

Great Northern vein system

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FILED UNDER
 82KNW030

003892

PROPERTY FILE

List of drawings

- Fig. α - Great Northern sub-area: 1" = 100'
- " β - Sketch^{plan} of major faults & fault blocks.
- " γ - Composite geological plan of Broadview adv.
1" = 40'.
- " δ - True Fissure - Blue Bell vein outcrops;
1" = 40'
- " ϵ - True Fissure & Blue Bell mines - composite
surface & underground plan of vein; 1" = 40'.
- Sec. AA' through Broadview Nos. 1 & 2 levels; 1" = 40'
- " DD' " True Fissure " 2, 3, & 4 " & north
raise 2 \leftarrow 3; 1" = 40'.
- " EE' through lower Blue Bell ~~drift~~^{drift} & cut
south of True Fissure Creek; 1" = 40'.
- " FF' through south end upper Blue Bell drift,
1" = 40'.
- " GG' through Blue Bell raise; 1" = 40'

Plot on 100-scale

~~Bdvw shaft & ck for Tremline plan~~ ✓

~~TF new face for reduc.~~ ✓

~~o/c nr Δ 38~~ ✓

Data for Keele's Bdvw map

see Edwards re G.N. drains.

TF composite level plan ✓

Sections

~~Blue Bell - St. Elms? - 2023~~

Samples arranged ✓

work on insite

TS

F. A. replottng for final

over

.00,000 05
1,

Secide

o/c on Fig. α?

to-ords?

no. of secs?

name? - sub-area, vein system area?

Keele's assays (old, & new T.F. to. now defunct).

claims or claim reg?

weather fine, hot

TRUE FISSURE, 19-8-57

GN 1

Radman's Eastwood
lost (many) grooves

lying in adits and continuing
around the establishment.

Sta	FS on Sta	BS on Sta	H.I.	RI	V \angle	H.P.	ΔE	Final ΔE	H.D. hor. distance	elev. of pt.	comments & witnesses
$\Delta 17$ (5183 @)	01		4'	3.7 ^{hh}	+12° 55'	1.3	+174'	+176.7'	710'	5260.5	mouth of Bluebell #2 adit
	02		"	3.3 ^{hh}	+12° 20'	0	+140'	+136.3'	631'	5320.3	in middle of top of tunnel
	03		"	3.1 ^{hh}	+10° 37'	3.0	+114'	+115'	600'	3290.9	on camp creek
	04		"	2.3 ^{hh}	+7° 57'	4.0	+39 $\frac{1}{2}$ '	+39 $\frac{1}{2}$ '	451'	5223.3	near side of dump on adit
	05			2.25 ^{wh}	-0° 20'	8.0	-1.3'	-5.3'	225'	5178.5	mouth, on near side of Bluebell #2 adit
LUNCH											
	A2		4'	1.81 ^{wh}	-12° 58'	3.4	-17.2'	-16.6'	78'	5167.2	sta. on surface side of road on bank of pt. 5 ca.
	06		"	2.8 ^{wh}	+20° 32'	5.5	+91.5'	+93'	249'	5276.2	on hillside 250' SW of #2
	07		"	1.9 ^{hh}	+21° 37'	8	+128'	+124'	330'	5307.8	above pt. 6 on bank
	08 ^h		"	3.00 ^{hh}	+8° 22'	6'	+96'	+94'	590'	5277.8	edge of pit of Bluebell #2
	09		"	3.7 ^{hh}	+16° 50'	5'	+207'	+206'	678'	5329.8	edge of vein take place
	010 ^h		"	2.9 ^{hh}	+10° 55'	9'	+85.5'	+83.5'	468'	5267.3	on bank 'contour' E of pt.
	011		"	4.4 ^{hh}	+14° 37'	5'	+212'	+211'	817'	5394.8	pts. in lower (big) on under 20' to 30' from
	012 ^h		"	1.075 ^{wh}	+16° 03'	3'	+113'	+114'	401'	5297.8	blow continued E of pt.
	013 ^h		"	2.9 ^{wh}	+11° 26'	7'	+56'	+53'	250'	5236.3	blow continues E
	014 ^h		"	1.85 ^{wh}	+0° 35'	6'	+1.9'	+0'	185'	5134	sta. cont. 600' W

82KNW030

20' AN plan

W sunny
hotTRUE FISSURE

19-8-57

6N

2

Sta	FS.	BS	H.I	RI	V.A	H.D	ΔE_{in}	Final ΔE	H.D.	day pt.	Comments
$\Delta 1$	015		4'	4.85 hh	+20°13'	5	+312'	+311'	850'	549 ¹ / ₈	slab under into down from the down
5123.2)	016(h)		5	2.4 wh	+1°40'	4	+7	+7	237	5121	had rods cut & blasted away
	017.			8.25 wh	+18°49'	5	+250	+249	742	5133	into, big and
	018.			2.7 hh	+14°16'	5.5	+128'	+126 ¹ / ₂	505	5310 ¹ / ₂	bottom of slab face of rod, containing the
	019			3.55 hh	+19°39'	5	+225	+224	631	5408	top of bolt 5' face.
	020			3 hh	+14°44'	3	+147 ¹ / ₂	148 ¹ / ₂	560	5332 ¹ / ₂	"on contact"
	021			3.42 hh	14°55'	6'	+170	168	640	5352	in weeds, on nose giving a good quality of floor
	022			3.6 hh	15°57'	6	+189	187	678	5371	on weeds
	023										

82KNW030

Petes shots

weulhen.
warrn, dallisch.

TRUE FISSURE

20-8-57

GN 3

-same general area as yesterday

Sta	FS	B.S.	H.I.	RI	V.A.	H.P.	D. elev (calc)	Final DE	H.D.	elev of point	Comments
Δ2		Δ1.	3'	'8 wh.	+10°33'	3.4	+14.5	+14.1	779'	5169.7	20' 20' 20' 20'
(5168.5)	016		"	2.6 hh.	+9°31'	2	+85'	+86'	505'	5254.5	muscle number
	017			6.3 wh	+13°35'	6.7'	+144'	+140.3	599'	5302.8	still in weeds
	018			3.45 hh	+15°39'	7	+155'	+151'	640'	5319.5	higher, indistinct
→	Δ4			4.5 hh	+18°13'	5	+126.6'	244	810'	5450.5	in weeds 200' R. of pt/h. (10)
Δ5.	019		3½	.60 hh.	-10°54'	4.	-22.4	-22.6	145½'	5095.5	center of rd 200' below

82KNW030

w. sultry brooding.
TRUE FISSURE

20-8-57.

Blains data

GN4

Sta	F.S.	B.S.	H.I.	R.I.	V.A.	H.P.	Delta	Final Elev	H.D.	elev pt.	Comments
22 (5145.5)	TA)		3	3' 4h.	13°33'	10'	+35½	+128½	570'	539.7	mouth of hollow cut by ditch 35' 600.5-777.0
	Δ5.			2.8wh.	-10°42'	2.3'	-51.6	-50.9	271'	5117.6	on N edge of rd, up p.m.
Δ5 (5123.9)	Δ2	3½		14 hh.	+9°23'	3.6	+45.5	+45.4	271'		
	8(6)			35 hh.	-9°08'	3	-26.5	-26'	165'		by creek, small can 10' N, 10' down in on dump's E end (belongs to the Morgan crosscut (TS #4)
	9(5)			5.05 wh.	-26°47'	4.5	-200'	-201'	101'		
	1(9)			77 hh.	-29°30'	5.0	-132'	-133½	232'		10' N of 10' about on 150' upstream of 9(6).
	Δ2	3½		2.8wh.	+9°46'	5.4	+46.1	+44.2			- check shot on Sta 2. the Sta 2 → Sta 5 for a right hand way cut angle.
				5.6		3.5		say 45'			

STA	CHURN	HT	RT	BEAMAN	HA	HD	VH	Δ ELEV	ELEVATION	H' FEED	REMARKS
					August 30th 1957		TRUE	PICTURE			
45	Δ 2	4.0 ⁺	2.75 ⁺	+18	8.24 ⁻	265.7	+39.5 ⁺	+35.1	5752.7	3.4	ELEV. 5752.7 B.S.
	Δ 6	"	2.2	-18	5.0	213.0	-39.6	-38.6	5079.0	3.4	on inside of road halfway
	Δ 7	"	3.0	-7	7.5 ⁻	293.0	-21.0	-17.5 ⁻	5700.1	.7	
47	Δ 5	"	3.0	+7	7.8 ⁺	~	~	~	~	.7	B.S. agrees ✓ Elev 5700.1
	020	"	.9	+34	9.5 ⁺	78.1	+30.6	+25.1	5725.2	13.2	angling uphill west of table
	021	"	1.4	+34	8.7	121.5	+47.6	+42.9	5143.0	13.2	" " " "
	022	"	1.3	+45	8.6	96.2	+59.5	+53.9	5154.0	26	in woods directly uphill from table
	023	"	1.4	+45	3.0	140.6	+85.5	+86.5	5126.6	26	contour just starts to widen for road
46	Δ 5	"	2.2	+18	5.0	~	~	~	~	3.4	B.S. agrees elev 5079.0
	024	"	2.7	-6	5.6	263.0	-43.2	-41.6	5037.4	2.6	at corner of house corner
	Δ 8	"	5.1	-18	7.5	496.8	-91.8	-89.3	4989.7	3.4	
48	Δ 6	"	5.2	+18	7.6	~	~	~	~	3.4	B.S.
	025	"	1.1	-21	2.5 ⁺	105 ⁺	-23.1	-24.6	4965.1	4.6	Elev = 4965.1 inside of road at bend
	026	"	3.2	-18	5.4	309.1	-57.6	-56.2	4933.5	3.4	
	Δ 9	"	7.0	-18	5.5	3676.2	-12.6	-124.5	4865.2	3.4	outside of road at telephone pole

August 31, 1957

TRAIL PISCUE

Destination =
21°45'

GN6

STATION	SECTION	HI	RI	BENCHMARK	HD	HD	± Vh	Δ ELEV	ELEVATION	H ROAD	REMARKS
Δ1	Δ10	4.2	6.3	+30	9.2	567	-189.0	+188.0	5367.8	10	ELEV Δ1 = 5367.8 F.S.
Δ10	Δ1	4.3	6.2	-30	9.1	558	-186.0	~	~	10	B.S. ELEV Δ10 = 5367.8
Δ11	"	"	3.6	-16	9.0	352.6	-57.6	-57.9	5313.7	2.6	F.S.
Δ21	"	"	1.8	+21	10.0	171.5	+27.9	+32.1	5399.9	4.7	Very small ridge
Δ12	"	"	5.2	+33	9.6	456.0	+171.6	+166.0	5333.8	12.3	
Δ12	Δ18	"	5.2	-28	9.6	-	-	-	-	12.3	B.S. of trees ✓
Δ22	"	"	1.9	-5	9.0	189.0	-95	-142	5519.6	1.5	Good B.S. = 5533.8 Situated on down near edge of ridge with small bench mark
Δ24	"	"	2.8	-12	8.0	272.5	-33.6	-37.6	5496.2	1.6	Good B.S. = 5533.8 More to west side of small ridge
Δ30	"	"	1.2	-35	9.6	105.0	-42.0	-28.4	5505.4	11.2	First ridge dump at edge of road
Δ31	"	"	1.4	-24	8.7	106.0	-61.6	-60.0	5267.8	24	
Δ32	"	"	11.0	-30	6.5	90	-30.0	-34.7	5499.1	10	
Δ13	"	"	2.0	+16	8.0	389	+61.4	+60.3	5594.1	2.7	On top of ridge Elev Δ13 = 5552.4
Δ14	"	"	0.8	+33	9.4	70	+26.4	+21	5554.8	12.3	
Δ14 Sept. 12, 57	Δ33	4.0	0.4	+29	6.4	36.2	+11.6	+9.2	5564.0	9.4	on trail directly uphill from table
Δ34	"	"	0.65	+30	3.6	68.5	+19.5	+10.4	5574.7	10	working uphill from table
Δ35	"	"	1.6	+18	5.7	154.6	+28.8	+27.1	5581.9	3.4	

82KNW030

Sept 1st, 1957

TRUE DISTANCE

STA	SIGHT	HI	RT	BEAMAN	HP	HD	VH	AEIK	ELEVATION	LI' REAR	REMARKS
ΔB	Δ12	4.0	4.0	76	8	~	~	~	~	2.7	Elev. Δ12 = 5594.4 B.S. 09102 ✓
	036	"	1.8	+3	2.1	179.5	+5.4	+5.2	5599.4	.3	43rd way across road
	037	"	2.0	+12	5.0	196.8	+24	+23	5617.1	1.6	
	038	"	2.2	+6	4.8	215.1	+3.2	+14.0	5608.1	.6	
	039	"	2.5	+15	4.6	244.2	+37.5	+36.9	5631.0	2.3	
	040	"	1.9	+15	4.0	185.6	+28.5	+28.5	5622.6	2.3	outcrop to S.E. of table
	Δ15	"	2.5	+19	8.2	238.2	+47.5	+43.3	5641.4	4.7	
	041	"	1.5	+11	8.7	145.8	+25.5	+20.8	5614.9	2.8	
	Δ16	"	3.6	±0	9.2	360	±0	±0	5594.1	0	Across drain
Δ15	Δ13	"	2.5	-18	2.2	~	~	~	~	2.6	B.S. 09102 = 5594.4 Elev. Δ13 = 5594.4
	047	"	5.0	-4	4.0	498	-20	-7.4	5617.4	4	
	042	"	1.75	±0	3.9	175	±0	±0	5641.6	0	on top
	043	"	1.60	+2	3.8	159.7	+3.2	+3.4	5640.8	.2	in drain (10 ft to left)
	Δ18	"	2.4	+16	5.0	233.5	+3.8	+37.6	5678.8	2.7	
	044	"	1.4	+10	9.4	132.6	+14	+8.6	5650.0	1	
	045	"	1.2	±0	2.6	119.3	+7.2	+2.6	5644.0	.6	
Δ17	Δ15	"	5.0	-4	8.0	~	~	~	~	4	

B2K NW 030

SEPT. 14, 1917 TRIANGLE.

STA	SIGHT ON	HI	RT	REAMAN	H.D.	H.O.	K.H.C.	DIFFER.	ELEVATION	STARS	REMARKS
Δ17	046	41.0 ⁺	0.9	-15	9.5	9.8	-13.5 ⁺	-8	5609.4	2.3	ELEV 217 = 5617.4 in woods down hill to north.
	Δ19	"	2.4	-32	4.9	213.0	-76.8	-75.8	5541.6	11.7	
	047	"	1.0	-36	8.5	74.7	-36.0	-31.5	5585.9	15.3	
Sept. 10/17 Δ19	Δ17	"	2.4	+32	3.0	~	~	~	~	11.7	B.S. agrees Elev 219 = 5522.10
	048	"	2.3 ^{1/2}	+24	5.0	215.7	+55.2	+54.2	5595.8	6.2	abt to right of drape
	049	"	1.4	+22	6.4	132.9	+30.8	+28.4	5570.0	5.1	behind brown dump
	050	"	1.1	+18	5.6	106.4	+10.8	+9.2	5550.8	3.5	
	051	"	0.7	+15	2.5	68.3	+10.5	+12	5553.6	2.4	
	052	"	0.8	-26	3.4	74.2	-20.8	-20.2	5521.4	7.2	end of dump
	053	"	0.6	+13	6.6	58.0	+10.8	+8.2	5549.8	3.3	
	054	"	1.2	+27	4.4	110.7	+32.4	+32	5573.6	7.8	
	055	"	1.4	+21	8.7	133.4	+29.4	+24.7	5566.3	4.7	
	056	"	1.0	-7	3.5	99.5	-7.0	-6.5	5555.1	-7	
	057	"	1.9	-17	4.0	184.5	-32.3	-32.3	5509.3	2.9	in weeds off end of water course

Sept 10/57 (Cont'd)

Sugar River

GN9

STATION	START OF	HT	RT	REMBRN	HP	HO	±VH	±AELEV.	ELEVATION	H Reen	REMARKS
Δ19	Δ20	±0	1.4	-1	2.6	140.0	-14	±0	5541.6	0.1	Elev Δ19 = 5541.6 E.S.
Δ20	Δ19	"	1.4	0	2.4	~	~	~	~	0	E.S. Elev Δ20 = 5541.6
058	"	0.35	+3	3.2	3.2	35.0	+1.05	+0.2	5571.8	.3	outcrop to left of abt (SE abt)
059	"	0.4	+24	3.4	3.4	84.4	+21.6	+22.2	5563.0	6.2	above abt
060	"	1.0	+24	3.5	3.5	93.8	+24	+24.5	5566.1	6.2	above to right of abt
061	"	2.3	-21	3.0	3.0	212.0	-62.1	-58.1	5483.5	7.8	dump of lower abt
062	"	22.0	-7	4.0	4.0	2184.6	-154.0	-158.0	5387.6	0.7	large hole in hill (Rembrn)
063	"	22.0	-7	4.0	4.0	2184.6	-154.0	-158.0	5387.6	0.7	containing a grey lens OFF SHEET
064	"	22.4	-3	4.0	4.0	2234.2	-67.2	-67.2	5474.4	0.3	dump above to right of gravel lens OFF SHEET
065	"	26.0	±0	3.0	3.0	2670	±0	±0	5541.6	0.0	above to left of obvious abt
066	"	26.0	±0	4.0	4.0	2600	±0	±0	5541.6	0.0	above to left of hole in hill
SEPT 12, 1957											
Δ16	Δ13	"	4.0	±0	8.5	100	±0	±0	55594.1	0.0	Elev Δ16 = 55594.1 E.S.
057	"	1.1	-23	4.5	4.5	103.8	-25.3	-28.0	5569.3	3.6	massed bank with some 24.0
058	"	1.1	+9	4.4	4.4	109	+9.9	+9.5	5603.6	0.9	
Δ21	"	1.1	+26	5.0	5.0	102.1	+28.4	+27.1	5621.2	7.2	

82KNW030

SEPT. 12, 1947 (cont'd)

GN 10

STATION	HORIZONTAL	RT	DEPTH	TEMP	SP. COND.	WIND	WAVE	SEA LEVEL	WIND DIRECTION	WAVE PERIOD	REMARKS
A21	A16	8.20	11	-25	8.4	-	-	-	-	-	B.S. 51100 ✓
	069	-	0.4	+11	3.5	84.2	+5.6	+5.8	5617.0	2	Elev 21 = 5621.2 all alt.
	070	-	1.5	+32	6.3	132.5	+4.8	+45.7	5666.9	11.7	Directly upwind from
	A22	-	2.0	+7	5.0	198.6	+1.4	+13.0	5634.2	7	FS
A22	A21	-	2.0	+7	5.0	-	-	-	-	7	B.S. 51100 ✓
	071	-	0.8	-21	9.4	75.2	-19.2	-13.8	5620.4	6	Elev 22 = 5624.0
	072	-	.4	-34	9.4	77.7	-21.6	-26.2	5608.13	13.7	
	073	-	1.6	-24	8.7	120.4	-3.8	-33.7	5600.5	6	
	A23	-	2.8	-9	8.4	277.5	-25.2	-20.8	5613.4	9	
A23	A22	6	2.8	+10	8.4	-	-	-	-	10	B.S.
	A23 1/2	-	-	-	-	-	-	-	-	-	REVERSE 145 - PICTURE TAKEN!
	074	-	0.2	+8	8.4	89.3	+7.2	+7.8	5621.2	3	Elev 23 = 5618.4
	075	-	0.8	-2	3.2	110.0	-1.8	± 0	5613.4	1.2	
	076	-	0.7	+6	3.3	69.6	+4.2	+4.9	5618.3	6	
	A24	-	1.4	+5	4.4	139.3	+7.0	+6.6	5606.8	5	
	077	-	1.3	+29	8.6	117.8	+39.7	+33.1	5646.5	9.4	
	078	-	0.8	-11	9.4	79.0	-8.8	-3.4	5610.0	1.2	

02KNW030

STATION	SECTION	HT	R ₂	BEAMAN	UD	4D	UD	ΔELEV	ELEVATION	U _{Beam}	Remarks
124	123	4.0	1.4	+5	4.4	~	~	~	~	1.5	B.S. 091025 ✓
	079	"	1.4	-4	8.8	139.5	-5.6	-0.8	5606.0	2	ENVD 200 = 5606.8
	080	"	1.3	+9	6.0	1126.4	+32.7	+36.7	5613.5	4	OFF SHEET
	081	"	1.0	+10	7.0	594.4	+6.0	+5.7	5613.8	1	OFF SHEET ^{Final} 9/24/11 6/10/12
	082	"	5.0	±0	5.3	500	±0	±0	5605.8	10.0	OFF SHEET 8/15/12 (checked)
	125	"	2.3	-2	1.2	225.4	-4.6	-0.4	5606.4	1.7	FS
125	124	"	2.3	+2	2.2	~	~	~	~		B.S. 091025 ✓
	083	"	1.3	-1	4.4	130.0	-1.3	-1.7	5604.7	1	ENVD 1.5 = 5605.2
	084	"	1.6	+5	8.8	159	+8.6	+3.2	5603.2	5	
	126	"	1.8	-3	0.9	179.5	-3.4	-1.5	5606.0	3	FS
126	125	"	1.8	+4	8.9	~	~	~	~	1.4	B.S. 091025 ✓
	085	"	1.0	-7	8.5	1.00	-7.0	-2.5	5603.5	7	ENVD 236 = 5603.0
	086	"	1.2	±0	8.6	120.1	±0	±0	5606.0	±0	
	087	"	2.4	+2	4.7	240	11.8	+4.1	5610.1	12	
	088	"	.8	-17	2.4	77.7	-13.6	-13.0	5603.0	2.9	

82KNW030

Elev. = Elev. Sta. + H. I. - H. Pt. + V

GN12

At	To	H.I.	R.I.	Vert. L.	H. Pt.	H	V	ΔE	Elevation	Remarks
$\Delta 17$	$\Delta 29$	3.8'	1.64'	0° 59'	6'	164'	+2.8'	+ .6'	5618.0'	$\frac{5}{6.69}$ Elev. $\Delta 17 = 5617.4'$
$\Delta 29$	$\Delta 17$	4.2'	1.64'	0°	4.8'	164'	0'	-.6'	5617.4'	$\frac{5}{6.69}$ Elev. $\Delta 29 = 5618'$
$\Delta 29$	089	4.2'	1.02'	17° 15'	9'	92'	+28.6'	+23.8'	5642.2'	$\frac{8}{9.02}$
$\Delta 29$	090	4.2'	.58'	25° 8'	6'	47'	+22.3'	+20.5'	5638.5'	$\frac{6}{6.58}$
$\Delta 29$	$\Delta 30$	4.2'	.71'	6° 23'	4'	70'	-7.9'	-7.7'	5610.3'	$\frac{3}{3.71}$ Elev. $\Delta 30 = 5610.3'$
$\Delta 30$	$\Delta 29$	4.1'	.71'	7° 47'	6'	70'	+9.6'	+7.7'	5618'	$\frac{6}{6.71}$
$\Delta 30$	092	4.1'	.87'	8° 30'	9'	85'	-12.7'	-17.6'	5593'	$\frac{7}{10.87}$
$\Delta 30$	093	4.1'	.84'	6° 34'	6'	83'	-9.6'	-11.5'	5599'	$\frac{6}{6.84}$
$\Delta 30$	$\Delta 31$	4.1'	1.92'	2° 44'	7'	191'	-9.2'	-12.1'	5598.2'	$\frac{8}{6.08}$
$\Delta 31$	$\Delta 30$	4.0'	1.93'	5° 10'	6'	191'	+17.4'	+15.4'	5599.2'	$\frac{7}{6.93}$ Elev. $\Delta 31 = 5599.9'$
$\Delta 31$	094	4.0'	1.86'	16° 34'	6'	165'	-49.0'	-51.0'	5544'	$\frac{7}{6.86}$
$\Delta 31$	$\Delta 30$	4.0'	1.95'	6° 4'	9'	192'	+20.5'	+15.5'	5599.2'	$\frac{8}{9.95}$
$\Delta 31$	$\Delta 32$	4.0'	1.42'	6° 58'	4'	140'	-17.1'	-17.1'	5592.8'	$\frac{5}{3.58}$
$\Delta 31$	095	4.0'	.56'	26° 33'	6'	45'	+22.3'	+21.3'	5616'	$\frac{6}{6.56}$
$\Delta 31$	096	4.0'	101'	25° 15'	7'	82'	+39'	+36'	5631'	$\frac{5}{6.01}$
$\Delta 31$	$\Delta 33$	4.0'	2.20'	26° 2'	5'	177'	+86.6'	+85.6'	5680.5'	$\frac{9}{3.80}$ Elev. $\Delta 33 = 5681.1'$
$\Delta 33$	$\Delta 31$	3.9'	2.11'	27° 37'	5'	168'	-85.8'	-86.9'	5593.6'	$\frac{6}{3.89}$

82KNW030

At To	H.I.	R.I.	Vert.	H. Pt.	H.	V.	ΔE	Elevation	Remarks
Δ33 097	3.9'	.87'	26°35'	9'	70'	-34.8'	-39.9'	5641'	$\frac{5}{8.82}$ Elev Δ33
Δ33 099	3.9'	1.00'	13°41'	9'	94'	+23.1'	+19'	5700'	$\frac{5}{8.50} = 5681.1'$
Δ33 Δ34	3.9'	2.07'	22°29'	5'	177'	+73.1'	+72'	5753.1'	$\frac{5}{8.07}$
Δ34 Δ33	3.3'	1.96'	20°41'	9'	173'	-64.9'	-70.6'	5682.5'	$\frac{5}{8.95}$ Elev Δ34 = 5752.4'
Δ34 0100	3.3'	1.16'	27°14'	9'	92'	-47.1'	-52.8'	5700'	$\frac{5}{8.96}$
Δ34 0101	3.3'	.83'	3°11'	9'	83'	+4.4'	-1.3'	5757'	$\frac{5}{8.89}$
Δ34 Δ35	3.3'	.73'	24°48'	6'	60'	+27.6'	+24.9'	5777.3'	$\frac{5}{8.73}$ Elev Δ35 = 5777.3'
Δ35 Δ35	4.0'	.67'	18°42'	9'	60'	-20.3'	-25.3'	5762.0'	$\frac{5}{8.67}$
Δ35 0102	4.0'	.65'	9°58'	4'	63'	-11.1'	-11.1'	5766'	$\frac{5}{8.65}$
Δ35 0103	4.0'	1.18'	8°	11.2'	118'	0'	-7.8'	5770'	$\frac{5}{8.68}$
Δ35 Δ36	4.0'	1.80'	24°8'	4'	150'	+67.3'	+67.3'	5844.8'	$\frac{5}{8.20}$ Elev Δ36 = 5844.8'
Δ36 Δ35	4.1'	1.73'	23°24'	7'	147'	-63.4'	-66.3'	5778.5'	$\frac{5}{8.73}$
Δ36 0104	4.1'	1.81'	3°43'	4'	180'	-11.7'	-11.6'	5833'	$\frac{5}{8.79}$
Δ36 0105	4.1'	1.38'	9°7'	6'	135'	+21.7'	+19.8'	5864'	$\frac{5}{8.38}$
Δ36 0106	4.1'	.98'	2°21'	6'	98'	+4.0'	+2.1'	5846'	$\frac{5}{8.98}$
Δ36 0107	4.1'	1.15'	19°27'	4'	105'	+37.6'	+37.1'	5881'	$\frac{5}{8.82}$
Δ36 0108	4.1'	1.60'	24°8'	4'	133'	+59.9'	+60'	5904'	$\frac{5}{8.60}$

AC	To	H.I.	R.I.	Vert. Ang.	H. Pl.	H.	V.	ΔE	Elevation	Remarks
Δ18	Δ15	3.8'	2.53'	9°35'	4'	244'	-41.7'	-41.9'	5636.9'	$\frac{1}{3.53}$ Elev Δ18 = 5683.3
Δ18	0109	3.8'	1.55'	6°32'	9'	153'	-17.6'	-22.8'	5660.5'	$\frac{8}{9.55}$
Δ18	0110	3.8'	1.12'	2°38'	9'	112'	+5.2'	+2.0'	5685'	$\frac{8}{6.89}$
Δ18	Δ37	3.8'	.78'	0°	10.4'	78'	0'	-6.6'	5676.7'	$\frac{3}{3.78}$ Elev Δ37 = 5676.3
Δ37	Δ18	3.8'	.78'	4°56'	3.5'	78'	+6.7'	+7.0'	5683.5'	$\frac{3}{3.78}$
Δ37	0111	3.8'	1.58'	2°3'	3'	158'	-5.7'	-4.9'	5672'	$\frac{2}{3.58}$
Δ37	0112	3.8'	1.92'	6°38'	3'	189'	-22.0'	-21.2'	5655'	$\frac{2}{3.92}$
Δ37	Δ38	3.8'	3.60'	4°4'	8'	358'	+25.5'	+21.3'	5697.8'	$\frac{1}{4.60}$
Δ37	0113	3.8'	1.40'	0°	2'	140'	0'	+1.8'	5678.5'	$\frac{2}{3.40}$
Δ37	0114	3.8'	2.40'	10°41'	5'	230'	+44.0'	+42.8'	5719'	$\frac{6}{3.60}$ Elev Δ38 = 5697.2
Δ38	Δ37	4.0'	3.59'	3°11'	5'	358'	-20.0'	-21.0'	5676.8'	$\frac{1}{3.41}$
Δ38	0115	4.0'	1.97'	10°41'	3'	190'	+36.0'	+37.6'	5735'	$\frac{2}{3.97}$
Δ38	0116	4.0'	2.42'	17°42'	2'	220'	+70.5'	+72.5'	5770'	$\frac{1}{3.42}$
Δ38	0117	4.0'	3.28'	14°10'	5'	308'	+78.0'	+79.6'	5777'	$\frac{2}{3.72}$
Δ38	0118	4.0'	1.89'	14°10'	6"	177'	+45.0'	+43.0'	5741'	$\frac{1}{3.89}$
Δ38	0119	4.0'	1.34'	1°58'	4'	134'	+4.6'	+4.6'	5702'	$\frac{5}{3.66}$
Δ38	0120	4.0'	1.21'	7°6'	4'	119'	-15.0'	-15.0'	5783'	$\frac{5}{3.79}$

82ENW030

At	To	H.I.	R.I.	Vert. Ang.	H. 1 st	H.	V.	ΔE	Elevation	Remarks
$\Delta 38$	0121	4.0'	1.70'	0°	4.8'	170'	0'	-5'	5697'	5.70 Elev $\Delta 38 = 5892$
$\Delta 38$	0122	4.0'	2.18'	0° 55'	5'	218'	+3.5'	+2.5'	5700'	5.18
$\Delta 38$	$\Delta 39$	4.0'	3.63'	4° 8'	8'	360'	-26.0'	-30.6'	5667.7'	5.23
$\Delta 38$	0123	4.0'	2.07'	17° 45'	5'	187'	+60.0'	+59.0'	5757'	5.43
$\Delta 38$	0124	4.0'	2.10'	3° 18'	2'	210'	+12.2'	+14.2'	5712'	5.10
$\Delta 38$	0125	4.0'	1.99'	5° 15'	9'	197'	-18.3'	-23.3'	5674'	5.99
^{Sept. 30} $\Delta 38$		3.5'	The Sun She is a shining & the clouds they are a coming!							
$\Delta 38$	0126	3.5'	2.82'	16° 51'	8'	258'	+78.0'	+73.5'	5771'	5.82
$\Delta 38$	0127	3.5'	3.02'	22° 5'	5'	259'	+105.5'	+104'	5802'	5.51
$\Delta 38$	0128	3.5'	4.70'	23° 22'	7'	395'	+171'	+167.5'	5865'	5.70
$\Delta 38$	0129	3.5'	5.43'	21° 25'	7'	461'	+184'	+180.5'	5878'	5.43
$\Delta 38$	0130	3.5'	5.36'	19° 26'	7'	475'	+166.5'	+163'	5861'	5.36
$\Delta 38$	0131	3.5'	4.63'	17° 12'	7'	421'	+130.5'	+127'	5825'	5.63
$\Delta 38$	0132	3.5'	1.50'	0°	5.3'	150'	0'	-18'	5696'	5.52
$\Delta 38$	0133	3.5'	1.44'	5° 34'	9'	143'	+14.1'	+8.5'	5706'	5.44
$\Delta 38$	0134	3.5'	3.02'	12° 8'	8'	289'	+62.5'	+58'	5756'	5.98
$\Delta 38$	0135	3.5'	3.64'	15° 10'	5'	339'	+92.0'	+90.5'	5788'	5.36

Ab To	H.I.	R.I.	Vert. L.	H. Pt.	H.	V.	ΔE	Elevation	Remarks.
$\Delta 38$ 0136	3.5'	3.65'	20° 7'	5'	321'	+117.5'	+116'	5814'	$\frac{3.35}{3.35}$ Elev $\Delta 38 = 5697.7'$
$\Delta 38$ 0137	3.5'	4.95'	17° 33'	7'	450'	+142.5'	+139'	5837'	$\frac{5.95}{5.95}$
$\Delta 38$ 0138	3.5'	4.10'	14° 1'	7'	384'	+96.5'	+93'	5791'	$\frac{5.10}{5.10}$
$\Delta 39$ $\Delta 38$	4.0'	3.66'	5° 27'	8'	360'	+34.5'	+30.5'	5698.2'	$\frac{6.66}{6.66}$ Elev $\Delta 39 = 5667.5'$
$\Delta 39$ 0139	4.0'	1.22'	2° 15'	3'	128'	+5.1'	+6.1'	5674'	$\frac{1.22}{3.28}$
$\Delta 39$ 0140	4.0'	1.73'	10° 23'	6'	166'	+30.8'	+28.8'	5696'	$\frac{5.73}{5.73}$
$\Delta 39$ 0141	4.0'	2.30'	13° 16'	8'	217'	+51.0'	+47'	5714.5'	$\frac{9.70}{9.70}$
$\Delta 39$ 0142	4.0'	2.41'	7° 29'	8'	238'	+31.1'	+23.1'	5695'	$\frac{2.59}{2.59}$
$\Delta 39$ 0143	4.0'	3.13'	5° 41'	5'	310'	+31'	+30'	5697.5'	$\frac{3.87}{3.87}$
Ser. 4 th	Der Wetter. Et ist Wunderbar.							Flies	Schlecht!!
$\Delta 10$ 0144	2.9'	.73'	3° 0'	9'	73'	+3.8'	-2.3'	5365.5'	$\frac{9.73}{9.73}$ Elev $\Delta 10 = 5367.8'$
$\Delta 10$ 0145	2.9'	1.27'	0°	0.8'	127'	0'	+2.1'	5370'	$\frac{2.13}{2.13}$
$\Delta 10$ 0146	2.9'	1.77'	13° 58"	9'	166'	+41.2'	+35.1'	5403'	$\frac{2.77}{2.77}$
$\Delta 10$ 0147	2.9'	1.57'	9° 46'	3'	153'	+26.1'	+26'	5394'	$\frac{2.57}{2.57}$
$\Delta 10$ 0148	2.9'	1.53'	6° 33'	1'	151'	+17.5'	+19.4'	5387'	$\frac{2.47}{2.47}$
$\Delta 10$ 0149	2.9'	1.78'	11° 48'	3'	170'	+35.7'	+35.6'	5403.4'	$\frac{2.78}{2.78}$
$\Delta 10$ 0150	2.9'	1.63'	7° 54'	3'	158'	+27.7'	+27.6'	5393.4'	$\frac{2.63}{2.63}$

At	To	H.I.	R.I.	Vert. L.	H. Pt.	H.	V.	ΔE	Elevation	Remarks
$\Delta 10$	0151	2.9'	1.65'	7° 0'	1'	163'	+20.0'	+21.9'	5390'	$\frac{2}{0.95}$ Elev. No = 53628
$\Delta 10$	0152	2.9'	1.50'	5° 28'	9'	148'	+14.3'	+8.2'	5376'	$\frac{2}{8.50}$
$\Delta 10$	0153	2.9'	1.61'	6° 36'	3'	159'	+18.5'	+18.4'	5386'	$\frac{2}{2.61}$
$\Delta 10$	0154	2.9'	1.83'	6° 35'	3'	180'	+20.9'	+20.8'	5388.6'	$\frac{2}{2.83}$
$\Delta 10$	0155	2.9'	1.96'	8° 31'	3'	192'	+28.9'	+28.8'	5396.6'	$\frac{2}{2.96}$
$\Delta 10$	0156	2.9'	1.87'	10° 58'	3'	180'	+34.8'	+34.7'	5402.5'	$\frac{2}{2.87}$
$\Delta 10$	0157	2.9'	2.36'	17° 22'	5'	215'	+67.0'	+64.9'	5433'	$\frac{2}{2.36}$
$\Delta 10$	0158	2.9'	2.02'	14° 41'	2'	190'	+49.8'	+50.7'	5418.5'	$\frac{2}{2.02}$
$\Delta 10$	0159	2.9'	2.50'	18° 2'	2'	226'	+73.5'	+74.4'	5442'	$\frac{2}{2.50}$
$\Delta 10$	0160	2.9'	2.65'	19° 48'	5'	235'	+84.4'	+82.3'	5450'	$\frac{2}{2.65}$
$\Delta 10$	0161	2.9'	3.02'	20° 33'	6'	265'	+99.0'	+95.9'	5464'	$\frac{2}{3.02}$
$\Delta 10$	0162	2.9'	3.17'	19° 20'	8'	270'	+98.5'	+93.4'	5461'	$\frac{2}{3.17}$
$\Delta 10$	0163	2.9'	2.78'	18° 11'	8'	247'	+81.0'	+75.9'	5444'	$\frac{2}{2.78}$
$\Delta 10$	0164	2.9'	2.62'	15° 42'	8'	243'	+68.6'	+63.5'	5431'	$\frac{2}{2.62}$
$\Delta 10$	0165	2.9'	2.90'	15° 57'	8'	269'	+76.3'	+71.2'	5439'	$\frac{2}{2.90}$
$\Delta 10$	0166	2.9'	3.42'	17° 38'	8'	311'	+99.1'	+94.0'	5462'	$\frac{2}{3.42}$
$\Delta 10$	0167	2.9'	3.89'	17° 53'	8'	351'	+103.1'	+98.0'	5466'	$\frac{2}{3.89}$

At	To	H.I.	R.I.	Vert. A.	H.P.A.	H.	V.	ΔE	Elevation	Remarks
Δ10	0168	2.9'	4.37'	15°14'	6'	404'	+110.1'	+107.0'	5475'	$\frac{9}{3.63}$ Elev. No = 5367.8
Δ10	0169	2.9'	4.19'	20°26'	7'	368'	+137.1'	+133.0'	5501'	$\frac{5}{4.17}$
Δ10	0170	2.9'	5.32'	21°14'	7'	462'	+178.5'	+174.4'	5542'	$\frac{4}{3.32}$
Δ10	0171	2.9'	3.30'	18°59'	5'	294'	+101.8'	+99.7'	5467.5'	$\frac{2}{3.20}$
Δ10	0172	2.9'	3.80'	21°52'	8'	328'	+131.1'	+126.0'	5494'	$\frac{10}{6.20}$
Δ10	0173	2.9'	3.34'	20°56'	5'	293'	+111.1'	+109.0'	5477'	$\frac{2}{3.66}$
Δ10	0174	2.9'	2.64'	19°55'	5'	234'	+84.8'	+82.7'	5450.5'	$\frac{6}{6.36}$
Δ10	0175	2.9'	2.35'	19°31'	8'	209'	+72.6'	+67.5'	5435'	$\frac{7}{4.35}$
Δ10	0176	2.9'	2.22'	16°0'	5'	206'	+59.0'	+56.9'	5425'	$\frac{6}{3.78}$
Sept 5 th										
Δ10	0177	3.0'	1.59'	2°22'	3'	159'	-6.6'	-6.6'	5361'	$\frac{2}{3.54}$
Δ10	0178	3.0'	1.93'	0°	3.1'	193'	0'	-1'	5368'	$\frac{2}{4.93}$
Δ10	0179	3.0'	1.94'	5°57'	4'	192'	-20.1'	-21.1'	5347'	$\frac{5}{3.24}$
Δ10	0180	3.0'	1.20'	9°43'	3'	116'	-20.0'	-20.0'	5348'	$\frac{2}{6.20}$
Δ10	0181	3.0'	.45'	8°52'	9'	44'	-6.9'	-12.9'	5355'	$\frac{9}{4.45}$
Δ10	Δ40	3.0'	1.87'	21°33'	9'	162'	+63.5'	+69.5'	5298.3'	$\frac{8}{4.87}$
Δ10	0182	3.0'	2.91'	11°34'	5'	280'	-57.3'	-59.3'	5308.5'	$\frac{1}{3.09}$

BRKUNW020

At	To	H.I.	I.T.	Vert.	R.P.	H.	V.	ΔE	Elevation	Remarks
$\Delta 10$	0183	3.0'	3.23'	2° 17'	5'	322'	-12.9'	-14.9'	5353'	$\frac{3}{8.28}$ Elev. A18 = 5367.8'
$\Delta 10$	0184	3.0'	2.38'	1° 14'	2'	238'	+5.1'	+6.1'	5374'	$\frac{1}{3.32}$
$\Delta 10$	0185	3.0'	2.71'	1° 38'	5'	271'	+7.8'	+5.8'	5373.6'	$\frac{6}{3.29}$
$\Delta 10$	0186	3.0'	3.03	4° 0'	6'	301'	+21.1'	+18.1'	5386'	$\frac{7}{3.97}$
$\Delta 10$	0187	3.0'	4.22	1° 19'	4'	422'	-9.8'	-10.8'	5357'	$\frac{2}{6.22}$
$\Delta 10$	0188	3.0'	A.60	0°	3.8'	460'	0'	-.8'	5367'	$\frac{5}{4.60}$
$\Delta 10$	01	3.0'	8.29	1° 23'	5'	827'	-20.1'	-22.1'	5345.7'	$\frac{1}{9.30}$
$\Delta 10$	0189	3.0'	.47'	20° 1'	6'	41'	+15.2'	+12.2'	5380'	$\frac{6}{6.27}$
$\Delta 10$	0190	3.0'	1.49'	8° 56'	9'	146'	-22.9'	-28.9'	5339'	$\frac{1}{9.49}$
$\Delta 10$	0191	3.0'	1.65'	11° 44'	3'	158'	+32.8'	+32.8'	5400.6'	$\frac{2}{3.65}$
$\Delta 10$	0192	3.0'	2.48'	6° 28'	5'	245'	+27.8'	+25.8'	5393.6'	$\frac{2}{3.52}$
$\Delta 10$	0193	3.0'	2.48'	10° 27'	5'	240'	+44.1'	+42.1'	5410'	$\frac{6}{3.52}$
$\Delta 10$	0194	3.0'	2.80'	12° 1'	5'	268'	+57.0'	+55.0'	5423'	$\frac{6}{3.20}$
$\Delta 10$	0195	3.0'	2.70	5° 53'	5'	267'	+27.5'	+25.5'	5393'	$\frac{4}{6.71}$
$\Delta 10$	0196	3.0'	3.37	7° 7'	5'	331'	+41.5'	+39.5'	5407'	$\frac{1}{6.07}$
$\Delta 10$	0197	3.0'	4.86	7° 26'	7'	478'	+62.3'	+58.3'	5426'	$\frac{5}{9.86}$
$\Delta 10$	0198	3.0'	4.74	9° 30'	4'	460'	+77.2	+76.2	5444'	$\frac{2}{6.74}$

AI	To	H.I.	R.I.	Vert. L	H. Pt	A	V	ΔE	Elevation	Remarks
Δ10	0217	3.0'	5.04'	12°13'	7'	472'	+104.5	+100.5	5468'	4/9.00 Elev. Δ17 = 5342.8
Δ10	0218	3.0'	4.00'	12°11'	7'	381'	+82.0'	+78.0'	5446'	5/9.00
Δ10	0201	3.0'	4.50'	13°17'	6'	426'	+100.0'	+97.0'	5465'	8/3.50
Δ10	0202	3.0'	3.50	14°50'	8'	328'	+87.0'	+82.0'	5450'	6/5.50
Δ10	0203	3.0'	4.00	14°29'	7'	374'	+96.5'	+92.5'	5460'	5/9.00
Δ10	0204	3.0'	4.40	18°25'	7'	395'	+131.5	+127.5	5495'	5/9.00 Elev. Δ40 = 5297.2
Δ40	Δ10	3.8'	2.00	24°11'	7'	166'	+74.9'	+71.7'	5370.0	8/6.00
Δ40	0205	3.8'	.90'	19°35'	3"	80'	+28.4	+29.2'	5326.4	3/1.70
Δ40	0206	3.8'	.50	8°22'	10'	49'	-7.2'	-13.4'	5284	9/9.50
Δ40	0207	3.8'	1.04'	9°47'	3"	101'	-17.5'	-16.7'	5280.5	2/3.00
Δ40	0208	3.8'	2.36'	23°43'	5'	198'	-86.7'	-87.9'	5209'	6/3.64 + #87.50 6' above bench
Δ40	0209	3.8'	2.02'	19°56'	5'	179'	-64.9'	-66.1'	5231'	1/3.98
Sept. 6	h					The significance of 2 more days.				PREVIOUS Elev. Δ11 = 5314
Δ11	01	3.2'	9.50	2°23'	5'	947'	+39.4'	+37.6'	5351.6	10/1.05 UPPER BENCH FOR SKI 12/17/80
Δ11	0211	3.2'	.76'	10°15'	9'	93'	-16.9'	-22.7'	5302'	9/9.06 Bench in trail
Δ11	0212	3.2'	1.66'	14°46'	7'	155'	-40.9'	-44.7'	5280'	9/8.34 Elev. Δ11 = 5324.9
Δ11	0213	3.2'	1.48	19°22'	7'	133'	-46.6'	-50.4'	5274.5	8/8.1

At	To	H.T.	R.I.	Vert.	H. Pt.	H.	V.	DE	Elevation	Remarks
Δ11	0214	3.2'	1.82'	13°57'	9'	171'	-42.5'	-48.3	5276.6'	8.82 Elev. All = 5324'
Δ11	0215	3.2'	1.12'	3°54'	7'	112'	-7.6'	-11.4	5313.5'	8.88
Δ11	0216	3.2'	1.78'	5°22'	9'	176'	+16.7'	+10.9'	5336'	8.98
Δ11	0217	3.2'	2.40'	9°18'	8'	243'	+38.0'	+33.2'	5358'	9.06
Δ11	0218	3.2'	3.17'	10°52'	8'	305'	+58.4'	+53.6'	5378.5'	9.13
Δ11	0219	3.2'	4.26'	11°22'	6'	409'	+82.0'	+79.2'	5404'	9.23
Δ11	0220	3.2'	1.74'	10°7'	11'	168'	+30.0'	+22.2'	5347'	9.28
Δ11	0221	3.2'	3.30'	10°21'	13'	319'	+58.0'	+48.2'	5373'	9.36
Δ11	0222	3.2'	8.50'	2°59'	5'	846'	+44.0'	+42.2'	5367'	9.50 Shots near UN. BL. BELL
Δ11	0223	3.2'	9.86'	4°39'	3'	980'	+79.5'	+79.7'	5404.6'	9.57
Δ11	0224	3.2'	12.00'	8°57'	5'	1168'	+184.4'	+182.6'	5507.5'	9.60 ↓
Δ11	0225	3.2'	10.82'	9°17'	7'	1038'	+154.6'	+150.8'	5476'	9.61
Δ11	0226	3.2'	11.80'	10°56'	6'	1138'	+219'	+216.2'	5541'	9.68
Δ11	0227	3.2'	12.90'	12°36'	6'	1230'	+273.4'	+270.6'	5595.5'	9.75
Δ11	0228	3.2'	13.88'	13°28'	6'	1308'	+312'	+309.2'	5634'	9.81
Δ11	0229	3.2'	12.88'	10°55'	6'	1236'	+237'	+234.2'	5559'	9.88
Δ11	0230	3.2'	13.90'	7°46'	6'	1360'	+188'	+185.2'	5510'	9.95

B2KNW030

At	TO	H.I.	R.I	Vert. L.	H. Pt.	H.	V.	ΔE	Elevation	Remarks
Δ11	0231	3.2'	14.08	8°54'	5'	1364'	+214'	+202.2'	5537'	$\frac{2}{3.00}$ Elev. Δ11 = 5324.0
Δ11	0232	3.2'	16.86	4°39'	8'	1072'	+87.6'	+82.8'	5408'	$\frac{2}{3.70}$
Sunday Sept. 7 th . Concerned with train tickets!										Elev. = 5360.0
Δ1	01	3.1'	7.34	15°34'	6'	699'	+167'	+164.4'	5348.2	$\frac{2}{3.30}$ PREVIOUS ELEV. Δ1 = 5183.8
Δ1	0233	3.4'	4.17	9°15'	6'	406'	+66.2'	+63.6'	5260'	$\frac{2}{3.03}$ Elev. Δ1 = 5196.1
Δ1	ΔA1	3.2'	2.20	6°34'	8'	217'	+25.1'	+20.5'	5216.6'	$\frac{2}{3.00}$ Elev. used from 0233.00
Δ1	0234	3.4'	1.09	15°54'	3'	181'	+28.8'	+29.2'	5225'	$\frac{2}{3.59}$
Δ1	0235	3.4'	1.83	2°50'	9'	182'	-9.1'	-14.7'	5181'	$\frac{2}{3.83}$
Δ1	0236	3.4'	1.42	0°	2.2'	142'	0'	+1.2'	5197'	$\frac{2}{3.02}$
Δ1	0237	3.4'	1.82	0°	4.1'	182'	0'	-.7'	5195'	$\frac{2}{3.82}$
Δ1	Δ2	3.4'	.80	7°15'	9'	79'	-10.1'	-15.7'	5180.4'	$\frac{2}{3.80}$ ORIENTATION CHECKS
ΔA1	Δ1	4.0'	2.18	4°14'	8'	216'	-16.2'	-20.2'	5196.4'	$\frac{2}{3.17}$
ΔA1	0238	4.0'	2.34	9°14'	5'	228'	+36.1'	+35.1'	5131'	$\frac{2}{3.66}$ Elev. ΔA1 = 5216.5
ΔA1	0239	4.0'	1.50	3°6'	3'	150'	+8.2'	+9.2'	5226'	$\frac{2}{3.50}$
ΔA1	0240	4.0'	3.35	5°56'	8'	330'	+34.4'	+30.4'	5247'	$\frac{2}{3.35}$
ΔA1	0241	4.0'	3.70	17°10'	7'	338'	+104.0'	+106.0'	5317.5'	$\frac{2}{3.30}$
ΔA1	0242	4.0'	4.59	19°25'	6'	408'	+143.4'	+141.4'	5359'	$\frac{2}{3.51}$

82KNW080

AI	To	H.I.	R.I.	Vert. L.	H. Py.	H.	V.	ΔE	Elevation	Remarks
$\Delta 5$	$\Delta 2$	4.0'	2.80'	9°50'	3'	272'	+47.1'	+48.1	5165.7'	R.I.S Elev $\Delta 2 = 5180.2$
$\Delta 5$	0243	4.0'	2.00	18°31'	3'	180'	-60.3'	-59.3	5073'	PREVIOUS Elev $\Delta 5 = 5112.6$
$\Delta 5$	$\Delta 42$	4.0'	4.10'	26°58'	6'	327'	-165'	-167'	4965.1'	
$\Delta 42$	$\Delta 5$	3.8'	2.26	27°46'	7'	343'	+174'	+170.2	5135.3	R.I.S fused in 0243 in Elev $\Delta 5 = 5132.1$
$\Delta 42$	0244	3.8'	2.24	22°50'	10'	191'	+80'	+73.8'	5038'	
$\Delta 42$	0245	3.8'	2.33	16°54'	2'	214'	+64.9'	+65.7'	5030'	Elev $\Delta 42 = 4966.5$
$\Delta 42$	0246	3.8'	2.50'	16°4'	5'	230'	+66.9'	+65.7'	5030'	
$\Delta 42$	0247	3.8'	1.11'	1°55'	4'	111'	+3.7'	+3.5'	4968'	Partial M.K.C.
$\Delta 42$	0248	3.8'	1.21'	0°	2.7'	121'	0'	+1.1'	4965.6'	
$\Delta 42$	0249	3.8'	1.23	0°	3.6'	123'	0'	+1.2'	4965'	

BZKNW030

Stn	Tr	HT	HT	Vert. A	HT	S	HT	ΔE	Elevation	Remarks
Δ5	Δ2	4.0'	2.80'	9°50'	3'	27'	+42.1'	+48.1'	5165.7'	1/3.80 R.K.5 Elev. Δ2 = 5180.2
Δ5	Δ243	4.0'	2.00'	18°31'	3'	180'	-60.3'	-59.3'	5073'	2/4.00 PRT11045 Elev Δ5 = 5112.6
Δ5	Δ42	4.0'	4.10'	26°58'	6'	321'	-165'	-167'	4965.1'	3/4.00
Δ42	Δ5	3.8'	Δ26	27°46'	7'	342'	+174'	+172.2'	5135.3'	4/3.80 R.A.5 Fused in. Q243 in
Δ42	Q243	3.8'	2.24'	22°50'	10'	191'	+80'	+73.8'	5038'	5/3.80 Elev Δ5 = 5132.1'
Δ42	Q245	3.8'	2.33'	16°54'	2'	214'	+64.9'	+65.7'	5030'	6/3.80 Elev Δ42 = 4966.5
Δ42	Q246	3.8'	2.50'	16°4'	5'	230'	+66.9'	+65.7'	5030'	7/3.80
Δ42	Q247	3.8'	1.11'	1°55'	4'	111'	+2.7'	+3.5'	4965'	8/3.80 Part in c.c.
Δ42	Q248	3.8'	1.21'	0°	2.7'	121'	0'	+1.1'	4965.6'	9/3.80
Δ42	Q249	3.8'	1.23'	0°	3.6'	123'	0'	+1.2'	4965'	10/3.80

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