1
WF 72+50S 78+50W	8	16	14	35	.3	9	5	338	7.13	2	5	ND	1	22	.2	2	2	235	.21	.010	4	42	.52	12	.48	3	2.35	.01	.02	1	4
WF 72+50S 78+25W	1	37	9	50	.2	18	9	409	3.17	2	5	ND	1	24	.2	2	2	97	.31	.029	7	40	.99	12	.26	6	2.56	.02	.03	1	3
WF 72+50S 78+00W	1	10	6	33	.3	10	4	321	2.61	2	5	ND	2	24	.2	2	2	159	.22	.010	4	40	.37	14	.21	5	1.45	.02	.03	2	1
WF 72+50S 77+50W	1	5	9	19	.3	3	1	147	3.74	4	5	ND	1	10	.2	2	2	177	.09	.011	6	19	.14	8	.22	2	1.39	.01	.02	1	2
WF 72+50S 77+25W	1	29	11	54	.3	15	8	359	8.96	2	6	ND	2	19	.2	3	2	165	.16	.022	5	51	.78	12	.23	6	2.96	.01	.04	1	1
WF 72+50S 77+00W	2	27	11	80	.3	34	17	1017	6.39	2	5	ND	1	20	.2	3	2	140	.20	.041	5	68	1.29	15	.22	4	3.18	.01	.05	1	1
WF 72+50S 76+75W	1	1	7	32	.2	9	3	222	2.44	2	5	ND	1	27	.2	2	2	109	.20	.021	4	24	.28	6	.31	7	.99	.02	.02	2	1
WF 72+50S 76+50W	1	19	10	22	.3	3	4	184	8.19	2	6	ND	2	8	.2	3	2	206	.06	.029	5	26	.07	8	.26	5	1.56	.01	.03	1	1
WF 72+50S 76+25W	1	8	13	58	.2	10	10	1245	12.60	10	5	ND	1	6	1.1	2	2	215	.33	.173	5	19	1.44	6	.18	3	2.91	.01	.05	1	5
WF 72+50S 76+00W	1	19	7	25	.2	2	5	201	10.19	2	5	ND	1	2	.2	4	2	298	.01	.050	4	16	.07	3	.02	6	1.06	.01	.02	2	3
WF 72+50S 75+75W	1	22	11	67	.4	16	10	345	5.05	2	5	ND	1	13	.2	2	2	126	.12	.041	5	34	.91	13	.05	5	2.66	.01	.04	1	1
WF 72+50S 75+50W	1	29	12	114	.1	25	27	1481	6.41	2	5	ND	1	21	.2	2	3	119	.24	.068	7	48	1.22	64	.05	7	3.15	.02	.06	1	1
WF 72+50S 75+25W	1	4	6	53	.3	9	3	201	4.27	2	5	ND	1	6	.2	2	2	80	.06	.071	4	28	.36	10	.04	4	1.60	.02	.05	1	1
WF 72+50S 75+00W	1	17	6	36	.2	2	3	180	1.95	2	5	ND	1	9	.2	2	2	122	.09	.023	6	12	.14	27	.09	2	1.11	.01	.04	2	2
WF 73+00S 83+00W	1	3	10	21	.2	1	1	68	1.09	2	5	ND	1	10	.2	2	2	57	.08	.028	9	6	.10	12	.05	3	1.10	.02	.04	2	3
WF 73+00S 82+75W	1	11	18	35	.3	2	35	868	16.59	2	6	ND	3	6	.3	2	2	141	.04	.053	8	22	.18	14	.03	3	2.93	.01	.06	1	1
STANDARD C/AU-S	18	57	41	130	6.9	72	32	1047	3.96	42	18	7	38	53	18.5	15	18	57	.52	.098	38	59	.89	181	.09	36	1.89	.06	.14	11	48

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
WF 73+00S 82+50W	1	4	3	27	.2	2	4	201	5.96	2	5	ND	1	6	.2	2	2	92	.17	.042	16	4	.27	20	.05	2	1.19	.01	.04	1	2
WF 73+00S 82+25W	1	32	8	72	.2	9	7	540	9.71	7	7	ND	2	3	.2	3	2	135	.04	.064	8	49	.52	20	.01	2	4.83	.01	.05	1	2
WF 73+00S 81+50W	1	9	7	52	.3	19	8	340	4.35	6	5	ND	2	6	.2	2	2	135	.05	.035	6	55	.69	15	.02	2	3.09	.01	.05	1	1
WF 73+00S 81+25W	1	18	6	46	.3	13	5	259	7.30	12	5	ND	2	4	.2	2	2	204	.03	.061	3	46	.43	12	.01	2	1.65	.02	.06	1	4
WF 73+00S 81+00W	1	103	10	203	.2	14	16	823	13.29	13	6	ND	2	3	.2	3	4	139	.06	.120	8	15	.17	30	.01	3	1.63	.01	.08	1	1
WF 73+00S 80+75W	1	14	4	31	.2	4	5	236	5.03	6	5	ND	2	6	.2	2	2	204	.05	.013	6	20	.03	6	.22	4	.44	.01	.02	2	1
WF 73+00S 80+50W	1	6	8	28	.3	5	3	169	6.13	2	6	ND	2	13	.2	2	2	243	.12	.024	4	28	.24	11	.50	2	1.82	.01	.04	1	2
WF 73+00S 80+00W	1	24	11	52	.3	17	7	388	7.51	4	8	ND	2	18	.2	2	2	197	.20	.024	4	47	.80	7	.45	4	2.76	.02	.03	1	2
WF 73+00S 79+75W	1	23	6	38	.3	7	4	226	6.70	3	5	ND	1	16	.2	2	2	164	.17	.022	4	28	.30	7	.32	2	1.65	.01	.03	1	2
WF 73+00S 79+50W P	1	28	7	42	.3	10	5	267	7.16	4	6	ND	2	20	.2	2	2	182	.20	.021	4	36	.50	8	.38	4	2.22	.01	.04	1	1
WF 73+00S 79+25W P	1	19	5	68	.4	15	6	251	3.94	2	5	ND	1	56	.2	2	2	120	.69	.040	4	26	.57	8	.39	5	2.01	.03	.05	1	1
WF 73+00S 79+00W P	7	44	6	106	.1	25	34	2071	6.24	3	5	ND	1	37	.2	2	2	119	.47	.040	6	53	1.18	14	.27	6	3.76	.02	.04	1	1
WF 73+00S 78+75W	7	49	6	108	.1	26	36	2170	6.66	8	5	ND	1	33	.3	2	4	128	.44	.041	7	53	1.35	15	.28	4	3.90	.03	.05	1	3
WF 73+00S 78+25W	11	79	8	97	.1	24	14	684	4.10	5	5	ND	1	22	.2	2	2	121	.25	.023	6	48	1.33	17	.18	4	2.95	.01	.03	1	1
WF 73+00S 78+00W	12	69	7	120	.2	23	13	705	4.02	15	5	ND	1	21	.2	2	3	123	.24	.025	5	47	1.33	16	.18	3	2.77	.01	.04	1	1
WF 73+00S 78+00W A	54	26	11	82	.2	17	44	841	8.21	12	5	ND	1	16	.2	2	2	159	.16	.055	8	54	.75	15	.16	6	4.20	.01	.04	1	1
WF 73+00S 77+50W	1	27	6	47	.1	14	13	498	2.72	2	5	ND	1	18	.2	2	2	89	.20	.038	5	31	.62	18	.09	6	1.77	.02	.03	1	1
WF 73+00S 77+25W	1	15	8	73	.3	17	10	414	7.63	5	5	ND	1	15	.2	2	2	162	.15	.032	4	50	.93	12	.08	6	2.28	.05	.05	1	1
WF 73+00S 77+00W	1	21	6	46	.1	14	12	396	2.70	5	5	ND	1	17	.2	2	2	91	.18	.043	5	31	.56	19	.08	5	1.83	.02	.03	1	1
WF 73+00S 76+50W	2	45	7	53	.3	8	7	227	2.27	2	5	ND	1	15	.2	2	2	62	.17	.057	5	24	.37	14	.11	4	1.91	.02	.03	1	1
WF 73+00S 76+25W P	1	11	7	52	.3	14	6	330	3.99	6	5	ND	1	26	.2	2	2	100	.27	.033	3	34	.53	12	.28	3	1.54	.03	.05	1	1
WF 73+00S 76+00W	1	8	9	30	.2	5	2	147	1.35	7	5	ND	1	24	.2	2	2	67	.24	.023	4	24	.19	11	.28	4	1.29	.02	.03	2	2
WF 73+50S 83+00W	1	17	9	32	.3	5	4	327	10.62	2	6	ND	1	4	.2	2	4	221	.02	.039	6	49	.19	14	.04	2	2.67	.01	.04	1	4
WF 73+50S 82+75W	1	24	6	24	.3	3	5	199	12.44	2	7	ND	2	4	.2	2	4	326	.03	.025	6	16	.11	12	.09	2	1.44	.01	.03	1	3
WF 73+50S 82+25W P	1	26	7	124	.1	26	20	7028	6.29	3	5	ND	1	25	.4	2	2	101	1.25	.162	11	43	1.17	202	.05	4	2.78	.02	.07	1	1
WF 73+50S 82+00W	1	24	10	57	.3	19	7	387	12.20	5	6	ND	2	10	.4	2	2	201	.15	.030	3	54	.53	15	.15	2	2.01	.01	.04	1	1
WF 73+50S 81+75W	1	17	12	49	.3	16	8	381	9.80	8	7	ND	2	26	.4	2	2	153	.22	.036	3	41	.74	16	.17	4	3.03	.02	.04	1	3
WF 73+50S 81+25W	1	9	9	45	.4	13	7	278	5.92	2	5	ND	2	21	.2	2	2	197	.19	.040	4	31	.49	12	.41	3	1.60	.02	.05	1	3
WF 73+50S 81+00W	1	12	11	60	.3	15	8	471	5.47	16	5	ND	1	25	.2	2	2	190	.20	.034	3	40	.94	7	.45	2	1.99	.02	.04	1	3
WF 73+50S 80+75W	1	2	12	22	.2	2	1	99	1.18	2	5	ND	1	25	.2	2	3	154	.22	.020	4	32	.12	11	.53	2	1.52	.01	.03	2	1
WF 73+50S 80+50W P	1	26	9	98	.3	19	12	495	6.93	3	5	ND	1	24	.2	2	2	154	.25	.096	4	42	.60	11	.18	4	1.91	.03	.06	1	1
WF 73+50S 80+25W	1	11	11	25	.2	4	1	147	2.33	6	5	ND	1	17	.2	2	2	182	.16	.014	5	16	.16	5	.26	2	1.39	.01	.04	2	2
WF 73+50S 80+00W	1	13	7	35	.4	10	4	233	6.63	8	5	ND	2	21	.2	2	2	204	.19	.018	4	29	.43	7	.30	2	1.74	.01	.04	1	1
WF 73+50S 79+75W	1	13	8	35	.2	12	5	271	7.56	7	5	ND	1	24	.2	2	2	215	.20	.019	4	34	.52	8	.31	3	1.92	.01	.04	1	2
WF 73+50S 79+50W P	1	18	9	66	.3	18	10	514	5.57	2	5	ND	2	32	.2	2	2	137	.34	.020	4	42	1.08	10	.34	2	2.41	.02	.05	1	1
WF 73+50S 79+25W P	1	16	7	62	.3	20	10	566	5.41	5	5	ND	1	27	.2	2	2	129	.29	.026	4	42	1.16	10	.35	5	2.19	.03	.05	1	1
STANDARD C/AU-S	18	59	42	130	6.8	73	31	1049	3.96	40	16	7	39	52	18.6	15	19	58	.58	.096	39	60	.89	182	.09	35	1.89	.06	.13	11	53

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
WF 73+50S 79+00W P	8	14	6	79	.1	22	12	689	6.04	2	5	ND	1	44	1.0	2	2	125	.75	.019	3	46	1.21	36	.24	4	2.05	.03	.03	1	1
WF 73+50S 78+75W P	10	13	9	89	.1	22	12	737	5.51	5	5	ND	1	40	.8	3	2	118	.67	.027	7	49	1.14	36	.26	8	2.09	.04	.03	1	1
WF 73+50S 78+50W	13	23	6	46	.1	16	7	291	2.84	3	5	ND	1	24	.5	2	2	82	.26	.021	6	38	.73	28	.18	2	2.05	.02	.03	1	1
WF 73+50S 78+25W	12	22	7	54	.1	16	8	299	2.93	2	5	ND	1	22	.2	2	2	80	.24	.021	6	39	.79	26	.16	3	2.02	.01	.03	1	2
WF 73+50S 77+75W	55	26	4	85	.1	18	47	809	9.43	16	5	ND	1	13	.8	2	2	147	.11	.056	9	60	.66	11	.12	2	4.30	.01	.03	1	1
WF 73+50S 77+50W	2	5	8	30	.1	1	2	99	2.70	2	5	ND	1	11	.4	2	2	95	.04	.016	8	6	.10	10	.11	3	.81	.01	.02	1	3
WF 73+50S 77+25W	1	3	7	23	.1	1	1	99	2.60	2	5	ND	1	8	.8	2	2	98	.05	.021	8	3	.09	6	.15	3	.67	.01	.03	1	1
WF 73+50S 77+00W	2	13	13	46	.1	11	7	243	3.13	2	5	ND	1	15	.3	2	2	139	.13	.023	7	35	.39	14	.12	4	2.11	.02	.03	1	1
WF 73+50S 76+75W	3	13	16	33	.1	7	6	212	2.74	5	5	ND	1	15	.3	2	2	134	.14	.023	7	29	.31	15	.09	3	2.17	.01	.03	1	1
WF 73+50S 76+50W	1	6	11	35	.2	10	5	246	5.77	3	5	ND	1	13	1.0	2	2	166	.11	.020	6	27	.40	8	.17	2	1.68	.01	.02	1	5
WF 73+50S 76+25W	1	8	4	39	.1	15	6	333	5.56	3	5	ND	1	18	1.0	2	2	128	.16	.018	5	35	.65	9	.15	2	1.95	.01	.03	1	1
WF 73+50S 76+00W P	1	6	9	37	.1	3	3	181	2.36	2	5	ND	1	44	1.0	2	2	96	.43	.028	5	10	.32	11	.35	3	1.02	.03	.03	1	2
NO NUMBER	1	15	15	24	.1	6	1	109	4.17	2	5	ND	1	37	.6	2	4	209	.22	.019	4	17	.26	2	.15	3	1.30	.01	.02	1	27
STANDARD C/AU-S	19	60	45	134	7.1	72	31	1053	3.97	42	15	7	38	53	18.4	16	19	57	.51	.092	39	60	.90	182	.08	37	1.89	.06	.13	13	48

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

Stevenson & Assoc. PROJECT WILF File # 90-4247 Page 1

303 - 475 Howe St., Vancouver BC V6B 2C3

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
56+00S 85+00W	1	4	15	33	.3	6	20	365	3.50	2	5	ND	1	8	.4	2	2	56	.12	.021	5	15	.13	17	.01	2	1.93	.01	.03	2	2
56+00S 84+75W	1	6	8	65	.1	9	232	3704	4.01	4	5	ND	1	7	.2	2	2	54	.09	.086	4	31	.33	18	.02	4	2.63	.04	.06	2	3
56+00S 84+50W	2	3	8	37	.1	11	38	501	8.95	11	5	ND	1	12	.3	2	2	164	.14	.019	3	53	.46	6	.23	4	2.83	.01	.02	1	2
56+00S 84+25W	1	1	13	21	.1	5	2	86	1.35	4	5	ND	1	18	.5	2	11	72	.27	.012	4	25	.08	3	.18	7	.28	.03	.02	2	4
56+00S 84+00W	4	6	13	19	.1	5	7	109	7.41	60	5	ND	1	15	.2	2	2	274	.19	.014	2	36	.21	1	.36	2	1.20	.02	.03	1	2
56+00S 83+75W	9	30	2	61	.1	24	21	234	10.44	235	5	ND	2	7	.5	3	3	157	.08	.032	2	94	.58	8	.06	2	9.26	.01	.02	1	450
56+00S 83+50W	9	29	2	69	.1	23	21	258	10.56	224	5	ND	2	7	.6	2	2	157	.10	.032	2	86	.62	8	.06	4	8.09	.01	.02	1	26
56+00S 83+25W	2	9	3	20	.1	7	11	106	7.08	54	5	ND	1	8	.2	2	2	239	.10	.017	3	37	.15	1	.23	2	.89	.01	.01	1	6
56+00S 83+00W	2	13	2	39	.1	16	11	317	6.16	3	5	ND	1	21	.3	2	2	184	.25	.012	3	41	.80	15	.21	2	2.43	.02	.02	2	9
56+00S 82+75W	2	12	8	21	.1	8	8	136	5.90	6	5	ND	1	12	.2	2	2	162	.13	.011	3	32	.22	9	.24	2	1.79	.02	.02	1	3
56+00S 82+50W	1	5	2	27	.1	6	10	192	8.41	10	5	ND	1	12	1.2	2	6	183	.17	.017	2	34	.40	7	.33	2	1.89	.01	.02	1	6
56+00S 82+25W	1	9	8	33	.1	9	6	139	5.45	5	5	ND	1	18	.2	2	6	131	.22	.017	3	30	.25	14	.22	6	1.42	.02	.03	2	2
56+00S 82+00W	1	9	7	29	.1	10	7	189	5.47	6	5	ND	2	16	.2	2	2	151	.19	.011	4	36	.41	8	.20	3	2.46	.01	.03	2	3
56+00S 81+75W	1	5	6	30	.1	10	8	223	4.62	8	5	ND	1	18	.2	2	2	132	.22	.011	5	30	.56	14	.17	4	2.47	.01	.03	1	1
56+00S 81+50W	1	21	6	40	.1	13	11	299	6.16	10	5	ND	1	14	.3	2	2	139	.16	.019	4	46	.70	16	.17	2	3.52	.01	.02	2	1
6+00S 81+25W	1	12	11	21	.1	7	6	138	4.08	5	5	ND	1	12	.2	2	2	134	.15	.010	5	24	.30	8	.14	3	2.32	.01	.02	1	5
6+00S 81+00W	1	7	2	20	.1	8	9	153	6.96	3	5	ND	1	7	.3	2	2	194	.10	.007	3	31	.26	1	.23	2	1.37	.01	.02	1	3
6+00S 80+75W	2	52	6	49	.1	19	12	359	5.23	10	5	ND	1	17	.2	2	2	124	.23	.020	4	50	.97	22	.18	4	3.51	.01	.02	1	3
6+00S 80+50W	6	2	2	11	.1	3	2	57	1.36	5	5	ND	1	11	.3	2	2	57	.15	.008	8	9	.13	4	.04	2	1.36	.01	.02	1	2
6+00S 80+25W	1	2	7	18	.1	7	2	95	.81	8	5	ND	1	13	.4	2	2	30	.16	.010	7	17	.26	1	.05	2	1.40	.02	.02	1	1
6+00S 80+00W	3	1	7	18	.1	1	4	40	5.22	23	5	ND	1	8	.2	3	4	90	.09	.012	7	12	.08	9	.05	3	1.08	.01	.01	1	2
6+00S 79+75W	1	1	8	16	.1	1	1	10	.23	2	5	ND	1	6	.6	2	3	18	.08	.013	2	9	.03	6	.09	2	.31	.02	.01	1	1
6+00S 79+50W	2	11	8	31	.1	10	8	165	6.95	26	5	ND	3	10	.2	2	2	103	.12	.012	6	33	.37	6	.11	2	2.71	.01	.01	1	2
6+00S 79+25W	1	2	3	15	.1	3	2	95	1.09	9	5	ND	1	8	.5	2	4	70	.14	.006	9	10	.10	1	.18	2	1.06	.01	.01	1	1
6+00S 79+00W	2	22	9	27	.1	10	6	210	2.12	14	5	ND	1	15	.3	2	3	68	.18	.009	10	30	.58	8	.05	2	2.60	.01	.01	1	1
6+00S 78+75W	2	5	2	27	.1	10	8	205	6.14	110	5	ND	1	14	.2	2	2	79	.21	.008	6	22	.57	16	.04	5	1.97	.01	.01	1	2
6+00S 78+50W	3	1	2	23	.1	5	9	132	10.42	40	5	ND	3	5	.6	2	2	50	.07	.011	5	11	.38	11	.01	2	1.60	.01	.01	1	1
6+00S 78+25W	3	1	9	26	.1	4	6	87	6.34	32	5	ND	2	6	.2	2	2	54	.08	.012	6	9	.23	6	.02	2	1.38	.01	.01	1	1
6+00S 78+00W	1	2	2	15	.2	2	1	12	.48	5	5	ND	2	2	.7	2	2	19	.03	.006	9	4	.02	1	.01	2	.33	.01	.01	1	1
6+00S 77+75W	2	18	5	27	.1	9	6	162	3.08	5	5	ND	2	8	.2	2	2	36	.11	.027	12	14	.36	14	.01	3	1.18	.02	.02	1	1
6+00S 77+50W	3	15	6	26	.1	7	7	167	3.51	3	5	ND	2	8	.2	2	2	39	.11	.030	13	15	.37	15	.01	4	1.29	.01	.03	2	1
6+00S 77+25W	4	2	11	12	.1	3	2	62	1.36	2	5	ND	1	9	.5	2	2	49	.10	.011	10	7	.07	5	.06	3	1.08	.01	.03	1	1
6+00S 77+00W	5	41	6	68	.2	21	22	306	5.92	27	5	ND	2	3	.2	6	2	134	.04	.030	3	29	.06	5	.01	4	.62	.01	.01	1	1
6+00S 76+75W	1	6	5	23	.2	3	3	27	.90	4	5	ND	2	5	.2	2	4	10	.14	.011	5	1	.03	3	.01	4	.25	.03	.03	1	3
6+00S 76+50W	5	2	7	40	.2	17	7	315	3.13	3	5	ND	1	15	.2	2	2	76	.18	.017	4	46	.95	6	.06	2	1.85	.01	.02	1	1
6+00S 76+25W	1	5	2	16	.1	4	6	29	2.21	4	5	ND	1	7	.3	2	2	41	.09	.009	2	12	.02	3	.04	4	.29	.04	.01	1	1
TANDARD C/AU-S	19	57	39	131	6.8	70	31	1054	3.96	40	20	6	38	52	18.9	15	22	55	.52	.093	38	57	.90	181	.07	35	1.89	.06	.14	13	46

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: P1-P3 SOIL P4 ROCK AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE

DATE RECEIVED: SEP 7 1990 DATE REPORT MAILED: Sept 14/90. SIGNED BY.........D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
66+00S 76+00W	1	4	12	20	.1	4	1	108	1.05	2	5	ND	2	9	.3	2	4	89	.09	.014	6	23	.17	8	.36	2	1.07	.02	.04	2	9
66+00S 75+75W	1	4	2	12	.1	2	3	57	1.21	3	5	ND	2	10	.3	2	2	49	.11	.009	2	8	.04	4	.04	3	.51	.02	.02	2	2
66+00S 75+50W	1	1	4	22	.1	1	4	50	.86	2	5	ND	2	17	.4	2	2	21	.12	.016	2	2	.13	8	.02	2	.44	.02	.03	2	4
66+50S 81+00W	1	17	6	52	.1	24	12	499	4.53	2	5	ND	3	23	.2	2	2	116	.21	.010	5	42	1.35	30	.18	2	3.17	.01	.06	1	5
66+50S 79+25W	1	4	4	20	.1	1	1	16	.17	3	5	ND	2	5	.5	2	2	15	.05	.011	10	4	.03	2	.04	2	.45	.03	.02	2	1
66+50S 79+00W P	1	6	3	82	.1	1	2	47	.43	2	5	ND	2	20	.6	2	2	2	.18	.034	2	1	.11	4	.01	4	.41	.03	.04	1	1
66+50S 77+75W	2	10	4	39	.2	6	3	105	3.07	9	5	ND	5	4	.2	2	2	47	.03	.016	10	16	.35	7	.01	2	1.29	.01	.07	1	5
66+50S 76+75W	5	4	8	22	.2	1	1	28	.56	4	5	ND	2	12	.5	2	2	33	.12	.018	9	7	.07	8	.03	2	1.13	.02	.04	2	1
66+50S 75+50W	2	1	8	31	.1	1	1	39	2,16	2	5	ND	2	12	.2	2	2	71	.10	.028	6	8	.06	7	.09	2	.93	.02	.05	1	1
68+00S 85+00W P	1	25	9	87	.2	12	26	208	3.05	12	5	ND	2	21	.2	2	2	57	.35	.066	3	11	.35	16	.10	4	1.36	.04	.05	1	1
68+00S 84+75W P	1	29	13	142	.2	11	21	278	.98	7	5	ND	2	24	.7	2	2	17	.37	.134	4	4	.12	19	.02	6	1.26	.03	.07	1	1
68+00S 84+50W	1	27	8	28	.1	7	21	131	8.32	3	5	ND	2	11	.2	2	2	228	.14	.040	4	27	.21	9	.42	2	1.56	.02	.04	1	1
68+00S 84+25W	2	33	9	31	.1	6	18	116	8.80	2	5	ND	2	12	.2	2	4	230	.13	.046	3	29	.12	10	.39	2	1.65	.01	.04	1	1
68+00S 84+00W P	1	29	13	98	.3	11	30	267	2.73	13	5	ND	2	19	.5	2	2	59	.26	.094	4	11	.16	16	.08	5	1.39	.04	.07	1	1
68+00S 83+75W P	1	34	10	107	.4	8	131	1401	1.91	3	5	ND	2	15	.4	2	2	22	.21	.182	4	9	.10	15	.02	6	1.74	.03	.10	1	1
68+00S 83+50W P	1	30	9	72	.4	7	94	1248	2.81	3	5	ND	2	11	.2	2	2	27	.15	.142	3	9	.36	11	.02	4	1.76	.03	.09	1	1
68+00S 83+25W P	1	24	14	54	.4	6	171	2533	3.44	2	5	ND	2	17	.2	2	2	60	.21	.096	4	12	.10	14	.08	4	1.35	.02	.07	1	1
68+00S 83+00W P	1	9	5	82	.3	6	11	26	.18	3	5	ND	2	50	.5	2	3	3	.28	.057	2	2	.18	21	.01	4	.28	.04	.06	1	1
68+00S 82+75W P	1	10	3	100	.2	6	11	40	.23	2	5	ND	1	47	.9	2	2	4	.26	.053	2	2	.18	22	.01	3	.27	.04	.05	1	2
68+00S 82+50W P	1	9	8	57	.2	5	19	99	2.48	6	5	ND	1	29	.2	2	2	45	.41	.041	3	5	.27	20	.08	3	.69	.02	.04	1	1
68+00S 82+25W P	2	19	9	76	.2	6	32	110	4.00	6	5	ND	2	21	.2	2	2	71	.28	.062	3	8	.34	17	.13	3	.83	.03	.05	1	1
68+00S 82+00W	4	11	5	21	.1	10	51	183	6.74	10	5	ND	3	8	.2	2	2	145	.09	.024	5	25	.30	8	.29	2	1.08	.01	.03	1	2
68+00S 81+75W P	3	24	6	74	.2	21	95	563	4.26	17	5	ND	3	14	.2	2	2	63	.20	.062	5	31	.72	12	.10	2	2.88	.02	.05	1	1
68+00S 81+50W P	2	7	10	62	.3	2	2	29	.47	2	5	ND	3	10	.5	2	2	43	.09	.048	3	7	.06	6	.12	3	.51	.03	.05	1	1
68+00S 81+25W P	3	4	7	84	.2	5	2	47	1.31	2	5	ND	2	11	.2	2	2	72	.09	.036	3	9	.11	6	.16	4	.62	.03	.05	1	1
68+00S 81+00W P	5	4	11	31	.2	2	1	30	1.01	4	5	ND	2	8	.3	2	4	98	.07	.019	5	11	.04	5	.23	2	.61	.02	.04	1	1
68+00S 80+75W P	3	4	16	44	.1	2	2	29	.57	2	5	ND	1	11	.3	2	2	82	.08	.035	4	8	.05	5	.22	4	.49	.03	.05	1	2
68+00S 80+50W P	2	4	5	57	.2	3	7	20	.74	19	5	ND	1	21	.5	2	2	78	.22	,030	2	2	.06	9	.05	6	.17	.02	.04	1	4
68+00S 80+25W P	5	4	6	42	.2	2	1	22	1.07	7	5	ND	1	9	.4	2	2	37	.08	.032	4	5	.12	5	.11	3	.32	.02	.04	1	2
68+00S 80+00W P	1	3	3	66	.3	2	1	20	.65	4	5	ND	2	23	.4	2	2	21	.10	.037	3	4	.09	7	.03	4	.30	.03	.05	1	1
68+00S 79+75W P	1	8	2	108	.2	1	1	16	.10	2	5	ND	2	64	.6	2	2	2	.31	.025	2	1	.25	11	.01	3	.11	.03	.04	1	1
68+00S 79+50W P	1	49	9	30	.3	2	1	11	1.22	2	5	ND	2	9	.3	2	2	54	.07	.027	6	31	.04	7	.04	2	1.40	.02	.03	1	1
68+00S 79+25W P	1	3	5	20	.1	2	2	50	3.52	2	5	ND	2	9	.2	2	2	167	.07	.009	4	19	.10	3	.21	2	.72	.01	.02	1	6
68+00S 79+00W P	1	25	4	119	.3	4	2	128	.96	3	5	ND	2	9	.3	2	2	16	.14	.107	5	12	.02	12	.01	2	2.34	.02	.03	1	1
68+00S 78+75W	1	22	5	30	.1	20	4	140	7.12	5	5	ND	2	6	.2	2	2	187	.05	.014	5	114	.65	4	.17	2	1.23	.01	.02	1	2
68+00S 78+50W	1	68	5	32	.1	10	6	225	1.91	5	5	ND	1	15	.2	2	2	42	.16	.017	5	19	.70	7	.07	2	1.25	.02	.01	1	1
STANDARD C/AU-S	19	58	37	132	6.8	72	31	1047	3.96	38	22	7	39	56	19.7	15	18	58	.52	.094	39	60	.89	182	.09	35	1.89	.06	.13	13	45

P = PULVERIZING

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb
68+00S 78+25W	1	6	6	33	.2	2	2	122	2.23	2	5	ND	1	12	.2	2	2	63	.14	.024	4	7	.49	3	.02	2	.97	.04	.03	1	4
68+00S 78+00W P	1	8	5	115	.1	3	2	127	1.45	11	5	ND	1	30	.2	2	2	45	.23	.040	2	9	.18	8	.10	4	.56	.04	.05	1	4
68+00S 77+75W	1	15	8	29	.1	10	15	164	12.30	5	5	ND	2	17	.6	2	5	235	.17	.033	3	60	.37	7	.52	2	3.03	.02	.03	1	14
68+00S 77+50W	1	13	9	35	.1	5	3	201	2.18	10	5	ND	1	23	.2	2	2	112	.24	.015	5	35	.24	9	.34	2	1.37	.02	.03	1	2
68+00S 77+25W	2	17	3	23	.1	7	5	157	8.70	2	5	ND	2	15	.2	2	3	280	.17	.022	3	43	.23	7	.47	2	1.69	.02	.04	1	4
68+00S 77+00W	1	8	7	8	.1	2	1	26	.20	2	5	ND	1	6	.3	2	3	20	.06	.007	5	6	.02	4	.10	2	.65	.03	.02	1	1
68+00S 76+75W	2	14	5	29	.1	13	5	177	6.42	12	5	ND	1	16	.2	2	2	166	.20	.012	4	37	.48	6	.25	2	2.03	.02	.03	1	1
68+00S 76+50W	1	12	3	24	.2	6	4	121	6.05	4	5	ND	2	13	.2	2	3	166	.15	.011	6	25	.37	5	.20	2	1.81	.02	.03	1	1
68+00S 76+25W P	1	7	4	104	.2	1	1	33	.63	2	5	ND	1	27	.4	3	2	6	.31	.035	2	2	.06	5	.03	4	.32	.05	.04	1	2
68+00S 76+00W P	1	7	3	86	.1	2	1	61	.44	2	5	ND	1	29	.4	2	2	5	.43	.034	2	4	.07	6	.03	4	.19	.05	.04	1	1
68+00S 75+75W P	1	9	4	89	.2	1	1	18	.13	4	5	ND	1	17	.7	2	2	3	.27	.067	2	4	.07	6	.01	5	.48	.03	.04	1	1
68+00S 75+50W P	1	6	5	38	.1	1	1	31	.93	4	5	ND	1	10	.3	2	2	12	.09	.060	2	4	.12	5	.02	2	.70	.04	.03	1	1
68+00S 75+25W P	1	1	2	60	.1	2	1	21	.62	2	5	ND	1	16	.4	2	2	12	.09	.065	2	7	.10	6	.05	5	.63	.04	.03	1	1
68+00S 75+00W	2	9	4	31	.1	4	8	89	6.12	6	5	ND	1	12	.2	2	2	158	.13	.022	3	19	.14	4	.30	2	1.15	.02	.03	1	1
68+50S 84+50W	1	19	4	21	.1	4	4	128	8.11	12	5	ND	2	14	.2	2	4	202	.17	.014	4	36	.22	8	.32	2	1.78	.02	.02	1	2
68+50S 82+00W	1	13	3	24	.1	5	3	151	8.08	9	5	ND	3	16	.2	2	5	192	.18	.015	4	35	.23	8	.35	2	1.74	.02	.04	1	2
68+50S 81+75W P	1	13	4	36	.1	6	4	152	5.11	3	5	ND	1	15	.2	2	2	117	.17	.023	4	25	.36	7	.22	2	1.43	.02	.03	1	3
69+00S 83+00W	1	29	5	39	.1	5	7	174	8.40	6	5	ND	2	13	.2	2	4	181	.15	.034	5	25	.25	9	.29	2	1.44	.02	.04	1	4
69+00S 81+50W	1	63	3	77	.2	27	13	557	5.64	7	5	ND	1	22	.2	2	2	117	.22	.028	5	51	1.40	24	.21	2	3.54	.02	.04	1	1
69+00S 81+25W	2	30	6	32	.1	9	5	248	6.00	5	5	ND	1	13	.2	2	2	197	.12	.014	5	35	.43	8	.23	2	2.51	.01	.02	1	1
69+00S 81+00W	4	16	5	18	.2	3	2	110	5.47	2	5	ND	3	16	.2	2	2	148	.17	.011	5	23	.12	8	.24	2	1.21	.02	.03	1	5
69+00S 80+75W	4	28	5	38	.1	12	7	297	4.37	3	5	ND	2	20	.2	2	2	163	.21	.014	4	34	.58	16	.23	3	2.29	.02	.05	1	1
69+00S 80+50W	16	8	6	29	.1	5	1	186	1.87	6	5	ND	1	10	.2	2	2	100	.10	.010	5	25	.21	8	.11	2	1.47	.01	.02	1	1
69+00S 80+25W P	1	2	7	67	.3	4	1	49	2.18	2	5	ND	1	10	.2	2	2	99	.14	.027	3	34	.22	8	.32	3	.77	.03	.04	1	1
69+00S 79+75W P	1	5	5	86	.1	1	1	19	.21	2	5	ND	1	17	.5	3	2	17	.05	.027	2	2	.08	5	.08	6	.20	.04	.03	1	5
69+00S 76+25W	10	20	5	38	.1	17	8	258	3.20	15	5	ND	1	22	.2	2	2	122	.27	.016	6	38	.82	16	.22	2	2.51	.02	.02	1	6
69+00S 75+75W	2	4	7	18	.1	6	2	111	2.27	13	5	ND	2	18	.2	3	2	128	.26	.009	5	27	.47	9	.26	2	1.22	.02	.02	1	1
69+00S 75+50W	2	15	2	21	.1	8	4	189	3.24	11	5	ND	1	21	.2	2	2	176	.23	.008	5	32	.51	13	.27	2	2.44	.02	.04	1	3
STANDARD C/AU-S	19	59	37	132	7.2	72	31	1049	3.97	40	21	7	39	56	18.9	14	19	58	.52	.097	40	60	.90	182	.09	35	1.90	.06	.13	13	48

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Au*
	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	%	ppm	ppm	%	ppm	%	ppm	%	%	%	ppm	ppb
TRENCH 2	4	15503 ✓	19	27	2.8	47	174	183	36.35	19	5	ND	1	10	1.2	9	6	63	.17	.001	2	31	.17	3	.02	2	.28	.01	.01	65	179
TRENCH 3	1	35447 ✓	22	21	2.5	92	223	145	12.15	9	5	ND	1	34	2.7	3	15	44	.36	.003	2	29	.44	1	.07	2	.59	.01	.01	1	141

✓ASSAY RECOMMENDED

ACME ANALYTICAL LABORATORIES LTD.
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE(604)253-3158 FAX(604)253-1716

DATE RECEIVED: NOV 1 1990
DATE REPORT MAILED: Nov 8/90

ASSAY CERTIFICATE

Stevenson & Assoc. FILE # 90-5673
303 - 475 Howe St., Vancouver BC V6B 2C3

SAMPLE#	Cu %	Ag** oz/t	Au** oz/t
WF1 TR2-GR1	.79	.07	.001

AG** AND AU** BY FIRE ASSAY FROM 1 A.T.
- SAMPLE TYPE: ROCK

SIGNED BY........ D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

Peter Christopher & Associates Inc.
GEOLOGICAL & EXPLORATION SERVICES
3707 West 34th Ave., Vancouver, B.C. V6N 2K9

Office/Res: 263-6152

April 30, 1991

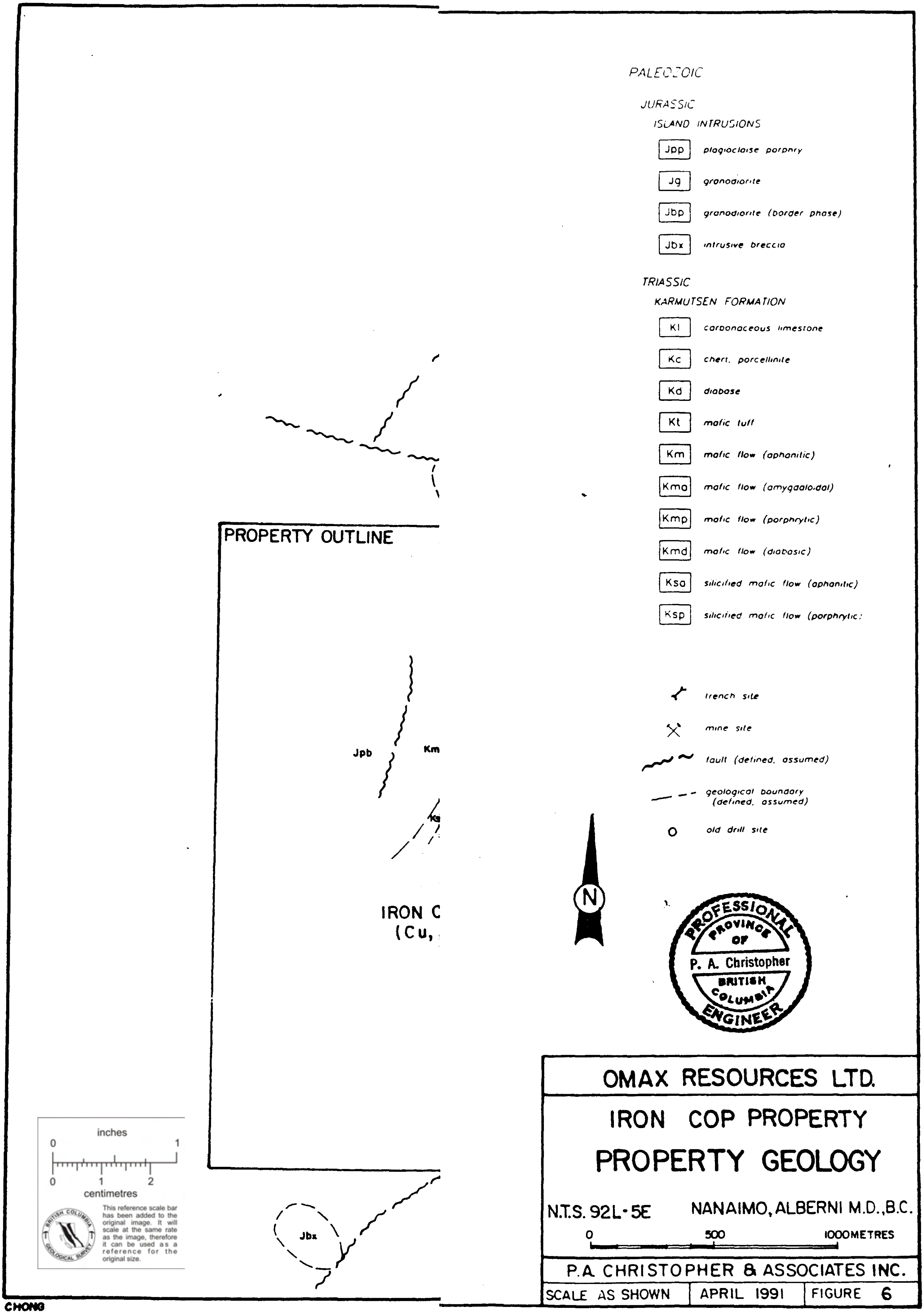
Omax Resources Ltd.
1500 - 789 West Pender Street
Vancouver, British Columbia

Dear Sirs:

I Peter A. Christopher, PhD., P.Eng., hereby consent to the use of my report dated April 30, 1991 on the Iron Cop Property, Alberni and Nanaimo Mining Divisions, British Columbia, in any Filing Statement, Statement of Material Facts, or Prospectus by Omax Resources Ltd.

DATED at Vancouver, British Columbia, this 30th day of April, 1990.

Peter A. Christopher, Ph.D., P.Eng.


PALEOZOIC
JURASSIC
ISLAND INTRUSIONS
Jpp plagioclaise porphry
Jg granodiorite
Jbp granodiorite (border phase)
Jbx intrusive breccia
TRIASSIC
KARMUTSEN FORMATION
Kl carbonaceous limestone
Kc chert, porcellinite
Kd diabase
Kt mafic tuff
Km mafic flow (aphanitic)
Kma mafic flow (amygdaloidal)
Kmp mafic flow (porphrytic)
Kmd mafic flow (diabasic)
Ksa silicified mafic flow (aphanitic)
Ksp silicified mafic flow (porphrytic)
trench site
mine site
fault (defined, assumed)
geological boundary (defined, assumed)
old drill site
PROPERTY OUTLINE
Jpb
Km
Jbx
IRON C
(Cu,
N
PROFESSIONAL ENGINEER
PROVINCE OF BRITISH COLUMBIA
P. A. Christopher
OMAX RESOURCES LTD.
IRON COP PROPERTY
PROPERTY GEOLOGY
N.T.S. 92L-5E
NANAIMO, ALBERNI M.D., B.C.
0 500 1000 METRES
P.A. CHRISTOPHER & ASSOCIATES INC.
SCALE AS SHOWN
APRIL 1991
FIGURE 6
inches
0 1
0 1 2
centimetres
This reference scale bar has been added to the original image. It will scale at the same rate as the image, therefore it can be used as a reference for the original size.
BRITISH COLUMBIA GEOLOGICAL SURVEY
CHONG