Middle Vein Prospect 92F/2E Victoria / GP 007038 THIS PROSPECTUS CONSTITUTES A PUBLIC OFFERING OF THESE SECURITIES ONLY IN THOSE JURISDICTIONS WHERE THEY MAY BE LAWFULLY OFFERED FOR SALE AND THEREIN ONLY BY PERSONS PERMITTED TO SELL SUCH SECURITIES. NO SECURITIES COMMISSION OR SIMILAR AUTHORITY IN CANADA HAS IN ANY WAY PASSED UPON THE MERITS OF THE SECURITIES OFFERED FOR SALE BY THIS PROSPECTUS AND ANY REPRESENTATION TO THE CONTRARY IS AN OFFENCE.

**PROPERTY FILE** NEW ISSUE

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CANADIAN IMPERIAL MINES INC. (the "Issuer") (Incorporated in British Columbia)

DEC 1 7 1991

ROSPECTUS~-

Geological Survey Branch MEMPR

COMMON SHARE OFFERING: 600,000 COMMON SHARES

 
 Price to Public
 Commission(1)
 Net Proceeds to the Issuer(2)

 Per Share
 \$0.40
 \$0.04
 \$0.36

 Total
 \$240,000
 \$24,000
 \$216,000

#### FLOW-THROUGH COMMON SHARE OFFERING: 200,000 COMMON SHARES

| · · · · · · · · · · · · · · · · · · · | Price to Public | Commission(1)(3) | Net Proceeds<br>to the Issuer |  |
|---------------------------------------|-----------------|------------------|-------------------------------|--|
| Per Share                             | \$0.40          | Nil              | \$0.40                        |  |
| Total                                 | \$80,000        | Nil              | \$80,000                      |  |

(1) In addition, the Agent will be granted Agent's Warrants as described in the section captioned "Plan of Distribution".

(2) Before deduction of the balance of costs of this Prospectus estimated at \$30,000.

(3) The Issuer will pay a fee of \$8,000 to the Agent, from general working capital, in respect of the sale of the Flow-Through Common Shares.

THE PRICE TO THE PUBLIC WAS ESTABLISHED PURSUANT TO NEGOTIATIONS BETWEEN THE ISSUER AND THE AGENT.

THERE IS PRESENTLY NO MARKET THROUGH WHICH THE SECURITIES OF THE ISSUER MAY BE SOLD AND A PURCHASE OF THE SHARES OFFERED BY THIS PROSPECTUS MUST BE CONSIDERED A SPECULATION. THE ISSUER'S MINERAL PROPERTY IS IN THE PRELIMINARY STAGES OF EXPLORATION AND DEVELOPMENT AND THERE IS NO KNOWN BODY OF COMMERCIAL ORE PRESENT ON THE PROPERTY. REFERENCE IS MADE TO THE SECTIONS CAPTIONED "RISK FACTORS" AND "DILUTION".

NO PERSON IS AUTHORIZED BY THE ISSUER TO PROVIDE ANY INFORMATION OR TO MAKE ANY REPRESENTATION OTHER THAN THOSE CONTAINED IN THIS PROSPECTUS OR IN CONNECTION WITH THE ISSUE AND SALE OF THE SECURITIES OFFERED BY THE ISSUER.

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THE OFFERING OF FLOW-THROUGH COMMON SHARES IS INTENDED TO ALLOW INVESTORS TO ACHIEVE CERTAIN TAX BENEFITS IN THE YEAR OF SUBSCRIPTION. THE ACHIEVING OF SUCH BENEFITS BY THE INVESTORS AND THE INCURRING OF EXPENDITURES BY THE ISSUER ON BEHALF OF THE INVESTORS ARE SUBJECT TO RISK AND UNCERTAINTY WHICH ARE DESCRIBED IN THE SECTIONS CAPTIONED "CANADIAN INCOME TAX CONSIDERATIONS OF FLOW-THROUGH SHARES" AND "RISK FACTORS".

ONE OR MORE OF THE DIRECTORS OF THE ISSUER ARE DIRECTORS OF OTHER NATURAL RESOURCE COMPANIES AND HAVE POTENTIAL CONFLICTS OF INTERESTS WHEN SERVING IN SUCH CAPACITIES. REFERENCE IS MADE TO THE SECTION CAPTIONED "DIRECTORS AND OFFICERS".

FOR COMPARISON OF THE SHARES BEING OFFERED TO THE PUBLIC FOR CASH AND THOSE ISSUED TO PRO-MOTERS, DIRECTORS AND OTHER INSIDERS, REFERENCE IS MADE TO THE SECTION CAPTIONED "PRINCI-PAL SHAREHOLDERS". UPON COMPLETION OF THIS OFFERING, THE SECURITIES OFFERED HEREUNDER WILL REPRESENT 29.244% OF THE ISSUED SHARES OF THE ISSUER THEN OUTSTANDING WHILE THE DIRECTORS AND SENIOR OFFICERS OF THE ISSUER WILL HOLD 49.323% OF THE ISSUED SHARES THEN OUTSTANDING. THE PUBLIC WILL EXPERIENCE DILUTION OF \$0.28 PER SHARE OR 70%. REFERENCE IS MADE TO THE SECTIONS CAPTIONED "DILUTION" AND "PRINCIPAL SHAREHOLDERS".

THE AGENT'S WARRANTS HAVE BEEN DISTRIBUTED UNDER THIS PROSPECTUS. ANY SHARES ACQUIRED BY THE AGENT UNDER THE GUARANTEE WILL ALSO BE DISTRIBUTED UNDER THIS PROSPECTUS THROUGH THE FACILITIES OF THE VANCOUVER STOCK EXCHANGE AT THE MARKET PRICE AT THE TIME OF SALE. REFERENCE IS MADE TO THE SECTION CAPTIONED "PLAN OF DISTRIBUTION".

THE VANCOUVER STOCK EXCHANGE HAS CONDITIONALLY LISTED THE SECURITIES OFFERED PURSUANT TO THIS PROSPECTUS. LISTING IS SUBJECT TO THE ISSUER FULFILLING ALL THE LISTING REQUIREMENTS OF THE EXCHANGE ON OR BEFORE DECEMBER 11, 1991 INCLUDING PRESCRIBED DISTRIBUTION AND FINANCIAL REQUIREMENTS.

WE, AS AGENT, CONDITIONALLY OFFER THESE SECURITIES SUBJECT TO PRIOR SALE, IF, AS AND WHEN ISSUED BY THE ISSUER AND ACCEPTED BY US IN ACCORDANCE WITH THE CONDITIONS CONTAINED IN THE AGENCY AGREEMENT REFERRED TO IN THE SECTION CAPTIONED "PLAN OF DISTRIBUTION".

THIS PROSPECTUS IS DATED THE 4TH DAY OF NOVEMBER, 1991.

#### AGENT

BRINK HUDSON & LEFEVER LTD. 1200 - 595 Burrard Street Vancouver, B.C. V7X 1J1

EFFECTIVE DATE: NOVEMBER 5, 1991

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92 F/2 Latitude: 49 06'N Longitude: 124 35'W

# **REVISED GEOLOGICAL REPORT**

#### MIDDLE VEIN PROSPECT

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Mount McQuillan Area Victoria Mining Division, B.C.

for

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# CANADIAN IMPERIAL MINES INC. #777 - 1177 West Hastings Street Vancouver, B.C. V6E 2K3

By

Kucera & Associates Consultants Richard E. Kucera, Ph.D.

September 20, 1991



#### SUMMARY

Canadian Imperial Mines Inc. holds seven reverted Crown Grants (Middle Vein Prospect) in the Mt. McQuillan area, located 21 kilometres southeast of Port Alberni, Vancouver Island, B.C. (92F/2). Elevations range from 1200 to 1500 metres. Present access to the property is either by helicopter or by trail from China Creek or Nitinat River. The end of an old logging road lies 2.2 kilometres southeast of the property.

The Middle Vein Prospect is located on the Cowichan-Horn Lake Uplift, a geologically favourable area and contains past producers of the Mt. McQuillan-China Creek mining camps. The property is largely underlain by the lower part of the Sicker Group rocks, represented here by the Duck Lake Formation, composed of grey to greenish andesite, dacite tuffs and breccias. Gabbroic rocks (Island Intrusions) also occur locally.

Mineralization on the property consists of lenticular quartz-carbonate veins, up to 5 metres long and 20 cm wide, associated with a very strong and persistent NNE trending shear zone 2 to 3 metres wide that cuts light to dark brown weathered andesite. This mineralized zone has been referred to as the Middle Vein. The Middle Vein is exposed only in the Middle Vein workings for a distance of 5 metres. The veins and shear zone at this locality strike N 10 degrees to 18 degrees East and dip 78 degrees to 85 degrees East. Some of the veins are found associated with light-coloured feldspar-hornblende dykes that are as much as 2 metres wide. One 20 cm channel sample assayed 0.88 oz/ton Au.

Although the shear zone is largely obscured by overburden, it is also exposed for a distance of 350 metres on the northern portion of the property. There is no indication of the Middle Vein shear zone by VLF-EM survey on the Apex and Skyline claims nor on the War Lion and Conqueror claims. Exploration by Canadian Imperial Mines Inc. in 1989 and 1991 included establishing grid lines, collecting chip and channel samples, geological mapping and geophysical surveys. The writer has taken no independent check samples but he directed sampling by employees of the vendor.

Individual quartz veins assay up 1.4 oz/ton Au across widths of up to 10 cm. Sampling by Sawyer Consultants (1980) reported values of up to 2.20 oz/ton Au and 2.09 oz/ton Ag.

The Middle Vein is judged to be a good target. A two stage exploration program is recommended. Stage One would consist of detailed geological mapping and sampling, aerial photo interpretation and trenching. Stage Two would consist mainly of diamond drilling.

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## INTRODUCTION

This report was prepared at the request of Mr. Clive Ashworth, on behalf of Canadian Imperial Mines Inc. The purpose of this report is to describe the results of geological exploration and assess the potential of the Middle Vein Prospect (seven reverted Crown grants) held by Canadian Imperial Mines Inc. in the Mt. McQuillan area, southeast of Port Alberni, Vancouver Island.

The report discusses the results of mapping, sampling and geophysical surveys carried out by Ashworth Explorations Limited in 1989 and Hi-Tec Resource Management Ltd. in 1991. In addition, observations made in conjunction with a drilling program carried out on an adjacent property in the early 1980's have been useful in this report.

The primary target is a mineralized zone (Middle Vein) consisting of quartzcarbonate veins associated with a very strong and persistent NNE trending shear zone. Examination of existing data followed by the 1989 and 1991 work programs have demonstrated the presence of gold anomolies in rocks with values up to 1.4 oz/ton across widths of up to 10 cm.

Certain recommendations are made in this report to explore the Middle Vein on the surface as well as at depth. The writer judges the exploration merit of the property to be good.

#### SOURCE OF INFORMATION

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The primary source of information of which this report is based on included geological data, maps, and assays contained in a report by Mr. Hugo Laanela, Consulting Geologist, Nanaimo, B.C. In his report of August 8, 1989, for Ashworth Explorations Ltd., he summarized the work done on the property during the late 1970's and early 1980's by Lode Resources Corp. Laanela also reports on some geophysics and prospecting carried out in the summer of 1989 by Ashworth Explorations Ltd.

In addition, the present writer has drawn upon other appropriate sources including Annual Reports by the Minister of Mines, GSC Papers, and unpublished geological and geophysical reports on adjoining properties. He also had numerous discussions with Mr. Fayz Yacoub, Project Geologist for Ashworth Explorations Ltd.

The writer examined the northern part of the Middle Vein Prospect on October 16, 1989 and mapped a portion of the geology in the vicinity of the Middle Vein on the Apex claim. He was also accompanied by Mr. Yacoub and supervised sampling of the Middle Vein workings.

The results of geologic mapping, rock sampling and geophysical work by Hi-Tec Resource Management during June 1991 have been incorporated in this revised report.

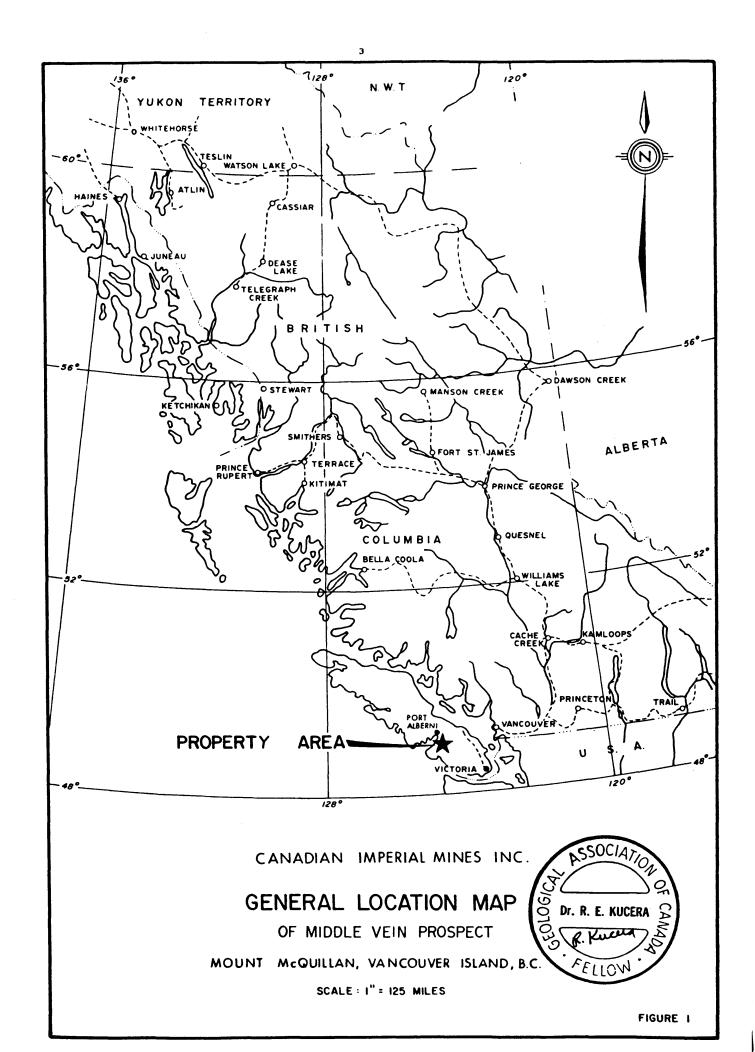
#### LOCATION AND ACCESS

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The Middle Vein Prospect is located 21 kilometres southeast of Port Alberni, Vancouver Island, B.C. (NTS map sheet 92 F/2). The geographical coordinates are 49 degrees 06'N, 124 degrees 35'W in the Victoria Mining Division.

The property is located along the east flank of McQuillan Ridge, the southern spur of Mt. McQuillan. The area lies west of the headwaters of the Middle Fork of Nitinat River.

Present access to the property is either by helicopter (12 minutes from Nanaimo) or by trail from China Creek or Nitinat River. However, a network of roads do exist in the area. The terminus of an old logging road located at the headwaters of the Middle Fork of Nitinat River lies 2.2 kilometres southeast of the workings at the Middle Vein.



# PHYSIOGRAPHY

The Claim Group lies along the west flank of a ridge extending south of Mt. McQuillan. The area is bounded on the east by the steep valley of Nitinat River (Middle Fork). Elevations on the property range from about 1500 metres along the northern part of the ridge to about 1200 metres toward the eastern and southern parts. The easterly-facing slopes on the property average about 30 degrees - 45 degrees, often with steep rocky cliffs or gullies. Short stream courses drain the property and some segments exhibit distinct structural control. Summit Lake lies at the headwaters of China Creek, 0.5 km. northeast of the Apex Claim, at an elevation of 1020 metres. The property is covered with some heavy stands of timber, with dense underbrush. There are some open areas on the property.

#### **PROPERTY STATISTICS**

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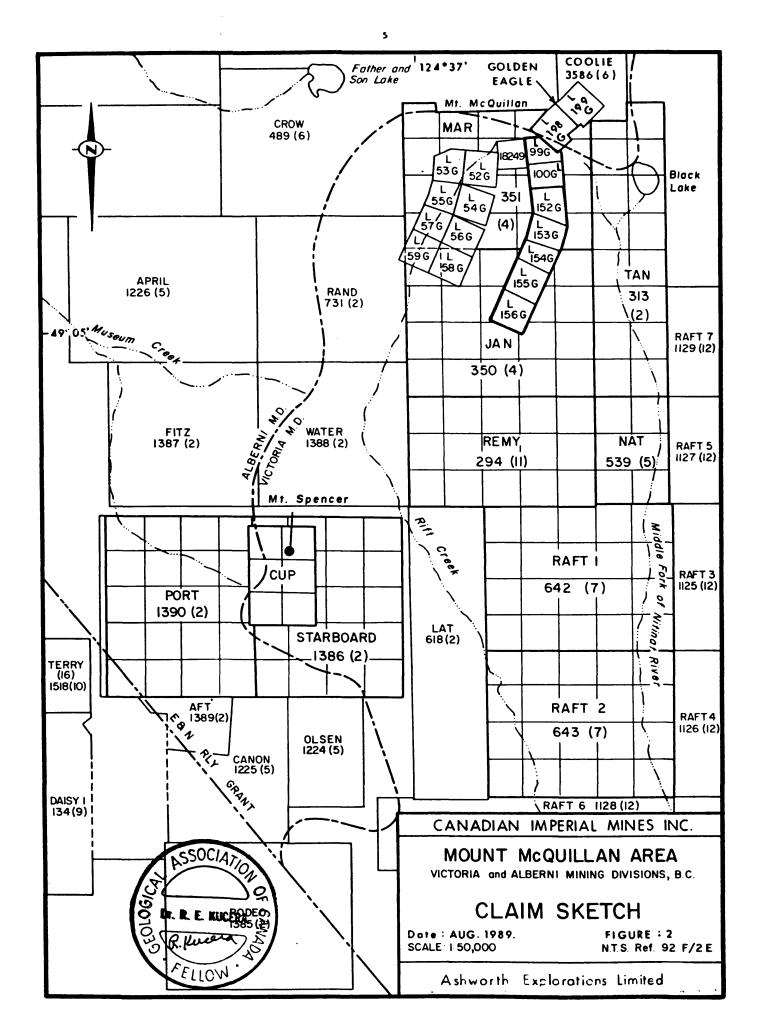
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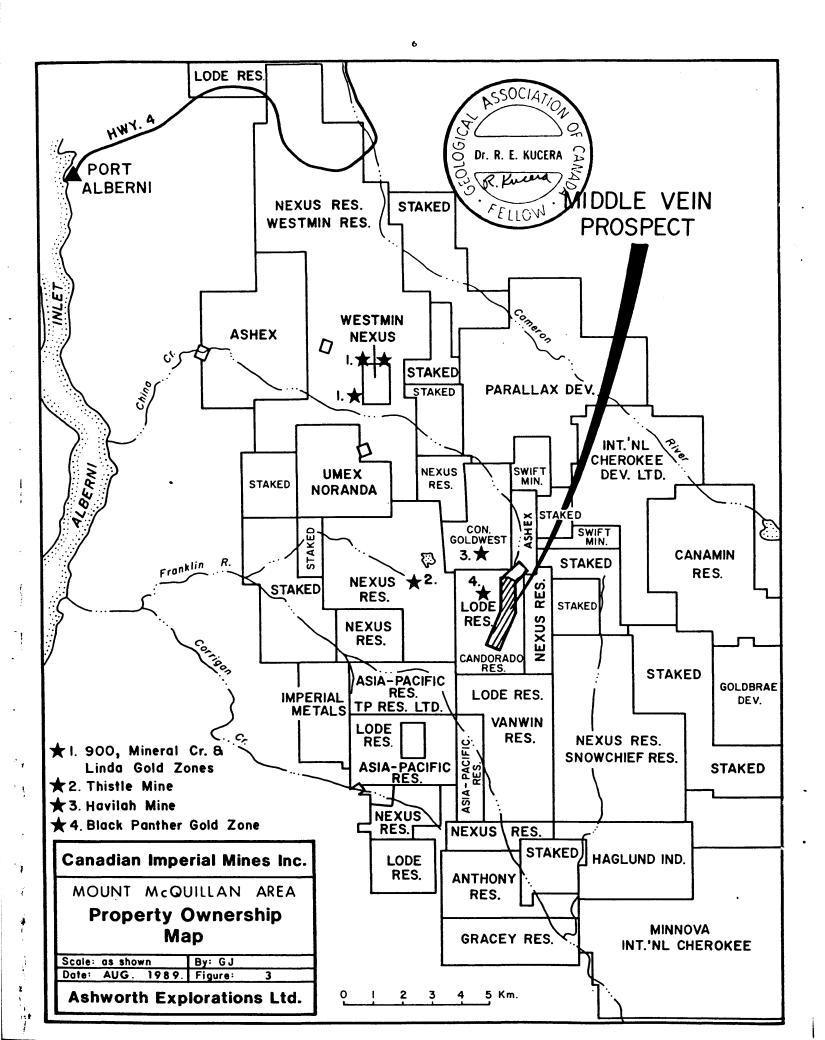
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The Middle Vein Prospect consists of seven reverted Crown Grant 2-post claims (from Laanela, 1989). The property is owned by Mr. Clive Ashworth of West Vancouver, B.C.

| <u>Lot #</u> | Record # | <b>Record Date</b> | Claim Name       | Area (hectares) |
|--------------|----------|--------------------|------------------|-----------------|
| 99G          | 1577 (9) | Sept. 9, 1985      | Apex             | 12.75           |
| 100G         | 1578 (9) | Sept. 9, 1985      | Skyline          | 14.97           |
| 152G         | 1541 (7) | July 4, 1985       | War Lion         | 19.78           |
| 153G         | 1542 (7) | July 4, 1985       | Conqueror        | 16.83           |
| 154G         | 1543 (7) | July 4, 1985       | Majestic         | 14.25           |
| 155G         | 1544 (7) | July 4, 1985       | Empress of India | 20.90           |
| 156G         | 1545 (7) | July 4, 1985       | IXL              | 20.90           |
|              |          |                    | Total Hectares   | = 120.38        |
|              |          |                    | (297.5 acres / 2 | 1.204 sq. km.)  |

The claim group is held under option by the Canadian Imperial Mines Inc. The Apex and Skyline claims were surveyed by J.E. Anderson and Associates, Surveyors and Engineers during June, 1989.





The Crown grants and claims are shown on the B.C. Dept. of Energy, Mines and Petroleum Claim Map M92 F/2E as well as on Figures 2, 3, and 5 of this report. The locations of the 7 Crown Grant claims were not verified in the field as none of the claim posts or survey pins were inspected.

#### HISTORY OF EXPLORATION

The following summary of exploration and mining activity in the general area of the Middle Vein Prospect is condensed from a report by Mr. H. Laanela, 1989, Consulting Geologist.

Gold in the area was first discovered in the gravels of China Creek, just north of the Middle Vein property in 1862, followed by staking rushes and much mining activity. The Mt. McQuillan-China Creek area contains several modest past producers and numerous Au-Ag prospects, mostly vein-type, including the Black Panther mine, Havilah, Debbie Propsect, Golden Eagle, plus several less explored prospects in the area. These various mineral occurrences and the old mines are described by Stevenson (1945) in his report on the China Creek area.

During the 1960's Gunnex Ltd. carried out various regional and detailed surveys for minerals on the E and N Railway Land Grant on Vancouver Island. The results of these programs later led to the staking of favourable properties on Mt. McQuillan.

During the late 1970's and early 1980's Lode Resources Corp. had secured most of the favourable ground in the Mt. McQuillan area, including the High Grade Vein and Middle Vein area. Lode Resources sampled and drilled several of these properties including the High Grade Vein with encouraging results during 1980 and 1983. The High Grade Vein is located just west and outside of the Middle Vein Prospect, dipping steeply to the west of the property boundary. (See Figure 5).

### **REGIONAL GEOLOGY**

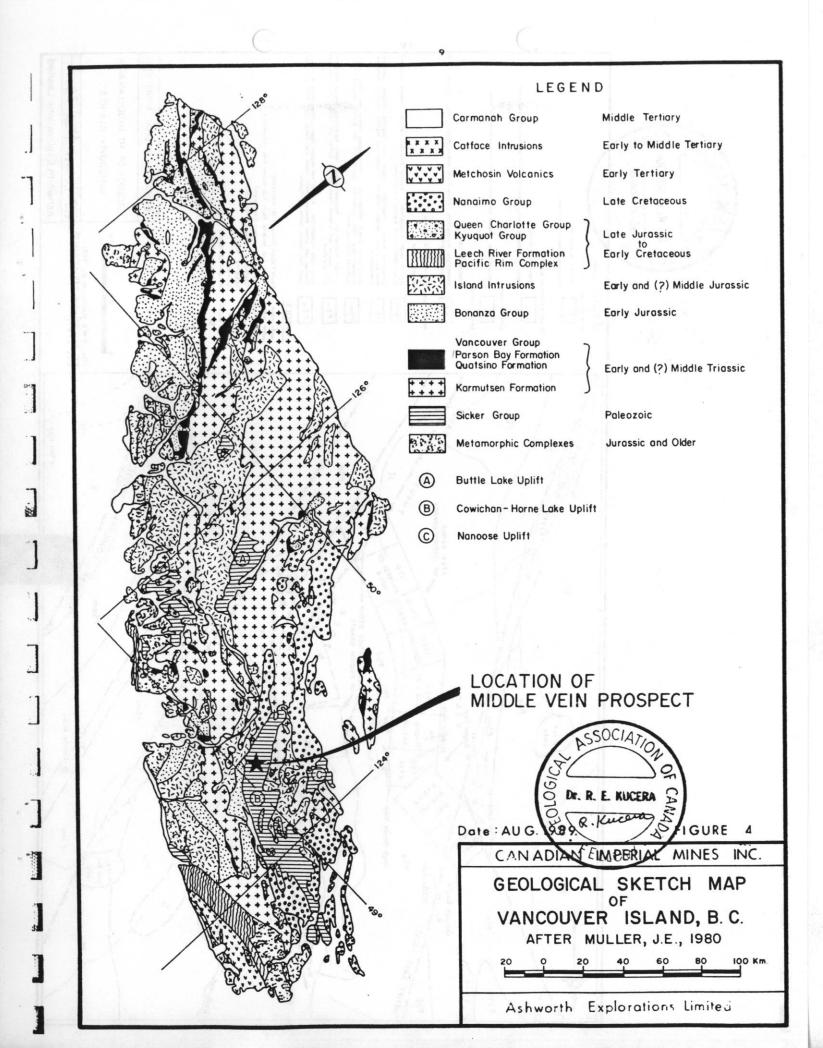
The Middle Vein Claim Group is located on the Cowichan-Horn Lake Uplift, a geologically and economically favourable area on Vancouver Island. This uplift is some 125 kilometres long and 15-22 kilometres wide and it contains the past producers of the Mt. McQuillan - China Creek mining camps. The area is underlain by the Sicker Group volcanics and associated sedimentary rocks. (Figure 4).

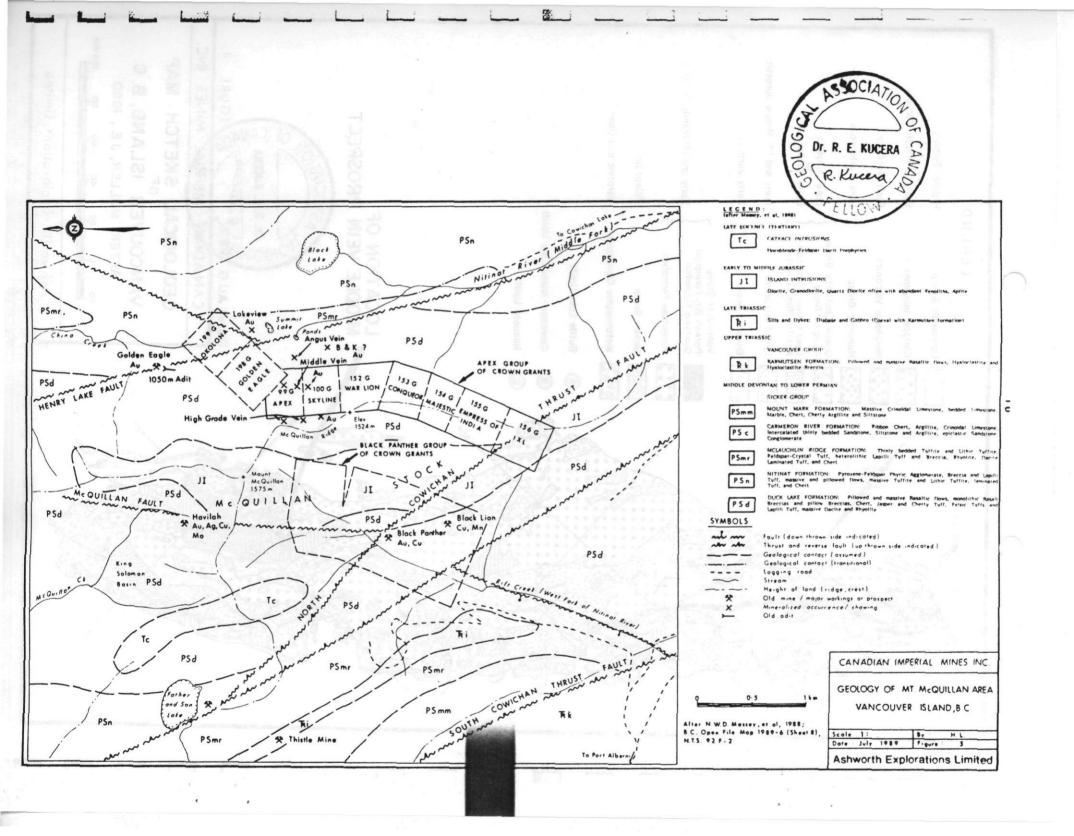
# Stratigraphy

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The regional stratigraphy has been studied by the GSC (Muller, 1977, 1980 and updating of the Sicker Group by Massey et al, 1988). Laanela, 1989, summarizes the pertinent stratigraphy related to Mt. McQuillan.

| <u>Era</u> | Period or Epoch                  | Name                  | Lithology  |
|------------|----------------------------------|-----------------------|--|
| CENOZOI    | Early to<br>C Middle<br>Tertiary | Catfish<br>Intrusions | Sills, dykes and small plutons of feld-<br>spar hornblende-plagioclase) porphyry.<br>Associated with mineralized veins.  |
|            | Upper<br>Cretaceous              | Nanaimo<br>Group      | Conglomerate, sandstone, shale and coal  |
| MESOZOI    | Early and Middle<br>Jurassic     | Island<br>Intrusions  | Granitoid batholiths and stocks, largely dioritic composition.   |
|            | Early<br>Jurassic                | Bonanza<br>Group      | Lava, tuff and breccia of basaltic and rhyolitic composition.  |
|            | Late to Middle<br>Triassic       | Vancouver<br>Group    | Limestone, argillites, greywackes and<br>Karmutsen - basalts, pillow lavas, tuffs.   |
|            | Middle Penn.<br>to Early Permian | Sicker<br>Group       | St. Marys Lake fm - volcanic sandstone and conglomerate, argillite.  |
|            |                                  |                       | Mount Mark fm - crinoidal limestone, chert, argillite.   |
|            | Devonian                         |                       | <u>Cameron River fm</u> - ribbon chert,<br>argillite, limestone, sandstone.  |
| PALEOZO    | IC                               |                       | <u>McLaughlin Ridge fm</u> - tuffite, feldspar<br>- crystal tuff, breccia, dacite.<br><u>Nitinat fm</u> - meta basaltic lavas,<br>agglomerate, massive tuffite.  |
|            |                                  |                       | Duck Lake fm - pillowed and massive<br>basaltic flows, breccias, cherty tuff,<br>massive dacite and rhyolite. Largely<br>occupies the Middle Vein property area. |





#### Stucture and Igneous Intrusives

The Sicker Group rocks are buried under the Mesozoic cover except where they are now exposed in major uplift areas, such as the Cowichan-Horne Lake Uplift. The structure of the Sicker Group appears to be the result of a complex structural history including normal and transcurrent faulting and folding. The rocks are steeply folded and are in places highly sheared and metamorphosed to chloritic schists.

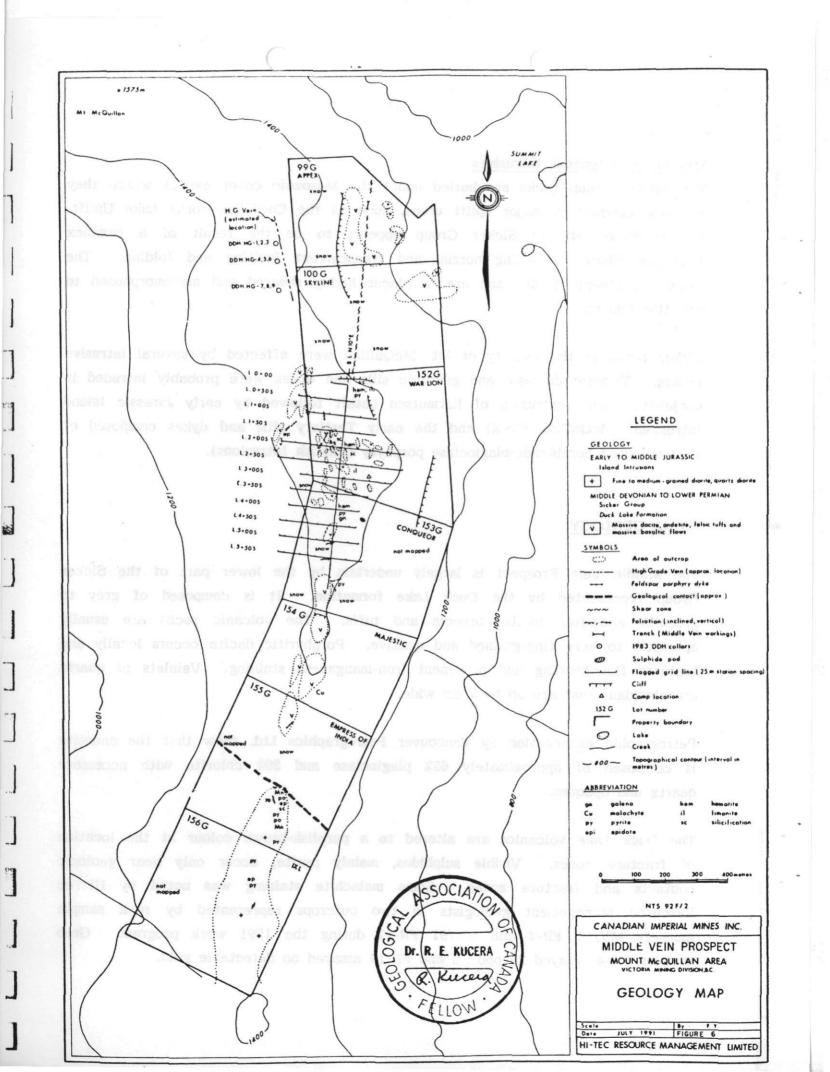
Sicker rocks in the vicinity of Mt. McQuillan were affected by several intrusive events. Triassic diabasic and gabbroic sills and dykes were probably intruded in conjunction with extrusion of Karmutsen basalt followed by early Jurassic Island Intrusions (McQuillan stock) and the early Tertiary sills and dykes composed of light-coloured hornblende-plagioclase porphyry (Catfish Intrusions).

#### LOCAL GEOLOGY

The Middle Vein Prospect is largely underlain by the lower part of the Sicker Group represented by the Duck Lake formation. It is composed of grey to greenish andesite, dacite, breccia and tuffs. The volcanic rocks are usually aphanitic to very fine-grained and massive. Porphyritic dacite occurs locally and features flow-banding and prominent iron-manganese staining. Veinlets of quartz are abundant that are up to 5 cm wide.

Petrographic examination by Vancouver Petrographics Ltd. show that the andesite is composed of approximately 65% plagioclase and 20% chlorite with accessory quartz and opaques.

The Duck Lake volcanics are altered to a purplish-brown colour at the location of fracture zones. Visible sulphides, mainly pyrite, occur only near geologic contacts and fracture zones. Some malachite staining was noted by Hi-Tec Resource Management geologists in two outcrops represented by rock sample numbers MV/91 FR-4 and MV/91 FR-17 during the 1991 work program. Grab samples FR-4 assayed 20 ppb Au and FR-14 assayed no detectable gold.



Mapping by Hi-Tec Resource Management shows that gabbro, diorite and quartzdiorite rocks (Island Intrusions) outcrop on the IXL and Empress of India claims, at the south end of the property (Figure 6). The writer also mapped gabbroic intrusive rocks on a portion of the Apex claim.

A thin-section of the gabbro show that it is fine to medium-grained, composed essentially of an intergrowth of plagioclose (50%) and pyroxene (40%). The plagioclase shows strong saussuritization. The rock is notably low in opaques.

Generally, the rocks are quite fresh and unaltered but show more epidote, chlorite, quartz-calcite veining and pyrite adjacent to the contact of the Duck Lake formation. Geological mapping indicates the contact is gradational within a zone of 30-50 metres. Within this zone both rock units are usually highly altered, and the volcanic rocks are light green with intense chlorite and sericitic alteration. Fractures are more intense with iron-manganese staining.

Mapping shows the presence of quartz-feldspar porphyry dikes in several places on the War Lion and Conqueror claims and also at the Middle Vein workings on the Apex claim. They are 1 to 2 metres wide and strike N 10 degrees E at the Middle Vein workings to N 20 degrees W at L+50S 0+65 W.

In thin-section, the porphyry of dacitic composition, is composed of phenocrysts of plagioclase (20%), quartz (15%) and minor altered mafics in a microgranular groundmass of fresh plagioclase (50%) with minor intergrowth quartz (6%) and chlorite (4%). The plagioclase phenocrysts show mild pervasive epidotization.

Early geological explorations refer to a mineralized vein on the property as the Middle Vein. The term Middle Vein as used in this report refers to narrow quartz lenses associated with a very well-defined structure, a 2-3 metre wide shear zone that strikes N10 degrees to 18 degrees E and dips 78 degrees to 85 degrees E. Although the shear zone can be traced on aerial photographs for a distance of at least 500 metres on the Apex, Skyline and War Lion claims (Figure 7), the associated quartz lenses are exposed only in the vicinity of the Middle Vein workings for 5 metres. Samples collected from the Middle Vein and shear zone are designated MV (see page 23).

The Middle Vein and associated shear is exposed in the early workings and in rock cuts adjacent to a small tributary creek located in the centre of the Apex claim (L99G). To the south, the shear zone is seen in a very steep rocky ravine on the Skyline claim (100G). This ravine owes its existence to differential erosion of the NNE trending shear zone.

According to Laanela (1989) the shear zone becomes hidden by a small snowbank on the War Lion claim (152G) but it probably continues farther south along the steep east slope of McQuillan ridge, where it trends northeast along the line of the old Crown Grants (L153G to 156G). (See Figure 5). Recent mapping by Hi-Tec Resource Management has not confirmed the presence of the shear zone nor the Middle Vein on the War Lion and Conqueror claims (Figure 6).

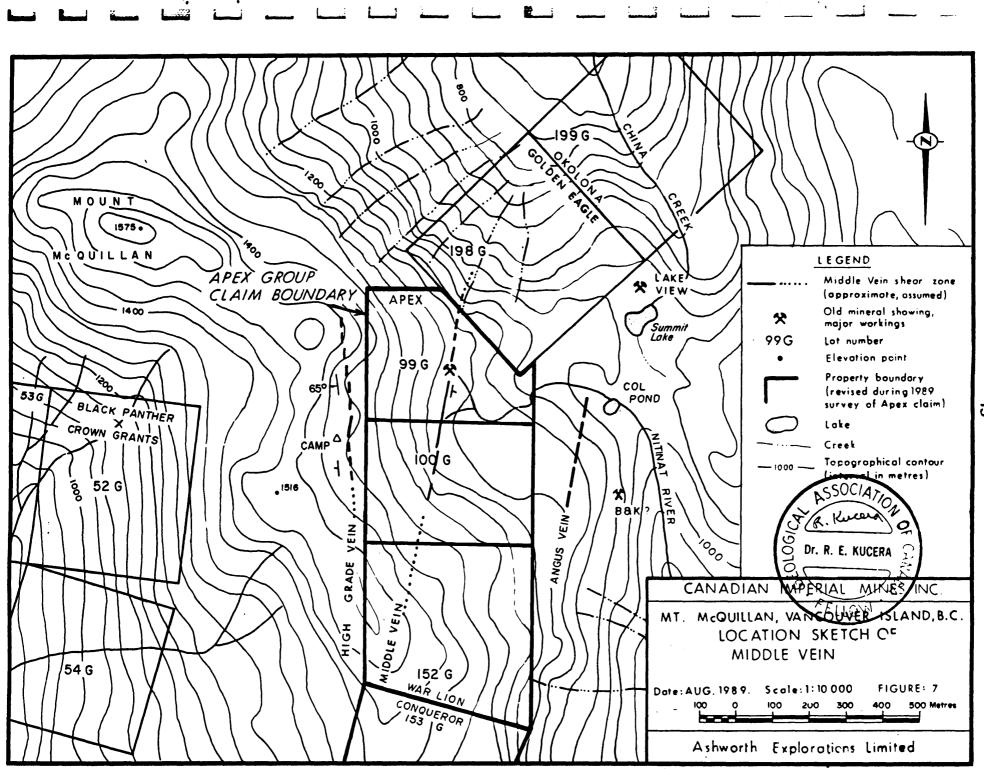
To the north, the veins and attendent shear zone, while being covered by overburden near the workings on the Apex claim, reappear in the China Creek headwaters, on the Golden Eagle claim. As Laanela (1989) points out, the Golden Eagle vein may be the northern extension of the Middle Vein, as both appear to have a similar attitude.

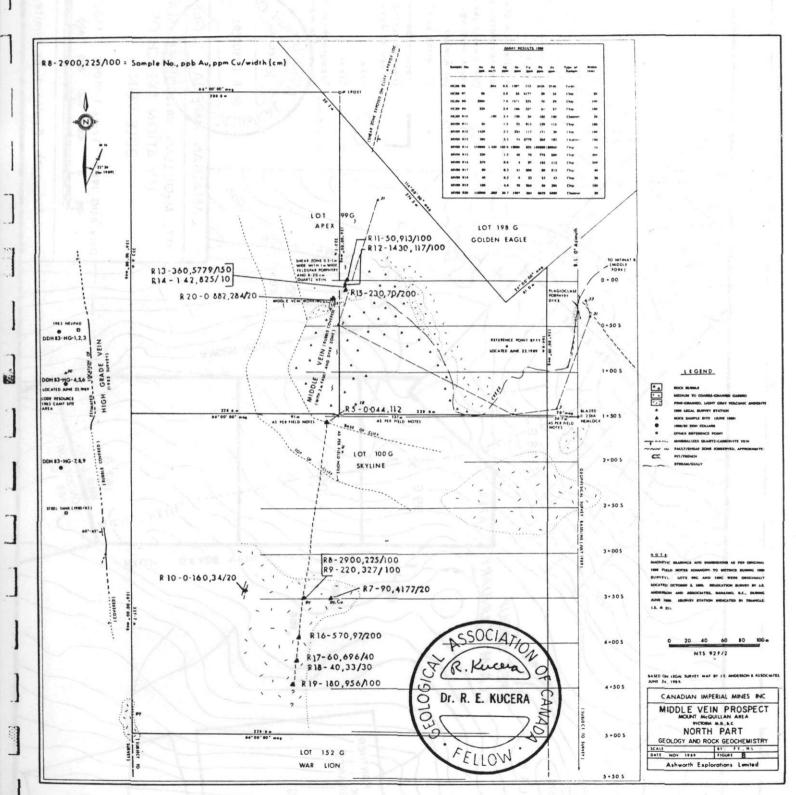
Immediately south of the Middle Vein workings, the Middle Vein structure is obscured for a distance of 110 metres by glacial debris, capped by rock rubble that was swept out of a ravine by debris flows and landslides from the eroded shear zone at the northern border of the Skyline claim. The presence of a quartz vein at depth is suggested by mineralized float located immediately downstream from its postulated trend.

#### Middle Vein Workings and Mineralization

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The fault zone at the Middle Vein workings on the Apex claim consists of two distinct shears. The main shear is exposed near the base of the rocky cliffs, just south of an east flowing stream. The shear is one metre wide and strikes N 18 degrees E and dips 78 degrees E. The shear cuts grey andesite that is moderately silicified and strongly weathered with light to dark brown rusty colour. Sulphide minerals are 1-2% fine-grained pyrite with traces of malachite.





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Mineralized quartz-carbonate lenses up to 10 cm thick and 5 metres long are hosted by sheared, rusty light to dark brown andesite. A 10 cm chip sample (MV89-14) across a quartz-carbonate vein assayed 1.42 oz/ton Au. Isolated pyrite-rich lenses occur in the andesite west of the shear zone. The andesite in this area is cut by intersecting joint sets of N 20 degrees W and N 40 degrees W.

The writer has observed another shear that occurs 14 metres west of the main shear. It is exposed at its top of 10 metre high bluff, along the south side of the same creek that flows past the main shear. The shear is .5 to 1.0 metre wide, strikes N 10 degrees E and dips 85 degrees E. This shear has not been sampled.

A light coloured feldspar-hornblende porphyry dike, 1-2 metres wide is found associated with this shear. The dike weathers a light brown. The feldspar porphyry dike, in which the vein occurs, is very similar in appearance to numerous Tertiary porphyry intrusions occurring elsewhere in the area. Refer to a petrographic analysis by Vancouver Petrographics of a specimen of this dyke material (Appendix F).

A mineralized quartz-carbonate vein, 8 to 20 cm wide is associated with the shear zone as mentioned in the above paragraphs. One channel sample MV89 R20 collected across 20 cm of quartz vein strikes N 10 degrees E, and dips 85 degrees E. The vein is mineralized with 20% sulphides mainly pyrite, chalcopyrite and galena. Copper staining is associated with light brown feldspar porphyry. Sample MV89 R20 assayed 0.88 oz/ton Au. An old trench, 2 metres long, occurs at creek level here. Another trench 20 metres to the south, attempted to reach the vein through rock rubble.

Samples MV89 R11 to MV89 R15 were collected from the Middle Vein structure (the shear zone) where a small quartz carbonate vein, 10 cm wide, is exposed for 5 metres. It is represented by chip sample MV89 R14 which returned a value of 1.42 oz/ton Au. Refer to Appendix A for the gold content and width of samples MV89 R11 to MV89 R15.

The writer has mapped gabbroic dike rock cutting massive andesite north of the creek about 80 metres east of the Middle Vein workings. It trends N 20 degrees to N 40 degrees W and is as much as 10 metres wide. Its southern extension is covered with overburden. (See Figure 8).

The strong shear structure and associated mineralized veins appear to terminate at this creek on the north side of the workings. Although overburden (landslides and moraine) mantle the bedrock north of the creek, it might be possible that lateral movement of a cross fault has offset this shear zone toward the northwest. Inspection of the aerial photographs reveal a subtle lineament that extends N40 degrees W from the northeast corner of the Skyline claim, across the "flat" area of the Apex claim where it fades out in the bedrock bluff northwest of the Middle Vein workings.

# **RECENT EXPLORATION**

Canadian Imperial Mines Inc. did work on the Apex Group property during June and July, 1989 under the direction of Mr. F. Yacoub, Project Geologist, Ashworth Explorations Ltd. This work included:

1. Established grid lines.

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- 2. Legal survey to relocate the Apex and Skyline claims on the ground by J.E. Anderson and Associates, Surveyors and Engineers.
- 3. VLF-EM and Magnetic survey by Ashworth Explorations Ltd. with interpretation by Mr. T. Matich, Geophysicist of Interpretex Resources Ltd.
- 4. At the request of Canadian Imperial Mines Inc., Dr. Kucera visited the property on October 16, 1989 and was accompanied by Mr. Yacoub. Dr. Kucera mapped a portion of the Apex claim and supervised sampling of the Middle Vein.

Hi-Tec Resource Management did work on the southern portion of the Middle Vein Prospect during June 1991. This work included geological mapping prospecting, rock sampling and a magnetometer and VLF-EM survey. Three kilometres of grid lines were surveyed on the War Lion and Conqueror claim blocks.

#### Geophysical Surveys

Ashworth Explorations Ltd. conducted a combined VLF-EM and magnetometer survey on the Apex and Skyline claims. The survey was run on an E-W line grid, totalling 3 line kilometres, using a Scintrex Omni Plus combined VLF-EM and magnetometer. A total of 12 lines, located at 50 metre intervals were established nearly perpendicular to the strike of the known vein system with station spacing at 12 metres.

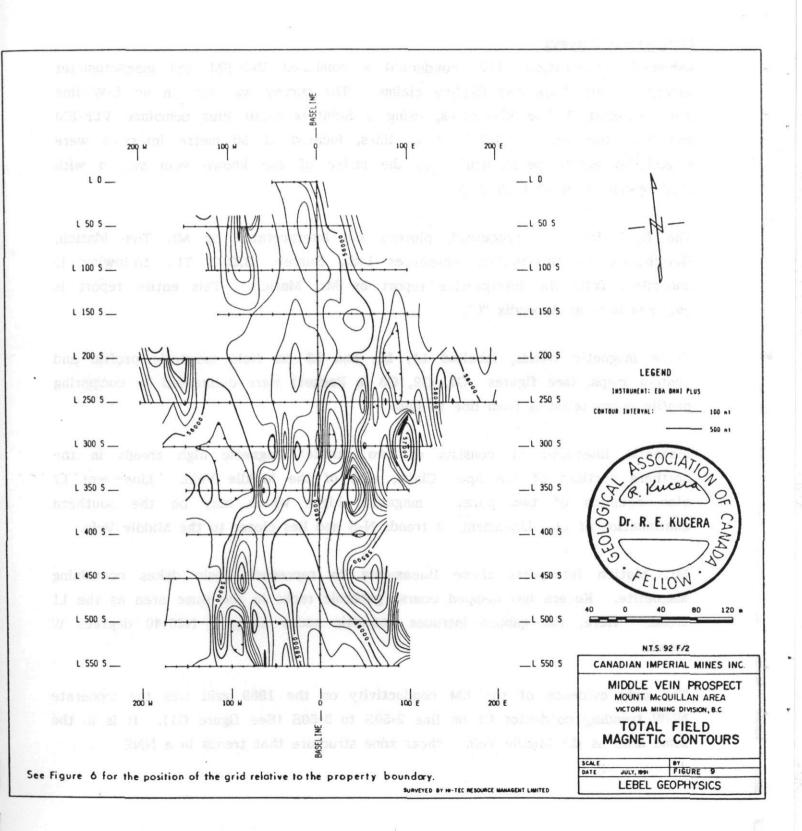
The field data was processed, plotted and interpretated by Mr. Tom Matich, Geophysist of Interpretex Resources Ltd., Surrey, B.C. The following is condensed from the interpretive report by Mr. Matich. This entire report is enclosed here as Appendix "C".

Three magnetic trends, labelled L1, L2, and L3 on field magnetic profile and contour maps, (see figures G1, G2, G3 in Pocket) were delineated by comparing profile characteristics from line to line.

Magnetic lineament L1 consists of two parallel magnetic high trends in the northern portions of the Apex Claim, east of the Middle Vein. Lineament L2 also consists of two parallel magnetic highs which may be the southern continuation of L1. Lineament L3 trends N-S and lies closer to the Middle Vein.

Mr. Matich interprets these lineaments to represent basic dykes containing magnetite. Kucera has mapped coarse gabbroic rocks in the same area as the L1 trend. Here, the gabbro intrudes andesitic rocks along a N20-40 degrees W trend.

The only evidence of the EM conductivity on the 1989 grid was the moderate NNW trending conductor C1 on line 2+50S to 3+50S (See figure G1). It is in the same area as the Middle Vein - shear zone structure that trends in a NNE



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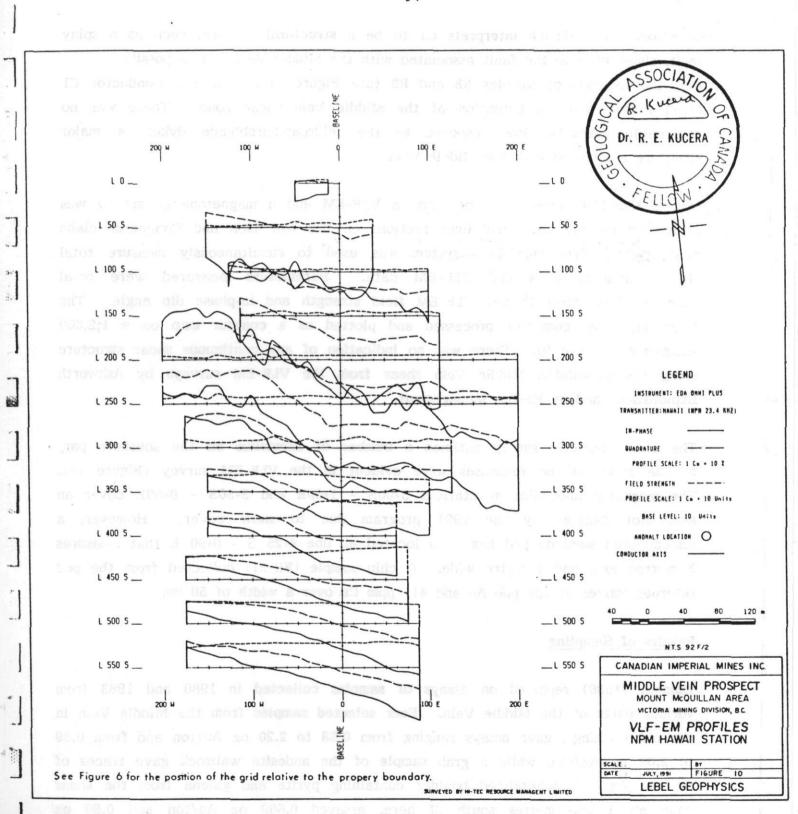
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direction. Mr. Matich interprets C1 to be a structural feature, such as a splay fault, subparallel to the fault associated with the Middle Vein. It is possible that the location of samples R8 and R9 (see Figure 7) are on the Conductor C1 trend rather than an extension of the Middle Vein shear zone. There was no noticeable magnetic low response to the feldspar-hornblende dykes or major structure associated with the Middle Vein.

During the 1991 exploration program, a VLF-EM and a magnetometer survey was performed on the 1991 grid over sections on the War Lion and Conqueror claim blocks. An EDA Omni-Plus system was used to simultaneously measure total field magnetics data and VLF-EM data. Parameters measured were total magnetic field strength and VLF-EM field strength and in-phase dip angle. The field data was computer processed and plotted as a contour map on a 1;2,000 scale map (Figure 9). There was no indication of any continuous shear structure along the postulated Middle Vein shear from the VLF-EM surveys by Ashworth Explorations and by Hi-Tec Management.

The 1991 magnetic survey outlined a number of anomolies on the southern part of the field but no responses were evident in the VLF-EM survey (Figure 10). The magnetic anomalies at stations 3+00S - 1+00E and 3+50S - 0+50E cover an area not mapped by the 1991 program due to snow cover. However, a disseminated sulphide pod has been located at line 4+25 S - 0+90 E that measures 3 metres long and 1 metre wide. A chip sample (FR-21) collected from the pod returned values of 130 ppb Au and 411 ppm Cu over a width of 50 cm.

## **Results of Sampling**

Laanela (1989) reported on assays of samples collected in 1980 and 1983 from various parts of the Middle Vein. Four selected samples from the Middle Vein in the old workings, gave assays ranging from 0.58 to 2.20 oz Au/ton and from 0.89 to 2.09 oz Ag/ton, while a grab sample of the andesite wallrock gave traces of Au and Ag. A mineralized boulder containing pyrite and galena from the shear zone about 200 metres south of here, assayed 0.689 oz Au/ton and 0.60 oz Ag/ton. No samples were taken from the shear zone at this locality. Chip

samples across one metre of the mineralized vein/dyke further to the south below the snowfield (Skyline Claim) assayed 0.028 oz Au/ton and 0.20 oz Ag/ton.

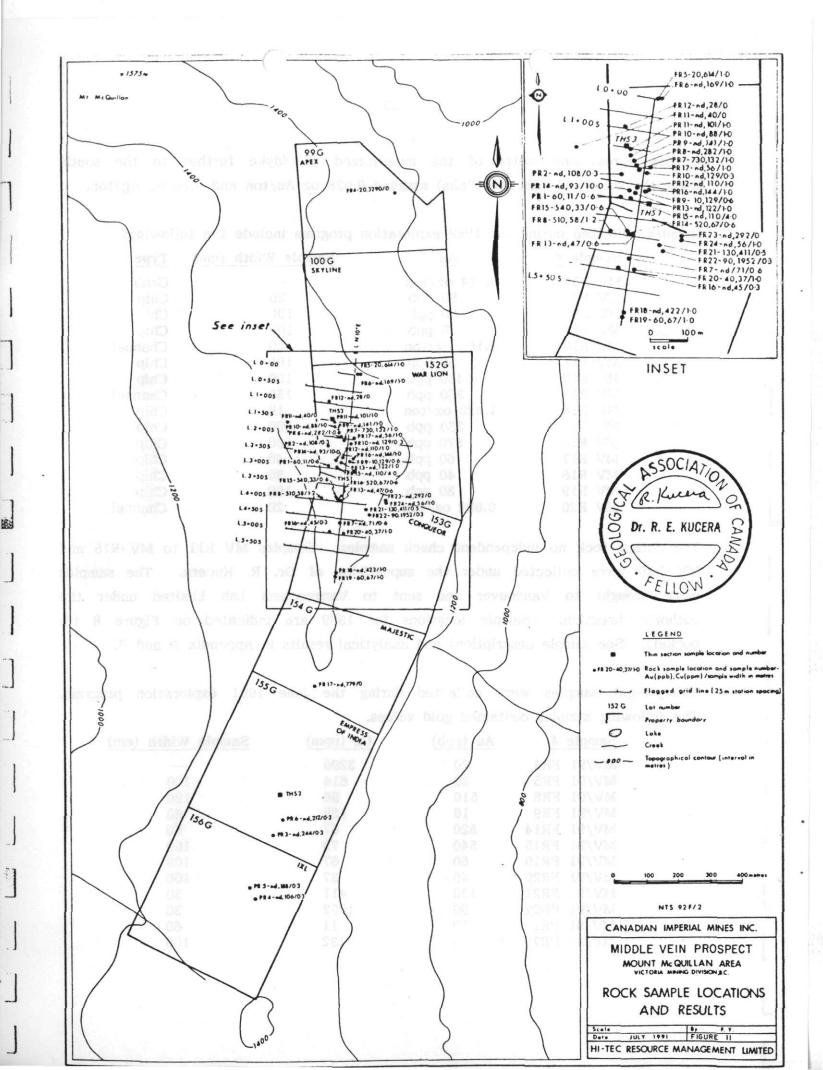
Samples collected during the 1989 exploration program include the following:

Sample Width (cm) Sample # Au Туре 0.044 oz/ton MV R5 Grab **MV R7** 90 ppb 20 Chip 2900 ppb **MV R8** 100 Chip MV R9 220 ppb 100 Chip **MV R10** 0.169 oz/ton20 Channel **MV R11** 100 Chip 50 ppb **MV R12** 1430 ppb 100 Chip Channel **MV R13** 360 ppb 150 **MV R14** 1.420 oz/ton10 Chip **MV R15** 230 ppb 200 Chip **MV R16** 570 ppb 200 Chip **MV R17** 60 ppb 40 Chip Chip **MV R18** 40 ppb 30 **MV R19** 80 ppb 100 Chip **MV R20** 0.882 oz/ton 20 Channel

The author took no independent check samples. Samples MV R11 to MV R15 and MV R20 were collected under the supervision of Dr. R. Kucera. The samples were brought to Vancouver and sent to Vangeochem Lab Limited under the author's direction. Sample locations for 1989 are indicated on Figure 8 (in pocket). See sample descriptions and analytical results in Appendix A and B.

Thirty-eight samples were collected during the June 1991 exploration program. The following samples contained gold values.

| Sample #   | <u>Au (ppb)</u> | Cu (ppm) | Sample Width (cm) |
|------------|-----------------|----------|-------------------|
| MV/91 FR4  | 20              | 3290     |                   |
| MV/91 FR5  | 20              | 614      | 100               |
| MV/91 FR8  | 510             | 58       | 120               |
| MV/91 FR9  | 10              | 129      | 60                |
| MV/91 FR14 | <b>520</b>      | 67       | 60                |
| MV/91 FR15 | 540             | 73       | 100               |
| MV/91 FR19 | 60              | 67       | 100               |
| MV/91 FR20 | 40              | 37       | 100               |
| MV/91 FR21 | 130             | 411      | 50                |
| MV/91 FR22 | 90              | 1952     | 30                |
| MV/91 PR1  | 60              | 11       | 60                |
| MV/91 PR7  | 730             | 132      | 100               |



Rock sample locations and analytical results for gold and copper are plotted on Figure 11 at a scale of 1:5,000.

Summary statistics for 38 rock sample analyses for Au and Cu suggest that 60 ppb Au and 130 ppm Cu might be considered geochemically anomalous and >500 ppb Au and >400 ppm Cu as highly anomalous. No predictable relationship exists between high Au and high Cu values. Because of the small sample of Au and Cu values, a statistical test is not easily supported.

#### CONCLUSIONS AND RECOMMENDATIONS

The 1980 and 1983 program by Lode Resources, and the 1989 work program by Ashworth Explorations Limited and the 1991 program by Hi-Tec Resource Management on the Middle Vein Prospect have demonstrated the presence of gold. Gold values range up to 2900 ppb across 100 cm of the shear zone whereas individual quartz-carbonate veins assay up to 1.4 oz Au/ton across widths of up to 10 cm. Exploration potential of the Middle Vein Prospect is judged to be good. Further development of this property is justified.

A two-stage program is recommended to explore the Middle Vein on the surface and at depth. The initial stage consists of aerial photo coverage, stereo-photo interpretation, compilation of a topographic base map, legal surveys, detailed geologic mapping, extensive sampling and surface trenching. The second stage of work, contingent on obtaining encouraging results from the first stage, is also recommended. This stage consists of 600 metres of diamond drilling to explore the Middle Vein at depth.

# STAGE I

## Aerial Photographs - Base Map

Low-level aerial photographs should be obtained of the property and used for stereo-photo interpretation and compilation of a topographic base-map. Careful stereoscopic examination of the aerial photos will help delineate rock types, locate very subtle fractures and facilitate tracing of the NNE shear-vein structure on the steep slopes of the southernmost claims.

Because of abrupt topographic relief on the property, a map produced directly from photo overlays will exhibit severe scale differences across the map area. Because of this, I recommend that a topographic map be compiled from the aerial photos. Using this map as a base, the geologic information on the aerial photos can be transferred to the base map, including all mineral outcroppings, trenches and sample locations.

#### Geological Mapping - Prospect the Middle Vein

Trace the vein structure and sample the Middle Vein particularly toward the south along the main ridge. Any new mineralized zones should be examined and sampled. Helicopter reconnaissance and stereoscopic study of the aerial photographs will prove useful.

#### Legal Survey

Claim boundaries on the southern part of the property may also have to be relocated on the ground by legal survey, similar to the recent survey on the Apex and Skyline claims. The location of the Middle Vein should be surveyed and accurately shown on the base map.

## Trenching

Trenching by a small backhoe, brought in by helicopter, has to be considered the next logical step to explore the vein below the surface.

# STAGE II

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## Drilling Program

I recommend a diamond drilling program, initially on the Apex Claim. Drill sites would be on gently sloping ground east of the Middle Vein and have a nearby water supply.

Drill sites located approximately 40 metres east of the shear-vein structure seem reasonable. Drill holes at - 45 will intersect the vein at depths ranging from 40 to 60 metres. Additional holes at - 70 should be drilled from the same initial set-ups.

Drilling along additional sections farther to the south should then be considered if the results of surface sampling warrant it. Although the topography is quite precipitous, a few drillsites could be located south of the rocky ravine on the Skyline and War Lion claims.

# RECOMMENDED PROGRAM AND COST ESTIMATES

# Stage I

| Establish additional grid - 10 km      | 1,500    |
|--|----------|
| Topographic Base Map from photos       | 4,000    |
| Aerial Photo Interpretation            | 2,500    |
| Geologic Mapping (20 days @ \$500/day) | 10,000   |
| Sampling (250 samples @ \$40/sample)   | 10,000   |
| Legal Surveys                          | 7,500    |
| Transportation (helicopter @ \$600/hr) | 18,000   |
| Trenching                              | 8,000    |
| Reporting and Administration           | 7,000    |
| Contingency Allowance                  | 6,500    |
| ESTIMATED STAGE I COSTS                | \$75,000 |

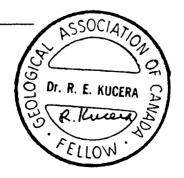
# Stage II

A second stage program contingent on obtaining encouraging results from Stage I is recommended. It would include diamond drilling to test the middle vein at depth, assays and further geological work.

**KUCERA & ASSOCIATES CONSULTANTS** 

Richard E. Kucara

Richard E. Kucera, Ph.D.



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- Stevenson J.S., 1945: Geology and ore deposits of China Creek area, Vancouver Island, B.C., in Annual Report of B.C.M.M., 1944, pp. A143-A161.

#### CERTIFICATE OF QUALIFICATION

- I. Richard E.Kucera, hereby certify:
- That I am an associate of Kucera & Associates Consultants of #201, 810 1. West Broadway, Vancouver, B.C., V5Z 4C9.
- That I am a Fellow of the Geological Association of Canada and a Member 2. of the American Association of Petroleum Geologists and Geological Society of America.
- That I hold B.Sc. and M.Sc. degrees from Ohio State University, U.S.A. and 3. a Ph.D. from the University of Colorado, U.S.A.
- That I have been practicing my profession as a Geologist for over 25 years. 4.
- That I have no direct or indirect interest nor do I expect to have any 5. direct or indirect interest in the properties or securites of Canadian Imperial Mines Inc. I have no direct or indirect interest in the properties of the vendor.
- That the statements made in Kucera & Associates Consultants report of July 6. 15, 1991 on the Middle Vein Prospect were based on an examination of the property on October 16, 1989 and from information as specified in the report.
- That the report has been prepared for exclusive use of participants of the 7. project and no part of it shall be reproduced, distributed or made available to any other person, company, regulatory body or organization without the complete context of the report or without my permission.
- 8. Consent is hereby granted to use the report, in its complete form only, in a Filing Statement, Statement of Material Facts, or Prospectus by Canadian Imperial Mines, Inc.

Dated at Vancouver this 20th day of September, 1991.

Richard E. Kucera, Ph.D.

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# APPENDIX A

# ROCK SAMPLE DESCRIPTIONS

(1989, 1991)

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### MIDDLE VEIN PROSPECT

## ROCK SAMPLE DESCRIPTIONS

| Sample No. | Sample Description   | Width<br>(cm) | Au<br>ppb      |
|------------|--|---------------|----------------|
| HG89 R7    | Chip sample across 20 cm of altered grey,<br>fine-grained volcanic andesite, quartz vein<br>3 cm wide mineralized with 2% fine-grained<br>pyrite, minor green malachite. Sample taken<br>at L3+50 S 2+70 W.  | 20            | 90             |
| HG89 R8    | Chip; shear zone of light brown buff volcanic<br>andesite, rusty on weathering surface hosting<br>quartz vein 5 cm wide, mineralized with $1$ %<br>pyrite, vugs filled with dark oxide minerals.<br>Sample across the shear zone and the vein at<br>3+50 S $3+00$ W. | 100           | 2900           |
| HG89 R9    | Chip; shear zone of light to dark brown altered<br>volcanics with slickenside striated surface,<br>20% dark brown rusty oxides in vugs, minor<br>silicification. Sample at L 3+50 S 3+00 W.  | 100           | 220            |
| HG89 R10   | Channel; quartz vein, 10 cm wide, massive<br>quartz in a shear zone strikes N 10 E, dipping<br>75 W, mineralized with 2% fine-grained pyrite,<br>1% chalopyrite, minor galena, the vein exposed<br>at L3+40 S 3+60 W.  | 20            | .169<br>oz/ton |
| MV89 R11   | Chip; well defined shear zone, dark grey<br>andesite moderately silicified with 5% quartz,<br>rusty oxedized sulphide on weathered surface<br>quartz-carbonate vein up to 5 cm wide, strikes<br>N18 E, dips 78 E.  | 100           | 50             |
| MV89 R12   | Chip; shear zone, grey andesite, some silifica-<br>tion, 1-2% fine-grained pyrite, weathered buff<br>to dark brown, quartz vein up to 3 cm wide.   | 100           | 1430           |
| MV89 R13   | Channel, quartz-carbonate vein 10 cm wide<br>fine-grained volcanic andesite with minor<br>silicification, 1-2% pyrite.   | 150           | 360            |

| Sample No. | Sample Description   | Width<br>(cm) | Au<br>ppb                   |
|------------|--|---------------|-----------------------------|
| MV89 R14   | Chip across 10 cm wide quartz carbonate vein<br>up to 8% sulphides (5% pyrite, 3% chalopyrite)<br>and copper staining, intercalated with grey<br>andesite, vein at contact with shear zone (east)<br>and grey andesite (west), fine-grained sulphides,<br>pyrite decrease from about 8% at contact of<br>andesite and vein to less than 1% in the<br>andesite in a distance of 100 cm. | 10            | >10,000<br>(1.42<br>oz/ton) |
| MV89 R15   | Chip across two metre, shear zone, aphanitic andesite moderatly silicified with 10% quartz.  | 200           | 230                         |
| MV89 R16   | Chip; well defined shear zone, buff to dark<br>brown, rusty fine-grained volcanic andesite,<br>1-2% fine-grained pyrite dissemination, minor<br>silicification. Slickenside and scratched<br>surface two metres wide, strikes N 10 E.  | 200           | 570                         |
| MV89 R17   | Chip across 40 cm of massive, barren quartz<br>lense in a shear zone of buff fine-grained<br>volcanic andesite, no obvious sulphides.  | 40            | 60                          |
| MV89 R18   | Chip across 30 cm of the same quartz lense as above in R17. No sulphides.  | 30            | 40                          |
| MV89 R19   | Chip sample collected across one metre of a shear, dark brown, rusty fine-grained volcanic andesite with 1-2% fine-grained disseminated pyrite.  | 100           | 180                         |
| MV89 R20   | Channel sample collected across 20 cm of<br>quartz vein, strikes N 10 E, dips 85 E,<br>mineralized with 20% sulphides, copper<br>staining, associated with light brown feldspar<br>porphyry.   | 20            | >1000<br>(.882<br>oz/ton)   |

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## ASSAY RESULTS 1989

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| Sample No | . Au<br>ppb | Au<br>oz/t | Ag<br>ppm | As<br>ppm | Cu<br>ppm | Pb<br>1 ppm | Zn<br>ppm | Type of<br>Sample | Width<br>(cm) |
|-----------|-------------|------------|-----------|-----------|-----------|-------------|-----------|-------------------|---------------|
| HG89 R5   |             | .044       | 6.5       | 1287      | 112       | 3435        | 3740      | Grab              | <b>_</b>      |
| HG89 R7   | 90          |            | 2.0       | 55        | 4177      | 39          | 32        | Chip              | 20            |
| HG89 R8   | 2900        |            | 7.6       | 1571      | 225       | 70          | 29        | Chip              | 100           |
| HG89 R9   | 220         |            | 2.9       | 106       | 327       | 51          | 57        | Chip              | 100           |
| HG89 R10  |             | .160       | 3.4       | 198       | 34        | 182         | 160       | Channel           | 20            |
| MV89 R11  | 50          |            | 1.5       | 23        | 913       | 129         | 115       | Chip              | 100           |
| MV89 R12  | 1430        |            | 2.5       | 224       | 117       | 171         | 39        | Chip              | 100           |
| MV89 R13  | 360         | •          | 3.3       | 74        | 5779      | 358         | 183       | Channel           | 150           |
| MV89 R14  | >10000      | 1.420      | >50.0     | >2000     | 825       | >20000>     | 20000     | Chip              | 10            |
| MV89 R15  | 230         |            | 1.2       | 46        | 70        | 778         | 590       | Chip              | 200           |
| MV89 R16  | 570         |            | 0.6       | 4         | 97        | 103         | 113       | Chip              | 200           |
| MV89 R17  | 60          |            | 0.3       | 41        | 696       | 88          | 213       | Chip              | 40            |
| MV89 R18  | 40          |            | 0.2       | 9         | 33        | 53          | 43        | Chip              | 30            |
| MV89 R19  | 180         |            | 4.6       | 70        | 956       | 66          | 395       | Chip              | 100           |
| MV89 R20  | >10000      | .882       | 30.7      | 1997      | 284       | 6828        | 5860      | Channel           | 20            |

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## MIDDLE VEIN PROSPECT

## Rock Sample Descriptions

1991

| Sample No. | Description   | Width (cm) |
|------------|---|------------|
| FR - 4     | Grab Sample; rusty, dark grey to black massive<br>volcanic basalt, mineralized with copper staining<br>trace of fine-grained pyrite.  |            |
| FR - 5     | Chip sample across one metre of altered, light grey<br>massive volcanic andesite, strong hematitic alteration,<br>silicification with fine to very fine-grained pyrite.   | <b>100</b> |
| FR - 6     | Chip; altered limonitic volcanic andesite outcrop,<br>1% fine-grained pyrite.   | 100        |
| FR - 7     | Brecciated light brown altered volcanic outcrop,<br>moderate limonitic alteration, no sulphides. Chip<br>sample over 60 centimetres.  | 60         |
| FR - 8     | Chip sample across 120 centimetres of feldspar-<br>hornblende porphyry dyke, light brown hematite along<br>fractures, altered hornblende.   | 120        |
| FR - 9     | Weathered, altered light grey, fine-grained volcanic<br>andesite, moderate silification with up to 3% secondary<br>quartz, fractures oriented N-20 degrees east filled<br>with oxides (limonite). Chip sample over 60 centimetres                       | 60<br>5.   |
| FR - 10    | Silicified zone hosted by fine-grained volcanic<br>andesite, secondary quartz in cavities, the zone exposed<br>for 5 metres, 30 centimetres wide. Chip over the width<br>of the zone.   |            |
| FR - 11    | Grab; light grey, fine-grained volcanic andesite<br>outcrop, quartz veinlets up to 1 cm wide, minor epidote   |            |
| FR - 12    | Grab; strong silicified zone at the contact between feldspar porphyry dyke and basic altered volcanic andesite, 25% brown, rusty hematite.  |            |
| FR - 13    | Chip; silicified zone of subcrop volcanic andesite<br>with up to 20% brown, hematitic quartz disseminated<br>with <1% very fine-grained pyrite, trace of galena,<br>the zone can be followed for 10 metres, 60 centimetres<br>wide, strike 240 degrees. | 60         |

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| Sample No. | Description  | Width (cm |
|------------|--|-----------|
| FR - 14    | Chip sample collected from the same silicified zone as in FR-13, possible native copper.   | 60        |
| FR - 15    | Chip; altered bleached volcanic andesite (subcrop), strong silicification, $<1$ % sulphides mainly pyrite and galena, 10% manganese oxide.   | 60        |
| FR - 16    | Chip; small fracture zone within massive dark grey<br>volcanic outcrop, .5 cm quartz vein strike 320 degrees,<br>hosted by the same outcrop. No mineralization.                          | 30        |
| FR - 17    | Grab; fresh, light green plagioclase porphyry dyke<br>strike N-10 degrees east, small 2-3 cm bands of<br>malachite staining. The dyke is two metres wide hosted<br>by volcanic andesite. |           |
| FR - 18    | Altered bleached volcanic andesite, rusty dark brown<br>Fe02, <1% fine-grained disseminated pyrite. Shear zone<br>strike 240 degrees exposed for 10 metres. Chip over<br>1 metre.        | 100       |
| FR - 19    | The same as FR-18. Chip sample taken across another<br>shear zone strike 310 degrees, 10 metres north of FR-18<br>Chip over one metre across the shear zone.                             | 100<br>3. |
| FR - 20    | Chip; quartz lense, brown hematitic quartz <1% pyrite<br>dissemination, hematite staining between fractures.<br>Light grey fine-grained silicified volcanic andesite<br>host rock.       | 100       |
| FR - 21    | Sulphide pod 3 metres long, 50 centimetres wide,<br>strike 290 degrees, mineralized with 5% oxidized fine-<br>grained pyrite.  | 50        |
| FR - 22    | Reddish to dark brown bleached volcanic outcrop,<br>moderate to strong manganese oxide. Chip across 30 cm  | 30<br>ns. |
| FR - 23    | Grab; light grey slightly mineralized volcanic andesite outcrop, <1% disseminated pyrite, trace of galena.   |           |
| FR - 24    | Chip across 1 metres of disseminated volcanic andesite <1% fine-grained pyrite intense oxidation, limonite veinlets.   | 100       |

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| Sample No. | Description   | Width (cm |
|------------|---|-----------|
| PR - 1     | Slightly sheared basic volcanics, trace of fine-<br>grained pyrite, Mn stain/Fe rust. Chip over 60 cms.   | 60        |
| PR - 2     | Silicifed dark grey volcanic andesite outcrop, quartz<br>veinlets up to 15 mm thick. No visible mineralization.<br>Chip sample over 30 cms.   | 30        |
| PR - 3     | Intrusive diorite 60% plagioclase, 40% hornblende,<br>quartz veinlets 1 mm, <1% pyrite. Fractures within<br>the rocks 146 degrees/70 west, Mn-staining. Chip<br>sample over 30 cms.   | 30        |
| PR - 4     | Fine to very fine-grained diorite hosting quartz<br>veinlets <1 cm, fractures/joints 20 degrees/90 degrees.<br>Chip sample.   | 30        |
| PR - 5     | Chip; fine to medium-grained diorite, 2% disseminated pyrite, 1% in quartz veinlets 2 mm thick.   | 30        |
| PR - 6     | Chip; medium-grained intrusive diorite intercalated<br>with altered to light grey volcanics (contact zone)<br>up to 5% disseminated pyrite, chalcopyrite, 1-2 mm<br>quartz veinlets.  | 30        |
| PR - 7     | Chip sample over 1 metre of shear zone trending 315<br>degrees, dip approximately 80 degrees west, quartz<br>veins 1-15 mm within the zone disseminated with 1%<br>pyrite and galena, hosted by slightly sheared basic<br>volcanics with strong Mn stain and Fe rust. | 100       |
| PR - 8     | The same shear zone as PR-7 quartz veins 2-40 mm with 2% Py <1% galena hosted by slightly sheared volcanics with intense Mn and Fe staining. Chip sample over 1 metre.  | h 100     |
| PR - 9     | The same shear zone on the same trend as PR-7 and PR-8, quartz vein $\langle 2 \text{ cm} \text{ wide}, 1\%$ disseminated pyrite, hosted by basic volcanic andesite. Chip over 1 metre of the shear zone.   | 100       |
| PR - 10    | Quartz veinlets, swarms and blebs $\langle 2 \text{ mm up to } 7\%$ pyrite in volcanic host, along the same trend with PR-7, PR-8 and PR-9. Chip sample over 1 metre.   | 100       |
| PR - 11    | Slightly sheared dark volcanic andesite, silicification<br>with up to 3% pyrite dissemination along the same<br>strike as PR-7 - PR-10. Chip sample.  | 100       |

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| Sample No. | Description  | Width (cm) |
|------------|--|------------|
| PR - 12    | Sheared basic volcanics with quartz blebs/veinlets,<br>1% disseminated pyrite, Fe/Mn stained. Chip sample.   | 100        |
| PR - 13    | Sheared zone of basic volcanics, 1% disseminated pyrite, Fe/Mn stained, quartz blebs and quartz veinlets. Chip sample over 1 metre.                            | 100        |
| PR - 14    | Chip; porphyritic basic unaltered volcanic, <5 mm phenocrysts, flow/shear texture aligned with fractured direction 360 degrees/90 degrees.                     | 1000       |
| PR - 15    | Chip over 4 metres of sheared basic volcanics, 2% disseminated pyrite. Shearing 309 degrees and vertical, fractures at 301 degrees/70 degrees south.           | 400        |
| PR - 16    | Grey, reddish basic volcanic hosting quartz veinlets with 1% disseminated pyrite chip over 1 metre.  | 100        |
| PR - 17    | Highly silicified basic volcanics, white and red<br>bleached, rusted rocks with >30% quartz; Fe/Mn stained<br>3% Py mostly oxidized. Chip sample over 1 metre. | 100        |

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## APPENDIX B

ANALYTICAL RESULTS (1980, 1983, 1989, 1991)

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| 130 Pumb<br>North Val<br>Canada V | ndorver, B.C.<br>77 283<br>04) 985-0681 |                                   |                      |           |                  | EC        | ND          |                  | ·····            |           |           |           | Geoche<br>Lab F | emical<br>leport   |
|-----------------------------------|---|-----------------------------------|----------------------|-----------|------------------|-----------|-------------|------------------|------------------|-----------|-----------|-----------|-----------------|--------------------|
|                                   |   | Mf                                | . Mc                 | Quil      | 1c.              | (         |             |                  |                  | RECE      | EIVEI     | ) O C T 2 | 1 198           | 3                  |
| REPORTS                           | 123-3260                                |                                   |                      |           |                  |           |             |                  | PROJEC           | T: NOME 6 | SIVEN     | PA        | 6E 1            |                    |
| SAMPLE<br>MUNDER                  | ELENENT<br>UNITS                        | Cu<br>PPN                         | Pb<br>PPN            | Zn<br>PPN | <b>Ad</b><br>PPN | Au<br>PPB | NOTES       | SAMPLE<br>NUMBER | ELEHENT<br>UNITS | Cu<br>PPN | РЪ<br>РРН | Zn<br>PPH | As<br>PPN       | Au<br>PPB          |
| R 12905                           | ¥ Hiddl                                 | e Vain                            | 20005                | 84 7 =    | < <0.2           |           | = 20.000146 | ₿ 12860          | $\uparrow$       |           |           | 0.11972 = | = 4,1           | <b>60</b> 0.       |
| 130 Pass<br>North Vi<br>Canada    | 604) 985-0681                           | L <b>A</b> .                      |                      |           |                  |           |             |                  | n Diteite<br>E F |           |           |           | Cert<br>of A    | ificate<br>nalysis |
|                                   |   |                                   |                      |           |                  |           |             | <u></u>          | R                | ECEIV     | EDI       | IOV 7     | 1983            |                    |
| EPORT: 4                          | 123-3491                                |                                   |                      |           |                  | }         |             |                  | PROJECT          | I; HIGH G | ADE       | · 146     | E 1 .           |                    |
| anple<br>undet:                   | ELENENT<br>HNITS                        | · Au<br>OPT                       | As<br>DP1            |           |                  |           | HOTES       |                  |                  | · ·       |           |           |                 |                    |
| 87383<br>87384<br>87385<br>87386  | HVain                                   | 0.002-<br>0.548<br>0.061<br>0.902 | 0.71<br>0.14<br>0.02 | } ~~~     | hit in           | Vei.      | ×           |                  |                  |           |           |           | •               |                    |
|                                   |   |                                   |                      |           |                  |           |             |                  |                  |           |           |           |                 |                    |
| <br>                              |   |                                   |                      |           |                  |           |             |                  |                  |           |           |           |                 |                    |
|                                   |   | ·                                 |                      |           |                  |           |             |                  |                  |           |           |           |                 |                    |
|                                   |   |                                   |                      |           |                  |           |             |                  |                  |           |           |           |                 |                    |
|                                   |   |                                   |                      |           |                  |           |             |                  |                  |           |           |           |                 |                    |
| 2                                 |   |                                   |                      |           |                  |           |             |                  |                  |           |           |           |                 |                    |
|                                   |   |                                   |                      |           |                  |           |             |                  |                  |           |           |           |                 |                    |
|                                   |   |                                   |                      |           |                  |           |             |                  |                  |           |           |           |                 |                    |
|                                   |   | ·                                 |                      |           |                  |           |             |                  |                  |           |           |           |                 |                    |

| Beening Orge & Company Ltd.<br>130 Pemberion Ave.<br>North Vancouve, B.C.<br>Canada V7F 285<br>Phone: (60) 985-0681<br>Telen: 04-352667   |                           | BONDA           | R-CLEGG             | Certificate<br>of Analysis             |
|---|---------------------------|-----------------|---------------------|--|
| EPORT: 423-3284   |                           | ]               | PROJECT: NOME GIVEN | PAGE 1                                 |
| ANPLE ELEMENT AU<br>UMRER UNITS OPT   |                           | Zn NOTES<br>PCT |                     |  |
| 12812 Middle (0.002<br>12813 Van (0.002<br>12814 Van <u>0.028</u>   | 2 0.04<br>3 0.10 - M.V. e | 0.19 - 1+10     |                     | 4 Urn pj *go<br>2420 15602 16.0 > 1960 |
| Bander-Chag & Company Ltd.<br>130 Penderton Ave.<br>North Venctorer, B.C.<br>Classite V77 223<br>Phone (400) 925-0811<br>Teles: 04:352467 |                           |                 |                     | Certificat<br>of Analyzi               |
| REPORT: 423-3140  |                           |                 | PROJECT; NONE STU   | EN PHE 1                               |
|   | Au Ad<br>PT gPT           | NOTES           |                     |  |
| R 12804 JAV 9.64  | 89 9.60 ti                | d'e van         |                     |  |
|   |                           |                 |                     |  |
| •   |                           |                 |                     |  |
|   |                           |                 |                     |  |
|   |                           |                 |                     |  |



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VANGEOCHEM LAB LTD. 1521 PEMBERTON AVE., NORTH VANCOUVER, B.C., CANADA V7P 2S3

TELEPHONE: 986-5211 AREA CODE: 604

• Specialising in Trace Elements Analyses •

# **Certificate of Geochemical Analyses**

-IN ACCOUNT WITH-Lode Resources Corp. Suite 1020 - 475 Howe Street Vancouver, B.C. V6C 2B3 Attention: Report No:83-01-046Page 1of 1Samples Arrived:October 3, 1983Report Completed:October 13, 1983For Project:MIDDLE VEINJob No.83-381Analyst:D. ChiuInvoice No.7554

|   | GEOCH                   | and the second se |             | ASSA        |                 |                                   |
|---|-------------------------|---|-------------|-------------|-----------------|-----------------------------------|
| Sample Marking  | Ag<br>ppm               | Au<br>ppb   |             | Ag<br>oz/st | Au<br>oz/st     |                                   |
| N. EXTENTION  | 2.3                     | 345   |             |             |                 | D. O. MAY IN                      |
| N. EXTENTION SOIL   | 2.5                     | 1475  |             |             | -               | Saloy MhV, to N                   |
| N. EXTENTION ROCK   |                         |   |             | 9.11        | 0.018<br>% 0.02 | Thead with of<br>threach (G.E. () |
|   | السينية (منا<br>منها ال |   | -           | • • • •     |                 |                                   |
|   |                         |   |             |             |                 |                                   |
| Mequician   | -M.                     | idle  | Vein        | -c/         | ie /7           | sounth.                           |
| الحال الجمالية المحاج مورد الم  |                         | L   |             | P           |                 |                                   |
|   |                         |   |             |             |                 |                                   |
| n an a star an  | · · · ·                 | • • •   |             |             |                 |                                   |
|   |                         |   |             |             |                 |                                   |
| n a tra an  | <b>.</b>                | n in <b>Fr</b><br>North   |             |             |                 |                                   |
|   |                         |   |             |             |                 |                                   |
| taning second | -                       |   |             |             |                 |                                   |
| ****  |                         |   |             |             |                 |                                   |
| n daar tee oo ah  |                         |   |             |             |                 |                                   |
| MARKS: One copy se  | nt to Ash               | worth Expl  | L           | Ltd.        | Provincia       | al Registered/Assaye              |
|   |                         | <b>·</b> ·  |             |             | Signed          | 122.                              |
| MG x 1.6683 - % MoSa 1 Tr   | ory oz./ton = 34        | 1.28 pom  | 1 pom = 0.0 | 001%        | nd = none det   | ected . pom = parts per mul       |

# C VANGEOCHEM LAB LIMITED

MAIN OFFICE 1988 TRIUMPH ST VANCOUVER, B C V5L 1K5 • (604) 251:5656 • FAX (604) 254:5717 BRANCH OFFICES PASADENA, NI LD BATHURST, N B MISSISSAUGA, ON1 RENO, NEVADA, U S A

# ASSAY ANALYTICAL REPORT

CLIENT: ASHWORTH EXPLORATION LTD.DATE: AUGUST 2 1989ADDRESS: 718 - 744 W. HASTINGS ST..: Vancouver, B.C..: VEC 1A5.DB#: 890403

PROJECT#: HG SAMPLES ARRIVED: AUGUST 1 1989 REPORT COMPLETED: AUGUST 2 1989 ANALYSED FOR: Au INVOICE#: 890403 NA TOTAL SAMPLES: 2 REJECTS/PULPS: 90 DAYS/1 YR SAMPLE TYPE: 2 ROCK

SAMPLES FROM: ASHWORTH EXPLORATION LTD. COPY SENT TO: ASHWORTH EXPLORATION LTD.

PREPARED FOR: CLIVE ASHWORTH

ANALYSED BY: Raymond Chan

SIGNED:

L'Ege-22-2-

Registered Provincial Assayer

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GENERAL REMARK: None



|                          | HEM LAB LIMITE     | MAIN OFFICE<br>1988 TRIUMPH ST<br>VANCOUVER, B C V5L 1K5<br>• (604) 251-5656<br>• FAX (604) 254 5717 | BRANCH OFFICES<br>PASADENA, NELD<br>BATHURST N B<br>MISSISSAUGA ONT<br>RENO NEVADA U S A |
|--------------------------|--------------------|--|--|
| REPORT NUMBER: 890403 AA | JOB WUMBER: 890403 | ASHWORTH EXPLORATION LTD.  | PAGE 1 OF 1  |
| SAMPLE #                 | Au<br>oz/st        |  |  |

| R-5  | .044 |
|------|------|
| R-10 | .169 |

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DETECTION LIMIT 1 Troy oz/short ton = 34.28 ppm .005 1 ppa = 0.00011

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ppm = parts per million < = less than</pre>

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signed:

#### 1988 Triven Street, vancouver, B.c. VSL 1KS Ph: (604) 251-5656 Fax: (604) 254-5717

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#### ICAP GEOCHEMICAL ANALYSIS

#### A .5 gram sample is digested with 5 ml of 3:1:2 HCl to HNO, to HyO at 95 °C for 90 minutes and is diluted to 10 ml with water. This leach is partial for Al, Ba, Ca, Cr, Fe, K, Mg, Mn, Na, P, Pd, Pt, Sn, Sr and W.

|                          |            |         |         |         |        |       |             |           |        |             |        |       |          |         |      |       |       |       |       | A    |      | 51:   | 20  | 1.0    |       |
|--------------------------|------------|---------|---------|---------|--------|-------|-------------|-----------|--------|-------------|--------|-------|----------|---------|------|-------|-------|-------|-------|------|------|-------|-----|--------|-------|
| REPORT 8: 890403 PA      |            | ٨       | SHVORTH | EIPL    |        | Pro   | j: H5       |           | Dat    | e in: 89    | /08/01 | Dat   | te Out:8 | 9/08/04 | Att: |       |       |       |       |      |      |       | Pag | e 1 of | f 1   |
| Sample Mumber            | Ag         | A1      | As      | 82      | Bı     | i.    | Cđ          | Co        | Cr     | Ĉu          | fe     | ĸ     | Ħọ       | fin     | Ro   | Na    | Nı    | F     | fb    | Sb   | Sn   | Sr    | U   | ¥      | In    |
|                          | poe        | 1       | ppe     | ppe     | 000    | 1     | <b>00</b> 0 | 000       | ppe    | <b>pp</b> • | 1      | 1     | 1        | 000     | 008  | 1     | 000   | 1     | 000   | 008  | 004  | 000   | 008 | 000    |       |
| R- 5                     | 6.5        | 0.20    | 1287    | 13      | - (3   | 1.17  | 36.5        | 1         | 108    | 112         | 2.59   | 0.25  | 0.54     | 1015    | 2    | 0.07  | :2    | D.04  | 3435  | (2   | (2   | 32    | 3   | < 3    | 3740  |
| R-10                     | 3.4        | 0.20    | 198     | 40      | (3     | 2.26  | 1.2         | 8         | 109    | 34          | 2.24   | 0.40  | 0.39     | 1405    | 2    | 0.01  | 9     | 0.01  | 182   | <2   | <2   | 31    | <5  | (3     | 160   |
| Minimum Detection        | 0.;        | 0.01    | 3       | 1       | 3      | 0.01  | 0.1         | 1         | 1      | 1           | 0.01   | 0.01  | 0.01     | 1       | 1    | 0.01  | 1     | 0.01  | 2     | 2    | 2    | 1     | 5   | 3      | 1     |
| <b>Nazisus</b> Detection | 50.0       | 10.00   | 2000    | 1000    | 1000   | 10.00 | 1000.0      | 20000     | 1000   | 20000       | 10.00  | 10.00 | 10.00    | 20000   | 1000 | 10.00 | 20000 | 10.00 | 20000 | 2000 | 1000 | 10000 | 100 | 1000   | 20000 |
| <= Less than Minzaum     | is = Insuf | ficient | Sample  | ns = No | sanole | ):5   | reater t    | han Kassi | ue Auf | A = Fire    | assay/ | AAS   |          |         |      |       |       |       |       |      |      |       |     |        |       |

#### ANOMALOUS RESULTS: FURTHER ANALYSES BY ALTERNATE METHODS SUGGESTED

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VANGEOCHEM LAB LIMITED

MAIN OFFICE 1988 TRIUMPH ST VANCOUVER, B C V5L 1K5 • (604) 251-5656 • FAX (604) 254-5717 BRANCH OFFICES PASADENA, NFLD BATHURST, N B. MISSISSAUGA, ONT. RENO, NEVADA, U.S A

# GEOCHEMICAL ANALYTICAL REPORT

CLIENT: ASHWORTH EXPLORATION LTD. ADDRESS: 718 - 744 W. Hastings St. : Vancouver, BC : V6C 1A5 DATE: OCT. 25 1989

REPORT#: 890765 GA JOB#: 890765

PROJECT#: 287 SAMPLES ARRIVED: OCT. 18 1989 REPORT COMPLETED: OCT. 25 1989 ANALYSED FOR: Au (FA/AAS) ICP

INVOICE#: 890765 NA TOTAL SAMPLES: 13 SAMPLE TYPE: 13 ROCK REJECTS: SAVED

SAMPLES FROM: MR. F. YACOUB COPY SENT TO: ASHWORTH EXPLORATION LTD.

PREPARED FOR: MR. F. YACOUB



ANALYSED BY: VGC Staff

Ram 1 h SIGNED:

**GENERAL REMARK: None** 

# VGC VANGEOCHEM LAB LIMITED

MAIN OFFICE 1988 TRIUMPH ST VANCOUVER, B.C. V5L 1K5 • (604) 251-5656 • FAX (604) 254-5717

### BRANCH OFFICES

PASADENA, NFLD BATHURST, N.B MISSISSAUGA, ONT RENO, NEVADA, U S A

| REPORT NUMBER: 0 | 90765 GA JOB N | UNBER: 890765 | ASHNORTH EXPLORATION LTD. | PAGE 1 OF 1 |
|------------------|----------------|---------------|---------------------------|-------------|
| SAMPLE B         | Au             |               |                           |             |
|                  | ppb            |               |                           |             |
| NV 89 R 7        | 90             |               |                           |             |
| NV 89 R 8        | 2900           |               |                           |             |
| NV 89 R 9        | 220            |               |                           |             |
| NV 89 R11        | 50             |               |                           |             |
| NV 89 R12        | 1430           |               |                           |             |
| NV 89 R13        | 360            |               |                           |             |
| NV 89 R14        | > 10000        |               |                           |             |
| NV 89 R15        | 230            |               |                           |             |
| NV 89 R16        | 570            |               |                           |             |
| NV 89 R17        | 60             |               |                           |             |
| MV 89 R18        | 40             |               |                           |             |
| MV 89 R19        | 180            |               |                           |             |
| MV 89 R20        | > 10000        |               |                           |             |

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1988 Triuoph Street, Vancouver, B.C. V5L 1K5 Phi(604)251-5656 Faxi(604)254-5717

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#### ICAP GEOCHEMICAL ANALYSIS

A .5 gram sample is digested with 5 ml of 3:1:2 HCl to HNO<sub>5</sub> to H<sub>2</sub>O at 95 °C for 90 minutes and is diluted to 10 ml with water. This leach is partial for Al, Ba, Ca, Cr, Fe, K, Mg, Mn, Na, P, Pd, Pt, Sn, Sr and W.

|                                     |                      |                   |                 |                   |                 |         |                   |                  |                  |                   |                   |                    |          |                   |                  |       |               |       |        |      | C    |       |      |                     |           |
|-------------------------------------|----------------------|-------------------|-----------------|-------------------|-----------------|---------|-------------------|------------------|------------------|-------------------|-------------------|--------------------|----------|-------------------|------------------|-------|---------------|-------|--------|------|------|-------|------|---------------------|-----------|
| ORT 4: 890765 PA                    |                      | ASI               | WORTH EX        | PL                |                 | Proj: 2 | 87                |                  | Date In          | : 89/10/          | 18 0              | ate Out:           | 89/10/26 | Atte              | F YACO           | JB    |               |       |        |      |      | Page  | 1 of | 1                   |           |
| ple Number                          | Ag                   | A1                | As              | Ba                | Bi              | Ca      | Cđ                | Co               | Cr               | Cu                | Fe                | ĸ                  | Ng       | Ħn                | Ho               | Na    | Wi            | P     | Pb     | Sb   | Sa   | Sr    | U    | ¥                   | In        |
|                                     | ppe                  | 1                 | ppe             | ppe               | ppe             | I       | ppe               | ppe              | ppe              | ppe               | 1                 | 1                  | Ì        | ppe               | ppe              | 1     | ppe           | I     | ppe    | ppe  | ppe  | ppe   | ppe  | <b>D</b> D <b>B</b> | <b>DD</b> |
| 89 R 7                              | 2.0                  | 2.34              | 55              | 22                | (3              | 0.17    | 0.7               | 38               | 28               | 4177              | 7.40              | 0.25               | 1.57     | 986               | 4                | 0.01  | 14            | 0.06  | 39     | (2   | <2   | 11    | <5   | (3                  | 32        |
| 89 R 8                              | 7.6                  | 0.16              | 1571            | 16                | (3              | 0.01    | 0.1               | 11               | 44               | 225               | 6.01              | 0.19               | 0.06     | 2170              | 2                | 0.01  | 16            | 0.01  | 70     | <2   | <2   | 3     | (5   | (3                  | 29        |
| 89 R 9                              | 2.9                  | 2.15              | 106             | 23                | <3              | 1.33    | 0.1               | 31               | 23               | 327               | 6.00              | 0.38               | 2.18     | 1395              | 1                | 0.01  | 39            | 0.06  | 51     | <2   | <2   | 29    | <5   | <3                  | 57        |
| 89 R11                              | 1.5                  | 1.66              | 23              | 18                | (3              | 2.64    | 0.1               | 29               | 26               | 913               | 5.28              | 0.55               | 2.96     | 1520              | 2                | 0.01  | 35            | 0.03  | 129    | (2   | (2   | 54    | <5   | (3                  | 115       |
| 89 R12                              | 2.5                  | 0.38              | 224             | 17                | (3              | 2.16    | 0.1               | 13               | 68               | 117               | 3.24              | 0.42               | 1.23     | 2387              | (1               | 0.01  | 16            | 0.01  | 171    | <2   | <2   | 38    | (5   | (3                  | 39        |
| 89 R13                              | 3.3                  | 3.78              | 74              | 14                | 3               | 0.97    | 1.1               | 61               | 8                | 5779              | 8.61              | 0.41               | 3.34     | 1456              | 7                | 0.01  | 22            | 0.07  | 358    | <2   | <2   | 19    | (5   | (3                  | 183       |
| 89 R14                              | >50.0                | 0.16              | >2000           | 7                 | 3               | 0.03    | 226.3             | 7                | 97               | 825               | >10.00            | 0.32               | 0.09     | 74                | 12               | 0.01  | 14            | 0.01  | >20000 | <2   | (2   | 1     | <5   | (3                  | >20000    |
| 89 R15                              | 1.2                  | 0.35              | 46              | 246               | (3              | 8.83    | 3.8               | 15               | 15               | 70                | 4.37              | 1.43               | 0.53     | 982               | (1               | 0.01  | . 12          | 0.05  | 778    | (2   | (2   | 74    | (5   | (3                  | 590       |
| 99 R16                              | 0.6                  | 0.47              | 4               | 22                | <3              | 0.28    | 0.1               | 4                | 64               | 97                | 1.51              | 0.08               | 0.37     | 312               | 1                | 0.01  | 6             | 0.03  | 103    | <2   | (2   | 4     | (5   | (3                  | 113       |
| 89 R17                              | 0.3                  | 1.49              | 41              | 38                | (3              | 3.69    | 0.1               | 25               | 39               | 696               | 4.79              | 0.70               | 2.64     | 2376              | 1                | 0.01  | 38            | 0.03  | 88     | <2   | <2   | 62    | (5   | (3                  | 213       |
| 89 R18                              | 0.2                  | 0.14              | 9               | 14                | (3              | 0.09    | 0.1               | 6                | 145              | 33                | 1.39              | 0.05               | 0.10     | 533               | (1               | 0.02  | 6             | 0.01  | 53     | (2   | <2   | 2     | (5   | (3                  | 43        |
| 99 R19                              | 4.6                  | 0.99              | 70              | 1                 | (3              | 0.04    | 0.7               | 24               | 29               | 956               | 9.25              | 0.28               | 0.96     | 568               | 9                | 0.01  | 11            | 0.02  | 66     | <2   | (2   | 1     | (5   | (3                  | 395       |
| 89 R20                              | 30.7                 | 0.13              | 1997            | 7                 | (3              | 0.17    | 62.3              | 9                | 54               | 284               | 4.21              | 0.15               | 0.10     | 237               | 4                | 0.01  | 11            | 0.01  | 6828   | (2   | (2   | 5     | (5   | (3                  | 5860      |
| ious Detection                      | 0.1                  | 0.01              | 3               | 1                 | 3               | 0.01    | 0.1               | 1                | 1                | 1                 | 0.01              | 0.01               | 0.01     | ı                 | 1                | 0.01  | 1             | 0.01  | 2      | 2    | 2    | ı     | 5    | 3                   | 1         |
| ious Detection<br>Less than Minious | 50.0<br>is = Insuffi | 10.00<br>icient S | 2000<br>ample n | 1000<br>s = No sa | 1000<br>mople > | 10.00   | 1000.0<br>er than | 20000<br>Maximum | 1000<br>ANOMALOU | 20000<br>IS RESUL | 10.00<br>TS = Fur | 10.00<br>ther Anal | 10.00    | 20000<br>Alternat | 1000<br>e Nethod | 10.00 | 20000<br>sted | 10.00 | 20000  | 2000 | 1000 | 10000 | 100  | 1000                | 20000     |

ANALYST:

# GC VANGEOCHEM LAB LIMITED

MAIN OFFICE 1988 TRIUMPH ST VANCOUVER, B.C. V5L 1K5 • (604) 251-5656 • FAX (604) 254-5717 BRANCH OFFICES PASADENA, NFLD BATHURST, N B MISSISSAUGA, ONT RENO, NEVADA, U S A

# ASSAY ANALYTICAL REPORT

### CLIENT: ASHWORTH EXPLORATION LTD.

ADDRESS: 718 - 744 W. Hastings St. : Vancouver, BC : V6C 1A5 DATE: OCT. 25 1989

REPORT#: 890765 AA JOB#: 890765

PROJECT#: 287 SAMPLES ARRIVED: OCT. 18 1989 REPORT COMPLETED: OCT. 25 1989 ANALYSED FOR: Au INVDICE#: 890765 NA TOTAL SAMPLES: 2 REJECTS/PULPS: 90 DAYS/1 YR SAMPLE TYPE: 2 ROCK

SAMPLES FROM: MR. F. YACOUB COPY SENT TO: ASHWORTH EXPLORATION LTD.

PREPARED FOR: MR. F. YACOUB



ANALYSED BY:

Raymond Chan

SIGNED:

and h

Registered Provincial Assayer

GENERAL REMARK: None

# ► VANGEOCHEM LAB LIMITED

MAIN OFFICE 1988 TRIUMPH ST VANCOUVER, B.C. V5L 1K5 • (604) 251 5656 • FAX (604) 254 5717

#### BRANCH OFFICES PASADENA, NFLD BATHURST, N.B MISSISSAUGA, ONT

RENO, NEVADA, U S A

 REPORT NUMBER: 890765 AA
 JOB NUMBER: 890765
 ASHMORTH EXPLORATION LTD.
 PAGE 1 OF 1

 SAMPLE #
 Au
 OZ/St
 OZ/St

 MV 89 R14
 1.420
 1.420

MV 89 R20 .882

DETECTION LIMIT 1 Troy oz/short ton = 34.28 ppm

2000

-12

.005 1 ppm = 0.00011

ppm = parts per million

< = less than</pre>

1 hr signed:

GC VANGEOCHEM LAB LIMITED

MAIN OFFICE 1630 PANDORA STREET VANCOUVER, B.C. V5L 1L6 TEL (604) 251-5656 FAX (604) 254-5717 BRANCH OFFICES BATHURST, N.B. RENO, NEVADA, U.S.A.

# GEOCHEMICAL ANALYTICAL REPORT

CLIENT: HI-TEC RESOURCE MANAGEMENT LTD. DATE: JUNE 28 1991 ADDRESS: 1500 - 409 Granville St. : Vancouver, BC : V7Y 1G5 REPORT#: 910079 GA JOB#: 910079

PROJECT#: MIDDLE VIEN SAMPLES ARRIVED: JUNE 27 1991 REPORT COMPLETED: JUNE 28 1991 ANALYSED FOR: AU (FA/AAS) ICP

INVOICE#: 910079 NA TOTAL SAMPLES: 38 SAMPLE TYPE: 38 ROCK REJECTS: SAVED

SAMPLES FROM: CANADIAN IMPERIAL MINE INC. COPY SENT TO: HI-TEC RESOURCE MANAGEMENT LTD.

PREPARED FOR: CANADIAN IMPERIAL MINE LTD.

ANALYSED BY: Raymond Chan SIGNED:

**GENERAL REMARK: None** 

# 1630 Pandora Street, Vancouver, B.C. V5L 1L6 Ph: (604)251-5656 Fax: (604)254-5717

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#### ICAP GEOCHEMICAL ANALYSIS

A .S gram sample is digested with 5 ml of 3:1:2 HCL to HNO<sub>2</sub> to H<sub>2</sub>O at 95 °C for 90 minutes and is diluted to 10 ml with water. This leach is partial for Al, Ba, Ca, Cr, Fe, K, Mg, Mn, Ma, P, Sn, Sr and W.

ANALYST

| MPH FM         52         2.9         G         G         G         Lo         Lo <thlo< th="">         Lo         Lo</thlo<>   | REPORT #: 910079 PA   | н    | I-TEC RE | SOURCE NE | WT LTD. |      |    | PROJI | ECT: MIDI | NE VIEN |      |       | DATE | E IN: JUK | E 27 199 | L DAT | E OUT: . | IUNE 28 | 1991 / | TTENTIO | I: CANADI | AN IMPER   | TAL NINE | INC.  |     | PAGE 1    | OF 1      |
|--|-----------------------|------|----------|-----------|---------|------|----|-------|-----------|---------|------|-------|------|-----------|----------|-------|----------|---------|--------|---------|-----------|------------|----------|-------|-----|-----------|-----------|
| MPH FM         52         2.9         G         G         G         Lo         Lo <thlo< th="">         Lo         Lo</thlo<>   | Sample Name           | •    |          |           | -       |      |    |       |           |         |      |       |      | ĸ         | •        |       |          |         |        | •       |           |            | -        |       | -   | V         | [n<br>pp• |
| mmin 199         dia         1/4         dia         1/4         dia         1/4         1/  |                       |      | -        |           | ••      |      | •• | -     |           |         |      |       | -    | 10 01     | -        |       |          | -       | .,     | -       | ••        |            | • •      |       | • · | • •       | 57        |
| mmin         min         m   |                       |      |          |           |         |      | -  |       |           |         |      |       |      |           |          |       |          |         |        |         |           |            |          |       |     |           | 76        |
| mmin 1972         GL         SI         SI        <   |                       |      |          |           |         |      |    |       |           |         |      |       |      |           |          |       |          |         |        |         |           |            |          |       |     |           | 151       |
| Medi File         GL 1         LI 1         G 1         S 10         G 1         G 1         G 1         S 10         G 1         G 1         S 10         G 1         S 10         G 1         S 10         G 1         S 10         G 1         G 1         S 10         G 1         S 10         G 1         G 1         G 1         G 1         G 1         G 1         G 1         G 1         G 1 <thg 1<="" th=""> <thg 1<="" td="" th<=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>120</td></thg></thg>   |                       |      |          |           |         |      |    |       |           |         |      |       |      |           |          |       |          |         |        |         |           |            |          |       |     |           | 120       |
| Marting         GL, 1         Link  |                       |      |          |           |         | -    |    |       |           |         | -    | -     |      |           |          |       |          |         | -      |         |           |            |          |       |     |           |           |
| Main Train         Col:         2.2         Ci:         Ci:         2.3         2.4         Ci:         2.3         311         Ci:         Ci: <thci:< th="">         Ci:         <thci:< th=""> <thci< td=""><td>WV91 FR8</td><td>(0.1</td><td>2.11</td><td>(3</td><td>510</td><td>Ω</td><td>(3</td><td>0.13</td><td>(0.1</td><td>17</td><td>61</td><td>58</td><td>4.58</td><td>(0.01</td><td>2.17</td><td>653</td><td>0</td><td>(0.01</td><td>Q</td><td>0.04</td><td>Q</td><td>Q</td><td>Q</td><td>1</td><td>()</td><td>(3</td><td>119</td></thci<></thci:<></thci:<>   | WV91 FR8              | (0.1 | 2.11     | (3        | 510     | Ω    | (3 | 0.13  | (0.1      | 17      | 61   | 58    | 4.58 | (0.01     | 2.17     | 653   | 0        | (0.01   | Q      | 0.04    | Q         | Q          | Q        | 1     | ()  | (3        | 119       |
| mmp1 mm1         CO.1         L.23         C3         C3         C3         C3         C3         C3         C3         C3         C4         C3         C4         C3         C4         C3         C4         C4 <thc4< th="">         C4         <thc4< th=""></thc4<></thc4<>   |                       |      |          |           |         |      |    |       |           |         |      |       |      | (0.01     | 3.76     |       |          |         |        |         |           |            |          |       |     |           | 105       |
| mmin riging         col.   | NV91 FR10             |      |          |           |         | 9    |    |       | (0.1      | 25      |      | 129   | 3.68 | (0.01     | 2.93     |       |          |         |        |         |           |            |          | •     | -   |           | 65        |
| mmm         reti         c.a         c.a <thc></thc>   | NV91 FR11             | (0.1 | 1.73     |           | (5      | 4    | (3 | 0.28  | (0.1      | 29      | 76   | 40    | 2.97 | (0.01     | 2.35     | 975   | (1       | <0.01   | 21     | 0.02    |           | (2         |          |       |     |           | 30        |
| Number         Numbr         Numbr         Numbr <td>NV91 FR12</td> <td>&lt;0.1</td> <td>0.47</td> <td>(3</td> <td>(5</td> <td>8</td> <td>(3</td> <td>0.08</td> <td>(0.1</td> <td>13</td> <td>109</td> <td>28</td> <td>1.49</td> <td>(0.01</td> <td>0.42</td> <td>468</td> <td>(1</td> <td>0.02</td> <td>&lt;1</td> <td>0.01</td> <td>&lt;2</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>19</td>  | NV91 FR12             | <0.1 | 0.47     | (3        | (5      | 8    | (3 | 0.08  | (0.1      | 13      | 109  | 28    | 1.49 | (0.01     | 0.42     | 468   | (1       | 0.02    | <1     | 0.01    | <2        |            |          |       |     |           | 19        |
| Interprets         (a)   | NV91 FR13             | <0.1 | 0,83     | (3        | (5      | 59   | (3 | 0.20  | (0.1      | 13      | 32   | 47    | 1.68 | (0.01     | 0.19     | 407   | 4        | 0.08    | 8      | 0.05    | 9         | (2         | <2       | 6     | <5  | (3        | 39        |
| mmm1         mmm1 <th< td=""><td>NV91 FR14</td><td>0.2</td><td>1.92</td><td>(3</td><td>520</td><td>15</td><td>(3</td><td>0.12</td><td>(0.1</td><td>18</td><td>64</td><td>67</td><td>3.67</td><td>&lt;0.01</td><td>1.89</td><td>719</td><td>(1</td><td>(0.01</td><td>10</td><td>0.04</td><td>(2</td><td>&lt;2</td><td>(2</td><td>1</td><td>(5</td><td>(3</td><td>100</td></th<>   | NV91 FR14             | 0.2  | 1.92     | (3        | 520     | 15   | (3 | 0.12  | (0.1      | 18      | 64   | 67    | 3.67 | <0.01     | 1.89     | 719   | (1       | (0.01   | 10     | 0.04    | (2        | <2         | (2       | 1     | (5  | (3        | 100       |
| MP1 FI216       (G1, 12,71)       (G3, G5, 5)       (G3, 0,42, 6)       (G1, 15, 6, 7)       (G1, 114, G3, G5, 7)       (G3, 0,42, 6)       (G1, 15, 6, 7)       (G1, 11, 7)       (G3, 11, 7)       (G1, 11, 7)   | HV91 FRIS             | (0.1 | 1.80     | (3        | 540     | 3    | (3 | 0.08  | (0.1      | 18      | 50   | 73    | 3.43 | (0.01     | 1.90     | 860   | (1       | (0.01   | (1     | 0.03    | <2        | <2         | <2       | (1    | (5  | (3        | 86        |
| MMMI FIRIT         (6.1         1.14         (3         (3         7         (3         0.42         (0.1         14         (0.1         1.73         (3         (3         (1         (2         (1)         (0.1         1.73         (3         (3         (1         (1) </td <td></td> <td></td> <td></td> <td></td> <td></td> <td>5</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>(0.01</td> <td></td> <td></td> <td>(1</td> <td>(0.01</td> <td>30</td> <td>0.03</td> <td>2</td> <td>&lt;2</td> <td>(2</td> <td>1</td> <td>(5</td> <td>(3</td> <td>56</td>   |                       |      |          |           |         | 5    |    |       |           |         |      |       |      | (0.01     |          |       | (1       | (0.01   | 30     | 0.03    | 2         | <2         | (2       | 1     | (5  | (3        | 56        |
| MM31 FR18         G0.1         1.73         G3         G3         16         G3         0.1         470         722         422         4.39         G0.1         1.59         331         G1         0.03         G1         0.66         G2         <  |                       |      |          |           |         | •    |    |       |           |         |      |       |      |           |          |       |          |         |        |         |           |            |          | 16    |     |           | 28        |
| MY91 FR20       (0.1       1.7       (3       40       9       (3       0.21       0.3       13       75       37       3.78       (0.01)       1.21       25       (1       (0.01)       15       0.03       17       (2       (2       2       (1       (5       (1       0.03)       17       (2       (2       (2       (1       (5       (3       (1       (3       0.10       (1       (3       0.10       (1       (3       0.10       (1       (3       0.11       (1       (1       0.01       (1   |                       |      |          |           |         | -    |    |       |           |         |      |       |      |           |          |       |          |         |        |         |           |            |          |       |     |           | 29        |
| MY91 FR20       (0.1       1.7       (3       40       9       (3       0.21       0.3       13       75       37       3.78       (0.01)       1.21       25       (1       (0.01)       15       0.03       17       (2       (2       2       (1       (5       (1       0.03)       17       (2       (2       (2       (1       (5       (3       (1       (3       0.10       (1       (3       0.10       (1       (3       0.10       (1       (3       0.11       (1       (1       0.01       (1   |                       | /6 1 | 2 45     | 19        | ~~      | •/   | 12 |       | /         |         |      |       | < A0 | /         | • •      |       |          | /4 41   | 20     |         | /1        | <b>/</b> 3 | 13       | •     | /5  | <b>/3</b> | 42        |
| MMM1 FR21       0.7 <th0.1< th="">       233       0.7</th0.1<>  |                       |      |          |           |         |      |    |       |           |         |      |       |      |           |          |       |          |         |        |         |           |            |          |       |     |           | 42        |
| MM91 FR22       1.4       2.35       G3       59       G1       G3       6.1       2.0       1.5       2.0       4.53       G1       G0.01       C1       G3.01       C1       G3       G1       G3   |                       |      |          |           |         | -    |    |       |           |         |      |       |      |           |          |       |          |         |        |         |           |            | -        | •     |     |           | 305       |
| NY91 FR23       (0.1       3.37       (3       (5       (1       (3       0.1       25       15       292       6,33       (0,01       3.71       826       (1       (0,01)       (1       0.08       (2  |                       |      |          |           |         |      |    |       |           |         |      |       |      |           |          |       |          |         |        |         |           |            |          |       |     |           | 97        |
| NY91 F824       0.2       2.74       (3)       (5)       61       (3)       0.36       (6)       1       25       24       56       (4)       0.10       1.10       (1)       0.10       1.10       (1)       0.10       1.10       (1)       0.10       1.10       (1)       0.10       1.10       (1)       0.10       1.10       (1)       0.10       1.10       (1)       0.10       1.10       0.11       0.10       1.10       0.11       0.10       1.10       0.11       0.10       1.10       0.11       0.10       1.10       0.11       0.10       1.10       0.11       0.10   |                       |      |          |           |         |      |    |       |           |         |      |       | 9.10 | <0.01     | 2.04     | 453   | (1       | <0.01   | (1     | 0.04    |           |            |          |       |     |           | 69        |
| NYS1 PR1       0.2       1.10       (3       60       15       (3)       0.12       (0.1)       8       135       11       2.28       (0.01)       1,16       471       (1)       (0.01)       8       0.02       20       (2)       (2)       (2)       (3)       (3)       (1)       (1)       (1)       (0.01)       4       (0.01)       22       (2)       (3)       (3)       (1)       (2)       235       108       3.94       (0.01)       2.21       641       (1)       (0.01)       4       0.07       (2)       (   | NV91 FR23             | (0.1 | 3.37     | (3        | (5      | (1   | (3 | 0.17  | (0.1      | 25      | 15   | 292   | 6.93 | <0.01     | 3.71     | 826   | a        | (0.01   | (1     | 0.08    | (2        | <2         | (2       | 4     | (5  | (3        | 216       |
| NY1 PP2       0.2       2.06       (3)       (5)       12       (3)       0.21       (0.1)       22       35       108       3.94       (0.01)       2.21       641       (1)       (0.01)       4       0.07       (2)       (2)       (2)       (3)  | NV91 FR24             | 0.2  | 2.74     | (3        | (5      | 61   | <3 | 0.36  | (0.1      | 25      | 24   | 56    | 4.99 | (0.01     | 2.81     | 1170  | (1       | <0.01   | 104    | 0.07    | 4         | <2         | (2       | 5     | (5  | (3        | 189       |
| HY91 PR3       (0.1       2.39       (3       (3       (4       (3       0.70       (0.1       25       101       244       2.44       (0.01       2.38       652       (1       0.03       657       0.02       (2       (2       (2       13       (5       (3         HY91 PR4       (0.1       1.199       (3       (5       (1       (3       0.77       (0.1       31       63       106       2.12       (0.01       1.89       447       (1       0.01       27       0.02       15       (2       (2       13       (5       (3         HY91 PR5       (0.1       1.70       (3       (5       (1       (3       0.16       0.1       37       19       188       2.49       (0.01       1.64       616       (1       0.02       4       0.03       (2       (2       (2       63       (3 <td>NV91 PRI</td> <td>0.2</td> <td>1.10</td> <td>(3</td> <td>60</td> <td>19</td> <td>(3</td> <td>0.12</td> <td>(0.1</td> <td>8</td> <td>135</td> <td>11</td> <td>2.28</td> <td>(0.01</td> <td>1.16</td> <td>471</td> <td>(1</td> <td>(0.01</td> <td>8</td> <td>0.02</td> <td>20</td> <td>(2</td> <td>(2</td> <td>2</td> <td>(5</td> <td>(3</td> <td>44</td>  | NV91 PRI              | 0.2  | 1.10     | (3        | 60      | 19   | (3 | 0.12  | (0.1      | 8       | 135  | 11    | 2.28 | (0.01     | 1.16     | 471   | (1       | (0.01   | 8      | 0.02    | 20        | (2         | (2       | 2     | (5  | (3        | 44        |
| NY91 PP3       (0.1       2.39       (3       (5       4       (3       0.70       (0.1       25       101       244       2.44       (0.01       2.38       452       (1       0.03       67       0.02       (3       (3       (3       (3       (3       (3       (3       (3       (3       (3       (1       (3       (1       (3       (1       (3       (1       (3       (1       (3       (1       (3       (1       (3       (1       (3       (1       (3       (1       (3       (1       (3       (1       (3       (1       (3       (1  | NV91 PR2              | 0.2  | 2.06     | (3        | (5      | 12   | (3 | 0.21  | (0.1      | 22      | 35   | 108   | 3.94 | (0.01     | 2.21     | 641   | (1       | <0.01   |        | 0.07    | (2        | <2         | (2       | 6     | (5  | (3        | 74        |
| MY91 PR4       (0.1       1.89       (3)       (5)       (1)       (3)       (5)       (1)       (3)       (5)       (1)       (3)       (5)       (1)       (3)       (5)       (1)       (3)       (5)       (1)       (3)       (5)       (1)       (3)       (5)       (1)       (3)       (5)       (1)       (3)       (5)       (1)       (3)       (5)       (1)       (3)       (5)       (1)       (3)       (5)       (1)       (3)       (5)       (1)       (3)       (5)       (1)       (3)       (5)       (1)       (3)       (5)       (1)       (3)       (5)       (1)       (3)       (1)       (2)       (2)       (2)       (2)       (2)       (2)       (2)       (2)       (2)       (2)       (2)       (2)       (2)       (2)       (2)       (2)       (2)       (3)       (3)       (3)       (3)       (1)   | NV91 PR3              | (0.1 | 2.39     | (3        | (5      | 4    | (3 | 0.70  | (0.1      |         | 101  | 244   | 2.44 | (0.01     |          |       |          |         | 67     |         |           |            |          | 15    |     |           | 44        |
| NY91 PR5       0.1       3.20       (3       (5       (1       (3       1.12       (0.1       49       31       212       5.32       (0.01       1.91       667       (1       0.18       11       0.02       (1       (5       (3       1       11       11       (1  | NV91 PR4              | <0.1 | 1.89     | (3        | <5      | a    | <3 | 0.77  | <0.1      | 31      | 63   | 106   | 2.12 | (0.01     | 1.89     | 447   | (1       | 0.01    | 27     | 0.02    | 15        | <2         | <2       | 32    | (5  | (3        | 35        |
| NY91 PR5       0.1       3.20       (3       (5       (1       (3       1.12       (0.1       49       31       212       5.32       (0.01       1.91       667       (1       0.18       11       0.02       (1       (5       (3       1       11       11       (1  | NV91 PR5              | (0.1 | 1.70     | (3        | (5      | a    | (3 | 0.60  | (0.1      | 37      | 19   | 188   | 2.49 | (0.01     | 1.64     | 616   | (1       | 0 02    |        | 0.03    | ()        | 0          | 0        | 27    | (5  | (3        | 46        |
| W91 P87       (0.1 3.34       (3 730       56       (3 0.40       (0.1 31       34       132       4.74       (0.01       4.00       6       0.03       17       (2       (2       10       (5       (3       1         W91 P88       0.1       2.97       (3       (5       143       (3       0.15       (0.1       26       32       282       4.28       (0.01       4.16       990       (1       (0.01       6       0.05       91       (2       (2       (4       (5       (3)       11         W91 P89       (0.1       4.14       (3       (5       3       (3       0.12       (0.1       30       28       141       5.35       (0.01       4.16       990       (1       (0.01       6       0.07       (2       (2       (1       (5       (3)       11       11       11       5.5       (0.01       4.16       990       (1       (0.01       6       0.07       (2       (2       (2       (1       (5       (3)       11       11       11       5.5       10       15       110       5.16       (0.01       4.10       11       5.6       (3)       110       5.16   | NV91 PR6              |      |          |           |         |      |    |       |           |         |      |       |      |           |          |       |          |         |        |         |           |            |          |       |     |           | 70        |
| WY91 PR9       0.1       2.97       (3       (5       143       (3       0.15       (0.1       26       32       222       4.28       (0.01       4.16       990       (1       (0.01)       6       0.05       91       (2       (2       4       (5       (3)       (1       (3)       (2       (2       (2       (1       (5       (3)       (1       (3)       (1       (1       (2)       (2       (2       (1       (5)       (3)       (3)       (3)       (3)       (3)       (1       (2)   | NU91 PP7              |      |          |           |         |      | -  |       |           |         |      |       |      |           |          |       |          |         |        |         |           |            |          |       |     |           | 114       |
| WY91 PR9       (0.1       4.14       (3       (5       48       (3       0.12       (0.1       30       28       141       5.35       (0.01       5.92       1298       (1       (0.01)       17       0.05       (2       (2       (2       (1       (5       (3       1         W91 PR10       (0.1       3.64       (3       (5       3       (3       0.12       (0.1       25       26       88       5.43       (0.01       4.72       1413       (1       (0.01       6       0.07       (2       (2       (2       (1       (5       (3       1       1       1       1       1       0.01       6       0.07       (2       (2       (2       (1       (5       (3       1       1       1       1       1       0.01       6       0.07       (2       (2       (2       (1       (5       (3       1  |                       |      |          |           |         |      |    |       |           |         |      |       |      |           |          |       |          |         | ç      |         |           |            |          |       |     |           | 165       |
| HV91 PR11       (0.1       3.72       (3       (5       7       (3       0.30       (0.1       22       15       101       5.16       (0.01       4.50       1109       (1       (0.01       (1       0.07       (2       (2       (2       4       (5       (3       1         HV91 PR12       (0.1       3.75       (3       (5       6       (3       0.44       (0.1       35       24       110       5.84       (0.01       4.61       1355       (1       (0.01       (2       (2       (2       (2       (2       (2       19       (5       (3  | NV91 PR9              |      |          |           |         |      |    |       |           |         |      |       |      |           |          |       |          |         | -      |         |           |            |          |       |     |           | 171       |
| HV91 PR11       (0.1       3.72       (3       (5       7       (3       0.30       (0.1       22       15       101       5.16       (0.01       4.50       1109       (1       (0.01       (1       0.07       (2       (2       (2       4       (5       (3       1         HV91 PR12       (0.1       3.75       (3       (5       6       (3       0.44       (0.1       35       24       110       5.84       (0.01       4.61       1355       (1       (0.01       (2       (2       (2       (2       (2       (2       19       (5       (3  |                       |      | • • •    |           |         | _    |    |       |           |         |      |       |      |           |          |       |          |         |        |         |           |            |          |       |     |           |           |
| WY91 PR12       (0.1       3.75       (3       (5       6       (3       0.44       (0.1       35       24       110       5.84       (0.01       4.46       1052       (1       (0.01       15       0.10       (2       (2       6       (3       (4       (0.1       35       24       110       5.84       (0.01       4.46       1052       (1       (0.01       15       0.10       (2       (2       (2       19       (5       (3       (3       (5       7       (3       0.90       (0.1       35       39       122       6.05       (0.01       4.61       1355       (1       (0.01       15       0.11       (2       (2       (2       19       (5       (3       (3       (3       (5       (3       (5       (1       10       1355       (1       (0.01       15       0.11       (2       (2       (2       (2       (3       (  |                       |      |          |           |         |      |    |       |           |         |      |       |      |           |          |       |          |         |        | 0.07    |           |            |          | (1    |     |           | 249       |
| WY91 PR13       (0.1       3.87       (3       (5       7       (3       0.90       (0.1       35       39       122       6.05       (0.01       135       (1       (0.01       25       0.11       (2       (2       (2       19       (5       (3       195       (3       1.95       (0.1       35       39       122       6.05       (0.01       1355       (1       (0.01       174       0.15       (2       (2       (2       63       (5       (3       (5       (3       (5       (3       (5       (0.1       35       39       122       6.05       (0.01       5.50       1337       (1       (0.01       174       0.15       (2       (2       (2       63       (5       (3       (5       (3       (5       (1       201       93       5.06       (0.01       4.61       1355       (1       (0.01       174       0.15       (2       (2       (2       (3   |                       |      |          |           |         |      |    |       |           |         | 15   | 101   | 5.16 | (0.01     | 4.50     | 1109  | (1       | (0.01   | (1     | 0.07    | <2        | (2         | <2       | 4     | (5  | (3        | 213       |
| NV91 PR14       (0.1       3.69       (3       (5       156       (3       1.95       (0.1       41       201       93       5.06       (0.01       100  |                       | <0.1 |          |           |         | 6    | (3 | 0.44  | (0.1      | 35      | 24   | 110   | 5.84 | <0.01     | 4.48     | 1052  | (1       | (0.0)   | 15     | 0.10    | (2        | (2         | (2       | 8     | (5  | (3        | 298       |
| NV91 PR14       (0.1       3.69       (3       (5       156       (3       1.95       (0.1       41       201       93       5.06       (0.01       5.50       1337       (1       (0.01       174       0.15       (2       (2       (2       63       (3       (3       (5       (3       1.95       (0.1       31.95       (0.1       31.95       (0.1       41       201       93       5.06       (0.01       5.50       1337       (1       (0.01       174       0.15       (2       (2       (2       (3       (3       (3       (3       (3       (3       (3       (3       (5       91       10       6.02       (0.01       4.84       1462       (1       (0.01       12       0.07       (2       (2       (2       (3       (3       (5       (3       (5       (3       (5       (3       (5       (1       (3       0.55       (1       3.56       (3.01       1376       (1       (0.01       12       0.07       (2       (2       (2       (3       (3       (5       (3       (5       (3       (5       (3       (5       (3       (5       (3       (5       (3 <th< td=""><td>NV91 PR13</td><td>(0.1</td><td></td><td></td><td></td><td>•</td><td>(3</td><td>0.90</td><td>(0.1</td><td>35</td><td>39</td><td>122</td><td>6.05</td><td>(0.01</td><td>4.61</td><td>1355</td><td>(1</td><td>(0.01</td><td>25</td><td>0.11</td><td>&lt;2</td><td>&lt;2</td><td>&lt;2</td><td>19</td><td>(5</td><td>(3</td><td>361</td></th<>   | NV91 PR13             | (0.1 |          |           |         | •    | (3 | 0.90  | (0.1      | 35      | 39   | 122   | 6.05 | (0.01     | 4.61     | 1355  | (1       | (0.01   | 25     | 0.11    | <2        | <2         | <2       | 19    | (5  | (3        | 361       |
| MV91 PR16       (0.1 3.66       (3       (5       18       (3       0.54       (0.1       35       50       144       5.56       (0.01       1376       (1       (0.01       38       0.06       (2       (2       (2       13       (5       (3         MV91 PR17       (0.1       1.98       (3       (5       12       (3       0.18       (0.1       13       15       53       3.98       (0.01       1.99       673       (1       (0.01       27       0.05       16       (2       (2       3       (3  | NV91 PR14             | (0.1 | 3.69     | (3        | (5      | 156  | (3 | 1.95  | (0.1      | 41      | 201  | 93    | 5.06 | (0.01     |          |       |          |         |        |         |           |            |          |       |     |           | 147       |
| MV91 PR16       (0.1 3.66 (3) (5) 18 (3) 0.54 (0.1 35) 50 144 5.56 (0.01 5.01 1376 (1) (0.01 38) 0.06 (2) (2) (2) 13 (5) (3) 149 (0.1 1.99) 673 (1) (0.01 38) 0.06 (2) (2) (2) (2) (2) (2) (3) (3) (3) (3) (3) (3) (3) (3) (3) (3  | NV91 PRIS             | (0.1 | 3.76     | (3        | (5      | 41   | (3 | 0.82  | (0.1      | 35      | 69   | 110   | 6.02 | (0.01     | 4.84     | 1462  | (1       | (0.01   | 42     | 0.07    | (2        | (7         | 0        | 20    | (5  | (3        | 326       |
| MV91 PR17       <0.1   | NV91 PR16             | (0.1 | 3.66     |           |         |      |    |       |           |         |      |       |      |           |          |       |          |         | -      |         |           |            |          |       |     |           | 169       |
| Maximum Detection 50.0 10.00 2000 10000 1000 1000 10.00 1000.0 20000 1000 20000 10.00 10.00 10.00 10.00 200  | NV91 PR17             |      |          |           |         |      |    |       |           |         |      |       |      |           |          |       |          |         |        |         |           |            |          |       |     |           | 67        |
| Maximum Detection 50.0 10.00 2000 10000 1000 1000 10.00 1000.0 20000 1000 20000 10.00 10.00 10.00 10.00 200  | Kinigun Detertion     | 0.1  | 0.01     | 1         | ٢       | 1    | 2  | 0 01  | 0.1       |         | 1    |       | 0.01 | 0.01      |          |       |          |         |        | • • •   | •         | •          | •        |       |     | -         |           |
| A face the finite of the finit |                       |      |          | -         | -       | 1000 |    |       |           | 20000   | 1000 | 20000 |      |           |          | 1     | 1        |         | 1      |         | -         | -          | -        | 1     | •   | •         | 1         |
| C = Less Than Minister > - Greater Than Maximum is - Insulficient Sample ns - No Sample +Au Analysis Done By Fire Assay Concentration / AAS Finish.  | ( - Less Than Minieue |      |          |           |         |      |    |       |           |         |      |       |      |           |          |       |          |         |        | 10.00   | 20000     | 2000       | 1000     | 10000 | 100 | 1000      | 20000     |

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# BRANCH OFFICES BATHURST, N.B RENO, NEVADA, U.S.A

| REPORT NUMBER: 916079 GL | JOB NUMBER: 910079 | BI-TEC RESOURCE HABAGEMENT LTD. | PAGE 1 OF 1 |
|--------------------------|--------------------|---------------------------------|-------------|
| SAMPLE #                 | Au                 |                                 |             |
|                          | ppb                |                                 |             |
| MV91 FR4                 | 20                 |                                 |             |
| MV91 FR5                 | 20                 |                                 |             |
| MV91 FR6                 | nd                 |                                 |             |
| MV91 FR7                 | nd                 |                                 |             |
| MV91 FR8                 | 510                |                                 |             |
| MV91 FR9                 | 10                 |                                 |             |
| MV91 FR10                | nd                 |                                 |             |
| MV91 FR11                | nð                 |                                 |             |
| MV91 FR12                | nd                 |                                 |             |
| MV91 FR13                | nd                 |                                 |             |
| MV91 FR14                | 520                |                                 |             |
| MV91.FR15                | 540                |                                 |             |
| MV91 FR16                | nd                 |                                 |             |
| MV91 FR17                | nd                 |                                 |             |
| MV91 FR18                | nđ                 |                                 |             |
| MV91 FR19                | 60                 |                                 |             |
| MV91 FR20                | 40                 |                                 |             |
| MV91 FR21                | 130                |                                 |             |
| MV91 FR22                | 90                 |                                 |             |
| MV91 FR23                | nd                 |                                 |             |
| MV91 FR24                | nd                 |                                 |             |
| MV91 PR1                 | 60                 |                                 |             |
| MV91 PR2                 | nđ                 |                                 |             |
| MV91 PR3                 | nd                 |                                 |             |
| MV91 PR4                 | nd                 |                                 |             |
| MV91 PR5                 | nd                 |                                 |             |
| MV91 PR6                 | nd                 |                                 |             |
| MV91 PR7                 | 730                |                                 |             |
| MV91 PR8                 | nd                 |                                 |             |
| MV91 PR9                 | nd                 |                                 |             |
| MV91 PR10                | nd                 |                                 |             |
| MV91 PR11                | nđ                 |                                 |             |
| MV91 PR12                | nđ                 |                                 |             |
| MV91 PR13                | nd                 |                                 |             |
| MV91 PR14                | nd                 |                                 |             |
| MV91 PR15                | nd                 |                                 |             |
| MV91 PR16                | nd                 |                                 |             |
| MV91 PR17                | nd                 |                                 |             |
|                          | -                  |                                 |             |
| DETECTION LIMIT          | ς .                |                                 |             |

DETECTION LIMIT nd = none detected

### APPENDIX C

# INTERPRETATION OF THE GEOPHYSICAL SURVEY

## ON THE APEX GROUP

FIGURE G-1, G-2, G-3

#### 1. INTRODUCTION

A geophysical program consisting of electromagnetic (VLF-EM) and magnetic surveys was carried out on a single grid located in the Victoria Mining District near Port Alberni, B.C. The survey was carried out in July 1989.

#### 2. OBJECTIVES

- to establish a correlation between magnetic minerals and mineralized trends,
- to test the effectiveness of VLF-EM in following possible mineralized trends and to establish new unrecognized conductive trends,
- to establish geophysical areas of interest for future exploration.
- 3. SURVEY SPECIFICATIONS

Survey Parameters

- survey line separation 50 m
- survey station spacing 12.5 m
- VLF-EM survey total 3.0 km
- magnetic survey total 3.0 km

#### Equipment Parameters

- VLF-EM and Magnetic Surveys

- Scintrex Omni Plus combined VLF-EM and magnetometer
- Dip Angle (in-phase) and Quadratur (out-of-phase)
- measured in percent at each static
- VLF-EM Field Strength measured at each station
- transmitting stations used NLK (24.8 kHz) Seattle, Wash.
   NAA (21.4 kHz) Cutler, Ma.
- earth's total magnetic field measured in gammas (nT)
- magnetic variations controlled by automatic magnetic base station recording every 30 seconds
- instrument accuracy +/- 0.1 gamma
- station repeatability better than +/- 3 gammas in low gradients.

Equipment Specifications - see Appendix I

4. DATA

Calculations

Total Field Magnetic Survey

Total field magnetic readings were individually corrected for variations in the earth's magnetic field using magnetic base station values. The formula used for magnetic corrections was; CTFR = TFR + (DBL - BSR)

> where: CTFR = Corrected Total Field Reading TFR = Total Field Reading DBL = Datum Base Level = 56800 gammas BSR = Base Station Reading

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#### Presentation

- VLF-EM in-phase, out-of-phase and field strength readings are presented in profile form on Figure # G-1 at a scale of 1:1000
- Magnetic data were profiled and are presented on Figure # G-2 at a scale of 1:1000
- Magnetic data were contoured and are presented on Figure # G-3 at a scale of 1:1000
- Field readings and calculated values are listed in Appendix II.

#### 4. INTERPRETATION

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Discussion of Results

Total field magnetic data in the Middle Vein area were quiet with no cultural sources observed. Magnetic readings range from 55000 nT to 57700 nT within a relatively stable background of approximately 55900 nT. Three magnetic high trends were delineated by comparing profile character from line to line. Magnetic lineaments are labeled "L1", "L2" and "L3" on the total field magnetic profile and contour maps, Figure #2 and Figure #3 respectively.

Magnetic lineament "L1" consists of two parallel magnetic high trends in the northern portion of the Middle Vein grid. Lineament "L2" also consists of two parallel magnetic highs which may be the southern continuation of "L1". Due to steep terrain it was not possible to continue surveying line 200S, making delineation between "L1" and "L2" difficult. Magnetic highs on line 500S and 550S may indicate that "L2" continues to the south, but again incomplete coverage due to extreme terrain prevent delineation of these anomalies. Both "L1" and "L2" exhibit anomalies ranging from 500 nT. to 1500 nT. above background. Located on the western edge of the grid, lineament "L3" trends north-south and runs 50 meters to the east of conductor "C1". "L3" exhibits anomalous magnetic highs from 300 nT. to 500 nT. above the background of 55900 nT.

Within the survey area VLF-EM data show a response to topography seen as a positive bias on in-phase results. The topographic effect is not considered to be a problem because the slope was relatively even and therefore the topographic effect was fairly constant.

VLF-EM results over the Middle Vein grid were quiet. Only one conductor, labeled "C1" on figure # 1, was observed on the grid. Conductor "C1" is a north-south trending, weak to moderate conductive feature characterized by moderate in-phase, strong field strength and weak positive quadrature response. The magnitude of the field atrength response may be amplified due to better reception as the operator approached the top of the ridge.

#### Conclusions

Magnetic results have delineated a number of magnetic high trends which, due to the long narrow geometry of these features, are interpreted to represent basic dykes containing magnetite. There was no noticeable magnetic low response to feldspar-hornblende dykes or major structure associated with the Middle Vein, perhaps due to deep overburden or insuficient sampling intervals.

The only evidence of conductivity on the Middle Vein grid was conductor "C1". Conductor "C1" is a NNW trending, moderate conductor located in the same area as the NNE trending Middle Vein structure. "C1" is interpreted to be a structural feature, such as a splay fault, sub-parallel to the fault associated with the Middle Vein. There are a number of reasons why the Middle vein and associated structure did not respond to the VLF-EM method. One possibility is that the fault containing the Middle Vein was rehealed, perhaps by the Middle Vein itself. While conductive overburden does not appear to be present, it is possible that conductive overburden may have masked any response from the Middle Vein fault.

#### 5. RECOMMENDATIONS

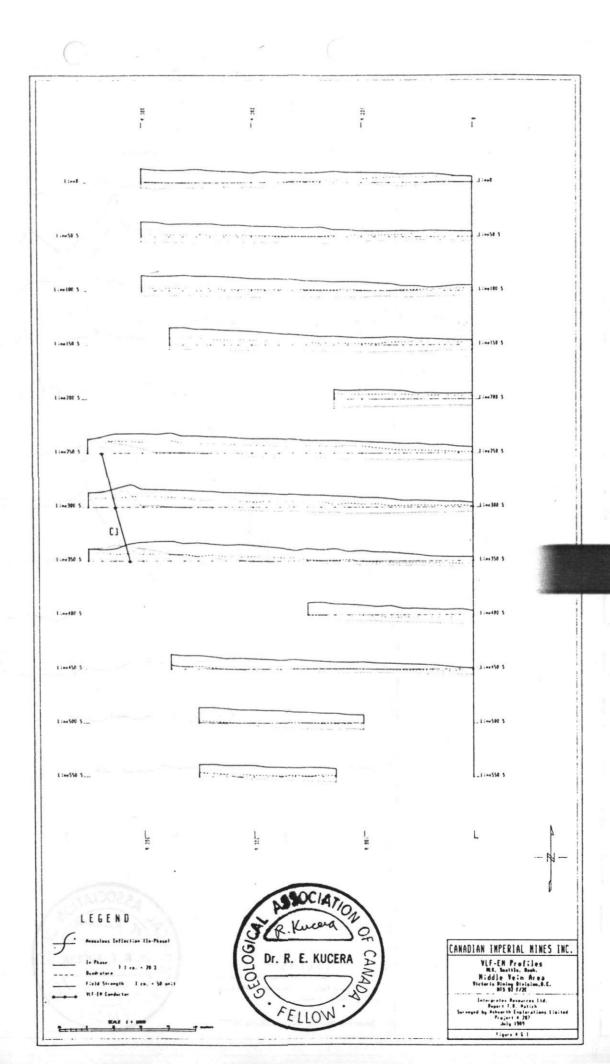
The VLF-EM and magnetic method did not appear to be succesful in delineating the Middle Vein structure. However conductor "C1" may reflect a conductive fault, therefore geological investigation of this conductor is recommended. While there is no magnetic response to known structure in the area, magnetic anomalies, interpreted as basic dykes, should be investigated to determine if any mineralization is present. The Middle Vein fault and associated feldspar-horneblende dykes would be expected to give a magnetic low response and thus a detailed gradient magnetic survey may help delineate structure in the area. An induced polarization/resistivity survey may be helpful to determine the extent of disseminated mineralization in the area and is recommended if further geophysical surveys are planned.

#### AUTHOR'S NOTE

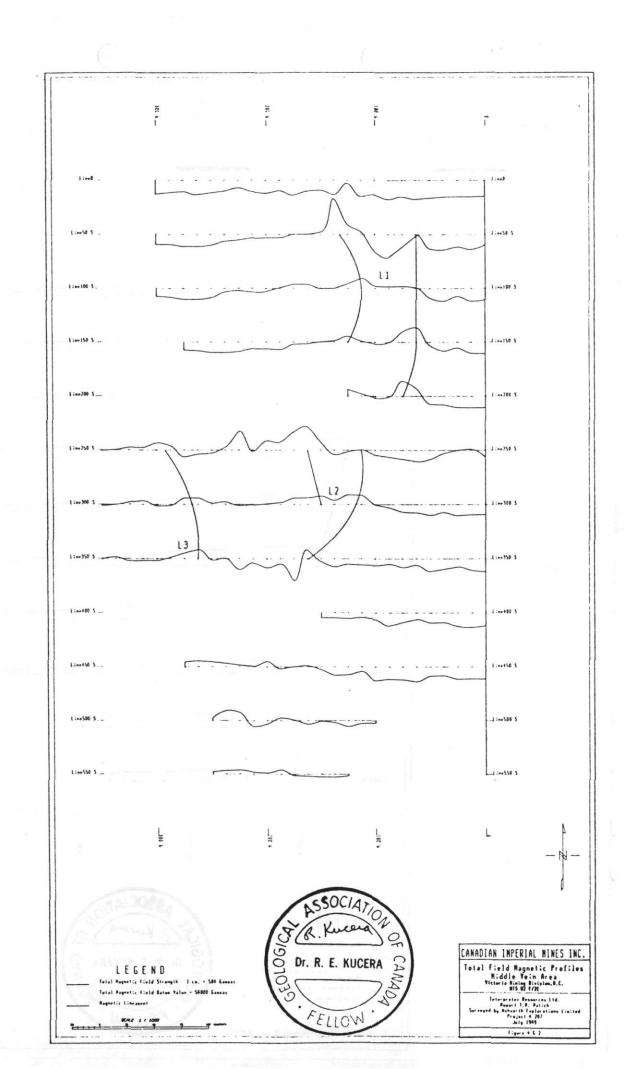
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Data interpreted in this report were accumulated without supervision by Interpretex Resources Ltd. and were supplied by the Client to the writer(s). These data and the locations on the ground from which these data were accumulated are, except when specified otherwise by the writer(s), assumed to be reliable and correct and were interpreted using this assumption.

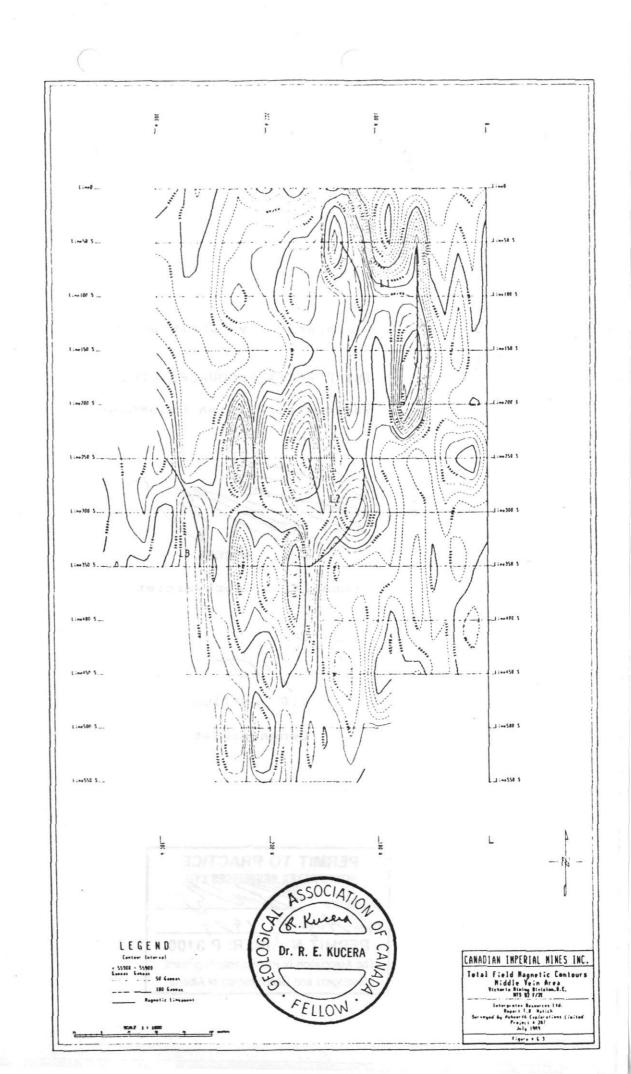


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Respectfully Submitted

INTERPRETEX RESOURCES LTD.

Vancouver, British Columbia

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E.R. ROCKEL

Consulting Geophysicist

T.R. MATICH

Geophysicist

| PERMIT TO PRACTICE<br>INTERPRETEX BESOURCES 17D.                                      |
|---|
| Signature   |
| Date Aus- 8, 19,29  |
| PERMIT NUMBER: P 3100   |
| The Association of Professional Engineers,<br>Geologists and Geophysicists of Alberta |
| dovogists and deephysicists of hiberta  |

## APPENDIX D

# GEOPHYSICAL FIELD DATA WORKSHEETS

(1989, 1991)

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| Area:        |            | SOURCES<br>ALBERN |                | ata listin         | <b>y</b> (L  | 3181       |                | Northings<br>jouthings | and Westin   |                                      |
|--------------|------------|-------------------|----------------|--------------------|--------------|------------|----------------|------------------------|--------------|--------------------------------------|
| Grid:        |            | LE VEIN           |                |                    |              |            |                |                        |              |                                      |
| Date:        |            | , 1983            |                |                    |              |            |                |                        |              |                                      |
| data type    |            | ,                 |                |                    |              | NS         | TRUMENT TY     | (PE:                   |              | DATA DETAILS:                        |
| # 1.         |            | l Field           | Macrieta       | c Values           |              |            | A VLF-EM/I     |                        | System       | Corrected total wagnetic field       |
| ₹ 2.         |            |                   | hase Val       |                    |              | -          | •              |                        | •            | Facing westerly using Seattle Transm |
| <b>\$</b> 3. | VLF-       | EM Quad           | Irature (      | Out-of-Pha         | se)          | •          | •              |                        | P            | Facing westerly using Seattle Transm |
| \$ 4.        | VLF-       | EM Fiel           | d Streng       | th                 |              | •          | •              | · •                    | •            | Seattie total field strength         |
| <b>\$</b> 5. | VLF-       | EN In-P           | Phase Val      | ues                |              | •          | •              | M                      | •            | Facing westerly using Cutler Transmi |
| <b>\$</b> 6. | VLF-       | EM Quad           | irature (      | Dut-of-Pha         | ise)         | •          | •              |                        | 4            | Facing westerly using Cutler Transmi |
| <b>#</b> 7.  | VLF-       | EM Fiel           | ld Streng      | th                 |              | •          | •              | •                      | •            | Cutler total field strength          |
| E/₩          | N/S        |                   |                |                    |              |            |                |                        |              |                                      |
| STATION      | LINE       |                   |                | <b>\$</b> 1.       | <b>\$</b> 2. | # 3.       | # 4            | # 5.                   | <b>#</b> E.  | # 7.                                 |
| line         | -350       |                   |                |                    |              |            |                |                        |              |                                      |
|              | 50         | -350              |                | 56020.0            | 23.6         | 15.0       | 410.5          | 4.1                    | 11.0         | 7.0                                  |
| -337         |            | -350              |                | 56114.3            | 22.5         | 15.1       | 412.9          | 5.7                    | 11.3         | 7.4                                  |
|              | 625        | -350              |                | 55940.7            | 24.3         | 12.3       | 425.6          | 4.4                    | 9.7          | 7.6                                  |
| -312         |            | -350              |                | 55956.8            | 32.9         | 13.7       | 418.9          | 3.4                    | 5.3          | 7.5                                  |
|              | 300        | -350              |                | 55954.3            | 36.3         | 12.5       | 410.1          | 2.5                    | 4.7          | 7.5                                  |
| -287         |            | -350              |                | 56106.3            | 37.5         | 12.8       | 401.Ú          | 1.5                    | E. 9         | 7.5                                  |
|              | 275        | -350              | -275           | 56297.7            | 38.0         | 11.5       | 385.1          | 0.3                    | 4.1          | 7.6                                  |
| -262         |            | -350              | -262.5         | 56449.4            | 33.8         | 11.9       | 378.5          | 1.6                    | 5.3          | 7.7                                  |
|              | 250        | -350              | -250           | 55978.3            | 35.0         | 8.6        | 372.6          | 1.6                    | 3.1          | 7.5                                  |
| -237         |            | -350              | -237.5         | 56062.6            | 32.6         | 10.8       | 365.6          | -1.3                   | 8 <b>.</b> 6 | 5.0                                  |
|              | 225        | -350              | -225           | 55536.0            | 30.7         | 8.2        | 363.3          | -2.3                   | - 4          | 7.8                                  |
| -212         |            | -350              | -212.5         | 55847.4            | 31.8         | 7.5        | 358.3          | -1.2                   | ·            | 7.7                                  |
|              | 200        | -350              | -200           | 55624.5            | 30.3         | 8.1        | 350.6          | -1.5                   | 5.0          | 7.8                                  |
| -187         |            | -350              | -187.5         | 55799.5            | 28.0         | 7.3        | 350.6          | -2.4                   | 4.5          | 6.0                                  |
|              | 175        | -350              | -175           | 55033.2            | 25.8         | 6.2        | 347.7          | -3.9                   | ÷.3          | 8.0                                  |
| -16          |            | -350              | -162.5         | 56433.9            | 20.9         | 5.4        | 347.5          | -6.2                   | 5.7          | <u>8.2</u>                           |
|              | 150        | -350              | -150           | 55909.6<br>55672.6 | 24.0         | 1.9        | 342.4          | -4.7<br>-6.3           | 1.2<br>0.5   | e. 1<br>6. 6                         |
|              | 7.5<br>125 | -350<br>-350      | -137.5<br>-125 | 55797.0            | 22.1<br>23.9 | 0.8<br>1.1 | 342.8<br>341.7 | -6.3<br>-4.5           | i.4          | 8.3                                  |
|              | 2.5        | -350              |                | 55755.7            | 19.5         | 2.7        | 341.7<br>346.4 | -4.J<br>-6.6           | 0.9          | 8.5                                  |
|              | 100        | -350              |                | 55734.1            | 20.8         | -1.0       | 335.3          | -5.6                   | 0.9<br>0.0   | 6.J<br>8.4                           |
|              | 17.5       | -350              |                | 55797.9            | 18.3         | -2.1       | 338.8          | -7.4                   | 0.3          | 8.7                                  |
|              | -75        | -350              |                | 55643.2            | 17.8         | -3.1       | 335.5          | -6.8                   | -2.0         | 8.5                                  |
|              | 2.5        | -350              |                | 55755.4            | 15.6         | -3.5       | 332.9          | -7.9                   | -2.2         | 8.6                                  |
|              | -50        | -350              |                | 55464.6            | 13.4         | -2.4       | 335.0          | -8.8                   | -1.4         | 8.8                                  |
|              | 37.5       | -350              |                | 55561.1            | 10.3         | -3.2       | 331.9          | -11.1                  | -3.9         | 8.7                                  |
|              | -25        | -350              |                | 55668.4            | 9.5          | -4.1       | 330.0          | -12.9                  | -4.2         | 8.6                                  |
|              | 12.5       | -350              | -12.5          |                    | 9.2          | -4.3       | 327.9          | -12.6                  | -4.5         | 8.6                                  |
| •            | 0          | -350              |                | 55450.0            | 9.0          | -4.8       | 327.3          | -13.3                  | -5.0         | 8.6                                  |
| line         | -3         |                   | •              |                    |              |            | 02.10          |                        | 0.0          |                                      |
|              | -350       | -300              | -350           | 55979.1            | 28.4         | 16.6       | 419.0          | 6.6                    | 11.3         | 7.2                                  |
|              | 37.5       | -300              | -337.5         |                    | 29.1         | 16.4       | 426.4          | 7.7                    | 10.5         | 7.1                                  |
|              | -325       | -300              |                | 56135.1            | 36.0         | 17.7       | 433.3          | 6.5                    | 11.4         | 7.0                                  |
|              | 12.5       | -300              | -312.5         |                    | 42.8         | 19.2       | 414.6          | 8.4                    | 3.4          | 7.4                                  |
|              | -300       | -300              | -300           |                    | 34.9         | 21.1       | 359.5          | 8.0                    | 1.3          | 7.8                                  |
|              | 87.5       | -300              | -287.5         |                    | 34.2         | 19.4       | 361.0          | 8.3                    | 2.9          | 7.8                                  |
|              | -275       | -300              |                | 56326.7            | 33.5         | 18.3       | 354.9          | 4.2                    | 9.0          | 8.4                                  |
|              | 62.5       | -300              | -262.5         |                    | 32.8         | 17.3       | 351.2          | 4.7                    | 8.4          | 7.7                                  |
|              | -250       | -300              |                | 56098.6            | 31.3         | 13.1       | 346.9          | 5.5                    | 5.8          | 7.9                                  |

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|--|--------|------|--------|---------|------|-------|--------|------|---------|------|
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |        |      |        |         | -    |       |        |      |         | 8.0  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | -225   |      |        |         |      | 13.4  |        |      |         |      |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | -212.5 | -300 |        |         | 28.3 | 11.4  | 340.1  | 3.0  | 6.5     | 8.0  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | -200   |      |        | 56073.1 |      | 9.4   |        | 3.1  | 6.0     | 8.1  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | -187.5 | -300 |        |         |      | 11.0  | 334.8  | 2.4  | 6.6     | 8.1  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | -175   | -300 | -175   | 56330.4 | 25.6 | 10.5  | 334.9  | 2.8  | 6.2     | 8.3  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | -162.5 | -300 | -162.5 | 56339.0 | 24.9 | 10.0  | 334.0  | 3.3  | 6.1     | 8.2  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | -150   | -300 | -150   | 56420.3 | 23.7 | 9.3   | 331.6  | 2.7  | 6.0     | 8.3  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | -137.5 | -300 | -137.5 | 56224.3 | 23.6 | 10.0  | 329.5  | 4.8  | 2.2     | 8.6  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | -125   | -300 | -125   | 56481.7 | 22.2 | 4.8   | 331.2  | 2.1  | 5.4     | 8.5  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | -112.5 | -300 | -112.5 | 56460.1 | 21.5 | 7.6   | 324.7  | 3.3  | 5.8     | 8.6  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | -100   | -300 | -100   | 56027.6 | 19.4 | 5.7   | 325.6  | 1.8  | 5.4     | 8.6  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | -87.5  | -300 | -87.5  | 55892.7 | 19.4 | 6.0   | 325.4  | 2.8  | 3.1     | 8.7  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | -75    | -300 | -75    | 55695.1 | 17.1 | 3.1   | 326.5  | 0.2  | 1.8     | 8. 9 |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | -62.5  | -300 | -62.5  | 55660.5 | 13.9 | 3.3   |        |      | 3.3     | 3. ú |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |        | -300 |        |         |      |       |        | -1.0 |         |      |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |        |      |        |         |      |       |        |      |         |      |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |        |      |        |         |      |       |        |      |         |      |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $   |        |      |        |         |      |       |        |      |         |      |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$  |        |      |        |         |      |       |        |      |         |      |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |        |      | •      | 0001110 |      |       | 00212  |      |         |      |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |        |      | - 750  | 56025 2 | × 1  | 17 9  | A22 5  | 9.2  | 77      | 6.9  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |        |      |        |         |      |       |        |      |         |      |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |        |      |        |         |      |       |        |      |         |      |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |        |      |        |         |      |       |        |      |         |      |
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| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |        |      |        |         |      |       |        |      |         |      |
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| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |        |      |        |         |      |       |        |      |         |      |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |        |      |        |         |      |       |        |      |         |      |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |        |      |        |         |      |       |        |      |         |      |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |        |      |        |         |      |       |        |      |         |      |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |        |      |        |         |      | 13.1  |        | 3.9  | 8.6     | 7.7  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |        |      |        |         |      |       |        |      |         |      |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |        |      |        |         | 25.3 | 13.8  | 325.7  | 2.4  | 9.4     | 7.8  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | -137.5 |      |        |         |      | 13.2  | 332.0  | 3.8  | 8.8     | 7.8  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | -125   | -250 |        |         | 25.3 | 12.2  | 328.7  | 3.4  | 9.1     | 7.7  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | -112.5 | -250 | -112.5 | 56058.8 | 24.7 | 14.3  | 327.1  | 7.2  | 5.5     | 8.2  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | -100   | -250 | -100   | 55824.6 | 23.2 | 13.1  | 325.8  | 2.4  | 9.0     | 7.9  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | -75    | -250 | -75    | 55627.2 | 21.1 | 7.7   | 325.3  | 1.3  | 9.1     | 6.5  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | -62.5  | -250 | -62.5  | 55526.5 | 19.4 | 6.0   | 323.7  | -0.3 | 8.4     | 8.7  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | -50    | -250 | -50    | 55627.1 | 19.6 | 5.6   | 323.7  | -0.3 | 7.3     | 8.9  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | -37.5  | -250 | -37.5  | 558%.5  | 17.1 | 5.0   | 322.3  | -3.2 | 6.5     | 8.7  |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$  | -25    | ~250 | -ක     | 56035.0 | 17.0 | 3.8   |        |      |         |      |
| 0       -250       0       55714.1       12.9       2.3       321.1       -5.1       3.4       8.9         line       -200       -125       -6353.0       19.2       10.8       310.8       6.2       6.2       8.3         -112.5       -200       -112.5       56146.7       17.6       9.2       315.1       1.8       11.1       8.2         -100       -200       -100       55957.7       18.3       9.2       319.3       3.0       10.7       8.3         -87.5       -200       -87.5       55998.1       19.0       9.4       320.3       4.0       11.4       8.4         -75       -200       -75       56743.3       18.3       9.5       319.2       3.8       11.9       8.4                    | -12.5  | -250 | -12,5  | 56090.2 | 14.0 |       |        |      |         |      |
| line         -200           -125         -200         -125         56353.0         19.2         10.8         310.8         6.2         6.2         8.3           -112.5         -200         -112.5         56146.7         17.6         9.2         315.1         1.8         11.1         8.2           -100         -200         -100         55957.7         18.3         9.2         319.3         3.0         10.7         8.3           -87.5         -200         -87.5         55998.1         19.0         9.4         320.3         4.0         11.4         8.4           -75         -200         -75         56743.3         18.3         9.5         319.2         3.8         11.9         8.4 |        |      |        |         |      |       |        |      |         |      |
| -125       -200       -125       56353.0       19.2       10.8       310.8       6.2       6.2       8.3         -112.5       -200       -112.5       56146.7       17.6       9.2       315.1       1.8       11.1       8.2         -100       -200       -100       55957.7       18.3       9.2       319.3       3.0       10.7       8.3         -87.5       -200       -87.5       55998.1       19.0       9.4       320.3       4.0       11.4       8.4         -75       -200       -75       56743.3       18.3       9.5       319.2       3.8       11.9       8.4   | -      |      | •      |         |      |       |        |      | •       |      |
| -112.5       -200       -112.5       56146.7       17.6       9.2       315.1       1.8       11.1       8.2         -100       -200       -100       55957.7       18.3       9.2       319.3       3.0       10.7       8.3         -87.5       -200       -87.5       55998.1       19.0       9.4       320.3       4.0       11.4       8.4         -75       -200       -75       56743.3       18.3       9.5       319.2       3.8       11.9       8.4  |        |      | -125   | 56353.0 | 19.2 | 10. A | 310.A  | 6.2  | 6.2     | A Z  |
| -100       -200       -100       55957.7       18.3       9.2       319.3       3.0       10.7       8.3         -87.5       -200       -87.5       55998.1       19.0       9.4       320.3       4.0       11.4       8.4         -75       -200       -75       56743.3       18.3       9.5       319.2       3.8       11.9       8.4   |        |      |        |         |      |       |        |      |         |      |
| -87.5         -200         -87.5         55998.1         19.0         9.4         320.3         4.0         11.4         8.4           -75         -200         -75         56743.3         18.3         9.5         319.2         3.8         11.9         8.4  |        |      |        |         |      |       |        |      |         |      |
| -75 -200 -75 56743.3 18.3 9.5 319.2 3.8 11.9 8.4   |        |      |        |         |      |       |        |      |         |      |
|  |        |      |        |         |      |       |        |      |         |      |
|  |        |      |        |         |      |       |        |      |         |      |
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| -50            | -200 |        | 55662.6            | 12.6          | 7.6  | 323.8 |      | 9.0         | 8.8  |
|----------------|------|--------|--------------------|---------------|------|-------|------|-------------|------|
| -37.5          | -200 |        | 55638.1            | 12.7          | 7.1  | 324.2 | 0.0  | 8.4         | 8.9  |
| -25            | -200 |        | 55511.6            | 11.7          | 6.9  | 324.3 | -0.3 | 5.3         | 9.0  |
| -12.5          | -200 |        | 55497.3            | 11.8          | 5.9  | 325.3 | -0.4 | 5.6         | 9.1  |
| 0              | -200 | 0      | 55502.4            | 12.3          | 6.4  | 323.3 | 1.0  | 5.9         | 9.1  |
| line -1        |      |        |                    |               |      |       |      |             |      |
| -275           | -150 |        | 55679.4            | 33.5          | 12.6 | 332.2 | 4.4  | 7.1         | 6.9  |
| -262.5         | -150 | -262.5 | 55649.0            | 33.8          | 13.3 | 333.1 | 7.0  | 6.4         | 7.1  |
| -250           | -150 |        | 55566.0            | 30.7          | 12.5 | 334.0 | 3.2  | 7 <b>.9</b> | 7.1  |
| -237.5         | -150 | -237.5 | 55561.7            | 30.5          | 10.9 | 332.9 | 5.2  | 4.8         | 7.4  |
| -225           | -150 |        | 55606.6            | 28 <b>. 9</b> | 9.4  | 330.4 | 1.7  | 6.2         | 7.3  |
| -212.5         | -150 | -212.5 | 55739.5            | 28.1          | 10.3 | 328.4 | 1.3  | 7.1         | 7.5  |
| -200           | -150 | -200   | 55738.1            | 26.7          | 9.0  | 329.1 | 1.0  | 6.4         | 7.6  |
| -187.5         | -150 | -187.5 | 55702.0            | 24.8          | 8.4  | 329.8 | 0.6  | 6.7         | 7.6  |
| -175           | -150 | -175   | 55942.0            | 22.6          | 6.7  | 325.2 | 0.2  | 5.7         | 7.6  |
| -162.5         | -150 | -162.5 | 55968.5            | 20.9          | 5.1  | 325.7 | 0.3  | 4.7         | 7.7  |
| -150           | -150 | -150   | 56051.3            | 19.1          | 4.8  | 325.7 | 0.3  | 6.8         | 7.8  |
| -137.5         | -150 | -137.5 | 56108.7            | 17.3          | 3.3  | 328.0 | 0.6  | 6.3         | 7.7  |
| -125           | -150 | -125   | 56317.7            | 17.7          | 3.9  | 322.0 | 0.8  | 5.9         | 7.9  |
| -112.5         | -150 |        | 56090.7            | 16.2          | 3.1  | 321.8 | 0.0  | 5.3         | 7.8  |
| -100           | -150 |        | 55960.1            | 14.9          | 2.8  | 322.1 | -1.9 | 3.6         | 7.8  |
| -87.5          | -150 |        | 56032.9            | 15.1          | 2.6  | 322.0 | -1.3 | 2.8         | 7.7  |
| -75            | -150 |        | 56530.4            | 16.4          | 5.5  | 323.4 | 0.8  | 6.4         | 7.7  |
| -62.5          | -150 |        | 56724.2            | 16.1          | 5.6  | 323.4 | 1.9  | 7.5         | 7.8  |
| -50            | -150 |        | 55874.8            | 13.9          | 6.8  | 324.7 | 1.5  | 7.0         | 8.0  |
| -37.5          | -150 |        | 55633.1            | 13.2          | 5.9  | 325.7 | 2.0  | 7.1         | 8.1  |
| -25            | -150 |        | 55776.8            |               | 6.0  | 329.1 | 1.7  | 7.2         | 8.1  |
| -12.5          | -150 |        | 55526.9            |               | 4.8  |       | 1.5  | 6.3         | 8.3  |
| 0              | -150 |        | 55511.4            |               | 6.2  | 331.2 | 0.1  | 6.4         | 8.5  |
| line -:        |      | v      | 33311.4            | 10.0          | 0.1  | JJ1.C | 0.1  | 0. 4        | 0.5  |
| -300           | -100 | -700   | 55671.6            | 29.9          | 5.7  | 329.9 | 4.0  |             |      |
| -287.5         |      |        | 55632.3            | 28.2          | 4.7  | 330.4 | -4.0 |             | 6.8  |
| -275           |      |        | 55528.0            | 28.6          | 4.9  |       | -3.1 | 4.1         | 6.9  |
| -262.5         |      |        | 55521.1            | 29.7          |      | 330.4 | -1.1 |             | 7.1  |
| -250           |      |        | 55603.2            | 28.3          | 4.5  | 332.3 | -3.5 |             | 7.8  |
| -237.5         |      | -237.5 |                    |               | 4.5  |       | -1.9 |             | 7.2  |
|                |      |        |                    | 28.2          | 4.3  | 327.5 | -1.8 | 6.1         | 7.4  |
|                |      | -225   | 55935.4<br>55870.1 |               |      |       | -1.6 |             | 7.4  |
| -212.5         | -100 |        |                    | 25.8          | 2.3  | 324.7 | -1.5 | 4.5         |      |
| -200<br>-187.5 | -100 |        | 55905.7            | 23.7          | 2.5  |       | -2.8 | 4.1         | 7.5  |
|                | -100 |        | 56074.5            | 23.2          | 2.0  |       |      | 4.6         | 7.5  |
| -175           | -100 |        | 56236.4            | 23.3          | 2.2  | 325.2 | -1.9 |             | 7.6  |
| -162.5         | -100 |        | 56233.2            | 22.0          | 2.4  |       |      |             | 7.6  |
| -150           | -100 |        | 56022.2            | 19.4          | 1.7  |       |      | 5.7         | 7.7  |
| -137.5         | -100 |        | 5 56033.1          | 19.1          | 1.6  | 324.7 |      | 6.1         | 7.8  |
| -125           | -100 |        | 5 56252.5          | 17.8          | 1.6  | 324.8 | -1.4 | 6.3         | 7.B  |
| -112.5         | -100 |        | 5 56493.3          | 18.2          | 5.8  | 325.5 | -1.7 | 6.2         | 7.8  |
| -100           | -100 |        | 56155.1            | 17.8          | 1.0  | 323.8 | -0.7 | 5.4         | 8.0  |
| -87.5          | -100 |        | 5 56120.8          | 15.9          | 0.1  | 328.2 | 9    | 4.0         | 8.1  |
| -75            | -100 |        | 5 56134.1          | 14.6          | 0.3  | 329.0 |      | 3.7         | 8.1  |
| -62.5          |      |        | 5 56072.2          | 10.7          | 2.0  | 324.6 | -4.7 | 5.4         | 8. 1 |
| -50            |      |        | 0 55586.4          | 10.4          | 2.3  | 325.9 | -4.2 | 4.4         | 8.0  |
| -37.5          |      |        | 5 55439.4          | 7.9           | 2.7  | 328.1 | -4.8 | 5.0         | 8.2  |
| -25            |      |        | 5 55667.3          | 9.4           | 4.1  | 329.0 |      |             | 8.2  |
| -12.5          |      |        |                    | 11.7          | 4.3  | 331.1 |      | 5.1         | 8.3  |
| 0              |      |        | 0 55519.5          | 11.5          | 5.3  | 333.3 | -1.0 | 5.8         | 8.5  |
| line           | -50  |        |                    |               |      |       |      |             |      |
|                |      |        |                    |               |      |       |      |             |      |

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| -300     | -50  |           | 55575.1                   | 29.3         | 5.5  | 330.1  | ú.6  | 1.6  | 7.3  |
|----------|------|-----------|---------------------------|--------------|------|--------|------|------|------|
| -287.5   | -50  | -287.5    | 55570.8                   | 28.6         | 5.0  | 327.0  | 2.6  | 1.4  | 7.3  |
| -275     | -50  | -275      | 55482.9                   | 24.9         | 3.5  | 328.7  | 2.0  | 3.1  | 7.1  |
| -262.5   | -50  | -262.5    | 55485.9                   | 25.3         | 3.7  | 327.0  | 0.9  | 3.6  | 7.2  |
| -250     | -50  | -250      | 55541.5                   | 25.2         | 4.5  | 322.2  | 1.0  | 3.3  | 7.3  |
| -237.5   | -50  | -237.5    | 55730.5                   | 25.5         | 3.1  | 325. 3 | 0.2  | 3.1  | 7.3  |
| -225     | -50  |           | 55789.7                   | 23.0         | 3.3  | 325.9  | -0.4 | 3.9  | 7.4  |
| -212.5   | -50  |           | 55880.5                   | 23.1         | 3.0  | 327.5  | 1.0  | 3.6  | 7.6  |
| -200     | -50  |           | 55893.4                   | 21.4         | 2.4  | 325.7  | 0.0  | 4.3  | 7.4  |
| -187.5   | -50  | -187.5    |                           | 20.7         | 1.8  | 326.5  | 0.3  | 3.4  | 7.5  |
| -175     | -50  | -175      |                           | 20.1         |      |        |      |      |      |
| -162.5   |      | -162.5    |                           |              | 1.4  | 327.8  | 0.0  | 3.1  | 7.6  |
|          | -50  |           |                           | 18.3         | 0.8  | 327.9  | 0.3  | 3.0  | 7.7  |
| -150     | -50  | -150      |                           | 18.1         | 0.5  | 327.5  | 0.0  | 2.3  | 7.8  |
| -137.5   | -50  | -137.5    |                           | 19.2         | 0.8  | 324.7  | 0.5  | 4.1  | 7.8  |
| -125     | -50  | -125      |                           | 14.9         | 1.9  | 322.4  | 0.6  | 4.2  | 7.8  |
| -112.5   | -50  |           | 56156.1                   | 14.7         | 5.8  | 326.4  | 1.0  | 4.7  | 7.9  |
| -100     | -50  | -100      |                           | 12.5         | 3.3  | 330.8  | 0.0  | 5.7  | 8.0  |
| -87.5    | -50  | -87.5     | 54984.9                   | 12.2         | 3.0  | 337.0  | 0.5  | 5.6  | 8.3  |
| -75      | -50  | -75       | 55467.7                   | 12.5         | 3.5  | 335.9  | 1.1  | 4.5  | 8.2  |
| -62.5    | -50  | -62.5     | 55987.0                   | 13.1         | 4.1  | 335.6  | 2.4  | 5.2  | 8.2  |
| -50      | -50  | -50       | 55368.6                   | 12.4         | 6.4  | 341.6  | 3.6  | 6.9  | 8.5  |
| -37.5    | -50  | -37.5     | 55321.2                   | 13.3         | 7.0  | 338.8  | 4.7  | 7.2  | 8.4  |
| -25      | -50  |           | 55464.4                   | 12.6         | 7.3  | 338.8  | 3.8  | 7.3  | 8.6  |
| -12.5    | -50  |           | 55347.6                   | 11.8         | 6.3  | 335.7  |      | 6.0  | 8.5  |
| 0        | -50  |           | 55566.3                   | 11.5         | 9.6  | 332.9  |      | 7.7  | 8.5  |
| line 0   | 00   | v         | 500001.5                  |              | 1.0  | 332.3  | 4.0  | 1.1  | 0.0  |
|          | ٥    | -700      | 55405.8                   | 27.3         | 2.4  | 200.0  |      |      |      |
| -287.5   | ŏ    |           | 55473.5                   |              | 2.1  | 329.9  |      | 2.6  | 7.3  |
| -275     |      |           | 55518.0                   |              | 1.0  | 327.5  | -5.1 | 2.3  | 7.3  |
|          |      | -275      |                           | 23.8         | 0.1  | 325.6  | -3.3 | 2.3  | 7.4  |
| -262.5   | 0    |           | 55380.1                   | 24.3         | -0.7 | 328.8  |      | 1.9  | 7.4  |
| -250     | 0    | -250      | 55459.7                   | 25.9         | -0.1 | 328.0  | -4.7 | 1.5  | 7.5  |
| -237.5   | Û    | -237.5    | 55544.7                   | 23.7         | -0.2 | 332.6  | -5.6 | 1.6  | 7.6  |
| -225     | 0    | -225      | 55687.8                   | 22.3         | -0.3 | 333.2  | -4.6 | 2.6  | 7.6  |
| -212.5   | 0    | -212.5    | 55523.3                   | 21.4         | -0.3 | 330.9  | -3.9 | 3.5  | 7.8  |
| -200     | 0    | -200      | 55449.3                   | 19.0         | 0.0  | 332.1  | -4.5 | 3.3  | 7.9  |
| -187.5   | 0    | -187.5    | 55559.9                   | 20.9         | -0.1 | 331.8  | -3.3 | 3.9  | 7.9  |
| -175     | 0    | -175      | 55355.4                   | 19.5         | 0.4  | 335.7  | -1.5 | 4.4  | 8.0  |
| -162.5   | 0    | -162.5    | 55532.7                   | 18.9         | 1.5  | 337.6  | -1.7 | 4.5  | 8.0  |
| -150     | 0    | -150      | 55587.8                   | 18.5         | 1.7  | 338.2  | -1.1 | 5.3  | 8.1  |
| -137.5   | 0    | -137.5    | 55383.3                   | 19.5         | 2.5  | 337.9  | -0.1 | 5.3  | 8.2  |
| -125     | 0    | -125      | 55907.9                   | 21.7         | 3.6  | 340.5  | 1.3  | 5.9  | 8.3  |
| -112.5   | 0    |           | 55298.2                   | 20.1         | 6.0  | 340.7  | 1.6  | 8.0  | 8.3  |
| -100     | 0    |           | 55371.0                   | 19.9         | 7.0  | 341.8  | 2.0  | 9.0  | 8.6  |
| -87.5    | Ó    |           | 55158.0                   | 19.5         | 8.9  | 342.5  | 1.9  | 9.7  | 8.5  |
| -75      | 0    |           | 55278.7                   | 18.5         | 9.5  | 341.5  | 3.4  |      |      |
| -62.5    | ŏ    |           | 55169.4                   | 16.9         | 10.3 | 337.0  |      | 10.5 | 8.6  |
| -50      | ŏ    |           | 55222.0                   | 17.4         | 10.0 |        | 1.6  | 10.0 | 8.7  |
| -37.5    | ŏ    |           | 55270.6                   |              |      | 338.7  | 3.2  | 10.1 | 8.7  |
| -37.3    | 0    |           |                           | 17.7         | 11.4 | 355.3  | 3.1  | 10.5 | 10.7 |
| -12.5    |      |           | 55283.8                   | 15.7         | 10.5 | 358.4  | 3.6  | 9.1  | 10.3 |
|          | 0    |           | 55277.8                   | 12.6         | 11.2 | 355.9  | 2.1  | 8.1  | 10.4 |
| 0<br>1 i | 0    | 0         | 55295.7                   | 12.5         | 9.9  | 355.3  | 2.4  | 6.2  | 10.4 |
| line -5  |      | <b></b> . | <b>PP</b> • • • • • • • • | <b>•</b> • • | -    |        |      |      |      |
| -250     | -550 |           | 56148.1                   | 24.3         | 8.1  |        | -7.2 | -5.2 | 8.3  |
| -237.5   | -550 |           | 56203.9                   | 25.0         | 6.5  |        | -7.0 | -4.2 | 8.2  |
| -225     | -550 |           | 56224.0                   |              | 5.3  |        | -9.2 | -5.5 | 8.2  |
| -212.5   | -550 | -212.5    | 56137.1                   | 23.0         | 4.7  | 350.7  | -7.0 | -4.6 | 8.4  |
|          |      |           |                           |              |      |        |      |      |      |

|      | -200         | -550 | -200   | 56103.2   | 22.8 | 3.2  | 342.3 | -6.8  | -5.5 | 8.3         |
|------|--------------|------|--------|-----------|------|------|-------|-------|------|-------------|
|      | -187.5       | -550 | -187.5 | 56241.3   | 20.0 | 2.7  | 343.7 | -9.9  | -3.2 | 8.7         |
|      | -175         | -550 | -175   | 55976.0   | 19.6 | 1.4  | 339.2 | -11.7 | -4.6 | 8.4         |
|      | -162.5       | -550 | -162.5 | 55949.1   | 18.1 | 2.5  | 336.9 | -11.2 | -4.1 | 8.4         |
|      | -150         | -550 | -150   | 55912.7   | 18.8 | 0.8  | 332.4 | -10.1 | -4.1 | 8.5         |
|      | -137.5       | -550 | -137.5 | 55907.0   | 18.4 | 2.8  | 332.6 | -10.1 | -5.0 | 8.5         |
|      | -125         | -550 |        | 55972.6   | 16.1 | 2.0  | 328.2 | -10.3 | -2.6 | 8.5         |
| line | -50          |      |        |           |      |      |       |       |      |             |
|      | -250         | -500 | -250   | 56142.1   | 30.3 | 4.6  | 357.9 | -9.4  | -3.9 | 8.3         |
|      | -237.5       | -500 | -237.5 | 56494.0   | 30.4 | 3.0  | 354.4 | -8.4  | -2.6 | 8.4         |
|      | -225         | -500 | -225   | 56404.0   | 28.4 | 1.5  | 349.1 | -9.9  | -4.8 | 8.3         |
|      | -212.5       | -500 | -212.5 | 55767.9   | 26.2 | 0.2  | 341.3 | -10.9 | -3.3 | 8.4         |
|      | -200         | -500 | -200   | 55882.9   | 26.1 | 0.4  | 342.2 | -10.4 | -3.7 | 8.4         |
|      | -187.5       | -500 | -187.5 | 56161.8   | 25.0 | -0.3 | 338.1 | -11.9 | -4.5 | 8.4         |
|      | -175         | -500 | -175   | 56068.6   | 24.8 | 0.7  | 334.0 | -11.4 | -5.2 | <b>5. 4</b> |
|      | -162.5       | -500 | -162.5 | 55875.4   | 21.8 | 0.3  | 331.2 | -13.5 | -3.7 | 8.3         |
|      | -150         | -500 | -150   | 56003.9   | 21.3 | -0.7 | 326.9 | -12.9 | -3.5 | 8.3         |
|      | -137.5       | -500 | -137.5 | 55953.8   | 19.7 | -1.6 | 323.5 | -12.1 | -4.5 | 8.4         |
|      | -125         | -500 | -125   | 55769.3   | 19.4 | -1.8 | 323.5 | -12.7 | -3.0 | 8.4         |
|      | -112.5       | -500 | -112.5 | 55908.0   | 16.9 | -1.8 | 327.3 | -13.6 | -3.3 | 8.5         |
|      | -100         | -500 | -100   | 55935.6   | 16.6 | -2.3 | 322.5 | -14.4 | -4.5 | 8.6         |
| lin  | e -4         | 50   |        |           |      |      |       |       |      |             |
|      | -275         | -450 | -275   | 56261.5   | 28.5 | 8.1  | 368.9 | -1.8  | -3.1 | 8.4         |
|      | -262.5       | -450 | -262.5 | 56314.2   | 26.4 | 4.5  | 366.0 | -3.8  | -2.8 | 8.4         |
|      | -250         | -450 | -250   | 56274.0   | 26.5 | 5.6  | 360.3 | -2.4  | -2.9 | 8.5         |
|      | -237.5       | -450 | -237.5 | 56204.4   | 24.2 | 2.6  | 355.3 | -3.7  | -4.1 | 8.4         |
|      | -225         | -450 | -225   | 56119.5   | 21.1 | -0.4 | 355.1 | -7.8  | -4.1 | 8.5         |
|      | -212.5       | -450 | -212.5 | 56076.3   | 21.7 | -0.6 | 352.2 | -7.4  | -4.5 | 8.4         |
|      | -200         | -450 | -200   | 56294.5   | 20.6 | -0.1 | 344.3 | -5.5  | -5.7 | 8.5         |
|      | -187.5       | -450 | -187.5 | 55950.3   | 19.8 | 0.3  | 342.9 | -6.9  | -5.8 | 8.4         |
|      | -175         | -450 | -175   | 56052.2   | 18.1 | -0.4 | 342.8 | -9.1  | -5.4 | 8.5         |
|      | -162.5       | -450 | -162.5 | 56096.3   | 19.0 | 0.3  | 339.7 | -7.2  | -5.5 | 8.5         |
|      | -150         | -450 | -150   | 55912.2   | 17.2 | 0.2  | 339.4 | -8.8  | -4.6 | <b>S. 4</b> |
|      | -137.5       | -450 | -137.5 | 55647.8   | 15.8 | 0.6  | 340.2 | -9.0  | -3.9 | 8.6         |
|      | -125         | -450 | -125   | 55677.7   | 14.6 | 0.7  | 337.1 | -8.6  | -3.5 | 8.5         |
|      | -112.5       | -450 |        | 55836.3   | 14.2 | 0.9  | 335.3 | -9.5  | -3.8 | 8.E         |
|      | -100         | -450 |        | 55413.2   |      | 0.3  | 337.7 |       | -4.3 | <b>S.</b> 7 |
|      | -87.5        | -450 |        | 55472.7   | 12.9 | -0.8 | 336.4 | -9.4  | -4.0 |             |
|      | -75          | -450 |        | 5 55447.1 | 12.2 | -1.1 | 336.9 | -9.2  |      | 8.9         |
|      | -62.5        | -450 |        | 5 55361.0 | 11.2 | -2.1 |       | -10.9 |      |             |
|      | -50          | -450 |        | 55626.2   | 10.6 | -1.8 |       | -10.9 |      |             |
|      | -37.5        | -450 |        | 5 55638.0 | 9.4  | -2.2 |       |       | -6.6 |             |
|      | -25          | -450 |        | 5 55475.3 | 7.1  | -3.6 | 332.0 | -11.6 | -7.3 |             |
|      | -12.5        | -450 |        | 5 55486.4 | 4.6  | -3.0 |       | -14.8 |      |             |
|      | 0            | -450 | (      | 0 55476.4 | 3.5  | -2.8 | 329.0 | -15.5 | -6.9 | 8.9         |
| 11   |              | 400  |        |           |      |      |       |       |      |             |
|      | -150         |      |        | 0 55813.0 | 23.1 | -1.4 |       |       |      |             |
|      | -137.5       | -400 |        | 5 55815.1 | 24.6 | -0.8 |       | -5.5  |      | 8.5         |
|      | -125         | -400 |        | 5 55784.6 | 21.7 | -2.4 |       |       |      | 8.6         |
|      | -112.5       | -400 |        | 5 55832.8 | 21.1 | -2.4 |       |       |      | 8.6         |
|      | -100         | -400 |        | 0 55724.8 | 19.5 | -2.3 |       | -7.3  | -2.1 | 9.0         |
|      | -87.5        | -400 |        | 5 55439.0 | 17.2 | -1.7 |       |       | -2.1 | 8.7         |
|      | -75          | -400 |        | 5 55601.5 | 18.4 | -4.8 |       | -8.8  |      | 8.8         |
|      | -62.5        | -400 |        | 5 55741.7 | 13.7 | -3.7 |       |       |      | 8.9         |
|      | -50<br>-37.5 | -400 |        | 0 55578.0 | 13.8 | -4.1 |       |       |      | 8.9         |
|      | -31.3        | -400 | , -3/. | 5 55600.5 | 12.2 | -4.4 | 317.6 | -11.5 | -4.6 | 8.9         |

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| -25   | -400 | -25   | 55412.5 | 11.4 | -4.6 | 314.5 | -12.7 | -4.2 | 8.9 |
|-------|------|-------|---------|------|------|-------|-------|------|-----|
| -12.5 | -400 | -12.5 | 55375.9 | 12.3 | -3.9 | 313.1 | -12.3 | -4.0 | 8.9 |
| 0     | -400 | 0     | 55444.6 | 9.1  | -4.4 | 311.3 | -17.2 | -5.9 | 8.8 |

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DATA LISTING

Line & Station + = Northings and Eastings - = Southings and Westings

Area : Port Alberni Grid : Middle Vein Date : June, 1991

Data Type(s)

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Data Details

#1. Total Field Magnetic Values
#2. VLF-EM In-Phase Values
#3. VLF-EM Quadrature (out of Phase)
#4. VLF-EM Field Strength
#5. VLF-EM In-phase Values
#6. VLF-EM Quadrature (out of Phase)
#7. VLF-EM Field Strength

Corrected Total field Westerly using Annapolis station Westerly using Annapolis station Annapolis Total Field Strength Westerly using Hawaiian station Westerly using Hawaiian station Hawaii Total Field Strength

The instrument used was the EDA VLF-EM/Magnetic System in gathering all of the above data types.

| line                      | 0                      |             |                 |           |      |              |
|---------------------------|------------------------|-------------|-----------------|-----------|------|--------------|
| -50<br>-10.2 1.3          | 0<br>10 <b>.</b> 65    | -50         | 56181.4         | 5.3       | 14.5 | 7.17         |
| -37.5                     | 0                      | -37.5       | 56235.3         | 4.9       | 14.3 | 7.26         |
| -8 <b>.</b> 900001<br>-25 | 1.3 11<br>0            | L.45<br>-25 | 56213.1         | 5.8       | 13.6 | <b>7.</b> 55 |
| -6.5 .9<br>-12.5          | 11.99<br>0             | -12.5       | 56173.5         | 5.8       | 13.1 | 7.44         |
| -6.4 .3                   | 11.96                  |             |                 |           |      |              |
| 0<br>* *                  | 0<br>★                 | 0           | 56000.91        | *         | *    | *            |
| line                      | -50                    |             |                 |           |      |              |
| -150                      | -50                    | -150        | 56034.3         | -14.1     | .7   | 6.97         |
| -16.9 8.6<br>-137.5       | 11 <b>.</b> 29<br>-50  | 127 5       | 56010.8         | -16.3     | 3.8  | 6.8          |
| -21.3 7.2                 | -50                    | -13/.5      | 20010-0         | -10.5     | 3.0  | 0.0          |
| -125                      | -50                    | -125        | 56036           | -21.8     | 3.2  | 6.67         |
| -27.1 6.2                 | 10.62                  |             |                 |           |      | ••••         |
| -112.5                    | -50                    | -112.5      | 56081           | -15.5     | 3.3  | 6.82         |
| -29 5.1                   | 10.99                  |             |                 |           |      |              |
| -100                      | -50                    | -100        | 56210.6         | -13.6     | 5.2  | 6.82         |
| -27.9 4.1                 | 11.41                  |             |                 |           |      |              |
| -87.5                     | -50                    | -87.5       | 56556.8         | -13.7     | 5.5  | 6.94         |
| -30.4 2.7<br>-75          | 11.46<br>-50           | -75         | 55742.4         | -11.7     | 5.9  | 7.17         |
| -25.9 1.2                 | -50                    | -75         | 55742.4         | -11./     | 5.9  | /1/          |
| -62.5                     | -50                    | -62.5       | 56052.2         | -10       | 6    | 7.1          |
| -27.1 0                   | 11.6                   |             | 3003242         | 10        | 0    | /•1          |
| -50                       | -50                    | -50         | 56076.4         | -7.8      | 6.4  | 7.19         |
| -19.4 .1                  | 13.33                  |             |                 |           |      |              |
| -37.5                     | -50                    | -37.5       | 56157.7         | -11.9     | 5.3  | 7.11         |
| -31.3 -1.6                | 11.81                  |             |                 |           |      |              |
| -25                       | -50                    | -25         | 56276.7         | -7.5      | 4.3  | 7.21         |
| -33.2 -2.3                | 12.47                  | 105         | 5(200           | 0 400001  | •    | 7.04         |
| -12.5                     | -50                    | -12.5       | 56390 -         | -8.400001 | 4    | 7.04         |
| -36.7 -2.5<br>0           | 12.52<br>-50           | 0           | 56192.8         | -8.400001 | 4.3  | 7 76         |
| -34.8 -3.5                |                        |             | 30192.0         | -0.40001  | 4.3  | 7.26         |
| 12.5                      | -50                    | 12.5        | 55964.8         | -9.2      | 2.9  | 7.39         |
| -40.2 -6.5                | 12.94                  |             | 0070110         | 512       | 24.5 |              |
| 25                        | -50                    |             | 55968.3         | -7.9      | 2.8  | 7.22         |
| -38.4 -4.8                | 14.05                  |             |                 |           |      |              |
| 37.5                      | -50                    | 37.5        | 55 <b>756.7</b> | -2.2      | 6.3  | 7.36         |
| -26.9 -3.8                | 14.61                  |             |                 |           |      |              |
| line                      | -100                   |             |                 |           |      |              |
| -125                      | -100                   | -125        | 56379.4         | -12.2     | -4.8 | 6.59         |
| -8.7 4.5<br>-112.5        | 13.23<br>-100          | -112.5      | 56025.1         | -11.3     | _5 F | 6.00         |
| 7.2 5.5                   | -100<br>12 <b>.</b> 81 | 11240       | JUU2J•1         | -11-2     | -5.5 | 6.88         |
| -100                      | -100                   | -100        | 56252           | -8.8      | -3.4 | 6.67         |
| 2.6 1.9                   | 11.63                  |             |                 |           |      |              |
| -87.5                     | -100                   | -87.5       | 56385.9         | -7        | -2.3 | 6.66         |

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| 4.7      |                | 11.57                  | 75          | <b>F</b> (202) (                     | 7.4   |      |              |
|----------|----------------|------------------------|-------------|--------------------------------------|-------|------|--------------|
| 7        |                | -100<br>11 <b>.</b> 14 | -75         | 56323.6                              | -7.6  | -1.7 | 6.74         |
|          | -62.5          | -100                   | -62.5       | 56016                                | -3.1  | 5    | <b>6.7</b> 3 |
| 1.8      | -5.3           | 11.18                  |             | 56058.5                              |       |      |              |
|          | -50            | -100                   | -50         | 56058.5                              | -3    | -1.1 | 6.29         |
| -9.7     | -9             | 10.33<br>-100          | -37.5       | 56118.2                              | -5.1  | -1.7 | 7.12         |
| -4.2     | -8.5           | 11.4                   | 57.5        | 5011042                              | 3.1   | 1.,  | 7.12         |
| ,        | -25            | -100                   | -25         | 56118 <b>.</b> 2<br>56173 <b>.</b> 7 | -3.7  | -1.8 | 6.82         |
| -2.8     | -9.3           | 10.95                  |             |                                      |       |      |              |
|          | -12.5          | -100                   | -12.5       | 56218.4                              | -6.9  | -2.5 | 7.06         |
| -9.1     | -9 <b>.</b> 8  | 11.6<br>_100           |             | 0 56210.8                            | -65   | _1   | 4 6.88       |
| -8.40    | 0001 -         | 11.5 1                 | 1.43        | 0 30210-0                            | -0.5  |      | 4 0.00       |
| 0.40     | 12.5           | -100                   | 12.5        | 56227                                | -2.9  | -1.7 | 6.87         |
| -9.90    | 0001           | -9.1 1                 | 1.53        |                                      |       |      |              |
|          | 25             | -100                   | 23          | 56116.7                              | -4.3  | -1.3 | 7.02         |
| -10.4    | -8.8           | 11.35                  |             |                                      |       |      |              |
|          | 37.5           | -100                   | 37.5        | 55939                                | -5.3  | -2   | 7.14         |
| -15.9    | -9.3           | 11.33                  | <b>F</b> .0 |                                      |       | -    |              |
| 10.0     | 50             | -100                   | 50          | 55826.8                              | 2     | 2    | 7.03         |
| -10-8    | -10.3          | 10.76                  | 625         | 55843                                | -4.2  | -1.1 | <b>7.0</b> 5 |
| -167     | -9.900001      |                        |             | JJ043                                | -4.2  | -1.1 | 7.05         |
| 10.7     | 75             | -100                   | 75          | 55837.7                              | 4     | 3    | 6.91         |
|          | -12.8          |                        |             | 0000707                              | • 1   | •.5  | 0.91         |
|          | 87.5           | -100                   | 87.5        | 55878.7                              | -2.1  | .7   | 7.21         |
| -20.6    | -11.9          | 11.52                  |             | 55855.4                              |       |      |              |
|          | 100            | -100                   | 100         | 55855.4                              | -2    | 3.1  | 7.28         |
| - / 4. / |                | 11.7                   |             |                                      |       |      |              |
|          | line           | -150                   | 1125        |                                      | 17.4  |      | 6.00         |
| _12 2    | -1125          | -150                   | -112.5      | 20021-2                              | -1/.4 | -5.5 | 6.93         |
| -12•2    | -100           | -150                   | -100        | 56051.2<br>56068.4                   |       | -57  | 6.81         |
| -21.2    | 8.3            | 10.5                   | 100         | 30000.4                              | 20.9  | 5.7  | 0.01         |
|          | -87.5          | -150                   | -87.5       | 56065.6                              | -17.9 | -5.4 | 6.96         |
| -27.7    | 5.5            | 11.61                  |             |                                      |       |      |              |
|          | <b>-7</b> 5    | -150                   |             | 56098.4                              | -14.5 | -4.4 | 7.1          |
| -14.4    |                | 12.52                  |             |                                      |       |      |              |
| 20.2     | -62.5          |                        |             | 56116                                | -16.1 | -4.3 | 6.93         |
| -20.2    | -1.4<br>-50    | 12.53<br>-150          |             | 56138.2                              | -17.4 | -4.4 | 6.04         |
| -29.4    | -30            |                        | -30         | 30130.2                              | -1/.4 | -4.4 | 6.94         |
| 2.744    | -37 <b>.</b> 5 | -150                   |             | 56161.6                              | -16.5 | -3.2 | 6.97         |
| -26.2    |                | 11.29                  |             | 0010100                              | 2010  |      | 0.97         |
|          | -25            | -150                   |             | 56235                                | -18.2 | -3.9 | <b>7.0</b> 6 |
| -34.4    | -7.6           |                        |             |                                      |       |      |              |
|          | -12.5          |                        | -12.5       | 56185.5                              | -19.9 | -3.5 | 6.08         |
| -29.5    |                | 10.74                  |             | F/4 00 -                             |       |      |              |
| -39.3    | 0              | -150<br>11.4           |             | 56190.7                              | -19.4 | -4.3 | 6.93         |
| - 33.3   | 12.5           |                        |             | 55989.8                              | -20.4 | -5.9 | 7.18         |
| -45.3    |                | 12.89                  |             |                                      | 2007  | J•7  | 1•TO         |
|          |                |                        |             |                                      |       | ~    |              |

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| 50.0  | 25                    | -150                   | 25          | 56094.7          | -23      | -5.5    | 7.12         |
|-------|-----------------------|------------------------|-------------|------------------|----------|---------|--------------|
| 3     | 7.5                   | 12.62<br>-150          | 37.5        | 56137 <b>.</b> 8 | -21.7    | -6.4    | 6.98         |
| -48.3 | -15<br>50             | 11.92<br>-150          | 50          | 56105.8          | -21.9    | -6.5    | <b>7.1</b> 3 |
| -43.5 | -13.2                 | 11.65                  | 50          | 5010540          | 21.9     | 0.5     | 7.15         |
| 6     | 2.5                   | -150                   | 62.5        | 55983.1          | -17.2    | -6.5    | 7.06         |
| -39.2 | -12.9                 | 11.95                  | 76          |                  | 10.0     |         | <b>7</b> 00  |
|       |                       | -150<br>12 <b>.</b> 26 |             | 55890.5          | -19.8    | -/.1    | 7.23         |
| -42.9 | 7.5                   | -150                   | 87.5        | 55711.2          | -16.2    | -6.5    | 7.29         |
| _28   | _11 7                 | 1211                   |             |                  |          |         |              |
|       | 100                   | -150                   | 100         | 55817.2          | -15.5    | -3.1    | 6.84         |
| -52.9 | -15.7                 | 12.2                   |             | ==000            |          |         |              |
| 51 0  | .2.5                  | -150<br>11.53          | 112.5       | 55898.3          | -12.6    | -3.7    | 6.87         |
|       | -10.5<br>ne           |                        |             |                  |          |         |              |
|       |                       |                        | -200        | 56345.5          | -17.7    | -7      | 6.52         |
| 21.7  | 13.1                  | 12.11                  |             |                  |          |         |              |
| -18   | 7.5                   | -200 -                 | 187.5       | 56028.3          | -16.4    | -8.1    | 6.5          |
| 27    | 12.6                  | 11.9                   |             | 56045 0          |          | • •     | < <b>FP</b>  |
| -     | -175<br>18 <b>.</b> 3 | -200                   | -175        | 56045.3          | -11.8    | -8.2    | 6.57         |
| -16   | 10.5                  | -200                   | -162.5      | 56784.1          | -11.2    | -8.8    | 6.49         |
| 29.2  | 20.7                  | 11                     | 1020        | 5070111          | -13.3    | 0.0     | 0.49         |
| -     | -150                  | -200                   | -150        | 56618.1          | -13.3    | -7.7    | 6.45         |
| 24.1  | 20.8                  | 10.89                  |             |                  |          |         |              |
| -13   | 37.5                  | -200 ·<br>12.49        | -137.5      | 56058.1          | -13.8    | -8.3    | 6.58         |
| 21.5  | -125                  | -200                   | -125        | 56026-8          | -12.7    | -71     | 6 58         |
| 24.4  | 18.5                  | 11.57                  | 120         | 3002000          | 12.17    | /•1     | 0.00         |
| . 1 1 | 175                   | - 200                  | -112.5      | 56067.9          | -16.9    | -8.3    | 6.62         |
| 10    | 13.8                  | 11.1                   |             |                  | -14.8    |         |              |
| 170   | -100                  | -200                   | -100        | 56107.3          | -14.8    | -7.6    | 6.77         |
| 1/.3  | 13-5<br>97-5          | -200                   | -87.5       | 56140 4          | -17.4    | -67     | 6.8          |
|       | 10.3                  | 13.2                   |             |                  |          |         |              |
|       | -75                   | -200                   | <b>-7</b> 5 | 56135.6          | -15.1    | -6.5    | 6.82         |
| 6.2   | 8.5                   | 11.18                  |             |                  |          |         |              |
|       | 62.5                  | -200                   | -62.5       | 56156.5          | -15.7    | -7.1    | 6.84         |
| 8     | 4.5<br>-50            | -200                   | -50         | 561936           | -12.3    | _0 1    | 6 71         |
| -3.2  | -2.8                  | 12.4                   | -30         | 50195.0          | -12.5    | -0.1    | 0./1         |
|       | 37.5                  | -200                   | -37.5       | 56230.7          | -12.4    | -8.5    | 6.66         |
| -4.5  | -5.8                  | 12.3                   |             |                  |          |         |              |
|       | -25                   | -200                   | -25         | 56352.4          | -14.5    | -9      | 6.91         |
| -12.4 | -9.8                  | 12.32                  | _125        | ECOAD A          | -15.4 -9 | 400001  | 7.07         |
| -16.7 | -13                   | -200<br>12 <b>.</b> 44 | -12.0       | JUZ42+4          | -10.4 -5 | **0000T | 7.07         |
|       | 0                     | -200                   | C           | 56246.5          | -16.1    | -8.8    | <b>7.</b> 01 |
|       | -13.3                 | 12.72                  |             |                  |          |         |              |
|       |                       |                        |             | 56173.8          | -13.9    | -9.5    | 6.94         |
| -15.4 |                       | 12.52                  |             | 56076 2          | -15.6    | 0.0     | 3.01         |
|       | £0                    | -200                   | 20          | 5.01000          | 0.61-    | -8.8    | 7.01         |

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| -18.8               | -15                             | 12.46                  |        |                 |               |          |               |
|---------------------|---------------------------------|------------------------|--------|-----------------|---------------|----------|---------------|
|                     | <b>37.</b> 5                    | -200                   | 37.5   | 55982.9         | -19.2         | -9.5     | 7.09          |
|                     | -15.8<br>50                     | -200                   | 50     | 55999.2         | -15           | -9.3     | 7.01          |
| -29.9               | 62.5                            | -200                   | 62.5   | 55964.9         | -13.4 -8.     | 400001   | 7.1           |
| -22.1               |                                 | 12 <b>.</b> 49<br>-200 | 75     | 55604.9         | <b>-17.</b> 5 | -8.6     | 7.37          |
| -28.9               | -14                             | 12.66                  |        |                 | -15.4         |          | 7.13          |
| -23.2               | -13.4<br>100                    | 12.71                  |        |                 | -15.8         |          | 7.07          |
| -27.8               | -12.5                           | 12.73                  |        |                 |               |          |               |
| -34.2               | -14.7                           | 12.69                  |        |                 | -17.2         |          |               |
|                     | 125<br>-18 <b>.</b> 5           |                        |        | 55896           | -13.4         | -7.2     | 7.12          |
| 1                   |                                 | -200                   | 137.5  | 55926           | -14.2         | -7.6     | 7.21          |
|                     | 150                             | -200                   | 150    | 55947.1         | -14.1         | -6.8     | 7.34          |
| 1                   |                                 | -200                   | 162.5  | 56022.1         | -13.2         | -6.4     | 7.47          |
|                     | -18.5<br>175                    | -200                   | 175    | 56053.6         | -14.6         | -6.9     | 7.37          |
| -51 <b>.</b> 1      | -22.9<br>18 <b>7.</b> 5         | 13 <b>.</b> 56<br>-200 | 187.5  | 56182.3         | -9.3          | -6.6     | 7.6           |
| -46.4               | -22                             | 12.99                  | ) 200  | 56026 6         | -13.4         | -6.8     | 7.62          |
| -53                 | -22.2                           | 13.34                  |        | 50020.0         | -13.4         | -0.0     | 7.02          |
|                     | -200                            | -250<br>-250           | -200   | 56641           | -14.2         | -3       | 9.42          |
| 6 <b>.7</b><br>-]   | 17.7<br>187 <b>.</b> 5          | 13.01<br>-250          | -187.5 | 56341           | -14.1         | -2.5     | <b>9.</b> 55  |
| 4.3                 | 18                              | 13.29                  |        |                 |               | -3.3     | 9.84          |
| 6                   | 15                              | 15.49                  | -162.5 | 56009 0         | -13           | 2.2      |               |
| 3.5                 | 162.5<br>15.9                   | 14.64                  |        |                 | -13.8         | -3.2     | 9 <b>.7</b> 8 |
| 10.2                | -150<br>19 <b>.</b> 2           | -250<br>12 <b>.</b> 66 | -150   | 56357 <b>.7</b> | -14           | -2.8     | 9.44          |
| -:<br>10 <b>.</b> 2 | 137 <b>.</b> 5<br>15 <b>.</b> 5 | -250<br>15 <b>.</b> 66 | -137.5 | 56107.2         | -12           | -3       | 10.18         |
| .8                  | -125<br>17.5                    | -250<br>13 <b>.</b> 85 | -125   | 55965.8         | -15.4         | -3.7     | 9.71          |
| -                   | 112.5                           | -250                   | -112.5 | 55921.3         | -15.3         | -3.5 9   | 599999        |
| -1.9                | 18.6<br>-100                    | 13.57<br>-250          | -100   | 55968.8         | -13.4         | -3.3     | 9.48          |
| <b>4.</b> 6         | 18.8<br>-87.5                   | 13.54<br>-250          | -87.5  | 56052.9         | -15.6         | -3.8     | 9.52          |
| -5.3                | 16.1<br>-75                     | 13.62<br>-250          |        | 56100.9         | -15.6         | -4       | 9.59          |
| -8.8                | 12                              | 13.96                  |        |                 |               | -        |               |
| -12                 | 62.5<br>5.3                     | -250<br>14 <b>.</b> 13 | -02.0  | 56180.1         | -14.1         | -4.5 9.8 | 549999        |

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| 100   | -50                   | -250  | -50    | 56205.5         | -15.2          | -5.7   | 9.87         |
|-------|-----------------------|-------|--------|-----------------|----------------|--------|--------------|
| -19.8 | -37.5                 | -250  | -37.5  | 56266 <b>.7</b> | -15.6          | -5.4   | <b>9.9</b> 6 |
| -25.9 | -3.3<br>-25           | -250  | -25    | 56268.6         | -15.9          | -6.2   | 9.88         |
| -27.2 | -6.1                  | 14.38 |        |                 |                |        |              |
|       |                       |       |        |                 | -18.7          |        |              |
|       | -12.7<br>0<br>-11.9   | -250  | 0      | 56148.6         | -18.6          | -6.1   | 9.82         |
|       | 12.5                  | -250  | 12.5   | 55812.4         | -17.4          | -5.5   | 9.86         |
| -33.5 | -11.5<br>25           | -250  | 25     | 55913           | -16.2          | -5.2   | 10.13        |
| -36.2 | -11.7                 | 14.59 |        |                 |                |        |              |
| 27.0  | 37.5                  | -250  | 37.5   | 56105.7         | -16.2          | -5.3   | 10.26        |
| -3/.2 | -11.5<br>50<br>-12.4  | -250  | 50     | 56286.6         | -15.9          | -5.4   | 10.15        |
|       | 62.5                  | -250  | 62.5   | 55691.5         | -15.7          | -5.4   | 10.3         |
| -34.5 | -14.4                 | 16.12 |        |                 |                |        |              |
|       | 75                    | -250  | 75     | 56031.2         | -15.6          | -4.7   | 10.08        |
| -33.8 | -10.4<br>87.5         | -250  | 87.5   | 55660.1         | -16<br>-17.6   | -5     | 9.66         |
| -37.0 | -12.2                 | -250  | 100    | 55744.8         | -17.6          | -6.2   | 9.79         |
| -42.3 | -13.5                 | 13.32 |        |                 |                |        |              |
| 40 F  | 112.5                 | -250  | 112.5  | 55626           | -19.2          | -5.7   | 9.349999     |
| -43.5 | -14.6                 | -250  | 125    | 55830 8         | -19 <b>.</b> 2 | -51    | Q Q1         |
| -41.8 | -12                   | 13.47 |        |                 |                |        |              |
|       | 137.5                 | -250  | 137.5  | 56165.6         | -16.2          | -5.7   | 9.849999     |
| -47.5 | -13.8                 | 13.8  | 150    | 55762 1         | -15.7          | 57     | 0.76         |
| -51.4 | -15.1                 | -250  | 130    | 55762.4         | -10.7          | -5.7   | 9.70         |
|       | 162.5                 | -250  | 162.5  | 55945.6         | -22.3 -8.      | 400001 | 7.46         |
| -59.3 | -17.1                 | 14.07 |        |                 | -19.6          | -      |              |
| _59.1 | 175<br>-18.3          | -250  | 175    | 55975.9         | -19.6          | -7.3   | 7.52         |
| -30•1 | 187.5                 | -250  | 187.5  | 56016           | -20.9          | -7     | 7.53         |
| -60.6 | -22.4                 | 13.54 |        |                 |                |        |              |
|       |                       |       |        | 56129.6         | -18.7          | -6.8   | 7.54         |
| -61.1 | -20.4<br>line         | -300  |        |                 |                |        |              |
|       | -175                  | -300  | -175   | 55992           | -9.2           | 6      | 9.7          |
|       | 13                    |       |        | 00572           | <i>312</i>     | ••     |              |
| -     | -162.5                | -300  | -162.5 | 55972.9         | <b>-9.</b> 6   | -1 9   | •599999      |
|       | 17.7                  |       |        |                 | 10.7           |        |              |
| 15.6  | -150<br>19 <b>.</b> 1 | -300  | -150   | 55916.4         | -10.7          | -1.4   | 9.09         |
| -     | -137.5                | -300  | -137.5 | 55894.2         | -10.9          | -1.2   | 9.4          |
| 13.2  | 19.4                  | 12.89 |        |                 |                |        |              |
|       |                       |       |        | 55899           | -10.4          | -1.6   | 9.11         |
|       | 18 <b>.</b> 3         |       |        | 55878           | -10.1          | 9      | 9.77         |
| -     | TT7.J                 | -200  | -1140) | 53070           | -10.1          | 9      | 2.11         |

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|             | 18.4                 |                        |   |                |        |      |               |
|-------------|----------------------|------------------------|---|----------------|--------|------|---------------|
|             |                      |                        | -100                                      | 55903.1        | -10.8  | -1.1 | 9.719999      |
| 10.3        | 16.3                 | 14.12                  | _97 5                                     | 55938.4        | -11.6  | -2.5 | 0 70          |
|             | 12.9                 |                        | -07.5                                     | 22220.4        | -11.0  | -2.5 | <b>7</b> •/ 7 |
|             |                      |                        | -75                                       | 56027.6        | -12.9  | -4.1 | 10.4          |
|             | 7.4                  |                        |   | 3002/10        | 2209   |      | 2007          |
|             | -62.5                | -300                   | -62.5                                     | 56013.9        | -12.4  | -3.6 | 9.88          |
| -2.4        | <b>F</b> 4           | 12.0                   |   |                |        |      |               |
|             | -50                  | -300                   | -50                                       | 55922.4        | -11.8  | -4.1 | 9.9           |
|             | 2.6                  |                        |   |                |        |      |               |
| -           | -37.5                | -300                   | -37.5                                     | 56485.6        | -13    | -4.2 | 10            |
| -8          | .2                   | 14.97                  | 25  | 55040.2        | 11.0   | -    | 0.02          |
| 107         | -25<br>-5 <b>.</b> 6 | -300                   | -25                                       | 55942.3        | -11.8  | -5   | 9.83          |
| -12./       |                      | -300                   | -125                                      | 56051 5        | -13.8  | -63  | 10.01         |
| -20.3       | -10.1                | -300                   | -12•J                                     | 20021-2        | 13.0   | -0.5 | 10.01         |
| 20.5        | 0                    | -300                   | C   | 56252.2        | -14.1  | -5.5 | 10.3          |
| -22.7       | -11.1                | 14.34                  |   | 0010101        | 22     | 200  | 1000          |
|             | 12.5                 | -300                   | 12.5                                      | 55620.2        | -14.5  | . –5 | 10.6          |
| -19         | -11.1                | 15.62                  |   |                |        |      |               |
|             | 25                   | -300                   | 25  | 55733.2        | -15.5  | -5.6 | 10.32         |
| -22.1       | -11.7                | 16.28                  |   |                |        |      |               |
|             | 37.5                 | -300                   | 37.5                                      | 56186.7        | -14.6  | -6   | 10.22         |
| -24.8       | -10.7                | 13.52                  | 50  | <b>FFT22</b> 0 | 12.0   |      | 0.00000       |
| -25.2       |                      | -300                   | 50  | 55733.9        | -13.6  | -5.5 | 9.929999      |
| -23.2       | -12.3                | 12.94                  | 62 5                                      | 55883 3        | -13.2  | -58  | 0.82          |
| -24         | -13.6                | 1707                   |   |                |        |      |               |
| 27          |                      | -300                   | 75  | 55712.4        | -14.4  | -4.9 | 10.32         |
| -26.3       | -10.7                | 13.89                  |   | 001201         | 2.001  |      | 10052         |
|             |                      |                        |   | 56258.8        | -14.1  | -5.2 | 10.36         |
| -28.4       | 87.5<br>-12.3        | 13.55                  |   |                |        |      |               |
|             | 100                  | -300                   | 100                                       | 57613.3        | -14.7  | -4.9 | 10.25         |
| -24.2       | -12.6                | 15                     | ,<br>,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, |                |        |      |               |
|             |                      |                        |   | 55426.1        | -14    | -4.  | 7 10.27       |
| -23.8       |                      |                        |   | EECCO A        | -13.8  | E 4  | 10.39         |
| -25.8       | -12.9                |                        |   | 33000.4        | -13.0  | -5.4 | 10.39         |
| 2.3.0       | line                 |                        |   |                |        |      |               |
|             |                      |                        | -15                                       | 0 56043.7      | -9.5   |      | .6 9.58       |
| 8.9000      | 001 12               |                        |   |                |        |      |               |
| -           | -137.5               | -350                   |   | 55999.8 -9.    | 900001 | .5   | 9.71          |
|             | 12.4                 |                        |   |                |        |      |               |
|             |                      |                        | -125                                      | 56075.3        | -10.1  | •8   | 9.58          |
|             | 11.8                 |                        |   | 55000 4        |        |      | 0.84          |
|             | -112.5               | -350                   | -112.5                                    | 55882.1        | -10.7  | .1   | <b>9.7</b> 6  |
| 5.3         | 11.9<br>-100         | <b>19.4</b> 5          | _100                                      | 55873.9        | -10.2  | .6   | 9.8           |
| 5.2         | -100                 | -350<br>19 <b>.</b> 78 | -100                                      | JJ073•7        | -10•2  | 0.   | 7.0           |
| ~~ <b>~</b> | -87.5                |                        | -87.5                                     | 55881.4        | -11.2  | 5    | 9.83          |
| 2.5         | 9.400001             |                        |   |                | 1.2.°2 | •••  | 2000          |
|             | -75                  |                        | -75                                       | 55888.7        | -11.3  | -1.1 | 9.88          |
| -1.5        | 5.9                  | 20.33                  |   |                |        |      |               |

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|                |                       |                        | -62.5      | 56539.4          | -11.6 | -2.3    | <b>9.7</b> 6          |
|----------------|-----------------------|------------------------|------------|------------------|-------|---------|-----------------------|
| -5.6           |                       | -350                   | -50        | 56350.8          | -12.8 | -3.4    | 9.77                  |
|                | 1.4<br>-37.5          |                        | -37.5      | 56134.4          | -13.3 | -3.6    | <b>9.</b> 86          |
| -10.6          | 3                     | 19 <b>.</b> 84<br>-350 | 25         | 5(100            | 14.0  | -4.8    | 9.87                  |
| -14.2          | -2.5                  |                        |            | 56129            | -14.8 | -4.0    | 9.07                  |
| -15 <b>.</b> 9 | -12.5                 | -350<br>18.9           |            | 56301.7          | -14.1 | -4.9    | 9.92                  |
|                | 0                     | -350                   |            | 55813.1          | -14.1 | -4.5    | 9.969999              |
| -15.3          | - <b>4.</b> 8<br>12.5 |                        | 12.5       | 56016.5          | -14.7 | -3.7    | 9.79                  |
| -19.2          | -4.8                  | 18.15                  |            |                  |       |         |                       |
| -20.3          |                       | -350<br>17.6           | 25         | 56100            | -13.5 | -4.3    | <b>9.7</b> 3          |
|                | 37.5                  | -350<br>17.23          | 37.5       | 56982            | -13.7 | -4.2    | 9.59                  |
| -21.8          | 50                    | -350                   | 50         | 56537.3          | -14.6 | -4.3    | 9.92                  |
| -21.3          |                       | 17.33                  |            | 55001            | 107   |         | 0.00                  |
| -20.5          | 62 <b>.</b> 5<br>6.2  |                        | 62.5       | 55891            | -13.7 | -4      | 9.82                  |
|                | <b>7</b> 5            | -350                   | <b>7</b> 5 | 55604            | -15   | -4      | 10.01                 |
| -22.7          | -6.2<br>87.5          |                        |            | 55400.4          | -13.9 | -4.1    | 10.03                 |
| -24.9          | -6.2                  | 16,97                  |            |                  |       |         | 10.03                 |
| 247            | 100<br>-7.2           | -350<br>16.65          | 100        | 55725.6          | -14.6 | -4.1    | 10.14                 |
|                | -/.2<br>line          | -400                   |            |                  |       |         |                       |
|                | -150<br>13.8          | -400                   | -150       | 55843.3          | -8.6  | .7      | 9.54                  |
|                | 13.8<br>137.5         | 19.21<br>-400          | -1375      | 55831.9          | -9.7  | .5      | 9.37                  |
|                |                       | 19.53                  |            |                  | - 3•1 | ູ       | 201                   |
|                | -125                  |                        | -125       | 55864.1          | -9.5  | 2       | 9.42                  |
| 4.9            | 12.5<br>112.5         | 19.61                  | -1125      | 55989.8          | -9.7  | 3       | 9.36                  |
|                |                       | -400<br>19 <b>.</b> 51 | -112.5     | 22303-0          | -9.7  |         | 9.30                  |
| 115            | -100                  | -400                   |            | 55996 <b>.</b> 5 | -11.1 | 7       | 9.52                  |
| 2.8            | 12.2                  | 19.83                  |            |                  |       | •       |                       |
| c              | -87.5                 |                        | -87.5      | 56291.5          | -11.6 | -1.4    | 9.52                  |
| 6              | 10<br>-75             | 19.71<br>-400          | -75        | 56274.2          | -12.2 | -1.5    | 9.45                  |
| 7              | 10.1                  | 20.02                  | -75        | 50274.2          | -17•2 | -1•1    | <b>J</b> • <b>4</b> J |
| • *            | -62.5                 | -400                   | -62.5      | 56063.8          | -11.7 | -1.9 9. | 599999                |
| -2.8           | 7.8                   | 20.11                  |            |                  |       |         |                       |
|                | -50                   | -400                   | -50        | 55998.4          | -12.1 | -3.4    | 9.65                  |
| -7.5           | 3.9<br>-37.5          | 21.3<br>-400           | -37.5      | 55953.4          | -12.8 | -3.5    | 10.19                 |
| -10.9          |                       | 26.23                  |            |                  |       | 010     |                       |
|                | -25                   | -400                   |            | 55949.2          | -14   | -3.5    | 10.64                 |
| -14.5          | -1.1<br>-12.5         | 29 <b>.</b> 22<br>-400 | -12.5      | 56025.3          | -13   | -3.9    | 10.76                 |
| -15.1          |                       | 29.42                  |            |                  |       |         |                       |
|                | 0                     | -400                   | C          | 56031            | -13.7 | -4.3    | 10.97                 |

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| -16.6 | -2.6                  | 29.49                  |              |                 |       |             |               |
|-------|-----------------------|------------------------|--------------|-----------------|-------|-------------|---------------|
|       |                       |                        | 12.5         | 56107           | -14.9 | -4.5        | 11.01         |
| -17.7 | -2.8                  |                        |              |                 |       |             |               |
|       | 25                    |                        |              | 56249.9         | -14.5 | -4.7        | 11.11         |
| -19.5 | -3.5                  |                        |              | 5(10)           | 15.5  |             |               |
| -21.9 | 37.5<br>-3.6          |                        |              | 56181           | -15.5 | -4.3        | 11.13         |
| -21.0 | 50                    | <b>-40</b> 0           | 50           | 56172.1         | -15.6 | -3.8        | 11.13         |
| -22.2 | -4.3                  | 28.12                  |              |                 |       |             | 11110         |
|       | 62.5                  | -400                   | 62.5         | 56388 <b>.7</b> | -15.9 | -4          | 11.11         |
|       | -4.5                  |                        |              |                 |       |             |               |
|       | line                  |                        | 175          | 5501 A 7        | -8.3  | 24          | 0.15          |
|       | -175                  |                        | -175         | 55614.7         | -0.3  | 3.4         | 9.15          |
|       |                       |                        | -162.5       | 55791.9         | -8.1  | 3.2         | 9.22          |
| 7.9   | 13.4                  | 23.11                  |              |                 |       |             |               |
|       | -150                  | -450                   | -150         | 55792.8         | -8.1  | 4.2 9.0     | 99999         |
| 6.9   | 13.7                  | 23.34                  |              |                 |       |             |               |
|       | 137.5                 | -450 -                 | -137.5       | 55798.3         | -9    | 2.9         | 9.21          |
| 5./   | 12 <b>.7</b><br>-125  | 23.6                   | _125         | 55800           | -9.1  | .9          | 0.10          |
| 4.8   | 11.2                  | 23.8                   | -125         | 55633           | -9.1  | •9          | 9.19          |
|       | -112.5                |                        | -112.5       | 55863.3         | -9.8  | 1.7 9.30    | 9999          |
| 3.2   | 10.7                  | 23.85                  |              |                 |       |             |               |
|       | -100                  | -450                   | -100         | 56303           | -9.7  | .7          | 9.3           |
| 2.4   | 9.8                   | 24.21                  |              |                 |       |             |               |
|       | -87.5                 |                        |              | 56684.5         | -10.3 | 1 9.46      | 59999         |
| . •3  | <b>8.400001</b>       | 24.66                  | 75           | 56100 1         | -11   | 0           | 0.46          |
| -1.5  |                       | -430<br>24 <b>.</b> 75 |              | 50155.1         | -11   | 0           | 9.40          |
|       | -62.5                 |                        |              | 56197.1         | -11.7 | -1.7        | 9.66          |
| -3.6  | 5.7                   | 25.06                  |              |                 |       |             |               |
|       | -50                   | -450                   | -50          | 55939.3         | -11.7 | -1.9        | 9 <b>.7</b> 1 |
| -6.5  | 2.7                   | 25.44                  | 0 <b>7</b> F | 55000           |       |             |               |
| -8.2  | -37.5                 | -450<br>25 <b>.</b> 36 | -37.5        | 22282           | -12.4 | -1.8        | 9.71          |
| 0.2   | -25                   | -450                   | -25          | 55970           | -12.6 | -2          | <b>9.7</b> 6  |
| -11.2 |                       | 25.63                  |              |                 |       | -           | 5070          |
|       | -12.5                 | -450                   | -12.5        | 55892.7         | -13.6 | -2.1        | 9.88          |
| -13   | -2.4                  | 26.43                  |              |                 | _     |             |               |
| 14.0  | 0                     | -450                   |              | 55985.1         | -12.8 | -3.8        | 10.04         |
| -14.9 | -2.7<br>12.5          | 26 <b>.</b> 78<br>-450 | 12.5         | 56104.4         | -14.7 | -3          | 10.2          |
| -17.1 |                       |                        |              | 20104.4         | -14./ | -3          | 10.2          |
|       | 25                    | -450                   | 25           | 56250.6         | -14.2 | -3.2        | 10.37         |
| -18.5 |                       |                        |              |                 |       |             |               |
|       | 37.5                  | -450                   | 37.5         | 56628.5         | -15.3 | -3.7        | 10.32         |
| -19.4 |                       |                        |              |                 |       |             |               |
| -21.7 | 50                    | -450                   | 50           | 56621.1         | -15.2 | -3.9        | 10.42         |
| -21./ | - <b>4.</b> 2<br>62.5 | 27 <b>.</b> 93<br>-450 | 62.5         | 56799.9         | -15.6 | -4.6        | 10.54         |
| -21.6 |                       |                        |              | 5512362         | -13.0 | <b>4.</b> U | TA*14         |
|       | 75                    | -450                   | <b>7</b> 5   | 56464.2         | -16.4 | -4.9        | 10.59         |
| -24.1 | -8.1                  | 28.36                  |              |                 |       |             |               |

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| line              | -500          |            |           |             |         |              |
|-------------------|---------------|------------|-----------|-------------|---------|--------------|
| -175              |               | -175       | 55802.5   | -9.6        | .7      | 8.99         |
|                   | 22.37         | 175        | 33002.5   | 2.0         | • /     | 0.75         |
| -162.5            |               | -162.5     | 55777.5   | -9.6        | 1.5     | <b>8.9</b> 6 |
|                   | 22.51         | 102.0      | 501110    | 200         | 100     | 0150         |
| -150              | -500          | -150       | 55761.1   | -9.3        | .9      | 9.05         |
| 4.3 12            | 22.41         |            |           |             |         |              |
| -137.5            |               |            | 55744.9   | -10.6       | 0       | 8.88         |
| 2.1 11.4          | 22.45         |            |           |             |         |              |
| -125              | -500          | -125       | 55750.4   | -11.2       | 5 8     | 3.8899999    |
| 1.1 11.3          | 22.26         |            |           |             |         |              |
|                   |               | -112.5     | 56294.6   | -10.9       | -1.8    | 8.97         |
| .3 11.2           | 22.08         |            |           |             |         |              |
|                   |               | -100       | 55876.4   | -10.7       | -1.2    | 8.79         |
| 2 10.6            |               |            |           |             |         |              |
|                   |               |            | 55914.1   | -11.7       | -1.5    | 8.9          |
| -1.6 9.900001     |               |            |           |             |         |              |
|                   |               |            | 56573.5   | -13.6       | -2.3 8  | 3.639999     |
| -3.5 9            |               |            | 5 ( ADD 5 | 10.6        |         | 0.01         |
| -62.5             |               |            | 56433.5   | -12.6       | -3.4    | 8.91         |
| -4.5 7.8          | 21.67         | 50         |           | -13         | 2.2     | 0.01         |
|                   |               |            | 20244.0   | -13         | -2.2    | 8.91         |
| -5.7 6.4<br>-37.5 |               |            | 56220     | -13.5       |         | 0,00000      |
| -37.5             |               |            | 30220     | -13.5       | -4 (    | 3.8899999    |
|                   |               | -25        | 55868 1   | -13.9       | -4.4    | 8.99         |
|                   | 21.69         |            | 33000•1   | 13.5        | -4.4    | 0.99         |
| -12.5             |               |            | 55807.2   | -17.2       | -6.1    | 7.54         |
|                   | 21.3          |            | 3300742   | 17.2        | 0.1     | 7.54         |
| 0                 | -500          |            | 55815.8   | -18         | -5.8    | 7.94         |
|                   | 21.9          |            |           | 20          | 010     |              |
| 12.5              | -500          | 12.5       | 55930.5   | -19.4       | -6.3    | 7.84         |
| -16.7 -1.6        | 21.           | 7          |           |             |         |              |
| 25                | -500          | 25         | 55901.6   | -19.1       | -3.2    | 8.679999     |
| -18.1 -3.6        | 21.6          | 8          |           |             |         |              |
| 37.5              |               |            | 55978.4   | -20         | -6.8    | 7.57         |
| -21.4 -4.5        |               | 4          |           |             |         |              |
| 50                | -500          | 50         | 56093.1   | -21.4       | -6.9    | 7.64         |
|                   | 21.           |            |           |             | _       |              |
|                   | -500          |            | 56322.6   | -21.2       | -9      | 7.58         |
|                   | 21.2          | 1 75       |           | 22.6        | 000001  | 7.00         |
| 75                | -500          | <u>ح</u> ر | 26324.2   | -22.6 -8    | .900001 | 7.96         |
| -27.6 -8<br>87.5  | 20 <b>.</b> 8 |            | 55746 0   | <b>22 2</b> | -9.8    | 7.8          |
| -29.3 -8.8        | -200<br>20 8  | 2          | 33740.3   | -22.3       | -9.0    | 7.0          |
| line              | -550          | 2          |           |             |         |              |
| -175              | -550          | -175       | 55768.5   | -9.7        | 4.1     | 7.31         |
| 11.8 15.3         | 21.21         |            |           | 5.7         | 741     | /            |
| -162.5            |               |            | 55779.4   | -9.6        | 3       | 7.28         |
| 9.5 13.2          | 21.9          |            | •         |             | -       |              |
| -150              |               |            | 55787.4   | -10.5       | 2.9     | 7.39         |
| 7.8 12.3          | 22.45         |            |           |             |         | -1           |
| -137.5            |               |            | 55821.8   | -10.3       | 3.1     | 7.69         |
| 5.7 12            | 23.19         |            |           |             |         |              |

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| 5.7      | -125         |                       |          | 55829.5 - | 9.400001 | 2.5   | <b>7.7</b> 2 |
|----------|--------------|-----------------------|----------|-----------|----------|-------|--------------|
|          |              | 23 <b>.</b> 7<br>-550 |          | 55939.1   | -10.4    | 1.8   | 7.77         |
| 2.2      | 10.1         | 23.57                 |          |           |          |       |              |
|          | -100         | -550                  | -100     | 55986.2   | -11      | 2.1   | 7.78         |
| .7       |              | 23.82                 |          |           |          |       |              |
|          | -87.5        |                       | -87.5    | 55985.9   | -11.6    | 1     | 7.73         |
| 0        | 9.400001     | 23.8                  |          |           |          |       |              |
|          | -75          |                       | -75      | 55889.8   | -10.9    | 1     | <b>7.9</b> 3 |
| -1.4     | 7.8          | 24.03                 |          |           |          |       |              |
| <u> </u> | -62.5        | -550                  | -62.5    | 56533.2   | -10      | -1.2  | 7.9          |
| -2.5     | 7.1          | 23.87                 |          |           |          |       |              |
|          | -50          | -550                  | -50      | 56170.8   | -13.2    | -1.3  | 7.82         |
| -4.8     | 5.8          | 23.8                  |          |           |          |       |              |
| 6.0      | -37.5        | -550                  | -37.5    | 56399.6   | -12.5    | -2.9  | 7.7          |
| -6.3     | 2.9          | 23.77                 | 05       |           |          |       |              |
| -9       | -25          | -550                  | -25      | 56099.5   | -14.9    | -3.3  | 7.63         |
| -9       | 13           | 23.58                 | 105      |           |          |       |              |
| 10.7     | -12.5 0      | -220                  | -12.5    | 55754.9   | -14      | -2.7  | 8.37         |
| -10.7    | <u>n</u>     | - 660                 | <b>^</b> | 66763 1   | -15.6    | ()    |              |
| -12.9    | 0<br>2 _ 2 5 | -000                  | 0        | 22123.1   | -16.7    | -0.2  | 7.77         |
| -12.5    | 12.5         | -550                  | 125      | 55776 2   | 167      | 4.0   | 7.0          |
| -15      | -36          | -330                  | 12.5     | 55770-5   | -10.7    | -4.9  | 7.8          |
| 15       | -3.0<br>25   | -550                  | 25       | 55719 2   | -17.6    | -65   | 7 07         |
| -16.4    | 1 -5         | 23.97                 | 23       | 55710.2   | -17.0    | -0.5  | 7.02         |
| 10.7     | 37.5         |                       |          | 55711 /   | -17.8    | -7    | 8.04         |
| -18.2    |              | 24 (2                 |          |           |          | - /   | 0.04         |
| 1001     | 50           | -550                  | 50       | 55803.5   | -19.6    | -8.1  | 7.96         |
| -21      |              | 24.66                 |          | 55005.5   | 1.7.0    | 0.1   | 7.90         |
|          |              |                       |          | 55952.3   | -20.6    | -9.1  | 8.24         |
| -25.4    | -10          | 24.31                 | 0240     | 0070210   | 2010     | 2.1   | 0.24         |
|          | 75           | -550                  | 75       | 56065-2   | -22.3    | -8-5  | 8.04         |
| -27.8    | 3 -10.4      | 23.95                 |          |           |          | 0.0   |              |
|          | 87.5         | -550                  |          | 56365.6   | -20.1    | -10.2 | 7.8          |
| -30.2    | 2 -12.6      | 22.22                 |          |           |          |       | -            |

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## APPENDIX E

## **GEOPHYSICAL EQUIPMENT SPECIFICATIONS**

| Specifications*  |
|--|
| Frequency Tuning Range   |
| Transmitting Stations Measured Up to 3 stations can be automatically measured at any given grid location within frequency tuning range   |
| Recorded VLF Magnetic<br>Parameters  |
| Standard Memory Capacity 800 combined VLF magnetic and VLF electric<br>measurements as well as gradiometer and<br>magnetometer readings  |
| Display  |
| RS232C Serial I/O Interface  |
| Test ModeA. Diagnostic Testing (data and programmable memory)<br>B. Self Test (hardware)   |
| Sensor Head Contains 3 orthogonally mounted coils with automatic tilt compensation   |
| Operating Environmental<br>Range   |
| Power Supply   |
| Weights and Dimensions<br>Instrument Console2.8 kg, 128 x 150 x 250 mmSensor Head2.1 kg, 130 dia. x 130 mmVLF Electronics Module1.1 kg, 40 x 150 x 250 mmLead Acid Battery Cartridge1.8 kg, 235 x 105 x 90 mmLead Acid Battery Belt1.8 kg, 540 x 100 x 40 mmDisposable Battery Belt1.2 kg, 540 x 100 x 40 mm |
| *Preliminary   |

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EDA Instruments Inc., 4 Thorncliffe Park Drive, Toronto, Ontario Canada M4H 1H1 Telex: 06 23222 EDA TOR. Cables: Instruments Toro (416) 425-7800

In USA, EDA Instruments Inc., 5151 Ward Road, Wheat Ridge, Colorado U.S.A. 80033 (303) 422-9112

Printed In Canada

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| <u>+++++++++++++++++++++++++++++++++++++</u>                        |  |  |
|   |  |  |
| Specifications  |  |  |
| Dynamic Range   | 18,000 to 110,000 gammas. Roll-over display feature<br>suppresses first significant digit upon exceeding 100,000<br>gammas.                      |  |
| Tuning Method   | Tuning value is calculated accurately utilizing a specially developed tuning algorithm   |  |
|   | <ul> <li>± 15% relative to ambient field strength of last stored value</li> </ul>  |  |
| Display Resolution  |  |  |
| Processing Sensitivity<br>Statistical Error Resolution              |  |  |
| Absolute Accuracy   | + 1 gamma at 50,000 gammas at 23°C   |  |
|   | ± 2 gamma over total temperature range   |  |
| Standard Memory Capacity<br>Total Field or Gradient                 | , 1,200 data blocks or sets of readings  |  |
| Tie-Line Points<br>Base Station                                     | 100 data blocks or sets of readings  |  |
| Display   | Custom-designed, ruggedized liquid crystal display with an   |  |
|   | operating temperature range from -40°C to +55°C. The display contains six numeric digits, decimal point, battery                                 |  |
|   | status monitor, signal decay rate and signal amplitude<br>monitor and function descriptors.  |  |
| RS 232 Serial I/O Interface   |  |  |
| Gradient Tolerance  | <ul> <li>6,000 gammas per meter (field proven)</li> <li>A. Diagnostic testing (data and programmable memory)</li> </ul>                          |  |
|   | B. Self Test (hardware)  |  |
|   | Optimized miniature design. Magnetic cleanliness is consistent with the specified absolute accuracy.   |  |
|   | 0.5 meter sensor separation (standard), normalized to gammas/meter. Optional 1.0 meter sensor separation available. Horizontal sensors optional. |  |
|   | Remains flexible in temperature range specified, includes strain-relief connector  |  |
|   | Programmable from 5 seconds up to 60 minutes in 1 second increments  |  |
|   | <ul> <li>-40°C to +55°C; 0-100% relative humidity; weatherproof</li> <li>Non-magnetic rechargeable sealed lead-acid battery</li> </ul>           |  |
|   | cartridge or belt; rechargeable NiCad or Disposable battery<br>cartridge or belt; or 12V DC power source option for base<br>station operation.   |  |
| Battery Cartridge/Belt Ufe  | 2,000 to 5,000 readings, for sealed lead acid power supply, depending upon ambient temperature and rate of                                       |  |
| Weights and Dimensions  | readings   |  |
| Instrument Console Only   |  |  |
| NiCad or Alkaline Battery Cartridge                                 |  |  |
| NiCad or Alkaline Battery Belt                                      |  |  |
| Lead-Acid Battery Belt  | _ 1.8 kg, 540 x 100 x 40mm   |  |
| Sensor  | 1.2 kg, 56mm diameter x 200mm  | E D A Instruments Inc.   |
| Gradient Sensor<br>10.5 m separation - standard)<br>Gradient Sensor | . 2.1 kg, 56mm diameter x 790mm  | 4 Thorncliffe Park Drive<br>Toronto, Ontario<br>Canada M4H 1H1           |
| (1.0 m separation - optional)                                       | . 2.2 kg, 56mm diameter x 1300mm   | Telex: 06 23222 EDA TOR<br>Cable: Instruments Toron: 0<br>(416) 425 7800 |
| standard System Complement  | Instrument console; sensor; 3-meter cable, aluminum<br>sectional sensor staff, power supply, harness assembly,                                   | (416) 425 7800<br>In U.S.A.  |
|   | operations manual.   | E D A Instruments inc<br>S1S1 Ward Road                                  |
| Base Station Option   | Standard system plus 30 meter cable<br>Standard system plus 0.5 meter sensor   | Wheat Ridge Colorado<br>U.S.A. 80033                                     |
|   | - Server o starcus high 0.5 merce seriadi  | 1 (3()3) 472 9112  |

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### APPENDIX F

### PETROGRAPHIC ANALYSIS REPORTS

1983, 1991

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LODE RESUVELE CORP.

Vancouver Petrographics

JAMES VINNELL. Manager JOHN G. PAYNE. Ph. D. Geologist

Report for: Gordon House, Sawyer Consultants Inc., 675 W Hastings, #1201 VANCOUVER, B.C., V6B 1N2

P.O. BOX 39 8887 NASH STREET FORT LANGLEY, B.C. VOX LIO

PHONE (604) 888-1323 Invoice 4215

Sample: Lode Middle Vein Porphyry (Porphyritic Andesite dike in Sicker Gp.

The sample contains phenocrysts of plagioclase and hornblende and inclusions of plagioclase aggregates in a very fine grained groundmass dominated by plagioclase with lesser chlorite and Ti-oxides. Late patches possibly filling cavities, are dominated by calcite.

phenocrysts

- tract

| phenocryses  |                    |
|--------------|--------------------|
| plagioclase  | 7-8%               |
| hornblende   | 5- 7               |
| inclusions   |                    |
| diorite(?)   | 3-4                |
| groundmass   |                    |
| plagioclase  | 60-65              |
| calcite      | 7-10               |
| chlorite     | 5-7                |
| leucoxene    | $1 - 1\frac{1}{2}$ |
| opaque       | 0.3                |
| apatite      | 0.3                |
| late patches |                    |
| calcite      | 2-3                |
| plagioclase  | 0.2                |
| sericite     | minor              |
| chlorite     | minor              |
|              |                    |

Plagioclase forms subhedral to euhedral phenocrysts averaging 0.5-1 mm in size, with a few up to 1.5 mm long. Most are equant to prismatic in outline. Alteration is moderate to locally strong to extremely fine grained sericite flakes and patches of extremely fine to very fine grained calcite. Calcite distribution is more variable than that of sericite, but the overall abundances of both alteration minerals are about the same.

The inclusion? may be an early formed glomeroporphyroblastic aggregate of plagioclase averaging 1-1.5 mm in size. Grains show similar alteration to that of plagioclase phenocrysts. The patch contains scattered aggregates of muscovite up to 0.2 mm long, a few patches of interstitial, fine grained more-sodic plagioclase (relatively fresh), and minor disseminated semiopaqu (Ti-oxide).

Hornblende forms elongate prismatic to acicular phenocrysts averaging 1 mm in length, with a few up to 3.5 mm in length. The mineral is completel altered to aggregates of very fine grained chlorite and patches of very fine to fine grained calcite. Chlorite is pale green with brown and blue interference colors. Some grains contain clusters of orangish Ti-oxide, possibly after primary sphene. One cluster up to 3 mm across consists of an aggregate of hornblende phenocrysts, altered to chlorite, Ti-oxide, and calcite.

The groundmass is dominated by anhedral, interlocking grains of plagic clase averaging 0.05-0.1 mm in size. Lathy plagioclase grains of similar size are present in minor amounts. Alteration is to sericite and calcite as in the phenocrysts, but the intensity appears to be moderately less. (continued)

#### LMVP (page 2)

As well as alteration of phenocrysts, calcite forms irregular patches throughout the groundmass. These are in part alteration of groundmass, and possibly in part late patches (see below).

Chlorite forms irregular interstitial patches of very fine grained aggregates intergrown with groundmass plagioclase.

Leucoxene (almost opaque, medium brown Ti-oxide) occurs as irregular disseminated patches from 0.02-0.3 mm in size. Much of it may be after original ilmenite.

Opaque, possibly ilmenite or hematite, occurs in subhedral to irregul patches averaging 0.02-0.05 mm in size, with a few irregular patches up to 0.3 mm across.

Apatite forms scattered subhedral to euhedral grains from 0.1-0.15 mm in average size. In places it is concentrated with hornblende phenocrysts.

The rock contains a few well-defined, late patches up to a few mm long, dominated by fine to medium grained calcite. This forms slightly interlocking aggregates, in part with moderately abundant dusty inclusions of opaque. Plagioclase forms scattered grains and aggregates, commonly nea the borders of patches. A few unusual aggregates up to 0.15 mm in size consist of radiating clusters of extremely fine grained sericite grading outwards to a rim of chlorite. A few other sericite aggregates occur withi plagioclase grains.

film Glay.e John G. Payne,

John G. Payhe, November 1983

This sample we taken by Mr. G. House from the main workings of the Middle Verry, Mt. Mc Quillan, Vanc. 186., (due east from H.G. vern, on the lower flat), sample from parhyry dike (which contains the mineralzed quests versh)), in the creek bid. Dike rock appears to be timiler to Tertiary sills and dikes (Catfine Intrusions) in budy Vanaimo sediments, et al, in the area.



# Vancouver Petrographics Ltd.

JAMES VINNELL, Manager JOHN G. PAYNE, Ph.D. Geologist CRAIG LEITCH, Ph.D. Geologist JEFF HARRIS, Ph.D. Geologist KEN E. NORTHCOTE, Ph.D. Geologist

> Report for: Fayz Yacoub, Hi Tech Resources, 1500-609 Granville St., Vancouver, B.C.

P.O. BOX 39 8080 GLOVER ROAD, FORT LANGLEY, B.C. VOX 1J0 PHONE (604) 888-1323 FAX. (604) 888-3642

Job 204

July 5th, 1991

SAMPLES:

3 rock samples, numbered MV/91 TH-1, 2 and 3 from the Middle Vein project, for sectioning and petrographic examination.

SUMMARY:

These samples are igneous rocks of hypabyssal intrusive aspect. They are generally fresh, and show no evidence of deformation, veining etc.

TH-1 is a fine-grained, non-porphyritic, meshwork-textured rock of andesitic composition. It is made up essentially of plagioclase and chlorite with accessory quartz and opaques.

TH-2 is a fine to medium-grained gabbro composed essentially of an intergrowth of plagioclase and pyroxene. Most of the plagioclase shows strong, even saussuritization, but there is also a late phase which is clear and unaltered. The pyroxene is generally fresh. It shows incipient late-magmatic modification to hornblende - which also occurs as an interstitial accessory component. The rock is notably low in opaques.

TH-3 is a typical quartz-feldspar porphyry, of dacitic composition. It is composed of phenocrysts of plagioclase and quartz (and minor altered mafics) in a microgranular groundmass of fresh plagioclase with minor intergrown quartz and chlorite The plagioclase phenocrysts show mild pervasive epidotization.

Individual petrographic descriptions are attached.

/J.F. Harris Ph.D. (929-5867)

ANDESITE

Estimated mode

Plagioclase66Quartz5Chlorite22Carbonate3Opaques4

This is a fine-grained, non-porphyritic rock, having the textural aspect of a dyke.

It is composed predominantly of plagioclase as an even, interlocking, meshwork aggregate of blocky to elongate prismatic grains, 0.05 - 0.4mm in size. The plagioclase is strikingly fresh.

Quartz is a minor accessory, as sporadic grains of similar size to the plagioclase, sometimes aggregating as clumps. It also forms a few irregular cross-cutting veinlets.

The other principal constituent is chlorite. This forms an intimately intergrown, felted-textured, interstitial phase throughout the plagioclase aggregate. It presumably represents a totally altered primary mafic component.

Opaque and sub-opaque granules, 10 - 50 microns in size, sometimes forming skeletal clusters, occur more or less abundantly, in close association with the chlorite. These are probably mainly rutile and Fe-Ti oxides, but may include a proportion of very fine-grained sulfides.

Carbonate is a minor deuteric or alteration phase, as sporadic flecks and interstitial pockets. It also occurs intergrown with one of the guartz veinlets.

#### SAMPLE MN/91 TH-2

GABBRO

Estimated mode

Saussurite 45 Plagioclase 6 Pyroxene 38 Hornblende 6 Chlorite 5 Opaques trace

This rock has a grain size range of 0.2 - 4.0mm, and shows a fine to medium-grained, hypidiomorphic granular texture of typical intrusive aspect.

The cut-off block shows the typical speckled fabric of a gabbro, consisting of intergrown dark mafics and white-etched plagioclase.

The thin section shows that the principal mafic is clinopyroxene. This forms discrete, rather coarse, subhedral grains, fresh but for minor late magmatic modification to flecks of amphibole. A few pyroxene grains appear to have been converted almost totally to fibrous, secondary-type amphibole.

The accessory mafic is brownish hornblende, as an interstitial network in partial rimming relationship to the pyroxenes.

The majority of the plagioclase in this rock shows strong saussuritization in the form of even, virtually complete alteration to turbid, brownish, sub-opaque material. This forms clusters of blocky, subhedral-prismatic grains, alternating with the mafics, and corresponding with the white-etched areas of the cut-off block.

A small proportion of clear, unaltered, well-twinned plagioclase exists, as tiny individuals and small pockets, and as partial rims and overgrowths on the totally saussuritized material. The latter was apparently an early-formed component, and the clear plagioclase a late interstitial phase.

Chlorite is the remaining accessory - as sporadic, irregular, felted-textured pockets. This presumably represents deuteric alteration of some primary mafic component.

Opaques (oxides or sulfides) are extremely minor, and the rock is also distinguished by a notable lack of such typical accessories as apatite and sphene. Estimated mode

Phenocrysts

| Plagioclase | 21    |
|-------------|-------|
| Quartz      | 15    |
| Chlorite)   | 4     |
| Epidote)    | -1    |
| Groundmass  |       |
| Plagioclase | 50    |
| Quartz      | 6     |
| Chlorite    | 4     |
| Rutile      | trace |

This is a leucocratic rock made up of phenocrysts of quartz and plagioclase in an even, microgranular groundmass composed predominantly of plagioclase.

The phenocrysts range in size from 0.2 - 4.0mm. The plagioclase is subhedral-euhedral in form, and commonly occurs as clumps. It is generally fresh, except for minor alteration to flecks of epidote.

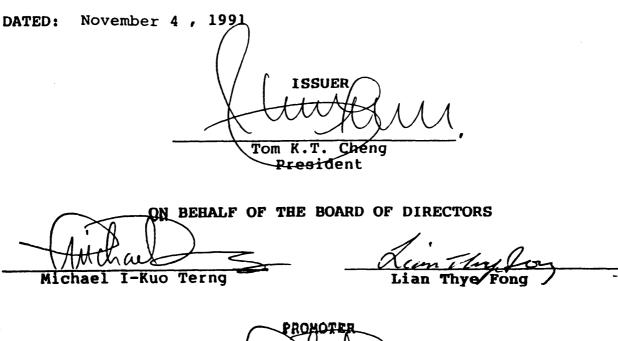
The quartz ranges from anhedral to subhedral in form, and sometimes shows embayed outlines and groundmass inclusions. The quartz phenocrysts tend to be larger than the plagioclase. Minor mafic phenocrysts are now totally altered, and are represented by irregular clumps of felted chlorite and cryptocrystalline to granular epidote.

The phenocrysts are set, with random orientation, in an equigranular groundmass of grain size 20 - 100 microns, composed essentially of an interlocking mosaic aggregate of fresh, anhedral plagioclase. Indeterminate (but apparently minor) proportions of quartz occur sporadically intergrown, and there are scattered intergranular pockets of chlorite, and flecks of cryptocrystalline rutile.

This rock is a typical quartz feldspar porphyry, of dacitic composition. It has the texture of a hypabyssal intrusive. It is notably fresh (except for alteration of the minor mafics).

#### CERTIFICATES

The foregoing constitutes full, true and plain disclosure of all material facts relating to the securities offered by this Prospectus as required by the Securities Act and its regulations.



Michael I-Kuo Terng

#### AGENT

To the best of our knowledge, information and belief, the foregoing constitutes full, true and plain disclosure of all material facts relating to the securities offered by this Prospectus as required by the Securities Act and its regulations.

DATED: November 4, 1991

BRINK HUDSON & LEFEVER LTD. Per: Brian D. Graves, President.

John L. Mathers, Vice-President.