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PROPERTY FILE Win Property

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THIS PROSPECTUS CONSTITUTES A PUBLIC OFFERING OF THESE SECURITIES ONLY IN THOSE JURISDICTIONS WHERE THEY MAY BE LAWFULLY OFFERED FOR SALE AND THEREIN ONLY BY PERSONS PERMITTED TO SELL SUCH SECURITIES.

NO SECURITIES COMMISSION OR SIMILAR AUTHORITY IN CANADA HAS IN ANY WAY PASSED UPON THE MERITS OF THE SECURITIES OFFERED HEREUNDER AND ANY REPRESENTATION TO THE CONTRARY IS AN OFFENCE.

PROSPECTUS

DATED: November 19, 1990

**ESSEX RESOURCE CORPORATION**

(the "Issuer")

1260 - 400 Burrard Street  
Vancouver, British Columbia

V6C 3A6

Telephone: (604) 684-4452

**NEW ISSUE**

**357,000 COMMON SHARES**

Shares	Price To Public	Commission Payable	Proceeds To Be Received by Issuer
Per Share	\$0.35 <sup>1</sup>	\$0.05	\$0.30
Total	\$124,950	\$17,850 <sup>3</sup>	\$107,100 <sup>2</sup>

**243,000 FLOW-THROUGH COMMON SHARES**

Shares	Price To Public	Commission Payable	Proceeds To Be Received by Issuer
Per Share	\$0.35 <sup>1</sup>	\$ NIL <sup>3</sup>	\$0.35
Total	\$85,050	\$ NIL	\$85,050

<sup>1</sup> The Offering Price of the Common Shares and Flow-Through Common Shares has been determined by the Issuer in negotiation with the Agent.

<sup>2</sup> Before deduction of expenses of this issue estimated not to exceed \$25,000.

<sup>3</sup> The Issuer will pay the Agent an additional fee of \$12,150 in respect of the sale of the Flow-Through Common Shares.

THERE IS NO MARKET THROUGH WHICH THESE SECURITIES MAY BE SOLD.

A PURCHASE OF THE SECURITIES OFFERED BY THIS PROSPECTUS MUST BE CONSIDERED AS SPECULATION. SEE HEADING "RISK FACTORS" HEREIN FOR A DETAILED DESCRIPTION OF RISKS.

72C 78

May 16/91

THE OFFERING OF FLOW-THROUGH SHARES IS INTENDED TO ALLOW INVESTORS TO ACHIEVE CERTAIN TAX BENEFITS IN THE YEAR OF SUBSCRIPTION. THE ACHIEVING OF SUCH BENEFITS BY THE INVESTORS AND THE EXPENDITURES BY THE ISSUER ON BEHALF OF THE INVESTORS ARE SUBJECT TO RISK AND UNCERTAINTY WHICH ARE DESCRIBED IN THE SECTIONS CAPTIONED "CANADIAN INCOME TAX CONSIDERATIONS" AND "RISK FACTORS".

No person is authorized by the Issuer to provide any information or to make any representation other than those contained in this Prospectus in connection with the issue and sale of the securities offered herein.

THIS OFFERING IS SUBJECT TO A MINIMUM SUBSCRIPTION OF ALL 357,000 COMMON SHARES AND 243,000 FLOW-THROUGH COMMON SHARES BEING SOLD ON THE OFFERING DAY. SEE "MINIMUM SUBSCRIPTION" UNDER THE HEADING "PLAN OF DISTRIBUTION" FOR DETAILS.

FOR COMPARISON OF THE SECURITIES BEING OFFERED TO THE PUBLIC FOR CASH AND THOSE ISSUED TO PROMOTERS, DIRECTORS AND OTHER INSIDERS OF THE ISSUER, REFERENCE IS MADE TO "PRINCIPAL HOLDERS OF SECURITIES" HEREIN.

ONE OR MORE OF THE DIRECTORS OF THE ISSUER ARE DIRECTORS OF OTHER REPORTING COMPANIES AND HAVE POTENTIAL CONFLICTS OF INTEREST WHEN SERVING IN SUCH CAPACITIES. REFERENCE IS MADE TO "CONFLICT OF INTEREST".

The Vancouver Stock Exchange has conditionally listed of the securities being offered pursuant to this Prospectus. Listing is subject to the Issuer fulfilling all the listing requirements of the Exchange on or before May 27, 1991, including prescribed distribution and financial requirements.

REFERENCE SHOULD BE MADE TO THE HEADING "DILUTION" HEREIN TO ASCERTAIN THE PERCENTAGE OF DILUTION IN THE BOOK VALUE OF EACH SHARE OF THE ISSUER UPON COMPLETION OF THIS OFFERING.

WE, AS AGENT, CONDITIONALLY OFFER THESE SECURITIES SUBJECT TO PRIOR SALE, IF, AS AND WHEN ISSUED BY THE ISSUER AND ACCEPTED BY US IN ACCORDANCE WITH THE CONDITIONS CONTAINED IN THE AGENCY AGREEMENT REFERRED TO UNDER THE "PLAN OF DISTRIBUTION" HEREIN.

**Agent:**

**UNION SECURITIES LTD.**  
1300 - 409 Granville Street  
Vancouver, B. C. V6C 1T2  
687-2201

**Effective Date: November 27, 1990**

Daiwan Engineering Ltd.  
1030 - 609 Granville Street, Vancouver, B.C. V7Y 1G5  
Phone: (604) 688-1508

**GEOLOGICAL, GEOCHEMICAL AND GEOPHYSICAL  
REPORT  
ON THE  
WIN CLAIM GROUP  
NORTHERN VANCOUVER ISLAND  
BRITISH COLUMBIA, CANADA**

NTS 92L/12

Latitude: 50°44'N

Longitude: 127°57'W

For

**Essex Resource Corporation**  
1260 - 400 Burrard Street  
Vancouver, B.C.  
V6C 3A6

By

Rod W. Husband, B.Sc.

and

Peter G. Dasler, M.Sc., F.G.A.C.

February 15, 1990

Revised September 10, 1990

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## SUMMARY

The Win property was evaluated by mapping, stream sediment and geochemical soil sampling and trenching in areas of previously noted sulphide mineralization in January 1990 by Daiwan Engineering Ltd.

During the program 640 soil samples, 72 rock samples, 4 pan concentrates and 1 silt sample were collected. The property was mapped on a scale of 1:5000. Locally more detailed information was collected by trenching across mineralized zones.

The property is located on northern Vancouver Island, approximately 360 kilometres (225 miles) northwest of Vancouver, British Columbia, Canada. The claim group covers a 5 kilometre stretch of ground west of Nahwitti Lake on N.T.S. topographic map 92L/12W. All areas of the property can be reached by well maintained logging roads and forest tracks.

The Win claim group is underlain by volcanics and sediments of the Karmutsen, Quatsino, Parson Bay, and Bonanza formations. The rocks are intruded by at least four distinct phases of intrusives. The attitudes of the rocks are generally northwest striking, southwest dipping except where the bedding has been disrupted by the intrusives and the northwest and northeast trending late stage faults.

Four different styles of base and precious metal mineralization were observed on the property. They include auriferous zinc metasomatic replacement, semi-massive copper-zinc sulphide veins, auriferous quartz veins and copper bearing intrusive. Each of these styles of mineralization have been found on other properties in the surrounding district.

The exploration program conducted in 1990 was successful in defining numerous targets for follow-up work. The geochemical survey outlined new exploration targets and supported the information obtained from earlier surveys.

A two phase program, including infill geochemistry and drilling, is proposed for follow-up work on this property. Phase I is budgeted at \$135,000, phase II, contingent upon the success of Phase I, is budgeted at \$165,000.

## INTRODUCTION

At the request of Mr. Michael Foley, President of Essex Resource Corporation, Daiwan Engineering Ltd. conducted an exploration program on the Win Group claims near Port Hardy B.C. The program consisted of geological mapping, stream sediment sampling and geochemical soil sampling in areas of previously noted sulphide mineralization.

During the program 640 soil samples, 72 rock samples, 4 pan concentrates and 1 silt sample were collected, and the property was mapped on a scale of 1:5000. Locally more detailed information was collected by trenching across mineralized zones.

This report is a description of work completed on the property between December 15, and February 15, 1990 and a compilation of previous reports of work in the area.

## LOCATION AND ACCESS

The Win property is located on northern Vancouver Island, approximately 360 kilometres (225 miles) northwest of Vancouver, British Columbia, Canada (Figure 1). The claim group covers a 5 kilometre (2.5 mile) stretch of ground west of Nahwitti Lake on N.T.S. topographic map 92L/12W (see Figures 1 & 2). All areas of the property can be reached by well maintained logging roads and forest tracks.

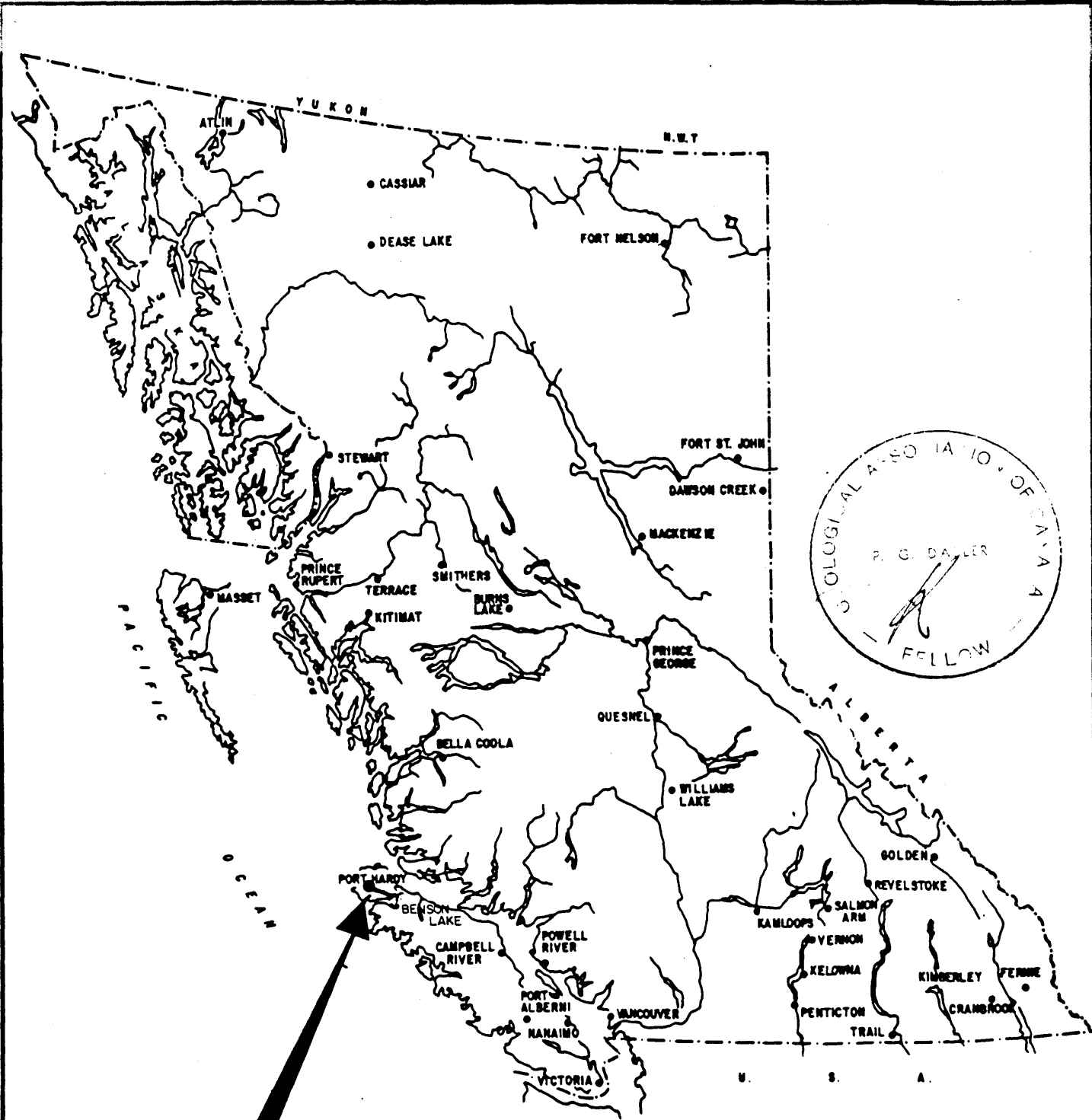
The main access to the claim block is by road "NE66" which leaves the Holberg-Port Hardy road at a point 13.5 road kilometres from Holberg. Access to the east end of the block is by the Nahwitti River logging road system (See Figure 2).

Regular Dash 7 air service is provided by both Air BC and Time Air from Vancouver to Port Hardy, each on a twice daily schedule. Alternately, there is good highway access, with travel from Vancouver taking 7 hours.

Port Hardy is the local commercial centre, but there are forestry and fishing centres at Coal Harbour and Holberg.

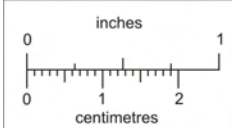
**Daiwan Engineering Ltd.**

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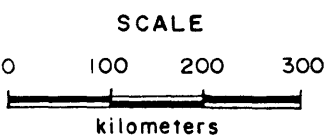


**PROPERTY**

ESSEX RESOURCE CORPORATION		
WIN PROPERTY		
NANAIMO MINING DIVISION, B.C.		
<b>LOCATION MAP</b>		
DAIWAN ENGINEERING LTD.		
SCALE	DATE	FIG.
As Shown	Jan., '90	1



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## PHYSIOGRAPHY AND CLIMATE

The property is characterized by two northwest to westerly trending hills and ridges bounded by narrow deeply incised valleys and steep slopes. Elevations range from sea level to over 650 metres (2,000 ft). Within the claim block ridge tops are commonly about 300 metres (1,000 ft) above valley bottom. The property is within N.T.S. topographic map 92L/12W. The claims are located within an active logging area, consequently forest cover varies from mature stands of fir, hemlock, spruce and cedar to dense second growth or to open clear-cut areas of recent logging. Low areas, especially along creeks are swampy and have thick brush and berry bushes.

Thick humus development on the forested slopes and scattered residual glacial gravels in the valley bottoms can restrict geological mapping in these areas. Rock exposure is limited to road cuts and well scoured creeks.

The area is characterized by warm summers and mild winters. Snowfall in winter is limited to the higher elevations and exploration can usually continue year round.

## PROPERTY

The property consists of 11 contiguous mining claims totalling 41 units within the Nanaimo Mining Division. The claims were staked as "Win, Helper, and Helper 1, 2," claims. Additional claims LOD 1-7 were staked during course of the exploration program. The claims are all recorded in the name of Daiwan Engineering, and are held in trust for Agilis Engineering Ltd and Western Magnetite Ltd. who have optioned the property to Essex Resource Corporation. The claim particulars are as follows:

<u>Claim</u>	<u>Rec. No.</u>	<u>Units</u>	<u>Expiry Date</u>
LOD 1-7	3674-80	7	January 16, 1991
Win 1	3212	20	December 9, 1996*
Helper	3237	12	January 31, 1994*
Helper 1	3694	1	February 3, 1991
Helper 2	3695	1	February 3, 1991

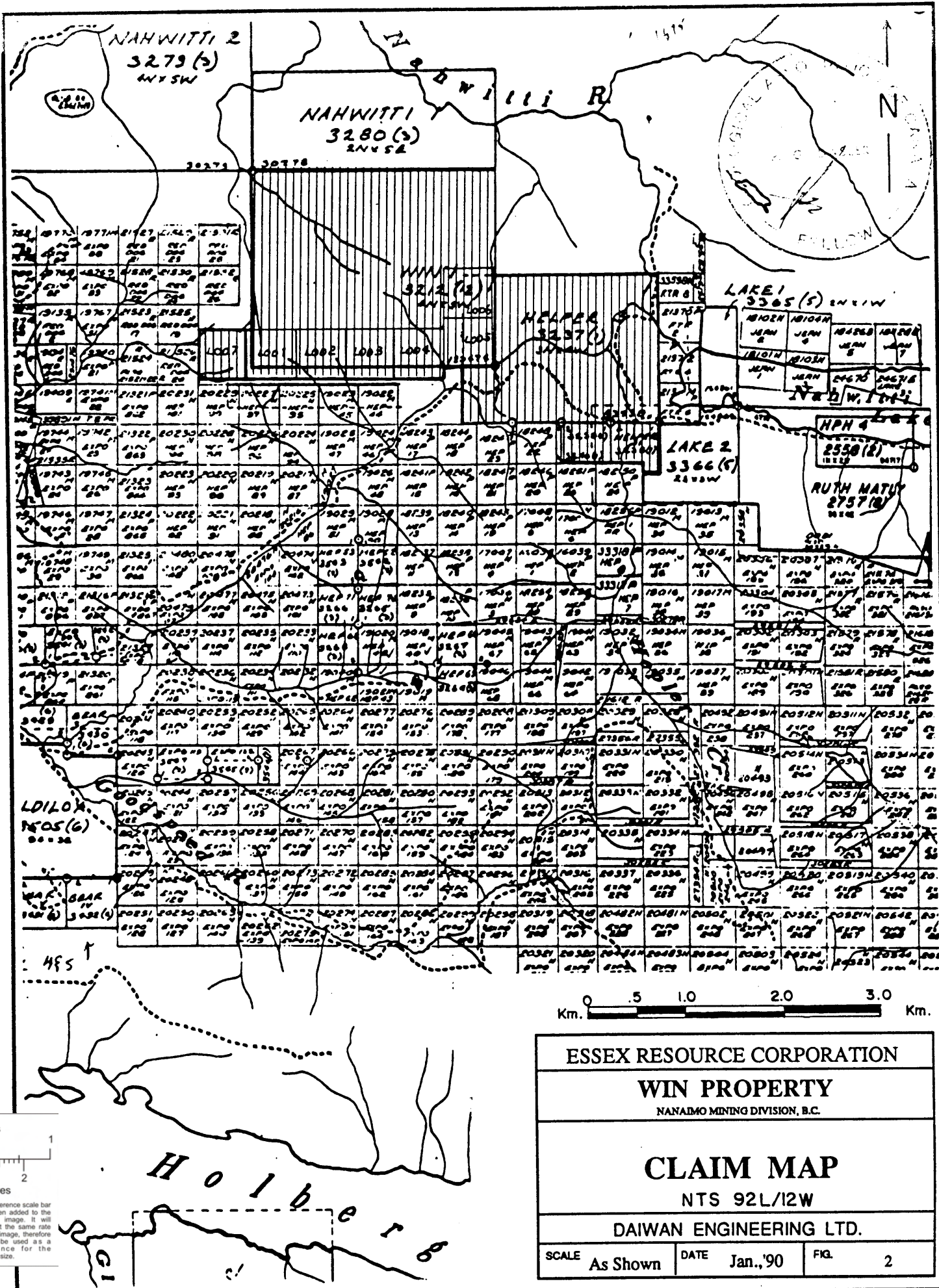
\* on acceptance of 4 years of assessment, filed in January 1990.

The Win claim is slightly misplotted on the government claim map, Figure 2. The additional Lod claims were staked to cover any fractions which occurred as a result of the misplotting. The Helper 1 & 2 claims were restaked for assessment purposes.

**Daiwan Engineering Ltd.**

(604) 688-1508, 1030-609 Granville Street, Vancouver, B.C. (604) 688-1508





0 5 1.0 2.0 3.0  
Km. Km.

ESSEX RESOURCE CORPORATION		
WIN PROPERTY NANAIMO MINING DIVISION, B.C.		
CLAIM MAP NTS 92L/12W		
DAIWAN ENGINEERING LTD.		
SCALE	DATE	FIG.
As Shown	Jan., '90	2

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inches

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centimetres

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## HISTORY

Northern Vancouver Island has been intermittently explored since the early 1800s. Copper was discovered in 1911 at Benson Lake, 25 miles southeast of Port Hardy. This property, known as Coast Copper Mine, was acquired by Cominco in 1916. They carried out considerable underground development work, but closed in 1931, remaining idle until 1960. It was then actively mined from 1962-72 producing copper and iron concentrates which were shipped to Japan.

Magnetite occurrences were located in the Benson Lake area in 1897 but were considered of interest only for their copper content until the early 1950s. They were explored for their iron content between 1950-56, then mined until 1967, when the operation ceased. Iron concentrates were shipped to Japan.

In 1963, the B.C. Department of Mines published the results of a recently completed aeromagnetic survey covering the northern end of Vancouver Island.<sup>2</sup> Since magnetite deposits were of interest at this time, considerable exploration activity was generated in the area examining all magnetic anomalies of interest.

One magnetic anomaly of fairly large areal extent was recorded on the eastern end of Rupert Inlet. Diligent prospecting in this area located a number of poorly exposed copper occurrences. A large number of claims were located in 1966 and subsequently the property was acquired by Utah Construction and Mining Company, now BHP-Utah Mines Ltd. Over the years, they added to the claim block and conducted extensive geological-geochemical-geophysical surveys and diamond drilling throughout the property. This work resulted in locating the large copper-molybdenum deposit which was developed into the Island Copper Mine. The mine commenced production in October 1971. Production to 1987 has been in excess of 200 million tonnes milled, for concentrate sales of 753,000 tonnes of copper, 23.1 million grams gold, 168 million grams silver, and 15.3 tonnes molybdenum<sup>14</sup>.

With the discovery of significant copper mineralization on the Utah property, a great deal of interest was generated in the area by individuals and companies searching for copper. Many copper occurrences were located but none were found to be economic at the time.

During the height of the exploration activity, Utah Mines Ltd. controlled most of the ground extending from the east end of Rupert Inlet to the west end of Holberg Inlet. The Win claims were at this stage located as the Ti, Bud, Mo, and Mon claims, immediately adjacent to the Utah Mines landholdings. The Utah Mines properties included the large block of claims covering the Island Copper deposit, as well as the Bonanza, Karmutsen, and Quatsino rocks to the northwest.

Exploration on these claims in 1968-74 located a large area of low grade copper-molybdenum mineralization in the Bonanza volcanics (the Hushamu zone) estimated to contain 58,420,000 mineable tonnes grading 0.32% Cu, 0.008% Mo and 413 ppb gold. The drill indicated reserve for the deposit is over 100 million tonnes at the same grade. It is presently being evaluated for open pit mining by Moraga Resources Ltd.

A number of other alteration zones, similar to that at Island Copper Mine and the Hushamu zone, also exist adjacent to the Win claim. Among these are the Red Dog and the Hep deposits, located one kilometre west and one kilometre south of the Win property respectively.

### Previous Work and Interpretations

Work on what is now the Win Group dates back to 1966 when Giant Explorations Ltd. examined a mineral occurrence (Aban showing) owned by G. Milbourne. The showing was reported as a skarn within the Quatsino limestone mineralized with sphalerite and galena. Three chip samples were taken and assays returned values of: 1.81% zinc, 0.97% lead and 0.06 oz/ton silver over 2.4 metres (8 feet); 2.78% zinc, 0.36% lead and 0.06 oz/ton silver over 3.05 metres (10 feet); and 1.71% zinc, 0.25% lead and 0.06 oz/ton silver over 1.83 metres (6 feet). No further work has been reported on this showing.

In 1968, Acheron Resources Ltd. began work on the TI, Mo, Mon, and Bud claims (now the Win 1, Nawhitti 1 and Lod 1-7 claims) located west of the Aban showing. Acheron explored the claims intermittently from 1968 through 1976 when the claims were abandoned. Work consisted of detailed geochemical and geophysical surveys and geological mapping. A compilation of work conducted by Acheron is shown on Figure 3. The geochemical survey produced several copper and zinc targets for additional work.

Copper anomalies with values in excess of 100 ppm Cu occur along the now recognized contact between a large diorite intrusive body with the Karmutsen volcanics. A sample of diorite float collected from a creek in this area assayed 0.1% copper and 5.14 g/t silver. An additional soil copper anomaly was outlined in the southwest corner of the current claim group but no further work was completed. This anomaly occurs in an area where diorite is now known to intrude Bonanza volcanics.

A large zinc anomaly was outlined in the center of the current Win claim. Hand trenching in 1973 and 1974 exposed zinc skarn within the Quatsino limestone. Samples of this zone (trench 2) taken in 1975 showed zinc mineralization with values of 3.72% and 3.97% zinc over 4.9 and 2.5 metres (16 feet and 8 feet). Trench 3 produced 6.02% zinc over a 4.9 metre (16 feet) width. A grab sample from trench 4 assayed 5.40% zinc.

The magnetometer surveys conducted in 1968 and 1970 outlined a small magnetic high adjacent to the zinc anomaly. This magnetic high corresponds to a small diorite intrusive. Another well defined magnetic high, with adjacent sharp low, occurs in the area of the copper soil anomalies. Mapping now shows this to represent the contact zone between diorite and the Karmutsen volcanics.

Since 1975 no significant work has been completed on the claims although they have been staked periodically.

### **REGIONAL GEOLOGY**

Vancouver Island, north of Holberg and Rupert Inlets, is underlain by rocks of the Vancouver Group. These rocks range in age from Upper Triassic to Lower Jurassic. They are intruded by rocks of Jurassic and Tertiary age and disconformably overlain by Cretaceous sedimentary rocks. Figure 3 shows the regional geological mapping of the northern part of the Island.

Faulting is prevalent in the area. Large-scale block faults with hundreds to thousands of metres of displacement are offset by younger strike-slip faults with displacements up to 750 metres (2,500 feet).

The Vancouver Group is described as follows:

(a) **Basal Sediment - Sill Unit: Middle and Upper Triassic Age**

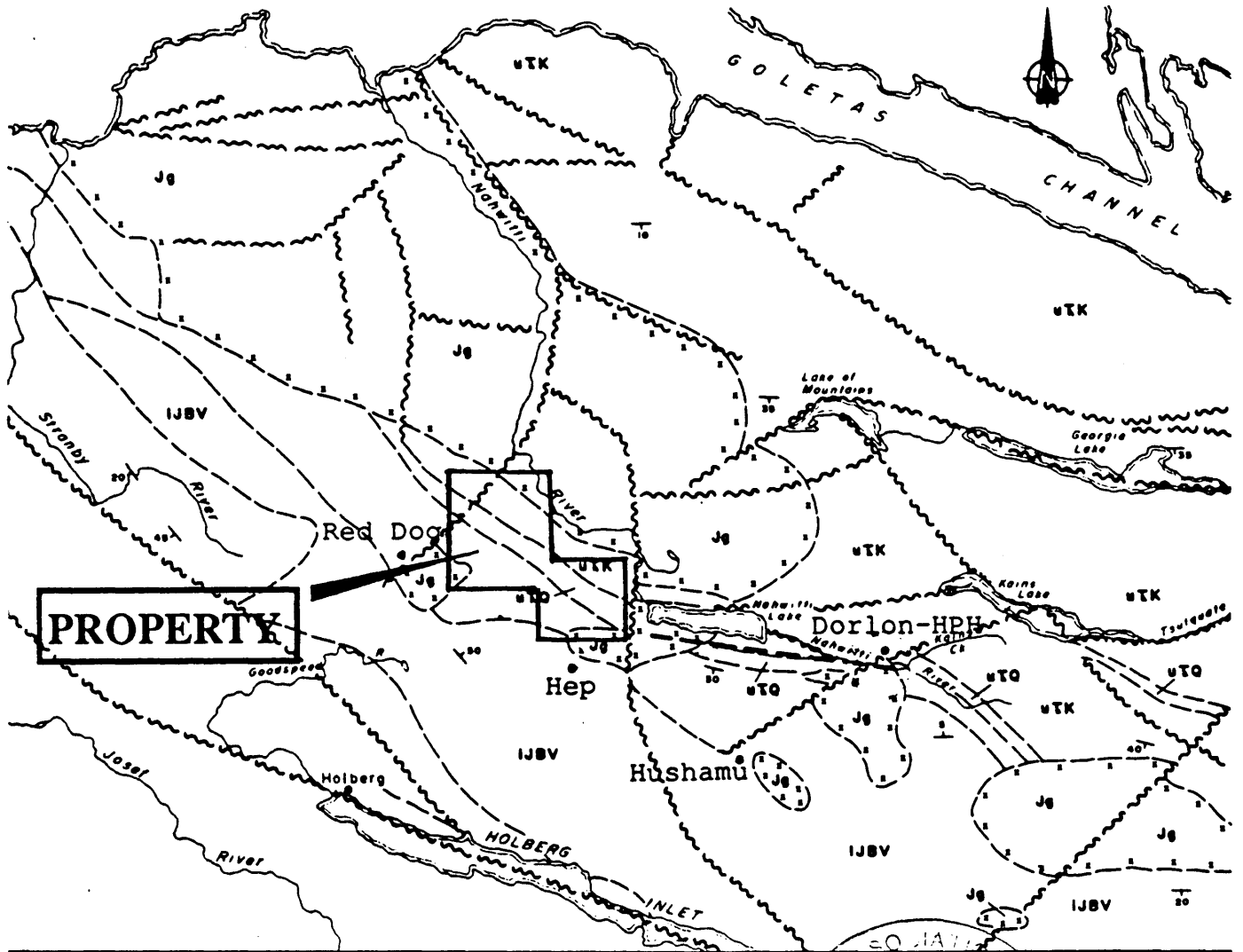
The basal sediment-sill unit consists of laminated to graded-bedded black shales and siltstones, silicified and invaded by diabase sills. The entire unit is estimated as 750-900 metres (2,500-3,000 feet) with the sedimentary portion being about 180 metres (600 feet) thick.

(b) **Karmutsen Formation: Upper Triassic Age**

Karmutsen Formation consists of 3,000-6,000 metres (10-20,000 feet) of volcanic flows, pyroclastics and minor sediments. It includes three distinct units: a lower pillow lava unit, a middle pillow breccia unit, and an upper lava flow unit. The latter consists of predominantly porphyritic and amygdaloidal basalt flows, individual flows of which range from 1-30 metres (to 100 feet) thick.

QUEEN CHARLOTTE  
SOUND

QUEEN CHARLOTTE  
STRAIT



**LEGEND**

**JURASSIC**



ISLAND INTRUSIONS: quartz diorite, grano-diorite, quartz monzonite, quartz feldspar porphyry.

**LOWER JURASSIC (BONANZA GROUP)**



Andesitic to rhyodacitic lava, tuff, breccia.

**TRIASSIC-UPPER TRIASSIC (VANCOUVER GROUP)**



QUATSINO FORMATION: limestone.



KARMTUSEN FORMATION: basaltic lava, pillow lava, breccia, aquagene tuff, greenstone; minor limestone.

**SYMBOLS**



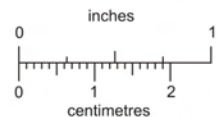
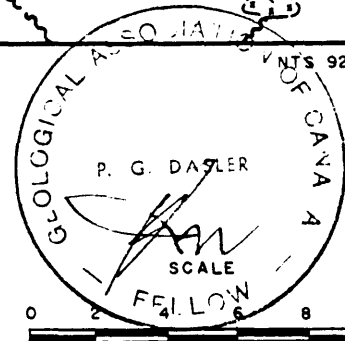
Geological Boundary.



Fault, Lineament (approximate)



Bedding.



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ESSEX RESOURCE CORPORATION		
WIN PROPERTY		
NANAIMO MINING DIVISION, B.C.		
<b>REGIONAL GEOLOGY</b>		
DAIWAN ENGINEERING LTD.		
SCALE As Shown	DATE Jan., '90	FIG. 4

Two thin bands of limestone occur near the top of the Karmutsen Formation. The distribution of limestone outcrops is erratic and suggests a series of lenses at the same general stratigraphic horizon rather than one continuous bed.

The lower contact of the formation has not been observed on the northern part of Vancouver Island. The upper contact with limestone of the Quatsino Formation generally is sharp and easily recognized, although limestones and basalt locally are interbedded over a narrow stratigraphic interval at this contact.

Low-grade metamorphism of the Karmutsen Formation rocks has resulted in pervasive chloritization and amygdules filled with epidote, carbonate, zeolite, prehnite, chlorite, and quartz.

Basaltic rocks along contacts with intrusive stocks are in many places converted to dark-coloured hornblende hornfels. Skarn zones occur sporadically along these contacts, both in the inter-lava limestones and in the basalts.

**(c) Quatsino Formation: Upper Triassic Age**

The Quatsino Formation ranges from 60-1,000 metres (200-3,500 feet) in thickness and consists almost entirely of limestone with a few thin andesite or basalt flows. It has conformable contacts with both the overlying Parson's Bay sediments and the underlying Karmutsen volcanics. The upper contact with the Parson's Bay Formation is gradational with limestone grading upward into carbonaceous argillites.

Within the contact metamorphic/metasomatic aureoles adjacent to intrusive stocks, skarn development and silicification of limestone, accompanied by chalcopyrite-magnetite or galena, sphalerite and silver mineralization has been noted.

**(d) Parson's Bay Formation: Upper Triassic Age**

The Parson's Bay Formation consists of between 60-360 metres (200-1,200 feet) of argillite, minor limestone, agglomeratic and tuffaceous limestone, tuff, quartzite and minor conglomerate. At both its base and top, the unit exhibits gradational contacts with the Quatsino and Harbledown Formations.

On a regional scale, the rocks are unmetamorphosed. Locally, adjacent to intrusive contacts, pyrite-magnetite replacement bands up to one-half inch thick in banded tuffs have been observed.

(e) **Harbledown Formation: Lower Jurassic Age**

The Harbledown Formation consists of 485 metres (1,600 feet), a non-volcanic argillite-greywacke sequence separating the Parson's Bay from the Bonanza Formation.

(f) **Bonanza Formation: Lower Jurassic Age**

The Bonanza Formation is approximately 1,500 metres (8,500 feet) thick. The lower portion consists of bedded and massive tuffs, formational breccias and rare amygdaloidal and porphyritic flows, in the compositional range andesite to basalt. Porphyritic dykes and sills intrude the lower part of the unit. In the upper part of the Bonanza, rhyodacite flows and breccias become more numerous and are interbedded with andesite and basalt flows, tuffs and tuff breccias.

Regional metamorphism within the Bonanza Volcanics is very low grade, possibly zeolite facies. Plagioclase commonly is albitized and saussuritized. Chlorite, epidote and laumontite occur within the matrix of volcanic breccias, in veinlets, and in amygdules. Coarse intraformational breccias locally are hematized.

Biotite and amphibolite hornfels occur adjacent to stocks which intrude the Bonanza Volcanics.

"Pyrobitumen", a black hydrocarbon erratically distributed within the Bonanza rocks, generally occurs as fracture fillings or in the centre of zeolite-carbonate veins. Its distribution is not related to the position of the intrusive stocks.

**Cretaceous Sediments**

The Vancouver Group is unconformably overlain by non-marine Cretaceous sediments of the Longarm Formation which are estimated to be about 300 metres (1,000 feet) thick in the Port Hardy area. These sediments, consisting of conglomerate, sandstone, greywacke, and siltstone and some carbonaceous and impure coal seams, occupy local basins. Early coal mining in the district was from several of these basins.

**Intrusive Rocks**

The Vancouver Group rocks are intruded by a number of Jurassic-aged stocks and batholiths. In the Holberg Inlet area a belt of northwest-trending stocks extend from the east end of Rupert Inlet to the mouth of Stranby River on the north coast of Vancouver Island<sup>15</sup>.

Quartz-feldspar porphyry dikes and irregular bodies occur along the south edge of the belt of stocks. Dykes are characterized by coarse, subhedral quartz and plagioclase phenocrysts set in a pink, very fine grained, quartz and feldspar matrix. They are commonly extensively altered and pyritized. At Island Copper Mine, these porphyries are enveloped by altered, brecciated, mineralized Bonanza sequence wallrocks. The porphyries, too, are cut by siliceous veins, pyritized, extensively altered, and are mineralized with copper where they have been brecciated. The quartz-feldspar porphyries are thought to be differentiates of middle Jurassic, felsic, intrusive rocks.

### Structure

The structure of the rocks north of Holberg and Rupert Inlets is that of shallow synclinal folding along a northwesterly fold axis. The steeper southwesterly limbs of the folds have apparently been truncated by faults roughly parallel to the fold axis. Failure of limestone during folding may have influenced the location of some of the faulting as indicated by the proximity of the Dawson and Stranby River Faults to the Quatsino horizon. Transverse faulting is pronounced and manifested by numerous north and northeasterly trending faults and topographic lineaments.

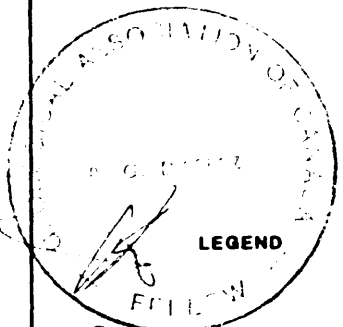
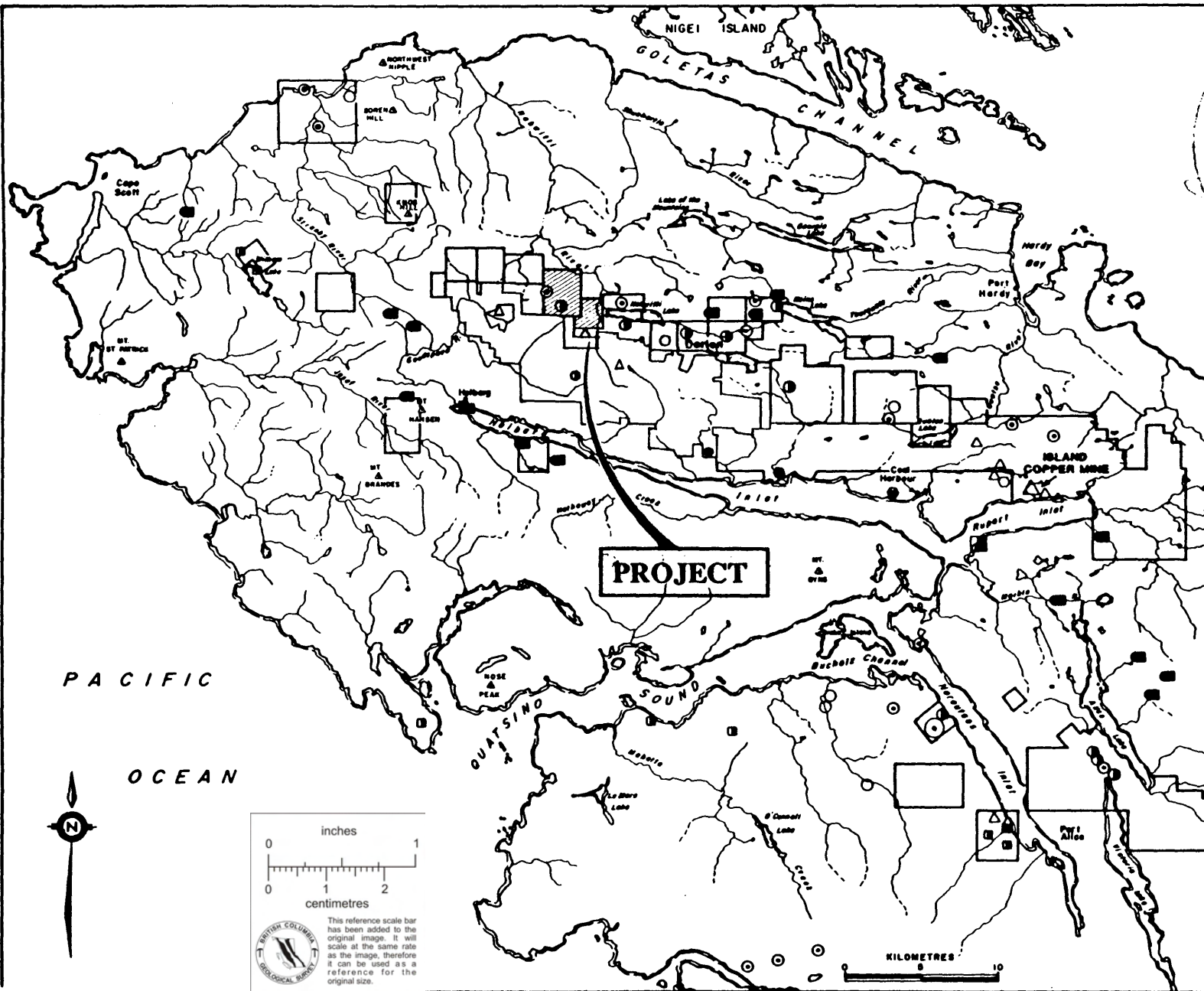
The northern part of Vancouver Island lies in a block faulted structural setting with post Lower Cretaceous northwesterly trending faults apparently being the major system (Figure 3). This system causes both repetition and loss of parts of the stratigraphic section, with aggregate movement in a vertical sense in the order of tens to hundreds of metres. The most significant of these fault systems trends west to northwest following Rupert and Holberg Inlets. Near the west end of the Holberg Inlet it splits with the main branch following the Holberg Inlet, the other branch passing through the west side of the Stranby Valley. Another northwesterly to westerly system passes through William Lake and still another smaller system passes through Nahwitti Lake.<sup>6</sup>

Northeasterly trending faults comprise a subordinate fault system. In some cases, apparent lateral displacement, in the order of a several hundred metres, can be measured on certain horizons. Movement, however, could be entirely vertical with the apparent offset resulting from the regional dip of the beds.

Recent computer modelling of the airborne magnetometer data has provided a very clear understanding of the relationship of secondary conjugate sets of northeast and northwesterly faults related to the major west-northwest trending breaks.<sup>7</sup> These conjugate fault sets appear to relate directly to the significant mineralization at the Island Copper, Hushamu, Hep and Red Dog copper/gold deposits.



90-100-5-D



- LEGEND**
- 80g Iron
  - Potassium-alumina
  - △ Porphyry copper
  - Gold quartz veins
  - Copper-bearing veins
  - Lead-zinc skarn or replacement in limestone
  - ⊙ Copper skarn
  - Iron skarn
  - Copper in volcanics
  - □ △ ○ Mineral occurrence
  - □ △ ○ Properties recording production
  - - Current Mineral Titles

(Data from British Columbia Department of Mines and Petroleum Resources, mineral inventory maps and cards; by E.V. Jackson and G.P. Eastwood)

ESSEX RESOURCE CORPORATION		
WIN PROPERTY		
KAMLAND MINING DIVISION, B.C.		
REGIONAL MINERALIZATION		
NORTHERN VANCOUVER ISLAND		
DAIWAN ENGINEERING LTD.		
SCALE As Shown	DATE Jan., '90	FIG. 4a

inches  
0 1

centimetres  
0 1 2

This reference scale bar has been added to the original image. It will scale at the same rate as the image, therefore it can be used as a reference for the original size.

KILOMETRES  
0 10

Generally, regional dip of the bedding is gentle to moderate southwesterly. Locally, in the area west of Holberg, dips are much steeper, but these are in close proximity to major faults. There is little folding or flexuring of bedding visible, except along loci of major faults where it is particularly conspicuous in thinly bedded sediments of Lower Bonanza. Bedding is generally inconspicuous in massive beds of Karmutsen, Quatsino and Bonanza rocks, particularly inland where outcrops are widely scattered.

### REGIONAL MINERALIZATION

A number of types of mineral occurrences are known on Northern Vancouver Island. These include:

1. Skarn deposits: copper-iron and lead-zinc skarns
2. Copper in basic volcanic rocks (Karmutsen): in amygdules, fractures, small shears and quartz-carbonate veins, with no apparent relationship to intrusive activity
3. Veins: with gold and/or base metal sulphides, related to intrusive rocks
4. Porphyry copper deposits: largely in the country rock surrounding or enveloping granitic rocks and their porphyritic phases.

Two significant discoveries on ground adjacent to the Win property illustrate the copper mineralization in the area:

The Hep claims which border the Win property to the south hosts an estimated 43,350 tonnes grading 0.80% copper at the intersection of two shear zones. The Hep claims are underlain by andesites and tuffs of the Bonanza Group which is intruded by quartz monzonite. Propylitic alteration is most common, but argillic and silica alteration occurs along fractures and adjacent to the volcanic-intrusive contacts. Pyrite with chalcopyrite and lesser bornite occurs along fractures and as fine disseminations within the andesite.

The Red Dog deposit is located 2 kilometres west of the Win property. Tuffs and tuff breccia of the Bonanza Group are intruded by diorite, quartz diorite, and quartz-feldspar porphyry of the island intrusions. The tuffs have been altered to hornblende biotite hornfels in contact zones with silicification and hydrothermal alteration in shear zones. Chalcopyrite occurs as fine grained

disseminations in the hornfels and in association with magnetite in siliceous breccia. Reserves are reported to be in excess of 45,359,000 tonnes grading 0.32% copper and 0.41 grams/tonne (.012 opt) gold.

Several showings around Nahwitti Lake, 3 kilometres east of the property, have been reported. These occurrences show significant zinc-gold mineralization near the transitional contact between Quatsino limestone and Bonanza group volcanics:

The Dorlon prospect includes three areas of mineralization within a 250 metre radius; the Zinc Vein, the Nose Showing, and the Shaft Showing.

The Zinc vein consists of sphalerite stringers up to 0.5 metres wide and 6.0 metres long striking north and dipping vertically. These stringers occur in silicified limestone adjacent to a felsic dyke. A 0.61 metre chip sample collected in 1966 assayed 19.2 grams/tonne (0.560 opt) gold, 24.0 g/t (0.701 opt) silver and 28.35% zinc. Channel samples of up to 0.30 metres returned values up to 18.49 g/t (0.54 opt) gold and 33.60% zinc.

The Nose showing consists of a 0.25 to 0.75 metre zone of massive sphalerite along a bedding plane in limestone. Trenching and drilling showed the mineralization to be gold bearing. A 2.0 metre chip sample assayed 4.18 g/t (0.122 opt) gold and 17.37% zinc, and grab samples of the massive sphalerite assayed up to 8.63 g/t (0.252 opt) gold and 32.19% zinc.

The Shaft showing consists of massive sphalerite within a breccia zone in limestone near a siliceous intrusive. A 1.6 metre channel sample assayed 10.31 g/t (0.301 opt) gold and 22.64% zinc, a 0.6 metre channel sample assayed 15.41 g/t (0.450 opt) gold and 29.63% zinc, grab samples assayed up to 14.79 g/t (0.432 opt) gold and 32.14% zinc.

The HPH is a further prospect which covers three showings of galena-sphalerite-silver mineralization. The first is a skarn within the Quatsino limestone adjacent to a felsic dyke. It is 3 metres wide and has been outlined along a strike length of 80 metres. Two shafts and one adit have been driven in the mineralization, which consists of galena and sphalerite with minor chalcopyrite, magnetite, pyrite and pyrrhotite. A 2.0 metre chip sample from the east wall of the east shaft assayed 3743.4 g/t (109.31 opt) silver, 38.1% lead and 10.6% zinc.

Galena and sphalerite stringers in silicified limestone near the contact with Karmutsen formation andesites assayed 267.4 g/t (7.81 opt) silver, 3.9% zinc, and 9.24% lead across 1.5 metres, and other areas of galena, sphalerite pyrite and sparse chalcopyrite mineralization in silicified Quatsino limestones occur near the contact with Bonanza Group volcanics.

The HPH and Dorlon prospects are managed by Hisway Resources Corp. and Silver Drake Resources Ltd.

### PROPERTY GEOLOGY

The Win claim group is underlain by volcanics and sediments of the Karmutsen, Quatsino, Parson Bay, and Bonanza formations. The rocks are intruded by at least four distinct phases of intrusives. The attitudes of the rocks are generally northwest striking, southwest dipping except where the bedding has been disrupted by the intrusives and the northwest and northeast trending late stage faults.

A description of the various formations encountered on the property is as follows:

The Karmutsen volcanics consists of aphanitic to porphyritic, dark green to black basalts and andesites. This unit trends northwest and is intruded by a large diorite batholith from the northeast. Near the contact with the intrusive, the volcanics contain abundant finely disseminated magnetite. The Karmutsen basalts are conformably overlain by the Quatsino limestones in the southeast portion of the claims. A major northwest trending fault is the upper contact in the northwest portion of the property.

The Quatsino formation consists of medium bedded to massive dark grey to black limestone. The limestone has been recrystallized near the contact with a small diorite plug. The limestone has been altered to an epidote-garnet to actinolite-garnet skarn with abundant sphalerite and pyrite.

Interbedded with the limestone at various locations on the property is a feldspar crystal tuff. The crystal tuff is highly siliceous with up to 2% disseminated pyrite. Beds range in thickness from a few centimetres to tens of metres.

The Parson Bay formation overlies the limestone and consists of very siliceous argillites, shales, and tuffs. These sediments are generally thin bedded, with andesitic flows (crystal tuffs?) interbedded. These sediments and volcanics outcrop in the southwest portion of the property. The sediments display northwest strikes and moderate southwesterly dips. The bedding has been disturbed adjacent to faults. The argillites and tuffs contain disseminated pyrite and are highly rusted and enriched with pyrite adjacent to the late stage faults.

Overlaying the Parson Bay sediments and outcropping in the extreme southwest portion of the property are andesites of the Bonanza Formation. The andesites exhibit varying degrees of alteration, depending on their proximity to faults and the intrusive bodies. Adjacent to the diorite intrusions the volcanics are highly siliceous and have abundant quartz stringers and magnetite disseminated throughout. Adjacent to faults the andesites display argillic alteration and areas with potassium feldspar alteration of stringers.

Intruding the volcanics and sediments are at least four distinct phases of intrusions. A large diorite batholith extends onto the property from the northeast. This diorite is medium grained and relatively unaltered. Fracture density ranges from low to moderate near faults and is blocky with no significant alteration. Only trace pyrite was noted in this diorite. The diorite is in contact with the Karmutsen basalts and probably influences the disseminated-magnetite in the basalts along the northwest-southeast contact zone.

Three outcrops of diorite occur near the contact of the limestone with the Parson Bay sediments. These plugs are dioritic in composition and may be related to the large batholith in the northeast. The pluton in the center of the Win claim has introduced zinc, copper, lead and gold mineralization into the limestone.

A large granodiorite pluton outcrops on the property in the southeast. The granodiorite is pink, potassium feldspar rich and medium grained. Alteration consists of potassium feldspar alteration of the stringers throughout the intrusive. The granodiorite is in fault contact with the limestone in the southeast corner of the claims. The fault is marked by a sharp topographic break and the lack of alteration in the limestone.

The third intrusive observed on the property is on the western edge, it consists of a quartz diorite that intrudes the sediments. The quartz-diorite is fine grained with quartz and feldspar phenocrysts in a dark green ground mass.

The fourth intrusives are the mafic dykes that cut the property. These dark green dykes are generally very weathered and appear controlled by late stage northeast and northwest trending faults.

## MINERALIZATION

Four different forms of potential base and precious metal mineralization were observed on the property. They include - metasomatic replacement, semi-massive sulphide veins, quartz veins and copper bearing intrusive.

In the centre of the Win claim, near the upper contact of the limestone adjacent to a diorite intrusive is a sulphide replacement zone<sup>18</sup>. In previous surveys in 1968 & 1975 the "skarn" was described as being up to 30 metres wide and 210 metres long. Holcapek<sup>18</sup> described the main exposed economic mineralization .."consists of sphalerite of dark or black colour (marmatite) and minor galena. The sphalerite occurs as massive lenses, streaks or fine disseminations with bright yellow staining where strongly oxidized. The galena normally is as very fine disseminations, not necessarily associated with the sphalerite.

"Sampling of the (1968 & 1975) trenches (by D. Reinke) suggest that the zinc values are distributed throughout the width of the skarn, but higher values appear to occur along the footwall." On the Win claim chip samples of up to 8.59% zinc and 0.22% copper over 1.5 metres and 3.60% zinc, and 1.99 g/tonne (0.058 opt) gold over 1.0 metres were obtained from the zone. These samples are shown on Figure 3. It is postulated that the zone of replacement will continue down dip and along the contact. Grades and widths are expected to vary down dip and can only be tested by drilling. Figures 10 and 11 in the appendix show interpreted cross-sections of part of the zone.

The mode of occurrence of this zinc-rich replacement zone is similar to that reported on Hisway Resources Dorlon-HPH property. There zinc-silver and gold mineralization occurs in the limestone, with the siliceous Parson Bay sediments acting as a barrier to the solutions.

Approximately 400 metres east of the skarn a large semi-massive sulphide vein occurs within the margin of a diorite plug. The vein strikes northeast (010°-050°) and dips southeast at 50°-60°. The vein is offset right laterally by 20 metres along a north west trending fault. The vein is up to 1.5 metres wide and varies in composition from footwall to hanging wall. Three adjacent samples across the various zones of the vein assayed 10.80% zinc, 0.93% copper, 0.36% lead, 15.60 g/tonne (0.455 opt) silver, and 0.137 g/tonne (0.004 opt) gold across 1.5 metres. Figure 12 in the Appendix is a sketch of the pit in which the vein was uncovered. Drill holes have been proposed to explore the extent of the vein and to check for parallel systems.

Locally derived quartz vein float was found in two areas of the claims. The first area was along logging road NE66 in the south of the Win claim, and consisted mainly of quartz with coarse crystal growth in small vugs. There was trace gold (62 ppb) in the sample.

The second area of quartz veining was 500 metres south of the skarn zone, near line 4+50E at 3+00N. Here the vein material consisted of banded quartz-amethyst with trace disseminated pyrite cut by magnetite veining. It was found adjacent to a mafic dyke. Trenching removed the vein

material, but indicated that the quartz and amethyst may form irregular pods and stringers alongside the dyke. The geochemical surveys conducted in 1968 and 1990 outlined a zinc anomaly in the area of the float. In the recent work soils showed anomalous zinc and weak gold (11 & 22 ppb Au). Samples of the vein material assayed up to 150 ppb Au, gold grades may increase at depth or along strike and additional work should be completed to trace the veining.

Two areas on the claims have geology favourable for "porphyry" copper-gold deposits similar to the Hushamu and Red Dog deposits. The first is along the eastern boundary of the Win claim where the Karmutsen volcanics have been intruded by a large diorite batholith. The geochemical survey conducted in this area in 1968 defined a large copper anomaly of +80 ppm with values up to 184 ppm (see Figure 3). A sample of diorite float from one of the creeks assayed 0.1% copper and 5.14 g/tonne (0.15 opt) silver (no gold value was reported). Further work is necessary in the area to expose outcrop. Two drill holes have been proposed (see Figures 10 and 11 in Appendix 3).

At the second area, in the southwest corner of the claims, the Bonanza volcanics are intruded by diorite with disseminated pyrite, chalcopyrite and molybdenite. The andesites are highly siliceous with fine quartz stringers and disseminated pyrite and magnetite. Rock samples collected in this program showed elevated copper and molybdenum with values ranging up to 281 ppm copper and 44 ppm molybdenum. Follow up work in this area is recommended and should consist of grid extension and a geochemical survey.

## SURVEY RESULTS 1990

### GEOCHEMICAL SURVEY

A total of 640 soil samples were collected from the property. The samples were collected at 25 metre stations on lines spaced 150 metres apart. The soil samples were collected from an average depth of 25 cm from the B horizon where possible, using a soil shovel and waterproof paper bags.

Five stream sediments were collected from four of the creeks that drain the claim group. The first sample was a silt collected from a creek that drains the area on the Helper claim near where the Aban showing is reported to occur. The remaining four stream samples were collected using a gold pan, the stream sediment was panned down to an approximate two tablespoon size and placed in a plastic bag. The process was repeated two to four times to ensure sufficient sample was collected.

The rock samples were representative chip samples, or float samples collected by R Husband or P Dasler. The rock samples were shipped to Acme Labs for crushing, grinding and analysis by 30 element I.C.P. and geochemical gold. Samples with highly anomalous values of zinc, copper, lead, silver, or gold were resubmitted for assay (gold by fire assay using 1/2 assay ton). Descriptions of all rock samples can be found in Appendix 1.

The samples were delivered to Acme Analytical Laboratories Ltd. in Vancouver where the silts and soils were dried and screened to -80 mesh and the rocks were crushed and powdered to -80 mesh. The samples were then analyzed for 30 elements by I.C.P. which involves the digestion of 0.5 grams of the sample with 3-1-2 HCl-HNO<sub>3</sub>-H<sub>2</sub>O acid at 95 degrees celsius for one hour. This sample is then diluted to 10 ml with water and analyzed. The samples were also analyzed for gold by acid leach and atomic absorption by Acme labs.

In 1968 an extensive regional geochemical survey was conducted by BHP Utah Mines Ltd. This survey resulted in 9592 soil samples being collected and analyzed. A detailed statistical analysis was conducted on the results and threshold values from Assessment report 2190<sup>19</sup> is included in Appendix 2. The calculated threshold values for the copper and zinc in each rock type in this area are as follows: Karmutsen - 68 ppm copper, 42 ppm zinc

Quatsino limestone - 109 ppm copper, 90 ppm zinc

Bonanza - 25 ppm copper, 44 ppm zinc

Intrusives - 31 ppm copper

Altered Rocks - 36 ppm copper 16.2 ppm zinc.

## Results:

### Stream Sediments

One silt sample and four pan samples were collected from various creeks that drain the claims. The sampling produced highly variable results, however anomalous values were found for varying elements in each sample.

The silt sample, (#109951), was collected from a small creek near where the Aban showing is reported. This silt assayed 14 ppb gold and 0.5 ppm silver. Values of copper, zinc and lead were background levels.

The two pan samples collected from the creek that drains the southwest corner of the claims showed variable results. Sample 109963 assayed 201 ppm zinc and 0.7 ppm silver with background levels of copper and lead. Sample 109966 contained 126 ppm copper and 88 ppm zinc with background levels of lead and silver.



Pan sample #109960 from the north-south flowing creek near line 21E contained 208 ppm zinc with background values in the remaining elements. Sample 109962 from the creek 100 metres southwest, near the diorite outcrop, contained 107 ppm copper.

### Rocks

The locations and assay results for the 72 rock samples taken from the claims are shown on Figure 4. A total of 14 samples were resubmitted for assay of lead, zinc, copper, gold and silver. The sampling highlighted several areas of interest on the claims.

The first is the zone of zinc replacement near the upper contact of the limestone at 8+00N, 3+00E. The zone is adjacent to a small diorite intrusive. Zinc mineralization was first discovered in this area in 1973 when several hand trenches were dug on it. It was reported to extend 210 metres along an attitude of 280/45°S. A 4.9 metre chip assayed 6.02% zinc, 0.04% lead and 4.8 g/tonne (0.140 oz/t) silver. The current program uncovered epidote-actinolite skarn mineralization in the area of the previous trenching. Sampling of the mineralization here returned 2.29% zinc and 1.13 g/tonne (0.033 oz/ton) gold over 0.3 metres, collected immediately under a 2.0 metre wide magnetite bed. Other samples along this zone yielded values of 8.59% zinc and 0.22% copper and 3.60% zinc and 0.058 oz/ton gold over 1.5 and 1.0 metre widths respectively.

Three adjacent samples across the zone exposed 120 metres southeast (7+00N, 4+50E) produced 1.66% zinc across 2.75 metres.

The semi massive sulphide vein located within the diorite at 7+50N, 8+50E averaged 10.80% zinc, 0.93% copper, 0.36% lead, 0.455 oz/t silver and 0.004 opt gold over 1.5 metres from three adjacent samples across the vein. A further sample assayed 13.33% zinc, 0.21% copper, 0.59% lead, 0.27 opt silver and 0.002 opt gold over 0.3 metres across a highly siliceous section of the vein.

A 0.4 metre sample across the extension of this vein across a northwest trending fault assayed 20.85% zinc, 1.17% copper, 0.01% lead, 21.6 g/tonne (0.63 opt) silver, and 0.377 g/tonne (0.011 opt) gold. This vein occurs within the margin of a small diorite stock.

A 1.0 metre chip sample of highly siliceous, fractured sediments, taken at 3+00S 20+00E, (#109495), assayed 0.31% copper 30.17 g/tonne (0.88 opt) silver and 0.377 g/tonne (0.011 opt) gold. This mineralization would indicate that there has been significant replacement style mineralization along bedding planes and faults.

A full list of assays is attached to Figure 5 and the assay certificates and sample descriptions are in Appendices 1 & 2.

### Soil Geochemistry

The results for gold, silver, zinc, copper, lead and arsenic are plotted on Figures 6a-6f. A frequency distribution graph was plotted for each of the six elements and results are shown in Appendix 2. The values contoured for each element were guided by this data, and by the regional survey data (Appendix 2), in order that all trends would be shown.

The values for gold in the 640 soil samples ranged from 1 to 38 ppb and contours were drawn at 10, 15, 20, 25, 30 ppb., Figure 6a. Anomalous gold in the soil generally occurs as single station anomalies throughout the grid. Areas of significant trends include:

Line 4+50E at 3+00N centres an anomaly that extends to lines 150 metres away to the east and west. This anomaly occurs in the area of the quartz-amethyst vein float.

In the vicinity of the skarn near the upper contact of the limestone, values of 26 and 37 ppb were obtained.

On the eastern portion of the grid anomalies are spotty, but appear more frequently near the upper contact of the limestone.

Silver values are plotted on Figure 6b and values range from 0.1 to 5.8 ppm. Contours were drawn at 1.0 and 1.5 ppm and are considered anomalous. In the area of the quartz-amethyst vein float silver values range to 1.6 ppm and in apparent east-west trend is shown. Along the contact of the limestone with the overlying Parson Bay sediments, numerous anomalous values occur and detailed geochem may assist in defining exact trends and provide further drill targets. The eastern portion of the grid hosts numerous spot anomalies with the highest value of 5.8 ppm occurring here. This area is approximately where the Aban showing is reported to occur although it could not be located in 1990 due to recent logging and dense undergrowth.

The zinc values are plotted in Figure 6c, and values range from 13 to 3185 ppm. The majority of the samples were collected across the Quatsino limestone, and many of the values surpass the (1968 survey<sup>19</sup>) 90 ppm Zn threshold, indicating that the whole area is anomalous in zinc. Values over 150 ppm were contoured and several areas of interest were defined. An approximate east-

west trending anomaly occurs where the quartz-amethyst vein float was found with values to 638 ppm Zn. A very extensive anomaly extends over the skarn zone. It trends northwest over 450 meters and has values up to 2242 ppm Zn. It follows the assumed upper contact of the limestone. A further very prominent northwest trending anomaly occurs approximately 200 metres to the north. Here values range up to 3185 ppm Zn, and appear to represent a parallel zone of zinc mineralization within the limestone. The eastern portion of the grid has several isolated anomalous zones and one very large anomaly (1039 ppm Zn) in the vicinity of the Aban showing.

Copper values are shown on Figure 6d and contoured at 50 ppm intervals. Copper values range from 1 to 827 ppm but are generally less than 75 ppm. The 50 ppm contour shows many spot anomalies. Values over 100 ppm are highly significant. Areas of elevated copper occur in the vicinity of the skarn zone and extend northwest along the contact. The most significant copper values occur near the contact of the limestone with the older Karmutsen volcanics to the north. In the northwest portion of the grid this contact is a major fault. Here values range up to 827 ppm Cu. In the eastern portion of the grid the formational contact is thought to be conformable. In this area copper values range to 252 ppm. Around the Aban showing a significant northwest copper trend is shown with values up to 288 ppm. This anomaly is centred on the showing, and extends 300 metres to the north and southeast. It ranges up to 75 metres wide.

Lead values from the survey range from 2 to 305 ppm and are shown on Figure 6e. Anomalous isolated lead values are occur throughout the grid. Significant trends occur near where the quartz-amethyst vein float was found with values up to 106 ppm Pb. Lead values around the Aban showing range up to 87 ppm.

Arsenic values are plotted on Figure 6f and range from 2 to 222 ppm. Contours at 25, 50, and 75 ppm were drawn to highlight any significant trends. Elevated arsenic occurs in the vicinity of the quartz-amethyst float. Arsenic does not appear to be related to other elements analyzed.

The contouring of the geochemical plots is heavily biased by the sample line spacing (150 metre spaced lines, 25 metre sample spacing). Infill lines in areas of significant anomalies would assist in delineating the true orientation of the anomalies.

## GEOPHYSICAL SURVEY

A total of 17.5 km of crossline was surveyed using a Scintrex MG-2 Proton Precession Magnetometer and a Sabre Electronics Model 27 VLF-EM. Readings were taken every 25 metres on lines spaced 150 metres apart.

### Magnetometer

This instrument measures the earth's total magnetic field to within one gamma. A base station was used to check for diurnal variations but these were found to be insignificant (less than 50 gammas). There were no strong variations observed in the earth's magnetic field during the survey.

The plotted results from the magnetometer survey are shown on Figure 7a. Contours were drawn at 500 gamma intervals and the background values were between 56,000 - 57,000 gammas. Values above 57,000 gammas are considered as high and values below 56,000 gammas as lows. Several small magnetic highs occur scattered throughout the grid. These highs are represented by "A" on the plan, and likely represent small intrusive bodies.

Areas marked by "B" on the map are magnetic lows and represent areas of alteration or changes in lithology. In the northwest portion of the grid a narrow low trends east-west and cuts different lithologies and probably represents alteration adjacent to a fault zone. In the vicinity of "B" sharp topographical features indicate faults.

The large magnetic highs illustrated by "C" on the map represent the large diorite batholith intruding the claims from the northeast.

### VLF-EM

For this survey the transmitter located at Seattle, Washington (24.8khz) was used for all readings. The Sabre Electronics Model 27 VLF-EM acts as a receiver only. Powerful radio transmitters set up throughout the world for the purpose of military communication and navigation generate a primary field in the 15-25 khz range. When this primary field encounters a buried conductor (eg. massive sulphides, geological facies change, water filled faults, etc.) a secondary field is induced which distorts the primary field. The VLF-EM measures this distortion of the field. For maximum coupling, best results are obtained when the transmitting station is located in the direction of the geological strike of the conductor.

It should be noted that a limitation of the VLF-EM Method is its relatively high frequency. This causes such things as ridge tops, groundwater, swamps, and creeks to be recorded as conductors. Also the penetration is limited to about 20 metres of overburden or 60 metres of bedrock.

The VLF-EM data was Fraser filtered using Scintrex's FRASER program. The results of the VLF-EM survey are plotted on Figure 7b. Well defined northwest trends are evident. The most obvious is the linear that crosses the grid near the center, this axis corresponds to the upper contact of the limestone with the overlying Parson Bay sediments. A parallel axis occurs north of this contact and about 100 metres south of the known lower contact of the limestone. This may represent the dip of the contact. Centred on line 4+50E at 4+25N is another significant east-west trending anomaly. This anomaly corresponds to the location of quartz-amethyst vein float and may indicate the attitude of the veining that was the source of the float.

### DISCUSSION OF RESULTS

The exploration on the Win group during January and February 1990 was hampered by excessive logging slash and underbrush developed following clearcut logging operations on the property in 1975. No evidence remained of the original survey grids, and there was no remnant of the (hand) trenching operations which had provided the original interest for this survey.

The area for the geochemical and geophysical survey was limited to the area of the Quatsino Formation and its contacts with the Karmutsen and Parsons Bay formations. This was because of the previously known mineralization on this property and on others in the district, and the budget constraints of the project.

A trenching programme was carried out using a Caterpillar 225 tracked excavator in an attempt to expose the skarn areas for sampling. This was not completely successful because of either the topography, overburden, or the very weathered nature of the sulphide zones. Further trenching is warranted. The current work was curtailed by a heavy snow fall.

The exploration program conducted in 1990 was successful in defining targets for follow-up work. The geochemical survey reinforced the information obtained from earlier surveys, and outlined new mineralized areas.

The zinc and silver plots outline the area of known zinc skarn near the upper contact of the limestone, as well as delineating probable extensions of it. The VLF-EM survey shows a strong anomaly that corresponds to this zone and the magnetometer survey defined three small highs along the zone that probably represent intrusives.

Rock samples taken from the exposed zinc mineralization assayed 8.59% zinc and 3.60% zinc 1.99 g/tonne and 0.058 oz/tonne gold over 1.5 and 1.0 metres respectively. Samples taken in 1968-75 and reported 50 metres northwest of this site, assayed 6.02% zinc 4.8 g/tonne (0.140 oz/ton) silver across 4.9 metres. The zone should be drill tested to explore the zone along strike and down dip and to check for parallel systems.

Other showings in the region (HPH - Dorlon) report skarn development along both the upper and the lower contact of the limestone. It appears as if the formational contacts provide solution paths for fluids generated by the numerous intrusives in the area. The intense silicification of large areas of the Parsons Bay sediments above the limestones highlights the wide areal extent of the mineralizing events, and the potential for large scale replacement sulphide mineralization in the limestone. Although no skarn was mapped near the lower contact due to limited outcrop a drill hole is proposed to cross the limestone and check for skarn mineralization at the lower contact.

A second area for follow up work is in the vicinity of the quartz-amethyst vein found as float. Here the geochemical survey outlined an approximate east west trending anomaly in zinc, silver, gold and to a lesser extent lead and arsenic. This anomaly extends for a minimum of 300 metres for each element. A strong east-west anomaly is also shown by the VLF-EM survey and may represent a sulphide bearing vein system. Samples of the float did not return highly anomalous values in any of the 30 elements tested; however they did contain slightly elevated amounts of gold (81.89 and 150 ppb). Follow up work in this area should include infill detailed geochemistry and geophysics followed by trenching and/or drilling, to determine the potential for epithermal style gold mineralization.

The third area for follow-up work is in the area of the Karmutsen volcanics and the large diorite batholith to the northeast. The survey conducted in 1968 and 1969 defined a significant (80+ ppm) copper anomaly (see Figure 3). There is extensive soil and overburden cover in this area, so no rock chip sampling has been completed, however the sample of diorite float which was collected in the earlier survey assayed 0.1% copper and 5.14 g/tonne (0.15 oz/ton) silver. The current mapping indicated intense felsic alteration in the diorite just east of the zone. A magnetometer survey conducted in 1969-1970 defines the contact zone between the volcanics and the diorite. Follow up work could consist of additional geochemistry followed by trenching/drilling to test the diorite. In this area the batholith may be mineralized with stringer copper mineralization, derived from the assimilation of the copper rich Karmutsen volcanics (see Figure 4a).

In the southwest corner of the claims, diorite with disseminated pyrite, chalcopyrite, and molybdenite which was found to intrude Bonanza volcanics defines the fourth area of interest. The most intense clay alteration and pyrite mineralization in this area is bisected by the claim boundary. The area to the south is heavily forested, and the zone was not traced further. No anomalous samples were collected during this program but the 1968 geochemical survey outlined a copper anomaly on the Win claims in this region and additional work is warranted.

The fifth target area is the old Aban showing, where in 1968 Giant Explorations Ltd reported a skarn mineralized with sphalerite and galena. Samples of 1.81% zinc, 0.97% lead and 2.78% zinc and 0.36% lead were reportedly taken across 2.4 and 3.05 metres. No evidence of the showing was found during this program due to recent logging and road building, and the area is covered with new forest plantings (1976), and thick undergrowth. The geochemical and geophysical survey clearly define an area for follow up work. Highly anomalous values of zinc, silver, gold, copper and lead were obtained from soils in the area where the Aban showing is reported to be located. The magnetometer survey shows a strong high to the northeast that likely represents intrusive rock. Limestone outcrops in the area. Follow up work consisting of infill detailed geochemistry and geophysics followed by limited trenching (because of new tree planting) and possibly drilling is recommended in this area.

The sixth target area is the semi massive sulphide vein that occurs within the margin of a small diorite intrusive. The vein was uncovered in a pit on the side of the road between two of the survey lines and no definite geochemical or geophysical signature was established. The northeast striking, southeast dipping vein has a width of 1.5 metres and is exposed over 8 metres in the bottom of the pit. It appears to be offset 20 metres right laterally by a northwest trending fault, see Figure 12. A series of three adjacent chip samples across the vein averaged 10.80% zinc, 0.93% copper, 0.36% lead, 15.60 g/tonnes (0.455 oz/t) silver and 0.137 g/tonne (0.004 oz/ton) gold across 1.5 metres. Another sample of the vein assayed 13.33% zinc 0.21% copper and 0.59% lead across 0.3 metres. A 0.4 metre chip across the extension of the vein across the fault assayed 20.85% zinc, 1.17% copper 21.60 g/tonne (0.63 oz/t) silver and 0.377 g/tonne (0.011 oz/t) gold. Further similar veining is possible in this area, however outcrop is very sparse. This zone could easily be tested at depth and along strike by drilling.

## CONCLUSIONS

- 1.0 The Win Claim Group is located in an area favourable for the occurrence of zinc-gold and copper-gold replacement style mineralization.
- 2.0 Zinc mineralization with gold can be traced on the claims near the upper limestone contact over a minimum of 170 metres. A persistent geochemical anomaly of +100 ppm Zn, and high of 3180 ppm Zn parallels this skarn 200 metres to the north and may represent a second major zone of replacement.
- 3.0 The Aban mineral occurrence, 1500 metres southeast of this area is in the limestone near the Parsons Bay Sediments contact. This appears to be another zone of significant replacement mineralization. Further trenching is required to establish if there is replacement along the whole Quatsino limestone-Parsons Bay sediments contact.
- 4.0 Gold values of up to 2.0 g/tonne (0.058 opt) over 1.0 metres were obtained from areas of the zinc mineralization on the Win property. On Hisway Resources Dorlon and HPH properties (zinc-gold replacement along the same formational contact), gold values up to 19.2 g/tonne (0.560 opt), over 0.61 metres are reported. Similar regional mineralizing processes are clearly evident.
- 5.0 Geochemical and geophysical surveys have delineated trenching and drill targets along the upper and lower limestone contacts.
- 6.0 Locally derived quartz-amethyst vein float containing gold values to 150 ppb Au was found within a zone of anomalous lead (59, 106 ppm Pb) and gold (11, 22 ppb Au) soil geochemistry. This zone is also characterized by a linear geophysical VLF-EM response.
- 7.0 A sulphide vein averaging 10.8% zinc and 0.93% copper over 1.5 metres in width and exposed over 8 metres in length, within the margin of a diorite intrusion may indicate a zone of remobilization and fracture replacement.
- 8.0 The previous geochemical soil surveys on the property indicate an irregular 700 metre X 500 metre anomaly with elevated (+80 ppm) copper within the diorite, near the contact of the Karmutsen volcanics. A float sample of the diorite which assayed 0.1% copper indicates a significant target for copper mineralization.



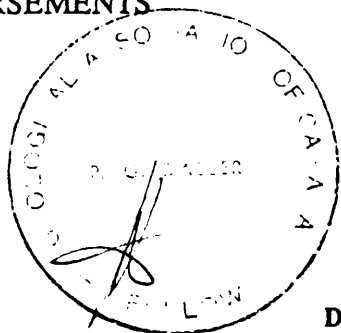
- 9.0 Potential copper-gold mineralization, similar to the Red Dog deposit, may occur where diorite with disseminated pyrite and lesser chalcopyrite and molybdenite, was found intruding Bonanza Group Volcanics in the southwest of the claim group.

### RECOMMENDATIONS

- 1.0 Drilling should be conducted along the areas of known zinc mineralization to explore grades and thicknesses at depth and along strike and also check for parallel zones of replacement.
- 2.0 Drilling should be conducted on the semi massive sulphide vein to explore the extent of the vein mineralization.
- 3.0 Infill geochemical soil sampling supported by VLF and magnetometer surveys should be carried out in the area of 3+00N, 21+00E to define the Aban showing. Limited trenching can be completed with possible drilling.
- 4.0 Detailed geochemistry, trenching, and prospecting is warranted in the area of the quartz-amethyst vein float followed by possible drilling.
- 5.0 Additional geochemical sampling should be carried out over the copper zone north of the of Karmutsen Formation-diorite contact with trenching to expose outcrop. Drilling may be necessary to achieve samples in this area, and to explore the diorite at depth.
- 6.0 Additional geochemical soil sampling supported by magnetometer and VLF surveys should be carried out in the southwest corner of the claims near the diorite-Bonanza Formation contact to explore for copper-gold mineralization.

**STATEMENT OF COSTS**

1.0	PERSONNEL	
	1 Senior Geologist 12.35 days @ \$380/day	4,693.00
	1 Project Geologist 48.4 days @ \$260/day	12,584.00
	2 Field Technicians 69 days @ \$280/day	19,320.00
	1 Draftsperson 9.4 days @ \$220/day	2,013.00
2.0	FOOD AND ACCOMMODATION	
	3 men 34 days @ \$44.15/day ea.	4,503.08
3.0	TRANSPORTATION	
	1 4x4 34 days @ \$99.33/day (incl. gas)	3,377.26
	1 4x4 4 days @ 101.10/day (incl. gas)	505.50
	Airline	850.20
4.0	FIELD SUPPLIES (flagging, topo, etc.)	1,521.05
5.0	EQUIPMENT RENTAL (mag, VLF, radios)	600.00
6.0	ASSAYS	
	640 soil samples @ \$9.06 ea.	5,799.25
	72 rocks	968.75
	5 stream sediments	20.50
7.0	HEAVY EQUIPMENT (backhoe)	9,563.50
8.0	MISCELLANEOUS (filing fees, contract labour, etc.)	1,221.00
9.0	DRAFTING	1,053.96
10.0	OFFICE COSTS (telephone, copying, etc.)	1,229.05
11.0	<b><u>DISBURSEMENTS</u></b>	<b><u>6,021.02</u></b>
	<b>TOTAL PROJECT COSTS</b>	<b><u>\$75,844.62</u></b>



**Daiwan Engineering Ltd.**

(604) 688-1508, 1030-609 Granville Street, Vancouver, B.C. (604) 688-1508

**RECOMMENDED BUDGET**

- infill geochem/geophysics and extend grid, trenching, road building and drilling

**Geochemical Survey:**

Grid Extension & Infill Lines - say 20 km flagged grid @ \$90/km 1,800  
800 soil samples @ \$4.50/each for collection 3,600

**Geophysical Survey:**

20 km @ \$150/km - 20 man days 3,000

**Assays:**

800 soils @ \$13.50 10,800  
say 50 rocks @ \$15 750

**Transportation:**

Geochemical and Geophysical - 30 days - 1 4x4 @ \$950/month 1,900  
Geologist  
1 4x4 @ \$950/month  
gas and repairs 1,500  
mileage 600

**Food and Accommodation:**

3 men - 30 days @ \$65/day 5,850

**Wages:**

1 helper - 20 days @ \$220/day 4,400  
1 geologist - 30 days @ \$260/day 7,800

**Field Supplies**

1,000

**Office**

750

**Excavator:**

Road Building (drill sites) 10,000

Trenching - 10 days @ \$1,000/day

**Diamond Drilling:**

Mobilization/Demobilization 3,000

3000' drilling @ \$22/foot 66,000

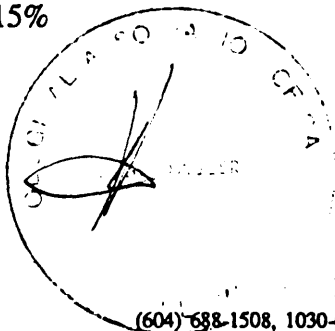
**Assay:**

say 150 samples @ \$15/sample 2,250 117,200

Contingency 15%

17,800

**TOTAL PHASE I say \$135,000**



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**PHASE II** (contingent on successful definition of Economic Grade Mineralization in Phase I)

## Drilling:

Additional 5000' @ \$22/foot	110,000
Mobilization/Demobilization	3,000

## Wages:

1 helper - 30 days @ \$220/day	6,600
1 geologist - 30 days @ \$260/day	7,800
1 P. Eng. - 5 days @ \$400/day	2,000

## Assays:

say 300 samples @ \$15	4,500
------------------------	-------

## Excavator:

(build drill sites) - 5 days @ \$1,000/day	5,000
--	-------

## Food and Accommodation:

35 man days @ \$65/day	2,275
------------------------	-------

## Transportation: (4x4)

30 days @ \$950/month	950	
gas and repairs	750	
mileage	<u>2,000</u>	143,175

Contingency 15% 21,825

Total Phase II 165,000

135,000

**TOTAL BOTH PHASES \$300,000**



Peter G. Dasler, M.Sc., F.G.A.C.  
September 10, 1990

**Daiwan Engineering Ltd.**

(604) 688-1508, 1030-609 Granville Street, Vancouver, B.C. (604) 688-1508

**CERTIFICATE OF QUALIFICATIONS**

I, Rod W. Husband, do hereby certify that:

1. I am a geologist for Daiwan Engineering Ltd. with offices at 1030 - 609 Granville Street, Vancouver, British Columbia.
2. I am a graduate from the University of British Columbia with a degree of B.Sc., Geology.
3. I have practised my profession since completion of my degree in December 1986.
4. This report is based on personal field work completed on the Win property from January 3 - February 5, and information obtained from previous reports by Professional Engineers and others who have examined the property.
5. I have no interest in the property or shares of Essex Resource Corporation or in any of the companies with claims contiguous to the Win Claim Group, nor do I expect to receive any.
6. This report, when quoted in full may be used by Essex Resource Corporation for Stock Exchange approval or for the raising of funds.



Rod W. Husband, B.Sc.

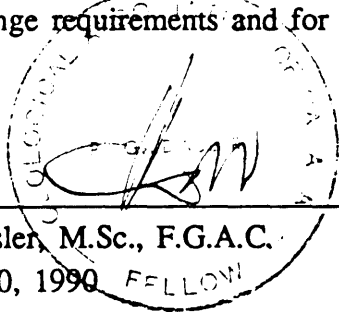
September 10, 1990

**CERTIFICATE OF QUALIFICATIONS**

I, Peter G. Dasler, do hereby certify that:

1. I am a geologist for Daiwan Engineering Ltd. with offices at 1030-609 Granville Street, Vancouver, British Columbia.
2. I am a graduate of the University of Canterbury, Christchurch, New Zealand with a degree of M.Sc., Geology.
3. I am a Fellow of the Geological Association Of Canada, a Member, in good standing, of the Australasian Institute of Mining and Metallurgy, and a Member of the Geological Society of New Zealand.
4. I have practised my profession continuously since 1975, and have held senior geological positions and managerial positions, including Mine Manager, with mining companies in Canada and New Zealand.
5. This report is based on a personal research and reports of Professional Engineers and others working in the area of the Win claims, and by my supervision of fieldwork on the property in January 1990. I visited the property for examinations on two occasions, January 4-7 1990 and May 24 1990.
6. I have no interest in the Win property or shares of Essex Resource Corporation, nor do I expect to receive any. I have a part interest in shares of Moraga Resources Ltd, which controls the Expo property to the south of the Win property.
7. This report when quoted in full may be used by Essex Resource Corporation for stock exchange requirements and for the raising of funds.

\_\_\_\_\_  
 Peter G. Dasler, M.Sc., F.G.A.C.  
 September 10, 1990



**Daiwan Engineering Ltd.**

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## **APPENDIX 1**

### **Sample Descriptions**

Win-90-01 QZ vein with crystals in cavities strike 050°N no obvious sulfides  
 Win-90-02 35cm of diorite (amphibole porphyry) trends 275 disseminated MO & PY  
 Win-90-03 grab of rubble at site of Win-90-02  
 Win-90-04 10cm QZ vein in road bed some MO greater than 1%  
 Win-90-05 1.0cm across diorite dyke in andesites mal stain, disseminated PY & CP?  
 Win-90-06 highly altered - bleached, silicified andesite mod-high fractures abundant PY  
 Win-90-07 QZ vein with hematite/limonite and trace disseminated PY  
 Win-90-08 locally derived QZ vein boulder with amethyst  
 Win-90-09 QZ veining - QZ supported breccia with host (andesitic) rock fragments  
 Win-90-10 QZ - carb vein float  
 109451 1M chip across light and dark banded recrystallized LST next to fault  
 109452 0.75 chip across fault gouge - rusty colour next to 451  
 109453 1.0m chip epidote - actinolite skarn highly silicified disseminated Py & SP next to '452  
 109454 75 cm chip across epidote - garnet skarn - highly altered & crumbly no obvious sulfides next to '453  
 109455 1.0m chip across epidote - actinolite skarn - highly siliceous disseminated Py & SP? next to 109454  
 109456 diorite - siliceous mod. fractured disseminated Py & Mo?  
 109457 30 cm of highly altered - gossanous with Mn staining siliceous seds  
 109458 highly siliceous sediments thin bedded disseminated Py.  
 109459 in trench 1 at lst-sed contact-highly fractured with rust and mn staining  
 109460 1.0m chip in highly fractured (350/90 & 040/90) thin bedded tuffs & sediments with epidote along fractures  
 109461 crystal tuff (felsite) with disseminated PY adjacent to lst and epidote-garnet skarn  
 109462 2.5m wide epidote-actinolite skarn highly siliceous QZ stringers throughout disseminated PY & SP. trench 1  
 109463 3.5m wide epidote-garnet skarn zone highly bleached  
 109464 float on road by lst pit - epidote - actinolite skarn disseminated py.cp sp with minor mal staining  
 109465 QZ vein float boulder - locally derived disseminated up to 1%  
 109466 as 109466  
 109467 50cm wide epidote - actinolite skarn in trench 1 at upper contact of lst w/ Parson Bay seds disseminated py, sp.  
 109468 highly altered contact zone of lst with Parson Bay - fault contact  
 109469 80cm across semi massive sulphide vein PY, SP cp? ga? abundant. 050/70 SE  
 109470 40cm chip of weathered rusty, mn stained portion of vein mal, cp PY adjacent to 109469  
 109471 30cm chip across upper section of vein galena? SP highly siliceous  
 109472 30cm epidote - garnet skarn on footwall of sulphide vein in diorite

- 109473 as 109471
- 109474 40 cm across semi massive sulphide vein 20 - 30% PY 010/52 E west wall offset from 109469
- 109475 45cm across semi massive sulphide portion of vein zone PY SP
- 109476 75cm chip in diorite with up to 1% dissem PY trace mo & cp
- 109477 old trench 4 - 30cm chip across epidote - actinolite skarn below mg PY SP ga highly siliceous
- 109478 1.4 m across massive magnetite bed above 109477 som PY & SP
- 109479 lower road 30 cm in karmutsen basalt andesite blocky fractures minor rust dissem PY to 1%
- 109480 35cm chip in highly fractured, kaolinized rusted volcanic?
- 109481 siliceous diorite med grained abundant dissem PY to 2%
- 109482 2.5m chip across dioritic sill in 1st - fault contact on both hanging & footwall dissem PY to 1%
- 109483 70cm chip at footwall of sill highly fractured, rusty
- 109484 60cm chip at hanging wall of sill highly fractured rusty
- 109485 45cm chip in highly siliceous thin bedded seds w/ PY & SP dissem and on fracture surfaces
- 109486 1.0m chip of highly rusted - gossanous zone in siliceous seds abundant PY
- 109487 1.2m chip at footwall of fault (345/80 SW) dissem PY in seds
- 109488 1.0m chip in mod siliceous seds dissem PY & SP & on bedding planes
- 109489 1.0m across highly fractured/rusted & mn stained siliceous sediments near fault
- 109490 trench 2 1m wide epidote-garnet skarn bleached crumbly 060/45° NW
- 109491 trench 2 1.0m chip of 2.5m wide siliceous Mn-gossanous skarn PY & SP with yellow oxide
- 109492 trench 2 1.5m chip as above next to 109491
- 109493 trench 2 - 1.5m chip actinolite-garnet-epidote skarn abundant PY, SP with yellow oxide? highly siliceous
- 109494 as previous 4 meters along trench 1m chip
- 109495 pit on south road 1.0m chip across heavily rusted abundant PY to 20% adjacent to fault 055/80° NW
- 109496 LST pit on main road 1.0m chip of QZ - feld crystal tuff, dissem PY & PY on fractures (calcite) 0/8/70°-90° W
- 10949 ST pit on main road 2.0m chip across crystal tuff - rusted w/abundant Py
- 109498 line 19+50E 4+25N karmutsen andesite - basalt aphanitic dark green abundant magnetite disseminated minor ed along fractures
- 109499 1m chip in highly fractured (350/65° W) karmutsen basalt with abundant hairline stringers. No obvious sulfides
- 109500 40cm in bleached volcanic adjacent to fault 350/65° W K-spar alter of stringers

- 109952 75m chip in med grained pink granodiorite moderately fractured 044/90 minor PY k\spar alteration along fractures
- 109953 2m chip across dioritic dyke in granodiorite 275/52° N
- 109954 6m wide dark green dioritic dyke 260/75° SE gossanous QZ - feld phenos in parts in black groundmass
- 109955 40cm in karmutsen basalt - aphinitic mod. fractures - clay stringers magnetite dissem throughout
- 109956 20+90E 4185N andesite - basalt with abundant dissem magnetite
- 109957 diorite with mod. fractures minor clay alteration along fractures; disseminated Py
- 109958 highly siliceous volcanic andesite? at contact with diorite disseminated magnetite and pyrite quartz stringers
- 109959 highly siliceous volcanic; disseminated pyrite quartz stringers
- 109961 diorite - fresh - disseminated magnetite to 1%
- 109963 highly siliceous volcanic abundant pyrite (to 20%) disseminated and along fractures
- 109965 15 cm quartz pyrite stringer zone in siliceous volcanics
- 109966 highly siliceous volcanic abundant pyrite
- 109967 10 cm quartz-pyrite stringer zone 060/80° SE at base of cliff
- 109951 silt sample
- 109960 pan sample - sediment panned down to ~2 tablespoon size; very few heavies; total sample 4 pans
- 109962 pan sample - sediment panned down to ~2 tablespoon size; magnetite 2-3%
- 109963 pan sample - 3 pans taken down to ~2 tablespoon size; minor heavies

**APPENDIX 2**

**Assay Certificates**

**and**

**Statistical Analysis**

STATISTICALLY ANOMALOUS SOIL GEOCHEMISTRY VALUES

NORTHERN VANCOUVER ISLAND AREA

(ASSESSMENT REPORT #2190)

---

Geology	Metal	Background				Anomalous		
		Population				Population		
		x	x-2s	x-s	x	x+s	x+2s	
Karmutsen Volcanics	Cu	14.5	68	112	189	318	522	
	Mo	-	-	-	.11	0.8	5.6	
	Zn	15.1	42	74	136	250	450	
Quatsino Limestone	Cu	18.5	109	155	220	315	445	
	Mo	-	-	-	1.3	5.0	19.5	
	Zn	24	90	140	220	345	535	
Bonanza Volcanics	Cu	7.4	25	35	48	69	96	
	Mo	0.23	3.3	4.8	7.15	10.5	15.5	
	Zn	13.8	44	61	85.5	120	165	
Altered Rocks	Cu	7.6	36	50	70	98	137	
	Mo	0.22	3.35	5.9	10.4	18.7	33	
	Zn	5.7	16.2	24.3	37	56	84	
Intrusives	Cu	9.0	31	40	52	68	87	
	Mo	0.24	3.7	6.2	10.5	17.8	30	
	Zn	-	-	-	24	43	71	

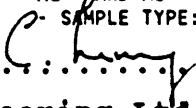
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ACME ANALYTICAL LABORATORIES LTD.  
S52 E. HASTINGS ST. VANCOUVER B.C. V6A 1R5  
PHONE(604)253-3158 FAX(604)253-1716

DATE RECEIVED: FEB 6 1990  
DATE REPORT MAILED: Feb. 12/90..

### ASSAY CERTIFICATE

AG\*\* AND AU\*\* BY FIRE ASSAY FROM 1/2 A.T.  
SAMPLE TYPE: ROCK PULP

SIGNED BY:  D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS  
Daiwan Engineering Ltd. PROJECT WIN FILE # 90-0207R

SAMPLE#	Cu %	Pb %	Zn %	Ag** OZ/T	Au** OZ/T
C 109453	.01	.01	2.37	.09	.001
C 109455	.01	.01	2.14	.02	.001
C 109467	.02	.01	1.87	.08	.001
C 109468	.01	.03	4.07	.17	.002
C 109469	.98	.06	14.31	.39	.002
C 109470	1.52	.26	10.44	.80	.010
C 109471	.02	1.31	1.94	.17	.006
C 109472	.20	.02	5.27	.06	.010
C 109473	.21	.59	13.33	.27	.002
C 109474	1.17	.01	20.85	.63	.011
C 109477	.05	.01	2.29	.10	.033

ACME ANALYTICAL LABORATORIES LTD.  
352 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6  
PHONE (604) 253-3158 FAX (604) 253-1716

DATE RECEIVED: FEB 6 1990

DATE REPORT MAILED: Feb. 12/90.

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AG\*\* AND AU\*\* BY FIRE ASSAY FROM 1/2 A.T.  
SAMPLE TYPE: ROCK PULP

SIGNED BY *C. King* D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS  
Daiwan Engineering Ltd. PROJECT WIN FILE # 90-0245R

SAMPLE#	Cu %	Pb %	Zn %	Ag** OZ/T	Au** OZ/T
C 109493	.22	.01	8.59	.28	.003
C 109494	.04	.01	3.60	.08	.058 *
C 109495	.31	.01	.07	.88	.011

\* Subject to reassay check



ACME ANALYTICAL LABORATORIES LTD.

DATE RECEIVED: FEB 14 1990

352 E. HASTINGS ST. VANCOUVER B.C. V6A 1R5

PHONE(604)253-3158 FAX(604)253-1716 DATE REPORT MAILED:

Feb. 13/90..

### GEOCHEMICAL ANALYSIS CERTIFICATE

- SAMPLE TYPE: P1 SILT PULP P2 ROCK PULP  
AU\* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

SIGNED BY... D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

Daiwan Engineering Ltd. PROJECT WIN FILE # 90-0321R Page 1

SAMPLE#	AU* ppb
C 109960	2
C 109962	3
C 109963	2
C 109966	8
C 109969	1

SAMPLE#	AU* ppb
C 109952	1
C 109953	1
C 109954	3
C 109955	5
C 109956	6
C 109957	7
C 109958	1
C 109959	3
C 109961	3
C 109964	2
C 109965	2
C 109967	8
C 109968	1

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.  
 - SAMPLE TYPE: P1 SILT P2 ROCK

DATE RECEIVED: FEB 7 1990 DATE REPORT MAILED: Feb 9/90. SIGNED BY: *C. Long* D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

Daiwan Engineering Ltd. PROJECT WIN File #, 90-0321 Page 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM
C 109960	2	37	18	208	12	19	10	491	2.56	9	5	ND	1	59	2	2	2	90	2.24	.033	4	24	.66	27	.22	2	1.63	.02	.02	1
C 109962	6	107	18	88	1	34	18	528	5.19	13	5	ND	1	94	1	2	2	98	.89	.053	4	49	1.54	45	.16	4	2.66	.03	.05	1
C 109963	3	38	28	201	7	18	12	691	3.96	12	5	ND	1	75	2	2	3	100	2.65	.030	4	25	.65	25	.19	5	1.68	.02	.02	1
C 109966	7	126	12	88	1	65	41	494	11.37	8	5	ND	1	73	1	2	2	130	.69	.052	4	46	1.26	33	.15	3	2.24	.02	.04	1
C 109969	7	37	9	263	3	51	19	2270	4.24	15	5	ND	1	44	5	2	2	102	.92	.094	6	24	.45	172	.01	3	1.91	.01	.05	1

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM
C 109952	2	29	7	28	.1	3	3	105	1.34	4	5	ND	3	91	1	2	2	27	2.73	.020	8	5	.27	24	.07	2	3.52	.02	.05	1
C 109953	1	17	52	89	.2	5	4	449	.80	3	5	ND	2	155	1	2	2	10	3.28	.011	3	4	.31	22	.05	2	4.31	.01	.05	1
C 109954	1	58	9	79	.1	11	14	650	3.03	3	5	ND	1	91	1	2	2	50	1.38	.033	4	6	1.46	24	.16	2	3.15	.01	.04	1
C 109955	1	62	9	21	.2	23	12	244	4.02	4	5	ND	1	108	1	2	2	125	2.51	.039	3	31	.65	14	.28	3	3.23	.40	.03	1
C 109956	1	638	13	47	.4	28	18	368	6.79	4	5	ND	1	43	1	2	2	162	2.27	.068	2	37	.73	22	.35	5	2.13	.15	.07	1
C 109957	43	277	7	47	.2	9	19	242	4.02	15	5	ND	3	34	1	2	2	46	.91	.037	6	5	.94	47	.08	2	2.02	.02	.06	1
C 109958	4	222	23	107	.4	58	14	545	4.69	4	5	ND	1	72	1	2	3	89	1.76	.068	6	210	1.89	51	.12	3	3.63	.08	.08	1
C 109959	44	281	11	26	.1	23	21	190	5.11	10	5	ND	1	27	1	2	2	217	.41	.023	3	189	2.11	42	.27	3	2.61	.02	.17	1
C 109961	1	60	6	33	.2	8	12	213	3.94	5	5	ND	1	136	1	2	2	139	2.08	.077	3	12	.70	134	.10	8	2.40	.14	.07	1
C 109964	1	20	24	38	.1	70	52	163	12.47	5	5	ND	1	114	1	2	2	23	2.33	.097	3	21	.31	15	.03	8	3.49	.41	.05	1
C 109965	1	29	226	187	.4	13	6	308	.86	2	5	ND	1	113	4	2	4	22	18.23	.010	2	25	.42	12	.04	2	5.64	.01	.03	1
C 109967	1	46	9	37	.1	47	23	323	4.65	3	5	ND	1	116	1	2	2	125	5.43	.070	4	87	2.35	27	.16	2	7.88	.02	.06	1
C 109968	5	42	10	15	.1	11	11	192	5.64	8	5	ND	2	78	1	2	2	78	1.47	.051	5	13	.89	87	.10	4	3.24	.03	.19	1
STD C	19	59	43	134	6.9	68	31	1013	3.90	42	22	7	38	48	19	16	17	59	.45	.099	38	53	.90	176	.07	40	1.92	.06	.13	12

**GEOCHEMICAL ANALYSIS CERTIFICATE**

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM. - SAMPLE TYPE: P1-P8 SOIL P9-ROCK P - PULVERIZED AU\* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

DATE RECEIVED: JAN 29 1990 DATE REPORT MAILED: *Feb 2/90* SIGNED BY: *[Signature]* D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

Daiwan Engineering Ltd. PROJECT WIN File # 90-0245 Page 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe X	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca X	P X	La PPM	Cr PPM	Mg X	Ba PPM	Ti X	B PPM	Al X	Na X	K X	W PPM	Au* PPM
L4+50E 14+25N P	2	84	30	77	.8	12	51	640	8.70	4	5	ND	1	17	1	3	2	116	.22	.037	4	51	.26	24	.18	7	3.78	.01	.04	2	5
L4+50E 14+00N P	1	63	14	63	.5	25	106	3615	8.75	5	5	ND	1	19	1	2	2	137	.30	.025	3	54	.56	28	.22	4	2.54	.01	.02	1	2
L4+50E 13+75N P	1	289	17	112	.6	70	37	346	8.03	12	5	ND	1	44	2	3	2	152	.87	.032	2	82	.86	70	.30	4	6.26	.02	.04	1	3
L4+50E 13+50N P	1	89	18	80	.5	34	32	1101	7.20	4	5	ND	1	27	2	3	2	130	.41	.027	3	55	.76	29	.24	6	3.26	.02	.03	1	6
L4+50E 13+25N P	1	59	18	53	.4	20	8	224	7.20	9	5	ND	1	23	1	2	7	146	.37	.020	2	46	.45	20	.26	8	2.11	.01	.02	3	3
L4+50E 13+00N P	3	35	46	373	.7	18	25	1775	4.94	19	5	ND	1	45	3	5	2	97	1.31	.033	5	30	.53	77	.08	5	3.09	.01	.03	1	3
L4+50E 12+75N P	4	30	35	95	.5	9	5	249	8.84	11	5	ND	1	18	1	5	3	153	.36	.020	2	38	.20	25	.19	6	3.63	.01	.02	1	2
L4+50E 12+50N P	1	5	2	93	.1	4	1	57	.25	2	5	ND	1	27	1	2	2	8	1.45	.046	2	7	.06	9	.01	8	.15	.01	.03	1	7
L4+50E 12+25N P	1	44	40	95	.3	23	5	332	4.77	5	5	ND	1	26	1	2	6	124	.64	.025	3	61	.54	23	.21	3	3.78	.01	.02	2	6
L4+50E 12+00N P	1	100	21	100	.3	24	15	585	3.81	10	5	ND	1	43	2	3	2	89	.71	.051	5	34	.61	71	.14	2	2.61	.02	.03	1	7
L7+50E 11+00N P	2	52	25	62	.4	11	9	334	7.75	5	5	ND	1	20	1	4	2	109	.33	.018	4	32	.29	17	.11	2	2.37	.01	.02	1	5
L7+50E 10+75N P	3	31	27	101	.7	3	2	53	8.01	4	5	ND	1	9	1	2	2	86	.10	.056	4	17	.04	16	.04	5	1.12	.01	.03	1	3
L7+50E 10+50N P	1	5	11	29	.1	2	1	93	.71	2	5	ND	1	15	1	2	2	16	.15	.012	3	6	.09	21	.04	5	.60	.02	.06	1	8
L7+50E 10+25N P	2	18	13	57	.1	7	5	179	3.12	10	5	ND	2	21	1	2	2	77	.33	.025	4	15	.25	23	.11	3	1.91	.01	.04	1	1
L7+50E 10+00N P	1	25	30	56	.3	8	5	224	5.98	69	5	ND	1	16	1	2	2	123	.45	.025	2	19	.33	21	.15	4	1.84	.01	.01	1	1
L7+50E 9+75N P	1	27	16	110	.1	12	12	485	5.63	8	5	ND	1	19	1	2	2	96	.26	.028	4	23	1.05	18	.01	4	4.72	.01	.03	2	1
L7+50E 9+50N P	1	12	14	114	.3	6	3	205	2.24	98	5	ND	1	45	1	2	5	46	2.96	.040	2	8	.17	11	.06	7	1.11	.01	.03	1	2
L7+50E 9+25N P	1	23	39	118	.1	14	6	302	5.96	147	5	ND	1	21	2	6	4	113	.46	.019	2	17	.09	25	.12	3	1.35	.01	.02	1	2
L7+50E 9+00N P	1	37	43	114	.4	12	5	254	4.27	13	5	ND	1	20	2	4	2	121	.41	.021	4	25	.33	36	.16	2	3.70	.01	.02	1	9
L7+50E 8+75N P	1	26	22	142	.5	8	4	232	1.66	7	5	ND	1	28	1	2	2	57	.46	.044	2	13	.21	27	.09	6	1.45	.02	.03	1	1
L7+50E 8+50N P	1	8	30	157	.2	5	1	150	1.50	4	5	ND	1	20	1	2	2	40	.34	.020	4	10	.13	27	.04	2	1.26	.01	.03	2	3
L7+50E 8+25N P	1	50	127	244	.2	20	5	374	4.72	23	5	ND	3	24	2	4	2	102	.61	.035	6	37	.40	41	.12	5	6.56	.01	.02	1	7
L7+50E 8+00N P	1	22	46	224	.3	13	6	392	3.72	11	5	ND	1	46	2	3	2	120	.99	.026	4	29	.38	35	.13	2	3.38	.01	.02	1	6
L7+50E 7+75N P	7	22	35	255	1.2	6	21	6354	16.73	9	5	ND	1	72	3	4	2	82	1.63	.129	3	20	.15	133	.03	8	1.59	.01	.03	1	4
L7+50E 7+50N P	1	9	8	182	.3	4	1	931	.49	2	5	ND	1	27	1	2	2	17	.88	.071	2	5	.07	18	.03	7	.37	.01	.04	1	2
L7+50E 7+25N P	2	27	39	122	.6	16	4	548	3.64	10	5	ND	1	26	2	2	2	123	.52	.043	3	30	.37	26	.16	2	1.64	.01	.02	1	3
L7+50E 7+00N P	1	5	16	52	.3	4	1	107	.76	6	5	ND	1	22	1	3	2	59	.15	.034	3	5	.07	30	.09	5	1.17	.01	.02	1	3
L7+50E 6+75N P	1	10	12	137	1.0	4	1	512	.53	2	5	ND	1	31	1	2	2	29	.57	.088	2	5	.04	20	.03	5	.33	.01	.05	1	1
L7+50E 6+50N P	2	43	22	129	.7	20	7	629	4.05	18	5	ND	1	25	1	2	2	150	.48	.037	4	35	.49	27	.14	4	2.23	.01	.02	1	4
L7+50E 6+25N P	2	20	27	101	.8	10	4	356	4.49	14	5	ND	1	20	1	2	3	169	.42	.020	3	27	.24	15	.20	2	1.45	.01	.02	1	3
L7+50E 6+00N P	4	35	41	78	.5	9	6	801	8.26	29	5	ND	1	16	1	4	2	320	.50	.033	3	30	.06	12	.25	3	1.06	.01	.01	1	2
L7+50E 5+75N P	4	8	19	57	1.2	8	2	308	2.03	14	5	ND	1	20	1	3	2	177	.37	.046	3	15	.06	10	.12	3	.46	.01	.02	1	6
L7+50E 5+50N P	3	17	24	116	1.0	8	2	366	1.78	13	5	ND	1	27	1	2	4	97	.37	.070	3	12	.07	28	.10	3	.91	.01	.03	2	5
L13+50E 6+50N P	1	67	98	149	.1	18	6	293	5.01	13	5	ND	1	18	1	3	3	114	.27	.027	3	46	.48	27	.16	2	4.71	.01	.02	1	7
L13+50E 6+25N P	2	13	305	70	.2	4	1	52	.39	3	5	ND	1	18	1	2	4	50	.19	.020	4	29	.04	21	.14	2	1.25	.01	.02	1	3
L13+50E 6+00N P	1	9	17	117	.2	3	1	230	.37	2	5	ND	1	25	1	2	2	13	.08	.042	2	8	.20	17	.03	5	.43	.03	.05	1	2
STD C/AU-S	18	57	43	128	6.8	68	29	926	4.07	38	20	7	36	47	18	15	18	56	.44	.091	36	56	.80	174	.06	39	1.91	.06	.14	13	47

Daiwan Engineering Ltd. / JECT WIN FILE # 90-0245

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L13+5OE 5+75N P	1	20	13	63	.4	7	1	115	.59	2	5	ND	1	16	1	2	3	44	.31	.066	2	28	.13	27	.08	5	1.24	.01	.02	2	1
L13+5OE 5+50N P	2	13	24	32	.1	5	2	115	2.05	7	5	ND	1	17	1	2	2	135	.32	.016	3	18	.15	16	.15	3	.92	.01	.02	2	6
L13+5OE 5+25N P	1	24	19	110	.6	7	1	15	.29	2	5	ND	1	8	1	2	2	24	.07	.127	2	22	.02	24	.03	4	1.26	.01	.01	1	2
L13+5OE 5+00N P	1	15	18	117	1.0	3	1	19	.60	2	5	ND	1	9	1	2	2	30	.10	.116	2	14	.03	21	.04	4	.79	.01	.02	1	5
L13+5OE 4+75N P	1	13	16	71	.3	2	1	10	.42	2	5	ND	1	2	1	2	2	38	.03	.058	2	6	.01	9	.02	2	.47	.01	.01	1	1
L13+5OE 4+50N P	2	14	23	50	.3	12	5	112	7.23	4	5	ND	1	10	1	4	5	231	.19	.012	2	32	.19	11	.32	3	.88	.01	.02	1	1
L13+5OE 4+25N P	1	10	14	71	.5	3	1	13	.27	2	5	ND	1	9	1	2	2	44	.09	.066	2	16	.02	17	.08	4	.85	.01	.01	1	3
L13+5OE 4+00N P	1	5	2	83	.1	3	1	25	2.89	2	5	ND	1	5	1	2	2	23	.06	.104	2	2	.02	13	.01	5	.40	.01	.04	1	4
L13+5OE 3+75N P	1	10	8	145	.2	3	1	26	1.93	2	5	ND	1	13	1	2	3	32	.25	.082	2	4	.02	21	.01	7	.41	.01	.02	1	1
L13+5OE 3+50N P	1	12	8	132	.3	2	1	40	.60	2	5	ND	1	20	1	2	2	37	.30	.076	2	2	.04	43	.01	4	.61	.02	.04	1	1
L13+5OE 3+25N P	5	44	30	184	.8	16	8	478	1.50	4	5	ND	1	56	2	2	2	74	.84	.071	4	32	.88	83	.09	4	2.33	.01	.05	1	4
L13+5OE 3+00N P	4	38	97	271	.3	29	8	436	1.64	8	5	ND	1	31	1	2	2	85	.78	.040	3	39	.65	152	.11	3	2.45	.01	.02	1	1
L13+5OE 2+50N P	5	9	18	30	.1	6	1	119	2.49	3	5	ND	1	15	1	2	2	112	.19	.010	3	18	.19	35	.16	2	1.14	.01	.02	1	6
L13+5OE 2+25N P	3	54	18	97	.2	21	5	310	3.38	8	5	ND	1	24	1	2	2	98	.39	.033	4	43	.68	32	.13	2	3.49	.01	.02	1	5
L13+5OE 2+00N P	4	65	17	91	.5	19	6	277	4.06	10	5	ND	1	20	1	3	3	90	.27	.054	6	53	.55	33	.15	2	7.13	.01	.02	1	3
L13+5OE 1+75N P	3	55	6	130	.2	20	13	617	3.32	15	5	ND	1	35	1	2	2	72	.56	.071	7	28	.76	47	.10	2	3.07	.01	.03	1	3
L13+5OE 1+50N P	3	39	18	101	.3	11	5	293	3.70	10	5	ND	1	21	1	2	2	89	.27	.040	5	21	.47	33	.14	2	2.92	.01	.02	1	9
L13+5OE 1+25N P	2	34	19	97	.4	10	6	334	5.06	9	5	ND	1	26	1	4	4	124	.32	.041	4	24	.44	33	.19	4	2.62	.01	.02	1	2
L13+5OE 1+00N P	2	48	26	106	.5	11	7	524	3.88	7	5	ND	1	23	1	3	2	88	.30	.038	4	23	.48	30	.14	5	3.11	.01	.02	1	1
L13+5OE 0+75N P	2	54	28	136	.4	19	6	345	4.43	16	5	ND	1	28	1	3	2	104	.41	.039	6	35	.63	33	.15	2	3.96	.01	.02	1	1
L13+5OE 0+50N P	3	121	31	139	.6	69	17	384	4.92	11	5	ND	1	30	1	5	2	97	.29	.059	4	111	1.24	66	.12	3	5.41	.01	.02	1	1
L13+5OE 0+25N P	5	91	13	85	.5	4	6	273	3.86	15	5	ND	1	31	1	2	2	63	.36	.078	7	10	.31	48	.10	2	3.52	.01	.02	1	3
L13+5OE 0+00N P	5	85	22	108	2.8	9	7	254	5.94	5	5	ND	1	30	1	3	2	116	.22	.065	6	18	.34	48	.11	3	3.82	.01	.02	1	8
L15+0OE 5+00N P	3	13	7	26	.3	6	4	79	2.28	4	5	ND	1	13	1	2	2	148	.19	.014	2	10	.06	14	.13	3	.53	.01	.01	1	1
L15+0OE 4+75N P	2	12	15	77	.7	4	2	91	2.01	7	5	ND	1	21	1	2	2	126	.28	.024	2	12	.14	18	.16	4	.59	.01	.04	1	1
L15+0OE 4+50N P	2	16	15	33	.2	5	4	131	3.20	5	5	ND	1	39	1	2	4	205	.29	.011	3	12	.28	15	.27	2	.91	.01	.01	1	4
L15+0OE 4+25N P	1	10	8	97	.5	2	1	23	.21	2	5	ND	1	22	1	2	2	14	.30	.066	2	6	.04	44	.03	7	.44	.01	.03	1	2
L15+0OE 4+00N P	1	4	8	91	.3	2	2	13	.34	2	5	ND	1	13	1	2	2	10	.23	.041	2	5	.02	26	.02	4	.34	.01	.01	1	2
L15+0OE 3+75N P	1	3	6	130	.1	2	1	16	.16	2	5	ND	1	25	1	2	2	5	.27	.045	2	2	.04	48	.01	3	.16	.01	.01	1	2
L15+0OE 3+50N P	1	4	5	69	.1	1	1	12	.04	2	5	ND	1	37	1	2	2	2	.45	.038	2	3	.11	23	.01	4	.06	.01	.03	1	2
L15+0OE 3+25N P	1	6	4	125	.3	2	1	20	.14	2	5	ND	1	34	1	2	2	6	.67	.047	2	3	.07	47	.01	5	.37	.01	.02	1	2
L15+0OE 3+00N P	3	18	8	115	.7	4	1	23	.41	2	5	ND	1	20	1	2	2	25	.59	.094	2	15	.03	32	.02	2	.79	.01	.02	1	1
L15+0OE 2+75N P	1	10	13	54	.2	9	2	194	.79	2	5	ND	1	25	1	2	2	44	.44	.015	2	25	.39	24	.13	2	1.23	.01	.02	1	1
L15+0OE 2+50N P	3	7	30	88	.3	5	1	54	.49	2	5	ND	1	19	1	2	3	35	.22	.045	3	17	.06	30	.07	4	1.12	.01	.02	1	5
L15+0OE 2+25N P	1	7	7	83	.4	3	1	28	.53	2	5	ND	1	9	1	2	2	19	.14	.140	2	11	.03	20	.02	4	.89	.01	.03	1	4
L15+0OE 2+00N P	4	7	28	77	.3	5	1	50	.44	2	5	ND	1	17	1	2	2	43	.18	.035	3	16	.05	30	.06	3	1.27	.01	.02	1	13
STD C/AU-S	18	57	37	127	6.8	68	29	933	3.94	44	19	8	36	47	18	16	18	56	.46	.098	36	55	.81	173	.06	38	1.86	.06	.14	12	51

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SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L15+00E 1+75N P	3	10	14	40	.1	5	1	97	.57	2	5	ND	1	23	1	2	2	41	.39	.012	3	12	.14	32	.08	2	1.00	.01	.02	2	9
L15+00E 1+50N P	5	13	16	64	.2	9	3	277	1.23	3	5	ND	1	28	1	2	2	68	.53	.015	3	21	.44	27	.13	2	1.35	.02	.02	1	11
L15+00E 1+25N P	1	7	6	109	.2	1	1	41	.07	2	5	ND	1	44	1	2	2	3	.44	.046	2	5	.10	28	.01	4	.11	.02	.04	1	4
L15+00E 1+00N P	4	31	30	65	.3	8	4	208	6.34	7	5	ND	1	21	2	2	2	153	.23	.023	3	31	.92	20	.21	2	2.11	.01	.01	1	2
L15+00E 0+75N P	7	11	19	79	.1	4	3	129	2.16	7	5	ND	1	18	1	2	2	123	.30	.012	3	14	.10	14	.12	3	.71	.01	.01	1	1
L15+00E 0+50N P	2	13	10	208	.4	5	2	135	.69	2	5	ND	1	68	2	2	2	18	3.08	.063	2	6	.16	78	.02	12	.59	.01	.05	1	2
L15+00E 0+25N P	1	40	24	330	.9	38	15	304	1.61	3	5	ND	1	47	1	3	2	52	1.76	.085	6	34	.76	62	.08	3	3.53	.01	.02	1	3
L15+00E 0+00N P	1	9	2	151	.6	2	1	1635	.19	2	5	ND	1	21	1	2	2	7	.83	.068	2	4	.06	26	.01	6	.14	.01	.04	1	1
L15+00E 0+25S P	5	10	12	89	.2	5	7	949	4.24	7	5	ND	1	56	1	2	2	134	.56	.029	3	11	.93	36	.14	2	1.76	.01	.02	1	2
L15+00E 0+50S P	4	12	15	76	.4	4	3	266	2.46	4	5	ND	1	46	2	3	2	95	.62	.027	3	11	.28	43	.14	3	1.18	.01	.03	1	1
L15+00E 0+75S P	2	9	5	88	.4	3	1	159	.34	2	5	ND	1	37	1	2	2	12	.71	.063	2	5	.15	48	.02	6	.26	.01	.05	1	1
L15+00E 1+25S P	9	24	10	109	.2	17	14	1356	4.14	7	5	ND	1	33	2	2	2	81	.79	.033	3	19	.56	36	.12	2	1.44	.02	.03	1	1
L15+00E 1+50S P	3	25	20	97	.4	9	4	245	4.00	6	5	ND	1	25	1	2	5	108	.45	.034	4	23	.43	31	.13	2	2.92	.01	.02	2	5
L15+00E 1+75S P	2	31	18	78	.4	9	7	271	3.85	5	5	ND	1	26	1	2	2	90	.23	.034	3	20	.39	55	.13	2	6.34	.01	.02	1	2
L15+00E 2+00S P	1	19	10	221	.3	5	3	901	1.86	5	5	ND	1	25	1	2	2	50	.81	.076	2	9	.34	35	.07	4	1.09	.02	.06	1	1
L15+00E 2+25S P	5	15	26	157	.4	7	15	1392	3.44	13	5	ND	1	33	2	2	3	87	1.25	.036	4	18	.22	45	.11	2	1.31	.01	.03	1	3
L15+00E 2+50S P	3	15	10	68	.3	4	2	100	2.03	5	5	ND	1	21	1	2	3	114	.40	.035	3	7	.10	26	.18	4	.65	.01	.03	1	1
L15+00E 2+75S P	3	10	10	130	.7	5	17	2507	1.23	6	5	ND	1	42	2	2	2	48	.81	.049	3	9	.13	76	.07	7	.65	.02	.05	1	1
L15+00E 3+00S P	12	19	31	315	1.3	18	12	1327	4.05	26	5	ND	1	35	3	2	3	145	1.00	.052	5	50	.30	55	.09	4	2.19	.01	.03	1	3
L15+00E 3+25S P	6	23	24	201	.4	14	11	1452	2.64	8	5	ND	1	37	3	2	2	87	.98	.044	4	28	.52	47	.09	3	1.83	.02	.03	1	1
L15+00E 3+50S P	11	21	23	256	1.1	12	9	1283	2.42	11	5	ND	1	39	4	2	2	105	1.26	.064	7	49	.24	54	.08	4	2.49	.01	.04	1	3
L15+00E 3+75S P	4	47	18	242	1.3	31	10	612	3.85	21	5	ND	1	49	1	2	2	104	1.19	.126	5	28	.27	94	.10	2	2.18	.02	.02	1	2
L15+50E 2+75N P	7	12	37	78	.3	13	2	180	.64	2	5	ND	1	27	1	2	3	75	.87	.021	3	29	.13	70	.13	2	1.31	.01	.02	1	2
L16+50E 3+00N P	2	15	23	64	.4	3	1	41	.89	2	5	ND	1	13	1	2	3	46	.15	.052	4	15	.04	24	.08	2	.94	.01	.03	1	8
L16+50E 4+75N P	2	32	26	98	.9	5	2	91	8.72	3	5	ND	1	18	1	2	6	99	.20	.048	3	24	.08	23	.13	4	1.09	.01	.04	1	4
L16+50E 4+50N P	1	37	16	144	.8	5	12	239	4.71	2	5	ND	1	26	1	2	2	38	.97	.117	7	11	.05	21	.02	6	1.38	.01	.03	1	2
L16+50E 4+25N P	1	52	12	106	.6	9	5	735	1.52	2	5	ND	1	75	2	3	2	17	4.24	.085	4	15	.09	27	.02	11	1.35	.01	.02	1	3
L16+50E 4+00N P	3	92	21	137	.8	21	12	3853	4.60	9	5	ND	1	54	2	3	2	77	2.12	.058	5	39	.35	53	.11	7	3.25	.01	.03	1	6
L16+50E 3+75N P	3	18	25	58	.2	3	3	250	1.28	4	5	ND	1	38	1	2	3	83	1.33	.022	5	19	.08	32	.12	2	1.02	.01	.02	1	13
L16+50E 3+50N P	3	55	22	99	.6	6	1	87	5.88	54	5	ND	1	12	1	2	2	109	.15	.105	4	15	.05	22	.02	2	1.45	.01	.03	1	3
L16+50E 3+00N P	3	24	20	61	.1	8	3	171	4.48	29	5	ND	1	24	1	2	2	128	.35	.020	3	23	.30	30	.13	2	1.42	.01	.02	1	5
L16+50E 2+75N P	4	5	19	80	.1	2	1	57	.44	2	5	ND	1	21	1	2	2	46	.26	.013	4	10	.05	19	.08	3	.61	.01	.03	1	13
L16+50E 2+25N P	1	53	18	166	.4	11	8	542	2.45	55	5	ND	1	138	2	4	2	43	18.74	.039	3	17	.26	25	.07	2	1.77	.01	.02	1	7
L16+50E 1+75N P	5	29	20	95	.3	11	6	253	5.41	7	5	ND	1	22	2	4	2	131	.52	.031	3	41	.48	26	.17	2	3.36	.01	.02	1	4
L16+50E 1+50N P	4	42	6	72	.4	23	6	312	4.05	7	5	ND	1	28	1	4	2	121	.67	.029	2	52	.84	32	.14	2	1.48	.02	.02	1	1
L16+50E 1+25N P	6	25	11	40	.2	7	5	126	4.12	8	5	ND	1	14	1	3	5	224	.39	.014	2	17	.08	12	.17	4	.63	.01	.01	1	4
STD C/AU-S	18	58	39	129	7.0	68	31	1009	4.05	42	17	8	36	48	19	16	19	58	.46	.092	37	55	.81	174	.07	38	1.93	.06	.14	12	53

Daiwan Engineering Ltd. I JECT WIN FILE # 90-0245

age 4

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L16+50E 1+00N P	1	19	2	66	.3	4	1	30	1.58	2	5	ND	1	9	1	2	2	24	.10	.049	2	6	.03	14	.05	2	.70	.01	.02	1	1
L16+50E 0+75N P	2	30	18	80	.3	8	3	114	2.95	2	5	ND	1	22	1	3	3	93	.21	.035	3	17	.21	27	.16	5	1.34	.02	.05	1	2
L16+50E 0+50N P	1	32	10	133	.3	4	1	43	6.03	2	5	ND	1	9	1	2	3	56	.09	.057	2	10	.04	15	.05	6	.96	.01	.03	1	1
L16+50E 0+25N P	1	25	4	130	.2	5	2	66	4.95	2	5	ND	1	9	1	2	2	40	.08	.059	2	5	.04	14	.03	2	.71	.02	.04	1	1
L16+50E 0+00N P	5	15	7	28	.3	4	3	112	2.76	5	5	ND	1	19	1	2	5	145	.39	.016	2	9	.12	19	.17	2	.65	.01	.02	1	1
L16+50E 0+25S P	4	16	14	79	.4	7	2	140	1.53	2	5	ND	1	25	1	2	4	50	.39	.037	3	16	.27	25	.08	3	.99	.01	.02	2	32
L16+50E 0+50S P	2	21	9	110	.2	11	3	120	.39	5	5	ND	1	38	1	3	2	15	1.30	.073	4	15	.09	52	.02	8	2.92	.01	.02	1	1
L16+50E 0+75S P	8	28	13	171	.5	14	31	1394	3.00	9	5	ND	1	35	2	2	2	70	1.02	.061	7	19	.22	50	.05	4	3.15	.01	.03	1	2
L16+50E 1+00S P	10	36	15	107	.7	7	49	3043	2.93	5	5	ND	1	26	2	4	2	67	.51	.095	6	18	.39	49	.05	9	3.09	.02	.03	1	1
L16+50E 1+25S P	9	24	20	113	1.1	9	19	2385	5.09	6	5	ND	1	21	1	2	2	73	.36	.060	4	18	.22	34	.06	6	2.72	.01	.04	1	1
L16+50E 1+50S P	6	20	32	101	1.7	5	5	236	.81	2	5	ND	1	16	1	3	4	34	.19	.067	4	14	.10	35	.06	7	2.01	.01	.03	1	3
L16+50E 1+75S P	14	22	18	112	.5	9	5	310	.94	14	7	ND	1	34	1	2	2	38	.77	.076	6	16	.26	38	.03	7	1.97	.01	.02	1	2
L16+50E 2+00S P	14	14	16	38	.1	7	4	295	4.38	8	5	ND	1	20	1	2	2	122	.43	.013	3	15	.19	21	.14	2	1.41	.01	.02	1	5
L16+50E 2+25S P	14	29	20	103	.5	13	6	332	3.45	14	5	ND	1	28	1	2	2	105	.47	.037	4	28	.46	30	.12	3	1.96	.01	.03	1	2
L16+50E 2+50S P	5	17	25	52	.2	9	3	166	1.16	4	5	ND	1	20	1	2	2	77	.79	.018	3	25	.34	18	.11	5	1.37	.01	.02	2	1
L16+50E 2+75S P	5	12	8	32	.1	5	1	115	.92	2	5	ND	1	23	1	2	4	82	1.24	.018	2	24	.09	28	.13	4	.70	.01	.01	1	4
L16+50E 3+00S P	3	19	10	95	2.1	4	1	47	.98	2	5	ND	1	16	1	3	2	32	.24	.157	4	9	.05	31	.04	9	1.05	.01	.04	1	2
L16+50E 3+25S P	6	14	20	50	.4	4	1	53	1.61	2	5	ND	1	16	1	2	6	65	.23	.065	4	13	.05	24	.07	2	1.28	.01	.03	1	1
L16+50E 3+50S P	5	8	15	61	.5	13	3	365	1.87	2	5	ND	1	17	1	2	4	66	.36	.072	4	35	.31	24	.09	4	1.03	.02	.04	1	1
L16+50E 4+00S P	4	15	17	74	.3	7	2	80	.76	2	5	ND	1	23	1	2	5	37	.34	.080	4	22	.12	31	.05	2	1.22	.01	.03	1	1
L18+00E 5+00N P	4	8	10	52	.9	3	1	75	1.03	2	5	ND	1	23	1	2	3	41	.44	.029	3	7	.09	22	.07	3	.79	.01	.03	1	1
L18+00E 4+75N P	5	31	24	170	1.3	3	24	952	3.47	2	5	ND	1	20	2	3	2	37	.40	.122	5	19	.06	32	.03	8	2.07	.01	.05	1	1
L18+00E 4+50N P	12	17	43	49	1.2	2	58	3475	27.95	14	5	ND	1	11	1	2	5	136	.16	.036	2	25	.07	21	.06	4	1.69	.01	.03	1	1
L18+00E 4+25N P	5	22	17	181	.9	5	8	322	2.12	2	5	ND	1	27	2	2	2	36	.44	.084	4	10	.10	52	.04	4	1.24	.01	.05	1	1
L18+00E 4+00N P	2	30	12	142	.2	5	6	284	3.93	2	5	ND	1	10	1	2	2	44	.10	.068	3	8	.03	15	.02	2	.74	.01	.03	1	1
L18+00E 3+75N P	1	15	2	114	.1	2	1	40	.45	2	5	ND	1	11	1	2	2	10	.11	.061	2	4	.02	18	.01	2	.42	.01	.02	1	1
L18+00E 3+50N P	2	31	2	111	.5	4	1	74	4.04	2	5	ND	1	7	1	2	2	82	.07	.095	4	13	.03	13	.02	4	1.10	.01	.04	1	1
L18+00E 3+25N P	1	5	2	143	.1	1	1	24	.14	2	5	ND	1	34	1	3	2	3	.53	.042	2	4	.08	23	.01	3	.11	.01	.03	1	1
L18+00E 3+25N A P	1	36	8	72	.2	10	7	350	4.30	12	5	ND	1	18	1	2	2	93	.56	.049	4	18	.54	13	.20	5	1.50	.01	.02	1	1
L18+00E 3+00N P	1	19	4	50	.1	14	3	135	.98	2	5	ND	1	22	1	2	2	40	.50	.016	2	31	.35	18	.22	2	.81	.01	.03	1	2
L18+00E 2+50N P	1	12	9	103	.4	5	2	78	.93	4	5	ND	1	32	1	2	2	22	.91	.065	2	6	.12	11	.04	11	.45	.02	.03	1	1
L18+00E 2+25N P	2	38	11	56	.6	11	6	204	3.97	12	5	ND	1	23	1	2	2	123	.40	.019	3	34	.33	17	.18	5	1.47	.02	.02	1	2
L18+00E 2+00N P	1	4	2	131	.3	2	1	34	.10	2	5	ND	1	35	1	2	2	4	.53	.041	2	3	.11	10	.01	8	.13	.03	.03	1	1
L18+00E 1+75N P	2	16	27	104	.4	14	11	2263	3.37	138	5	ND	1	20	1	5	2	36	.82	.101	6	14	.10	13	.03	3	2.51	.01	.02	1	2
L18+00E 1+25N P	1	20	7	100	.7	5	3	273	2.06	8	5	ND	1	16	1	2	3	100	.48	.034	2	11	.12	14	.12	6	.70	.01	.03	1	2
L18+00E 1+00N P	1	65	17	97	.1	17	9	530	4.28	60	5	ND	1	21	1	2	2	73	.43	.038	4	43	.41	24	.11	2	5.62	.01	.02	1	4
STD C/AU-8	17	57	37	130	7.0	68	31	956	3.99	44	18	8	36	47	18	15	22	57	.47	.090	36	55	.82	174	.06	40	1.93	.06	.14	12	52



Daiwan Engineering Ltd. I JECT WIN FILE # 90-0245

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Ag+ PPM
L18+00E 0+75N P	1	7	3	90	1.7	1	1	28	.14	2	5	ND	1	24	1	2	2	5	.54	.045	2	5	.08	6	.01	8	.13	.01	.03	1	1
L18+00E 0+50N P	1	8	5	108	.3	3	1	90	.30	2	5	ND	1	34	1	2	2	7	.55	.040	2	8	.16	22	.01	8	.46	.01	.02	1	1
L18+00E 0+25N P	1	4	2	97	.6	2	1	174	.06	2	5	ND	1	32	1	2	2	1	.80	.048	2	4	.06	24	.01	5	1.11	.01	.03	1	1
L18+00E 0+00N P	48	22	111	109	1.5	4	82	81611	8.32	7	5	ND	1	22	4	2	14	140	.50	.071	2	21	.01	548	.03	2	1.24	.01	.03	1	1
L18+00E 0+25S P	7	16	36	100	.3	9	3	324	1.15	5	5	ND	1	24	1	2	2	67	.42	.014	3	29	.40	24	.12	4	1.39	.01	.02	1	1
L18+00E 0+50S P	10	6	37	47	.2	3	5	4524	1.02	2	5	ND	1	18	1	2	2	54	.30	.024	3	15	.06	53	.12	3	.85	.01	.02	2	8
L18+00E 0+75S P	9	9	9	125	.3	2	22	1672	6.34	2	5	ND	1	15	1	2	2	66	.27	.075	3	17	.12	28	.03	2	.99	.02	.04	1	4
L18+00E 1+00S P	4	6	7	96	.2	3	1	247	.44	2	5	ND	1	19	1	2	2	23	.21	.087	3	11	.05	23	.03	2	.71	.01	.03	1	2
L18+00E 1+25S P	1	4	4	143	.2	1	1	170	.09	2	5	ND	1	29	1	2	2	2	1.06	.047	2	3	.05	19	.01	7	.05	.01	.05	1	1
L18+00E 1+50S P	7	12	38	104	.7	9	8	502	2.85	2	5	ND	1	26	1	2	2	55	.39	.061	3	24	.22	26	.07	2	1.03	.01	.04	1	2
L18+00E 1+75S P	6	29	29	178	.6	33	18	5245	3.11	9	5	ND	1	41	3	2	2	72	.68	.050	5	55	1.04	72	.10	2	2.86	.01	.03	1	5
L18+00E 2+00S P	16	11	18	57	.2	3	3	211	3.37	11	5	ND	1	20	1	2	2	101	.26	.023	4	8	.13	28	.08	2	1.09	.01	.03	2	8
L18+00E 2+25S P	5	25	11	115	1.0	6	11	838	4.42	4	5	ND	1	14	2	2	2	73	.21	.068	4	18	.12	26	.05	5	1.57	.01	.04	1	3
L18+00E 2+50S P	2	17	8	110	.4	3	1	64	2.82	2	5	ND	1	8	1	2	2	26	.09	.103	3	3	.03	20	.01	2	.64	.01	.04	1	1
L18+00E 2+75S P	4	22	13	49	.2	5	3	178	1.97	4	5	ND	1	19	1	2	2	103	.26	.017	3	18	.12	18	.12	4	.82	.01	.02	3	1
L18+00E 3+00S P	5	16	6	92	.3	3	1	61	5.55	8	5	ND	1	13	1	2	2	35	.27	.063	2	5	.03	19	.02	3	.65	.01	.03	1	1
L18+00E 3+25S P	12	20	19	41	.4	3	3	184	2.92	9	5	ND	1	22	1	2	3	108	.29	.018	3	13	.19	25	.11	2	1.16	.01	.03	1	16
L18+00E 3+50S P	10	28	9	137	.5	12	20	3600	5.44	10	5	ND	1	28	2	2	4	86	.57	.039	4	21	.46	54	.08	3	2.10	.01	.03	1	1
L18+00E 3+75S P	2	9	5	147	.2	3	1	376	.30	2	5	ND	1	46	1	2	2	11	1.17	.048	2	4	.11	48	.02	9	.25	.01	.05	1	1
L18+00E 4+00S P	8	13	18	135	.6	3	2	297	1.10	2	5	ND	1	22	1	2	2	29	.28	.074	3	9	.08	34	.06	4	.91	.01	.05	1	2
L19+50E 5+00N P	1	7	8	175	.3	4	1	305	.79	2	5	ND	1	24	1	2	3	42	.76	.039	2	11	.12	13	.13	6	.21	.02	.05	1	3
L19+50E 4+75N P	1	20	7	214	.1	5	4	345	3.46	2	5	ND	1	25	1	2	3	35	.29	.079	2	7	.06	30	.04	4	.64	.02	.03	1	1
L19+50E 4+50N P	1	50	6	98	1.0	13	6	128	8.00	2	5	ND	1	21	1	2	3	231	.19	.040	2	48	.24	25	.38	3	1.64	.01	.03	1	5
L19+50E 4+25N P	1	243	8	82	.5	59	16	442	6.07	6	5	ND	1	43	1	3	2	128	.53	.055	3	82	1.54	21	.26	2	3.23	.02	.02	1	5
L19+50E 4+00N P	2	61	2	115	.4	34	8	278	6.86	3	5	ND	1	20	1	2	2	156	.35	.028	2	70	.77	13	.32	2	1.99	.02	.03	1	1
L19+50E 3+75N P	2	69	10	124	.4	14	9	569	6.36	7	5	ND	1	21	1	3	7	106	.29	.025	3	33	.53	26	.13	3	2.35	.01	.02	1	10
L19+50E 3+50N P	4	22	11	61	.3	10	5	223	5.05	5	5	ND	1	22	1	2	2	132	.23	.022	3	27	.55	21	.16	3	1.38	.01	.02	2	1
L19+50E 3+25N P	1	11	9	176	.4	4	3	434	1.07	2	5	ND	1	21	1	2	2	52	.47	.051	2	10	.25	15	.07	5	.36	.02	.05	1	2
L19+50E 3+00N P	3	20	2	78	.5	7	3	97	2.73	4	5	ND	1	22	1	2	3	152	.29	.016	2	54	.10	7	.20	6	.48	.01	.01	1	1
L19+50E 2+75N P	2	116	17	172	3.8	12	16	617	2.16	7	5	ND	1	86	2	2	2	56	2.30	.088	4	12	1.09	51	.06	6	2.17	.02	.05	3	1
L19+50E 2+50N P	1	6	3	123	.3	2	1	45	.09	2	5	ND	1	26	1	2	2	4	.58	.049	2	3	.03	7	.01	6	.09	.02	.02	1	1
L19+50E 2+25N P	4	43	5	63	.4	7	6	393	6.71	5	5	ND	1	19	1	2	2	158	.34	.025	2	26	.23	16	.20	2	1.23	.01	.02	1	1
L19+50E 2+00N P	2	18	11	117	.8	4	2	79	2.05	2	5	ND	1	25	1	2	5	83	.32	.065	3	9	.08	27	.08	9	.78	.01	.04	1	1
L19+50E 1+75N P	2	23	4	95	.9	7	3	210	2.59	2	5	ND	1	24	1	2	6	66	.26	.044	2	11	.22	24	.08	3	.80	.02	.02	1	4
L19+50E 1+25N P	1	15	41	246	1.4	4	2	3342	.56	4	5	ND	1	51	1	2	2	10	3.14	.100	2	5	.09	17	.01	14	.39	.02	.07	1	1
L19+50E 1+00N P	3	34	18	54	.7	6	4	103	5.60	15	5	ND	1	10	1	3	2	128	.14	.021	2	19	.05	11	.17	2	.87	.01	.01	1	4
STD C/AU-S	18	58	35	131	7.0	68	30	1023	4.02	42	21	8	36	47	19	15	20	58	.47	.091	37	55	.83	174	.07	40	1.92	.06	.14	13	47

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SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au+ PPB
19+50E 0+75N	5	44	28	53	.3	8	4	113	6.53	35	5	ND	1	12	1	2	7	149	.14	.019	2	29	.19	9	.13	3	1.13	.01	.01	1	8
19+50E 0+50N	1	10	2	95	.2	3	1	29	.98	5	5	ND	1	16	1	2	2	32	.42	.031	2	6	.06	5	.03	2	.25	.01	.01	1	1
19+50E 0+25N	2	7	4	118	.2	4	1	56	1.60	3	5	ND	1	26	1	2	2	48	.51	.035	2	4	.07	20	.04	4	.31	.01	.02	1	1
19+50E 0+00S	3	15	14	39	.4	11	4	216	3.30	12	5	ND	1	18	1	2	2	126	.62	.020	2	21	.36	14	.17	2	.96	.01	.01	2	1
19+50E 0+25S	1	4	2	105	.5	3	1	30	.27	2	5	ND	1	36	1	2	2	12	.40	.055	2	4	.16	11	.02	4	.14	.02	.04	1	1
19+50E 0+50S	3	26	14	94	1.0	8	4	164	4.14	11	5	ND	1	18	1	2	4	116	.24	.089	2	25	.24	34	.12	2	1.70	.01	.01	1	4
L19+50E 0+50S A	4	16	6	50	.5	4	2	69	2.27	9	5	ND	1	16	1	3	2	137	.20	.019	2	11	.05	24	.14	2	.57	.01	.01	1	18
L19+50E 0+75S	3	60	19	168	.4	18	6	254	3.71	12	5	ND	1	21	1	2	2	94	.34	.030	3	34	.57	32	.13	2	2.93	.01	.02	1	4
L19+50E 1+00S	2	37	11	43	.3	10	4	108	4.17	10	5	ND	1	18	1	2	2	143	.21	.021	2	21	.25	18	.22	2	.86	.01	.02	2	9
L19+50E 1+25S	2	82	18	58	.2	19	8	239	5.24	9	5	ND	1	21	2	3	2	99	.25	.029	2	51	.58	17	.19	2	4.49	.01	.02	1	10
L19+50E 1+50S	3	38	12	53	.3	7	4	96	5.67	8	5	ND	1	14	1	2	4	199	.26	.031	2	24	.12	10	.21	2	.90	.01	.02	2	9
L19+50E 1+75S	4	24	2	69	.7	6	3	168	1.95	6	5	ND	1	25	1	2	3	93	.51	.041	2	16	.13	18	.08	4	.89	.01	.02	1	5
L19+50E 2+00S	2	91	13	68	.2	23	9	263	4.19	4	5	ND	1	22	2	2	2	107	.42	.031	2	36	.61	15	.21	2	2.93	.01	.02	1	5
L19+50E 2+25S	1	14	2	128	.7	5	2	83	1.18	2	5	ND	1	23	1	2	2	44	.58	.066	2	10	.11	15	.07	7	.42	.01	.03	1	3
L19+50E 2+50S	3	46	52	365	.3	14	11	1300	2.62	5	5	ND	1	44	4	2	2	60	1.41	.064	3	16	.38	61	.07	3	1.65	.01	.03	1	1
L19+50E 2+75S	1	58	13	88	.6	9	12	445	3.06	7	5	ND	1	91	1	2	2	76	1.87	.066	3	14	.70	349	.07	2	2.83	.02	.03	1	1
L19+50E 3+00S	1	35	22	242	1.5	12	11	1132	1.61	11	5	ND	1	78	2	2	2	39	2.00	.068	4	13	1.22	33	.08	2	1.72	.01	.01	1	1
L19+50E 3+25S	6	51	18	113	.6	12	8	396	3.34	11	5	ND	1	41	1	2	4	74	.76	.038	5	20	.63	46	.11	3	2.02	.01	.03	1	1
L19+50E 3+50S	5	70	15	115	.3	19	9	322	2.79	9	5	ND	1	40	2	2	2	75	.70	.044	4	31	.81	34	.11	2	2.18	.02	.04	1	5
L19+50E 3+75S	4	50	14	111	.3	13	6	227	5.39	7	5	ND	1	28	1	2	2	70	.42	.055	4	21	.45	29	.07	2	1.57	.02	.03	1	3
L19+50E 4+00S	3	22	13	78	.3	66	13	171	6.74	6	5	ND	1	7	1	5	2	121	.22	.038	2	90	1.64	11	.10	4	2.50	.03	.04	1	1
L21+00E 5+00N	1	252	11	131	.3	63	23	382	6.41	8	5	ND	1	58	2	6	2	140	.43	.026	2	100	1.50	40	.36	3	5.10	.01	.01	1	3
L21+00E 4+75N	1	26	15	53	.2	12	5	128	5.83	2	5	ND	1	16	1	2	2	201	.22	.025	2	26	.26	14	.30	2	1.17	.01	.02	1	6
L21+00E 4+50N	2	67	14	31	.3	14	7	160	9.68	3	5	ND	1	14	1	4	2	204	.24	.021	2	43	.41	6	.40	2	1.53	.01	.01	1	6
L21+00E 4+25N	1	64	5	39	.5	17	8	154	9.96	2	5	ND	1	15	2	4	2	218	.25	.020	2	71	.38	5	.50	2	3.71	.01	.01	2	5
L21+00E 4+00N	1	78	24	96	.4	34	12	410	5.73	5	5	ND	1	31	1	2	2	122	1.04	.021	2	71	1.12	6	.35	2	2.90	.01	.01	1	1
L21+00E 3+75N	4	37	15	26	.3	7	4	136	9.47	5	5	ND	1	13	1	2	2	189	.20	.022	2	37	.22	10	.26	2	1.17	.01	.01	1	1
L21+00E 3+50N	4	99	16	57	.2	21	8	328	5.87	10	5	ND	1	24	1	2	2	102	.40	.036	2	52	.79	19	.19	2	3.59	.02	.02	1	1
L21+00E 3+00N	1	10	4	68	.6	3	1	201	.90	2	5	ND	1	15	1	2	2	27	.70	.063	2	7	.08	6	.05	8	.22	.01	.03	1	4
L21+00E 2+50N	1	18	13	81	.3	4	2	694	.66	2	5	ND	1	25	1	2	2	17	.85	.078	2	9	.16	11	.04	7	.48	.01	.04	1	1
L21+00E 2+25N	1	64	15	73	.2	8	5	193	6.20	11	5	ND	1	18	1	2	2	114	.48	.018	2	32	.37	13	.13	2	3.17	.01	.01	1	9
L21+00E 2+00N	1	154	71	499	1.8	24	24	2357	5.08	19	6	ND	1	35	4	4	2	61	1.44	.341	8	48	.51	30	.09	4	6.69	.01	.02	1	4
L21+00E 1+75N	1	288	87	1039	2.8	48	43	10877	7.31	15	8	ND	1	36	8	2	2	67	1.47	.136	21	58	.52	68	.09	7	8.58	.01	.01	1	3
L21+00E 1+50N	1	160	35	374	1.8	28	31	11227	7.10	6	6	ND	1	39	5	2	2	88	1.70	.150	11	37	.24	73	.07	9	5.22	.01	.02	1	6
L21+00E 1+25N	1	35	19	83	1.1	12	9	4654	5.40	5	5	ND	1	33	2	2	2	173	1.00	.027	4	47	.10	50	.16	3	1.38	.01	.02	1	5
L21+00E 1+00N	1	37	14	31	.3	10	5	470	5.00	4	5	ND	1	91	2	2	2	145	.69	.021	2	30	.28	17	.32	2	1.64	.01	.01	2	10
STD C/AU-S	17	57	42	131	7.2	69	30	1019	4.18	43	20	8	36	48	20	15	21	59	.47	.094	37	57	.83	174	.07	38	1.96	.06	.14	13	49

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SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe X	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca X	P X	La PPM	Cr PPM	Mg X	Ba PPM	Ti X	B PPM	Al X	Na X	K X	W PPM	Al <sup>u</sup> PPM
L21+00E 0+75N	2	53	10	26	.1	8	4	220	4.15	3	5	ND	1	22	1	2	7	141	.27	.024	3	38	.35	13	.21	2	2.70	.01	.01	1	14
L21+00E 0+50N	1	40	22	35	.2	12	7	228	7.90	2	5	ND	1	27	1	2	5	202	.28	.022	2	39	.40	8	.35	2	1.28	.01	.02	1	12
L21+00E 0+25N	1	60	23	58	.2	15	11	482	6.45	8	5	ND	1	21	1	2	2	142	.53	.038	3	42	.85	12	.26	2	3.27	.02	.02	1	13
L21+00E 1+00S	1	30	22	458	1.6	27	14	334	6.58	30	5	ND	1	18	4	2	5	741	3.80	.042	5	103	.28	5	.20	7	2.15	.01	.02	1	6
L22+50E 5+00N	1	39	16	94	.3	12	7	204	6.24	8	5	ND	1	15	2	2	4	217	.54	.038	3	41	.35	10	.24	2	1.65	.01	.02	1	7
L22+50E 4+75N	1	9	5	32	.1	5	3	103	3.32	2	5	ND	1	10	1	2	5	223	.28	.007	2	13	.09	5	.23	2	.60	.01	.01	1	11
L22+50E 4+50N	1	27	7	93	.1	7	3	114	3.00	6	5	ND	1	31	1	2	5	88	.24	.040	2	19	.25	19	.16	2	.86	.01	.03	1	10
L22+50E 4+25N	1	21	12	18	.1	3	1	59	1.65	2	5	ND	1	12	1	2	2	108	.14	.012	3	29	.09	12	.24	2	1.09	.01	.02	1	4
L22+50E 4+00N	1	52	2	20	.4	10	11	520	13.25	2	5	ND	1	16	1	2	5	203	.25	.016	2	30	.35	7	.35	2	1.36	.01	.02	1	8
L22+50E 3+75N	1	74	2	27	.1	22	9	162	6.30	2	5	ND	1	46	1	2	5	210	.44	.016	2	34	.63	4	.42	2	.93	.01	.01	1	9
L22+50E 3+50N	1	7	10	13	.1	4	2	83	1.35	2	5	ND	1	11	1	2	5	81	.17	.005	2	22	.15	8	.20	2	.56	.01	.01	1	3
L22+50E 3+25N	1	9	13	35	.3	3	1	55	1.13	2	5	ND	1	17	1	3	4	78	.15	.020	2	22	.10	11	.12	2	.60	.01	.02	1	5
L22+50E 3+00N	1	8	6	24	.1	3	2	68	2.04	2	5	ND	1	10	1	2	4	194	.18	.011	2	14	.06	7	.22	2	.59	.01	.01	1	8
L22+50E 2+75N	1	8	2	62	.1	3	2	16	1.11	2	5	ND	1	7	1	2	2	13	.11	.049	3	2	.02	14	.01	2	.44	.01	.01	1	3
L22+50E 2+50N	1	15	2	33	.1	10	4	126	3.02	3	5	ND	1	7	1	2	3	124	.17	.021	3	42	.38	10	.17	2	.75	.02	.02	1	3
L22+50E 2+25N	1	8	12	31	.1	1	1	22	1.87	5	5	ND	1	10	1	2	2	42	.06	.020	2	12	.02	20	.10	2	.58	.01	.02	2	10
L22+50E 2+00N	1	8	4	54	.2	4	2	62	1.04	2	5	ND	1	28	1	2	3	47	.41	.033	2	16	.17	17	.08	4	.32	.01	.03	1	5
L22+50E 1+75N	1	5	3	64	.2	1	1	14	.52	2	5	ND	1	26	1	2	4	16	.07	.029	2	8	.09	19	.05	4	.24	.01	.03	1	4
L22+50E 1+50N	2	11	23	33	.2	2	1	37	1.04	2	5	ND	1	13	1	2	6	43	.10	.029	3	15	.05	18	.12	2	.83	.01	.03	1	11
L22+50E 1+25N	5	69	20	117	.3	15	8	336	2.93	9	5	ND	1	41	1	2	3	77	.76	.042	5	24	.68	30	.12	2	2.33	.01	.03	2	7
L22+50E 1+00N	1	53	10	78	.2	10	6	252	3.44	2	5	ND	1	34	1	2	3	130	.69	.033	3	23	.46	52	.16	2	1.82	.01	.03	1	6
L22+50E 0+75N	1	31	14	116	.2	6	4	388	1.29	2	5	ND	1	21	1	2	4	47	.52	.062	4	9	.11	22	.03	2	1.00	.01	.02	1	1
L22+50E 0+50N	2	5	17	24	.1	2	1	78	3.09	3	5	ND	1	10	1	2	5	158	.12	.010	4	22	.06	11	.15	2	.83	.01	.02	1	1
L22+50E 0+25N	1	21	12	77	.2	6	2	50	.76	2	5	ND	1	13	1	3	4	58	.16	.043	3	36	.04	21	.09	2	.96	.01	.01	1	9
L24+00E 0+25S	1	22	4	65	.2	1	1	27	.84	2	5	ND	1	10	1	2	2	41	.09	.121	3	8	.03	20	.02	2	.69	.01	.03	1	3
L24+00E 0+50S	1	21	3	68	.2	3	1	14	.34	2	5	ND	1	11	1	2	3	31	.12	.117	3	11	.03	18	.03	4	.85	.01	.03	1	5
L24+00E 0+75S	1	14	10	27	.5	9	2	71	1.31	11	5	ND	1	21	1	2	2	55	.39	.019	2	30	.08	4	.10	2	.36	.01	.01	1	6
L24+00E 1+00S	1	53	12	132	.5	7	4	371	.47	2	5	ND	1	32	1	2	2	23	1.69	.076	4	11	.04	21	.01	3	1.05	.01	.01	1	1
L24+00E 1+25S	1	21	16	28	.4	12	6	119	3.77	5	5	ND	1	23	2	2	7	149	.30	.017	2	19	.26	22	.30	2	.71	.02	.02	2	5
L24+00E 1+50S	3	35	26	39	.1	9	5	173	5.03	4	5	ND	1	18	1	2	5	141	.22	.015	2	34	.31	15	.25	2	1.12	.01	.02	1	14
L24+00E 1+75S	1	8	2	115	.4	2	1	37	.51	2	5	ND	1	38	1	2	2	24	.49	.043	2	6	.12	20	.05	4	.16	.02	.04	1	3
L24+00E 2+00S	2	13	7	68	.2	3	3	65	1.21	2	5	ND	1	31	1	2	5	29	.42	.091	3	6	.07	33	.03	4	.49	.02	.04	1	4
L24+00E 2+25S	1	7	3	87	.1	1	1	30	.30	2	5	ND	1	22	1	2	3	12	.36	.035	2	4	.04	17	.01	2	.20	.01	.02	1	8
L24+00E 2+50S	1	3	3	58	.1	1	1	24	.07	2	5	ND	1	52	1	2	2	2	.17	.041	2	5	.18	14	.01	4	.05	.02	.05	1	2
L24+00E 2+75S	1	6	2	51	.4	2	1	14	.07	2	5	ND	1	41	1	2	2	1	.48	.045	2	4	.11	25	.01	7	.10	.01	.04	1	1
L24+00E 3+00S	1	4	8	93	1.0	1	1	94	.06	2	5	ND	1	43	1	2	5	2	.60	.063	2	4	.11	21	.01	8	.06	.01	.05	1	1
STD C/AU-S	18	58	37	129	6.9	68	30	1019	3.91	40	19	8	36	47	18	16	20	56	.47	.090	36	56	.82	173	.06	40	1.90	.06	.14	13	53

Daiwan Engineering Ltd. PROJECT WIN FILE # 90-0245

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Al <sub>2</sub> O <sub>3</sub> PPM
L24+00E 3+25S	1	31	10	69	1.7	5	1	89	.55	2	5	ND	1	13	1	2	2	16	.18	.159	2	10	.04	21	.02	8	.66	.01	.04	1	5
L24+00E 3+50S	2	18	6	20	.3	6	3	36	1.92	3	5	ND	1	7	1	2	2	86	.04	.017	2	15	.03	11	.06	3	.59	.01	.01	1	13
L24+00E 3+75S	1	84	15	52	.3	24	9	227	4.20	8	5	ND	1	19	1	2	3	101	.38	.054	3	47	.61	21	.16	2	3.10	.02	.02	1	2
L24+00E 4+00S	1	13	2	59	.3	4	1	33	.61	2	5	ND	1	16	1	2	2	26	.26	.101	2	9	.04	18	.02	8	.44	.01	.04	1	3
L24+00E 5+00S	1	22	5	66	.4	5	1	718	1.13	2	5	ND	1	32	1	2	2	41	.90	.080	2	10	.13	19	.05	9	.49	.01	.06	1	6
L24+00E 5+25S	1	15	9	89	1.2	3	1	281	.49	2	5	ND	1	26	1	2	2	19	.52	.097	2	7	.07	23	.03	7	.36	.02	.05	1	1
L24+00E 5+50S	2	103	23	116	.3	19	8	296	4.87	9	5	ND	1	34	1	2	2	94	.55	.046	4	31	.78	38	.11	3	2.20	.03	.03	1	10
L25+50E 0+00S	2	63	24	94	.3	29	8	281	4.99	9	5	ND	1	28	1	2	3	99	.46	.032	3	37	.76	22	.22	3	1.42	.02	.03	1	4
L25+50E 0+25S	1	40	18	111	.1	13	6	424	2.34	3	5	ND	1	41	2	2	2	68	.74	.070	3	19	.65	18	.13	3	1.13	.01	.02	1	11
L25+50E 0+50S	2	65	16	85	.3	14	8	353	5.84	4	5	ND	1	58	1	2	6	147	.82	.043	3	24	.47	31	.23	3	1.59	.03	.04	1	6
L25+50E 0+75S	2	28	11	104	.3	7	4	231	1.73	6	5	ND	1	38	1	2	3	50	.53	.042	4	14	.34	26	.11	2	.93	.01	.03	1	1
L25+50E 1+00S	2	26	9	39	.2	6	4	633	3.06	24	5	ND	1	15	1	2	3	91	.39	.035	3	13	.13	15	.07	2	.95	.01	.01	1	3
L25+50E 1+25S	1	107	6	55	.2	7	5	285	3.14	21	5	ND	1	47	1	2	2	60	2.69	.041	2	10	.15	14	.13	7	.64	.01	.02	1	4
L25+50E 1+50S	1	6	7	54	.2	3	1	204	.20	2	5	ND	1	24	1	2	2	7	1.00	.063	2	4	.05	11	.01	8	.10	.01	.04	1	5
L25+50E 1+75S	1	17	5	63	.7	5	5	4191	7.11	10	5	ND	1	46	1	2	3	9	3.47	.125	2	6	.02	93	.01	7	.42	.01	.01	1	4
L25+50E 2+25S	2	41	16	23	.1	5	3	213	6.65	5	5	ND	1	10	1	3	6	194	.25	.023	2	23	.07	11	.27	2	.89	.01	.02	1	1
L25+50E 2+50S	2	15	16	15	.1	2	1	292	2.08	2	5	ND	1	17	1	2	2	131	.65	.021	3	13	.07	24	.17	2	.81	.01	.02	1	15
L25+50E 2+75S	2	16	16	32	.3	5	5	1382	4.09	4	5	ND	1	16	1	2	2	106	.61	.034	3	18	.06	24	.11	2	1.25	.01	.03	2	1
L25+50E 3+00S	37	17	16	48	.4	3	5	480	17.01	59	6	ND	1	19	1	2	3	131	.39	.046	5	20	.11	36	.03	6	1.20	.01	.02	1	5
L25+50E 3+25S	4	37	18	48	.1	6	4	286	5.02	23	5	ND	1	16	1	2	2	139	.25	.024	2	20	.13	13	.12	2	.95	.01	.02	2	12
L25+50E 3+50S	14	38	17	80	.6	7	5	256	5.07	17	7	ND	1	24	1	2	2	84	.42	.041	4	17	.29	30	.06	2	1.45	.01	.03	1	9
L25+50E 3+75S	2	9	13	25	.1	8	2	176	1.62	2	5	ND	1	13	1	2	2	88	.20	.009	3	27	.34	11	.18	2	.75	.01	.02	1	10
L25+50E 4+00S	2	18	19	157	.2	63	15	466	6.36	2	5	ND	1	19	1	2	2	91	.34	.032	2	149	1.44	14	.13	2	1.84	.01	.02	1	2
L25+50E 4+50S	1	6	3	91	.1	4	1	37	.39	2	5	ND	1	53	1	2	2	11	.86	.027	2	8	.10	24	.02	2	.21	.01	.01	1	6
L25+50E 4+75S	1	20	8	103	.4	11	3	80	1.12	2	5	ND	1	39	1	2	3	20	.77	.071	2	23	.19	39	.02	4	.60	.01	.02	1	3
L25+50E 5+00S	1	5	4	63	.1	2	1	22	.13	2	5	ND	1	45	1	2	2	3	2.10	.028	2	6	.09	11	.01	2	.08	.01	.01	1	6
STD C/AU-S	18	57	44	128	6.7	68	31	947	4.01	42	20	8	36	47	19	15	22	57	.46	.091	36	55	.82	173	.06	37	1.88	.06	.14	13	48

Daiwan Engineering Ltd. PROJECT WIN FILE # 90-0245

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
C 109478	1	12	34	1691	6	3	9	6810	36.51	64	5	ND	5	5	8	17	2	2	3.11	.013	3	5	.03	13	.01	4	.06	.01	.01	1	23
C 109479	1	166	9	40	3	61	16	244	3.44	5	5	ND	1	125	1	7	4	76	1.51	.048	2	49	1.02	19	.20	4	2.55	.21	.02	1	8
C 109480	2	110	7	65	2	31	6	245	3.54	17	5	ND	1	21	1	3	2	127	2.63	.049	2	117	.11	7	.46	2	2.38	.02	.01	1	4
C 109481	1	68	10	108	1	21	21	710	4.80	4	5	ND	1	584	1	3	2	110	.88	.062	2	23	2.14	62	.12	2	2.65	.10	.05	1	11
C 109482	1	37	2	26	1	8	8	269	2.35	6	5	ND	1	68	1	2	2	66	2.63	.079	6	8	.60	39	.16	6	2.22	.05	.03	1	1
C 109483	4	71	5	125	1	5	12	225	2.80	10	5	ND	1	62	1	4	5	37	4.25	.092	5	3	.32	20	.11	6	3.18	.03	.01	1	3
C 109484	1	36	7	33	1	10	13	315	1.89	6	5	ND	1	62	1	2	2	57	4.39	.086	4	6	.79	15	.13	7	3.16	.01	.01	1	5
C 109485	1	458	872	7318	8.9	9	18	4514	3.51	24	5	ND	1	8	88	2	18	11	1.48	.025	2	6	.22	13	.01	2	.12	.01	.01	1	10
C 109486	20	149	10	57	6	38	12	569	7.34	35	5	ND	1	59	1	2	2	228	1.26	.083	5	24	.31	10	.07	5	1.44	.01	.01	1	9
C 109487	6	152	125	343	5	41	10	1190	3.64	34	5	ND	1	42	3	2	2	86	3.41	.099	4	18	.08	9	.07	36	1.86	.01	.01	1	1
C 109488	8	92	63	637	7	37	10	412	2.69	17	5	ND	1	17	8	4	4	104	2.63	.069	5	31	.11	54	.11	5	1.52	.03	.01	1	1
C 109489	2	69	13	38	1	12	3	180	2.77	13	5	ND	1	14	1	3	3	71	.44	.055	6	22	.31	46	.22	2	.89	.04	.04	2	1
C 109490	1	5	3	615	1	2	1	2285	1.72	4	5	ND	1	269	4	3	2	12	2.24	.109	8	3	.15	9	.14	3	1.63	.01	.01	1	4
C 109491	1	131	19	583	2.8	1	18	12875	31.64	90	5	ND	5	3	7	2	28	11	4.87	.029	2	2	.03	16	.04	2	.19	.01	.01	1	260
C 109492	2	88	18	464	9	2	7	21026	26.07	80	6	ND	5	2	9	2	2	3	4.92	.013	2	2	.04	4	.01	2	.08	.01	.01	1	56
C 109493	1	2124	42	66476	8.1	3	49	12290	11.84	34	5	ND	2	3	812	2	8	2	1.86	.019	2	10	.14	3	.01	2	.13	.01	.01	3	27
C 109494	1	441	92	31254	1.6	2	16	7778	2.65	7	5	ND	1	33	295	2	2	8	1.17	.044	2	12	.16	2	.05	2	.24	.01	.01	1	13
C 109495	4	3056	29	534	25.7	74	228	1579	14.68	200	5	ND	1	20	4	2	30	59	5.38	.212	2	2	.70	4	.04	2	.98	.01	.01	2	280
C 109496	1	37	11	62	2	8	12	367	2.16	20	5	ND	1	83	1	2	2	38	2.33	.069	5	2	.53	106	.11	4	2.07	.07	.05	1	6
C 109497	15	65	7	56	4	6	9	376	3.31	26	5	ND	2	53	1	3	2	52	1.68	.073	6	5	.78	61	.13	3	1.91	.05	.05	1	14
C 109498	1	114	4	45	1	64	17	332	4.23	3	5	ND	1	108	1	4	2	122	.97	.046	3	78	1.48	15	.40	2	1.92	.03	.01	2	2
C 109499	1	193	7	28	1	21	9	254	2.23	10	5	ND	1	97	1	2	3	90	5.46	.030	2	42	.63	6	.22	4	6.07	.04	.04	1	7
C 109500	1	11	16	36	1	1	1	347	.93	8	5	ND	5	237	1	2	2	5	6.29	.010	10	1	.25	21	.06	2	9.45	.01	.07	1	9
STD C/AU-R	17	60	38	133	7.1	66	30	944	3.67	42	19	7	39	48	18	18	20	60	.46	.096	39	56	.84	184	.07	39	1.73	.06	.13	12	520

✓ ASSAY RECOMMENDED

ACME ANALY. LAB. LABORATORIES LTD.

852 E. HASTINGS ST. VAN. VER B.C. V6A 1R6

PHONE(604)253-3158 FAX(604) 53-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MO BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.  
 - SAMPLE TYPE: SILT/ROCK AU\*\* ANALYSIS BY FA/ICP FROM 30 GM SAMPLE.

DATE RECEIVED: JAN 8 1989 DATE REPORT MAILED: *Jan 12/90* SIGNED BY: *C. Leong* D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

Daiwan Engineering Ltd. PROJECT WIN File # 90-0081

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	AU**
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	%	%	%	%	PPM	PPM
C 109951	2	62	17	55	.5	10	11	972	4.85	5	5	ND	1	25	2	2	2	109	.77	.050	2	19	.26	37	.14	4	1.81	.01	.01	1	14
90-01	2	7	6	4	.1	6	1	58	.31	2	5	ND	2	15	1	2	2	22	.38	.003	10	32	.02	236	.13	2	.23	.03	.01	1	62
90-02	3	228	14	12	.3	6	14	136	5.09	5	5	ND	2	59	1	2	2	69	.12	.034	2	11	.82	56	.08	3	1.11	.04	.05	1	7
90-03	12	116	9	29	.1	6	7	199	3.05	5	5	ND	2	30	1	2	2	60	.73	.034	4	11	.81	16	.09	2	2.06	.01	.04	2	6
90-04	32	24	7	3	.1	7	1	36	.31	2	5	ND	1	9	1	2	2	4	.21	.014	5	8	.06	3	.01	2	.34	.01	.01	1	1
90-05	18	640	10	36	.1	6	7	140	1.74	2	5	ND	2	43	1	2	2	24	2.14	.030	5	7	.53	37	.03	3	2.09	.01	.03	1	17
90-06	10	39	11	28	.1	11	6	244	4.97	4	5	ND	1	14	1	3	2	86	.32	.056	2	64	1.37	24	.05	2	1.69	.01	.06	1	21
90-07	2	6	3	1	.1	6	1	67	.92	3	5	ND	1	1	1	2	2	1	.15	.002	2	5	.01	1	.01	2	.03	.01	.01	1	89
90-08	2	3	4	1	.1	10	2	250	2.40	25	5	ND	1	1	1	2	2	3	1.61	.005	2	5	.02	1	.01	3	.07	.01	.01	1	81
90-09	1	2	3	7	.1	6	11	633	6.41	75	5	ND	1	1	1	2	2	8	3.19	.029	2	9	.06	1	.01	5	.32	.01	.01	1	150
STD C/AU-R	18	57	42	130	6.5	68	30	941	3.92	40	20	8	38	48	19	15	22	58	.43	.095	38	55	.81	175	.07	39	1.82	.06	.14	13	480

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM. - SAMPLE TYPE: P1-P11 SOIL P12 ROCK AUP ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

DATE RECEIVED: JAN 23 1990 DATE REPORT MAILED: Jan 30/90 SIGNED BY: [Signature] D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

Daiwan Engineering Ltd. PROJECT WIN File # 90-0207 Page 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	AUP PPM
LO+00E 15+00N	2	16	27	49	.1	17	4	262	2.26	2	5	ND	1	25	1	2	2	97	.65	.015	3	35	.58	19	.22	4	1.49	.01	.02	1	8
LO+00E 14+75N	3	5	32	36	.3	5	1	88	1.94	2	5	ND	1	18	1	2	5	81	.32	.025	3	18	.09	17	.19	3	.86	.01	.03	1	9
LO+00E 14+50N	2	11	18	56	.8	3	1	18	2.25	2	5	ND	1	7	1	2	2	45	.09	.072	3	17	.03	12	.06	2	.68	.01	.04	1	5
LO+00E 14+25N	3	5	30	32	.1	5	1	109	1.01	3	5	ND	1	17	1	2	7	113	.27	.013	3	23	.13	13	.23	4	.85	.01	.02	3	5
LO+00E 14+00N	2	9	11	85	.1	2	1	47	1.35	2	5	ND	1	13	1	2	4	20	.16	.069	2	7	.04	19	.04	2	.46	.01	.03	1	4
LO+00E 13+75N	5	10	28	46	.1	11	3	208	6.38	6	5	ND	1	20	1	2	2	221	.34	.009	3	28	.39	15	.28	2	1.67	.01	.02	1	4
LO+00E 13+50N	5	9	27	43	.1	6	2	218	3.94	6	5	ND	1	22	1	2	5	178	.39	.007	3	22	.27	18	.24	3	1.45	.01	.02	2	9
LO+00E 13+00N	3	6	27	35	.1	5	1	30	1.85	3	5	ND	1	17	1	2	2	43	.15	.026	3	19	.05	24	.06	3	.98	.01	.03	1	3
LO+00E 12+75N	11	11	47	67	.4	6	4	39	13.04	24	5	ND	1	10	3	2	10	149	.12	.085	4	16	.04	21	.03	6	1.27	.01	.04	1	1
LO+00E 12+50N	5	19	36	76	.1	14	4	235	6.25	12	5	ND	1	22	2	2	2	167	.50	.023	4	28	.44	15	.16	4	2.24	.01	.02	3	9
LO+00E 12+25N	2	9	17	89	.8	5	1	48	1.86	2	5	ND	1	17	1	2	2	56	.24	.039	2	8	.05	23	.08	3	.52	.01	.05	1	5
LO+00E 12+00N	3	37	32	80	.1	17	7	362	4.32	11	5	ND	1	27	1	2	2	138	.60	.013	3	31	.50	37	.23	3	2.58	.01	.02	1	6
LO+00E 11+75N	2	8	20	40	.1	5	3	143	3.30	2	5	ND	1	18	1	2	2	150	.31	.011	2	9	.10	14	.19	4	.56	.01	.03	1	6
LO+00E 11+50N	5	26	28	170	.1	24	9	697	3.90	13	5	ND	1	34	1	2	3	113	.76	.027	4	33	.93	49	.19	2	3.14	.01	.04	1	4
LO+00E 11+25N	3	68	44	168	.1	20	11	455	3.31	12	5	ND	1	45	1	3	2	85	1.08	.050	4	27	.72	83	.15	2	2.65	.03	.03	1	4
LO+00E 11+00N	19	25	30	328	.2	29	26	3454	4.59	21	6	ND	1	37	6	2	2	123	1.02	.072	6	40	.82	69	.09	7	3.36	.01	.03	1	1
LO+00E 10+75N	6	27	20	179	.1	23	8	477	3.42	17	5	ND	1	38	1	2	2	89	.95	.057	6	28	.75	47	.14	2	2.62	.02	.03	1	4
LO+00E 10+50N	2	14	9	72	.3	6	2	575	.54	2	5	ND	1	47	1	2	3	15	1.44	.082	2	5	.11	36	.01	5	.38	.01	.04	1	3
LO+00E 10+25N	4	61	45	192	.1	23	10	626	2.97	8	5	ND	1	58	3	2	6	82	1.70	.065	5	24	.56	62	.13	7	1.78	.04	.04	1	8
LO+00E 10+00N	3	40	23	109	.1	19	10	879	3.20	8	5	ND	1	50	1	2	8	73	1.13	.052	5	22	.65	54	.11	4	2.21	.02	.03	1	7
LO+00E 9+75N	8	56	29	886	.3	30	21	5296	3.75	63	5	ND	1	44	13	2	2	106	1.66	.083	6	39	.34	109	.05	11	3.53	.02	.04	1	3
LO+00E 9+50N	2	66	33	203	.1	25	10	583	3.41	14	5	ND	1	46	3	2	2	95	1.40	.065	5	29	.71	77	.15	4	2.47	.02	.03	2	7
LO+00E 9+25N	4	25	17	66	.1	11	6	264	6.91	10	5	ND	1	24	2	2	2	192	.57	.031	3	24	.35	25	.30	2	1.77	.01	.03	1	2
LO+00E 9+00N	4	33	21	105	.1	21	9	595	3.65	13	5	ND	1	54	2	2	2	90	1.25	.037	4	23	.68	48	.14	2	2.22	.02	.03	1	4
LO+00E 8+75N	3	41	15	99	.2	25	11	610	3.41	18	5	ND	1	56	1	4	3	85	1.16	.060	5	29	.94	46	.15	5	2.27	.03	.03	1	2
LO+00E 8+50N	17	18	17	123	.2	15	32	1728	7.64	53	5	ND	1	34	2	2	2	206	1.05	.041	4	35	.38	50	.14	4	2.47	.01	.03	2	2
LO+00E 8+25N	3	10	12	84	.1	19	5	350	2.06	6	5	ND	1	31	1	2	2	71	.69	.022	5	26	.68	38	.15	2	2.06	.01	.02	1	5
LO+00E 7+75N	2	9	9	66	.1	16	5	369	2.06	3	5	ND	1	29	1	2	2	62	.56	.025	4	23	.75	33	.15	2	1.63	.01	.02	1	3
LO+00E 7+50N	17	17	17	28	.1	6	2	80	4.49	98	5	ND	1	12	1	2	2	179	.16	.037	5	24	.05	19	.08	2	2.39	.01	.01	1	5
LO+00E 7+25N	2	8	6	71	.1	17	9	5137	2.54	10	5	ND	1	35	1	2	2	64	.62	.013	3	24	.72	61	.19	5	1.51	.02	.03	1	3
LO+00E 7+00N	4	8	17	37	.1	7	1	294	2.92	11	5	ND	1	33	1	4	4	140	.65	.010	4	16	.21	24	.27	2	1.08	.01	.02	2	4
LO+00E 6+75N	4	32	19	60	.3	11	6	340	5.68	34	5	ND	2	33	1	4	2	104	.35	.024	3	31	.57	37	.13	2	3.37	.01	.02	1	1
LO+00E 6+50N	2	31	14	117	.1	22	7	535	3.93	54	5	ND	1	44	1	2	2	81	.65	.036	6	28	.92	55	.10	2	2.36	.02	.03	1	1
LO+00E 6+25N	3	67	35	161	.1	30	7	380	2.77	19	5	ND	1	51	1	4	2	80	.82	.055	7	30	.88	92	.11	3	3.54	.02	.03	1	3
LO+00E 6+00N	5	34	25	84	.1	15	6	361	4.20	40	5	ND	1	29	1	2	2	105	.43	.031	4	28	.68	55	.14	2	2.54	.02	.04	1	2
LO+00E 5+75N	1	7	2	66	.2	3	1	88	.28	2	5	ND	1	46	1	2	2	8	.37	.033	2	3	.07	34	.01	5	.20	.01	.03	1	1
STD C/AU-S	18	60	37	132	7.1	67	30	1018	4.14	42	18	7	36	44	19	15	16	57	.51	.092	34	56	.91	172	.06	38	1.89	.06	.14	13	51

Daiwan Engineering Ltd.

AJECT WIN FILE # 90-0207

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au <sup>+</sup> PPM	Pb <sup>+</sup> PPM
LO+00E 5+50N	2	20	23	40	.1	6	5	222	2.34	4	5	ND	1	17	1	2	2	29	.26	.019	5	8	.37	30	.02	7	1.38	.01	.05	1	4	
LO+00E 5+25N	4	21	17	46	.2	6	5	204	3.66	13	5	ND	1	24	1	3	2	69	.32	.020	5	14	.50	32	.07	2	1.94	.02	.04	1	3	
LO+00E 5+00N	1	24	8	68	.5	1	3	68	4.55	2	5	ND	1	8	1	2	2	27	.15	.089	4	4	.03	19	.01	2	1.14	.02	.04	1	7	
LO+00E 4+75N	2	33	19	161	.5	6	50	2613	8.12	9	7	ND	1	19	1	3	10	29	.81	.071	5	8	.05	53	.02	2	2.00	.02	.06	1	1	
LO+00E 4+50N	2	51	16	76	.7	1	2	85	.68	2	6	ND	1	13	1	2	2	20	.31	.130	9	6	.06	19	.01	3	2.22	.01	.04	1	6	
LO+00E 4+00N	4	49	19	72	.1	6	5	286	3.27	5	5	ND	1	28	1	2	8	58	.38	.032	7	12	.48	23	.08	3	2.82	.01	.04	1	3	
LO+00E 3+75N	6	54	23	62	.1	13	7	306	5.66	7	5	ND	1	38	1	2	2	81	.46	.032	7	16	.54	33	.10	2	3.39	.02	.04	1	7	
LO+00E 3+00N	7	51	31	78	.4	15	9	352	5.64	9	6	ND	1	30	1	4	2	94	.45	.065	6	22	.64	24	.13	3	4.11	.01	.04	1	4	
LO+00E 2+75N	11	66	45	99	.5	13	6	420	3.37	14	5	ND	2	50	1	7	2	109	.67	.047	8	23	.87	22	.21	2	4.31	.02	.04	6	4	
LO+00E 2+50N	7	42	21	74	.4	14	7	399	3.94	9	5	ND	1	47	1	2	2	107	.67	.045	6	20	.80	33	.20	5	2.20	.02	.04	1	1	
LO+00E 2+00N	8	41	35	71	.5	16	8	490	4.84	17	5	ND	1	48	1	2	2	125	.62	.039	6	29	.85	19	.24	6	3.05	.02	.03	1	4	
LO+00E 1+75N	5	32	25	92	.3	12	7	292	4.68	15	5	ND	1	50	1	6	2	116	.68	.067	6	14	.69	24	.20	7	3.64	.02	.03	1	11	
LO+00E 1+15N	6	27	24	60	.2	11	6	233	6.06	14	5	ND	1	43	1	2	2	172	.51	.037	5	19	.53	21	.33	2	2.17	.02	.03	1	2	
LO+00E 1+00N	7	58	34	87	.4	21	14	1395	5.54	20	5	ND	1	43	1	4	2	136	.53	.062	6	35	.86	27	.23	6	4.68	.02	.03	1	5	
LO+00E 0+75N	4	54	23	90	.2	12	9	414	5.07	12	5	ND	1	54	1	2	2	112	.70	.065	6	23	1.01	24	.19	2	3.49	.02	.04	3	2	
LO+00E 0+50N	6	38	25	75	.3	12	6	355	6.18	17	5	ND	1	39	1	6	2	151	.59	.048	8	30	.67	29	.26	2	3.88	.02	.02	1	6	
LO+00E 0+25N	4	73	16	88	.1	16	11	488	4.34	19	5	ND	1	65	1	2	2	98	1.22	.082	6	22	1.03	33	.17	2	4.19	.02	.06	1	3	
LO+00E 0+00N	5	76	23	94	.1	15	16	519	4.79	16	5	ND	1	84	1	4	2	96	1.76	.091	6	20	1.04	35	.16	4	5.05	.02	.08	1	3	
L1+50E 15+00N	2	34	14	136	.2	11	7	438	3.38	10	5	ND	1	41	1	2	2	89	1.06	.023	5	23	.53	38	.16	5	2.23	.02	.04	1	2	
L1+50E 14+75N	1	827	12	78	1.0	83	44	312	7.46	25	5	ND	1	141	3	2	2	114	2.73	.053	2	66	.96	28	.24	3	4.14	.02	.03	1	3	
L1+50E 14+50N	3	39	67	110	.1	14	8	360	3.78	13	5	ND	1	41	1	3	2	153	1.63	.016	5	32	.41	19	.27	8	3.08	.01	.02	1	3	
L1+50E 14+25N	1	23	20	52	.1	6	1	28	1.57	2	5	ND	1	12	1	2	2	35	.19	.091	2	17	.04	18	.04	5	1.04	.01	.03	1	3	
L1+50E 14+00N	2	6	7	51	.1	1	1	121	2.29	5	5	ND	1	14	1	3	2	74	.29	.018	2	9	.05	13	.14	5	.64	.01	.02	1	3	
L1+50E 13+75N	2	14	52	120	.5	3	1	107	1.67	2	5	ND	1	16	1	2	2	60	.23	.060	3	15	.16	24	.10	3	1.09	.01	.04	1	2	
L1+50E 13+50N	3	13	7	92	.3	3	2	41	2.56	2	5	ND	1	13	1	2	2	48	.18	.057	2	14	.03	19	.01	4	.97	.01	.03	1	3	
L1+50E 13+25N	20	30	49	137	.6	11	9	426	4.55	11	6	ND	1	30	1	6	2	169	.51	.041	6	37	.49	41	.12	9	3.23	.01	.03	4	5	
L1+50E 13+00N	6	12	48	68	.4	5	3	82	3.72	28	5	ND	1	18	1	4	2	145	.21	.053	4	20	.07	30	.05	3	1.52	.02	.05	3	4	
L1+50E 12+75N	1	7	9	109	.1	1	3	212	4.50	2	5	ND	1	23	1	2	2	26	.44	.091	2	6	.07	30	.01	2	.40	.02	.06	1	2	
L1+50E 12+50N	3	14	36	74	.1	18	7	549	4.71	12	5	ND	1	39	1	2	2	160	1.29	.033	4	27	.60	25	.20	3	1.84	.02	.03	1	1	
L1+50E 12+25N	1	13	25	153	.4	5	4	70	2.48	4	5	ND	1	12	1	2	2	100	.29	.087	4	13	.03	13	.01	6	.98	.01	.02	2	2	
L1+50E 12+00N	4	49	43	134	.1	21	6	347	3.21	16	5	ND	1	37	1	3	2	149	.91	.023	4	48	.67	35	.23	5	4.57	.01	.02	3	2	
L1+50E 11+75N	1	8	13	113	1.3	6	1	45	3.50	2	5	ND	1	14	1	2	4	41	.17	.066	2	7	.05	19	.05	9	.60	.01	.06	1	1	
L1+50E 11+50N	1	12	31	152	.7	3	1	53	1.25	3	5	ND	1	17	1	3	4	30	.26	.056	3	9	.08	28	.05	8	.80	.01	.05	1	2	
L1+50E 11+25N	2	9	12	101	.3	3	1	24	2.03	3	5	ND	1	8	1	2	2	33	.15	.099	3	8	.03	16	.03	5	.67	.01	.05	1	1	
L1+50E 11+00N	1	6	3	123	.2	5	1	70	.08	2	5	ND	1	33	2	2	2	2	.38	.045	2	2	.16	35	.01	9	.07	.02	.05	1	1	
L1+50E 10+75N	4	15	22	93	1.0	5	3	113	3.64	5	5	ND	1	24	1	2	2	85	1.05	.084	4	14	.06	43	.07	2	1.19	.01	.04	1	1	
STD C/AU-S	18	63	41	131	7.2	68	29	962	4.31	41	18	7	36	44	19	14	17	57	.51	.094	34	56	.92	173	.06	38	1.91	.06	.14	13	50	



Daiwan Engineering Ltd. I JECT WIN FILE # 90-0207

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au <sup>+</sup> PPM
L1+50E 10+50N	4	64	17	170	.1	24	8	508	4.87	17	5	ND	1	40	2	4	6	130	1.62	.030	4	47	.89	62	.21	6	5.08	.01	.03	3	9
L1+50E 10+25N	4	38	14	85	1.4	9	5	200	4.62	2	5	ND	1	28	1	2	2	124	.56	.034	3	27	.32	27	.20	3	2.24	.01	.03	1	16
L1+50E 10+00N	3	51	11	107	.1	20	8	487	5.01	11	5	ND	1	34	1	3	2	137	.81	.025	4	45	.73	33	.24	2	3.98	.01	.02	1	6
L1+50E 9+75N	3	16	17	38	.1	5	3	206	4.28	8	5	ND	1	30	1	3	10	167	.71	.014	3	22	.16	17	.24	4	1.27	.01	.02	1	3
L1+50E 9+50N	4	54	26	110	.2	19	7	396	5.33	13	5	ND	1	30	1	5	2	135	.60	.022	3	49	.74	29	.26	2	4.84	.01	.02	1	2
L1+50E 9+25N	4	29	20	66	.2	15	8	338	6.17	9	5	ND	1	28	1	4	4	162	.54	.018	4	37	.67	17	.30	4	2.29	.01	.02	3	1
L1+50E 9+00N	3	39	18	101	.1	15	6	338	4.19	16	5	ND	1	33	1	4	2	124	.65	.018	4	41	.70	26	.22	2	4.00	.01	.02	1	1
L1+50E 8+75N	19	72	17	2242	.7	49	11	7660	4.57	222	5	ND	1	43	44	3	5	232	3.37	.102	9	64	.31	172	.03	10	3.35	.01	.03	1	4
L1+50E 8+50N	6	48	24	562	.1	17	7	456	3.86	26	5	ND	1	31	2	6	11	148	.72	.023	4	43	.60	34	.21	4	4.14	.02	.02	2	6
L1+50E 8+25N	10	29	21	117	.1	9	3	311	3.16	26	5	ND	1	36	2	3	2	141	.81	.010	5	31	.29	23	.22	2	3.31	.02	.02	3	4
L1+50E 8+00N	19	27	16	169	.7	17	8	420	2.22	18	5	ND	1	38	2	2	2	133	1.11	.077	6	38	.53	57	.07	6	2.76	.02	.04	1	3
L1+50E 7+75N	21	24	22	127	1.5	15	5	197	2.51	29	8	ND	1	24	2	6	4	103	.44	.072	7	51	.33	40	.07	4	3.17	.01	.03	2	1
L1+50E 7+50N	12	16	22	67	2.1	8	3	158	1.49	7	5	ND	1	23	3	2	4	96	.58	.091	7	28	.16	37	.03	4	2.40	.01	.04	2	1
L1+50E 7+25N	2	12	13	51	.3	7	1	94	1.31	2	5	ND	1	18	1	2	2	29	.28	.056	2	11	.13	16	.04	4	.88	.01	.03	1	1
L1+50E 7+00N	12	14	2	119	.3	4	6	291	3.48	2	5	ND	1	17	2	2	3	29	.42	.112	2	7	.05	29	.01	6	.45	.01	.10	1	1
L1+50E 6+75N	4	9	9	60	.5	4	2	89	1.19	2	5	ND	1	10	1	2	2	33	.27	.104	3	12	.04	10	.01	2	.70	.01	.04	1	1
L1+50E 6+50N	6	15	7	45	.7	2	2	29	.68	8	5	ND	1	10	1	2	2	69	.40	.071	4	12	.03	13	.01	3	1.05	.01	.01	2	1
L1+50E 6+25N	8	14	10	57	.4	2	3	228	1.67	3	5	ND	1	7	1	2	2	60	.18	.083	4	11	.02	11	.01	3	.95	.01	.02	1	1
L1+50E 6+00N	2	12	14	38	.3	3	1	255	.90	2	5	ND	1	11	1	2	2	21	.13	.056	4	13	.02	28	.03	3	1.00	.02	.02	2	4
L1+50E 5+75N	9	25	13	61	1.5	6	1	96	.71	2	5	ND	1	20	1	2	3	30	.33	.088	4	28	.08	23	.02	2	1.33	.01	.04	1	2
L1+50E 5+50N	15	40	37	237	.7	23	16	556	5.20	27	5	ND	1	34	1	7	4	125	.91	.034	6	60	.71	41	.21	5	4.22	.01	.03	1	4
L1+50E 5+25N	12	31	18	103	.9	7	5	97	.67	2	5	ND	1	39	3	2	3	30	1.40	.092	8	14	.13	35	.02	7	1.79	.01	.02	1	1
L1+50E 5+00N	5	44	59	148	.4	19	6	566	3.59	28	5	ND	1	30	2	4	9	86	1.14	.082	7	33	.47	45	.12	8	4.27	.01	.02	2	3
L1+50E 4+75N	9	42	18	140	.1	24	12	776	4.23	40	5	ND	1	54	1	2	2	108	2.00	.069	6	33	1.09	43	.18	2	2.76	.02	.03	2	1
L1+50E 4+50N	11	32	13	91	.1	25	9	504	3.42	10	5	ND	1	50	1	2	7	100	1.20	.042	5	32	1.20	49	.21	2	2.86	.02	.03	3	2
L1+50E 4+25N	12	26	14	56	.2	5	3	135	2.81	27	5	ND	1	52	1	2	2	69	.53	.037	2	9	.32	28	.13	3	.71	.02	.02	1	3
L1+50E 4+00N	4	43	16	98	.3	20	7	348	2.71	10	5	ND	1	43	1	4	2	80	1.03	.074	6	31	.79	40	.14	2	2.28	.02	.03	2	2
L1+50E 3+75N	3	14	8	67	.1	8	4	231	2.43	9	5	ND	1	30	1	2	2	67	.58	.075	5	19	.33	21	.10	2	1.29	.02	.03	1	1
L1+50E 3+50N	5	19	10	56	.1	17	6	336	3.40	12	5	ND	1	41	1	3	5	98	.76	.031	5	30	.76	24	.23	2	2.17	.02	.03	1	1
L1+50E 3+25N	6	31	12	71	.1	20	6	423	4.33	15	5	ND	1	41	1	2	2	153	.84	.039	5	31	.92	15	.26	2	2.56	.02	.02	1	1
L1+50E 3+00N	6	30	29	79	.2	29	8	465	3.45	12	5	ND	1	57	1	3	2	144	1.01	.035	6	41	.93	19	.23	2	2.46	.02	.03	1	1
L1+50E 2+75N	4	29	22	65	.1	17	6	450	2.62	8	5	ND	1	56	1	3	2	79	1.43	.045	6	25	.73	28	.13	2	2.84	.01	.03	1	1
L1+50E 2+50N	3	31	19	56	.1	15	5	363	4.74	4	5	ND	1	51	1	3	4	125	.67	.024	5	39	.79	20	.23	2	4.27	.01	.02	1	1
L1+50E 2+25N	3	58	17	69	.1	24	8	463	3.33	15	5	ND	1	45	1	4	3	118	.75	.034	6	45	.96	22	.21	2	4.24	.01	.02	1	8
L1+50E 2+00N	4	49	30	70	.1	26	10	544	5.12	14	5	ND	1	54	1	5	2	125	.75	.022	5	55	1.08	20	.25	2	4.52	.01	.02	5	3
L1+50E 1+75N	4	32	23	79	.2	21	7	742	3.20	14	5	ND	1	103	1	5	6	117	1.76	.028	5	40	.89	11	.27	2	3.63	.01	.01	1	2
STD C/AU-S	18	63	38	131	7.4	67	30	1017	4.23	44	17	8	36	45	19	15	23	57	.52	.093	34	52	.92	172	.07	39	1.96	.06	.14	11	52

Daiwan Engineering Ltd. P TECT WIN FILE # 90-0207

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au <sup>+</sup> PPM
L1+50E 1+50N	1	39	14	100	.2	18	12	772	4.22	5	5	ND	1	67	1	3	6	119	.89	.088	7	25	1.99	19	.20	2	5.05	.01	.03	1	6
L1+50E 1+25N	5	18	17	75	.1	22	6	442	3.00	10	5	ND	1	43	1	2	7	93	.46	.041	4	39	.77	19	.20	2	1.80	.01	.02	1	1
L1+50E 1+00N	3	88	20	143	.3	17	19	1059	4.37	21	5	ND	1	128	2	2	2	109	2.19	.116	6	24	1.54	47	.20	2	4.60	.01	.05	2	2
L1+50E 0+75N	4	29	11	59	.1	22	7	445	2.82	11	5	ND	1	63	1	2	2	102	.62	.039	5	41	.88	22	.19	2	2.53	.01	.03	1	2
L1+50E 0+50N	3	30	2	73	.1	26	9	663	2.10	7	5	ND	1	85	1	2	2	61	1.13	.096	5	15	.59	19	.11	2	1.88	.01	.03	1	1
L1+50E 0+25N	1	52	15	185	.2	103	28	1876	5.48	5	5	ND	1	119	1	4	2	98	1.22	.041	3	189	3.18	23	.16	2	4.93	.01	.03	1	2
L3+00E 15+00N	1	69	50	419	.5	26	10	427	2.96	13	5	ND	1	36	4	2	2	80	.67	.033	6	38	.59	32	.15	2	2.52	.01	.02	1	6
L3+00E 14+75N	1	37	59	199	.2	25	19	2028	7.31	8	5	ND	1	30	1	2	2	141	.66	.020	3	40	.67	35	.25	2	2.07	.02	.03	1	4
L3+00E 14+50N	1	8	2	77	.5	3	1	64	.12	2	5	ND	1	30	1	3	2	4	.71	.037	2	5	.09	11	.01	9	.11	.02	.04	1	1
L3+00E 14+25N	1	60	39	48	.7	31	9	252	13.24	2	5	2	1	24	1	5	2	261	.25	.016	2	120	.53	13	.62	2	2.25	.02	.02	1	4
L3+00E 14+00N	1	69	45	760	.3	37	12	414	4.13	13	5	ND	1	39	2	2	2	103	.79	.036	4	55	.85	34	.21	4	2.49	.03	.03	1	5
L3+00E 13+75N	1	42	42	196	.1	32	9	309	5.22	13	5	ND	1	30	2	2	2	119	.50	.070	8	54	.62	45	.14	2	5.04	.02	.03	1	7
L3+00E 13+50N	1	70	30	115	.2	40	10	302	6.24	13	5	ND	1	26	1	4	2	158	.40	.025	3	95	.94	32	.28	2	5.17	.01	.02	1	6
L3+00E 13+25N	2	35	67	123	.2	15	6	429	6.51	16	5	ND	1	25	1	4	2	143	.43	.020	3	45	.52	24	.22	2	3.54	.01	.02	2	8
L3+00E 13+00N	2	25	81	127	.3	16	6	416	6.08	14	5	ND	1	28	1	2	6	177	.76	.015	2	39	.33	20	.27	2	1.62	.01	.02	1	3
L3+00E 12+75N	3	22	39	214	.4	6	28	1939	3.35	8	5	ND	1	21	2	2	3	67	.28	.106	4	23	.13	36	.09	6	1.76	.01	.07	1	2
L3+00E 12+50N	1	7	7	140	.2	2	1	128	.20	2	5	ND	1	27	1	2	2	8	.49	.043	2	5	.08	14	.02	5	.11	.01	.07	1	1
L3+00E 12+25N	1	19	30	95	.1	15	5	332	3.23	10	5	ND	1	33	1	2	3	115	.57	.023	4	30	.55	28	.19	2	2.02	.01	.03	1	3
L3+00E 12+00N	1	29	35	121	.1	18	7	356	4.51	16	5	ND	1	36	2	3	4	145	.75	.020	4	33	.52	31	.24	2	1.87	.01	.03	1	3
L3+00E 11+75N	1	6	5	157	.2	3	1	127	.16	2	5	ND	1	39	1	2	2	7	.23	.042	2	6	.17	20	.01	8	.14	.02	.03	1	1
L3+00E 11+25N	1	51	43	121	.1	18	6	321	3.62	14	5	ND	1	26	1	2	2	134	.50	.020	5	40	.53	28	.20	4	3.77	.02	.02	1	7
L3+00E 11+00N	1	27	26	159	.1	13	5	247	4.32	11	5	ND	1	26	1	2	2	141	.59	.017	4	29	.29	25	.23	2	2.64	.01	.02	1	4
L3+00E 10+50N	1	25	31	114	.1	13	7	234	4.72	29	5	ND	1	18	1	3	4	117	.35	.037	3	22	.29	24	.08	2	2.63	.01	.02	1	2
L3+00E 10+25N	1	58	71	474	.3	16	7	765	9.01	26	5	ND	1	25	1	3	2	159	.65	.020	3	46	.35	33	.25	2	3.18	.01	.02	1	4
L3+00E 10+00N	1	49	43	340	.1	12	6	548	7.07	26	5	ND	1	24	1	4	2	145	.66	.024	3	31	.26	22	.22	2	2.49	.01	.02	1	9
L3+00E 9+75N	1	66	31	155	.1	22	10	642	4.70	19	5	ND	1	32	1	4	2	126	.58	.028	5	43	.60	53	.19	2	3.71	.01	.02	1	6
L3+00E 9+50N	2	40	23	129	.2	19	6	462	4.82	20	5	ND	1	25	1	4	2	138	.44	.035	5	44	.48	33	.20	7	3.55	.01	.02	2	4
L3+00E 9+25N	2	45	24	101	.5	18	8	737	7.32	14	5	ND	1	39	1	4	2	152	.66	.027	5	51	.49	45	.26	2	3.69	.02	.03	2	3
L3+00E 9+00N	2	18	20	55	.2	12	3	253	1.71	8	5	ND	1	31	1	4	2	84	.48	.022	4	27	.40	34	.19	3	1.94	.01	.02	2	4
L3+00E 8+75N	2	38	25	114	.4	15	5	396	4.42	14	5	ND	1	27	1	2	5	137	.43	.029	4	36	.38	35	.21	2	2.92	.02	.02	1	6
L3+00E 8+50N	1	61	29	220	.1	23	9	516	5.22	12	5	ND	1	28	1	2	2	126	.46	.027	4	47	.60	40	.26	2	3.96	.02	.03	1	8
L3+00E 8+25N	1	41	24	294	.1	23	18	900	5.42	22	5	ND	2	26	1	5	2	125	.48	.029	4	38	.38	79	.18	2	4.44	.02	.02	1	6
L3+00E 8+00N	1	44	30	152	.1	17	7	494	5.14	22	5	ND	1	28	1	2	3	133	.55	.025	5	38	.41	40	.23	2	3.52	.02	.02	2	6
L3+00E 7+75N	1	43	17	141	.4	20	7	682	4.03	15	5	ND	1	28	1	2	2	134	.39	.045	5	33	.57	34	.18	2	2.94	.01	.02	1	4
L3+00E 7+50N	4	54	20	184	.2	36	6	346	4.55	53	5	ND	1	24	1	4	2	175	.51	.029	7	48	.48	37	.19	3	4.96	.02	.02	1	7
L3+00E 7+25N	2	48	28	219	.7	35	6	346	3.41	24	5	ND	1	20	1	8	2	197	.49	.041	5	52	.53	36	.16	5	5.45	.02	.03	1	5
STD C/AU-S	17	59	41	132	6.7	68	31	1013	4.21	42	18	8	37	48	19	14	23	59	.45	.099	38	56	.85	176	.07	39	1.92	.06	.13	11	49

Daiwan Engineering Ltd. PROJECT WIN FILE # 90-0207

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPM
L3+00E 7+00N	4	49	19	123	.3	20	6	341	3.89	18	5	ND	1	24	1	3	2	122	.50	.038	5	46	.67	34	.17	3	4.36	.01	.02	4	7
L3+00E 6+75N	5	27	19	120	.4	14	4	266	4.35	19	5	ND	1	18	1	4	3	146	.35	.019	5	47	.44	31	.16	2	3.75	.01	.02	2	6
L3+00E 6+50N	6	30	22	74	.3	16	5	284	4.61	12	5	ND	1	26	1	2	3	146	.45	.021	5	40	.51	20	.22	2	3.36	.01	.02	1	5
L3+00E 6+25N	5	37	39	110	.6	23	7	398	4.70	20	5	ND	1	28	1	5	2	128	.57	.031	5	40	.64	31	.19	5	3.64	.01	.02	2	9
L3+00E 6+00N	4	21	19	57	.1	12	6	263	7.16	7	5	ND	1	29	1	2	2	174	.50	.014	4	36	.51	20	.32	2	1.82	.01	.02	1	3
L3+00E 5+75N	1	7	2	95	.7	2	1	34	.39	2	5	ND	1	43	1	2	2	9	.60	.054	2	6	.15	31	.02	6	.26	.01	.03	1	1
L3+00E 5+50N	5	12	21	70	1.4	7	1	50	3.56	4	5	ND	1	27	1	3	2	76	1.13	.049	4	14	.08	34	.13	5	1.29	.01	.03	1	5
L3+00E 5+25N	3	40	26	112	.2	23	7	474	4.01	17	5	ND	1	31	1	6	2	97	.72	.049	6	30	.79	39	.17	2	3.52	.01	.03	2	1
L3+00E 5+00N	3	12	13	59	.7	5	1	33	.90	2	5	ND	1	19	1	2	2	35	.52	.053	3	14	.05	37	.09	3	1.00	.01	.02	1	2
L3+00E 4+75N	5	37	33	200	.1	31	11	539	3.29	12	5	ND	1	40	1	2	2	107	.98	.051	6	36	.95	47	.18	3	2.96	.02	.02	1	2
L3+00E 4+50N	5	38	19	170	.3	27	9	409	2.72	11	5	ND	1	32	1	2	2	100	.76	.041	6	40	.73	40	.18	6	3.49	.01	.02	1	4
L3+00E 4+25N	4	46	15	310	.1	36	11	1399	3.67	17	5	ND	1	47	1	2	2	77	1.50	.079	7	29	.77	55	.13	2	2.76	.01	.02	1	7
L3+00E 4+00N	1	8	4	145	.3	4	1	59	.34	2	5	ND	1	47	1	2	2	11	.50	.043	2	7	.29	29	.02	7	.36	.01	.03	1	1
L3+00E 3+50N	3	18	20	61	.1	10	4	280	8.05	22	5	ND	1	18	2	2	2	137	.45	.027	4	20	.47	26	.17	2	1.88	.01	.03	1	1
L3+00E 3+25N	3	31	19	64	.1	23	6	373	2.83	15	5	ND	1	33	1	5	2	108	.57	.036	5	34	.89	30	.22	5	2.93	.01	.02	1	3
L3+00E 3+00N	2	26	20	58	.1	14	7	364	3.56	13	5	ND	1	35	1	3	2	103	.67	.025	5	26	.87	30	.24	2	2.89	.01	.02	1	1
L3+00E 2+75N	2	46	22	88	.1	20	8	428	3.49	12	5	ND	1	44	1	5	2	112	.68	.041	5	29	.99	89	.22	2	3.83	.03	.03	1	2
L3+00E 2+50N	2	19	11	79	1.6	3	2	79	1.92	4	5	ND	1	15	1	6	7	29	.17	.104	5	9	.13	24	.04	8	1.90	.01	.03	2	3
L3+00E 2+25N	3	29	11	52	.1	10	4	234	4.11	20	5	ND	1	17	1	2	3	112	.28	.026	4	29	.61	20	.20	3	2.91	.01	.02	1	11
L3+00E 1+75N	1	9	2	109	.1	4	2	40	.46	2	5	ND	1	66	1	2	2	9	.58	.037	2	5	.18	59	.02	7	.64	.01	.02	1	3
L3+00E 1+50N	5	22	23	77	.2	13	6	233	3.65	14	5	ND	1	33	1	4	2	94	.35	.043	5	32	.65	25	.16	2	2.18	.01	.03	1	7
L3+00E 1+25N	5	54	20	95	.1	17	15	648	4.35	30	5	ND	1	66	1	3	2	101	2.06	.103	8	19	.88	39	.16	2	3.59	.02	.04	1	2
L3+00E 1+00N	1	37	10	80	.1	7	1	23	.32	2	5	ND	1	9	1	2	3	13	.09	.168	5	10	.04	15	.01	7	2.50	.01	.01	1	8
L3+00E 0+75N	3	14	11	65	.1	6	2	159	1.65	14	5	ND	1	24	1	2	4	74	.48	.056	5	18	.25	22	.12	2	1.52	.01	.02	1	4
L3+00E 0+50N	2	37	12	101	.1	9	5	199	3.35	10	5	ND	1	23	1	2	8	84	.53	.102	5	11	.52	30	.10	2	2.02	.01	.03	1	1
L3+00E 0+25N	1	4	2	99	.1	1	1	17	.10	2	5	ND	1	32	1	2	6	3	.68	.052	2	2	.13	11	.01	9	.14	.02	.03	1	1
L3+00E 0+00N	3	20	10	39	.1	59	10	278	3.35	10	5	ND	1	30	1	2	5	108	.83	.024	3	103	1.34	25	.22	3	2.13	.03	.03	3	1
L4+50E 11+75N	3	32	22	76	.1	18	5	312	3.14	10	5	ND	1	27	1	3	2	113	.79	.027	3	37	.56	30	.20	2	2.84	.01	.02	1	1
L4+50E 11+50N	3	17	45	85	.1	13	5	295	2.66	8	5	ND	1	32	1	2	2	145	.80	.021	4	35	.54	39	.20	2	2.55	.01	.02	1	1
L4+50E 11+25N	2	11	21	88	.2	7	18	1940	3.18	5	5	ND	1	35	1	2	2	87	1.10	.033	4	20	.21	35	.11	2	1.44	.01	.03	1	2
L4+50E 11+00N	3	18	42	201	.1	17	7	442	4.77	10	5	ND	1	39	1	2	2	151	.94	.026	4	32	.56	33	.20	5	2.03	.01	.02	1	2
L4+50E 10+50N	1	12	2	248	.1	4	3	318	.79	2	5	ND	1	32	4	2	2	25	1.40	.034	2	8	.11	18	.03	2	.47	.01	.02	1	1
L4+50E 10+25N	2	36	10	3185	.8	7	1	1766	.48	4	5	ND	1	102	44	2	2	17	5.93	.073	2	7	.08	39	.01	11	.45	.01	.02	1	1
L4+50E 10+00N	1	10	2	1290	.4	4	1	71	.06	2	5	ND	1	85	13	2	2	2	4.52	.033	2	8	.05	17	.01	10	.07	.01	.01	1	1
L4+50E 9+75N	1	3	2	135	.3	1	1	186	.15	2	5	ND	1	21	1	2	2	3	.84	.045	2	3	.09	7	.01	3	.05	.01	.03	1	3
L4+50E 9+50N	3	16	17	69	.2	8	4	512	4.26	7	5	ND	1	31	1	2	2	123	1.38	.020	3	19	.18	18	.16	2	1.46	.01	.01	1	1
STD C/AU-8	20	58	40	132	7.6	73	31	1025	4.29	42	17	8	36	47	20	15	20	60	.51	.092	36	56	.94	173	.07	39	2.00	.06	.14	12	48

Daiwan Engineering Ltd. I JECT WIN FILE # 90-0207

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Au*
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM
L4+50E 9+25N	3	25	23	64	1.6	13	5	361	3.81	6	5	ND	1	38	1	6	2	129	.72	.025	4	22	.40	21	.19	4	1.35	.02	.03	1	6
L4+50E 9+00N	3	29	37	238	1.4	12	10	17720	3.84	2	5	ND	1	33	4	6	2	98	.79	.080	5	27	.38	73	.09	2	2.50	.02	.05	1	8
L4+50E 8+75N	3	34	19	86	.5	13	8	1570	4.68	6	5	ND	1	35	2	7	2	119	.83	.036	4	29	.40	19	.20	5	2.99	.01	.03	1	6
L4+50E 8+50N	2	17	23	95	.5	11	7	2080	4.59	9	5	ND	1	70	1	7	2	82	1.74	.038	4	15	.46	19	.16	7	2.04	.01	.02	1	5
L4+50E 8+25N	1	8	7	90	.4	4	1	296	.97	2	5	ND	1	45	1	2	7	11	.61	.039	2	4	.19	15	.03	3	.35	.01	.02	1	5
L4+50E 8+00N	1	82	40	687	1.2	7	18	38234	16.21	167	5	ND	5	15	16	2	4	32	5.24	.040	4	6	.11	77	.03	2	1.30	.01	.01	3	37
L4+50E 7+75N	4	42	29	129	.8	20	8	1061	4.67	13	5	ND	2	31	1	7	7	135	.67	.026	5	32	.54	53	.14	8	2.62	.01	.05	1	5
L4+50E 7+50N	3	71	72	388	.4	17	8	1199	4.77	38	5	ND	1	45	2	9	8	140	.94	.062	8	22	.82	85	.16	7	4.36	.03	.05	1	6
L4+50E 7+25N	3	35	27	91	.4	16	5	428	3.33	13	5	ND	1	33	1	7	2	115	.72	.030	6	28	.54	30	.16	8	2.38	.01	.03	1	2
L4+50E 7+00N	1	30	29	133	.3	8	4	815	2.11	5	5	ND	2	44	1	4	2	36	1.30	.036	16	10	.32	55	.06	6	2.53	.02	.06	1	3
L4+50E 6+75N	1	5	9	64	.4	1	1	105	1.41	2	5	ND	1	7	1	5	4	22	.12	.018	8	6	.09	23	.02	4	1.87	.01	.05	1	3
L4+50E 6+50N	3	18	11	59	.3	6	4	314	3.79	8	5	ND	1	38	1	4	9	141	.70	.021	3	17	.25	20	.22	2	1.25	.02	.03	1	2
L4+50E 6+25N	2	12	9	43	.6	11	4	394	2.10	12	5	ND	1	60	1	5	2	120	.92	.025	3	18	.18	16	.19	7	.77	.01	.02	3	5
L4+50E 6+00N	3	45	21	100	.3	23	8	493	3.41	9	5	ND	1	42	1	7	6	93	.93	.069	7	28	.97	45	.18	3	3.70	.02	.04	2	4
L4+50E 5+75N	3	66	17	127	.1	31	11	618	4.22	8	5	ND	1	51	1	5	2	107	1.02	.063	6	38	1.17	49	.20	3	3.41	.02	.04	1	6
L4+50E 5+50N	3	40	22	120	.2	26	7	533	3.44	13	5	ND	1	37	1	3	6	97	.88	.061	6	32	1.06	50	.18	3	3.10	.02	.04	1	3
L4+50E 5+25N	4	47	30	315	.6	84	21	4605	4.92	140	5	ND	1	57	3	9	2	137	1.60	.079	10	133	1.42	59	.16	4	4.66	.02	.06	1	4
L4+50E 5+00N	3	66	26	390	.6	45	12	1773	4.12	38	5	ND	1	59	5	6	2	126	2.35	.124	10	55	.93	113	.14	6	3.40	.04	.06	1	3
L4+50E 4+75N	5	23	42	95	.4	25	7	918	3.59	12	5	ND	1	59	1	3	2	103	1.12	.033	5	37	.63	34	.19	3	1.75	.02	.03	1	1
L4+50E 4+50N	22	25	27	66	.4	22	9	793	4.98	2	5	ND	1	46	1	2	2	127	1.14	.030	6	61	.46	34	.22	6	2.50	.02	.02	1	3
L4+50E 4+25N	3	20	21	94	.1	13	7	1375	2.83	7	5	ND	1	43	1	2	2	61	.96	.046	9	16	.44	40	.09	4	1.97	.02	.06	1	3
L4+50E 4+00N	4	54	37	155	.7	26	15	1564	3.77	15	6	ND	1	51	1	7	2	88	1.16	.057	9	24	.75	50	.15	2	3.53	.02	.03	1	1
L4+50E 3+75N	5	22	88	137	.8	14	24	15263	6.41	10	5	ND	1	48	1	4	2	209	1.87	.145	6	27	.22	43	.14	6	2.38	.01	.04	1	3
L4+50E 3+50N	2	66	22	151	.3	25	16	1180	3.73	13	5	ND	1	79	1	6	2	89	2.13	.075	7	24	.97	74	.14	6	4.60	.05	.04	1	5
L4+50E 3+25N	2	72	12	129	.1	30	22	996	3.82	43	5	ND	1	94	1	6	2	77	2.95	.063	5	17	.95	76	.12	6	5.42	.04	.04	1	7
L4+50E 3+00N	1	33	50	218	.4	20	14	4081	7.61	47	6	ND	2	40	2	6	2	64	5.58	.066	5	20	.68	35	.12	2	3.26	.02	.03	3	22
L4+50E 2+75N	4	52	21	160	1.5	33	19	1979	6.59	27	6	ND	3	35	2	7	6	120	4.06	.082	6	40	.73	33	.19	2	3.88	.01	.02	3	4
L4+50E 2+50N	3	51	16	83	.3	17	6	690	3.36	18	5	ND	1	43	1	3	15	78	1.08	.066	7	17	.47	86	.17	5	2.34	.05	.03	1	1
L4+50E 2+25N	2	17	19	57	.2	7	2	178	.79	2	5	ND	1	23	1	3	2	42	.45	.080	4	13	.09	51	.08	2	1.39	.01	.03	1	1
L4+50E 2+00N	2	10	14	47	.4	4	1	86	.50	2	5	ND	1	24	1	2	4	32	.28	.059	4	13	.08	37	.10	2	1.04	.01	.03	2	1
L4+50E 1+75N	2	14	13	48	.1	7	4	304	3.76	2	5	ND	1	37	1	3	2	102	.58	.040	5	14	.84	32	.27	4	2.49	.02	.03	1	2
L4+50E 1+50N	3	20	15	42	.7	9	36	14947	16.06	52	5	ND	2	24	4	5	2	119	.41	.061	5	12	.45	53	.08	11	2.12	.02	.04	1	1
L4+50E 1+25N	3	36	15	35	.1	17	5	316	5.73	17	5	ND	1	35	1	2	2	178	.57	.026	6	25	.34	40	.36	4	2.10	.02	.02	1	1
L4+50E 1+00N	1	9	2	82	.5	3	4	451	2.35	2	5	ND	1	14	1	3	2	20	.15	.096	2	7	.07	28	.02	3	.91	.01	.03	1	1
L4+50E 0+75N	1	11	15	103	.2	1	1	81	.98	2	5	ND	1	18	1	2	2	18	.15	.093	2	5	.07	26	.03	2	.41	.01	.06	1	3
L4+50E 0+50N	1	6	5	83	.1	1	1	52	3.11	2	5	ND	1	6	1	2	2	23	.05	.099	2	4	.03	24	.01	2	.44	.01	.03	1	2
STD C/AU-S	18	62	44	131	7.6	68	30	1025	4.18	41	18	7	36	45	20	15	18	58	.51	.091	35	53	.94	172	.07	40	1.93	.06	.14	12	47

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SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	U PPM	Al <sup>2+</sup> PPM
L4+50E 0+25N	1	2	2	53	.1	2	1	35	1.31	2	5	ND	1	4	1	2	2	6	.05	.053	2	3	.02	10	.01	2	.20	.01	.02	1	1
L4+50E 0+00N	1	8	8	85	.1	1	1	51	.55	2	5	ND	1	14	1	2	2	15	.10	.057	2	3	.05	31	.06	2	.41	.02	.04	1	2
L6+00E 12+00N	2	18	16	65	.1	13	5	304	4.18	5	5	ND	1	27	1	2	4	76	1.12	.022	3	19	.56	22	.16	6	1.30	.02	.03	1	2
L6+00E 11+75N	2	19	13	35	.3	7	5	341	5.80	10	5	ND	1	16	1	2	8	114	2.37	.010	3	22	.24	15	.23	5	1.72	.01	.02	1	3
L6+00E 11+25N	4	47	36	548	.4	25	15	1715	4.94	28	5	ND	1	52	5	2	2	113	1.94	.042	7	29	.67	120	.11	2	3.21	.01	.05	1	4
L6+00E 11+00N	1	36	11	71	.1	11	5	213	5.94	11	5	ND	1	24	2	2	2	138	.77	.019	4	38	.40	24	.23	2	3.63	.02	.02	1	5
L6+00E 10+75N	2	50	34	96	.7	13	6	361	5.13	9	5	ND	1	37	2	2	2	128	.90	.015	4	46	.55	30	.26	2	4.37	.02	.03	3	4
L6+00E 10+50N	2	57	23	115	.2	17	7	396	4.28	15	5	ND	1	31	2	6	2	112	1.10	.056	4	45	.66	46	.19	3	5.03	.02	.02	1	3
L6+00E 10+25N	1	11	6	139	1.4	4	1	43	.35	2	5	ND	1	38	1	2	2	8	.27	.023	2	9	.21	15	.02	3	.30	.03	.02	1	4
L6+00E 9+75N	1	49	48	173	.1	15	4	259	1.60	5	5	ND	1	48	1	2	2	73	1.01	.027	4	26	.70	64	.20	2	2.58	.03	.04	1	6
L6+00E 9+50N	1	53	71	172	.5	1	2	29	.39	2	5	ND	1	23	4	2	3	19	.50	.041	3	7	.04	29	.02	3	.84	.02	.02	1	5
L6+00E 9+25N	2	17	81	205	.1	7	3	545	1.45	6	5	ND	1	50	1	2	2	48	1.07	.017	4	14	.56	35	.12	4	1.79	.01	.03	1	3
L6+00E 9+00N	6	31	82	104	1.2	7	2	80	3.16	10	5	ND	1	26	2	2	6	89	.46	.066	8	22	.10	52	.04	3	2.18	.01	.03	1	4
L6+00E 8+75N	1	17	18	116	.9	5	3	142	.46	2	5	ND	1	26	1	2	2	15	.43	.086	5	6	.08	41	.02	2	1.13	.02	.03	1	4
L6+00E 8+50N	8	54	29	139	.1	19	6	424	3.79	12	5	ND	1	41	1	3	2	142	1.31	.039	7	39	.68	39	.18	2	4.13	.01	.02	1	2
L6+00E 8+00N	5	32	24	87	1.1	12	16	876	4.47	7	5	ND	1	26	1	2	3	156	.69	.039	5	27	.34	20	.21	2	2.39	.01	.03	1	4
L6+00E 7+75N	9	63	14	62	.5	11	7	513	6.02	18	5	ND	1	49	2	6	7	188	1.70	.042	6	38	.29	41	.22	9	3.29	.02	.03	3	5
L6+00E 7+50N	3	53	20	100	.4	21	30	3442	3.93	12	5	ND	1	41	2	3	2	115	1.30	.049	5	33	.83	38	.19	6	2.58	.02	.03	1	5
L6+00E 7+25N	2	61	20	98	.1	16	8	470	4.51	15	5	ND	1	29	1	2	7	116	.75	.039	5	37	.75	39	.22	7	4.20	.03	.03	1	2
L6+00E 7+00N	2	78	14	136	.3	25	15	1154	4.76	17	5	ND	1	43	1	2	2	118	1.05	.045	5	35	.85	86	.22	6	3.54	.04	.04	1	5
L6+00E 6+75N	3	38	27	90	.3	13	16	1415	4.60	10	5	ND	1	49	1	2	2	125	.83	.039	5	21	.86	33	.20	2	2.33	.02	.03	1	3
L6+00E 6+50N	3	43	20	108	.1	18	12	1028	4.84	13	5	ND	1	26	1	3	2	118	.66	.028	7	35	.47	34	.17	7	3.11	.02	.03	1	3
L6+00E 6+25N	1	20	20	99	1.0	6	12	1433	1.98	8	5	ND	1	27	1	2	4	43	.36	.069	9	8	.19	35	.05	5	1.71	.01	.04	1	3
L6+00E 6+00N	5	61	75	256	.8	23	28	6413	7.68	29	5	ND	1	28	2	6	2	226	2.35	.107	5	43	.32	27	.12	11	3.30	.01	.03	2	15
L6+00E 5+75N	3	32	22	78	.3	9	9	656	4.86	15	5	ND	1	22	1	2	6	181	.45	.049	5	20	.34	25	.21	8	2.29	.01	.03	1	4
L6+00E 5+50N	8	71	29	381	.9	46	16	1877	5.70	31	5	ND	1	34	1	8	6	352	.92	.062	5	57	.44	43	.19	5	3.44	.01	.02	3	2
L6+00E 5+25N	3	42	19	110	.3	14	28	6253	5.93	20	5	ND	1	57	1	2	2	176	1.03	.050	7	26	.56	30	.24	3	3.18	.01	.02	1	5
L6+00E 5+00N	2	36	36	89	1.6	8	12	3798	3.91	13	5	ND	1	45	1	5	2	99	.77	.064	5	19	.41	35	.15	6	2.77	.01	.03	1	2
L6+00E 4+75N	5	53	21	67	.1	22	7	1278	5.48	30	5	ND	1	41	1	2	2	277	.70	.053	2	59	.69	25	.24	2	1.79	.02	.02	2	4
L6+00E 4+50N	4	38	32	86	.2	18	5	508	2.92	14	5	ND	1	36	1	3	2	108	.77	.079	6	76	.44	43	.17	2	4.93	.01	.02	1	6
L6+00E 4+25N	3	24	67	117	.6	12	76	17894	7.22	16	5	ND	1	27	1	2	2	115	.50	.129	5	68	.19	72	.09	7	2.60	.01	.04	2	6
L6+00E 4+00N	7	15	106	92	.8	19	7	760	2.31	19	5	ND	1	48	1	4	2	99	.80	.055	5	74	.32	50	.15	4	2.23	.01	.04	1	2
L6+00E 3+75N	14	48	71	638	.1	20	12	1722	6.50	28	5	ND	1	28	1	7	4	143	.79	.059	10	55	.83	55	.22	8	6.07	.01	.01	4	6
L6+00E 3+50N	3	22	25	61	.1	7	3	198	1.79	15	5	ND	1	28	1	7	4	81	.56	.025	6	25	.29	38	.19	6	3.03	.01	.02	1	4
L6+00E 3+25N	7	30	43	141	.1	15	8	1056	5.21	13	5	ND	1	29	1	2	2	154	.92	.062	6	34	.50	38	.21	5	3.26	.01	.02	1	5
L6+00E 3+00N	2	7	12	65	.7	5	2	426	1.65	6	5	ND	1	25	1	2	2	100	2.27	.020	6	13	.04	17	.09	2	.72	.01	.01	1	14
STD C/AU-8	18	63	38	132	7.5	67	31	1013	4.12	41	22	8	36	48	19	17	24	57	.48	.090	34	56	.94	173	.06	41	1.98	.06	.14	13	52

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe X	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca X	P X	La PPM	Cr PPM	Mg X	Ba PPM	Ti X	B PPM	Al X	Mn X	K X	W PPM	Au* PPB
L6+00E 2+75N	1	3	4	145	.1	2	1	61	.23	2	5	ND	1	33	1	2	2	6	.75	.058	2	5	.08	19	.01	8	.13	.03	.04	1	6
L6+00E 2+50N	1	8	6	101	.2	2	1	76	.54	2	5	ND	1	17	1	2	2	19	.21	.082	2	5	.04	20	.03	5	.48	.03	.05	1	3
L6+00E 2+25N	1	2	9	137	.1	4	1	272	.18	2	5	ND	1	19	1	2	2	3	.13	.076	2	2	.09	14	.01	8	.09	.02	.06	1	4
L6+00E 2+00N	1	4	8	98	.2	1	1	29	.26	2	5	ND	1	15	1	2	2	4	.11	.066	2	2	.04	17	.01	2	.20	.01	.02	1	2
L6+00E 1+75N	1	2	4	67	.7	2	1	11	.92	2	5	ND	1	4	1	2	2	24	.04	.064	2	6	.02	13	.04	3	.98	.01	.02	1	7
L6+00E 1+50N	1	15	14	75	.4	7	3	152	2.47	2	5	ND	1	19	1	2	2	62	.22	.038	2	9	.23	30	.14	6	.96	.01	.04	1	7
L6+00E 1+25N	1	6	9	158	.8	2	1	56	1.07	2	5	ND	1	13	1	2	7	32	.13	.053	3	6	.14	24	.06	4	.79	.01	.01	1	5
L6+00E 1+00N	2	52	21	71	.1	18	6	277	2.36	8	5	ND	1	34	1	2	3	105	.37	.018	5	35	.83	65	.20	2	3.57	.01	.01	1	10
L6+00E 0+75N	1	2	10	101	.3	3	1	20	.61	2	5	ND	1	18	1	2	2	3	.06	.056	2	2	.10	83	.01	4	.15	.02	.03	1	4
L6+00E 0+50N	1	4	11	155	.1	2	1	25	.22	2	5	ND	1	23	1	2	2	3	.11	.043	2	2	.09	29	.01	2	.11	.02	.02	1	4
L6+00E 0+25N	1	5	7	120	.1	4	1	37	.42	2	5	ND	1	11	1	2	2	9	.07	.029	2	4	.09	23	.02	2	.29	.01	.01	1	2
L6+00E 0+00N	1	1	5	150	.1	4	1	26	.42	2	5	ND	1	12	1	2	3	2	.10	.050	2	2	.06	12	.01	2	.19	.02	.02	1	4
L7+50E 5+25N	3	72	23	128	.8	25	15	1389	5.36	35	5	ND	1	22	1	5	2	153	.34	.081	5	39	.64	31	.15	5	3.55	.01	.03	1	10
L7+50E 5+00N	4	51	16	124	.9	17	13	989	5.14	40	5	ND	1	27	1	2	8	194	.37	.054	3	31	.47	30	.14	6	2.05	.01	.03	1	9
L7+50E 4+75N	4	90	28	130	.4	17	7	542	4.49	25	5	ND	1	26	2	2	5	137	.39	.078	4	29	.53	54	.14	2	3.30	.02	.03	1	3
L7+50E 4+50N	6	52	26	137	3.2	20	6	372	5.90	26	5	ND	1	22	2	2	2	189	.23	.126	5	38	.28	57	.10	7	2.40	.01	.05	2	5
L7+50E 4+25N	17	46	20	186	1.6	22	6	237	5.64	52	5	ND	1	14	2	3	2	393	.13	.055	3	43	.16	60	.26	5	1.99	.01	.03	1	5
L7+50E 4+00N	3	50	21	116	1.2	26	10	549	5.22	28	5	ND	1	23	1	2	2	123	.36	.041	4	46	.79	41	.17	6	2.62	.02	.03	1	7
L7+50E 3+75N	1	32	11	86	2.8	22	4	61	2.04	3	5	ND	1	19	1	3	2	17	.23	.142	7	11	.04	83	.02	2	2.06	.01	.04	1	1
L7+50E 3+50N	1	10	13	172	.5	3	1	51	.38	2	5	ND	1	29	1	2	2	7	.41	.066	2	4	.12	16	.01	6	.25	.02	.02	1	5
L7+50E 3+25N	3	59	20	145	.2	59	7	281	5.37	38	5	ND	1	19	1	2	2	155	.30	.038	4	98	1.00	43	.15	2	2.50	.02	.02	1	4
L7+50E 3+00N	3	22	16	108	.6	10	1	63	1.74	5	5	ND	1	9	1	2	2	36	.12	.147	3	15	.07	34	.02	2	.97	.02	.06	1	3
L7+50E 2+75N	2	16	7	91	1.0	7	1	21	1.35	3	5	ND	1	7	1	3	6	35	.06	.183	4	9	.06	28	.02	5	.99	.01	.04	1	6
L7+50E 2+50N	4	21	14	100	.9	5	2	47	2.65	8	7	ND	1	13	1	2	8	48	.17	.105	4	21	.08	21	.04	3	1.50	.01	.03	4	5
L7+50E 2+25N	4	29	23	71	.6	13	4	236	3.19	16	5	ND	1	18	1	2	2	124	.30	.027	3	24	.63	22	.19	2	2.20	.01	.02	1	5
L7+50E 2+00N	1	10	7	196	.2	3	2	108	.75	2	5	ND	1	41	1	2	5	16	.36	.064	2	4	.15	66	.02	2	.49	.02	.06	1	4
L7+50E 1+75N	1	5	10	133	.7	3	1	41	.67	3	6	2	1	13	1	3	2	12	.16	.060	2	5	.05	24	.02	8	.33	.01	.03	2	6
L7+50E 1+50N	1	2	5	146	.2	5	1	17	.44	2	5	ND	1	7	1	2	5	11	.05	.070	2	6	.05	20	.02	2	.34	.01	.02	1	4
L7+50E 1+25N	1	1	8	50	.1	4	1	4	.09	2	5	ND	1	10	1	2	6	3	.03	.047	2	4	.06	13	.01	4	.13	.01	.01	1	4
L7+50E 1+00N	1	3	2	118	.1	3	1	16	.05	2	5	ND	1	57	1	2	4	1	.64	.037	2	3	.17	3	.01	2	.06	.02	.03	1	1
L7+50E 0+75N	2	24	18	92	.3	14	4	183	2.18	6	5	ND	1	16	1	2	6	97	.42	.038	5	21	.46	20	.14	5	1.83	.01	.01	1	6
L7+50E 0+50N	1	57	20	167	.1	27	10	830	3.59	11	5	ND	1	31	1	4	3	80	.46	.033	3	35	.68	95	.18	2	3.16	.01	.02	1	4
L7+50E 0+25N	1	4	2	126	.4	3	1	20	.31	2	5	ND	1	10	1	3	6	3	.03	.044	2	3	.08	17	.01	2	.10	.01	.02	1	4
L7+50E 0+00N	1	27	5	181	.1	10	4	395	2.05	2	5	ND	1	21	1	2	6	42	.24	.032	2	16	.22	34	.08	3	.82	.01	.01	1	2
L9+00E 10+75N	2	49	22	71	.1	18	7	287	3.34	16	5	ND	2	19	1	2	2	102	.41	.021	4	29	.67	15	.18	2	2.32	.01	.03	1	5
L9+00E 10+50N	3	31	47	110	.3	8	143	4596	6.50	4	5	ND	1	19	1	4	10	72	.31	.038	3	25	.27	24	.09	10	1.77	.01	.03	1	8
STD C/AU-S	18	59	45	132	7.1	70	31	1021	4.27	42	17	8	36	45	19	16	20	58	.51	.098	35	56	.93	172	.07	37	2.04	.06	.14	13	51

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Air PPM
L9+00E 10+25N	1	4	9	107	.1	4	1	107	.19	2	5	ND	1	25	1	2	2	4	1.16	.041	2	3	.11	10	.01	7	.13	.01	.03	1	2
L9+00E 10+00N	2	11	13	75	.4	9	10	280	4.83	14	5	ND	1	36	1	2	8	94	1.61	.045	2	11	.17	25	.09	2	1.12	.01	.03	1	7
L9+00E 9+75N	2	35	27	67	.3	11	9	402	5.14	10	5	ND	1	32	1	6	7	77	.62	.045	6	15	.96	14	.16	5	4.09	.01	.02	1	4
L9+00E 9+50N	2	17	28	51	.3	6	5	210	6.31	2	5	ND	1	21	1	4	3	79	.53	.051	3	12	.20	24	.15	6	1.68	.01	.02	2	2
L9+00E 9+25N	3	57	46	118	.1	27	12	459	6.25	7	5	ND	1	27	2	6	2	160	1.15	.034	4	51	.85	39	.26	3	3.99	.01	.02	3	2
L9+00E 9+00N	1	8	5	120	.4	3	2	51	.29	2	5	ND	1	55	1	2	3	6	1.74	.086	2	3	.10	8	.01	11	.18	.01	.07	1	2
L9+00E 8+75N	3	42	47	107	.1	15	7	296	6.21	16	5	ND	1	27	1	4	13	115	.85	.086	3	37	.53	30	.18	5	4.08	.01	.02	1	5
L9+00E 8+50N	4	30	51	129	.7	14	11	593	5.41	19	5	ND	1	26	1	8	8	164	1.44	.051	4	33	.39	25	.22	10	3.88	.01	.02	8	2
L9+00E 8+25N	3	48	65	185	.2	21	10	481	4.43	9	5	ND	1	33	1	7	2	113	.97	.042	4	38	.67	38	.16	4	3.21	.01	.02	2	2
L9+00E 8+00N	1	7	2	111	.8	4	1	60	.30	2	5	ND	1	25	1	2	2	8	.77	.052	2	5	.13	7	.01	3	.22	.01	.03	1	1
L9+00E 7+75N	2	40	81	300	.7	41	14	1894	4.83	181	5	ND	1	41	3	9	5	119	3.04	.092	7	42	.89	50	.12	10	4.32	.01	.04	5	6
L9+00E 7+50N	2	19	25	120	2.8	10	3	257	2.35	8	5	ND	1	39	1	2	3	85	.81	.042	2	22	.41	32	.12	4	1.51	.01	.02	1	2
L9+00E 7+00N	4	60	41	168	.6	22	8	745	4.77	32	5	ND	1	29	2	5	2	145	.91	.082	4	40	.67	34	.15	5	3.17	.01	.03	2	8
L9+00E 6+75N	2	42	46	313	.9	24	14	8005	4.95	38	5	ND	1	33	3	6	2	112	1.38	.113	5	32	.34	49	.09	4	4.50	.01	.03	5	3
L9+00E 6+50N	1	9	10	116	.2	5	1	332	.25	2	5	ND	1	57	1	2	4	6	.30	.053	2	4	.23	16	.01	6	.27	.01	.02	1	2
L9+00E 6+25N	4	11	18	63	.1	10	1	352	2.03	6	5	ND	1	33	1	2	2	110	1.03	.035	3	25	.17	15	.16	2	1.19	.01	.02	3	1
L9+00E 6+00N	4	23	17	100	1.3	10	4	464	3.03	13	5	ND	1	34	1	4	7	149	.73	.069	3	22	.19	35	.14	9	1.24	.01	.04	1	10
L9+00E 5+75N	1	15	14	166	1.5	7	1	299	.52	2	5	ND	1	45	1	2	2	21	1.14	.129	2	7	.15	47	.02	7	.43	.01	.05	1	2
L9+00E 5+50N	5	41	34	322	.5	39	9	1772	4.51	21	5	ND	1	35	2	4	2	196	1.22	.079	4	31	.69	34	.15	2	3.23	.01	.03	2	8
L9+00E 5+25N	1	8	2	212	2.9	6	1	210	.37	2	5	ND	1	39	1	2	2	12	.46	.099	2	5	.15	17	.01	4	.35	.01	.04	1	2
L9+00E 5+00N	13	34	27	85	1.1	16	5	416	3.99	24	5	ND	1	30	1	2	6	195	1.12	.035	3	39	.12	22	.18	6	1.76	.01	.02	1	3
L9+00E 4+75N	17	55	12	465	2.4	41	66	10883	2.62	21	5	ND	1	26	9	2	2	88	.89	.190	9	88	.24	91	.07	11	9.23	.01	.02	2	1
L9+00E 4+50N	7	34	31	213	1.3	23	28	2676	4.21	19	5	ND	1	30	2	9	2	103	.67	.085	5	42	.61	36	.12	2	3.99	.01	.03	2	1
L9+00E 4+25N	3	66	32	412	.4	48	11	1311	3.29	14	5	ND	1	46	1	3	2	97	1.41	.088	5	53	.83	57	.12	3	2.69	.01	.02	1	1
L9+00E 4+00N	8	43	43	158	4.7	14	9	291	6.20	7	5	ND	1	20	2	8	2	78	.32	.124	6	31	.11	37	.04	9	3.00	.01	.06	3	2
L9+00E 3+75N	5	16	22	80	.7	8	4	232	3.22	13	5	ND	1	25	1	4	2	89	.42	.035	4	17	.32	22	.14	4	1.23	.01	.03	1	3
L9+00E 3+50N	5	39	19	102	.6	29	6	492	5.18	22	5	ND	1	37	1	4	2	149	.99	.030	4	58	.55	25	.13	9	2.10	.01	.03	3	3
L9+00E 3+25N	1	7	11	127	.4	3	1	105	.18	2	5	ND	1	28	1	2	5	5	.87	.060	2	3	.12	8	.01	9	.13	.01	.03	1	2
L9+00E 3+00N	2	11	8	69	2.1	6	1	236	1.16	3	5	ND	1	33	1	2	5	33	.59	.043	3	8	.11	53	.05	7	.60	.01	.06	1	1
L9+00E 2+75N	3	48	31	168	.3	31	11	770	4.17	21	5	ND	1	33	1	2	2	91	.86	.074	6	46	.96	47	.15	8	3.52	.02	.04	2	3
L9+00E 2+50N	1	24	16	176	1.0	17	4	532	2.31	7	5	ND	1	37	1	3	4	56	.87	.077	3	28	.40	41	.09	11	1.07	.01	.05	1	1
L9+00E 2+25N	1	11	10	258	.1	6	2	786	.71	2	5	ND	1	28	1	2	2	15	.96	.085	2	9	.22	53	.03	13	.47	.01	.05	2	4
L9+00E 2+00N	2	19	15	89	.5	9	2	64	2.31	2	5	ND	1	21	1	2	4	35	.34	.120	3	19	.13	53	.03	7	1.41	.01	.05	1	1
L9+00E 1+75N	2	34	10	85	.2	7	7	329	8.39	10	5	ND	1	20	3	4	2	161	.42	.055	4	13	.79	31	.25	2	2.51	.02	.06	1	1
L9+00E 1+50N	3	20	8	117	.1	15	9	514	4.93	7	5	ND	1	31	1	2	2	128	.49	.038	4	18	1.12	24	.19	10	2.61	.01	.03	1	1
L9+00E 1+25N	2	11	14	98	.4	6	7	321	3.43	5	5	ND	1	30	1	2	2	86	.62	.108	5	13	.91	39	.13	6	1.96	.02	.05	1	1
STD C/AU-S	18	62	38	131	7.9	66	31	1023	4.33	41	22	7	35	44	19	16	22	59	.53	.095	35	55	.92	173	.07	38	1.97	.06	.14	13	51

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SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au <sup>4</sup> PPM
L9+00E 1+00N	1	22	10	99	.1	46	3	291	4.39	28	5	ND	1	52	2	2	4	336	2.36	.988	25	78	.67	25	.05	4	1.16	.01	.03	1	5
L9+00E 0+75N	1	7	10	141	.2	6	1	37	.51	2	5	ND	1	14	1	2	2	14	.13	.138	3	11	.06	31	.02	2	.66	.02	.05	1	5
L9+00E 0+50N	3	8	13	123	.4	6	1	44	.50	2	5	ND	1	50	1	2	2	43	.26	.079	3	19	.14	68	.07	3	.48	.02	.03	1	2
L9+00E 0+25N	2	23	19	116	1.0	13	4	164	2.45	12	5	ND	1	35	1	4	2	72	.23	.033	3	19	.39	42	.15	4	1.09	.02	.03	1	15
L9+00E 0+00N	1	6	2	221	.3	2	1	38	.36	2	5	ND	1	25	1	2	2	3	.08	.074	2	2	.13	90	.01	5	.19	.03	.05	1	4
L21+00E 0+00S	2	87	3	43	.1	23	7	146	5.58	8	5	ND	1	24	2	2	2	136	.46	.052	2	114	1.04	22	.24	2	1.87	.05	.05	1	10
L21+00E 0+25S	2	34	5	33	.2	14	8	123	6.90	6	5	ND	2	10	2	3	6	249	.26	.024	2	48	.25	9	.26	4	1.15	.01	.03	1	9
L21+00E 0+50S	1	7	8	57	.3	4	1	37	.34	2	5	ND	1	24	1	2	2	11	.74	.072	2	7	.11	8	.02	5	.12	.01	.04	1	3
L21+00E 0+75S	1	12	6	88	.4	7	1	75	.23	2	5	ND	1	26	1	2	3	8	.65	.106	2	8	.09	10	.01	3	.09	.02	.06	1	4
L21+00E 1+25S	2	11	12	47	.5	3	1	40	2.14	2	5	ND	1	17	1	2	2	98	.55	.042	2	18	.05	12	.07	3	.37	.01	.02	2	9
L21+00E 1+50S	1	11	5	74	.2	1	1	70	.45	2	5	ND	1	20	1	2	2	6	.49	.121	2	3	.06	16	.01	5	.29	.02	.05	1	2
L21+00E 1+75S	1	18	7	74	.2	3	1	11	.28	2	5	ND	1	30	1	2	2	11	1.22	.113	3	3	.05	16	.01	6	.54	.02	.05	1	3
L21+00E 2+00S	3	131	47	128	.8	11	1	99	.72	3	5	ND	1	32	1	2	5	43	1.22	.091	8	37	.35	32	.04	2	2.88	.01	.02	1	9
L21+00E 2+25S	1	26	18	68	.3	5	1	34	.38	2	5	ND	1	19	1	2	4	17	.43	.100	3	23	.06	21	.02	4	.85	.01	.03	1	7
L21+00E 2+50S	1	43	8	40	.6	4	1	6	.20	2	5	ND	1	6	1	2	2	3	.08	.096	4	8	.01	16	.01	2	1.71	.01	.01	1	4
L21+00E 2+75S	1	25	7	31	.1	7	7	158	5.02	4	5	ND	3	10	1	2	2	124	.18	.018	2	29	.38	15	.22	2	.94	.01	.03	1	4
L21+00E 3+00S	1	14	7	61	.9	2	1	29	.28	2	5	ND	1	23	1	2	2	7	.53	.100	2	6	.09	15	.01	2	.37	.02	.05	1	2
L21+00E 3+25S	4	53	20	28	.1	2	6	61	6.16	9	5	ND	1	11	1	2	2	195	.15	.024	2	27	.08	10	.24	2	.91	.01	.03	1	8
L21+00E 3+50S	1	7	6	46	.3	4	1	47	.26	2	5	ND	1	51	1	2	2	8	.45	.041	2	4	.13	45	.01	5	.11	.02	.03	1	1
L21+00E 4+00S	3	17	14	39	.9	4	3	40	5.02	3	5	ND	1	14	1	2	2	119	.17	.063	3	19	.07	21	.13	4	.79	.01	.05	1	9
L22+50E 0+00S	4	45	23	50	.1	12	6	213	5.48	12	5	ND	1	21	2	2	2	172	.45	.017	3	63	.62	16	.26	2	2.15	.01	.03	1	22
L22+50E 0+25S	1	9	2	91	.1	8	3	16	3.50	2	5	ND	1	13	1	2	2	24	.38	.077	2	7	.03	15	.02	2	.34	.01	.03	1	1
L22+50E 0+50S	1	9	2	106	.3	1	7	14	17.57	4	5	ND	2	6	2	2	2	86	.07	.051	2	11	.03	13	.02	2	.42	.01	.02	1	6
L22+50E 0+75S	1	13	8	108	.1	2	1	16	1.15	2	5	ND	1	11	1	2	2	41	.16	.048	2	39	.04	11	.12	2	.38	.01	.03	1	3
L22+50E 1+00S	1	8	2	188	.4	1	1	22	.97	2	5	ND	1	33	1	2	2	6	.57	.066	2	3	.09	22	.01	2	.09	.01	.06	1	1
L22+50E 1+25S	1	5	2	108	.2	3	1	10	.13	2	5	ND	1	47	1	2	2	3	.44	.053	2	6	.19	18	.01	2	.09	.02	.04	1	1
L22+50E 1+50S	1	5	2	147	.1	2	1	22	.19	2	5	ND	1	59	1	2	3	1	.45	.056	2	5	.21	26	.01	4	.06	.02	.04	1	2
L22+50E 1+75S	1	7	3	114	.5	2	2	109	.17	2	5	ND	1	30	1	2	2	3	.51	.091	2	3	.11	15	.01	5	.14	.02	.07	1	2
L22+50E 2+00S	1	5	2	137	.6	4	1	14	.10	2	5	ND	1	30	1	2	2	1	.57	.083	2	4	.09	9	.01	2	.08	.02	.05	1	4
L22+50E 2+25S	1	18	10	90	1.4	2	1	11	.52	2	5	ND	1	9	1	2	2	16	.12	.098	2	5	.04	16	.03	4	.56	.01	.03	1	2
L22+50E 2+50S	2	33	11	28	.1	7	4	81	4.65	8	5	ND	2	11	1	2	2	184	.17	.016	2	36	.17	16	.24	2	.80	.01	.01	1	38
L22+50E 2+75S	1	4	2	70	.1	1	1	15	1.35	2	5	ND	1	15	1	2	2	4	.23	.068	2	3	.05	11	.01	5	.12	.01	.03	1	3
L22+50E 3+25S	6	35	8	47	.3	9	5	297	4.90	6	5	ND	2	11	1	2	2	149	.24	.019	3	22	.52	19	.18	3	1.60	.01	.02	3	16
L22+50E 3+50S	1	32	9	81	.2	9	6	276	2.63	4	5	ND	1	29	1	2	2	46	.55	.056	3	19	.69	36	.11	7	1.13	.02	.02	1	2
L22+50E 3+75S	2	180	46	109	.2	27	17	295	6.14	31	5	ND	2	20	3	2	4	127	.36	.033	4	50	.54	29	.26	3	6.13	.01	.02	1	9
L22+50E 4+00S	1	9	2	135	.8	3	1	28	.37	2	5	ND	1	43	1	2	2	10	.12	.037	2	5	.23	26	.02	7	.21	.02	.03	1	1
STD C/AU-8	18	63	41	132	8.9	68	31	951	4.19	43	18	6	36	44	18	15	19	56	.51	.098	37	55	.90	173	.06	38	1.92	.06	.14	11	53



SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Ag PPM
L22+50E 4+25S	3	76	26	79	4.7	12	7	166	5.19	4	5	ND	1	25	1	2	2	114	.47	.022	2	50	.45	17	.25	2	7.08	.01	.02	1	1
L22+50E 4+50S	1	17	9	112	.4	8	1	36	.96	2	5	ND	1	32	1	2	3	23	.79	.062	2	14	.14	14	.05	7	.65	.01	.05	1	5
L22+50E 4+75S	3	44	20	56	.5	15	10	226	8.47	9	5	ND	1	18	1	2	2	195	.37	.017	3	38	.37	24	.34	2	1.88	.01	.03	1	3
STD C/AU-8	18	98	42	132	7.0	67	31	933	4.31	36	18	7	36	45	19	16	19	57	.50	.089	35	52	.93	172	.06	40	2.07	.06	.13	13	51

Daiwan Engineering Ltd. I JECT WIN FILE # 90-0207

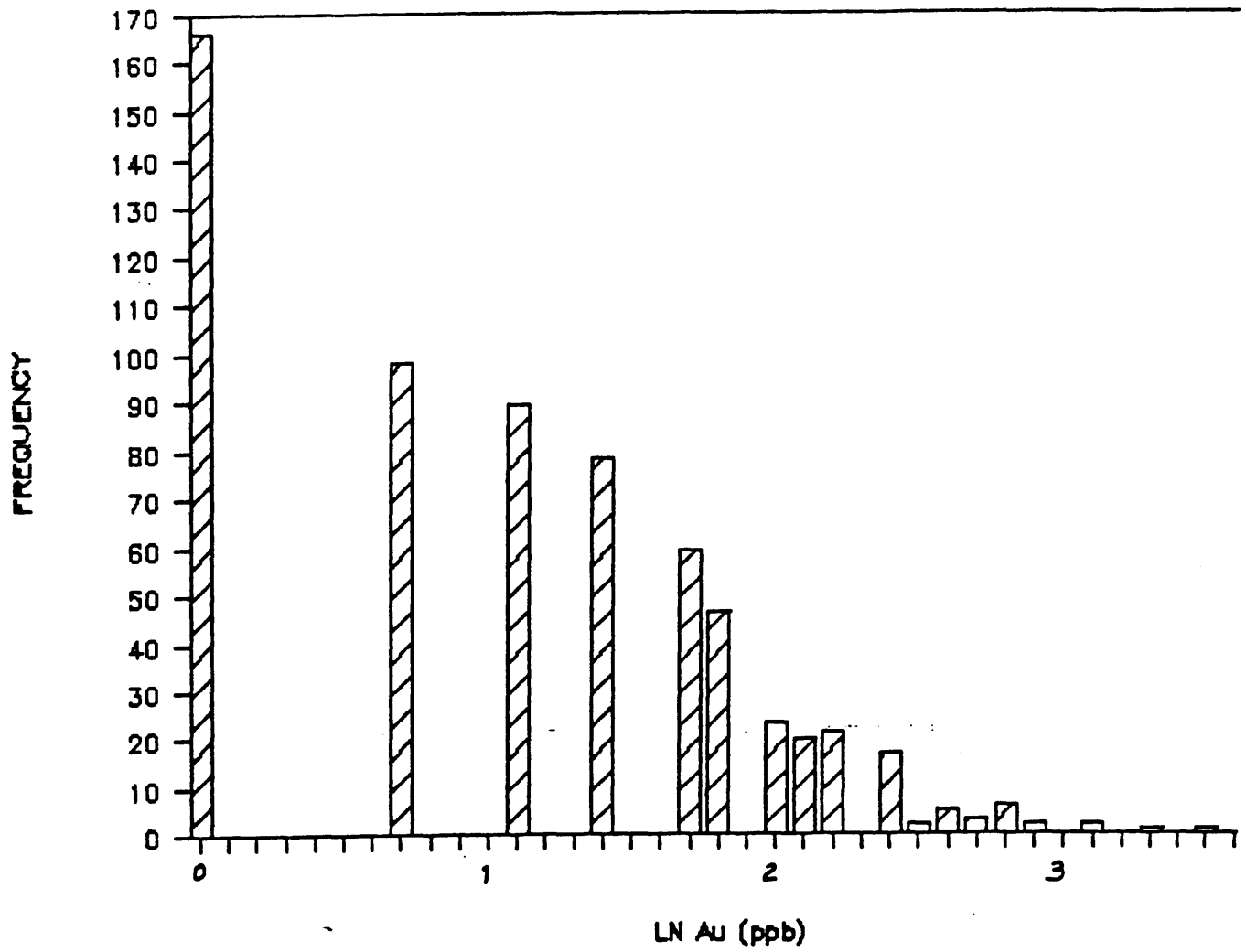
age 12

AMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au PPM
109451	1	1	4	37	.1	2	1	224	.04	6	5	ND	1	674	1	2	2	2	56.53	.024	2	2	.16	2	.01	2	.06	.01	.01	1	44
109452	2	25	33	238	.1	11	5	1081	2.48	22	5	ND	2	51	1	3	2	93	.80	.081	7	20	.34	89	.12	2	1.97	.07	.04	1	11
109453	1	87	108	21523	.3	1	10	18558	2.14	2	5	ND	1	27	154	2	2	1	1.85	.018	2	8	.11	23	.01	2	.05	.01	.01	1	48
109454	1	3	7	736	.1	4	1	3543	1.54	5	5	ND	2	207	7	2	2	14	2.32	.094	9	6	.36	10	.11	2	1.61	.01	.01	1	4
109455	1	45	44	18438	.2	2	11	17952	3.41	9	5	ND	1	19	136	2	2	2	1.02	.032	2	7	.18	13	.01	2	.18	.01	.01	1	1
109456	1	61	13	53	.1	6	10	190	4.08	4	5	ND	1	164	1	2	2	144	2.06	.122	2	5	.57	84	.10	2	3.25	.22	.05	2	5
109457	1	1	2	726	.1	39	13	8148	4.77	11	5	ND	1	2	4	2	2	8	2.51	.019	9	6	.46	150	.01	2	.28	.01	.01	1	3
109458	6	106	9	47	.1	23	5	3488	2.83	9	5	ND	1	62	2	2	2	104	1.44	.028	2	22	.23	77	.07	2	.69	.01	.01	1	7
109459	1	7	16	479	.1	5	3	3241	4.23	20	5	ND	3	60	6	4	2	6	.55	.010	17	5	.18	77	.01	3	1.85	.01	.07	1	6
109460	1	1	2	16	.1	3	1	190	.19	2	5	ND	3	4	1	2	2	1	.08	.016	11	3	.03	42	.01	3	.35	.02	.07	1	1
109461	2	1	2	47	.1	7	1	326	.30	3	5	ND	3	40	1	2	2	1	.63	.014	8	7	.06	166	.02	2	.38	.03	.06	1	5
109462	1	6	4	194	.4	2	10	12796	4.09	41	5	ND	2	83	1	3	2	5	11.66	.014	2	1	.91	11	.01	2	1.04	.01	.01	1	5
109463	1	1	7	23	.1	3	1	1430	1.66	3	5	ND	1	269	1	2	2	5	2.34	.014	11	3	.07	13	.03	2	1.33	.01	.04	1	8
109464	1	1112	5	26	3.5	36	23	136	1.55	2	5	ND	1	148	1	2	2	53	4.73	.020	2	43	.39	7	.18	6	2.13	.03	.01	1	20
109465	2	3	4	18	.1	8	7	220	6.88	67	5	ND	1	1	1	2	2	5	1.21	.011	2	7	.02	2	.01	2	.14	.01	.01	1	23
109466	2	8	5	11	.1	12	6	155	5.26	38	5	ND	1	1	1	2	2	4	.62	.006	2	10	.02	1	.01	2	.08	.01	.01	1	20
109467	1	146	95	16015	1.0	7	8	12236	3.73	14	5	ND	2	38	116	3	2	6	1.83	.013	2	12	.45	48	.01	2	.45	.01	.01	1	7
109468	4	23	239	32993	5.6	1	20	65549	13.32	32	6	ND	5	118	290	2	17	2	3.34	.020	2	16	.33	118	.01	2	.08	.01	.01	1	6
109469	1	9595	485	99999	15.2	2	43	1011	14.39	29	5	ND	1	4	889	2	2	2	.51	.013	2	24	.13	2	.01	2	.23	.01	.01	1	6
109470	1	14174	1597	67785	26.0	2	33	9347	31.07	54	5	ND	2	8	581	9	4	5	.15	.035	2	1	.12	15	.01	2	.35	.01	.01	3	40
109471	1	209	11098	16628	4.1	2	15	15523	1.71	9	5	ND	1	12	116	3	7	7	2.22	.027	2	8	2.24	19	.01	2	.66	.01	.01	1	8
109472	1	1768	133	50235	.8	7	49	752	1.87	10	5	ND	1	202	439	2	2	14	1.62	.063	2	1	.39	3	.07	2	1.34	.01	.01	2	8
109473	1	2012	4512	99999	6.4	3	24	5632	14.40	35	5	ND	1	4	879	2	5	3	.73	.025	2	1	1.19	2	.01	2	.17	.01	.01	3	13
109474	1	11671	103	99999	21.0	6	116	432	14.13	28	5	ND	1	3	1460	2	3	1	.04	.006	2	72	.01	1	.01	2	.04	.01	.01	1	39
109475	1	105	192	1936	.4	8	12	2119	6.88	20	5	ND	1	116	14	2	2	12	4.08	.058	2	7	1.20	31	.04	2	1.53	.01	.04	1	9
109476	6	79	9	652	.1	9	14	395	4.49	7	5	ND	2	99	5	2	2	123	.82	.083	3	10	1.55	102	.20	2	2.44	.09	.07	1	4
109477	1	406	39	18273	2.1	1	15	31130	16.22	336	6	ND	3	46	158	2	3	2	6.72	.017	2	6	.21	20	.01	2	.14	.01	.01	2	49
STD C/AU-R	18	57	36	137	7.0	66	30	1022	3.78	42	22	6	36	47	18	16	21	58	.44	.097	37	55	.87	171	.07	39	1.84	.06	.14	13	530

✓ ASSAY RECOMMENDED

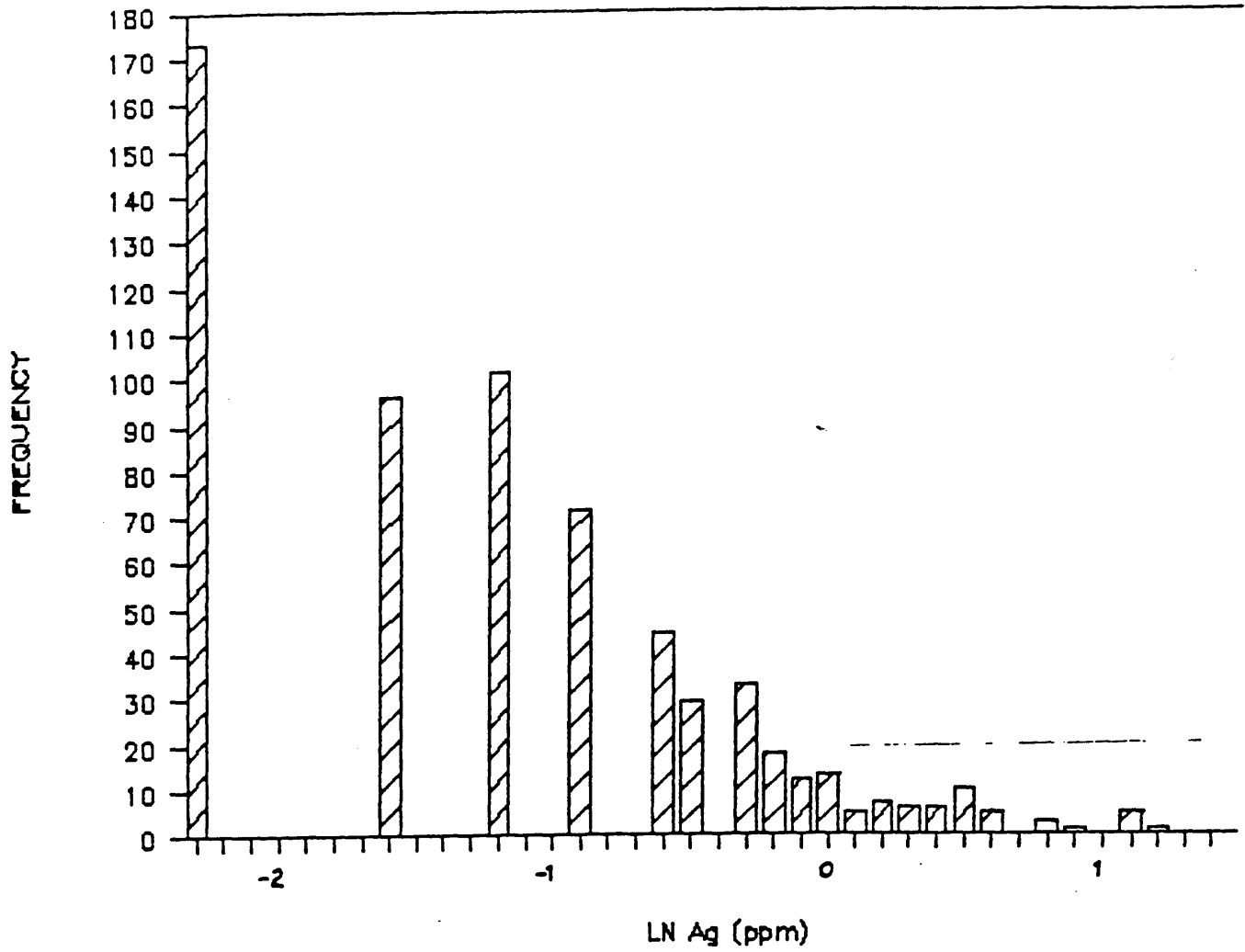
# DAIWAN ENGINEERING LTD.

## AU DISTRIBUTION



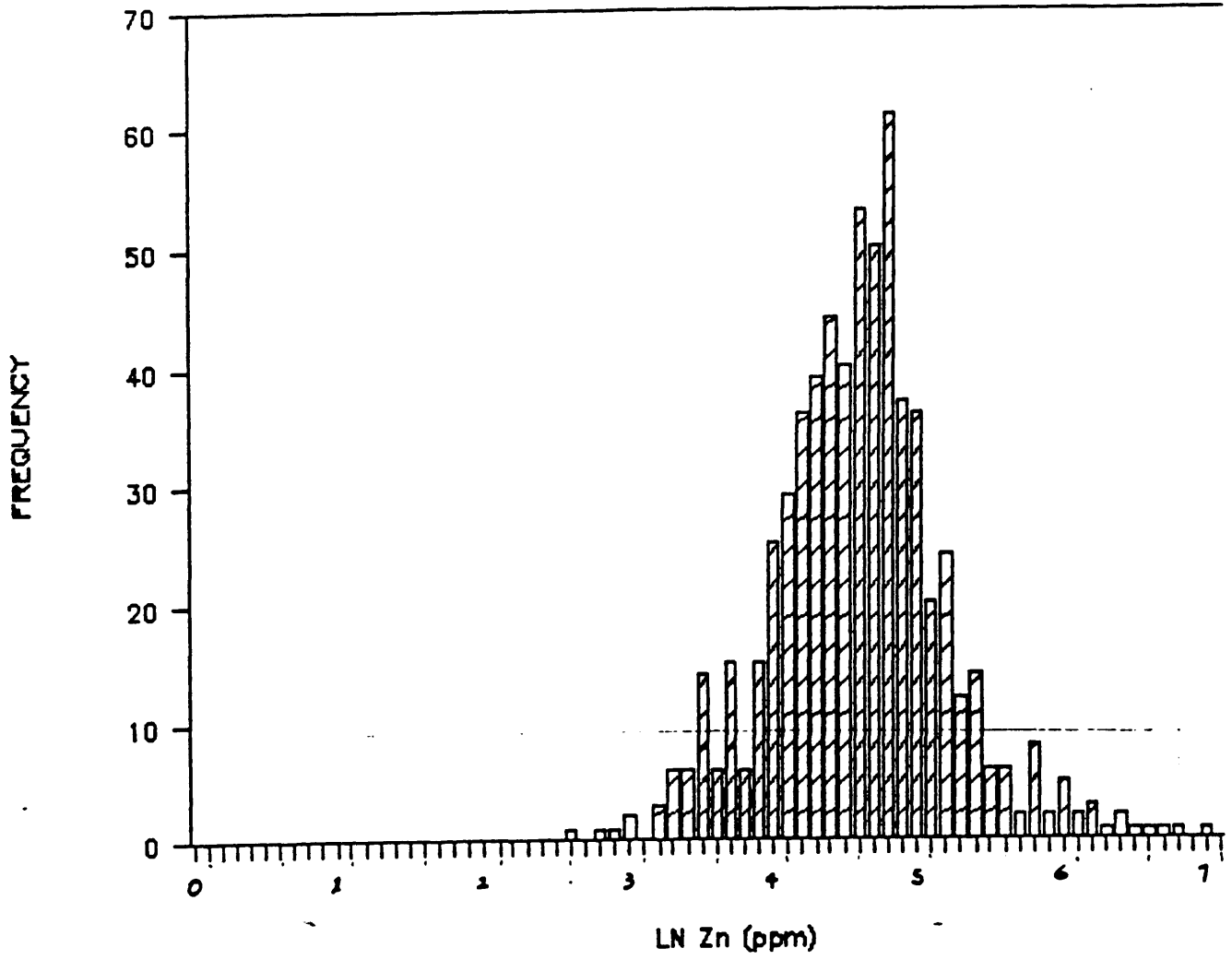
# DAIWAN ENGINEERING LTD.

## Ag DISTRIBUTION



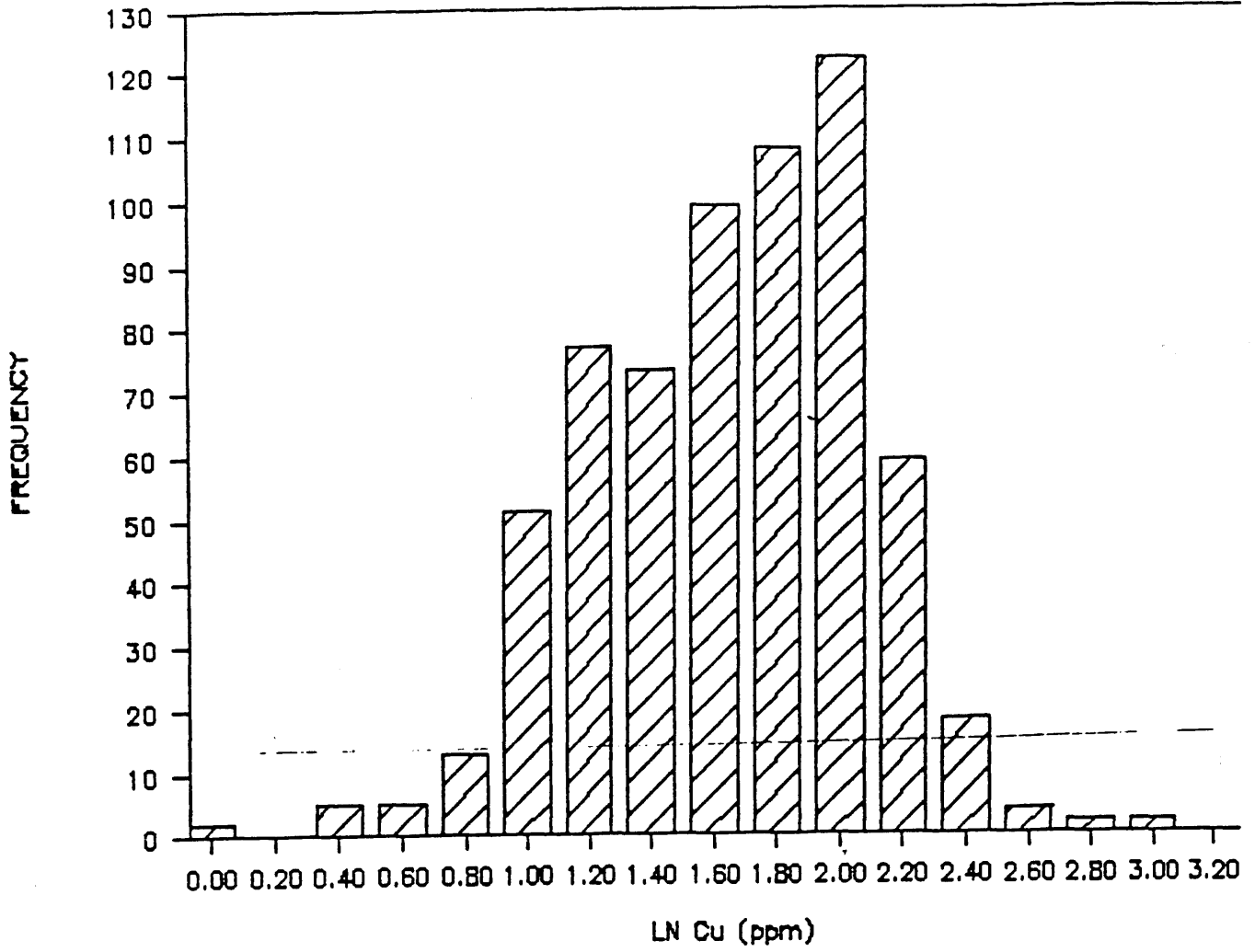
# DAIWAN ENGINEERING LTD.

## Zn DISTRIBUTION



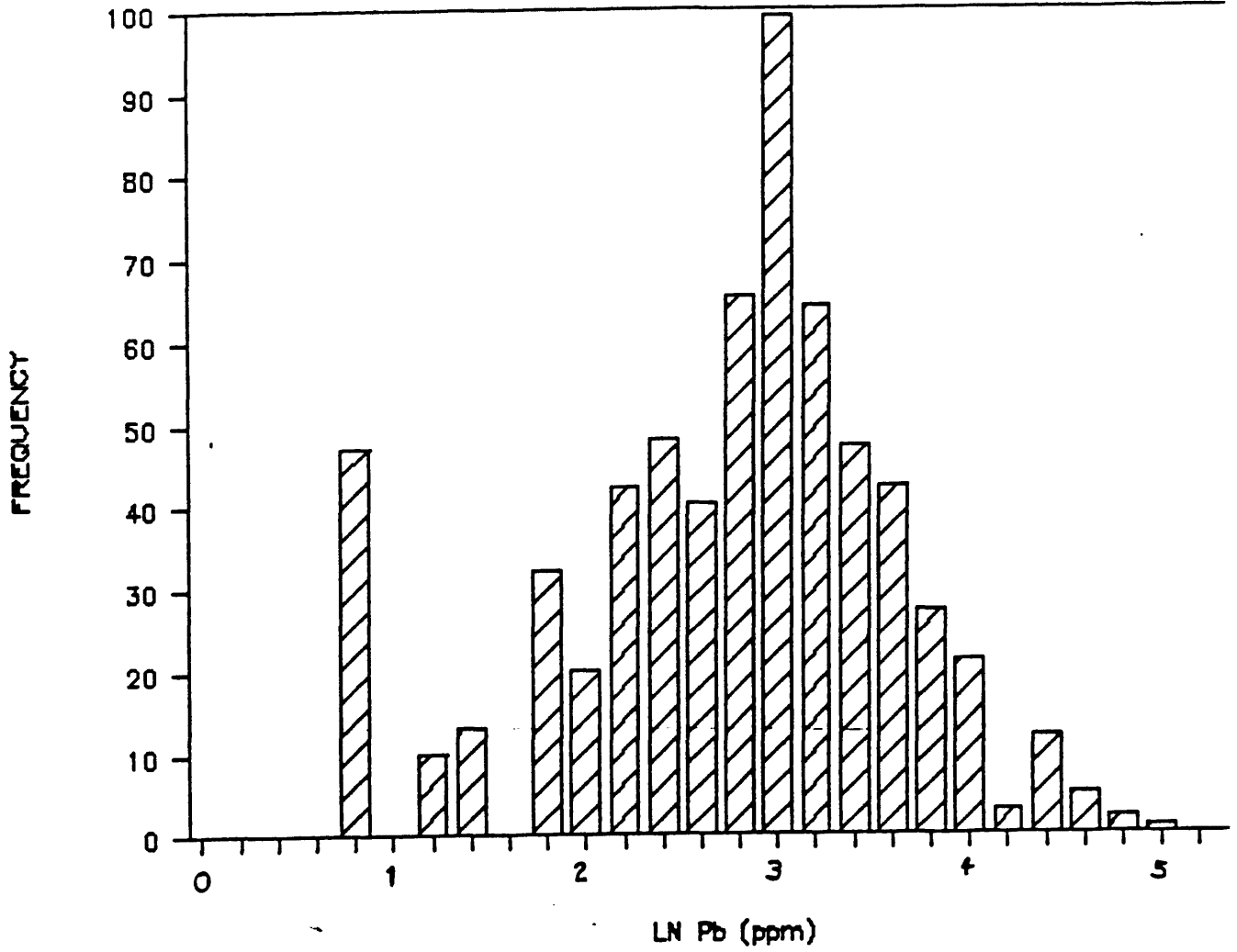
# DAIWAN ENGINEERING LTD.

## Cu DISTRIBUTION



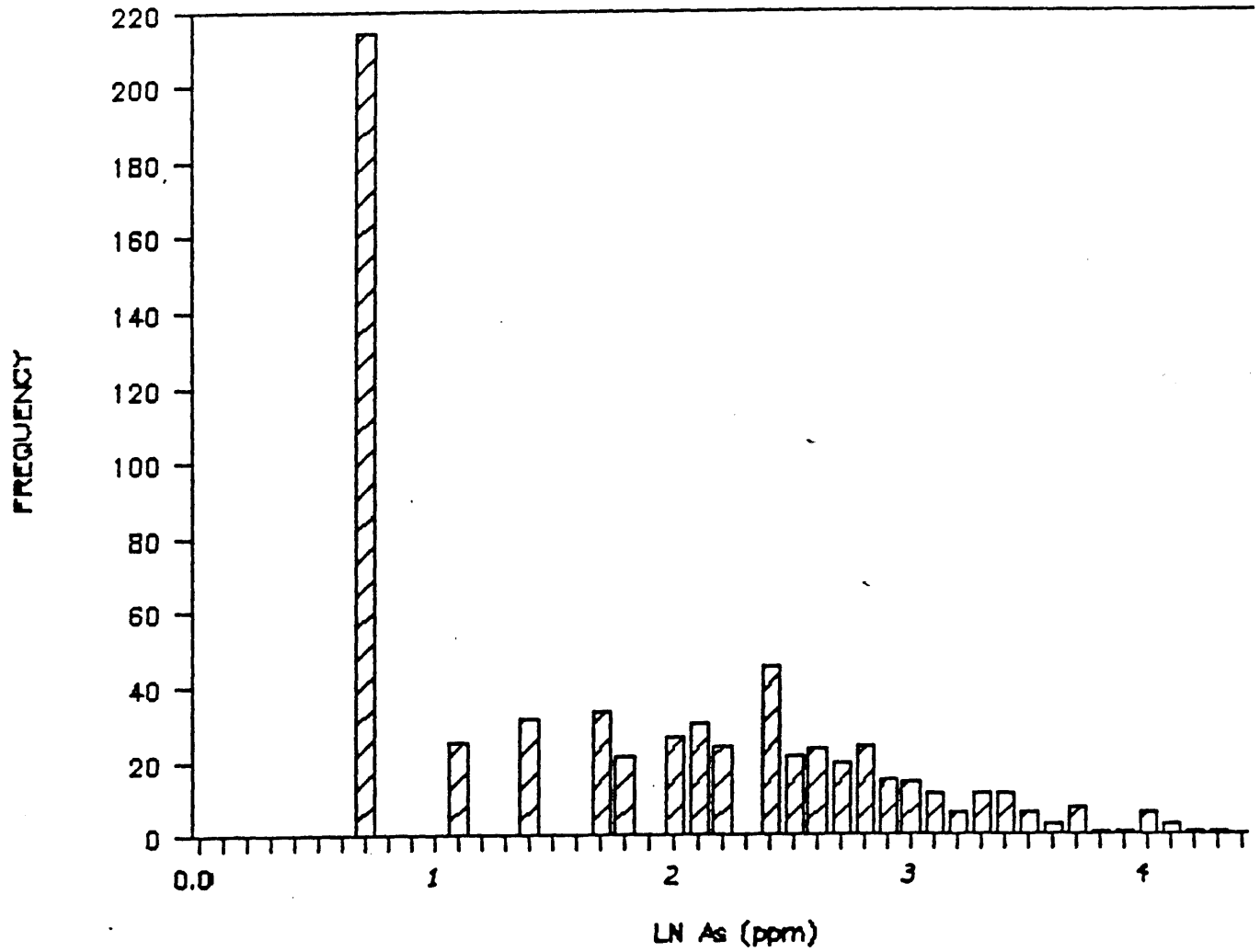
# DAIWAN ENGINEERING LTD.

## Pb DISTRIBUTION



# DAIWAN ENGINEERING LTD.

As DISTRIBUTION





## **APPENDIX 3**

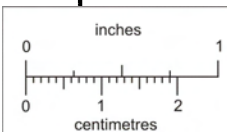
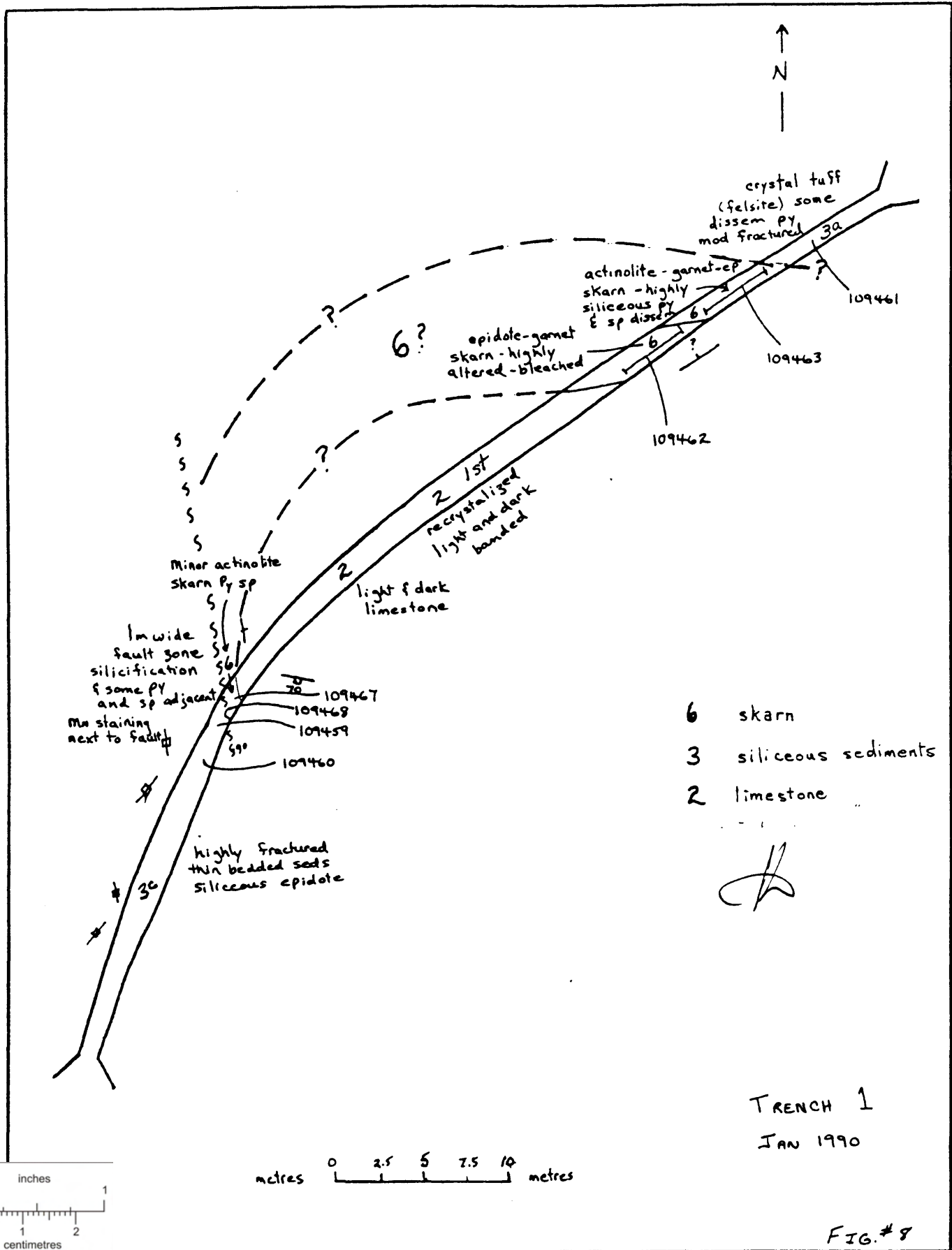
### **Geologist's Sketches**

**Daiwan Engineering Ltd.**

(604) 688-1508, 1030-609 Granville Street, Vancouver, B.C. (604) 688-1508

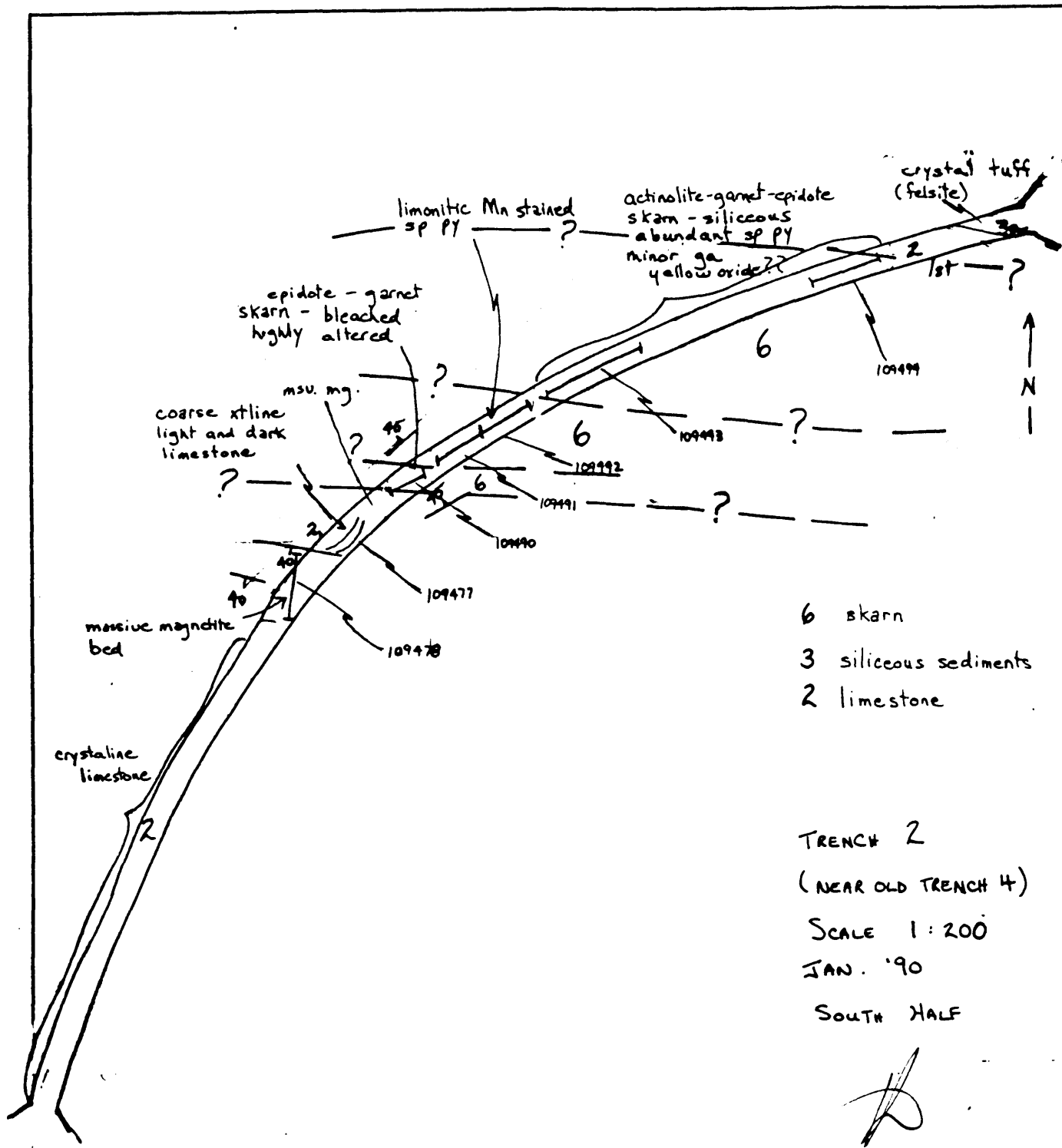
PROPOSED DRILL HOLE TABLE

<u>DDH</u>	<u>Purpose</u>	<u>Dip</u>	<u>Azimuth</u>	<u>Elevation</u>	<u>Length</u>
A	to test limestone at depth for skarn	60°	045°	500m	500-600'
B	to test karmutsen/diorite contact for source of copper anomalies	90°	---	500m	200-300'
C	as 'A'	90°	---	425m	250-400'
D	as 'A'	45°	045°	425m	400-500'
E	as 'A'	45°	045°	460m	400-500'
F	as 'B'	90°	---	400m	200-300'
G	to test semi massive sulphide vein along strike and down dip	45°	310°	370m	200-300'
H	as 'G'	45°	310°	370m	<u>200-300'</u>
				<b>TOTAL</b>	<b>2,350-3,200'</b>



This reference scale bar has been added to the original image. It will scale at the same rate as the image, therefore it can be used as a reference for the original size.

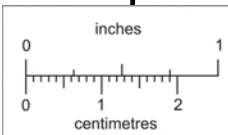




- 6 skarn
- 3 siliceous sediments
- 2 limestone

TRENCH 2  
 (NEAR OLD TRENCH 4)  
 SCALE 1:200  
 JAN. '90  
 SOUTH HALF

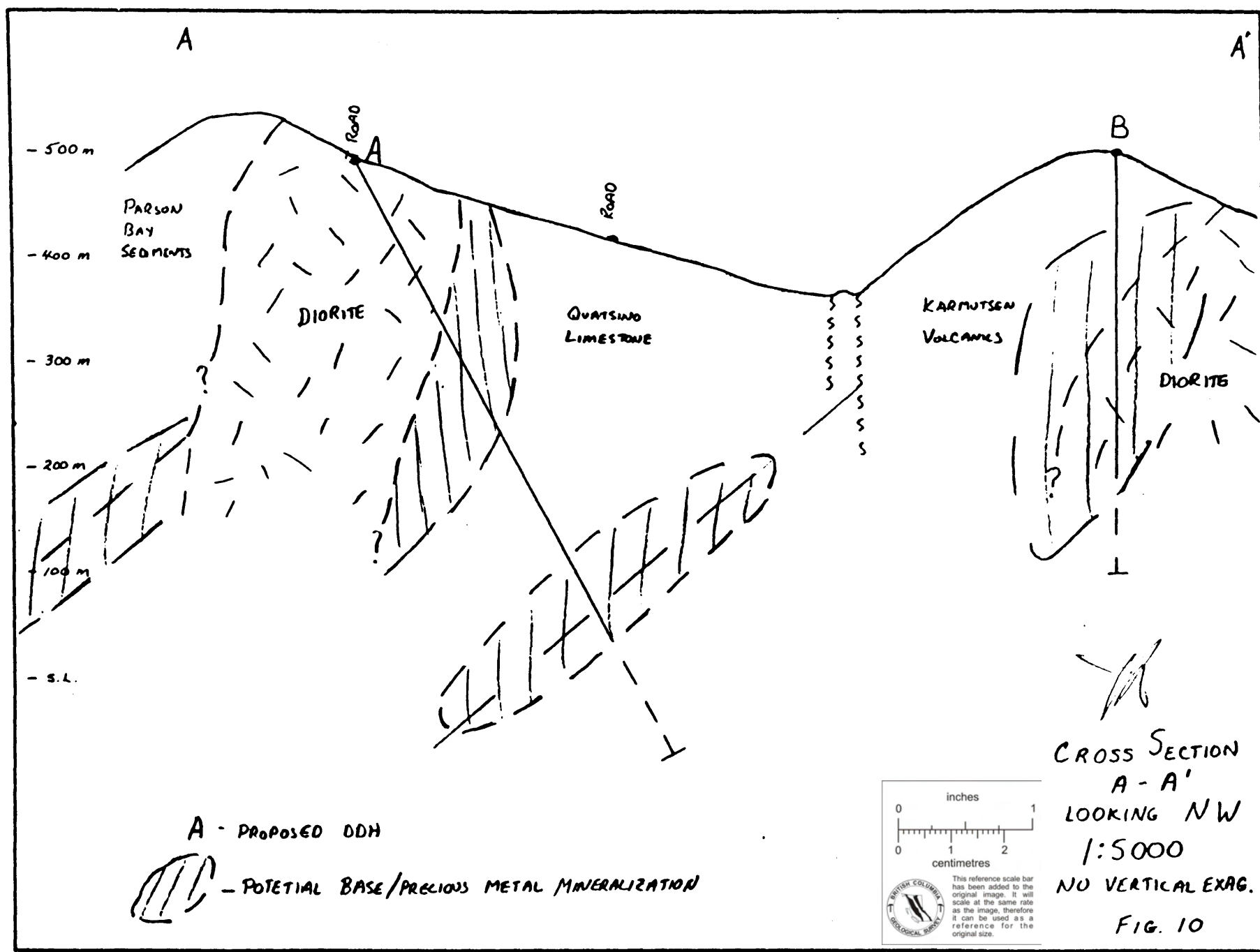
*[Signature]*



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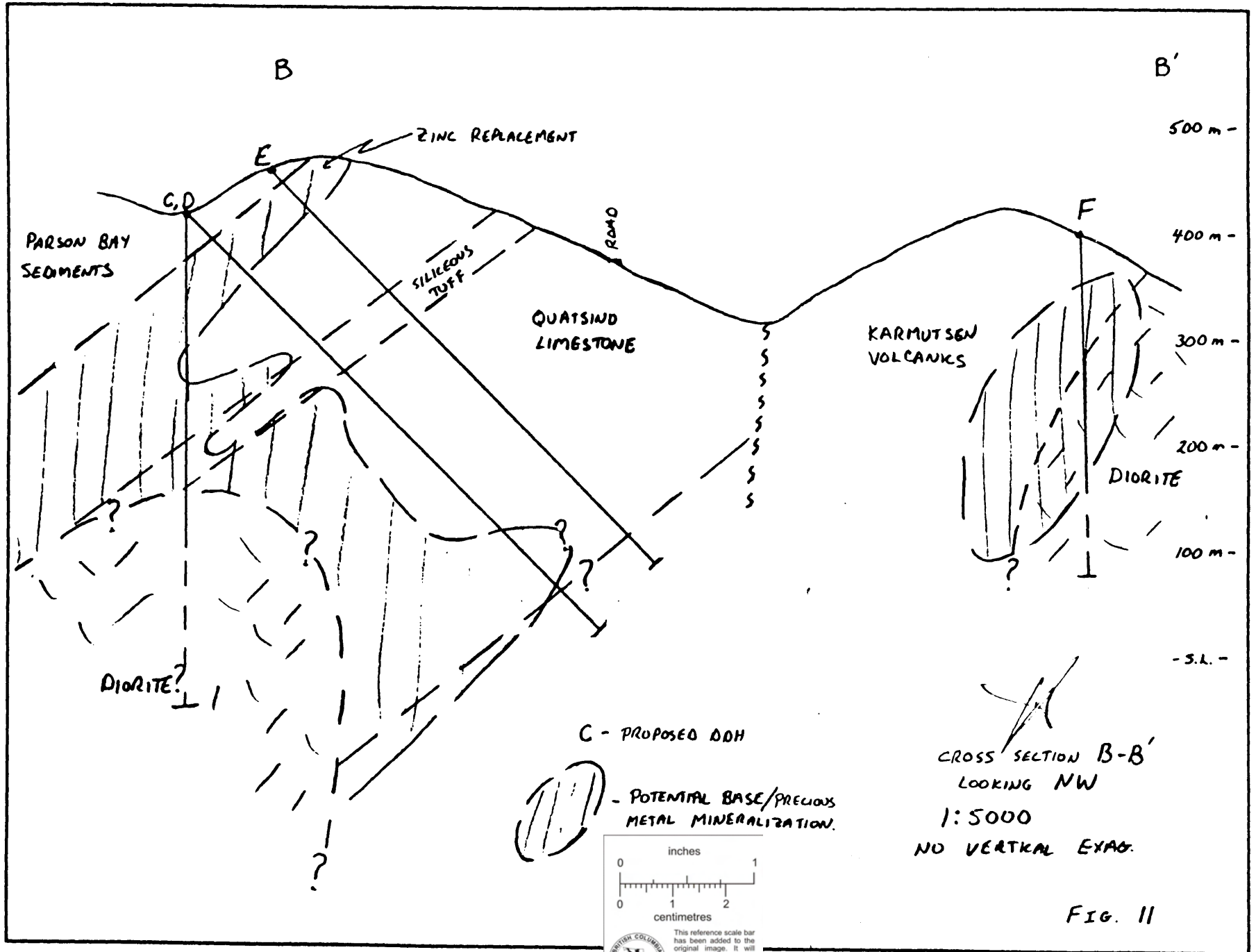
FIG. #9

Daitan Engineering Ltd.  
 1030 - 609 Granville Street, Vancouver, B. C.  
 (604) 688-1508



CROSS SECTION  
 A - A'  
 LOOKING NW  
 1:5000  
 NO VERTICAL EXAG.  
 FIG. 10

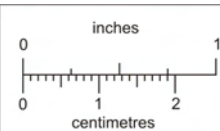
Daiwan Engineering Ltd.  
1030 - 609 Granville Street, Vancouver, B. C.  
(604) 688-1508



C - PROPOSED DDH



- POTENTIAL BASE/PREVIOUS METAL MINERALIZATION.

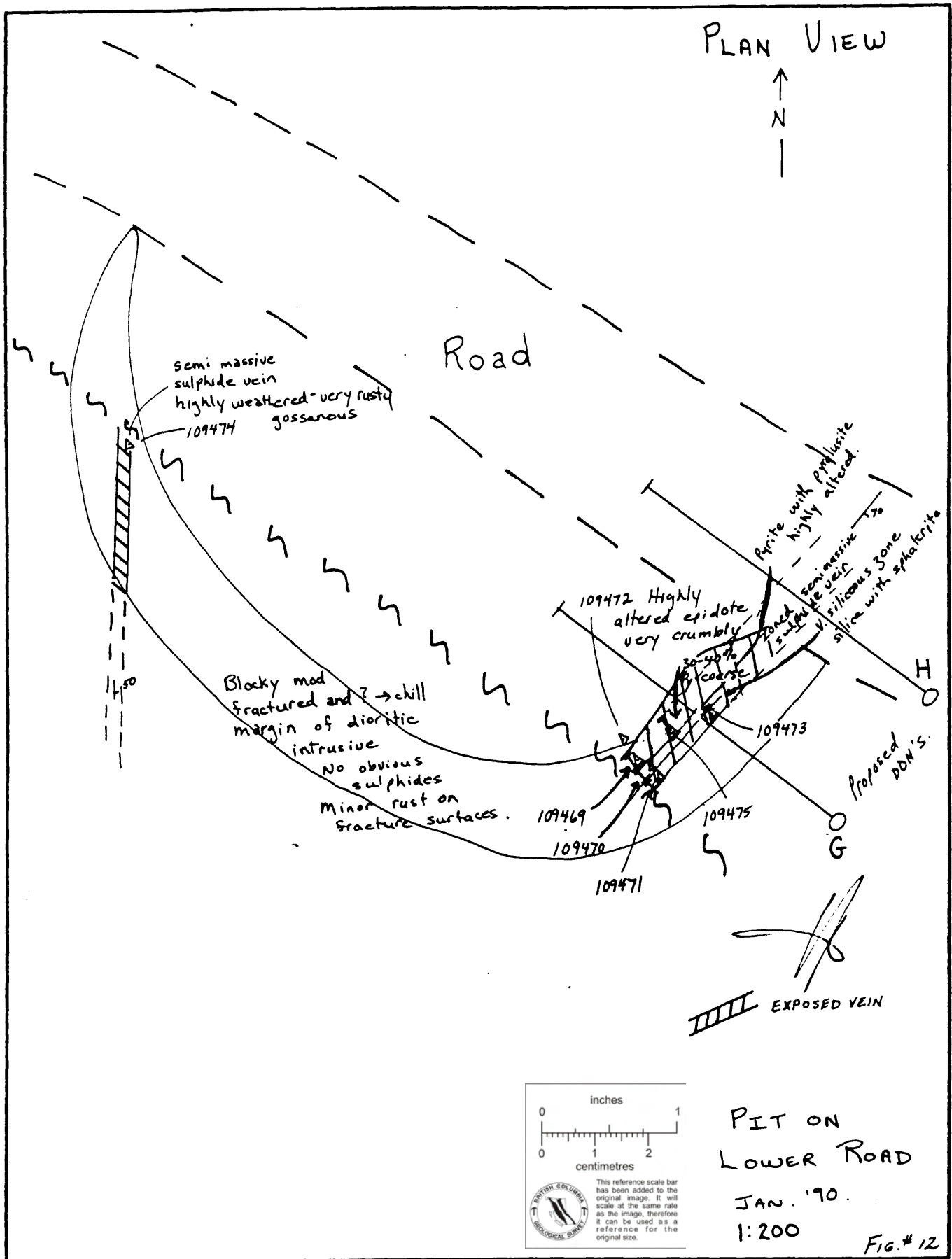


This reference scale bar has been added to the original image. It will scale at the same rate as the image, therefore it can be used as a reference for the original size.

CROSS SECTION B-B'  
LOOKING NW

1:5000  
NO VERTICAL EXAG.

FIG. II



**Daiwan Engineering Ltd.**  
1030 - 609 Granville Street, Vancouver, B.C. V7Y 1G5  
Phone: (604) 688-1508

Reductions of Maps to Accompany

the

**GEOLOGICAL, GEOCHEMICAL AND GEOPHYSICAL  
REPORT  
ON THE  
WIN CLAIM GROUP  
NORTHERN VANCOUVER ISLAND  
BRITISH COLUMBIA, CANADA**

By

Rod W. Husband, B.Sc.

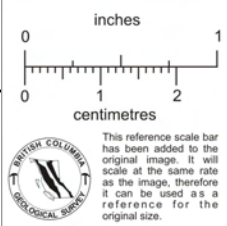
and

Peter G. Dasler, M.Sc., F.G.A.C.

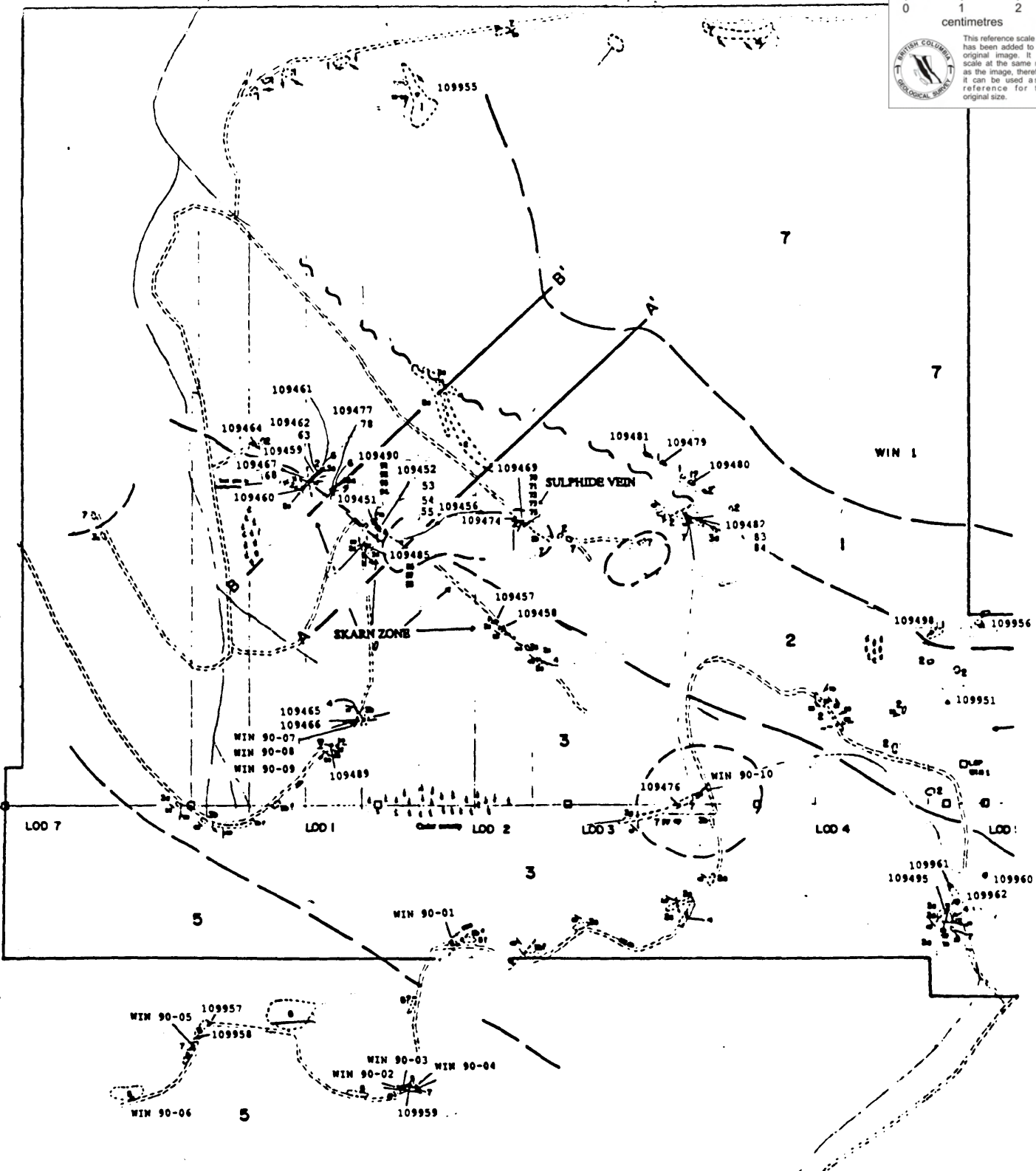
February 16, 1990

Revised September 10, 1990





20+00 N  
16+00 N  
10+00 N  
6+00 N  
Base Line  
6+00 S



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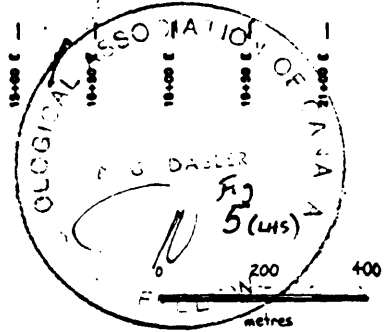
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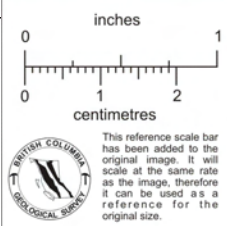
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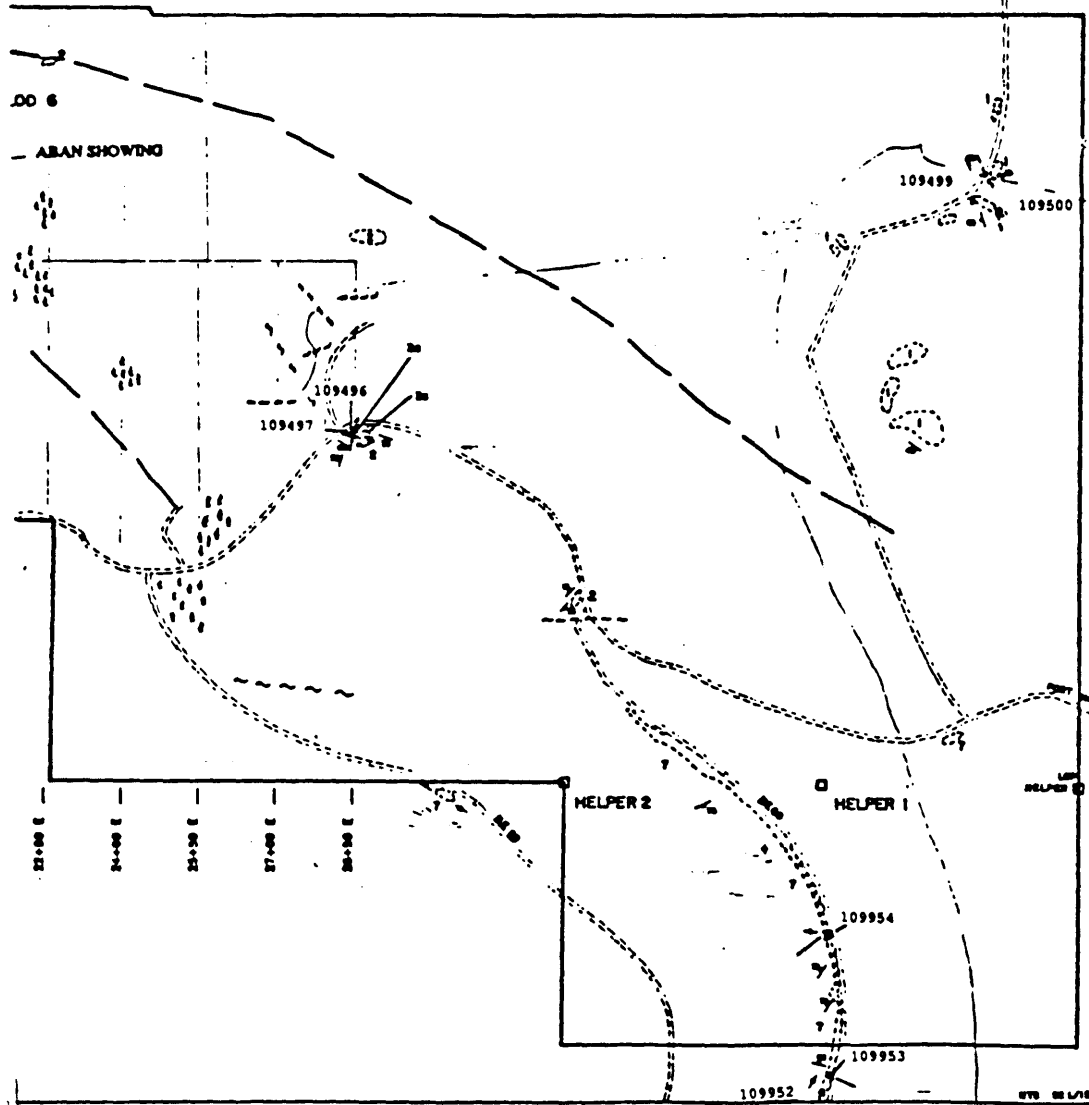
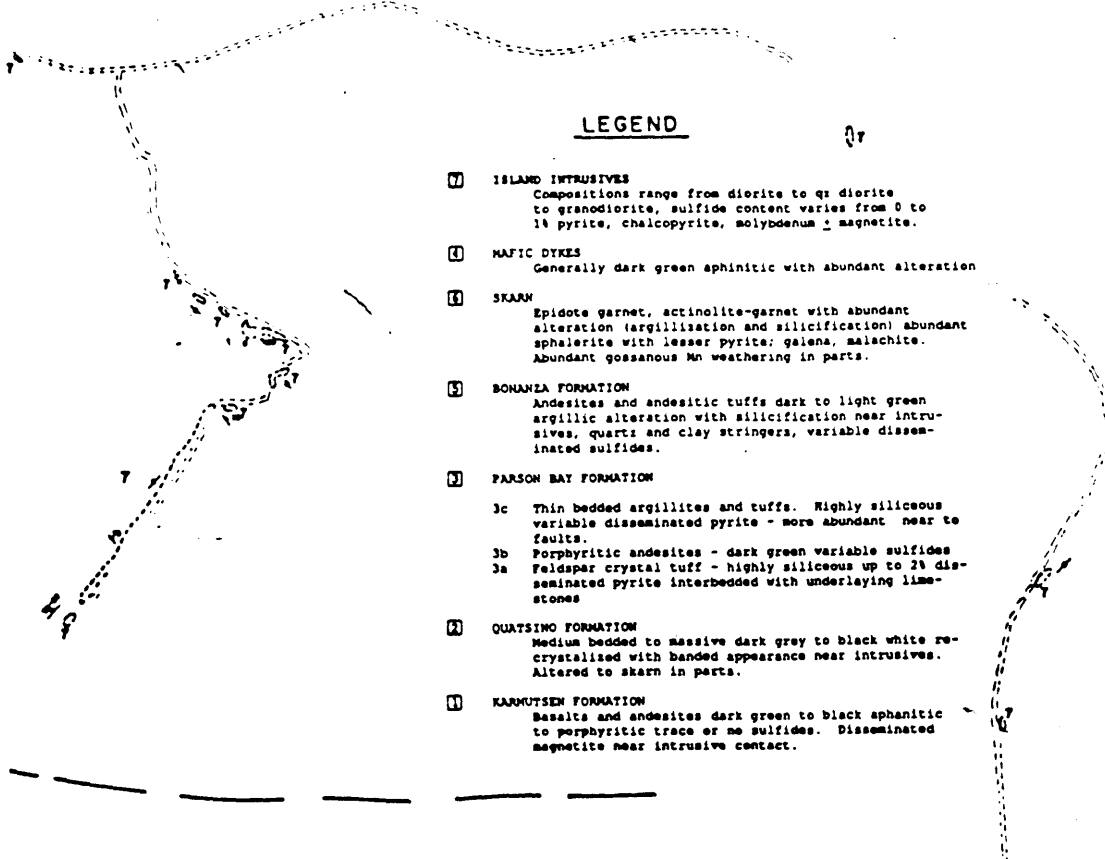
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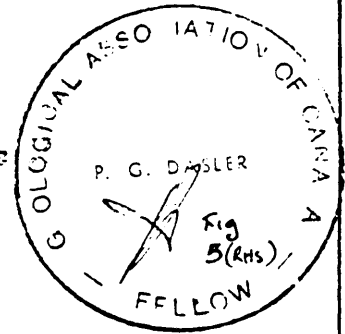
**LEGEND**

- ⑦ **ISLAND INTRUSIVES**  
Compositions range from diorite to quartz diorite to granodiorite, sulfide content varies from 0 to 14 pyrite, chalcopyrite, molybdenum, magnetite.
- ④ **MAFIC DYKES**  
Generally dark green aphanitic with abundant alteration
- ③ **SKARN**  
Epidote garnet, actinolite-garnet with abundant alteration (argillization and silicification) abundant sphalerite with lesser pyrite; galena, malachite. Abundant gossanous Mn weathering in parts.
- ⑤ **BOHANZA FORMATION**  
Andesites and andesitic tuffs dark to light green argillic alteration with silicification near intrusives, quartz and clay stringers, variable disseminated sulfides.
- ② **PARSON BAY FORMATION**
  - 3c Thin bedded argillites and tuffs. Highly siliceous variable disseminated pyrite - more abundant near to faults.
  - 3b Porphyritic andesites - dark green variable sulfides
  - 3a Feldspar crystal tuff - highly siliceous up to 2% disseminated pyrite interbedded with underlying limestones
- ① **QUATSINO FORMATION**  
Medium bedded to massive dark grey to black white recrystallized with banded appearance near intrusives. Altered to skarn in parts.
- ⑥ **KAMUTSEN FORMATION**  
Basalts and andesites dark green to black aphanitic to porphyritic trace or no sulfides. Disseminated magnetite near intrusive contact.

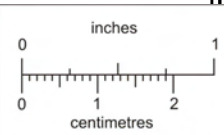
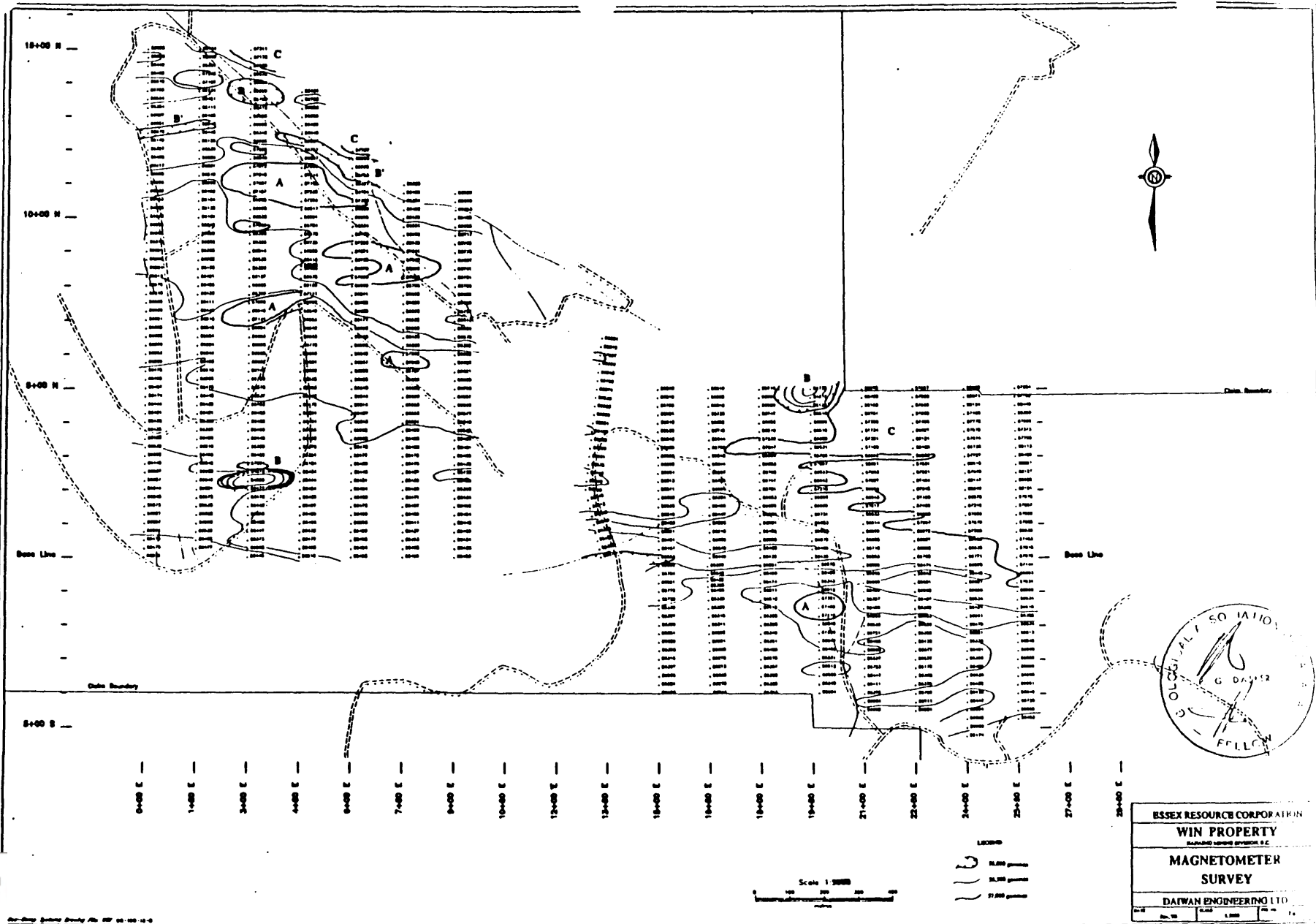


**SYMBOLS**

- ▼ Rock sample
- ▲ Silt sample
- Panned sample
- - - Fault
- - - Outcrop
- - - Geologic contact
- - - Bedding attitude
- - - Fractures
- - - Cross Section Locations

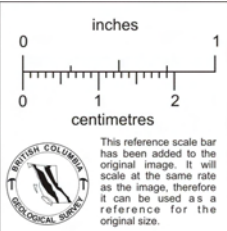
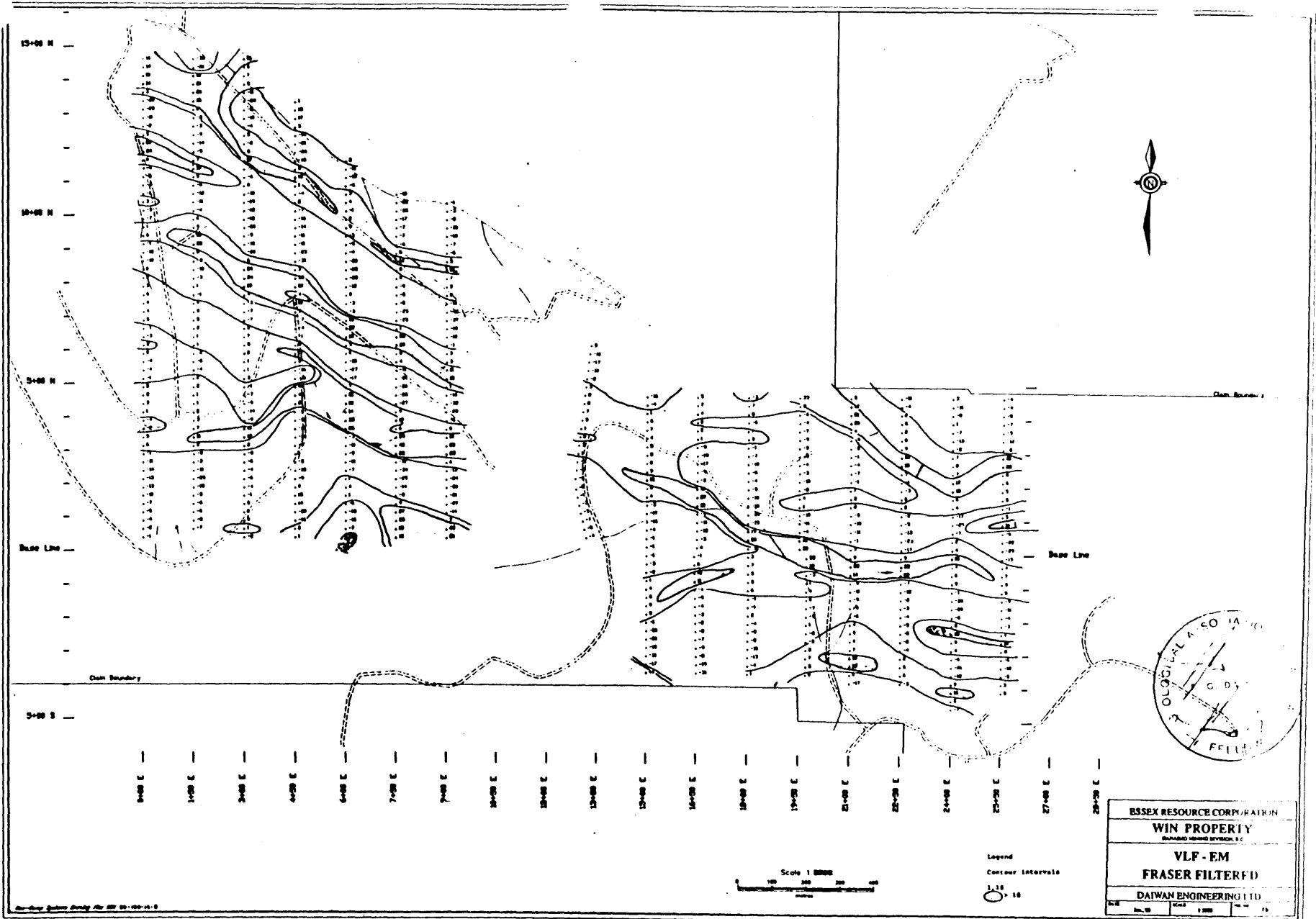


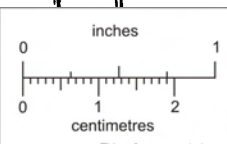
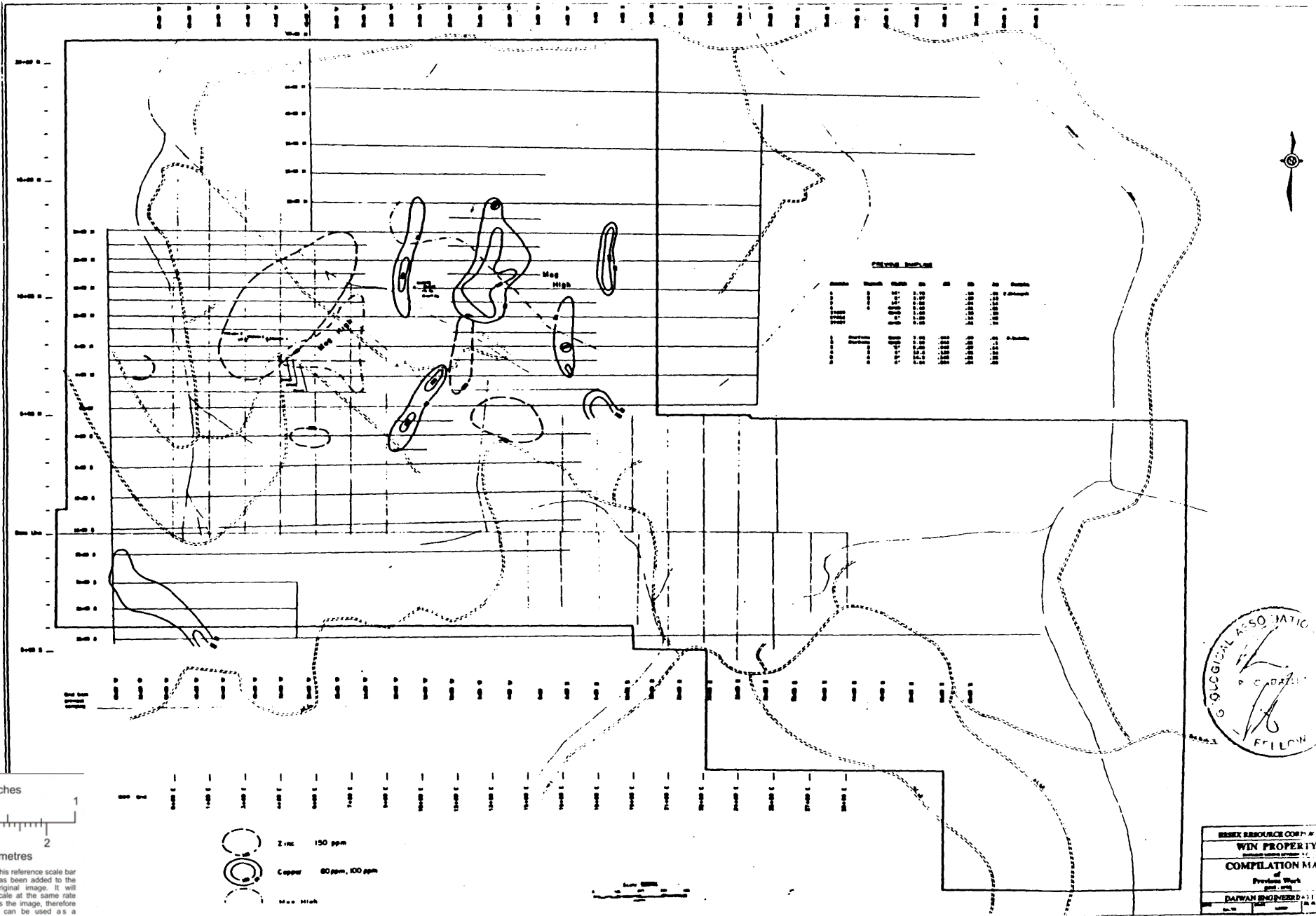
ESSEX RESOURCE CORPORATION	
WIN PROPERTY	
PROPERTY GEOLOGY & SAMPLE LOCATIONS	
DAIWAN ENGINEERING LTD.	



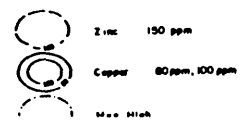
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BSSEX RESOURCE CORPORATION  
**WIN PROPERTY**  
 MAGNETOMETER SURVEY  
 DAIWAN ENGINEERING LTD

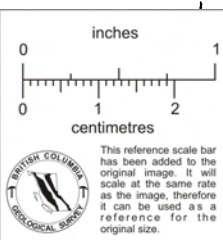
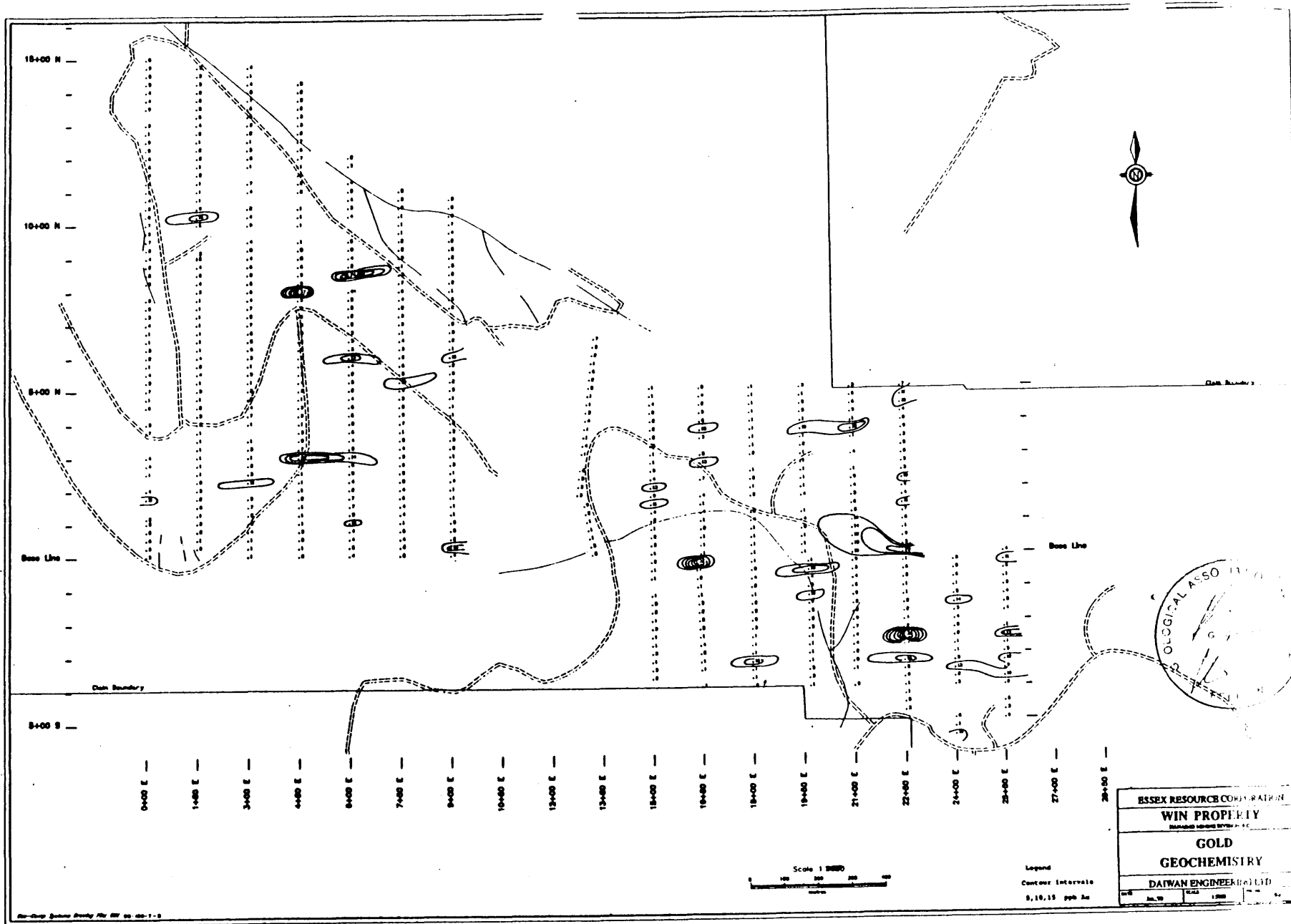


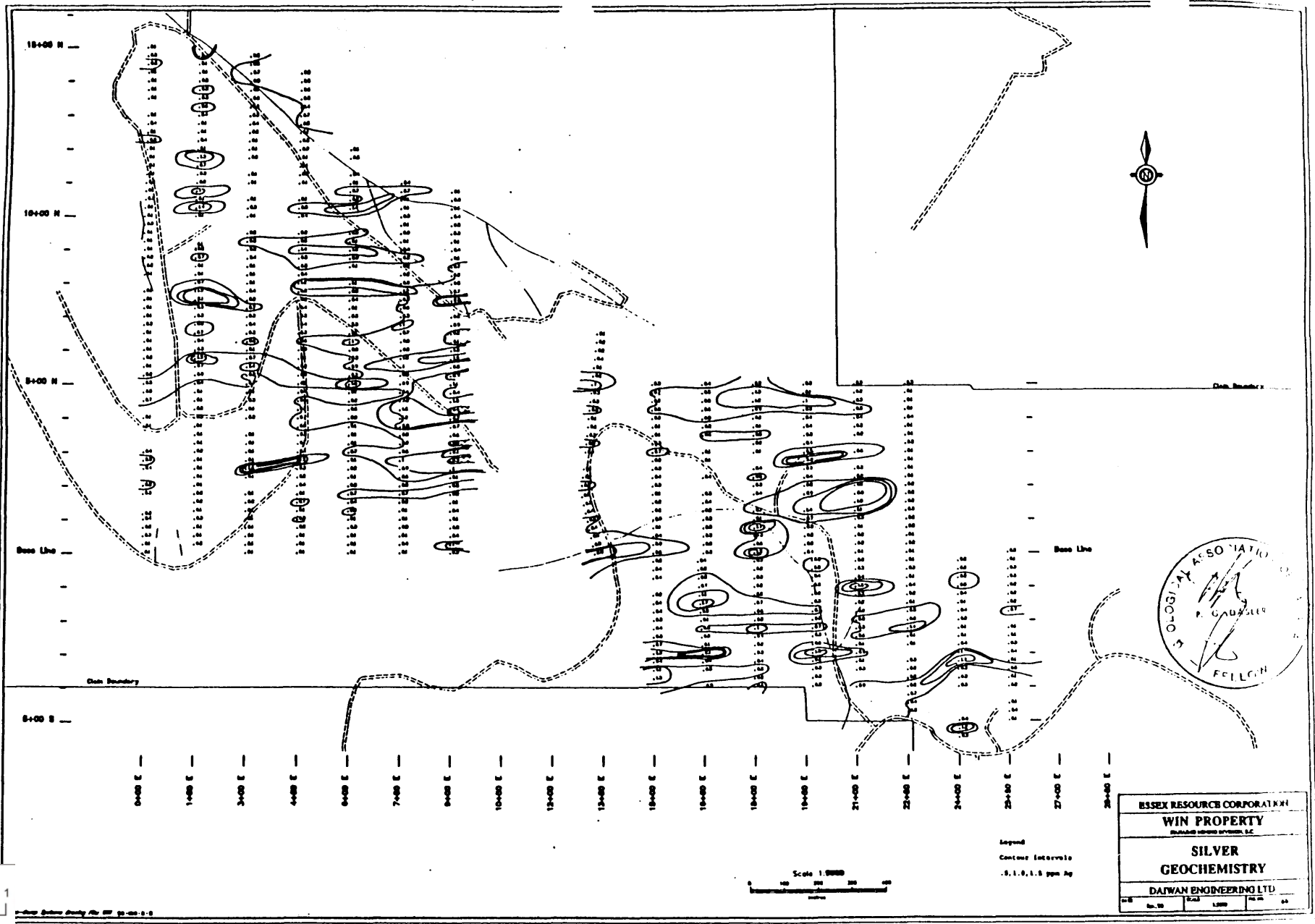


BRITISH COLUMBIA GEOLOGICAL SURVEY  
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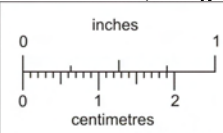
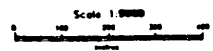
BRITISH RESOURCE CORPORATION  
**WIN PROPERTY**  
 COMPILATION MAP  
 of  
 Previous Work  
 done by  
**DAIWAH ENGINEERING**



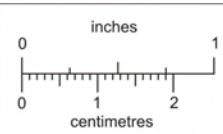
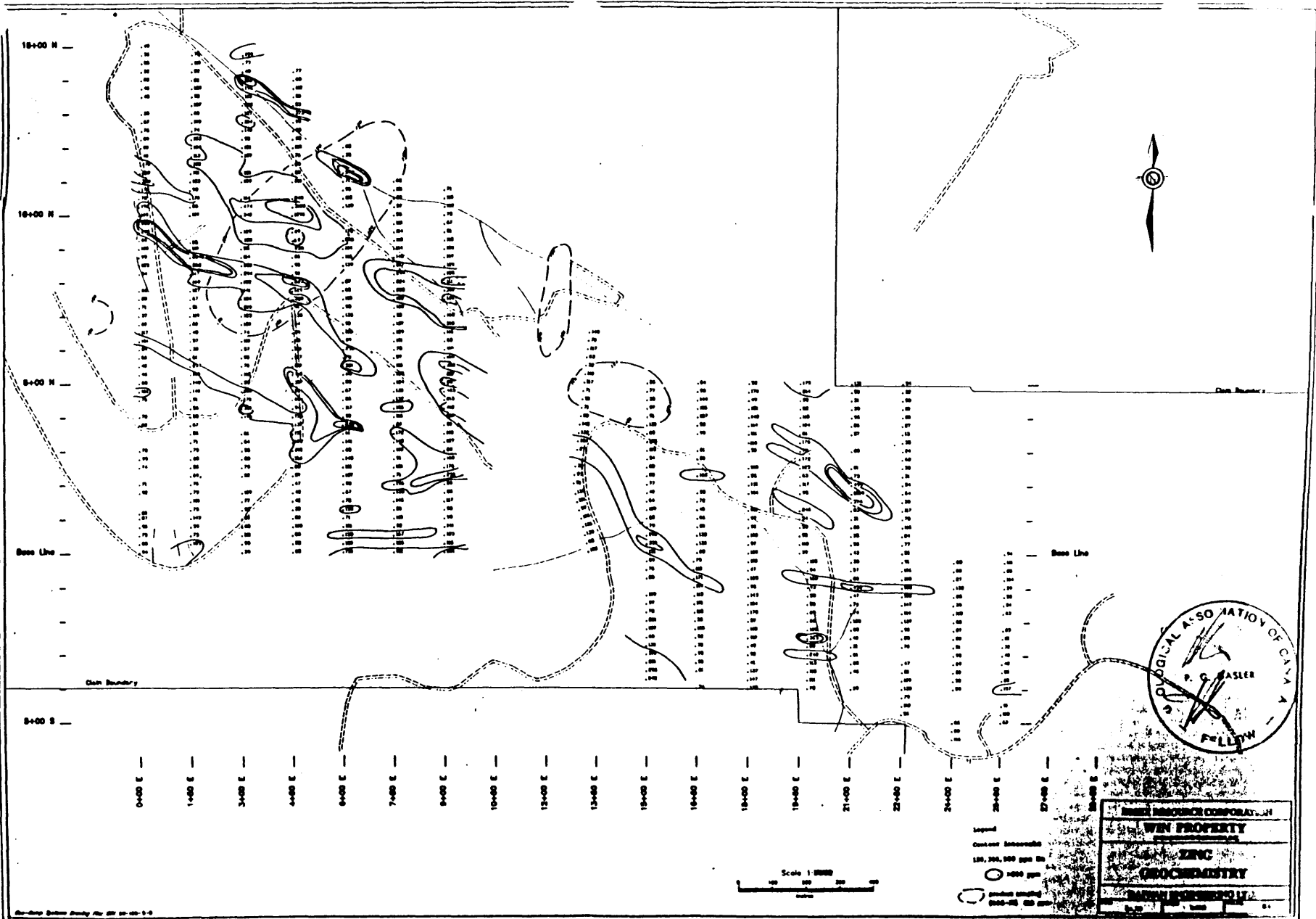


ESSEX RESOURCE CORPORATION	
WIN PROPERTY	
<small>(Detailed description of property, etc.)</small>	
SILVER	
GEOCHEMISTRY	
DAIWAN ENGINEERING LTD.	
<small>Scale</small>	<small>Sheet No.</small>

Legend  
Contour Interval  
5, 10, 15 ppm Ag



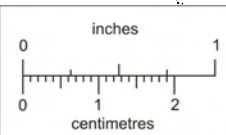
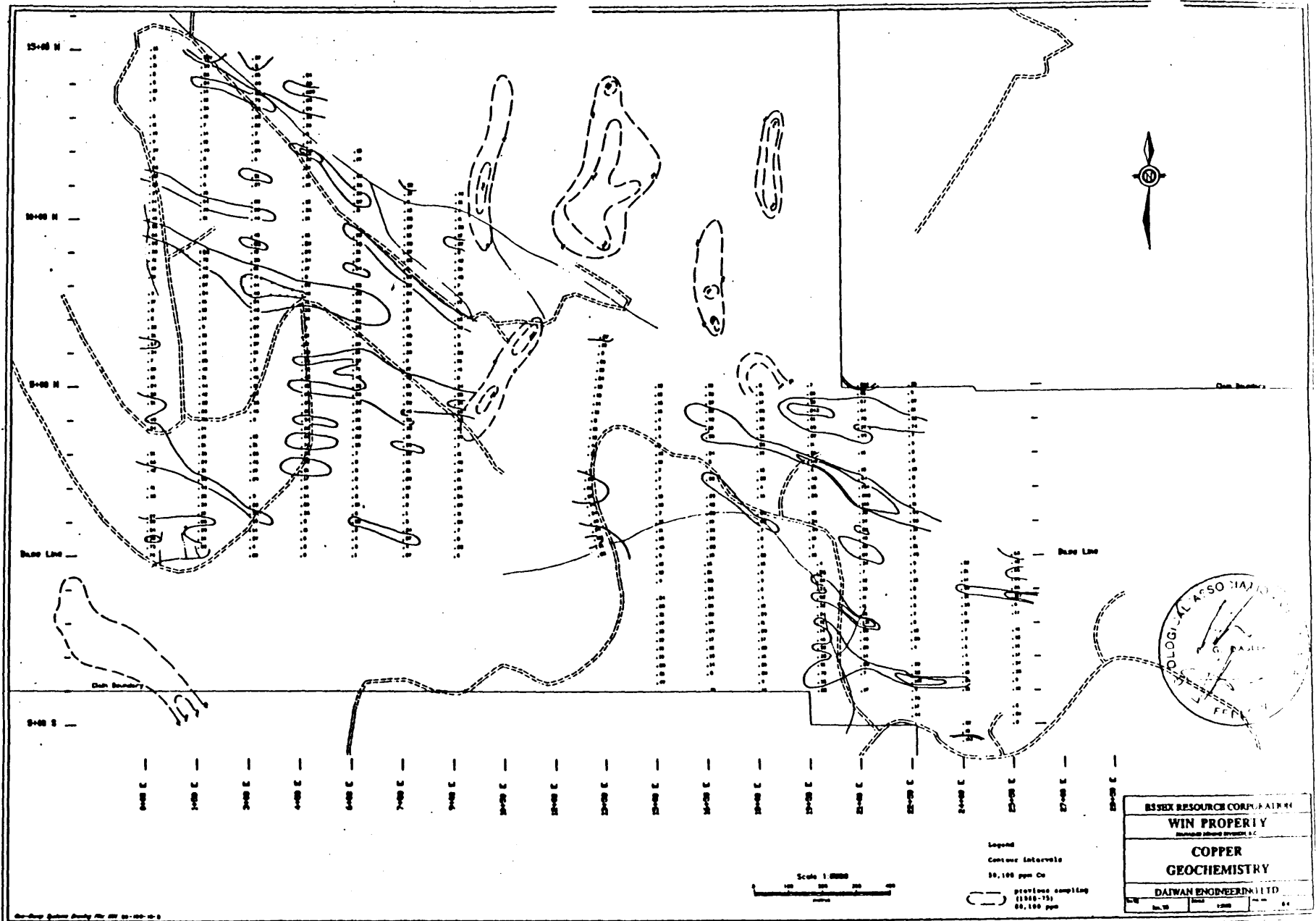
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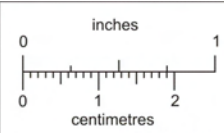
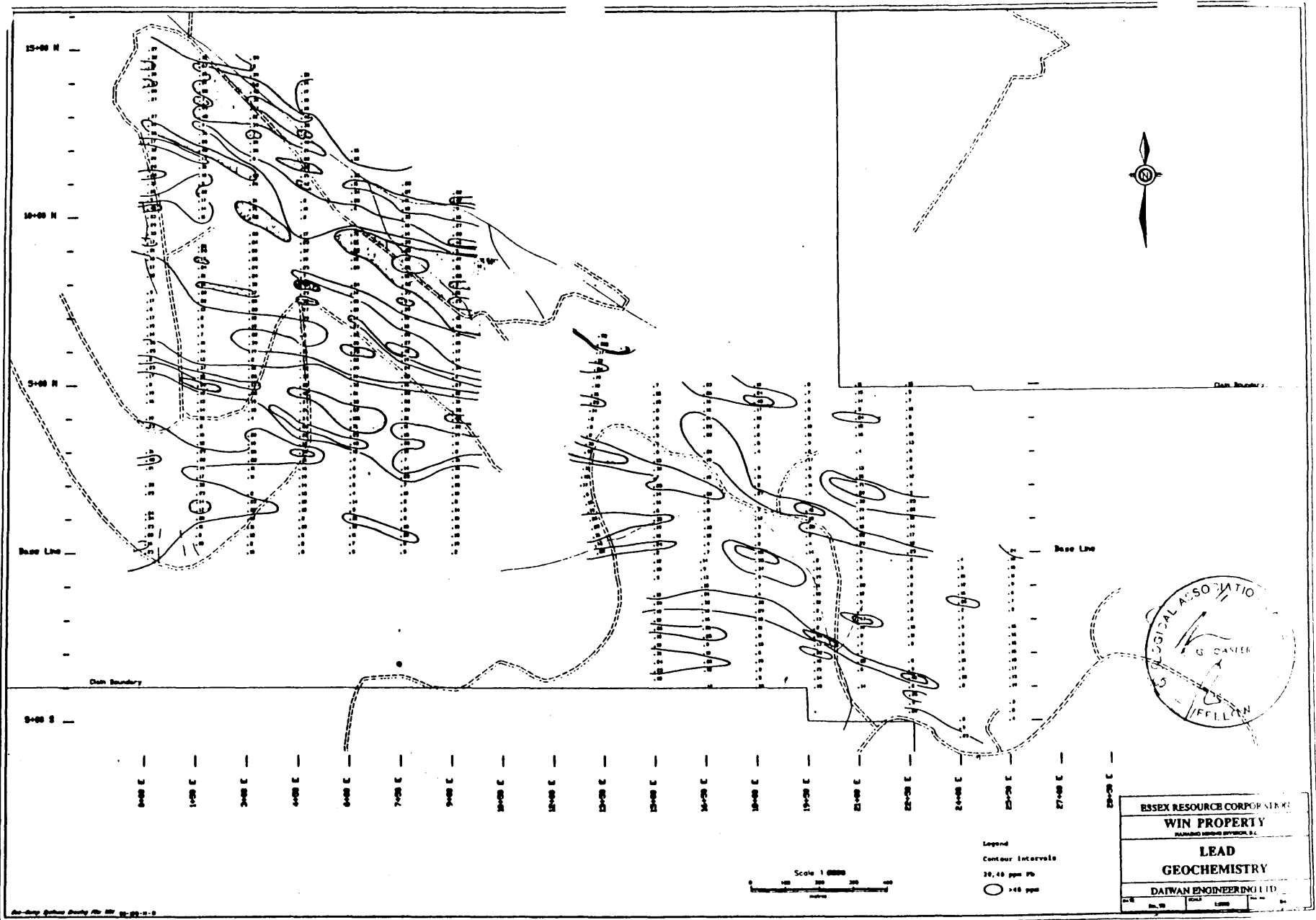
BRITISH COLUMBIA GEOLOGICAL SURVEY





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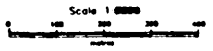
BRITISH COLUMBIA <b>WIN PROPERTY</b> <small>BRITISH COLUMBIA DIVISION OF MINES</small>	
<b>COPPER</b> <b>GEOCHEMISTRY</b>	
<b>DAIWAN ENGINEERING LTD.</b> <small>100-1000</small>	

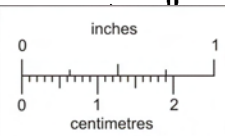
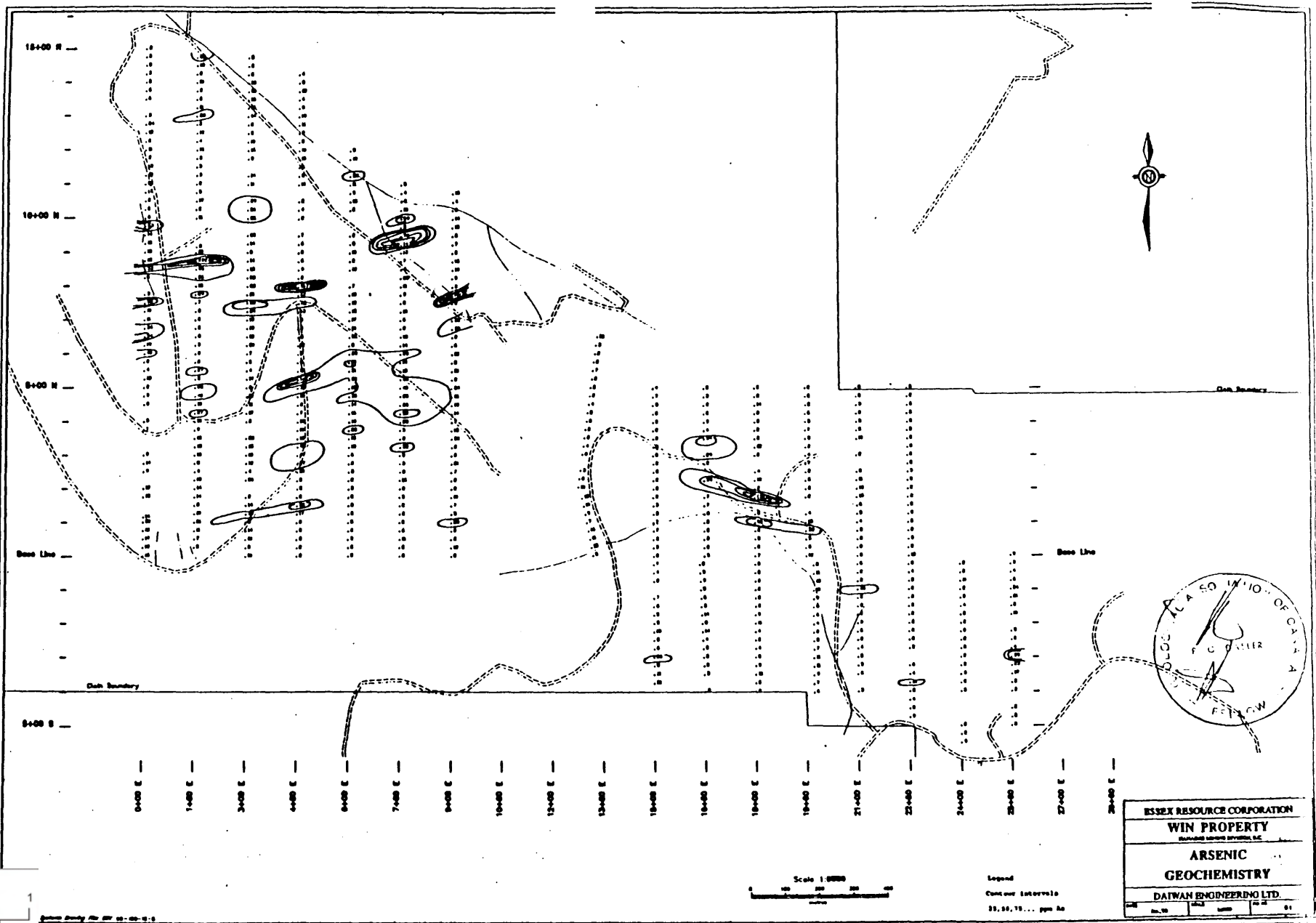


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BRITISH COLUMBIA GEOLOGICAL SURVEY	
ESSEX RESOURCE CORPORATION <b>WIN PROPERTY</b> <small>PLANNED MINING OPERATIONS S.S.</small>	
<b>LEAD GEOCHEMISTRY</b>	
DATWAN ENGINEERING LTD.	
<small>Map No.</small>	<small>Scale</small>

Legend  
 Contour intervals  
 10-40 ppm Pb  
 >40 ppm





This reference scale bar has been added to the original image. It will scale at the same rate as the image, therefore it can be used as a reference for the original size.

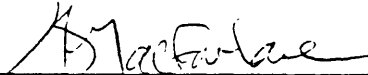


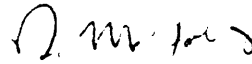
ESSEX RESOURCE CORPORATION  
 WIN PROPERTY  
 ARSENIC  
 GEOCHEMISTRY  
 DATWAN ENGINEERING LTD.

CERTIFICATE OF THE ISSUER

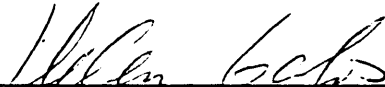
The foregoing constitutes full, true and plain disclosure of all material facts relating to the securities offered by this Prospectus as required by the Securities Act and its regulations.

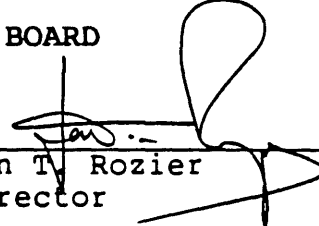
DATED at the City of Vancouver, in the Province of British Columbia, this 19th day of November, 1990.

  
\_\_\_\_\_  
Hamish Macfarlane  
Chief Executive Officer

  
\_\_\_\_\_  
Michael Foley  
Chief Financial Officer

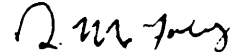
ON BEHALF OF THE BOARD

  
\_\_\_\_\_  
Helen Galos  
Director

  
\_\_\_\_\_  
Ian T. Rozier  
Director

PROMOTERS

  
\_\_\_\_\_  
Hamish Macfarlane

  
\_\_\_\_\_  
Michael Foley

CERTIFICATE OF THE AGENT

To the best of our knowledge, information and belief, the foregoing constitutes full, true and plain disclosure of all material facts relating to the securities offered by this Prospectus as required by the Securities Act and its Regulations.

DATED at the City of Vancouver, in the Province of British Columbia this 19th day of November, 1990.

UNION SECURITIES LTD.

Per:

  
Norman N. Thompson